

**Wireless RF, IF
and Transmitter
Device Data**

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FOREWORD

This publication includes technical information for the several product families that comprise the Motorola portfolio of Wireless RF, IF and Transmitter products. The product families include bipolar, LDMOS, MOSFET RF Power, and gallium arsenide chip technologies in a variety of ceramic and plastic surface mount packages. Discrete components, hybrid modules, and integrated circuits provide different levels of complexity in an effort to provide solutions for our customers' needs.


All devices are in alphanumeric order in the *Device Index* of this book. Just turn to the appropriate page for technical details of the known device. Complete device specifications are provided in the form of *Data Sheets* which are categorized by product type into six chapters for easy reference. *Selector Guides* by product family are provided at the beginning of the book as well as in the beginning of each chapter to enable quick comparisons of performance characteristics and to aid

you in identifying devices that meet your functional performance requirements of frequency, output power, gain, or other parameters.

Chapters on Tape and Reel Options, Packaging Information, Applications and Product Literature include additional information to aid you in the design process.

Applications assistance is only a phone call away — call the nearest Semiconductor Sales office or 1-800-521-6274. Please refer to our section on *On-line Access to Wireless Semiconductor Data* so that you will always have easy access to the most current information available on Motorola's Wireless RF, IF and Transmitter product portfolio.

The information in this book has been carefully checked and is believed to be accurate; however, no responsibility is assumed for inaccuracies.

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ABOUT THIS REVISION

This edition of the Wireless RF, IF and Transmitter Device Data Book encompasses a considerable number of changes that have occurred since our last printing. Some devices have been removed from this book due to package changes or new technology replacements and many new devices have been added.

Application Notes, Engineering Bulletins and Article Reprints of special interest to designers of RF and IF equipment are available on the Motorola Semiconductor Product Sector Web site or are available through the Motorola Literature Distribution Center. Phone and fax numbers for ordering literature are listed on the back cover of this book and in our Accessing Data On-line section. See Chapter Ten for a complete listing of Application Literature.

For Cross Reference information on Motorola replacement devices, please consult your local Distributor or Motorola Sales Office. See Chapter Eleven in this data book for a complete listing of Motorola Distributor and Worldwide Sales Offices.

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SPS, Technical Information Center
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Tokyo 106-8573 Japan
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Motorola Semiconductors H.K. Ltd.
Silicon Harbour Centre
2 Dai King Street, Tai Po Industrial Estate
Tai Po, N.T., Hong Kong
Phone: 852-26668334

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Chapter One

Wireless RF, IF and Transmitter Selector Guide

While Motorola is a worldwide leader in semiconductor products, there is not a category in which the selection is more diverse, or more complete, than in products designed for RF system applications. From MOS, bipolar power and signal transistors to integrated circuits, Motorola's RF components cover the entire spectrum from HF to microwave to personal communications. Yet, product expansion continues — not only to keep pace with the progressive needs of the industry, but to better serve the needs of designers for a reliable and comprehensive source of supply.

How to Use This Selector Guide

The RF Monolithic Integrated Circuits and the RF/IF Integrated Circuits products in this guide are divided into three major functional categories: RF Front End ICs, RF/IF Subsystem ICs and Frequency Synthesis. Each of these categories is further subdivided based on circuit functionality. This structure differentiates highly integrated subsystem ICs from fundamental circuit building blocks and discrete transistors.

The Power MOSFETs, Power GaAs Transistors, Power Bipolar Transistors, Power Amplifier Modules and CATV Distribution Amplifiers are FIRST divided into major categories by power level. SECOND, within each category parts are listed by frequency band. THIRD, within a frequency band, transistors are further grouped by operating voltage and, finally, output power.

To Replace Devices in an Existing Design

Call your local Motorola Sales Office or Distributor to determine Motorola's closest replacement device.

Applications Assistance

Applications assistance is only a phone call away — call the nearest Semiconductor Sales office or 1-800-521-6274.

Access Data On-Line!

Use the Motorola SPS Internet to access Motorola Semiconductor Product data at <http://www.motorola.com/semiconductors> or <http://www.motorola.com/semiconductors/rf/>. The SPS Internet provides you with instant access to data sheets, selector guide information, package outlines, on-line technical support and much more.

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Chapter One

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RF Front End ICs

Motorola's RF Front End integrated circuit devices provide an integrated solution for the personal communications market. These devices are available in plastic SOT-143, SOT-343, TSSOP-16, TSSOP-16EP, Micro-8, TSSOP-20EP, or BCC32++ packages.

Evaluation Boards

Evaluation boards are available for RF Front End Integrated Circuits. For a complete list of currently available boards and ones in development for newly introduced product, please contact your local Motorola Distributor or Sales Office.

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RF Front End ICs

RFICs

Upconverters/Exciters

Device	RF Freq. Range MHz	Supply Volt. Range Vdc	Supply Current mA (Typ)	Standby Current mA (Typ)	Conv. Gain dB (Typ)	Output IP3 dBm (Typ)	Case No./ Package	System Applicability
MRFIC0954(18b)	800 to 1000	2.7 to 5.0	65	5.0	31	28	948M/ TSSOP-20EP	CDMA, TDMA, ISM
MRFIC1813(18b)	1700 to 2000	2.7 to 4.5	25	0.1	15	11	948C/ TSSOP-16	DCS1800, PCS
MRFIC1854A(18b)	1700 to 2000	2.7 to 5.0	70	5.0	31	23	948M/ TSSOP-20EP	CDMA, TDMA, PCS
MRFIC1884(46a)	800 to 1000	2.7 to 3.2	60	5.0	32	28	1261A/ BCC32++	CDMA, TDMA, ISM, PCS
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Power Amplifiers

Device	Freq. Range MHz	Supply Volt. Range Vdc	Saturated Pout dBm (Typ)	PAE % (Typ)	Gain Pout/Pin dB (Typ)	Case No./ Package	System Applicability
MRFIC0919(18b)	800 to 1000	3.0 to 5.5	35.3	48	32.3	948L/ TSSOP-16EP	GSM
MRFIC1819(18b)	1700 to 2000	3.0 to 5.0	33	40	27	948L/ TSSOP-16EP	DCS1800, PCS
MRFIC1856(18b)	800 to 1000	3.0 to 5.6	32	50	32	948M/ TSSOP-20EP	TDMA, CDMA, AMPS
	1700 to 2000		30	35	30		TDMA, CDMA, PCS
MRFIC1859(18b)	800 to 1000	2.8 to 5.5	36.2	53	33.2	873E/ TQFP-32EP	GSM
	1700 to 2000		34	43	29		DCS1800, PCS
MRFIC1869(46a)★	800 to 1000	2.7 to 5.5	35.8	55	35.8	MLF-32	GSM900
	1700 to 2000		34	45	32		DCS1800, PCS

(18)Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units; f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

(46)To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Building Blocks

Amplifiers

Device	RF Freq. Range MHz	Supply Volt. Range Vdc	Supply Current mA (Typ)	Standby Current μ A (Typ)	Small Signal Gain dB (Typ)	Output IP3 dBm (Typ)	NF dB (Typ)	Case No./ Package	System Applicability
MBC13706 ^(46a) ★	800 to 1000	2.7 to 3.6	10	200	26	6.0	3.0	846A/ Micro-8	GSM, ISM
MRFIC0916 ^(18c)	100 to 2500	2.7 to 5.0	4.7	–	18.5	11	1.9	318A/ SOT-143	ISM, PCS, Cellular
MRFIC0930DM ^(18b)	800 to 1000	2.7 to 4.5	8.5	20	19	10	1.7	846A/ Micro-8	GSM, AMPS, ISM
MRFIC1808DM ^(18b)	1700 to 2100	2.7 to 4.5	5.0	8.0	18	13	1.6	846A/ Micro-8	DCS1800, PCS

Low Power Transistors

Device	Gain – Bandwidth		NFmin @ f		Gain @ f		Maximum Ratings		Case No./ Package
	f_t Typ GHz	I_C mA	Typ dB	GHz	Typ dB	GHz	V(BR) CEO Volts	I_C mA	
MBC13900 ^(46a) ★	15	20	1.0	1.0	17	1.0	7.0	20	318M/ SOT-343
			1.3	2.0	14	2.0			
MBC13901 ^(46a) ★	15	20	1.0	1.0	17	1.0	7.0	20	318M/ SOT-343
			1.3	2.0	14	2.0			

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units;

f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Front End Integrated Circuit Packages



CASE 318A
(SOT-143)



CASE 318M
(SOT-343)



CASE 846A
(Micro-8)



CASE 873E
(TOFP-32EP)



CASE 948C
(TSSOP-16)



CASE 948L
(TSSOP-16EP)



CASE 948M
(TSSOP-20EP)



CASE 1261A
(BCC32++)

RF/IF Subsystems

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RF/IF Subsystems

Cordless Phone Subsystem ICs

Device	V _{CC}	I _{CC} (Typ)	Dual Conversion Receiver	Universal Dual PLL	Compa ⁿ d and Audio Interface	CVSD Compatible	Low Battery Detect	Notes	Suffix/ Case No.
MC13110A	2.7 to 5.5 V	Active Mode 8.5 mA Inactive Mode 15 μA	✓	✓	✓	–	✓	CT-0	FB/848B FTA/932
MC13111A	2.7 to 5.5 V	Active Mode 8.5 mA Inactive Mode 15 μA	✓	✓	✓	–	✓	CT-0	FB/848B, FTA/932
MC13145	2.7 to 6.5 V	Active Mode 27 mA Inactive Mode 10 μA	✓	–	–	✓	–	Receiver with coilless demod CT-900	FTA/932
MC13146	2.7 to 6.5 V	Active Mode 18 mA Inactive Mode 10 μA	–	–	–	✓	–	Transmitter with VCO CT-900	FTA/977

Tranceivers

Device	V _{CC}	I _{CC}	GSM Receiver	TDMA/iDEN Receiver	Fractional-N PLL	Direct Launch GSM Transmitter	System Applicability	Case No./ Pkg Type
MC13760(46a)★	2.65 to 2.9 4.78 to 5.22 (Charge Pumps)	Transmit 20 mA Receive 30 mA	✓	✓	✓	✓	GSM/DCS, TDMA, iDEN, AMPS	1285/ BGA-104

(46)To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

Miscellaneous Functions

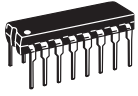
ADCs/DACs

Device	Function	I/O Format	Resolution	Number of Analog Channels	On-Chip Oscillator	Other Features	Suffix/ Case No.
MC144110	DAC	Serial	6 Bits	6	–	Emitter-Follower Outputs	DW/751D
MC144111				4			DW/751G

Encoders/Decoders

Device	Function	Number of Address Lines	Maximum Number of Address Codes	Number of Data Bits	Operation	Suffix/ Case No.
MC145026	Encoder	Depends on Decoder	Depends on Decoder	Depends on Decoder	Simplex	P/648, D/751B
MC145027	Decoder	5	243	4	Simplex	P/648, DW/751G
MC145028		9	19,683	0	Simplex	

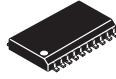
RF/IF Subsystems Packages



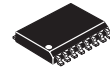
CASE 648
P SUFFIX
(DIP-16)



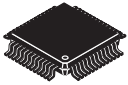
CASE 751B
D SUFFIX
(SO-16)



CASE 751D
DW SUFFIX
(SO-20L)



CASE 751G
DW SUFFIX
(SO-16W)



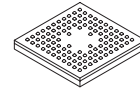
CASE 848B
FB SUFFIX
(QFP-52)



CASE 932
FTA SUFFIX
(LQFP-48)



CASE 977
FTA SUFFIX
(LQFP-24)



CASE 1285
(BGA-104)

Frequency Synthesis

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Frequency Synthesis

Single PLL Synthesizers

Maximum Frequency (MHz)	Supply Voltage (V)	Nominal Supply Current (mA)	Features	Device	Suffix/Case
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Parallel Interface	MC145151-2	DW/751F
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Parallel Interface, Uses External Dual-Modulus Prescaler	MC145152-2	DW/751F
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Serial Interface	MC145157-2	DW/751G
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Serial Interface, Uses External Dual-Modulus Prescaler	MC145158-2	DW/751G
100 @ 3.0 V 185 @ 4.5 V	2.7 to 5.5	2 @ 3 V 6 @ 5 V	Serial Interface, Auxiliary Reference Divider, Evaluation Kit – MC145170EVK	MC145170-2	P/648, D/751B, DT/948C
1100	2.7 to 5.5	7 @ 5 V	Serial Interface, Standby, Auxiliary Reference Divider, Evaluation Kit – MC145193EVK	MC145193	F/751J, DT/948D
2000	2.7 to 5.5	4 @ 3 V	Serial Interface, Standby, Auxiliary Reference Device, Evaluation Kit – MC145202-1EVK	MC145202-1	F/751J, DT/948D
2500	2.7 to 5.5	9.5	Serial Interface	MC12210	D/751B, DT/948E
2800	4.5 to 5.5	3.5	Fixed Divider	MC12179	D/751

Dual PLL Synthesizers

Maximum Frequency (MHz)	Supply Voltage (V)	Nominal Supply Current (mA)	Phase Detector	Device	Suffix/Case
1100 both loops	2.7 to 5.5	12	Serial Interface, Standby, Evaluation Kit – MC145220EVK	MC145220	F/803C, DT/948D

PLL Building Blocks

Prescalers

Frequency (MHz)	Divide Ratios	Single or Dual Modulus	Supply Voltage (V)	Supply Current (mA)	Features	Device	Suffix/Case
1100	64/65, 128/129	Dual	2.7 to 5.5	2.0 max	Low Power	MC12052A	D/751
1100	10,20,40,80	Single	4.5 to 5.5	5.0 max		MC12080	D/751
1100	2, 4, 8	Single	2.7 to 5.5	4.5 max	Standby	MC12093	D/751
2000	64/65, 128/129	Dual	2.7 to 5.5	2.6 max	Low Power	MC12054A	D/751
2500	2, 4	Single	2.7 to 5.5	14 max	Standby	MC12095	D/751
2800	64, 128, 256	Single	4.5 to 5.5	11.5 max		MC12079	D/751

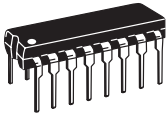
Voltage Control Oscillators

Frequency (MHz)	Supply Voltage (V)	Features	Device	Suffix/Case
1300	2.7 to 5.5	Two high drive open collector outputs (Q, QB), Adjustable output amplitude, Low drive output for prescaler	MC12149	D/751

Phase–Frequency Detectors

Frequency (MHz)	Supply Voltage (V)	Features	Device	Suffix/Case
800 (Typ)	4.75 to 5.5	MECL10H compatible	MCH12140	D/751
800 (Typ)	4.2 to 5.5	100K ECL compatible	MCK12140	D/751

Frequency Synthesis Packages



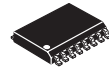
CASE 648
P SUFFIX
(DIP-16)



CASE 751
D SUFFIX
(SO-8)



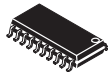
CASE 751B
D SUFFIX
(SO-16)



CASE 751G
DW SUFFIX
(SO-16W)



CASE 751J
F SUFFIX
(SO-20)



CASE 803C
F SUFFIX
(SO-20)



CASE 948C
DT SUFFIX
(TSSOP-16)



CASE 948D
DT SUFFIX
(TSSOP-20)



CASE 948E
DT SUFFIX
(TSSOP-20HS)

Motorola RF Discrete Transistors

Motorola offers the most extensive group of RF Discrete Transistors offered by any semiconductor manufacturer anywhere in the world today.

From Bipolar to FET, the user can choose from a variety of packages. They include plastic and ceramic that are microstrip circuit compatible or surface mountable. Many are designed for automated assembly equipment.

Major sub-headings are Power MOSFETs, Power GaAs and Bipolar Transistors.

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Motorola RF High Power Transistors

RF Power MOSFETs

Motorola RF Power MOSFETs are constructed using a planar process to enhance manufacturing repeatability. They are *N-channel field effect transistors* with an oxide insulated gate which controls vertical current flow.

Compared with bipolar transistors, RF Power FETs exhibit higher gain, higher input impedance, enhanced thermal stability and lower noise. The FETs listed in this section are specified for operation in RF Power Amplifiers and are grouped by frequency range of operation and type of application. Arrangement within each group is first by order of voltage then by increasing output power.

Table 1. 2 to 150 MHz HF/SSB – Vertical MOSFETs

For military and commercial HF/SSB fixed, mobile and marine transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	V _{DD} Volts	Class	Gain (Typ) @ 30 MHz dB	Typical IMD		θ _{JC} °C/W	Package/Style
							d ₃ dB	d ₁₁ dB		
MRF171A	U	2–225	30	28	AB	20	–32	—	1.52	211–07/2
MRF148A	U	2–225	30	50	AB	18	–35	–60	1.5	211–07/2
MRF150	U	2–150	150	50	AB	17	–32	–60	0.6	211–11/2
MRF154	U	2–100	600	50	AB	17	–25	—	0.13	368/2
MRF157	U	2–100	600	50	AB	20	–25	—	0.13	368/2

Table 2. 2 to 225 MHz VHF AM/FM – Vertical MOSFETs

For VHF military and commercial aircraft radio transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	V _{DD} Volts	Class	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Package/Style
MRF134	U	30–225	5	28	AB	14/150	55	10	211–07/2
MRF136	U	30–225	15	28	AB	16/150	60	3.2	211–07/2
MRF171A	U	30–225	45	28	AB	19.5/150	65	1.52	211–07/2
MRF173	U	30–225	80	28	AB	13/150	65	0.8	211–11/2
MRF174	U	30–225	125	28	AB	11.8/150	60	0.65	211–11/2
MRF141	U	2–175	150	28	AB	10/175	55	0.6	211–11/2
MRF141G	U	2–175	300	28	AB	13/175	55	0.35	375/2
MRF151	U	2–175	150	50	AB	13/175	45	0.6	211–11/2
MRF151G	U	2–175	300	50	AB	16/175	55	0.35	375/2

Table 3. 30 to 512 MHz VHF/UHF AM/FM – Vertical MOSFETs

For VHF/UHF military and commercial aircraft radio transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	V _{DD} Volts	Class	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Package/Style
MRF158	U	30–512	2	28	AB	17.5/500	52	13.2	305A/2
MRF160	U	30–512	4	28	AB	17/500	55	7.2	249/3
MRF166C	U	30–512	20	28	AB	16/500	55	2.5	319/3
MRF166W	U	30–512	40	28	AB	16/500	55	1.0	412/1
MRF177	U	100–400	100	28	AB	12/400	60	0.65	744A/2
MRF275L	U	150–512	100	28	AB	8.8/500	55	0.65	333/2
MRF275G	U	150–512	150	28	AB	11.2/500	55	0.44	375/2

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

RF Power MOSFETs (continued)

Table 4. Mobile – To 520 MHz

Designed for broadband VHF & UHF commercial and industrial applications. The high gain and broadband performance of these devices make them ideal for large-signal, common-source amplifier applications in 12.5/7.5 volt mobile, portable and base station operation.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Package/Style
VHF & UHF, Land Mobile Radio, Class AB – LDMOS Die							
MRF1511T1(18f)★	U	136–175	8	7.5	11.5/175	55	466/1
MRF1517T1(18f)★	U	430–520	8	7.5	11/520	55	466/1
MRF1513T1(18f)★	U	400–520	3	7.5/12.5	11/520	55	466/1
MRF1518T1(18f)★	U	400–520	8	12.5	11/520	55	466/1
MRF1535T1(18j)★	U	400–520	35	12.5	10(Min)/520	50(Min)	1264/1
MRF1550T1(18j)★	U	136–175	50	12.5	10(Min)/175	50(Min)	1264/1

Table 5. Broadcast – To 1.0 GHz – Lateral MOSFETs

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	IMD dBc	Package/Style
470 – 1000 MHz, Class AB – LDMOS Die								
MRF373A(46a)	U	470–860	75 CW	32	18/860	60	—	360B/1
MRF373AS(46a)	U	470–860	75 CW	32	18/860	60	—	360C/1
MRF374A(46a)	U	470–860	130 PEP	32	17.3/860	41	–31	375F/2
MRF372★	M	470–860	180 PEP	32	17/860	36	–35	375G/2
MRF377 ⁽⁹⁾	M	470–860	180 PEP	32	18/860	40	–30	375G/2
MRF376 ⁽⁹⁾	M	470–860	400 Pulsed	50	16/860	50	—	375G/2

Table 6. Cellular – To 1.0 GHz – Lateral MOSFETs

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/Style
800 – 1.0 GHz, Class AB – LDMOS Die								
MRF9002R2(18e,46a)	U	960	2 PEP	26	16/960	35	9	978/–
MRF9030MR1(18a,46b)	U	945	30 PEP	26	17/945	41	—	1265/1
MRF9030(46b)	U	945	30 PEP	26	17/945	40	1.9	360B/1
MRF9030S(18a,46b)	U	945	30 PEP	26	17/945	40	1.5	360C/1
MRF9045MR1(18a)★	U	945	45 PEP	28	18.5/945	41	0.8 ⁽⁵⁰⁾	1265/1
MRF9045★	U	945	45 PEP	28	18.8/945	42	1.4	360B/1
MRF9045S(18a)★	U	945	45 PEP	28	18.8/945	42	1.0	360C/1
MRF9060MR1(18a,46b)	U	945	60 PEP	26	17/945	40	—	1265/1
MRF9060(46a)	U	945	60 PEP	26	17/945	40	1.1	360B/1
MRF9060S(18a,46a)	U	945	60 PEP	26	17/945	40	0.8	360C/1
MRF6522–70(18i)	M	921–960	70 CW	26	16/921,960	58	1.1	465D/1
MRF9080★	M	921–960	75 CW	26	18.5/921,960	55	0.7	465/1
MRF9080S★	M	921–960	75 CW	26	18.5/921,960	55	0.7	465A/1
MRF9085★	M	880	90 PEP	26	17.9/880	40	0.7	465/1
MRF9085S★	M	880	90 PEP	26	17.9/880	40	0.7	465A/1

⁽⁹⁾In development.

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units;

f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

⁽⁵⁰⁾Simulated

★New Product

RF Power MOSFETs (continued)

Table 6. Cellular – To 1.0 GHz – Lateral MOSFETs (continued)

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style	
800 – 1.0 GHz, Class AB – LDMOS Die (continued)									
MRF9120 ^(46a)	M	880	120 PEP	2–Tone	26	16/880	39	0.7	375B/2
MRF9120S ^(46a)	M	880	120 PEP	2–Tone	26	16/880	39	0.7	375H/2
MRF9180★	M	880	170 PEP	2–Tone	26	17.5/880	39	0.45	375D/2
MRF9180S★	M	880	170 PEP	2–Tone	26	17.5/880	39	0.45	375E/2

Table 7. PCS and 3G – To 2.1 GHz – Lateral MOSFETs

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style	
1805 – 1990 MHz, Class AB – LDMOS Die (GSM1800, GSM1900, GSM EDGE and PCS TDMA)									
MRF18060A	M	1805–1880	60 CW	1–Tone	26	13/1805,1880	45	0.97	465/1
MRF18060AS	M	1805–1880	60 CW	1–Tone	26	13/1805,1880	45	0.97	465A/1
MRF18060B	M	1930–1990	60 CW	1–Tone	26	13/1930,1990	45	0.97	465/1
MRF18060BS	M	1930–1990	60 CW	1–Tone	26	13/1930,1990	45	0.97	465A/1
MRF18085A ^(46a)	M	1805–1880	85 CW	1–Tone	26	13/1805,1880	52	0.64	465/1
MRF18085AS ^(46a)	M	1805–1880	85 CW	1–Tone	26	13/1805,1880	53	0.64	465A/1
MRF18085B ^(46a)	M	1930–1990	85 CW	1–Tone	26	13/1930,1990	53	0.64	465/1
MRF18085BS ^(46a)	M	1930–1990	85 CW	1–Tone	26	13/1930,1990	52	0.64	465A/1
MRF18090A	M	1805–1880	90 CW	1–Tone	26	13.5/1805,1880	52	0.7	465B/1
MRF18090AS	M	1805–1880	90 CW	1–Tone	26	13.5/1805,1880	52	0.7	465C/1
MRF18090B	M	1930–1990	90 CW	1–Tone	26	13.5/1930,1990	45	0.7	465B/1
MRF18090BS	M	1930–1990	90 CW	1–Tone	26	13.5/1930,1990	45	0.7	465C/1

1.9 GHz, Class AB – LDMOS Die (2–CH N–CDMA)

MRF19030★	M	1930–1990	30 PEP	2–Tone	26	13/1990	36	2.1	465E/1
MRF19030S★	M	1930–1990	30 PEP	2–Tone	26	13/1990	36	2.1	465F/1
MRF19045 ^(46a)	M	1930–1990	9.5 AVG	N–CDMA	26	14.5/1990	23.5	1.97	465E/1
MRF19045S ^(46a)	M	1930–1990	9.5 AVG	N–CDMA	26	14.5/1990	23.5	1.97	465F/1
MRF19060	M	1930–1990	60 PEP	2–Tone	26	12.5/1990	36	0.97	465/1
MRF19060S	M	1930–1990	60 PEP	2–Tone	26	12.5/1990	36	0.97	465A/1
MRF19090	M	1930–1990	90 PEP	2–Tone	26	11.5/1990	35	0.65	465B/1
MRF19090S	M	1930–1990	90 PEP	2–Tone	26	11.5/1990	35	0.65	465C/1
MRF19085★	M	1930–1990	18 AVG	N–CDMA	26	13/1990	23	0.64	465/1
MRF19085S★	M	1930–1990	18 AVG	N–CDMA	26	13/1990	23	0.64	465A/1
MRF19120 ⁽³⁾ ★	M	1930–1990	120 PEP	2–Tone	26	11.7/1990	34	0.45	375D/2
MRF19120S ⁽³⁾ ★	M	1930–1990	120 PEP	2–Tone	26	11.7/1990	34	0.45	375E/2
MRF19125★	M	1930–1990	24 AVG	N–CDMA	26	13.5/1990	22	0.53	465B/1
MRF19125S★	M	1930–1990	24 AVG	N–CDMA	26	13.5/1990	22	0.53	465C/1

⁽³⁾Internal Impedance Matched Push-Pull Transistors

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units; f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Power MOSFETs (continued)

Table 7. PCS and 3G – To 2.1 GHz – Lateral MOSFETs (continued)

Device	Frequency Band ⁽³⁷⁾	Pout Watts	Test Signal	VDD Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style
2.0 GHz, Class A, AB – LDMOS Die								
MRF281SR1 ^(18a) ★	U	1930–2000	4 PEP	2–Tone	26	12.5/2000	33	458B/1
MRF281ZR1 ^(18a) ★	U	1930–2000	4 PEP	2–Tone	26	12.5/2000	33	458C/1
MRF282SR1 ^(18a) ★	U	1930–2000	10 PEP	2–Tone	26	11.5/2000	28(min)	458B/1
MRF282ZR1 ^(18a) ★	U	1930–2000	10 PEP	2–Tone	26	11.5/2000	28(min)	458C/1
MRF284	U	1930–2000	30 PEP	2–Tone	26	10.5/2000	35	360B/1
MRF284SR1 ^(18a)	U	1930–2000	30 PEP	2–Tone	26	10.5/2000	35	360C/1
MRF286 ^(46a)	M	1930–2000	60 PEP	2–Tone	26	10.5/2000	32	465/1
MRF286S ^(46a)	M	1930–2000	60 PEP	2–Tone	26	10.5/2000	32	465A/1
2.1 GHz, Class AB – LDMOS Die (2–CH W–CDMA, UMTS)								
MRF21010★	U	2110–2170	10 PEP	2–Tone	28	13.5/2170	35	360B/1
MRF21010S ^(46a)	U	2110–2170	10 PEP	2–Tone	28	13.5/2170	35	360C/1
MRF21030★	M	2110–2170	30 PEP	2–Tone	28	13/2170	33	465E/1
MRF21030S★	M	2110–2170	30 PEP	2–Tone	28	13/2170	33	465F/1
MRF21045★	M	2110–2170	10 AVG	W–CDMA	28	15/2170	23.5	465E/1
MRF21045S★	M	2110–2170	10 AVG	W–CDMA	28	15/2170	23.5	465F/1
MRF21060	M	2110–2170	60 PEP	2–Tone	28	12.5/2170	34	465/1
MRF21060S	M	2110–2170	60 PEP	2–Tone	28	12.5/2170	34	465A/1
MRF21085★	M	2110–2170	19 AVG	W–CDMA	28	13.6/2170	23	465/1
MRF21085S★	M	2110–2170	19 AVG	W–CDMA	28	13.6/2170	23	465A/1
MRF21090★	M	2110–2170	90 PEP	2–Tone	28	11.7/2170	33	465B/1
MRF21090S★	M	2110–2170	90 PEP	2–Tone	28	11.7/2170	33	465C/1
MRF21120 ⁽³⁾ ★	M	2110–2170	120 PEP	2–Tone	28	11.4/2170	34.5	375D/2
MRF21120S ⁽³⁾ ★	M	2110–2170	120 PEP	2–Tone	28	11.2/2170	34.5	375E/2
MRF21125	M	2110–2170	20 AVG	W–CDMA	28	13/2170	18	465B/1
MRF21125S	M	2110–2170	20 AVG	W–CDMA	28	13/2170	18	465C/1
MRF21180 ^(3,46a)	M	2110–2170	38 AVG	W–CDMA	28	12.5/2170	22	375D/2
MRF21180S ^(3,46a)	M	2110–2170	38 AVG	W–CDMA	28	12.5/2170	22	375E/2

⁽³⁾Internal Impedance Matched Push-Pull Transistors

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units;

f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Power GaAs Transistors

Motorola power GaAs transistors are made using an InGaAs PHEMT epitaxial structure for superior RF efficiency and linearity. The FETs listed in this section are designed for operation in base station infrastructure RF power amplifiers and are grouped according to frequency range and type of application. Parts are listed first by order of operating voltage, then by increasing output power.

Table 1. 3.5 GHz – Linear Transistors

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/GHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style
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3.5 GHz, Class AB – GaAs (WLL, BWA, W-CDMA)

MRFG35010 ⁽⁹⁾	U	3.5 G	1 AVG	W-CDMA	12	10/3.5	26	6	—
MRFG35030 ⁽⁹⁾	M	3.5 G	4 AVG	W-CDMA	12	10/3.5	24	—	—

⁽⁹⁾In development.

RF Power Bipolar Transistors

Motorola's broad line of bipolar RF power transistors are characterized for operation in RF power amplifiers. Typical applications are in base stations, military and commercial landmobile, avionics and marine radio transmitters. Groupings are by frequency band and type of application. Within each group, the arrangement of devices is by major supply voltage rating, then in the order of increasing output power. All devices are NPN polarity except where otherwise noted.

UHF Transistors

Table 1. 100 – 500 MHz Band

Designed for UHF military and commercial aircraft radio transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	Gain (Min)/Freq. dB/MHz	θ _{JC} °C/W	Package/Style
V_{CC} = 28 Volts, Class C						
MRF392 ⁽³⁾	M	100–400	125	8/400	0.65	744A/1
MRF393 ⁽³⁾	M	100–512	100	7.5/500	0.65	744A/1

900 MHz Transistors

Table 2. 900 – 960 MHz Band

Designed specifically for the 900 MHz mobile radio band, these devices offer superior gain, ruggedness, stability and broadband operation. Devices are for mobile and base station applications.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	Class	Gain (Min)/Freq. dB/MHz	θ _{JC} °C/W	Package/Style
V_{CC} = 24 Volts — Si Bipolar							
MRF858S	U	840–900	3.6 CW	A	11/900	6.9	319A/2
MRF897 ⁽³⁾	M	900	30	AB	10/900	1.7	395B/1
MRF897R ⁽³⁾	M	900	30	AB	10.5/900	1.7	395E/1
MRF898 ⁽²⁾	M	850–900	60 CW	C	7/900	1	333A/1
V_{CC} = 26 Volts — Si Bipolar							
MRF6409	M	921–960	20	AB	10/960	3.8	319/2
MRF6414	M	921–960	50	AB	8.5/960	1.3	333A/2
MRF899 ⁽³⁾	M	900	150	AB	8/900	0.8	375A/1

1.5 GHz Transistors

Table 3. 1600 – 1640 MHz Band

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	Class	Gain (Min)/Freq. dB/MHz	η Eff. (Min) %	θ _{JC} °C/W	Package/Style
MRF16006	M	1600–1640	6	C	7.4/1600	40	6.8	395C/2
MRF16030	M	1600–1640	30	C	7.5/1600	40	1.7	395C/2

⁽²⁾Internal Impedance Matched

⁽³⁾Internal Impedance Matched Push-Pull Transistors

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

Microwave Transistors

Table 4. L-Band Long Pulse Power

These products are designed for pulse power amplifier applications in the 960–1215 MHz frequency range. They are capable of handling up to 10 μ s pulses in long pulse trains resulting in up to a 50% duty cycle over a 3.5 millisecond interval. Overall duty cycle is limited to 25% maximum. The primary applications for devices of this type are military systems, specifically JTIDS and commercial systems, specifically Mode S. Package types are hermetic.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Gain (Min) @ 1215 MHz dB	θ_{JC} °C/W	Package/Style
V_{CC} = 28 Volts — Class C Common Base					
MRF10005	M 960–1215	5	8.5	8	336E/1
V_{CC} = 36 Volts — Class C Common Base					
MRF10031	M 960–1215	30	10	3	376B/1
MRF10120	M 960–1215	120	8	0.6	355C/1
V_{CC} = 50 Volts — Class C Common Base					
MRF10150	M 1025–1150	150	10 ⁽⁷⁾	0.25	376B/1
MRF10350	M 1025–1150	350	9 ⁽⁷⁾	0.11	355E/1
MRF10502	M 1025–1150	500	9 ⁽⁷⁾	0.12	355J/1

Linear Transistors

The following sections describe a wide variety of devices specifically characterized for linear amplification. Included are medium power and high power parts covering frequencies to 2.0 GHz.

Table 5. UHF Ultra Linear For TV Applications

The following device has been characterized for ultra-linear applications such as low-power TV transmitters in Band IV and Band V and features diffused ballast resistors and an all-gold metal system to provide enhanced reliability and ruggedness.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Gain (Typ)/Freq. Small Signal Gain dB/MHz	θ_{JC} °C/W	Package/Style
V_{CC} = 28 Volts, Class AB					
TPV8100B	M 470–860	100 ⁽¹¹⁾	9.5/860	0.7	398/1

Table 6. Microwave Linear for PCN Applications

The following devices have been developed for linear amplifiers in the 1.5–2 GHz region and have characteristics particularly suitable for PDC, PCS or DCS1800 base station applications.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Class	Gain (Typ)/Freq. dB/MHz	θ_{JC} °C/W	Package/Style
V_{CC} = 26 Volts–Bipolar Die						
MRF6404 ⁽¹⁶⁾	M 1860–1900	30	AB	8.2/1880	1.4	395C/1
MRF20030R	M 2000	30	AB	11/2000	1.4	395C/1
MRF20060R	M 2000	60	AB	9.8/2000	0.7	451/1
MRF20060RS	M 2000	60	AB	9.8/2000	0.7	451A/1

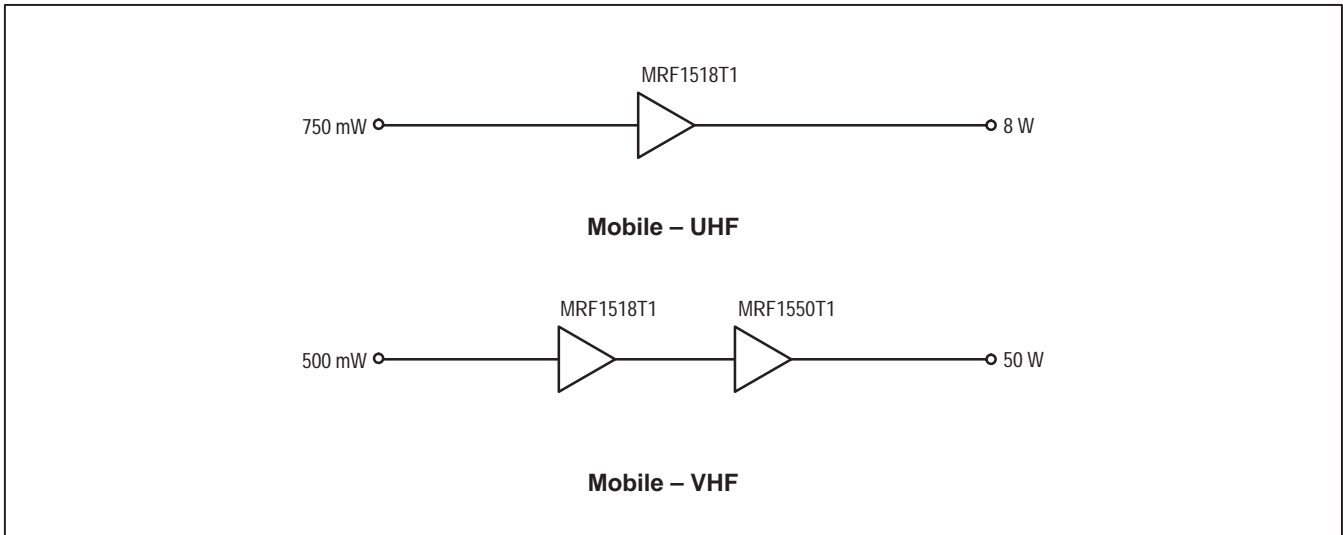
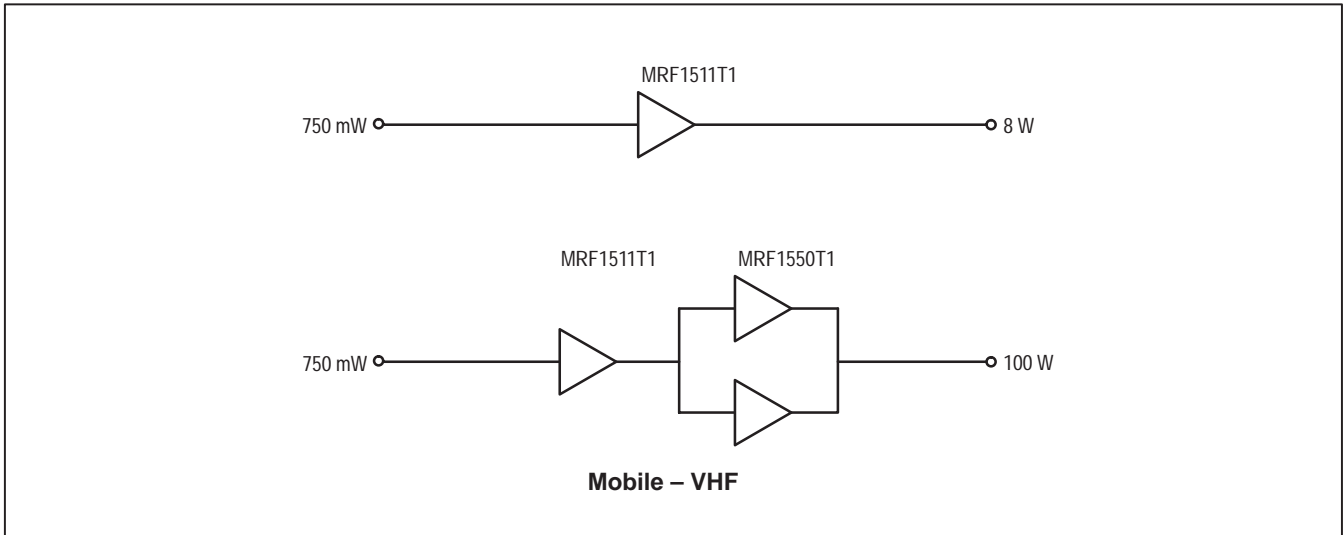
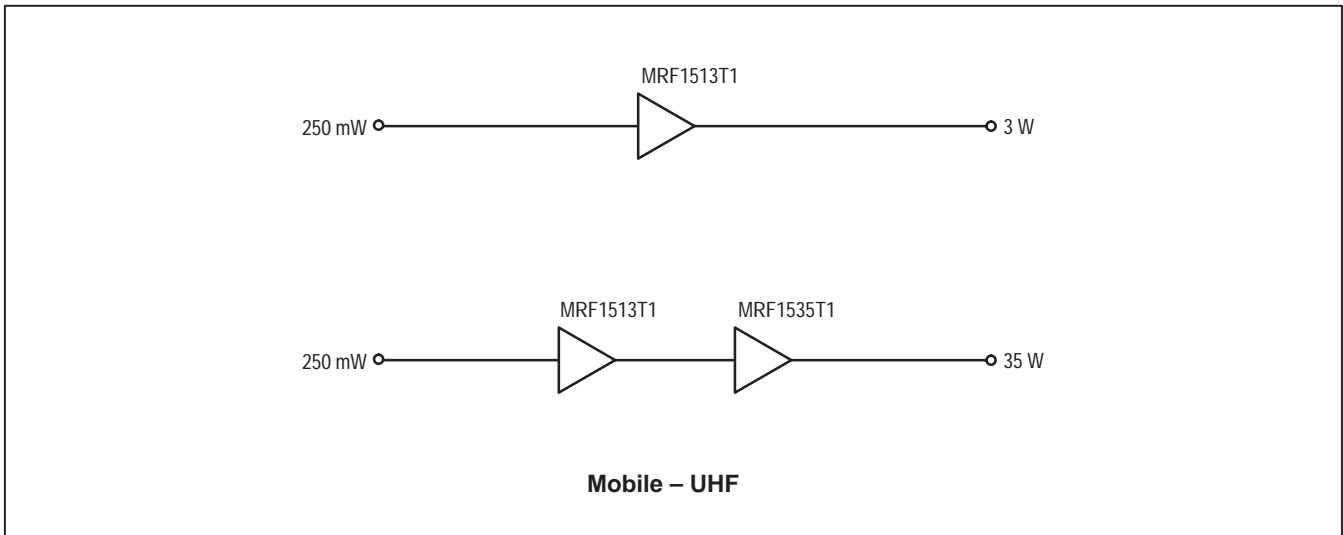
⁽⁷⁾Typical @ 1090 MHz

⁽¹¹⁾Output power at 1 dB compression in Class AB

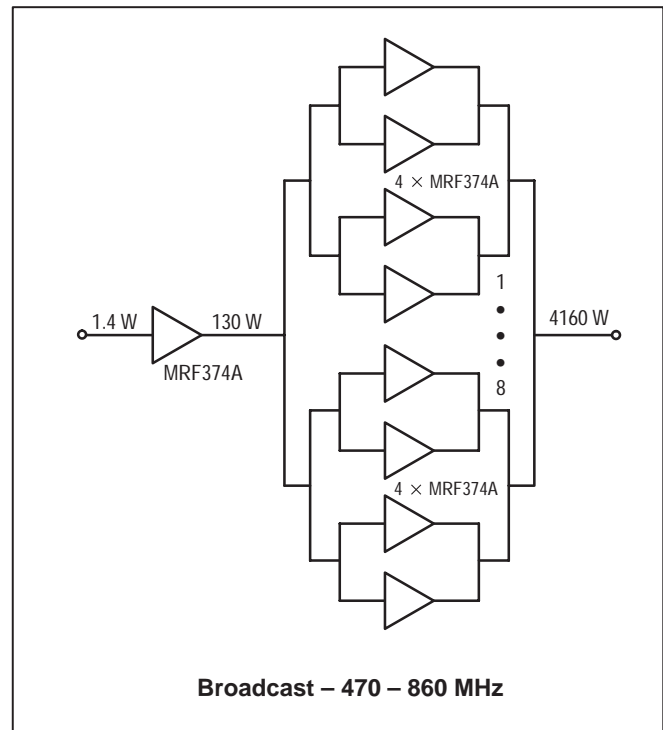
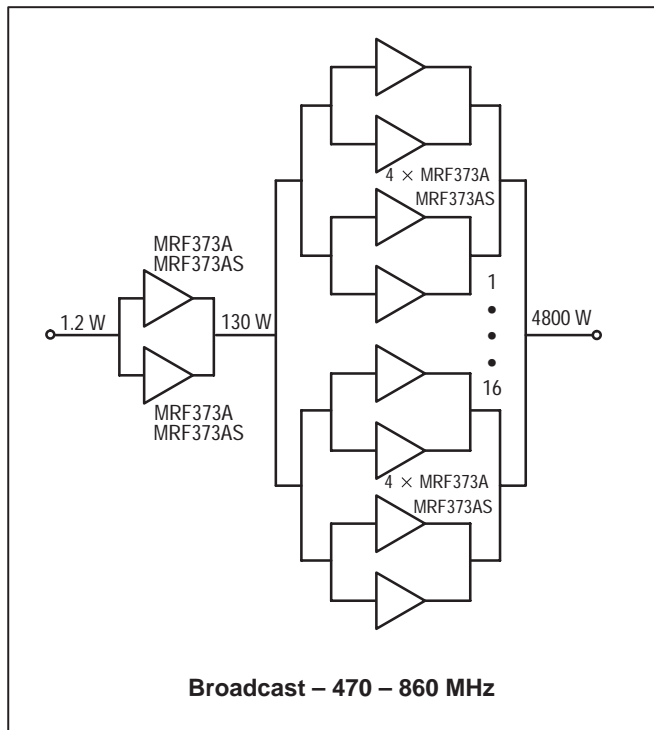
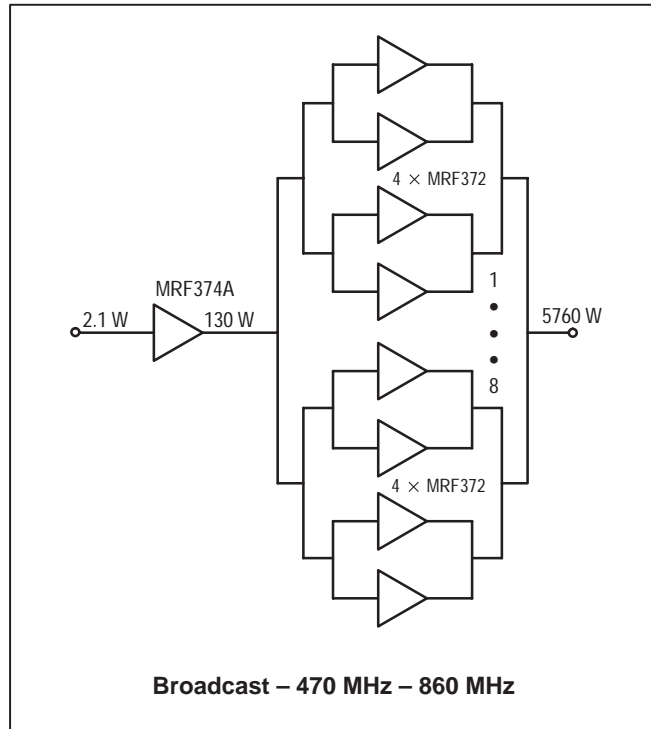
⁽¹⁶⁾Formerly known as "TP4035"

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

RF LDMOS High Power Transistor Amplifier Line-ups

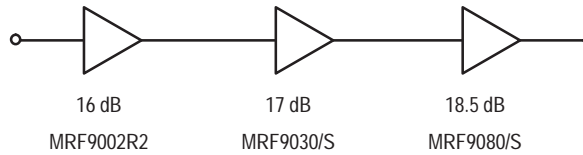


RF LDMOS High Power Transistor Amplifier Line-ups (continued)



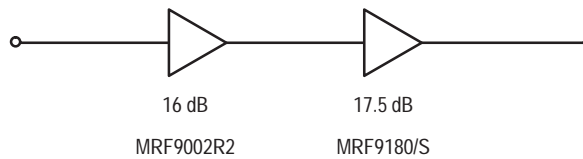
RF LDMOS High Power Transistor Amplifier Line-ups (continued)

GSM EDGE – 900 MHz



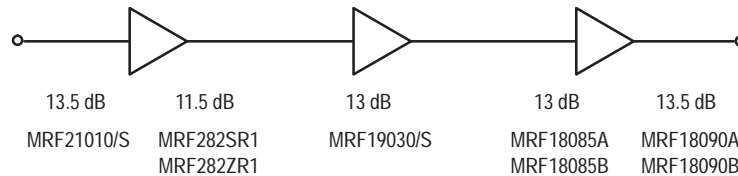
P_{in}	Amp1	Amp2	Amp3	P_{out}
0.602 mW	MRF9002R2	MRF9030/S	MRF9080/S	75 W

Cellular – 1.0 GHz



P_{in}	Amp1	Amp2	P_{out}
80 mW	MRF9002R2	MRF9180/S	170 W

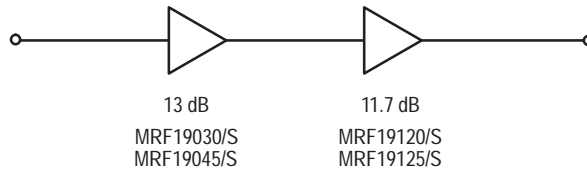
GSM1800, GSM1900, GSM EDGE and PCS TDMA – 1.8 – 1.9 GHz



P_{in}	Amp1	Amp2	Amp3	P_{out}
9.5 mW	MRF21010/S	MRF19030/S	MRF18085A	85 W
9.0 mW	MRF21010/S	MRF19030/S	MRF18090A	90 W
9.5 mW	MRF21010/S	MRF19030/S	MRF18085B	85 W
9.0 mW	MRF21010/S	MRF19030/S	MRF18090B	90 W
15 mW	MRF282SR1/ZR1	MRF19030/S	MRF18085A	85 W
14.2 mW	MRF282SR1/ZR1	MRF19030/S	MRF18090A	90 W
15 mW	MRF282SR1/ZR1	MRF19030/S	MRF18085B	85 W
14.2 mW	MRF282SR1/ZR1	MRF19030/S	MRF18090B	90 W

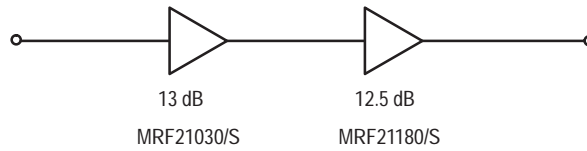
RF LDMOS High Power Transistor Amplifier Line-ups (continued)

2-CH N-CDMA – 1.9 GHz



P _{in}	Amp1	Amp2	P _{out}
406 mW	MRF19030/S	MRF19120/S	120 W
406 mW	MRF19045/S	MRF19125/S	120 W

2-CH W-CDMA, UMTS – 2.1 GHz

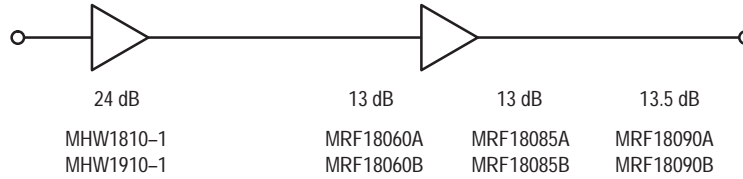


P _{in}	Amp1	Amp2	P _{out}
500 mW	MRF21030/S	MRF21180/S	180 W

RF LDMOS High Power Transistor Amplifier Line-ups (continued)

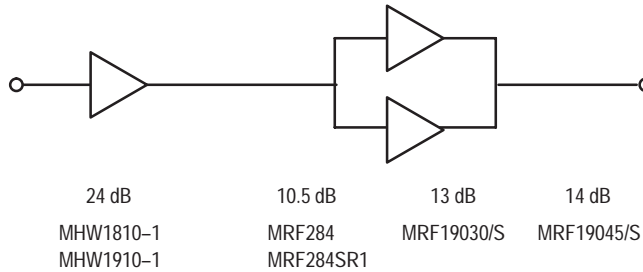
GSM1800, GSM1900 Base Station – Class 1: 30 – 90 Watts, 24 – 26 Volts

60 – 90 W Output



P _{in}	Amp1	Amp2	P _{out}
12 mW	MHW1810-1	MRF18060A	60 W
17 mW	MHW1810-1	MRF18085A	85 W
16 mW	MHW1810-1	MRF18090A	90 W
12 mW	MHW1910-1	MRF18060B	60 W
17 mW	MHW1910-1	MRF18085B	85 W
16 mW	MHW1910-1	MRF18090B	90 W

30 – 40 W Output

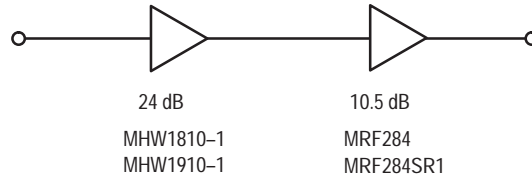


P _{in}	Amp1	Amp2	P _{out}
10.6 mW	MHW1810-1	MRF284/SR1	30 W
6.0 mW	MHW1810-1	MRF19030/S	30 W
7.13 mW	MHW1810-1	MRF19045/S	45 W
10.6 mW	MHW1910-1	MRF284/SR1	30 W
6.0 mW	MHW1910-1	MRF19030/S	30 W
7.13 mW	MHW1910-1	MRF19045/S	45 W

RF LDMOS High Power Transistor Amplifier Line-ups (continued)

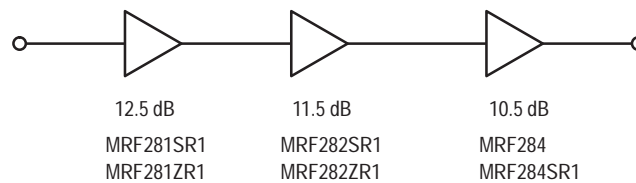
GSM1800, GSM1900 Base Station – Class 2: 30 – 45 Watts, 24 – 26 Volts

30 W Output



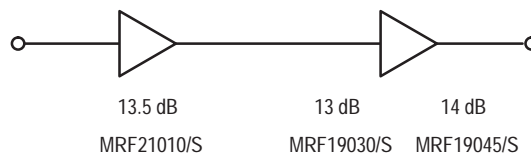
P _{in}	Amp1	Amp2	P _{out}
10.6 mW	MHW1810-1	MRF284/SR1	30 W
10.6 mW	MHW1910-1	MRF284/SR1	30 W

30 W Output



P _{in}	Amp1	Amp2	Amp3	P _{out}
10.6 mW	MRF281SR1/ZR1	MRF282SR1/ZR1	MRF284/SR1	30 W

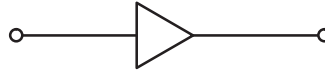
30 – 45 W Output



P _{in}	Amp1	Amp2	P _{out}
67 mW	MRF21010/S	MRF19030/S	30 W
80 mW	MRF21010/S	MRF19045/S	45 W

RF LDMOS High Power Transistor Amplifier Line-ups (continued)

GSM1800, GSM1900 Base Station – Class 3: 5 – 10 Watts, 24 – 26 Volts Microcell



24 dB
MHW1810-1
MHW1910-1

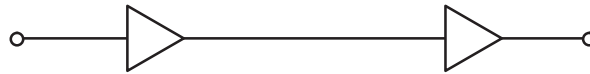
P _{in}	Amp1	P _{out}
40 mW	MHW1810-1	10 W
40 mW	MHW1910-1	10 W



12.5 dB 13.5 dB 11.5 dB
MRF281SR1 MRF21010/S MRF282SR1
MRF281ZR1 MRF282ZR1

P _{in}	Amp1	Amp2	P _{out}
25 mW	MRF281SR1/ZR1	MRF21010/S	10 W
40 mW	MRF281SR1/ZR2	MRF282SR1/ZR2	10 W

GSM900 Base Station – Class 4: 85 – 120 Watts, 24 – 26 Volts

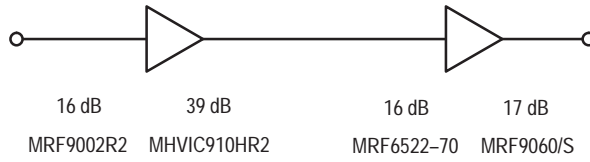


16 dB 39 dB 17.9 dB 16 dB
MRF9002R2 MHVIC910HR2 MRF9085/S MRF9120/S

P _{in}	Amp1	Amp2	P _{out}
37 mW	MRF9002R2	MRF9085/S	90 W
76 mW	MRF9002R2	MRF9120/S	120 W
0.183 mW	MHVIC910HR2	MRF9085/S	90 W
0.379 mW	MHVIC910HR2	MRF9120/S	120 W

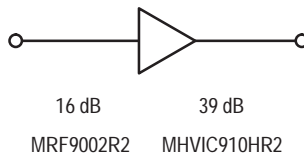
RF LDMOS High Power Transistor Amplifier Line-ups (continued)

GSM900 Base Station – Class 5: 60 – 70 Watts, 24 – 26 Volts



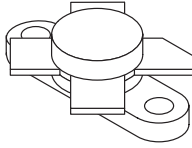
P _{in}	Amp1	Amp2	P _{out}
44 mW	MRF9002R2	MRF6522-70	70 W
30 mW	MRF9002R2	MRF9060/S	60 W
0.221 mW	MHVIC910HR2	MRF6522-70	70 W
0.151 mW	MHVIC910HR2	MRF9060/S	60 W

GSM900 Base Station – Class 7: 5 – 10 Watts, 24 – 26 Volts

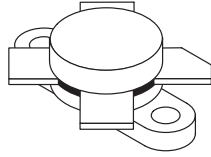


P _{in}	Amp1	P _{out}
252 mW	MRF9002R2	10 W
1.3 mW	MHVIC910HR2	10 W

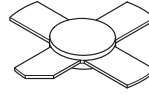
RF Power MOSFETs and Bipolar Transistors Packages



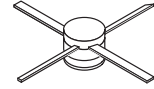
CASE 211-07
STYLE 2
(.380" FLANGE)



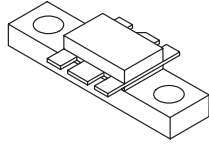
CASE 211-11
STYLE 2
(.500" FLANGE)



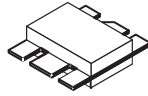
CASE 249
STYLE 3
(.280" PILL)



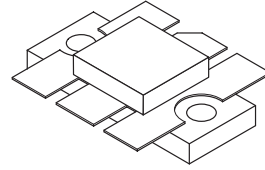
CASE 305A
STYLE 2
(.204" PILL)



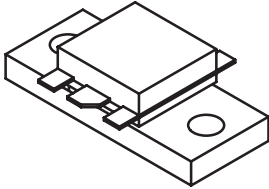
CASE 319
STYLE 2, 3
(CS-12)



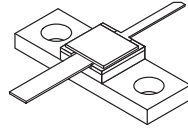
CASE 319A
STYLE 2



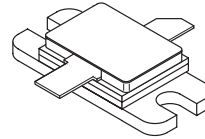
CASE 333
STYLE 2



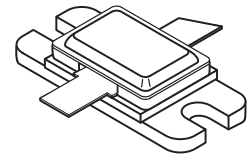
CASE 333A
STYLE 1, 2
(MAAC PAC)



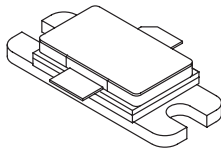
CASE 336E
STYLE 1



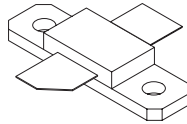
CASE 355C
STYLE 1



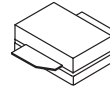
CASE 355E
STYLE 1



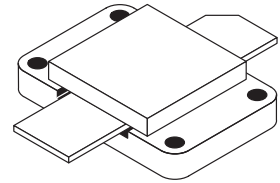
CASE 355J-02
STYLE 1



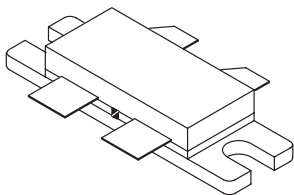
CASE 360B
STYLE 1
(Micro 250)



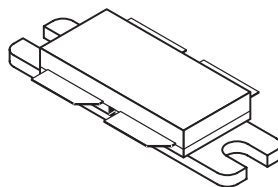
CASE 360C
STYLE 1
(Micro 250S)



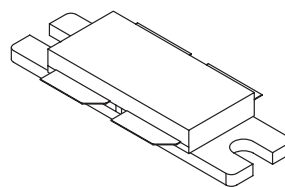
CASE 368
STYLE 2
(HOG PAC)



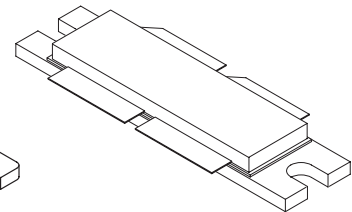
CASE 375
STYLE 2



CASE 375A
STYLE 1

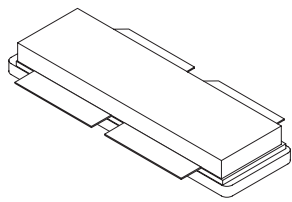


CASE 375B
STYLE 2
(Micro 860)

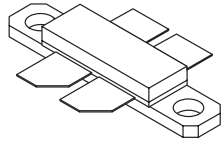


CASE 375D
STYLE 2

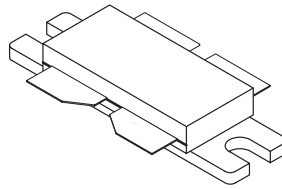
SCALE 1:1



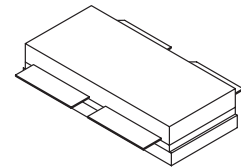
CASE 375E
STYLE 2



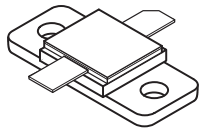
CASE 375F
STYLE 2



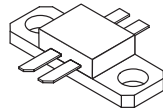
CASE 375G
STYLE 2



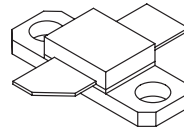
CASE 375H
STYLE 2



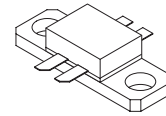
CASE 376B
STYLE 1



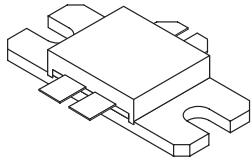
CASE 395B
STYLE 1



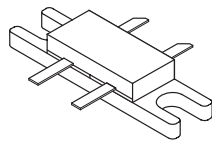
CASE 395C
STYLE 1, 2



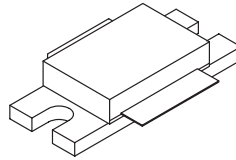
CASE 395E
STYLE 1



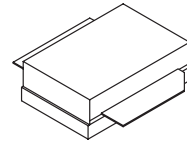
CASE 398
STYLE 1



CASE 412
STYLE 1



CASE 451
STYLE 1



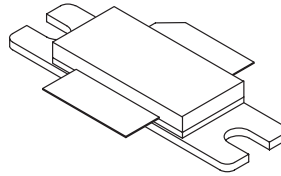
CASE 451A
STYLE 1



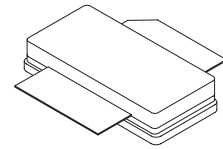
CASE 458B
STYLE 1
(Micro 200S)



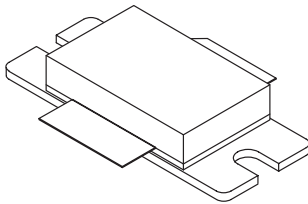
CASE 458C
STYLE 1
(Micro 200Z)



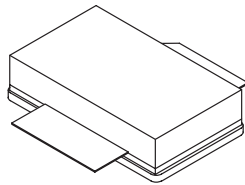
CASE 465
STYLE 1



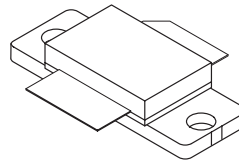
CASE 465A
STYLE 1



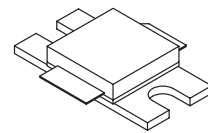
CASE 465B
STYLE 1



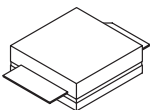
CASE 465C
STYLE 1



CASE 465D
STYLE 1



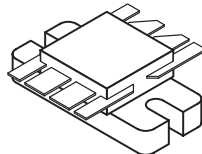
CASE 465E
STYLE 1



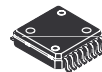
CASE 465F
STYLE 1



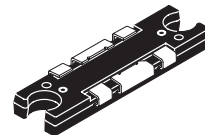
CASE 466
STYLE 1
PLASTIC
(PLD 1.5)



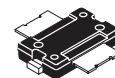
CASE 744A
STYLE 1, 2



CASE 978



CASE 1264
PLASTIC
(TO-272)
STYLE 1



CASE 1265
PLASTIC
(TO-270)
STYLE 1

SCALE 1:1

Motorola RF Amplifier Modules/ICs

Motorola's RF portfolio includes many hybrid designs optimized to perform either in narrowband base station transmitter applications, or in broadband linear amplifiers. Motorola modules feature two or more active transistors (LDMOS, GaAs, or Bipolar die technology) and their associated 50 ohm matching networks. Circuit substrate and metallization have been selected for optimum performance and reliability. For PA designers, hybrid modules offer the benefits of small and less complex system designs, in less time and at a lower overall cost.

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Wideband Linear Amplifiers	1.1-35
Packages	1.1-36

Motorola RF Amplifier Modules/ICs

Complete amplifiers with 50 ohm input and output impedances are available for all popular base station transmitter systems, including GSM and CDMA, covering frequencies from 800 MHz up to 2.2 GHz.

Base Stations

Designed for applications such as macrocell drivers and microcell output stage, these class AB amplifiers are ideal for base station systems at 900, 1800 and 1900 MHz, with power requirements up to 30 watts.

Table 1. Base Stations

Device	Frequency MHz	P1dB Watts	Gain (Min) dB	Supply Voltage Volts	Class	System Application	Die Technology	Package/Style
MHVIC910HR2(18e,46a)	921–960	10	38	26	AB	GSM900	LDMOS–IC	978/–
MHW1810–1	1805–1880	10	24	26	AB	GSM1800	LDMOS	301AW/1
MHW1810–2	1805–1880	10	32	26	AB	GSM1800	LDMOS	301AW/1
MHW1910–1	1930–1990	10	24	26	AB	GSM1900	LDMOS	301AW/1
MHPA19030(46a)	1930–1990	30	25	26	AB	PCS1900	LDMOS	301AP/1
MHPA21030(46a)	2110–2170	30	25	26	AB	W–CDMA	LDMOS	301AP/1

Table 2. Base Station Drivers

These 50 ohm amplifiers are recommended for modern multi–tone CDMA, TDMA and UMTS base station pre–driver applications. Their high third–order intercept point, tight phase and gain control, and excellent group delay characteristics make these devices ideal for use in high–power feedforward loops.

Ultra–Linear (for CDMA, W–CDMA, TDMA, Analog) – Class A (LDMOS Die) – Lateral MOSFETs

Device	Frequency Band MHz	VDD (Nom.) Volts	IDD (Nom.) mA	Gain (Nom.) dB	Gain Flatness (Typ) ±dB	P1dB (Typ) dBm	3rd Order Intercept (Typ) dBm	NF (Typ) dB	Case/Style
MHL9838	800–925	28	770	31	.1	39	50	3.7	301AP/1
MHL9236	800–960	26	550	30.5	.1	34	47	3.5	301AP/1
MHL9236M	800–960	26	550	30.5	.1	34	47	3.5	301AP/2
MHL9318	860–900	28	500	17.5	.1	35.5	49	3.0	301AS/1
MHL18336(46a)	1800–1900	26	500	30	.2	36	46	4.2	301AP/1
MHL18936(46a)	1800–1900	26	1400	30	.2	41	51	4.2	301AY/1
MHL19338	1900–2000	28	500	30	.1	36	46	4.2	301AP/1
MHL19936★	1900–2000	26	1400	29	.2	41	49.5	4.2	301AY/1
MHL21336	2110–2170	26	500	31	.15	35	45	4.5	301AP/1

(18)Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units; f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

(46)To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

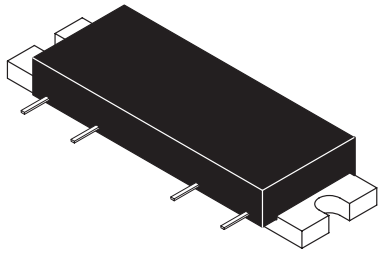
Wideband Linear Amplifiers

Table 1. Standard 50 Ohm Linear Hybrid

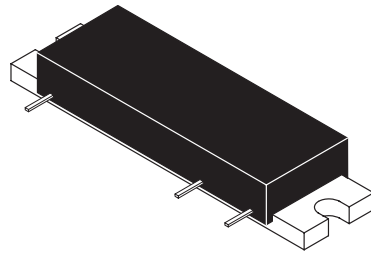
This series of RF linear hybrid amplifier has been optimized for wideband, 50 ohm applications. These amplifiers were designed for multi-purpose RF applications where linearity, dynamic range and wide bandwidth are of primary concern. The MHL series utilizes a new case style that provides microstrip input and output connections.

Device	Frequency Band MHz	V _{CC} (Nom.) Volts	I _{CC} (Nom.) mA	Gain/Freq. (Typ) dB/MHz	Gain Flatness (Typ) ±dB	P _{1dB} (Typ) dBm	3rd Order Intercept Point/Freq. (Typ) dBm/MHz	NF/Freq. (Typ) dB/MHz	Case/ Style
MHL8018	40– 1000	28	210	18.5/900	1	26	38/1000	7.5/1000	448/1
MHL8115	40–1000	15	700	17.5/900	1	30	41.5/1000	8.5/1000	448/2
MHL8118	40–1000	28	400	17.5/900	1	30	41.5/1000	8.5/1000	448/1

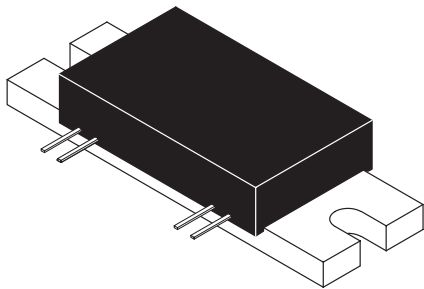
RF Amplifier Modules Packages



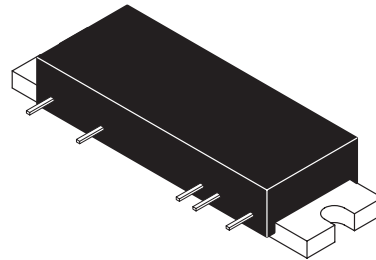
CASE 301AP
STYLE 1, 2



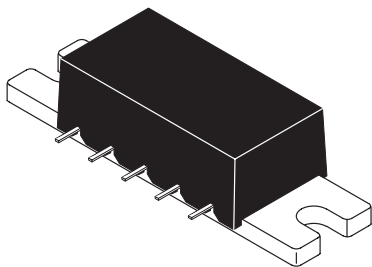
CASE 301AS
STYLE 1



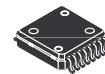
CASE 301AW
STYLE 1



CASE 301AY
STYLE 1



CASE 448
STYLE 1, 2



CASE 978

SCALE 1:1

Motorola RF CATV Distribution Amplifiers

Motorola Hybrids are manufactured using the latest CATV generation technology which has set new standards for CATV system performance and reliability. These hybrids have been optimized to provide premium performance in all CATV systems up to 152 channels. Additions to our CATV product family include 40–870 MHz high output gallium arsenide (GaAs) power doublers as well as low distortion, low power consumption reverse amplifiers.

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Reverse Amplifiers	1.1–40
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Motorola RF CATV Distribution Amplifiers

Motorola Hybrids are manufactured using the latest generation technology which has set new standards for CATV system performance and reliability. These hybrids have been optimized to provide premium performance in all CATV systems up to 152 channels.

Forward Amplifiers

40–1000 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 1000 MHz dB Max	Package/Style
			Output Level	2nd Order Test	Composite Triple Beat	Cross Modulation		
			dBmV	dB	dB 152 CH	dB 152 CH		
MHW9182B	18.5	152	+38	-63 ⁽⁴⁰⁾	-61	-61	7.5	714Y/1
MHW9242A	24	152	+38	-61 ⁽⁴⁰⁾	-58	-59	8.0	714Y/1

40–870 MHz High Output Gallium Arsenide Power Doubler

Device	Hybrid Gain (Nom.) @ 870 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 870 MHz dB Max	Package/Style
			Output Level	2nd Order Test	Composite Triple Beat	Cross Modulation		
			dBmV	dB	dB 132 CH	dB 132 CH		
MHW9187 ^(46b)	20	132	+48	-62 ⁽³⁴⁾	-58	-55	4.5	1302/1

40–860 MHz Hybrids

Device	Gain dB Typ @ 50 MHz	Frequency MHz	V_{CC} Volts	2nd Order IMD @ $V_{out} = 50$ dBmV/ch Max	DIN45004B @ $f=860$ MHz dB μ V Min	Noise Figure @ 860 MHz dB Max	Package/Style
CA901	17	40 – 860	24	-60	120	8.0	714P/2

Power Doubling Hybrids

CA922	17	40 – 860	24	-63	123	9.5	714P/2
CA922A	17	40 – 860	24	-67	123	9.5	714P/2

40–860 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 860 MHz dB Max	Package/Style
			Output Level	2nd Order Test	Composite Triple Beat	Cross Modulation FM = 55 MHz		
			dBmV	dB	dB 128 CH	dB 128 CH		
MHW8182B	18.5	128	+38	-64 ⁽⁴⁰⁾	-66	-65	7.5	714Y/1
MHW8222B★	21.9	128	+38	-60 ⁽⁴⁰⁾	-64	-63	7.0	1302/1
MHW8242A	24	128	+38	-62 ⁽⁴⁰⁾	-64	-62	7.5	714Y/1
MHW8272A	27.2	128	+38	-64 ⁽⁴⁰⁾	-64	-62	7.0	714Y/1
MHW8292	29	128	+38	-56 ⁽⁴⁰⁾	-60	-60	7.0	714Y/1

⁽³⁴⁾Composite 2nd Order; $V_{out} = +48$ dBmV/ch

⁽⁴⁰⁾Composite 2nd Order; $V_{out} = +38$ dBmV/ch

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

CATV Distribution: Forward Amplifiers (continued)

40–860 MHz Hybrids, V_{CC} = 24 Vdc, Class A (continued)

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 860 MHz dB Max	Package/ Style
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat	Cross Modulation FM = 55 MHz dB		
					dB	dB		
					128 CH	128 CH		

Power Doubling Hybrids

MHW8185L ⁽²¹⁾	18.5	128	+40	-62 ⁽³⁹⁾	-63	-64	8.5*	714Y/1
MHW8185LR ⁽²⁸⁾	18.5	128	+40	-62 ⁽³⁹⁾	-63	-64	8.5*	714Y/2
MHW8185	18.8	128	+40	-62 ⁽³⁹⁾	-64	-64	8.0	714Y/1
MHW8185R ⁽¹⁴⁾	18.8	128	+40	-62 ⁽³⁹⁾	-64	-64	8.0	714Y/2
MHW8205L ⁽²²⁾	19.5	128	+40	-60 ⁽³⁹⁾	-63	-64	8.5*	714Y/1
MHW8205	19.8	128	+40	-60 ⁽³⁹⁾	-63	-64	8.0	714Y/1
MHW8205R ⁽²⁴⁾	19.8	128	+40	-60 ⁽³⁹⁾	-63	-64	8.0	714Y/2

*@ 870 MHz

40–750 MHz Hybrids, V_{CC} = 24 Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 750 MHz dB Max	Package/ Style
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat	Cross Modulation FM = 55 MHz dB		
					dB	dB		
					110 CH	110 CH		

Power Doubling Hybrids

MHW7185CL ⁽²³⁾	18.5	110	+44	-64 ⁽³⁶⁾	-61	-63	7.5	714Y/1
MHW7185C	18.8	110	+44	-64 ⁽³⁶⁾	-62	-63	7.5	714Y/1
MHW7205CL ⁽²⁷⁾	19.5	110	+44	-63 ⁽³⁶⁾	-61	-62	7.5	714Y/1
MHW7205C	19.8	110	+44	-63 ⁽³⁶⁾	-61	-62	7.5	714Y/1

⁽¹⁴⁾Mirror Amplifier Version of MHW8185

⁽²¹⁾Low DC Current Version of MHW8185; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²²⁾Low DC Current Version of MHW8205; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²³⁾Low I_{CC} Version of MHW7185C; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²⁴⁾Mirror Amplifier Version of MHW8205

⁽²⁷⁾Low I_{CC} Version of MHW7205C; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²⁸⁾Mirror Amplifier Version of MHW8185L

⁽³⁶⁾Composite 2nd order; V_{out} = +44 dBmV/ch

⁽³⁹⁾Composite 2nd order; V_{out} = +40 dBmV/ch

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

CATV Distribution: Forward Amplifiers (continued)

40–550 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 550 MHz dB Max	Package/Style	
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat dB				Cross Modulation dB 77 CH
					77 CH	77 CH			
MHW6342T	34.5	77	+44	-64 ⁽³⁵⁾	-57	-57	6.5	1302/1	

Reverse Amplifiers

5–200 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications						Noise Figure @ 175 MHz dB Max	Package/Style
			Output Level dBmV	2nd Order Test ⁽³⁰⁾ dB	Composite Triple Beat dB		Cross Modulation dB			
					22 CH	26 CH	22 CH	26 CH		
MHW1224	22	22	+50	-72	-69	-68.5 ⁽¹⁹⁾	-62	-62 ⁽¹⁹⁾	5.5	714Y/1
MHW1244	24	22	+50	-72	-68	-67.5 ⁽¹⁹⁾	-61	-61 ⁽¹⁹⁾	5.0	714Y/1

Low Current Amplifiers — 5–200 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications								DC Current mA Typ.	Noise Figure @ 200 MHz dB Max	Pkg/Style
			Output Level dBmV	2nd Order Test dB		Composite Triple Beat dB		Cross Modulation dB					
				6 CH	10 CH	6 CH	10 CH	6 CH	10 CH				
MHW1223LA★	22.7	6,10	50	-68	-65	-75	-66	-65	-60	95	7.0	1302/1	
MHW1253LA★	25.5	6,10	50	-68	-66	-75	-66	-65	-61	95	6.5	1302/1	
MHW1303LA★	30.8	6,10	50	-68	-65	-74	-64	-64	-58	95	5.7	1302/1	

Low Current Amplifiers — 5–150 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications								DC Current mA Typ.	Noise Figure @ 150 MHz dB Max	Pkg/Style
			Output Level dBmV	2nd Order Test dB		Composite Triple Beat dB		Cross Modulation dB					
				6 CH	10 CH	6 CH	10 CH	6 CH	10 CH				
MHW1353LA★	35.2	6,10	50	-68	-65	-73	-62	-63	-57	95	5.4	1302/1	

⁽¹⁹⁾Typical

⁽³⁰⁾Channels 2 and A @ 7

⁽³⁵⁾Channels 2 and M30 @ M39

⁽³⁶⁾Composite 2nd order; $V_{Out} = +44$ dBmV/ch

★New Product

CATV Distribution: Reverse Amplifiers (continued)

Low Current Amplifiers — 5–65 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications							DC Current mA Typ.	Noise Figure @ 65 MHz dB Max	Pkg/ Style
			Output Level dBmV	2nd Order Test dB		Composite Triple Beat dB		Cross Modulation dB				
				6 CH	10 CH	6 CH	10 CH	6 CH	10 CH			
MHW1224LA★	22.7	6,10	50	-68	-65	-75	-66	-65	-60	95	7.0	1302/1
MHW1254LA★	25.5	6,10	50	-68	-66	-75	-66	-65	-61	95	6.5	1302/1
MHW1304LA★	30.8	6,10	50	-68	-65	-74	-64	-64	-58	95	5.7	1302/1
MHW1354LA★	35	6,10	50	-68	-65	-73	-62	-63	-57	95	5.2	1302/1

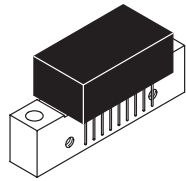
Low Current Amplifiers — 5–50 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	I _{DC} mA Max	Maximum Distortion Specifications				Noise Figure @ 50 MHz dB Max	Package/ Style
				Output Level dBmV	2nd Order Test ⁽³⁰⁾ dB	Composite Triple Beat dB	Cross Modulation dB		
						4 CH	4 CH		
MHW1254L	25	4	135	+50	-70	-70	-62	4.5	714Y/1
MHW1304L	30	4	135	+50	-70	-66	-57	4.5	714Y/1

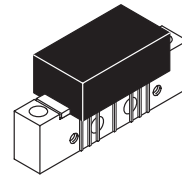
⁽³⁰⁾Channels 2 and A @ 7

★New Product

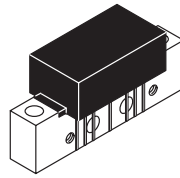
RF CATV Distribution Amplifiers Packages



CASE 714P
STYLE 2



CASE 714Y
STYLE 1, 2



CASE 1302
STYLE 1

SCALE 1:2

Chapter Two

RF Front End ICs

Section One	2.1-0
RF Front End ICs – Selector Guide	
Section Two	2.2-0
RF Front End ICs – Data Sheets	

Section One

Selector Guide

RF Front End ICs

Motorola's RF Front End integrated circuit devices provide an integrated solution for the personal communications market. These devices are available in plastic SOT-143, SOT-343, TSSOP-16, TSSOP-16EP, Micro-8, TSSOP-20EP, or BCC32++ packages.

Evaluation Boards

Evaluation boards are available for RF Front End Integrated Circuits. For a complete list of currently available boards and ones in development for newly introduced product, please contact your local Motorola Distributor or Sales Office.

Table of Contents

	Page
RF Front End ICs	2.1-1
RFICs	2.1-2
Upconverters/Exciters	2.1-2
Power Amplifiers	2.1-2
RF Building Blocks	2.1-3
Amplifiers	2.1-3
Low Power Transistors	2.1-3
Packages	2.1-4

RF Front End ICs

RFICs

Upconverters/Exciters

Device	RF Freq. Range MHz	Supply Volt. Range Vdc	Supply Current mA (Typ)	Standby Current mA (Typ)	Conv. Gain dB (Typ)	Output IP3 dBm (Typ)	Case No./ Package	System Applicability
MRFIC0954(18b)	800 to 1000	2.7 to 5.0	65	5.0	31	28	948M/ TSSOP-20EP	CDMA, TDMA, ISM
MRFIC1813(18b)	1700 to 2000	2.7 to 4.5	25	0.1	15	11	948C/ TSSOP-16	DCS1800, PCS
MRFIC1854A(18b)	1700 to 2000	2.7 to 5.0	70	5.0	31	23	948M/ TSSOP-20EP	CDMA, TDMA, PCS
MRFIC1884(46a)	800 to 1000	2.7 to 3.2	60	5.0	32	28	1261A/ BCC32++	CDMA, TDMA, ISM, PCS
	1700 to 2000					23		

Power Amplifiers

Device	Freq. Range MHz	Supply Volt. Range Vdc	Saturated Pout dBm (Typ)	PAE % (Typ)	Gain Pout/Pin dB (Typ)	Case No./ Package	System Applicability
MRFIC0919(18b)	800 to 1000	3.0 to 5.5	35.3	48	32.3	948L/ TSSOP-16EP	GSM
MRFIC1819(18b)	1700 to 2000	3.0 to 5.0	33	40	27	948L/ TSSOP-16EP	DCS1800, PCS
MRFIC1856(18b)	800 to 1000	3.0 to 5.6	32	50	32	948M/ TSSOP-20EP	TDMA, CDMA, AMPS
	1700 to 2000		30	35	30		TDMA, CDMA, PCS
MRFIC1859(18b)	800 to 1000	2.8 to 5.5	36.2	53	33.2	873E/ TQFP-32EP	GSM
	1700 to 2000		34	43	29		DCS1800, PCS
MRFIC1869(46a)★	800 to 1000	2.7 to 5.5	35.8	55	35.8	MLF-32	GSM900
	1700 to 2000		34	45	32		DCS1800, PCS

(18)Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units; f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

(46)To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Building Blocks

Amplifiers

Device	RF Freq. Range MHz	Supply Volt. Range Vdc	Supply Current mA (Typ)	Standby Current μ A (Typ)	Small Signal Gain dB (Typ)	Output IP3 dBm (Typ)	NF dB (Typ)	Case No./ Package	System Applicability
MBC13706 ^(46a) ★	800 to 1000	2.7 to 3.6	10	200	26	6.0	3.0	846A/ Micro-8	GSM, ISM
MRFIC0916 ^(18c)	100 to 2500	2.7 to 5.0	4.7	–	18.5	11	1.9	318A/ SOT-143	ISM, PCS, Cellular
MRFIC0930DM ^(18b)	800 to 1000	2.7 to 4.5	8.5	20	19	10	1.7	846A/ Micro-8	GSM, AMPS, ISM
MRFIC1808DM ^(18b)	1700 to 2100	2.7 to 4.5	5.0	8.0	18	13	1.6	846A/ Micro-8	DCS1800, PCS

Low Power Transistors

Device	Gain – Bandwidth		NFmin @ f		Gain @ f		Maximum Ratings		Case No./ Package
	f_t Typ GHz	I_C mA	Typ dB	GHz	Typ dB	GHz	V(BR) CEO Volts	I_C mA	
MBC13900 ^(46a) ★	15	20	1.0	1.0	17	1.0	7.0	20	318M/ SOT-343
			1.3	2.0	14	2.0			
MBC13901 ^(46a) ★	15	20	1.0	1.0	17	1.0	7.0	20	318M/ SOT-343
			1.3	2.0	14	2.0			

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units;

f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Front End Integrated Circuit Packages



CASE 318A
(SOT-143)



CASE 318M
(SOT-343)



CASE 846A
(Micro-8)



CASE 873E
(TOFP-32EP)



CASE 948C
(TSSOP-16)



CASE 948L
(TSSOP-16EP)



CASE 948M
(TSSOP-20EP)



CASE 1261A
(BCC32++)

Section Two

RF Front End ICs – Data Sheets

Device Number	Page Number
RFICs	
Upconverters/Exciters	
MRFIC0954	2.2-38
MRFIC1813	2.2-54
MRFIC1854A	2.2-70
MRFIC1884	2.2-100
Power Amplifiers	
MRFIC0919	2.2-21
MRFIC1819	2.2-60
MRFIC1856	2.2-79
MRFIC1859	2.2-86
MRFIC1869	2.2-98
RF Building Blocks	
Amplifiers	
MBC13706	2.2-3
MRFIC0915	2.2-6
MRFIC0916	2.2-14
MRFIC0930	2.2-31
MRFIC1808	2.2-47
Mixers	
MBC13900	2.2-4
MBC13901	2.2-5



Product Preview
The RF Building Block Series
GSM Low Noise Amplifier
with Gain Control

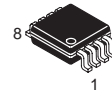
Designed primarily for use in GSM wireless communication systems. The MBC13706 is a silicon low noise amplifier with three available gain settings. Two gain control pins control the gain settings. The LNA can be turned off during transmit mode to save current by disabling the RX Enable pin. The LNA is packaged in a low-cost Micro-8 package.

- Usable Frequency Range: 925 to 960 MHz
- Three Gain States: 26, 18, and 0 dB
- 3.0 dB Max Noise @ Max Gain
- High Reverse Isolation: > 40 dB @ 945 MHz
- Low Power Consumption = 30 mW @ Max Gain, 3.0 V
- Low Standby Current = 200 μ A (Typ)
- Low Cost Surface Mount Plastic Package

MBC13706

GSM LNA WITH GAIN CONTROL

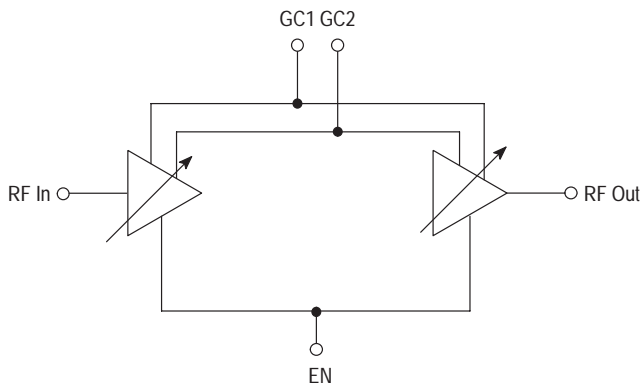
SEMICONDUCTOR TECHNICAL DATA



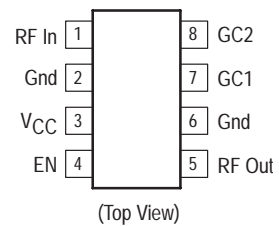
(Scale 2:1)

PLASTIC PACKAGE
CASE 846A
(Micro-8)

Simplified Block Diagram



PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MBC13706	T _A = -30 to 70°C	Micro-8



Product Preview

The RF Building Block Series

**NPN Silicon
Low Noise Transistor**

The MBC13900 is a high performance transistor fabricated using Motorola's 15 GHz f_T bipolar IC process. It is housed in the 4-lead SC-70 (SOT-343) surface mount plastic package resulting in a parasitic effect reduction and RF performance enhancements. The high performance at low power makes the MBC13900 suitable for front-end applications in portable wireless systems such as pagers, cellular and cordless phones.

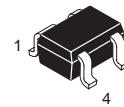
- Low Noise Figure, $NF_{min} = 1.0$ dB (Typ) @1.0 GHz, 3.0 V and 3.0 mA
- Maximum Stable Gain, 22 dB @ 1.0 GHz, 3.0 V and 3.0 mA
- Output Third Order Intercept, $OIP_3 = 23$ dBm @ 1.0 GHz, 3.0 V and 22 mA
- Ultra small SOT-343 Surface Mount Package
- Available Only in Tape and Reel Packaging

MBC13900

**RF NPN
SILICON TRANSISTOR**

$f_T = 15$ GHz
 $NF_{min} = 1.2$ dB
 $I_{C_{MAX}} = 20$ mA
 $V_{CEO} = 5.0$ V

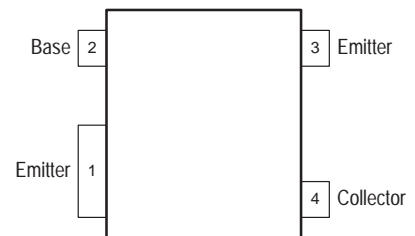
**SEMICONDUCTOR
TECHNICAL DATA**



(Scale 4:1)

PLASTIC PACKAGE
CASE 318M
(SOT-343, Tape & Reel Only)

PIN CONNECTIONS



ORDERING INFORMATION

Device	Package
MBC13900	SOT-343

Product Preview
The RF Building Block Series
**NPN Silicon
Low Noise Transistor**

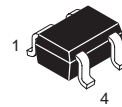
The MBC13901 is a high performance transistor fabricated using Motorola's 15 GHz f_T bipolar IC process. It is housed in the 4-lead SC-70 (SOT-343) surface mount plastic package resulting in a parasitic effect reduction and RF performance enhancements. The high performance at low power makes the MBC13901 suitable for front-end applications in portable wireless systems such as pagers, cellular and cordless phones.

- Low Noise Figure, $NF_{min} = 1.0$ dB (Typ) @ 1.0 GHz, 3.0 V and 3.0 mA
- Maximum Stable Gain, 22 dB @ 1.0 GHz, 3.0 V and 3.0 mA
- Output Third Order Intercept, $OIP_3 = 23$ dBm @ 1.0 GHz, 3.0 V and 22 mA
- Ultra small SOT-343 Surface Mount Package
- Available Only in Tape and Reel Packaging

MBC13901

**RF NPN
SILICON TRANSISTOR**

$f_T = 15$ GHz
 $NF_{min} = 1.2$ dB
 $I_{C_{MAX}} = 20$ mA
 $V_{CEO} = 5.0$ V

**SEMICONDUCTOR
TECHNICAL DATA**


(Scale 4:1)

PLASTIC PACKAGE
CASE 318M
(SOT-343, Tape & Reel Only)

ORDERING INFORMATION

Device	Package
MBC13901	SOT-343

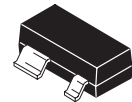
The MRFIC Line
**General Purpose
RF Cascode Amplifier**

The MRFIC0915 is a cost-effective, high isolation cascode silicon monolithic amplifier in the industry standard SOT-143 surface mount package designed for general purpose RF applications. The device is a lower current version of the MRFIC0916 and is appropriate for VCOs, VCO buffers and amplifiers. On-chip bias circuitry sets the bias point while matching is accomplished off chip affording the maximum in application flexibility.

- Usable Frequency Range = 100 to 2500 MHz
- Good Small Signal Gain at $V_{CC} = 2.7$ Volts
 - 16.2 dB Typ at 850 MHz
 - 9.6 dB Typ at 1800 MHz
 - 5.8 dB Typ at 2400 MHz
- -4.6 dBm typical Output Power at 1 dB Gain Compression at 850 MHz, $V_{CC} = 2.7$ Volts
- 38 dB Typical Reverse Isolation at 850 MHz
- 2.5 mA Max Bias Current at $V_{CC} = 2.7$ Volts
- 2.7 to 5 Volt Supply
- Order MRFIC0915T1 for Tape and Reel.
T1 Suffix = 3,000 Units per 8 mm, 7 inch Reel.
- Device Marking = 22

MRFIC0915

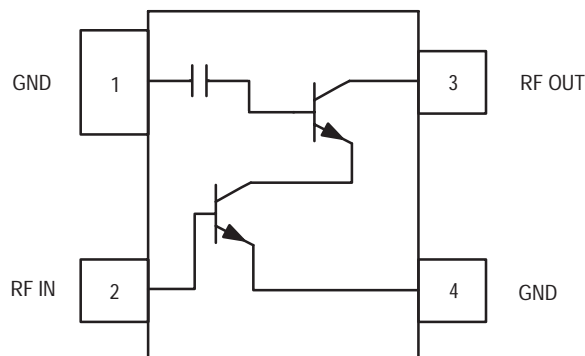
100 to 2500 MHz
SILICON GENERAL PURPOSE
RF CASCODE AMPLIFIER



CASE 318A-05
(SOT-143)

MAXIMUM RATINGS ($T_A = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Limit	Unit
Supply Voltage	V_{CC}	6	Vdc
RF Input Power	P_{RF}	10	dBm
Power Dissipation	P_{DIS}	100	mW
Supply Current	I_{CC}	10	mA
Thermal Resistance, Junction to Case	$R_{\theta JC}$	250	$^\circ\text{C/W}$
Storage Temperature Range	T_{stg}	- 65 to +150	$^\circ\text{C}$
Operating Case Temperature	T_C	- 40 to +100	$^\circ\text{C}$



Pin Connections and Functional Block Diagram

NOT RECOMMENDED FOR NEW DESIGNS

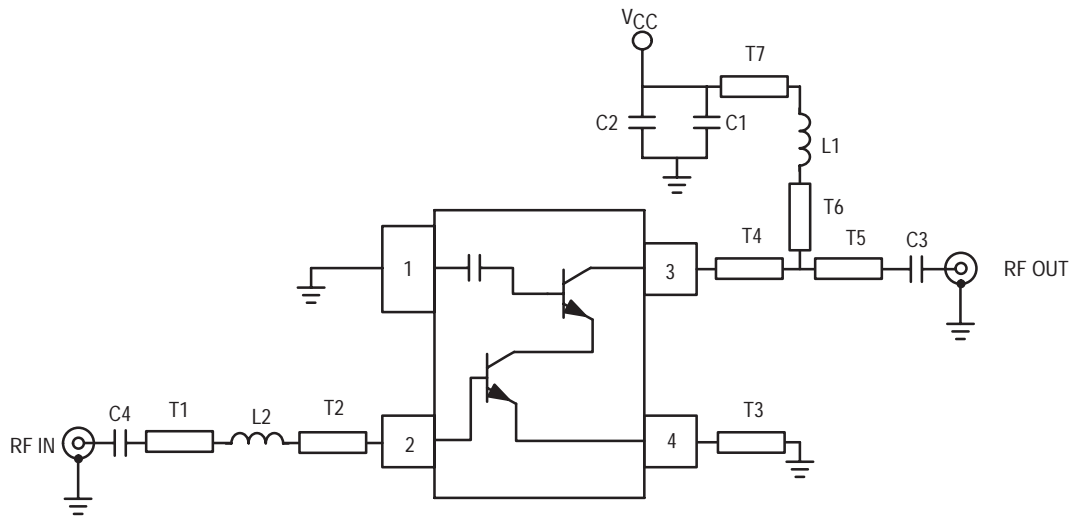
NOT RECOMMENDED FOR NEW DESIGNS

RECOMMENDED OPERATING RANGES

Parameter	Symbol	Value	Unit
RF Frequency	f_{RF}	100 to 2500	MHz
Supply Voltage	V_{CC}	2.7 to 5	Vdc

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7\text{ V}$, $T_A = 25^\circ\text{C}$)

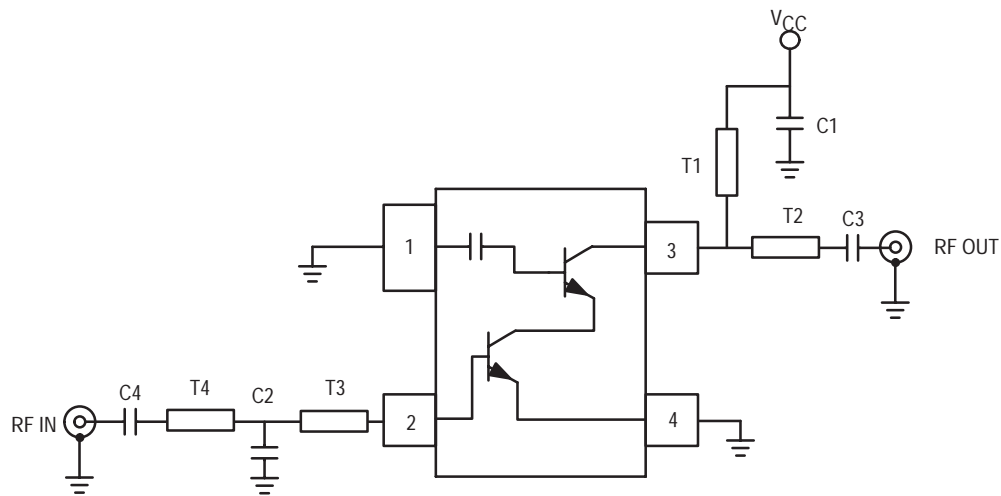
Characteristic	Min	Typ	Max	Unit	
Small Signal Gain	850 MHz	14.2	16.2	—	dB
	1800 MHz	7.4	9.6	—	dB
	2400 MHz	5	5.8	—	dB
Noise Figure	850	—	1.9	—	dB
	1800 MHz	—	3.6	—	dB
	2400 MHz	—	5.5	—	dB
Power Output at 1dB Gain Compression	850 MHz	—	-4.6	—	dBm
	1800 MHz	—	-7.8	—	dBm
	2400 MHz	—	-9.8	—	dBm
Output 3rd Order Intercept Point	850 MHz	—	4	—	dBm
	1800 MHz	—	1	—	dBm
	2400 MHz	—	-1	—	dBm
Reverse Isolation	850 MHz	—	38	—	dB
	1800 MHz	—	33	—	dB
	2400 MHz	—	29	—	dB
Supply Current	1.5	2.0	2.5	mA	



C1	10 pF, NPO/COG	T1	50 Ω MICROSTRIP, 0.13"
C2	0.01 μF	T2	76 Ω MICROSTRIP, 0.072"
C3	1.4 pF, NPO/COG	T3	100 Ω MICROSTRIP, 0.035"
C4	12 pF, NPO/COG	T4	50 Ω MICROSTRIP, 0.048"
L1	8.2 nH	T5	50 Ω MICROSTRIP, 0.08"
L2	10 nH	T6	76 Ω MICROSTRIP, 0.062"
		T7	76 Ω MICROSTRIP, 0.07"

BOARD MATERIAL: FR4, $\epsilon_r = 4.45$, THICKNESS = 0.014"

Figure 1. 850 MHz Applications Circuit Configuration



1.8 GHz DESCRIPTION		2.4 GHz DESCRIPTION	
C1	18 pF, NPO/COG	C1	12 pF, NPO/COG
C2	1.0 pF, NPO/COG	C2	1.2 pF, NPO/COG
C3	0.9 pF, NPO/COG	C3	0.7 pF, NPO/COG
C4	10 pF, NPO/COG	C4	10 pF, NPO/COG
T1	50 Ω MICROSTRIP, 0.41"	T1	50 Ω MICROSTRIP, 0.228"
T2	50 Ω MICROSTRIP, 0.076"	T2	50 Ω MICROSTRIP, 0.076"
T3	50 Ω MICROSTRIP, 0.528"	T3	50 Ω MICROSTRIP, 0.229"
T7	N/A	T4	50 Ω MICROSTRIP, 0.345"

BOARD MATERIAL: FR4, $\epsilon_r = 4.45$, THICKNESS = 0.014"

Figure 2. 1800 and 2400 MHz Applications Circuit Configuration

TYPICAL CHARACTERISTICS

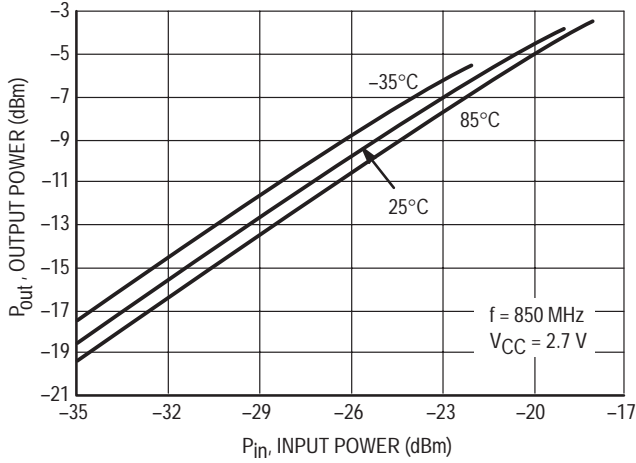


Figure 3. Output Power versus Input Power

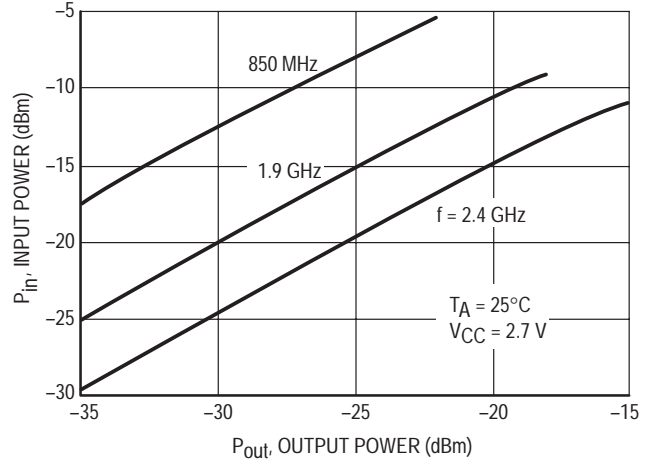


Figure 4. Output Power versus Input Power

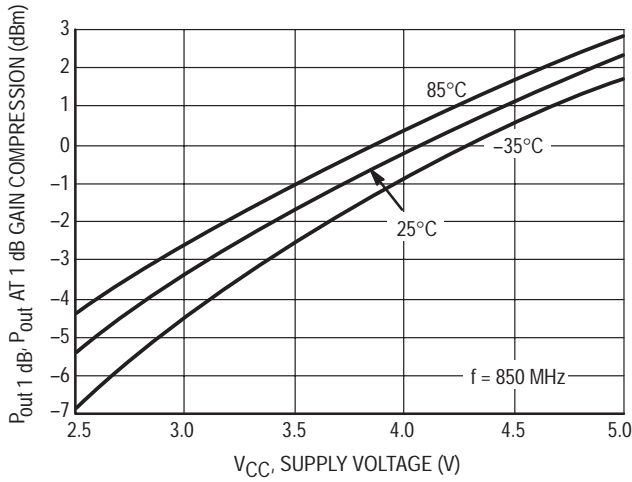


Figure 5. Output Power at 1 dB Gain Compression versus Supply Voltage

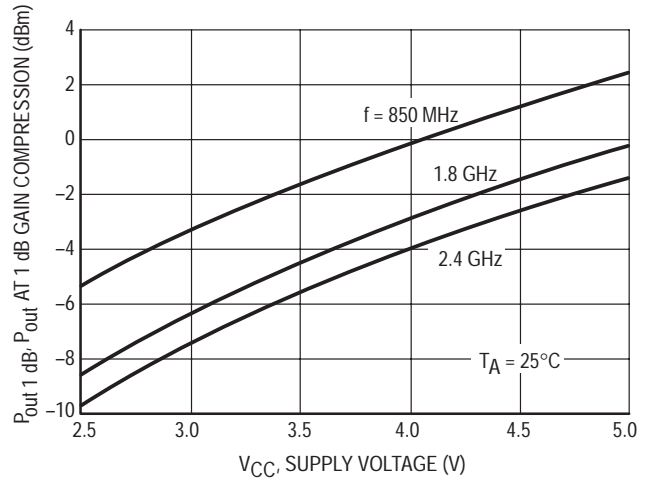


Figure 6. Output Power at 1 dB Gain Compression versus Supply Voltage

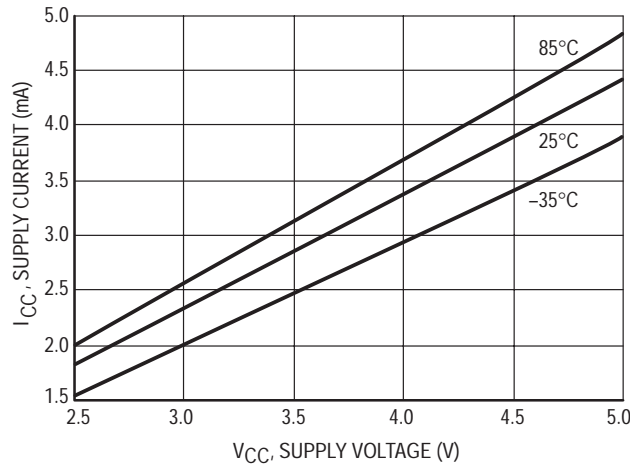


Figure 7. Supply Current versus Supply Voltage

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
100	0.91	-11	5.72	168	0.000	53	0.97	-3
200	0.90	-22	5.50	156	0.001	85	0.97	-7
300	0.86	-32	5.32	145	0.002	80	0.96	-10
400	0.82	-42	5.00	134	0.002	74	0.95	-13
500	0.75	-52	4.72	122	0.002	69	0.94	-16
600	0.70	-60	4.35	113	0.002	67	0.92	-18
700	0.66	-68	4.05	105	0.003	66	0.91	-21
800	0.63	-75	3.65	97	0.003	67	0.90	-24
900	0.57	-83	3.52	89	0.002	69	0.89	-26
1000	0.54	-90	3.28	82	0.002	73	0.87	-29
1100	0.50	-96	3.05	75	0.002	78	0.86	-32
1200	0.48	-103	2.81	69	0.002	92	0.85	-34
1300	0.45	-109	2.71	62	0.002	108	0.84	-37
1400	0.43	-114	2.53	56	0.002	129	0.83	-40
1500	0.41	-120	2.37	51	0.002	147	0.81	-42
1600	0.39	-125	2.28	45	0.003	160	0.80	-45
1700	0.38	-132	2.12	39	0.004	167	0.79	-48
1800	0.37	-137	2.00	34	0.005	113	0.78	-51
1900	0.36	-141	1.88	28	0.006	116	0.77	-53
2000	0.35	-146	1.78	23	0.008	-2	0.76	-56
2100	0.34	-150	1.71	18	0.010	-61	0.75	-59
2200	0.33	-155	1.65	12	0.012	-120	0.74	-62
2300	0.34	-159	1.51	7	0.013	-120	0.73	-65
2400	0.33	-161	1.51	2	0.016	-61	0.72	-69
2500	0.34	-167	1.39	-5	0.019	58	0.71	-73
2600	0.34	-171	1.32	-10	0.022	176	0.70	-77
2700	0.34	-173	1.26	-15	0.025	175	0.69	-80
2800	0.34	-176	1.20	-20	0.028	174	0.68	-83
2900	0.34	-119	1.14	-25	0.032	172	0.67	-86
3000	0.34	118	1.09	-30	0.036	170	0.66	-90

Table 1. S-Parameters (V_{CC} = 2.7 V, 50 Ω System)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
100	0.88	-12	8.65	167	0.001	48	0.97	-3
200	0.85	-23	8.23	154	0.001	93	0.97	-6
300	0.80	-34	7.73	142	0.002	82	0.96	-10
400	0.75	-44	7.15	131	0.002	73	0.95	-12
500	0.67	-53	6.56	119	0.002	68	0.93	-15
600	0.62	-60	5.99	111	0.002	66	0.92	-18
700	0.57	-67	5.47	102	0.002	63	0.91	-21
800	0.53	-74	5.02	95	0.002	65	0.90	-23
900	0.48	-80	4.67	88	0.002	66	0.88	-26
1000	0.44	-86	4.31	81	0.002	69	0.87	-29
1100	0.41	-92	3.98	75	0.001	79	0.86	-31
1200	0.38	-97	3.71	69	0.001	101	0.85	-34
1300	0.36	-102	3.49	63	0.001	139	0.84	-36
1400	0.34	-107	3.26	58	0.002	102	0.82	-39
1500	0.32	-111	3.07	53	0.003	-4	0.81	-42
1600	0.30	-116	2.89	49	0.004	-119	0.80	-44
1700	0.29	-122	2.72	43	0.005	-115	0.79	-47
1800	0.28	-126	2.56	38	0.007	-113	0.78	-50
1900	0.28	-130	2.42	33	0.008	-113	0.77	-53
2000	0.27	-134	2.30	29	0.010	-112	0.76	-55
2100	0.26	-137	2.20	24	0.012	-113	0.75	-58
2200	0.25	-141	2.08	19	0.014	-114	0.74	-61
2300	0.26	-146	1.98	14	0.017	-115	0.73	-64
2400	0.25	-147	1.90	10	0.019	-117	0.72	-68
2500	0.26	-153	1.79	5	0.022	-119	0.71	-72
2600	0.26	-157	1.71	0	0.025	59	0.70	-75
2700	0.27	-159	1.63	-5	0.028	177	0.69	-78
2800	0.27	-162	1.55	-9	0.032	175	0.68	-81
2900	0.27	-164	1.48	-14	0.036	173	0.67	-85
3000	0.27	-167	1.41	-18	0.040	171	0.66	-88

Table 2. S-Parameters (V_{CC} = 4.0 V, 50 Ω System)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
100	0.85	-12	11.04	166	0.00	39	0.97	-3
200	0.82	-24	10.44	152	0.00	94	0.97	-6
300	0.77	-35	9.79	140	0.00	82	0.96	-9
400	0.70	-44	8.95	128	0.00	74	0.96	-12
500	0.62	-53	8.16	117	0.00	69	0.94	-15
600	0.57	-59	7.34	109	0.00	64	0.93	-18
700	0.52	-66	6.70	100	0.00	63	0.92	-20
800	0.48	-72	6.02	93	0.00	65	0.90	-23
900	0.43	-77	5.58	86	0.00	68	0.89	-26
1000	0.39	-82	5.11	80	0.00	71	0.88	-28
1100	0.36	-87	4.71	75	0.00	81	0.87	-31
1200	0.34	-92	4.33	69	0.00	114	0.86	-33
1300	0.32	-95	4.08	63	0.00	152	0.84	-36
1400	0.30	-99	3.80	59	0.00	114	0.83	-38
1500	0.28	-104	3.54	54	0.00	-118	0.82	-41
1600	0.26	-108	3.35	49	0.00	-114	0.81	-44
1700	0.25	-113	3.13	44	0.01	-111	0.80	-47
1800	0.25	-117	2.96	40	0.01	-110	0.79	-49
1900	0.24	-120	2.79	35	0.01	-111	0.78	-52
2000	0.23	-123	2.64	31	0.01	-111	0.77	-55
2100	0.22	-126	2.52	26	0.01	-112	0.76	-58
2200	0.22	-130	2.40	22	0.01	-114	0.75	-61
2300	0.23	-135	2.25	18	0.02	-115	0.74	-64
2400	0.23	-136	2.19	13	0.02	-117	0.73	-67
2500	0.23	-142	2.05	8	0.02	-119	0.72	-71
2600	0.23	-146	1.96	4	0.02	-1	0.71	-74
2700	0.24	-149	1.87	0	0.03	177	0.70	-77
2800	0.24	-151	1.78	-4	0.03	175	0.69	-80
2900	0.25	-153	1.70	-9	0.03	173	0.68	-84
3000	0.25	-156	1.62	-13	0.04	171	0.68	-87

Table 3. S-Parameters (V_{CC} = 5.0 V, 50 Ω System)

VCC (Volts)	f (GHz)	NFmin (dB)	Γ_0		RN (Ω)
			MAG	$\angle \phi$	
2.7	0.30	1.26	0.47	18	0.47
	0.50	1.48	0.42	29	0.44
	0.70	1.71	0.38	41	0.42
	0.90	1.96	0.34	53	0.41
	1.00	2.09	0.33	60	0.40
	1.50	2.82	0.27	94	0.38
	2.00	3.67	0.25	132	0.36
2.40	4.43	0.25	165	0.36	
4.0	0.30	1.27	0.37	18	0.37
	0.50	1.41	0.33	29	0.35
	0.70	1.56	0.30	40	0.33
	0.90	1.73	0.27	52	0.32
	1.00	1.82	0.25	59	0.31
	1.50	2.32	0.21	93	0.30
	2.00	2.91	0.20	133	0.29
2.40	3.44	0.21	168	0.29	
4.5	0.30	1.41	0.38	18	0.40
	0.50	1.53	0.34	26	0.38
	0.70	1.67	0.31	36	0.37
	0.90	1.83	0.27	46	0.36
	1.00	1.92	0.26	52	0.35
	1.50	2.42	0.20	85	0.33
	2.00	3.03	0.17	126	0.32
2.40	3.61	0.16	165	0.34	
5.0	0.30	1.36	0.33	18	0.35
	0.50	1.47	0.29	28	0.33
	0.70	1.60	0.26	40	0.32
	0.90	1.74	0.24	52	0.31
	1.00	1.82	0.22	58	0.30
	1.50	2.25	0.18	93	0.29
	2.00	2.78	0.17	133	0.28
2.40	3.27	0.18	170	0.29	

Table 4. Typical Noise Parameters (50 Ω System)



MOTOROLA

General Purpose RF Cascode Amplifier

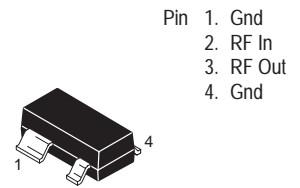
The MRFIC0916 is a cost-effective, high isolation cascode silicon monolithic amplifier in the industry standard SOT-143 surface mount package designed for general purpose RF applications. On chip bias circuitry sets the bias point while matching is accomplished off chip affording the maximum in application flexibility.

- Usable Frequency Range = 100 to 2500 MHz
- 18.5 dB typical gain at 850 MHz, $V_{CC} = 2.7\text{ V}$
- 2.3 dBm typical Output Power at 1.0 dB Gain Compression at 850 MHz, $V_{CC} = 2.7\text{ V}$
- 44 dB Typical Reverse Isolation at 850 MHz
- 5.6 mA Max Bias Current at $V_{CC} = 2.7\text{ V}$
- 2.7 to 5.0 V Supply

MRFIC0916

GENERAL PURPOSE RF CASCODE AMPLIFIER

SEMICONDUCTOR TECHNICAL DATA

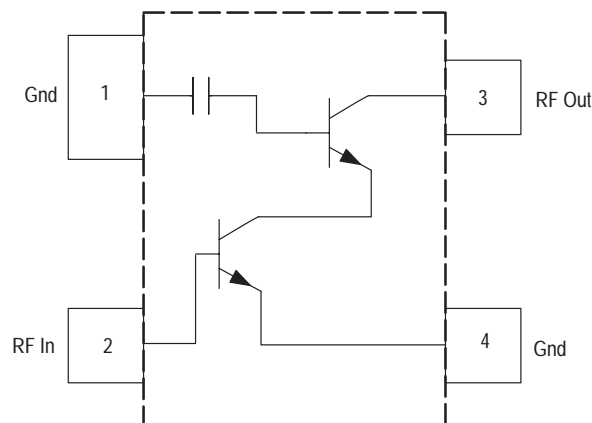


PLASTIC PACKAGE
CASE 318A
(SOT-143, Tape & Reel Only)

ORDERING INFORMATION

Device	Device Marking	Package
MRFIC0916T1	16	SOT-143

Functional Block Diagram



MRFIC0916

MAXIMUM RATINGS ($T_A = 25^\circ\text{C}$, unless otherwise noted)

Rating	Symbol	Value	Unit
Supply Voltage	V_{CC}	6.0	Vdc
RF Input Power	P_{RF}	10	dBm
Power Dissipation	P_{DIS}	100	mW
Supply Current	I_{CC}	20	mA
Thermal Resistance, Junction to Case	$R_{\theta JC}$	250	C/W
Storage Temperature Range	T_{stg}	-65 to 150	$^\circ\text{C}$
Operating Case Temperature	T_C	-40 to 100	$^\circ\text{C}$

NOTE: Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
RF Frequency	f_{RF}	100	-	2500	MHz
Supply Voltage	V_{CC}	2.7	-	5.0	Vdc

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7\text{ V}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 850\text{ MHz}$, Tested in Circuit Shown in Figure 1, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Small Signal Gain		16.5	18.5	20.5	dB
Noise Figure		-	1.9	-	dB
Power Output at 1.0 dB Gaim Compression		0	2.3	-	dBm
Output 3rd Order Intercept Point		-	11	-	dBm
Reverse Isolation		-	44	-	dB
Supply Current		3.8	4.7	5.6	mA

Figure 1. 850 MHz Applications Circuit Configuration

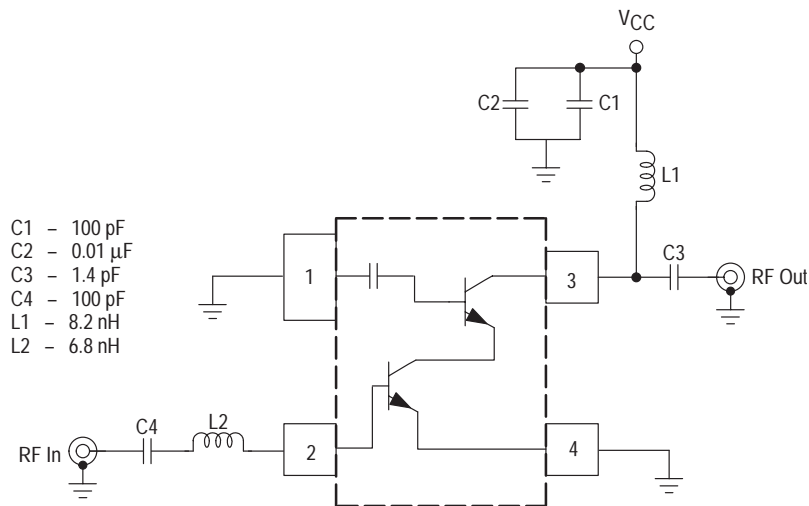


Figure 2. GU_{max} versus Frequency

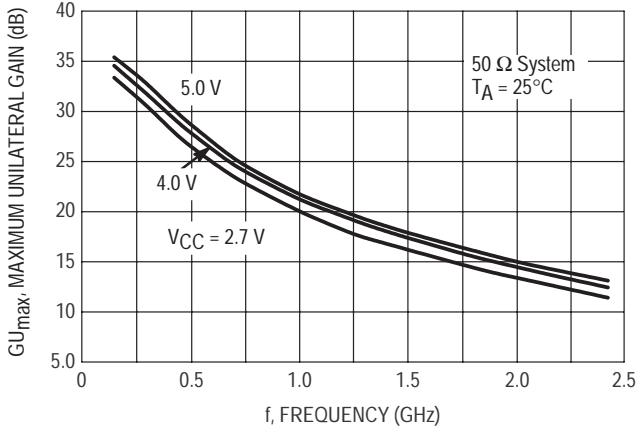


Figure 3. Output Power versus Input Power

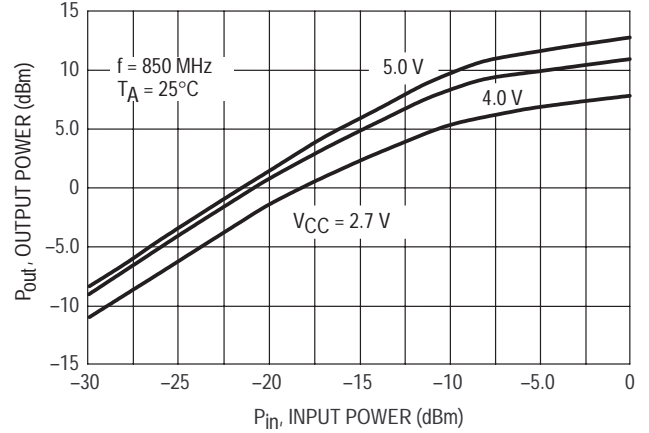
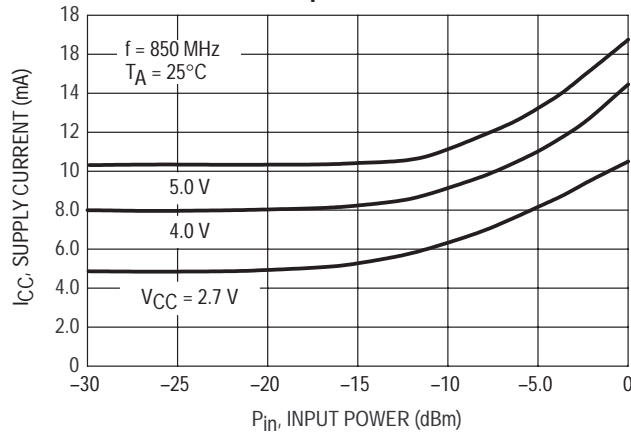


Figure 4. Supply Current versus Input Power



MRFIC0916

Table 1. Scattering Parameters
($V_{CC} = 2.7\text{ V}$, $50\ \Omega$ System)

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	∠φ	S ₂₁	∠φ	S ₁₂	∠φ	S ₂₂	∠φ
100	0.806	-17.01	12.03	162.32	0.001	-0.14	0.956	-4.69
200	0.765	-33.28	11.18	145.74	0.001	71.58	0.948	-8.69
300	0.713	-47.99	10.18	130.99	0.002	69.67	0.945	-13.23
400	0.652	-61.35	9.06	118.01	0.003	64.61	0.930	-17.35
500	0.574	-70.94	8.06	106.50	0.003	62.93	0.904	-20.85
600	0.533	-81.00	7.09	96.50	0.003	61.94	0.891	-24.71
700	0.493	-89.33	6.36	87.60	0.003	63.16	0.875	-28.18
800	0.469	-97.65	5.62	79.57	0.003	66.33	0.857	-31.89
900	0.432	-103.64	5.16	72.38	0.002	80.79	0.845	-35.21
1000	0.409	-110.68	4.70	65.39	0.002	100.33	0.831	-38.86
1100	0.396	-116.17	4.29	58.75	0.002	127.72	0.815	-42.52
1200	0.383	-122.20	3.91	52.55	0.003	152.57	0.799	-45.77
1300	0.373	-126.00	3.66	46.34	0.004	164.39	0.789	-49.49
1400	0.369	-131.29	3.38	40.61	0.006	169.63	0.776	-53.23
1500	0.366	-134.46	3.14	35.29	0.008	172.81	0.762	-56.86
1600	0.366	-140.07	2.93	29.63	0.011	172.47	0.751	-60.74
1700	0.364	-143.07	2.75	23.86	0.013	172.79	0.738	-64.66
1800	0.368	-147.48	2.58	18.42	0.016	171.54	0.727	-68.29
1900	0.377	-148.91	2.42	13.15	0.020	170.15	0.719	-72.29
2000	0.381	-153.42	2.27	7.58	0.023	167.89	0.707	-76.58
2100	0.394	-155.23	2.15	2.46	0.027	165.86	0.695	-80.50
2200	0.396	-158.91	2.03	-3.00	0.032	163.46	0.685	-84.85
2300	0.416	-160.43	1.90	-8.32	0.037	161.00	0.672	-88.93
2400	0.424	-162.98	1.81	-13.30	0.042	158.00	0.662	-93.38
2500	0.434	-166.35	1.68	-18.45	0.047	155.58	0.654	-97.89

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Table 2. Scattering Parameters
($V_{CC} = 4\text{ V}$, $50\ \Omega$ System)

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	∠φ	S ₂₁	∠φ	S ₁₂	∠φ	S ₂₂	∠φ
100	0.744	-17.43	16.979	160.38	0.001	-2.89	0.955	-4.40
200	0.691	-33.58	15.442	142.46	0.001	83.36	0.950	-8.33
300	0.627	-47.53	13.633	127.28	0.002	76.39	0.946	-12.79
400	0.558	-59.50	11.851	114.52	0.002	70.12	0.931	-16.75
500	0.482	-67.02	10.284	103.51	0.002	67.02	0.907	-20.11
600	0.440	-75.50	8.957	94.12	0.002	66.00	0.895	-23.85
700	0.401	-81.87	7.930	85.95	0.002	68.71	0.880	-27.22
800	0.377	-88.89	7.003	78.57	0.002	73.50	0.863	-30.83
900	0.348	-93.11	6.348	71.96	0.002	90.55	0.852	-34.06
1000	0.328	-98.88	5.747	65.59	0.002	113.74	0.838	-37.62
1100	0.317	-103.27	5.223	59.57	0.002	146.45	0.822	-41.18
1200	0.306	-108.54	4.765	53.98	0.003	165.49	0.808	-44.34
1300	0.301	-111.30	4.425	48.39	0.004	175.51	0.798	-47.95
1400	0.297	-116.30	4.082	43.18	0.006	177.46	0.785	-51.59
1500	0.298	-118.89	3.790	38.32	0.008	179.45	0.771	-55.11
1600	0.298	-124.58	3.531	33.13	0.011	178.69	0.760	-58.88
1700	0.301	-127.19	3.300	28.02	0.014	178.02	0.748	-62.66
1800	0.305	-131.73	3.093	23.10	0.016	176.25	0.737	-66.16
1900	0.319	-133.16	2.901	18.34	0.020	174.44	0.729	-70.03
2000	0.324	-137.94	2.724	13.33	0.023	172.03	0.717	-74.16
2100	0.339	-140.09	2.575	8.67	0.027	169.82	0.706	-77.92
2200	0.342	-143.98	2.434	3.79	0.032	166.99	0.696	-82.07
2300	0.367	-146.00	2.278	-0.98	0.036	164.37	0.684	-86.04
2400	0.375	-148.75	2.166	-5.56	0.042	161.35	0.674	-90.25
2500	0.387	-152.75	2.020	-10.12	0.046	158.69	0.666	-94.64

MRFIC0916

Table 3. Scattering Parameters
($V_{CC} = 5\text{ V}$, $50\ \Omega$ System)

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	∠φ	S ₂₁	∠φ	S ₁₂	∠φ	S ₂₂	∠φ
100	0.707	-17.56	20.04	159.03	0.001	-7.95	0.954	-4.25
200	0.648	-33.40	17.93	140.29	0.001	86.24	0.950	-8.15
300	0.579	-46.60	15.53	124.94	0.002	78.79	0.946	-12.54
400	0.509	-57.44	13.31	112.38	0.002	72.27	0.931	-16.42
500	0.438	-63.51	11.40	101.70	0.002	69.34	0.908	-19.68
600	0.397	-70.90	9.87	92.70	0.002	69.55	0.896	-23.35
700	0.363	-76.05	8.69	84.92	0.002	71.59	0.882	-26.64
800	0.340	-82.18	7.67	77.89	0.002	79.44	0.865	-30.20
900	0.316	-85.44	6.91	71.60	0.002	95.59	0.855	-33.36
1000	0.298	-90.52	6.24	65.56	0.001	121.55	0.841	-36.86
1100	0.290	-94.44	5.67	59.82	0.002	152.13	0.826	-40.37
1200	0.280	-99.17	5.17	54.53	0.003	169.84	0.811	-43.48
1300	0.277	-101.65	4.79	49.25	0.005	177.80	0.802	-47.02
1400	0.274	-106.49	4.42	44.27	0.006	-179.84	0.790	-50.59
1500	0.278	-109.07	4.10	39.65	0.008	-179.19	0.776	-54.04
1600	0.276	-114.88	3.82	34.68	0.011	-179.68	0.765	-57.73
1700	0.281	-117.46	3.56	29.88	0.013	179.47	0.753	-61.43
1800	0.285	-122.11	3.34	25.21	0.016	177.73	0.742	-64.85
1900	0.300	-123.94	3.14	20.70	0.019	175.80	0.734	-68.66
2000	0.305	-128.93	2.95	15.91	0.023	173.47	0.723	-72.71
2100	0.322	-131.48	2.78	11.50	0.027	171.04	0.712	-76.37
2200	0.324	-135.50	2.63	6.84	0.031	168.25	0.703	-80.42
2300	0.351	-138.04	2.47	2.33	0.036	165.47	0.691	-84.31
2400	0.358	-140.88	2.34	-2.05	0.041	162.71	0.681	-88.42
2500	0.371	-145.28	2.19	-6.40	0.046	160.19	0.674	-92.74

MRFIC0916

Table 4. Typical Noise Parameters
(50 Ω System)

V _{CC} (Volts)	f (GHz)	NF _{min} (dB)	Γ_0		R _N (Ω)
			MAG	$\angle \phi$	
2.7	0.3	1.48	0.08	-145	0.18
	0.5	1.48	0.11	-52	0.23
	0.7	1.52	0.14	27	0.25
	0.9	1.61	0.17	93	0.21
	1.0	1.67	0.19	121	0.18
	1.5	2.16	0.26	-152	0.17
	2.0	2.94	0.33	-150	0.22
	2.4	3.78	0.38	150	0.26
4.0	0.3	1.66	0.07	114	0.24
	0.5	1.62	0.09	118	0.21
	0.7	1.62	0.12	124	0.19
	0.9	1.67	0.14	130	0.18
	1.0	1.71	0.15	133	0.17
	1.5	2.08	0.21	152	0.17
	2.0	2.72	0.27	175	0.19
	2.4	3.44	0.32	-164	0.232
4.5	0.3	1.85	0.14	149	0.20
	0.5	1.74	0.14	146	0.18
	0.7	1.69	0.14	144	0.17
	0.9	1.69	0.15	144	0.17
	1.0	1.71	0.16	145	0.17
	1.5	2.04	0.20	155	0.18
	2.0	2.71	0.26	175	0.20
	2.4	3.50	0.33	-161	0.24
5.0	0.3	1.83	0.10	133	0.27
	0.5	1.76	0.11	136	0.23
	0.7	1.73	0.13	141	0.20
	0.9	1.75	0.14	146	0.18
	1.0	1.78	0.15	148	0.17
	1.5	2.10	0.19	163	0.17
	2.0	2.71	0.25	-179	0.20
	2.4	3.42	0.30	-163	0.25



MOTOROLA

3.6 V GSM GaAs Integrated Power Amplifier

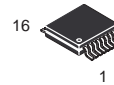
The MRFIC0919 is a single supply, RF power amplifier designed for the 2.0 W GSM900 handheld radio. The negative power supply is generated inside the chip using RF rectification, which avoids any spurious signal. A built in priority switch is provided to prevent Drain Voltage being applied on the RF lineup if not properly biased by the Negative Voltage. The device is packaged in the TSSOP-16EP package, with exposed backside pad, which allows excellent electrical and thermal performance through a solderable contact.

- Target 3.6 V Characteristics:
 - RF Input Power: 3.0 dBm
 - RF Output Power: 35.3 dBm Typical
 - Efficiency: 53% Typical
- Single Positive Supply Solution
- Negative Voltage Generator
- Positive Step-up Voltage Generator
- V_{SS} Check Switch for Gate-Drain Priority

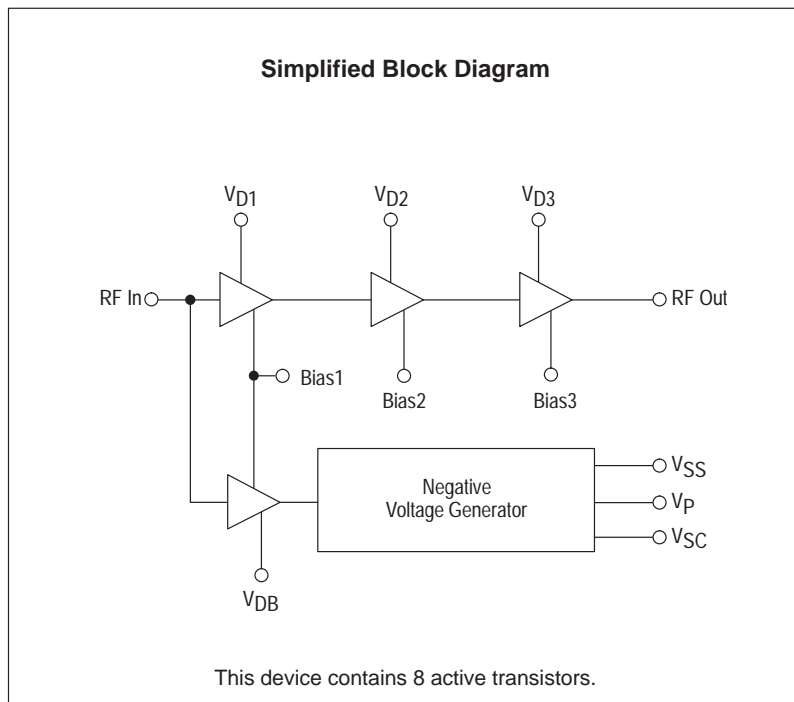
MRFIC0919

GSM 880 – 915 MHz INTEGRATED POWER AMPLIFIER

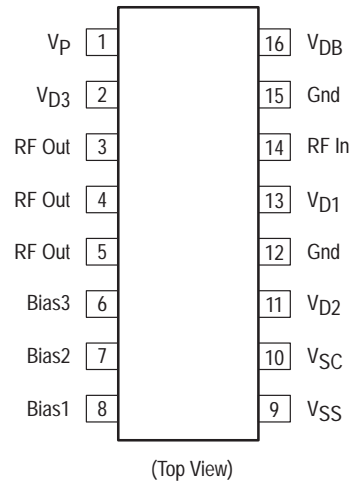
SEMICONDUCTOR TECHNICAL DATA



PLASTIC PACKAGE
CASE 948L
(TSSOP-16EP, Tape and Reel Only)



PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC0919R2	T _A = -40 to 85°C	TSSOP-16EP

MRFIC0919

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Supply Voltage	$V_{D1, 2, 3}$	6.0	V
RF Input Power	P_{in}	12	dBm
RF Output Power	P_{out}	38	dBm
Operating Case Temperature Range	T_C	-40 to 85	°C
Storage Temperature Range	T_{stg}	-55 to 150	°C

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions or Electrical Characteristics tables.
 2. ESD (electrostatic discharge) immunity meets Human Body Model (HBM) ≤ 250 V and Machine Model (MM) ≤ 60 V. This device is rated Moisture Sensitivity Level (MSL) 4. Additional ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Voltage	$V_{DB}, V_{D1, 2, 3}$	-	3.0 to 5.5	-	Vdc
Input Power	P_{in}	-	3.0 to 8.0	-	dBm

ELECTRICAL CHARACTERISTICS ($V_{DB} = 3.6$ V, $V_{D1, 2, 3} = 3.6$ V, $P_{in} = 3.0$ dBm, Peak measurement at 12.5% duty cycle, 4.6 ms Period, $T_A = 25^\circ\text{C}$, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	880	-	915	MHz
Output Power	P_{out}	34.5	35.3	-	dBm
Power Added Efficiency	PAE	45	53	-	%
Output Power at Low Voltage ($V_{D1, 2, 3} = 3.0$ V)	P_{out}	33	33.7	-	dBm
Harmonic Output					dBc
$2f_0$	-	-	40	35	
$\geq 3f_0$	-	-	45	40	
Input Return Loss	S11	-	12	-	dB
Output Power Isolation ($P_{in} = 8.0$ dBm, $V_{DB} = 3.0$ V, $V_{D1, 2\&3} = 0$ V)	P_{off}	-	-32	-	dBm
Noise Power in Rx band 925 to 960 MHz (100 kHz measurement bandwidth)	NP	-	-90	-	dBm
Negative Voltage ($P_{in} = 3.0$ dBm, $V_{DB} = 3.0$ V, $V_{D1, 2\&3} = 0$ V)	V_{SS}	-4.85	-	-	V
Negative Voltage Setting Time ($P_{in} = 3.0$ dBm, V_{DB} stepped from 0 to 3.0 V)	T_s	-	0.7	-	μs
Stability–Spurious Output ($P_{out} = 5.0$ to 35 dBm, Load VSWR 6:1 all phase angles, source VSWR = 3:1, at any phase angle, Adjust $V_{D1, 2\&3}$ for specified power)	P_{spur}	-	-	-60	dBc
Load Mismatch Stress ($P_{out} = 5.0$ to 35 dBm, Load VSWR = 10:1 all phase angles, 5 seconds, Adjust $V_{D1, 2\&3}$ for specified power)	No Degradation in Output Power Before & After Test				
Positive Voltage ($P_{in} = 3.0$ dBm, $V_{DB} = 3.0$ V)	V_P	6.0	-	-	V

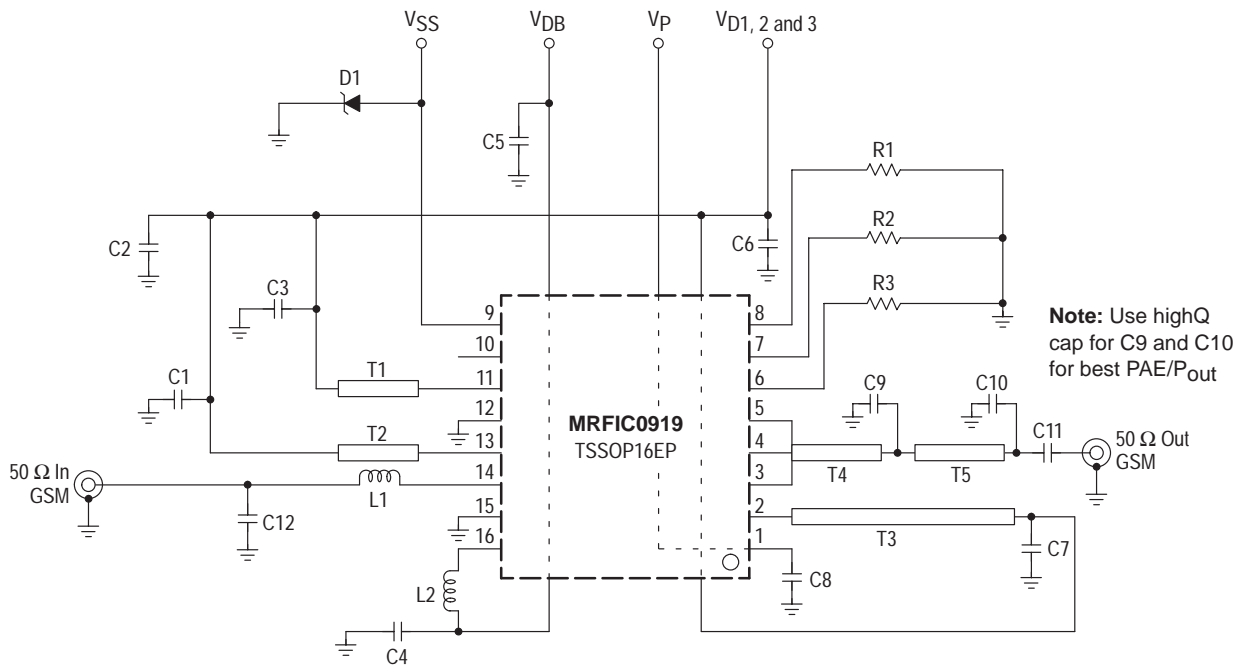
MRFIC0919

Table 1. Optimum Loads Derived from Circuit Characterization

f MHz	Z _{in} OHMS		Z _{OL} [*] OHMS	
	R	jX	R	jX
880	9.83	-75.84	1.79	2.34
885	9.88	-76.75	1.78	2.46
890	9.83	-77.65	1.76	2.57
895	9.82	-78.60	1.75	2.67
900	9.82	-79.50	1.74	2.80
905	9.79	-80.35	1.73	2.90
910	9.78	-81.23	1.71	3.00
915	9.75	-82.18	1.70	3.13

Z_{in} represents the input impedance of the device.
Z_{OL}^{*} represents the conjugate of the optimum output load to present to the device.

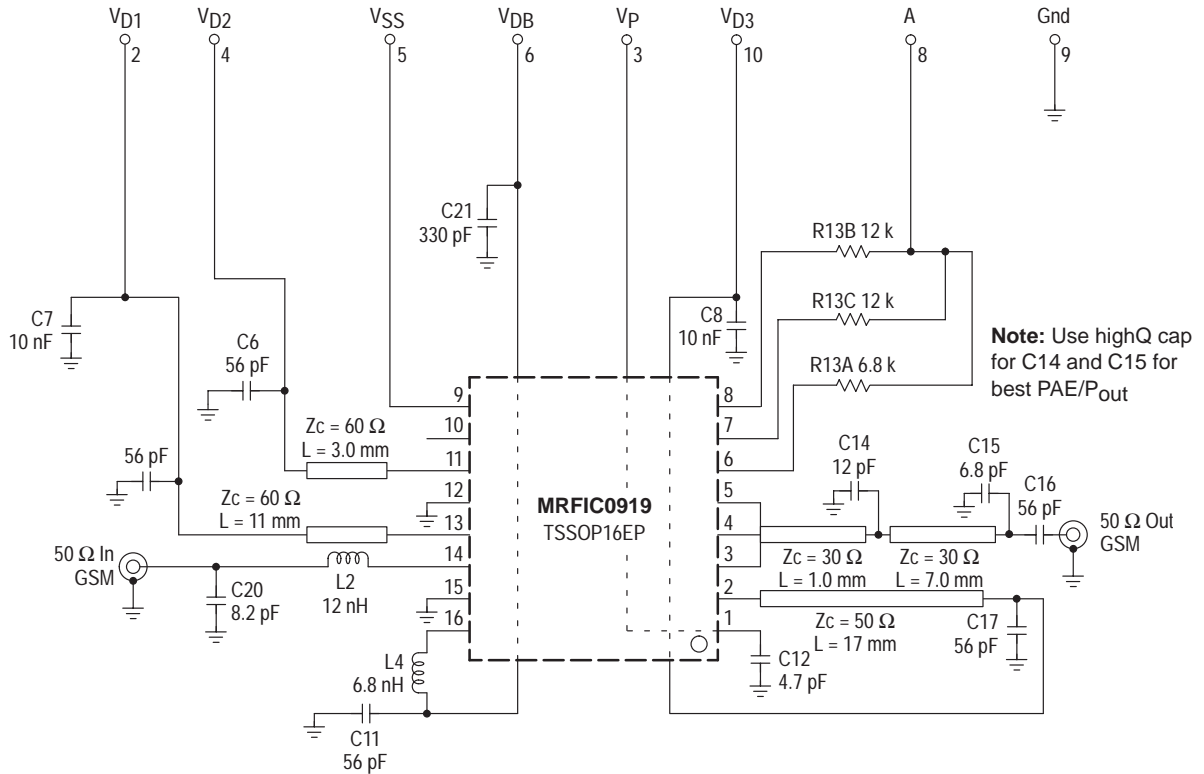
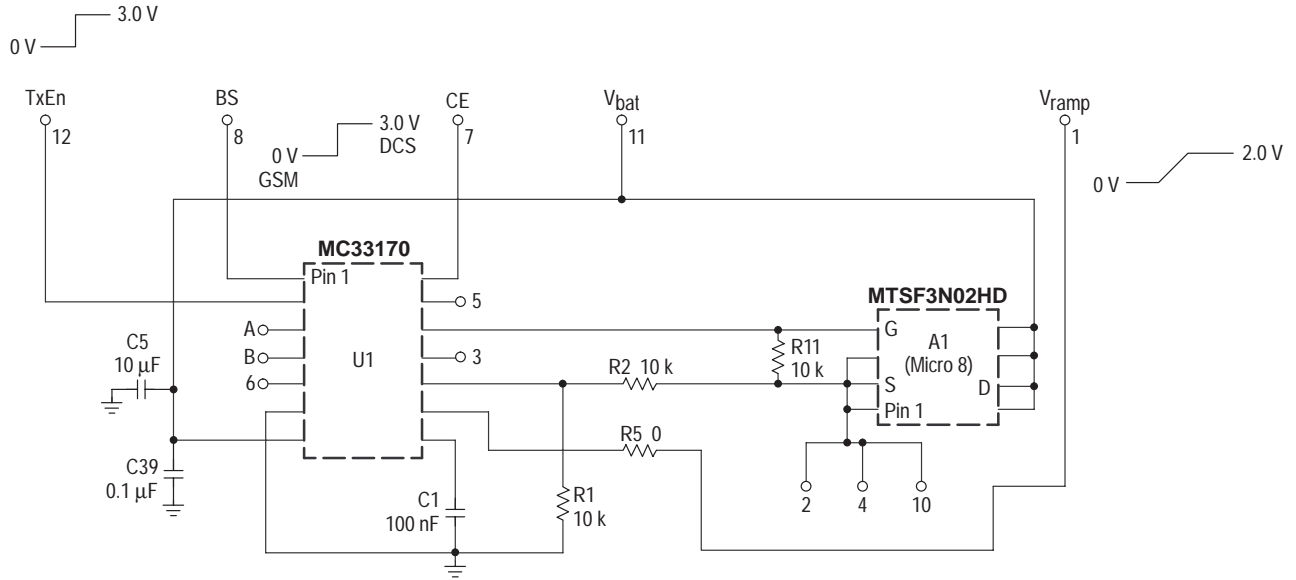
Figure 1. Reference Circuit



C1, C3, C4, C7, C11	56 pF	R1, R2	12 k
C2, C6	10 nF	R3	6.8 k
C5	330 pF	T1	60 Ω Microstrip Line, L = 3.0 mm
C8	4.7 pF	T2	60 Ω Microstrip Line, L = 11 mm
C9	12 pF	T3	50 Ω Microstrip Line, L = 17 mm
C10	6.8 pF	T4	30 Ω Microstrip Line, L = 1.0 mm
C12	8.2 pF	T5	30 Ω Microstrip Line, L = 7.0 mm
L1	12 nH		
L2	6.8 nH		
D1	Zener 5.1 V	MMSZ4689T1	

MRFIC0919

Figure 2. 3.6 V GSM IPA MRFIC0919 Application Circuit



Note: I/O labels and pin numbers refer to demoboard connector pin out.

MRFIC0919

Figure 3. 3.6 V GSM & DCS IPA Dual-Band Application Circuit with Companion Chip & NMOS Switch

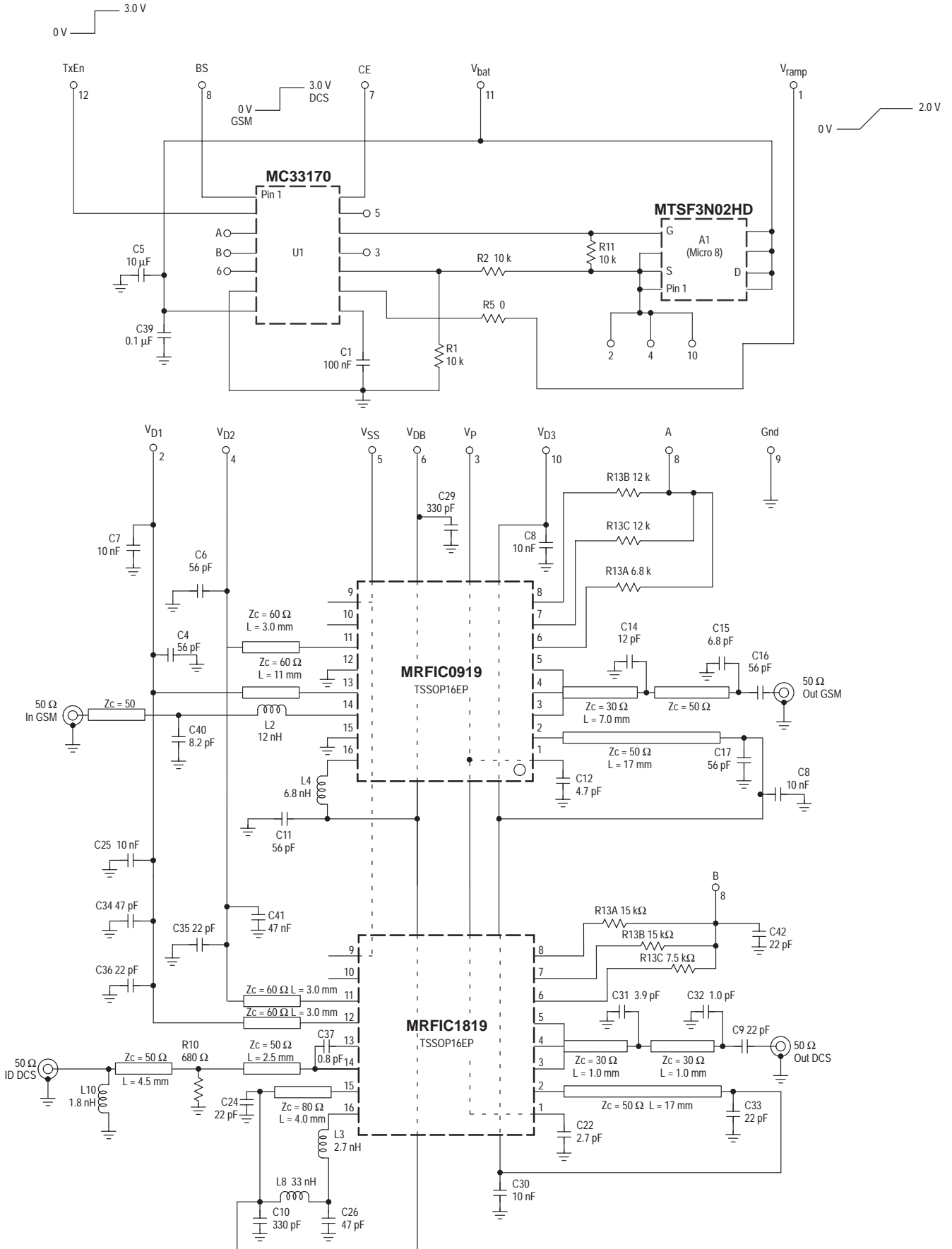


Figure 4. Output Power versus Frequency

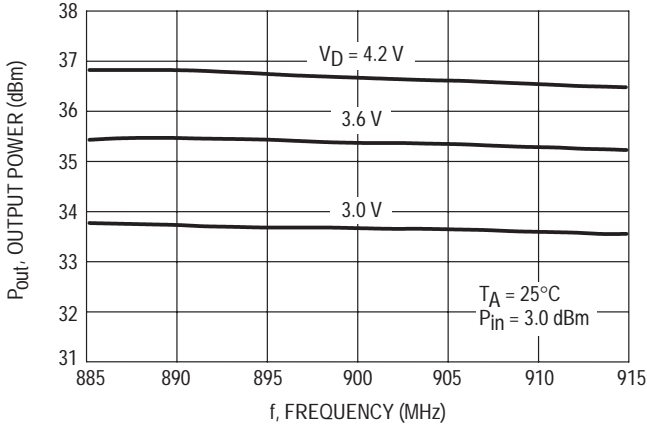


Figure 5. Power Added Efficiency versus Frequency

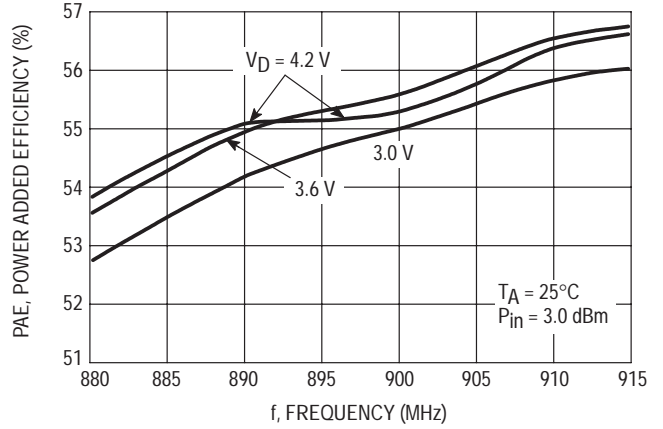


Figure 6. Output Power versus Frequency

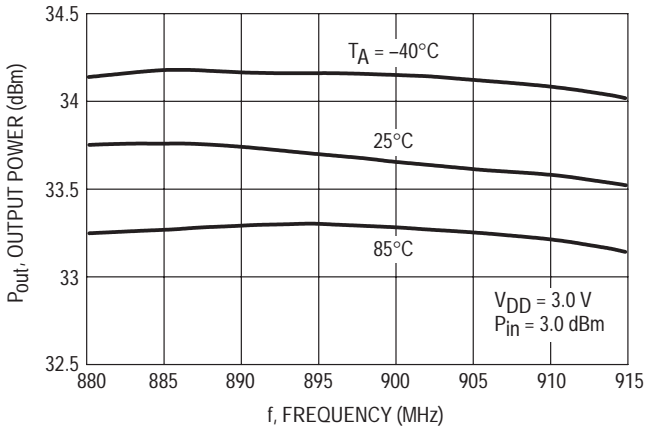


Figure 7. Output Power versus Frequency

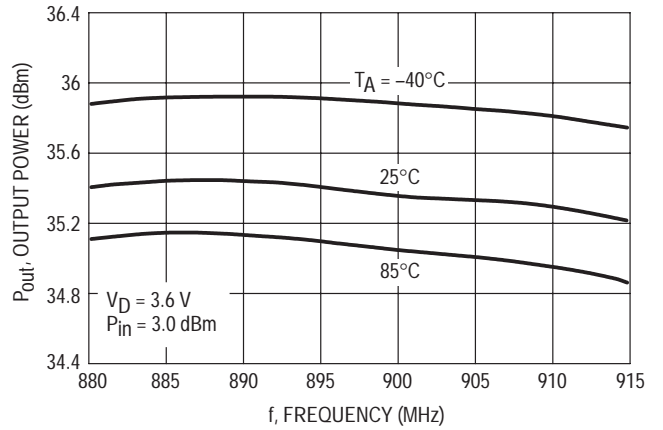


Figure 8. Output Power versus Frequency

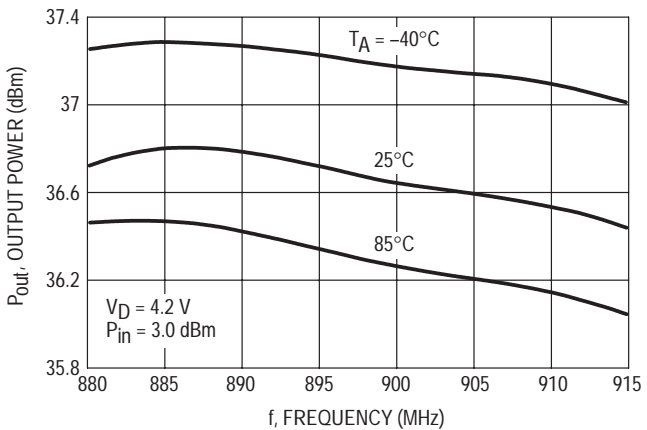


Figure 9. Power Added Efficiency versus Frequency

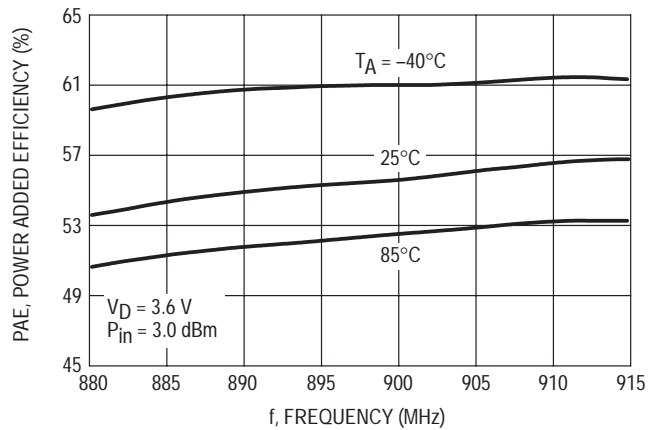


Figure 10. Output Power versus Drain Voltage

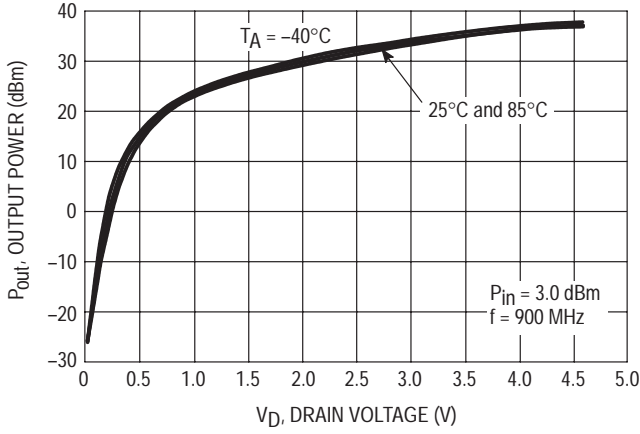


Figure 11. Power Added Efficiency versus Drain Voltage

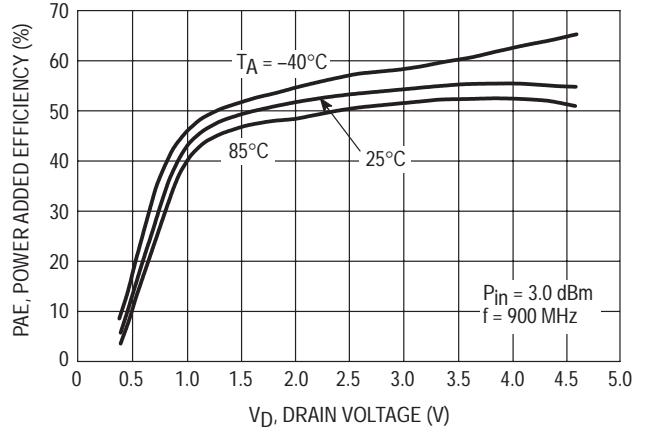


Figure 12. Positive Voltage Generator Output versus Drain Voltage

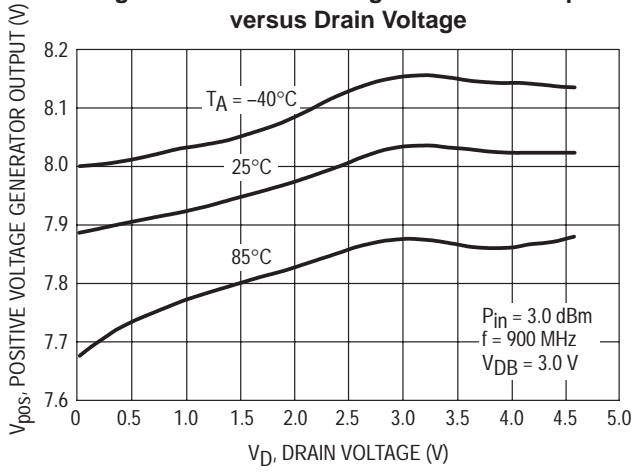


Figure 13. Positive Voltage Output versus Frequency

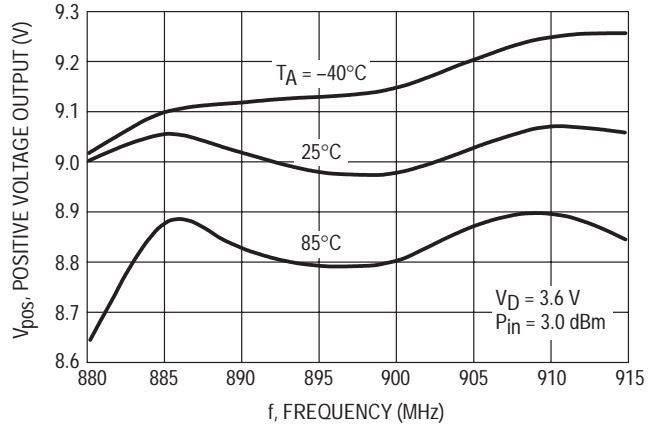


Figure 14. Second Harmonics versus Drain Voltage

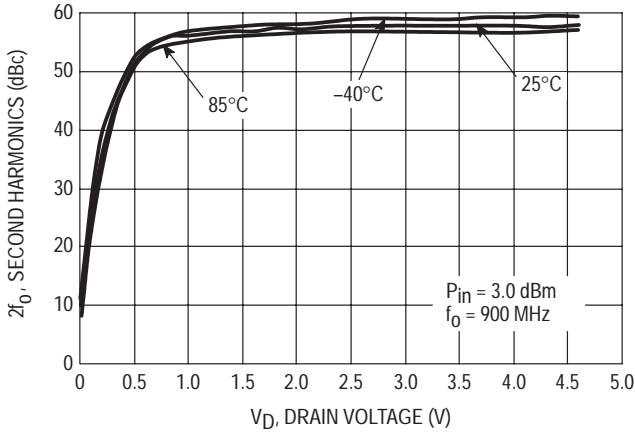
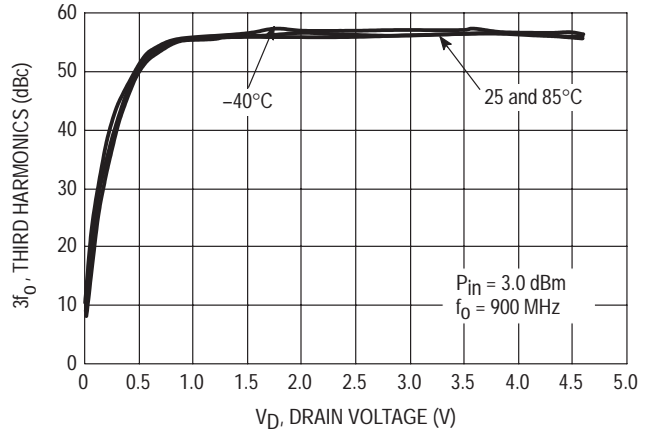


Figure 15. Third Harmonics versus Drain Voltage



MRFIC0919

APPLICATIONS INFORMATION

Design Philosophy

The MRFIC0919 is a high performance three stage GaAs IPA (Integrated Power Amplifier) designed for GSM handheld radios (880 to 915 MHz frequency band). With a 3.6 V battery supply, it delivers typically 35.3 dBm of Output Power with 53% Power Added Efficiency.

It features an internal Negative Voltage Generator based on RF rectification of the input carrier after its amplification by a dedicated buffer stage (see Internal Block Diagram). This method eliminates spurs found on the Output signal when using DC/DC converter type negative voltage generators, either on or off chip. The buffer also generates a step-up positive voltage which can be used to drive a N-MOS drain switch.

The RF input power is split internally to the 3 stage RF line-up (Q1,Q2 and Q3) and the Buffer. This arrangement allows separate operation of Voltage Generation and Power Amplification for maximum flexibility.

External Circuit Considerations

The MRFIC0919 can be tuned by changing the values and/or positions of the appropriate external components (see Figure 1. Reference Circuit). While tuning the RF line-up, it is recommended to apply external negative supply in order to prevent any damage to the power amplifier stages. Poor tuning on the input may not provide enough RF power to operate the negative voltage generator properly.

Input matching is a shunt-C, series-L low-pass structure and should be optimized at the rated RF Input power (e.g., 3.0 dBm). Since the Input line feeds both 1st stage and buffer, Input matching should be iterated with Buffer and Q1 drain matching. Note that a DC blocking capacitor is included on chip.

Buffer drain is supplied and matched through a discrete chip inductor. Its value is tuned to get the maximum output from voltage generator.

The step-up positive voltage available at Pin 1 is both decoupled and maximized by a small shunt capacitor. This positive voltage which is approximately twice the buffer drain voltage can be used to drive a N-MOS drain switch for best performance.

Q1 drain is supplied and matched through a printed microstrip line that could be replaced by a discrete chip inductor as well. Its length (or equivalent inductor value) is tuned by sliding the RF decoupling capacitor along to get the maximum gain on the first stage. Make sure when laying out the PCB to put enough ground pads and vias close to the microstrip lines to help for this fine tuning.

Q2 is supplied through a printed microstrip line that contributes also to the interstage matching in order to provide optimum drive to the final stage. The line length is very small so replacing it with a discrete inductor is not practical.

Q3 drain is fed via a printed line that must handle the high supply current of that stage (2.0 to 3.0 Amp peak) without significant voltage drop. This line can be buried in an inner layer to save PCB space or be a discrete RF choke.

Output matching is accomplished with a two stage low-pass network. Easy implementation is achieved with shunt capacitors mounted along a 30 Ω microstrip transmission line. Value and position are chosen to reach a load line of 1.8 Ω while conjugating the device output parasitics. The network must also properly terminate the

second and third harmonic to optimize efficiency and reduce harmonic level. Use of high Q capacitor for the output matching circuit is recommended in order to get the best Output Power and Efficiency performance.

Biasing Considerations

The internally generated negative voltage is clamped by an external Zener diode in order to eliminate variation linked to Input power or Buffer supply. This negative voltage is used by three independent bias circuits to set the proper quiescent current of all stages. Each bias circuit is equivalent to a current source sinking its value from the bias pin. When the bias pins are grounded, nominal quiescent current and operating point of each RF stage are selected.

Q1 and Buffer share the Bias1 (0.25 mA) while Q2 and Q3 have dedicated Bias2 (0.25 mA) and Bias3 (0.5 mA) respectively. It is also possible to reference those bias pins to higher voltage than Gnd by using a series resistor that drops the equivalent voltage.

If those pins are left open, the corresponding stages are pinched-off. Thus the bias pins can be used as a means to select the MRFIC0919 or MRFIC1819 in a dual band configuration. The MRFIC1819 is the partner device to the MRFIC0919 and is designed for DCS1800/PCS1900 applications.

Table 2. Pin Function Description

Pin	Symbol	Description
1	V _P	Positive voltage output
2	V _{D3}	Third stage drain supply
3	RF Out	RF output
4	RF Out	RF output
5	RF Out	RF output
6	Bias3	Third stage bias
7	Bias2	Second stage bias
8	Bias1	Buffer and first stage bias
9	V _{SS}	Negative voltage output
10	V _{SC}	Negative voltage check
11	V _{D2}	Second stage drain supply
12	Gnd	Tied to ground externally
13	V _{D1}	First stage drain supply
14	RF In	RF input
15	Gnd	Tied to ground externally
16	V _{DB}	Buffer stage drain supply

V_{SC} is an open drain internal FET switch which is biased through the negative voltage. Consequently, this pin is high impedance when negative voltage is okay and low impedance (about 40 Ω) when negative voltage is missing.

Operation Procedure

The MRFIC0919 is a standard MESFET GaAs Power Amplifier, presence of a negative voltage to bias the RF line-up is essential in order to avoid any damage to the parts. Due to the fact that the negative voltage is generated through rectification of the RF input signal, a minimum input power

level is needed for correct operation of the demoboard. The following procedure will guaranty safe operation for doing the RF measurements.

Note: make sure that Bias1 (Pin 8) is connected to ground or will have equivalent potential for nominal biasing of Buffer stage.

1. Apply RF input power (RF In) >3.0 dBm.
2. Apply $V_{DB} = 3.0$ to 5.0 V.
3. Check that V_{SS} reaches approximately -5.1 V (settling of the negative voltage).
4. Apply $V_{D1,2\&3} = 3.0$ to 5.5 V.
5. Measure RF output power and relevant parameters.

Proceed in the reverse order to switch off the Power Amplifier.

For linear operation, an external negative voltage will have to be supplied to the V_{SS} pin to maintain initial quiescent operating conditions of the FET amplifiers since the RF input will not provide sufficient voltage to operate the negative voltage generator. When using an external negative voltage supply, supply voltage to V_{DB} (Pin 16) would no longer be required.

Control Considerations

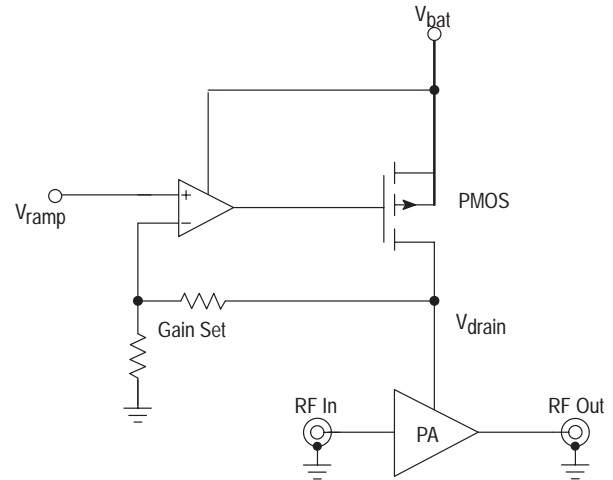
MRFIC0919 application uses the drain control technique developed for our previous range of GaAs IPAs (refer to application note AN1599). This method relies on the fact that for an RF amplifier operating in saturation mode, the RF output power is proportional to the square of the Amplifier drain voltage: $P_{Out}(Watt)=k \cdot V_D(Volt) \cdot V_D(Volt)$.

In the proposed application circuit (see Figure 2), a PMOS FET is used to switch the IPA drain and vary the drain supply voltage from 0 to battery voltage. As the PMOS FET has a non linear behavior, an OpAmp is included in the application. This OpAmp is linearizing the PMOS by sensing its drain output and gives a true linear relationship between the Control voltage and the RF output voltage.

The obtained power control transfer function is so linear and repeatable than it can be used to predict the output power within a dynamic range of 25 to 30 dB over frequency and temperature. This so called "open-loop" arrangement eliminates the need for coupler and detector required for the classical but complex closed-loop control and consequently reduces the Insertion Loss from Power Amplifier to the Antenna.

The block diagram (Figure 16) shows the principle of operation as implemented in the application circuit of Figure 2. The OpAmp is connected as an inverter to compensate the negative gain of the PMOS switch.

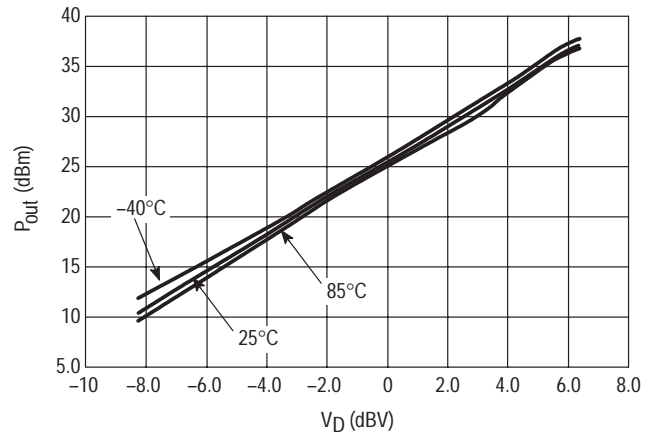
Figure 16. Drain Control through PMOS Switch



NOTE: The positive voltage generated by the Buffer stage can be used to supply the OpAmp and make it possible to drive a NMOS switch as a voltage follower. Doing so, the main advantage is to have a lower R_{dson} switch and better intrinsic linearity.

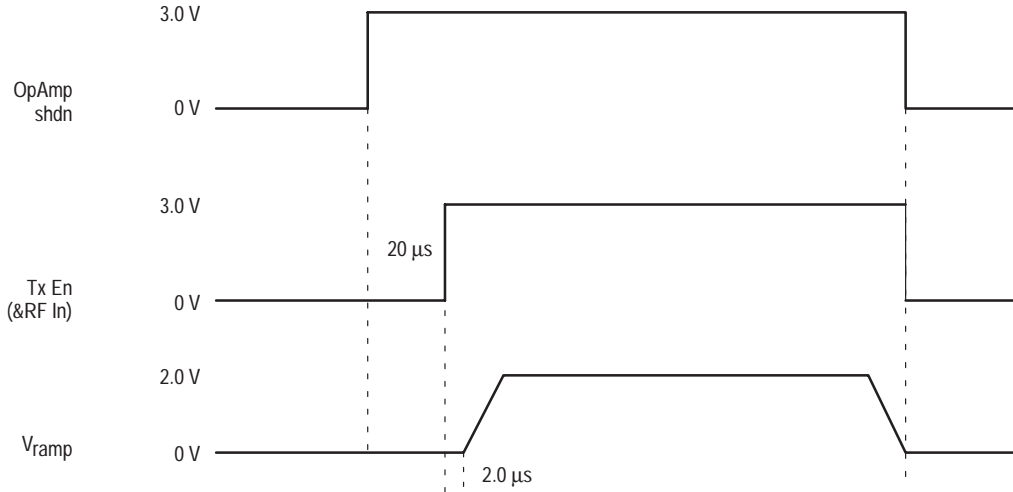
The following plot illustrates the "open-loop" performance as far as temperature stability. The measured datas are displayed in a log-scale in order to have a good representation of both the dynamic and the linearity of control. The variation of P_{Out} accross the frequency band are also very small (less than 1.0 dB ripple) and are kept to that small amount when controlling P_{Out} through the Drain voltage.

Figure 17. Pout versus VD



MRFIC0919

Figure 18. Timing Guide



Burst mode

Use Figure 18 as a guide line to perform burst mode measurements with the complete application circuit of Figure 2. Notice that the V_{SC} pin is connected to V_{ramp} (through a resistor) and act as a pull down when negative voltage is missing so that drain voltage is not applied to the RF line-up.

– Bursting the OpAmp with its Pin 8 (shdn) is not mandatory during a call as the OpAmp current consumption is very small (1.0 to 2.0 mA). This pin is mainly used for the idle mode of the radio. In any case, the wake-up time of the OpAmp is very short.

– V_{ramp} can be applied soon after Tx EN since the internal negative voltage generator settles in less than 2.0 μs.

– Tx EN signal can be used to switch the input power (using a driver or attenuator) in order to provide higher isolation for on/off burst dynamic.

References (Motorola application notes)

AN1599 – Power Control with the MRFIC0913 GaAs Integrated Power Amplifier and MC33169 Support IC.

AN1602 – 3.6 V and 4.8 V GSM/DCS1800 Dual Band PA Application with DECT capability Using Standard Motorola RFIC's.



MOTOROLA

900 MHz GaAs Low Noise Amplifier with Gain Control

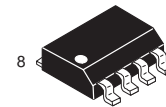
Designed primarily for use in 900 MHz wireless communication systems such as GSM, AMPS, and Industrial, Scientific, and Medical (ISM) band applications. The MRFIC0930 is a two-stage low noise amplifier with an integrated step attenuator and is packaged in a low-cost SO-8 package. The MRFIC0930DM is packaged in the smaller Micro-8 package. The attenuator is controlled by a V_{gain} Pin. The LNA can be turned off during transmit mode to save current by using the Rx Enable Pin. The amplifier can be matched to optimize gain or noise figure with simple off-chip input matching.

- Usable Frequency Range = 800 to 1000 MHz
- 19 dB Typ Gain
- Gain Attenuation = 18 dB (Typ)
- 1.7 dB Typ Noise Figure
- Simple Off-chip Matching for Maximum Gain/Noise Figure Flexibility
- High Reverse Isolation = 41 dB (Typ)
- Low Power Consumption = 24 mW (Typ)
- Single Bias Supply = 2.7 to 4.5 V
- Low Standby Current = 20 μ A (Typ)
- Low Cost Surface Mount Plastic Package

MRFIC0930

900 MHz GaAs LOW NOISE AMPLIFIER WITH GAIN CONTROL

SEMICONDUCTOR TECHNICAL DATA



1
(Scale 2:1)

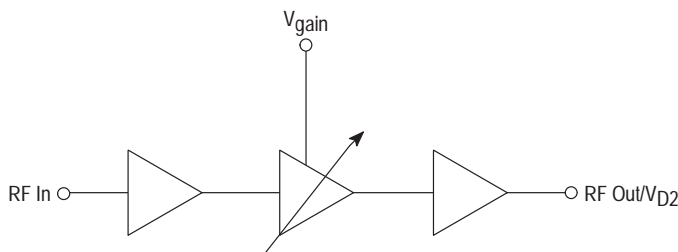
PLASTIC PACKAGE
CASE 751
(SO-8, Tape & Reel Only)



1
(Scale 2:1)

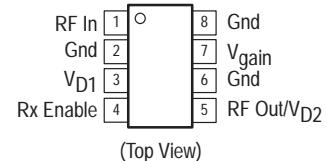
DM SUFFIX
PLASTIC PACKAGE
CASE 846A
(Micro-8, Tape & Reel Only)

Simplified Block Diagram



This device contains 12 active transistors.

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC0930R2	T _A = -30 to 70°C	SO-8* Tape & Reel
MRFIC0930DMR2		Micro-8** Tape & Reel

*2,500 Units per 16 mm, 13 inch reel.
**2,500 Units per 12 mm, 13 inch reel.

MRFIC0930

MAXIMUM RATINGS (T_A = 25°C, unless otherwise noted)

Rating	Symbol	Value	Unit
Supply Voltage	V _{D1} , V _{D2}	5.5	Vdc
RF Input Power	P _{RF}	3	dBm
Gain Control Voltage	V _{gain}	5.5	Vdc
Enable Voltage	RX Enable	5.5	Vdc
Storage Temperature Range	T _{stg}	-65 to 150	°C
Operating Ambient Temperature	T _A	-30 to 70	°C

NOTES: 1. Meets Human Body Model (HBM) ≤750 V and Machine Model (MM) ≤100 V.
2. ESD data available upon request.

RECOMMENDED OPERATING RANGES

Parameter	Symbol	Min	Typ	Max	Unit
RF Frequency	f _{RF}	800	–	1000	MHz
Supply Voltage	V _{D1} , V _{D2}	2.7	–	4.5	Vdc
V _{gain} , High Gain	V _{gain}	–	3.0	–	Vdc
V _{gain} , Low Gain	V _{gain}	–	0	–	Vdc
Rx Enable Voltage, On	Rx Enable	2.7	–	V _{D1} , V _{D2}	Vdc
Rx Enable Voltage, Off	Rx Enable	0	–	0.2	Vdc

NOTE: To bias, apply V_{D1} and V_{D2} before Rx Enable.

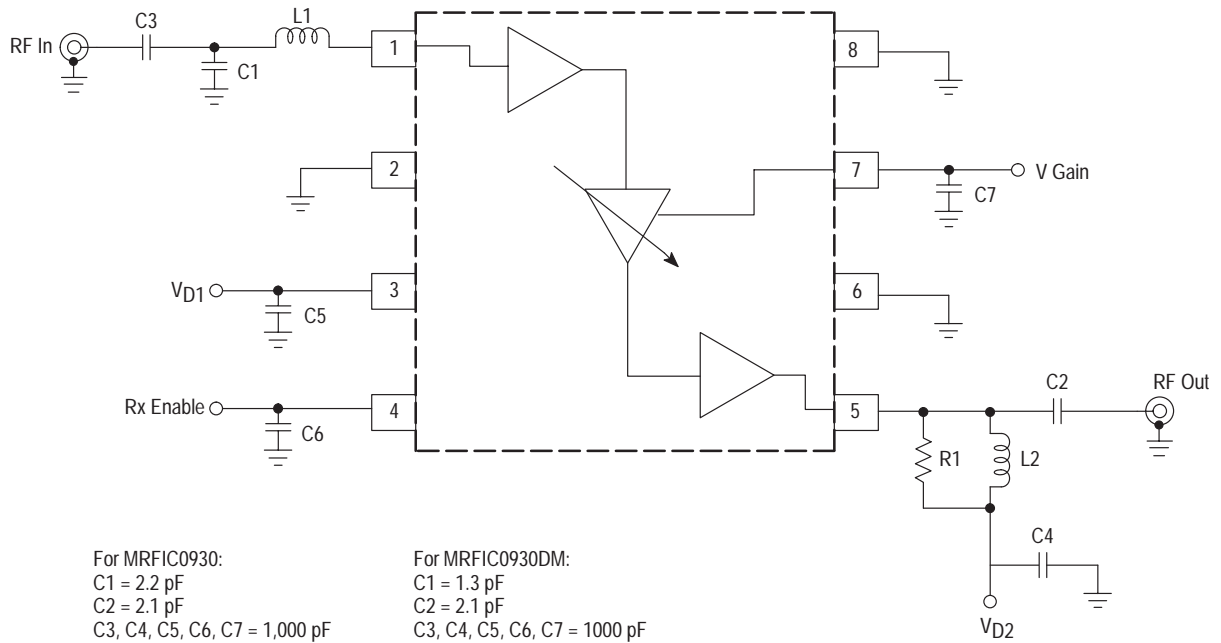
ELECTRICAL CHARACTERISTICS (V_{D1}, V_{D2} = 2.8 V, T_A = 25°C, RF = 940 MHz, Rx Enable = 2.8 V, V Gain = 2.8 V, RF In = -30 dBm, unless otherwise noted. Tested in Circuit Shown in Figure 1.)

Characteristic	Symbol	Min	Typ	Max	Unit
RF Gain MRFIC0930 MRFIC0930DM	S ₂₁	17 17.5	19 19	21 21.5	dB
RF Gain (V _{gain} = 0 V)	S ₂₁	–	0.8	4.0	dB
SSB Noise Figure [Note]	NF	–	1.7	3.0	dB
SSB Noise Figure (V _{gain} = 0 V) [Note]	NF	–	10.4	–	dB
RF Input 3rd Order Intercept Point [Note]	IIP3	-12	-9.0	–	dBm
RF Input 3rd Order Intercept Point (V _{gain} = 0 V) [Note]	IIP3	-7.0	-5.7	–	dBm
Input 1.0 dB Gain Compression [Note]	P _{1dB}	-21.5	-20.8	–	dBm
Input 1.0 dB Gain Compression (V _{gain} = 0 V) [Note]	P _{1dB}	-16	-11	–	dBm
Reverse Isolation (S ₁₂)	S ₁₂	–	41	–	dB
Input Return Loss	S ₁₁	–	15	–	dB
Input Return Loss (V _{gain} = 0 V)	S ₁₁	–	15	–	dB
Output Return Loss	S ₂₂	–	15	–	dB
Output Return Loss (V _{gain} = 0 V)	S ₂₂	–	12	–	dB
Supply Current Rx Mode	I _D	–	8.5	12	mA
Supply Current Standby Mode (Rx Enable = 0 V)	I _D	–	20	200	μA

NOTE: Guaranteed by design.

MRFIC0930

Figure 1. 900 MHz Test Circuit



For MRFIC0930:

- C1 = 2.2 pF
- C2 = 2.1 pF
- C3, C4, C5, C6, C7 = 1,000 pF
- L1 = 18 nH
- L2 = 10 nH
- R1 = 220 Ω

For MRFIC0930DM:

- C1 = 1.3 pF
- C2 = 2.1 pF
- C3, C4, C5, C6, C7 = 1000 pF
- L1 = 22 nH
- L2 = 8.2 nH
- R1 = 180 Ω

MRFIC0930

TYPICAL CHARACTERISTICS

(For SO-8 Packaged MRFIC0930)

Figure 2. Reverse Isolation versus Frequency

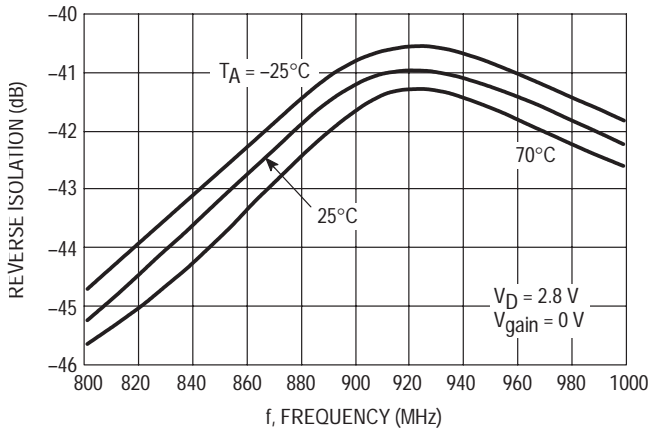


Figure 3. Reverse Isolation versus Frequency

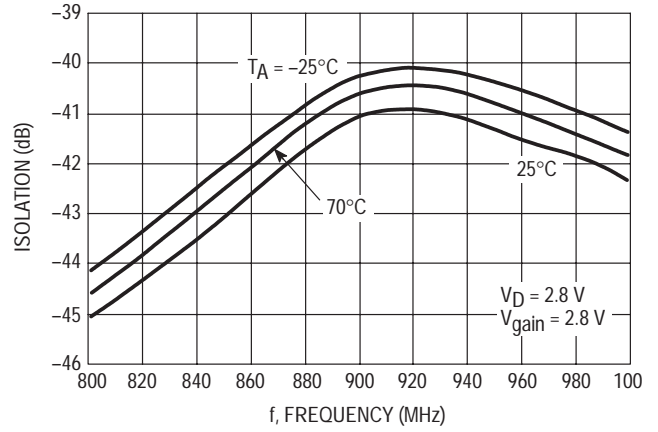


Figure 4. Gain versus Frequency

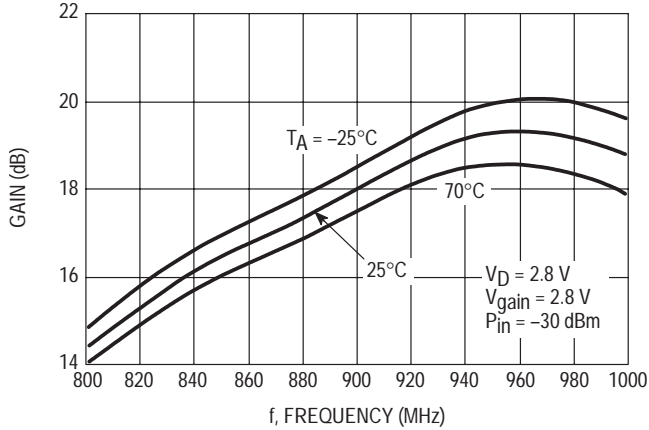


Figure 5. Gain Attenuation versus Frequency

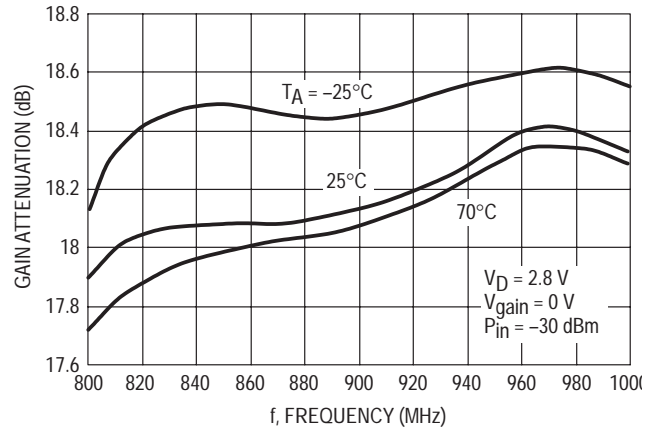


Figure 6. Gain versus Frequency

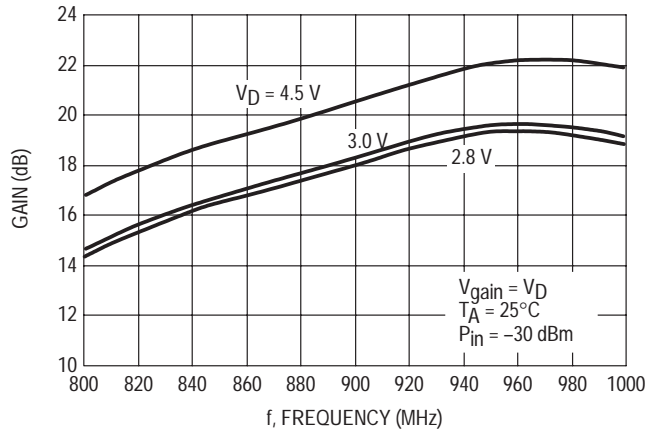
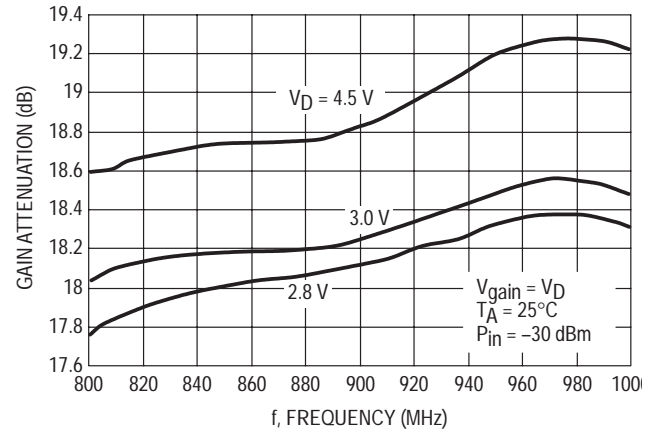


Figure 7. Gain Attenuation versus Frequency



MRFIC0930

TYPICAL CHARACTERISTICS

(For SO-8 Packaged MRFIC0930)

Figure 8. Input Power versus Output Power

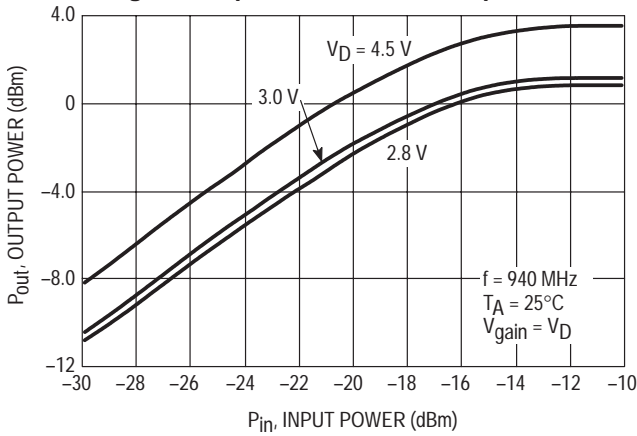


Figure 9. Input Power versus Output Power

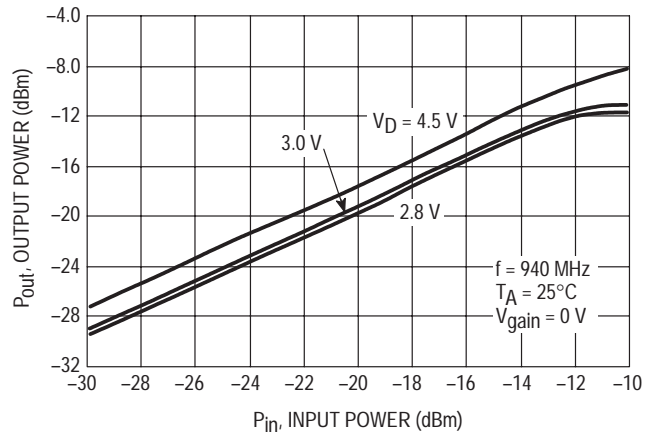


Figure 10. Input Power versus Output Power

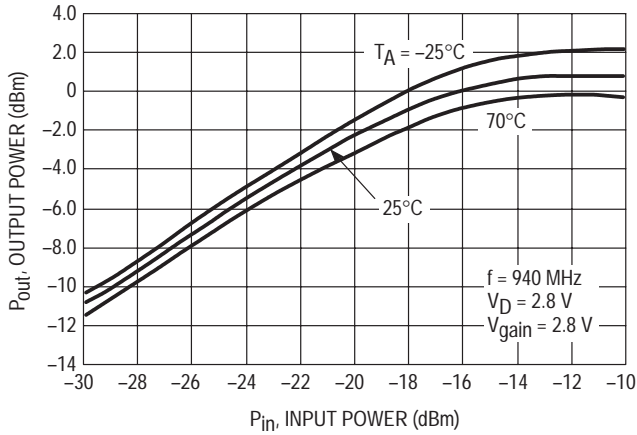


Figure 11. Input Power versus Output Power

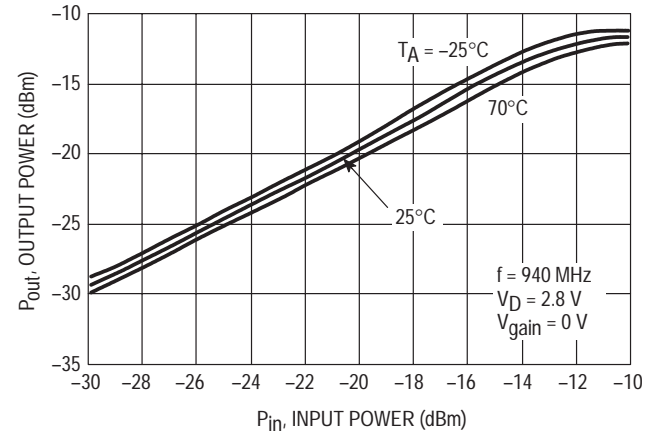


Figure 12. Noise Figure versus Frequency

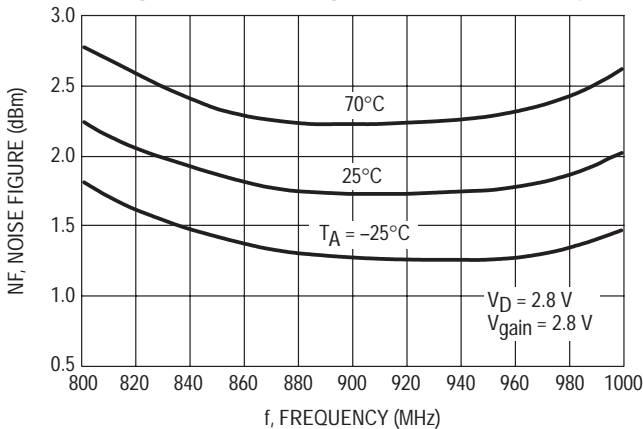
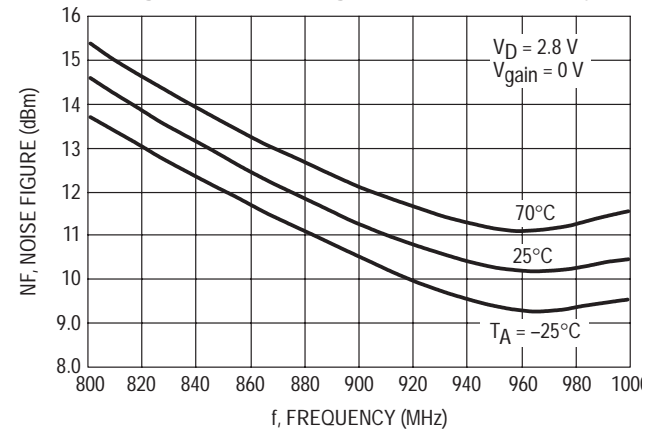


Figure 13. Noise Figure versus Frequency



MRFIC0930

TYPICAL CHARACTERISTICS (For Micro-8 Packaged MRFIC0930DM)

Figure 14. Reverse Isolation versus Frequency

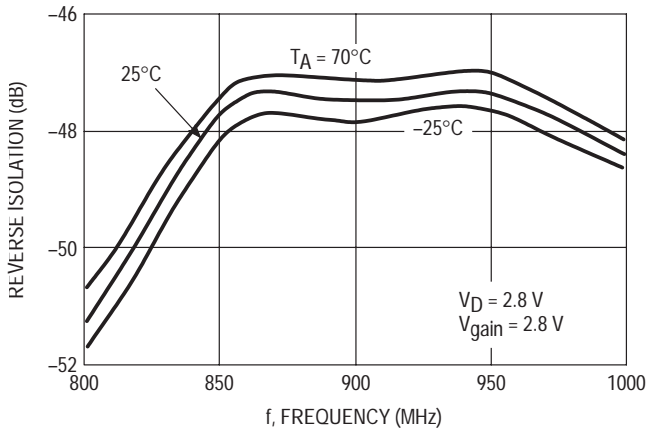


Figure 15. Reverse Isolation versus Frequency

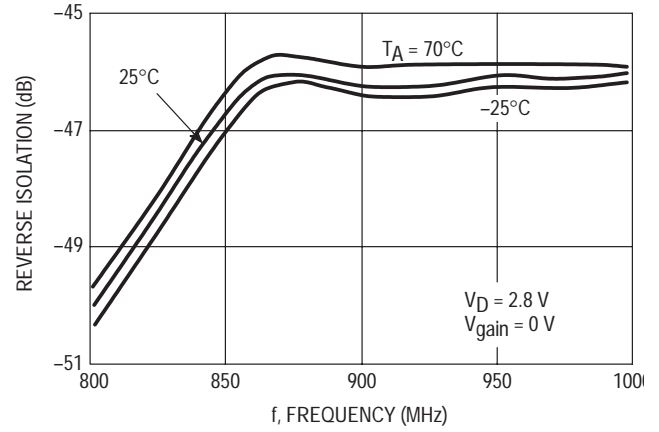


Figure 16. Gain versus Frequency

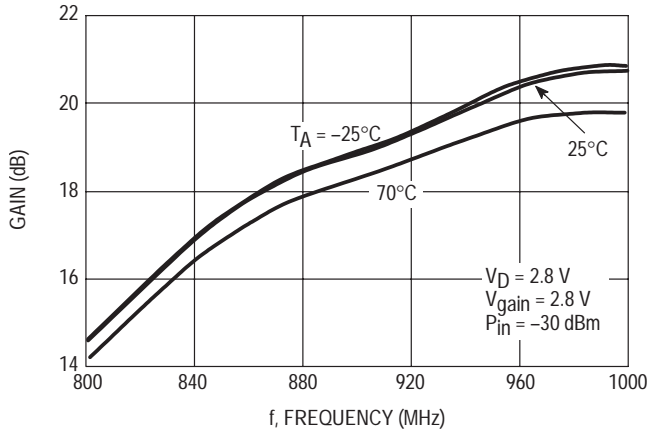


Figure 17. Gain Attenuation versus Frequency

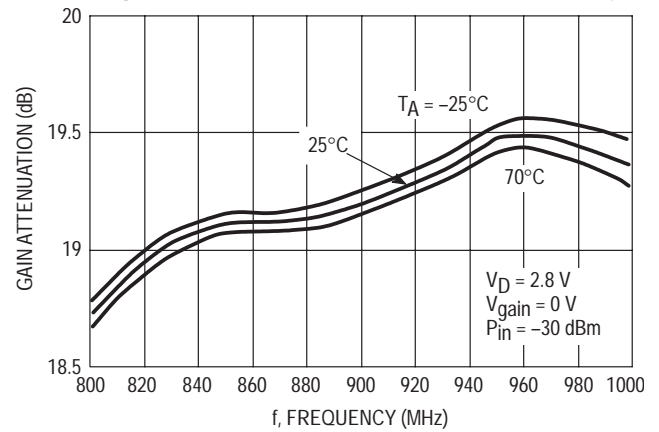


Figure 18. Gain versus Frequency

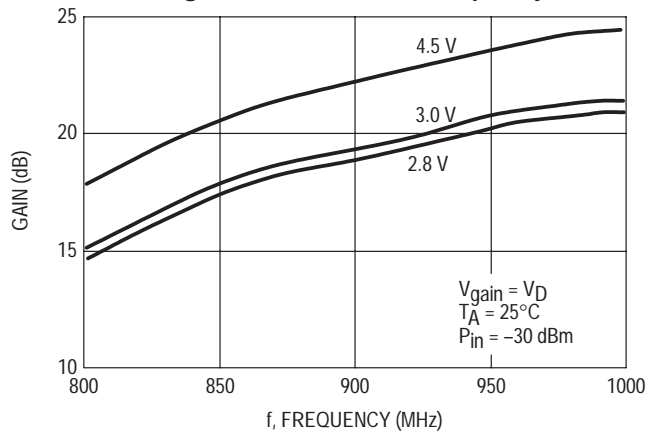
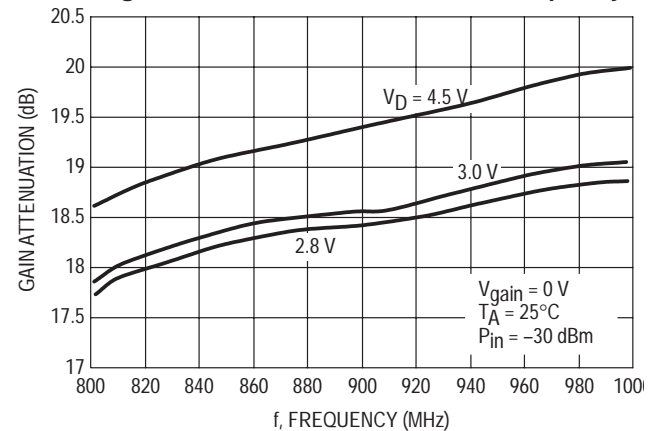


Figure 19. Gain Attenuation versus Frequency



MRFIC0930

TYPICAL CHARACTERISTICS (For Micro-8 Packaged MRFIC0930DM)

Figure 20. Input Power versus Output Power

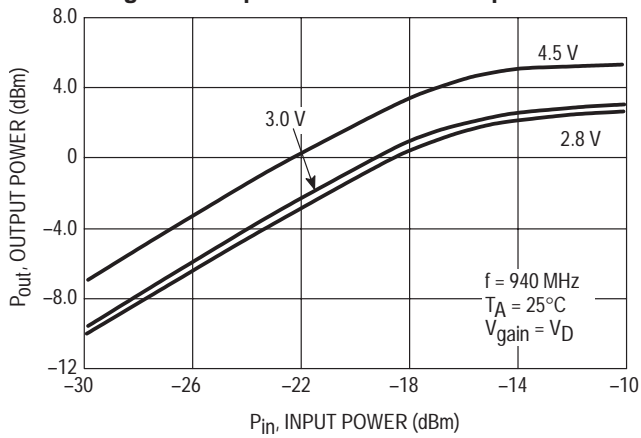


Figure 21. Input Power versus Output Power

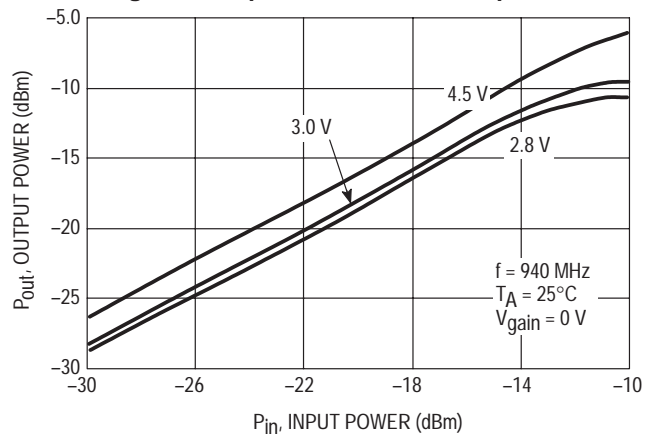


Figure 22. Input Power versus Output Power

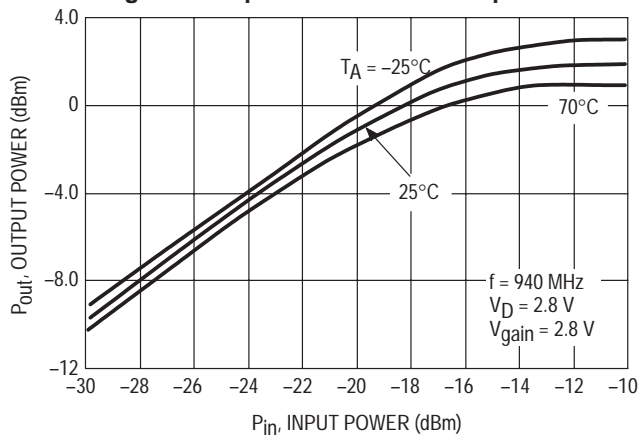


Figure 23. Input Power versus Output Power

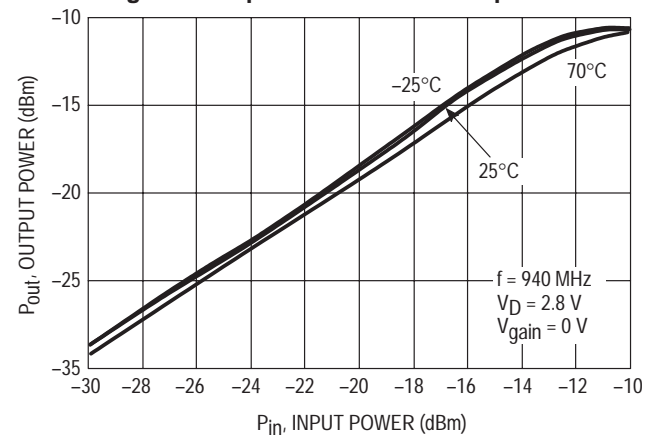


Figure 24. Noise Figure versus Frequency

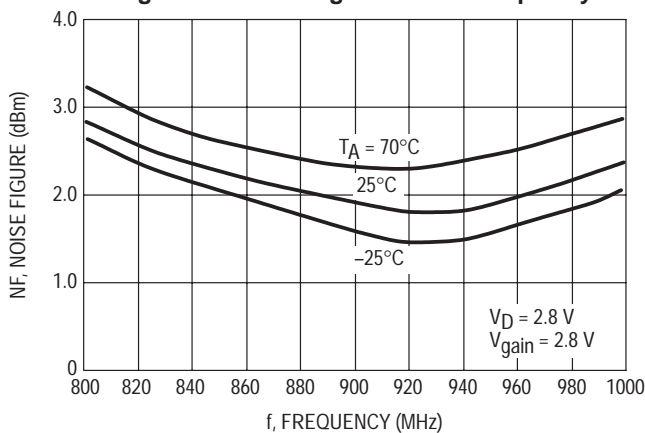
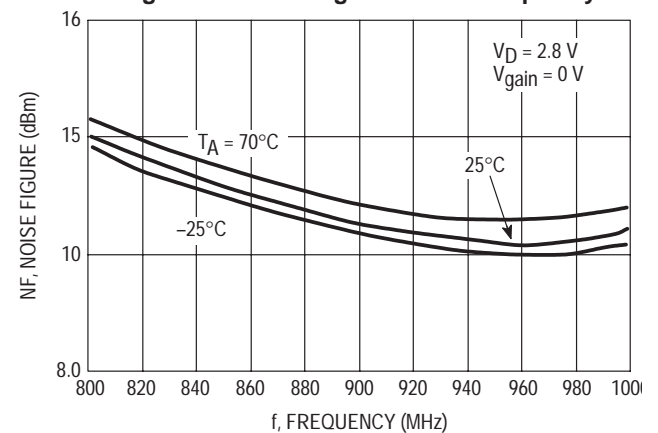


Figure 25. Noise Figure versus Frequency



800 MHz CDMA Upmixer/Exciter

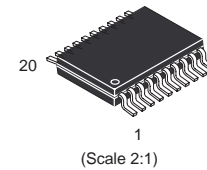
The MRFIC0954 is an integrated upmixer and exciter amplifier designed specifically for dual-mode CDMA/AMPS digital cellular radios. The exciter amplifier incorporates a temperature compensated linear gain control. The design utilizes Motorola's RF BiCMOS1 process to yield superior performance in a cost effective monolithic device.

- Designed for Dual-Mode Operation
 - Total Supply Current CDMA Mode = 55 mA Typical
 - Total Supply Current FM Mode = 35 mA Typical
- 30 dB Dynamic Range Gain Control on Exciter
- Upmixer Output IP₃ = 11 dBm Typical
- Exciter Output IP₃ = 28 dBm Typical
- Supply Voltage Range = 2.7 to 3.6 V
- Cascaded Adjacent Channel Power (P_{out} = 6.0 dBm)
 - @ 885 kHz Offset = -60 dBc Typical
 - @ 1.98 MHz Offset = -72 dBc Typical

MRFIC0954

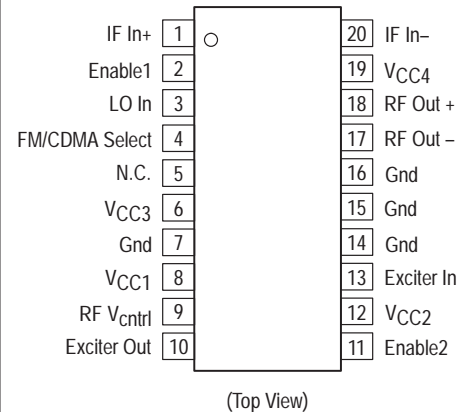
800 MHz DUAL-MODE CDMA/AMPS UPMIXER/EXCITER

SEMICONDUCTOR TECHNICAL DATA

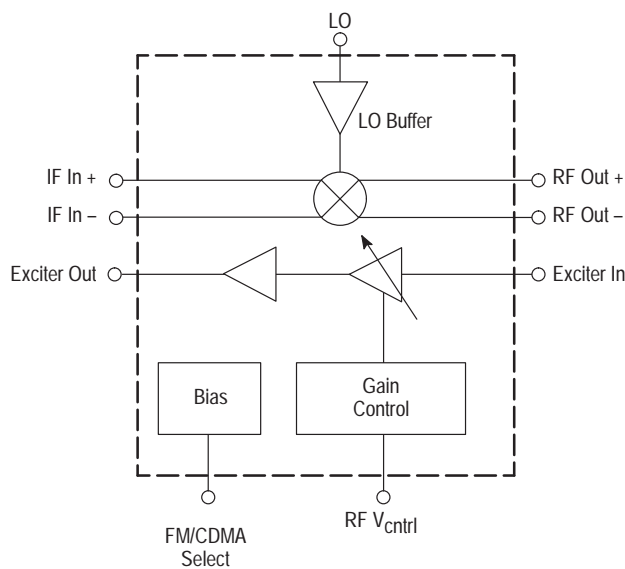


PLASTIC PACKAGE
CASE 948M
(TSSOP-20EP, Tape & Reel Only)

PIN CONNECTIONS



Simplified Block Diagram



This device contains 305 active transistors.

ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC0954R2	T _A = -40 to 85°C	TSSOP-20EP

MRFIC0954

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Supply Voltage	V_{CC}	5.0	V
IF Input	IF In+, IF In-	10	dBm
LO Input	LO	10	dBm
Operating Temperature	T_A	-40 to 85	°C
Storage Temperature	T_{stg}	-65 to 150	°C

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions and Electrical Characteristics tables or Pin Descriptions section.
 2. Meets Human Body Model (HBM) ≤ 50 V and Machine Model (MM) ≤ 40 V. This device is rated Moisture Sensitivity Level (MSL) 4. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Voltage	V_{CC}	2.7	-	3.6	V
RF Frequency Range	f_{RF}	800	-	960	MHz
IF Frequency Range	f_{IF}	70	-	250	MHz
LO Frequency Range	f_{LO}	600	-	1200	MHz
Gain Control Voltage Range	V_{ctrl}	0.1	-	1.7	V

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ V, $P_{LO} = -15$ dBm @ 967 MHz, $P_{IF} = -21$ dBm (differential) @ 130 MHz, $V_{Enable} = V_{TxEnable} = 2.4$ V, $T_A = 25^\circ\text{C}$, Test Circuit in Figure 1, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

CASCADE PERFORMANCE (Filter included between RF Out and Exciter input. Filter has an insertion loss of 4.0 dB) For CDMA mode FM/CDMA Select = 2.7 V. For FM mode FM/CDMA Select = 0 V.

Output Power CDMA Mode ($V_{ctrl} = 1.7$ V) FM Mode ($P_{IF} = -12$ dBm (differential)) CDMA Mode ($V_{ctrl} = 1.3$ V)	P_{out}	6.0 11 3.0	10 14 7.0	- - -	dBm
Dynamic Range ($RF_{V_{ctrl}} = 0.1$ to 1.7 V)	DR	25	38	-	dB
Adjacent Channel Power (CDMA Mode, $P_{out} = 6.0$ dBm, $P_{IF} = -21$ dBm (differential)) @ 885 kHz Offset @ 1.98 MHz Offset	ACPR	- -	-60 -72	-52 -62	dBc
Supply Current CDMA Mode, $P_{IF} = -21$ dBm (differential), $P_{out} = 6.0$ dBm (set by V_{ctrl}) FM Mode, $P_{IF} = -12$ dBm (differential), $P_{out} = 11$ dBm (set by V_{ctrl})	I_{CC}	- -	55 35	70 50	mA

MIXER SECTION

Conversion Gain	GC	-	7.0	-	dB
Noise Figure	NF	-	15	-	dB
Output Third Order Intercept Point	OIP3	-	11	-	dBm

EXCITER SECTION

Gain (No Attenuation)	GC	-	28	-	dB
Noise Figure	NF	-	5.0	-	dB
AGC Dynamic Range	DR	25	38	-	dB
Output Third Order Intercept Point	OIP3	-	25	-	dBm

MRFIC0954

PIN FUNCTION DESCRIPTION

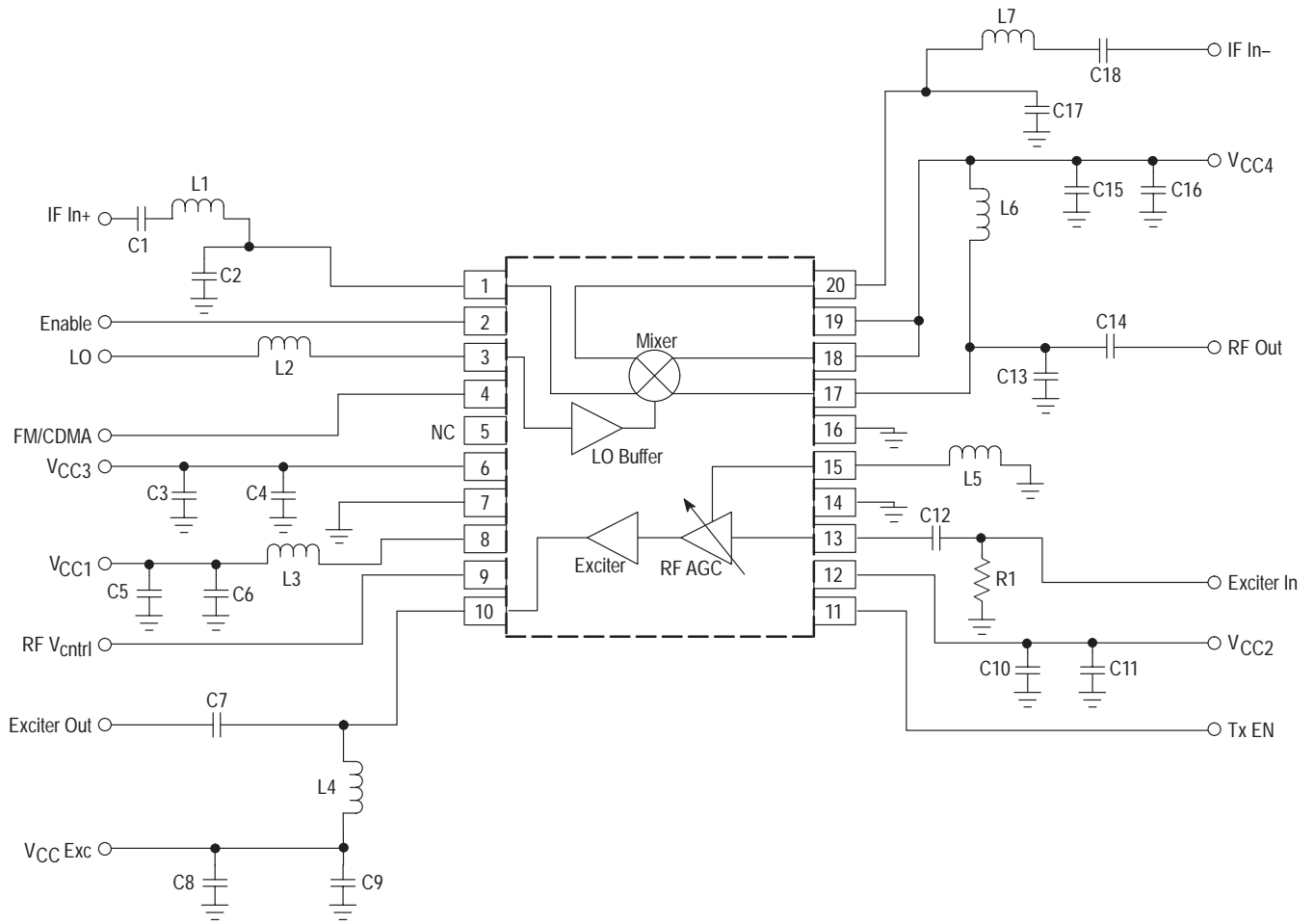
Pin	Function	Description	Voltage On (V)	Voltage Off (V)
1	IF In+	Mixer IF input pin. Input impedance is 500 Ω.	-24 dBm (Typ)	
2	Enable 1 (See Table 2)	Enable pin. A logic "High" (>2.4 V) enables entire chip and "Low" (<0.4 V) disables chip .	2.4 to 3.6	0 to 0.4
3	LO In	Mixer LO input pin.	-15 dBm (Typ)	
4	FM/CDMA Select	FM/CDMA select pin. Logic "High" (>2.4 V) selects CDMA mode for increased linearity and output power. "Low" (<0.4 V) selects FM mode for reduced current consumption.		
5	N.C.	No Connection		
6	VCC3	Supply Voltage.	2.7 to 3.6	
7	Gnd	Ground connection.	-	
8	VCC1	Supply Voltage	2.7 to 3.6	
9	RF AGC Control Voltage	RF AGC control pin. A 30 dB dynamic range can be achieved by adjusting voltage from 0.1 V (low gain) to 1.7 V (high gain).	0.1 to 1.7	
10	Exciter Out	RF exciter amplifier output pin.	-	
11	Enable 2 (See Table 2)	Tx Enable pin. A logic "High" (>2.4 V) enables Tx path and "Low" (<0.4 V) disables Tx path except LO Buffer .	2.4 to 3.6	0 to 0.4
12	VCC2	Supply Voltage	2.7 to 3.6	
13	Exciter In	RF exciter amplifier input pin.	-	
14	Gnd	Ground connection.	-	
15	Gnd	Ground connection.	-	
16	Gnd	Ground connection.	-	
17	RF Out-	Mixer RF output pin.		
18	RF Out+	Mixer RF output pin.		
19	VCC4	Supply Voltage	2.7 to 3.6	
20	IF In-	Mixer IF input pin. Input impedance is 500 Ω.	-24 dBm (Typ)	

Table 1. Enable Truth Table

Enable 1	Enable 2	Mode
0	0	Disabled
0	1	Not Applicable
1	0	Standby Mode: Disables mixer/exciter, except LO buffer
1	1	Tx Enabled

MRFIC0954

Figure 1. Applications Circuit



C1, C18	1.0 nF	L1, L7	220 nH
C2, C17	4.7 pF	L2	15 nH
C3, C5, C8, C11, C16	10 nF	L3, L4, L6	6.8 nH
C4, C6, C9, C10, C12, C15	100 pF	L5	1.0 nH
C7	4.3 pF		
C13	1.6 pF	R1	100 Ω
C14	1.3 pF		

- NOTES:**
1. IF ports matched to 50 Ω for testing purposes.
 2. L3 and C6 form part of RFAGC/Exciter interstage match.
 3. L5 can be varied to change gain.

Figure 2. Gain versus Frequency (FM Mode)

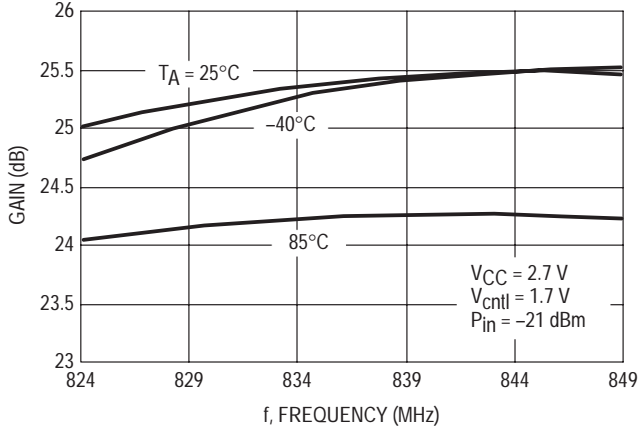


Figure 3. Gain versus Frequency (CDMA Mode)

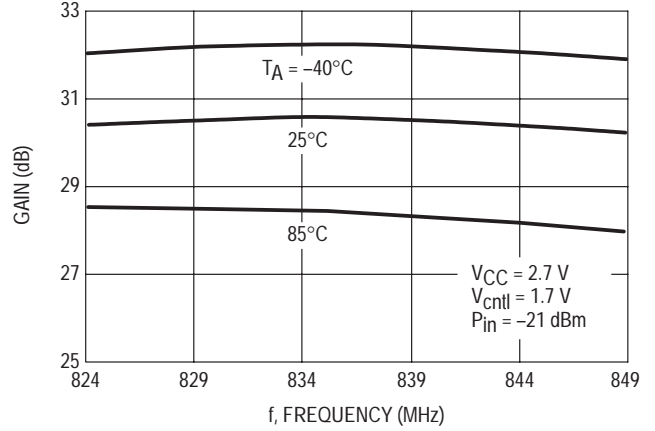


Figure 4. Gain versus LO Power (FM Mode)

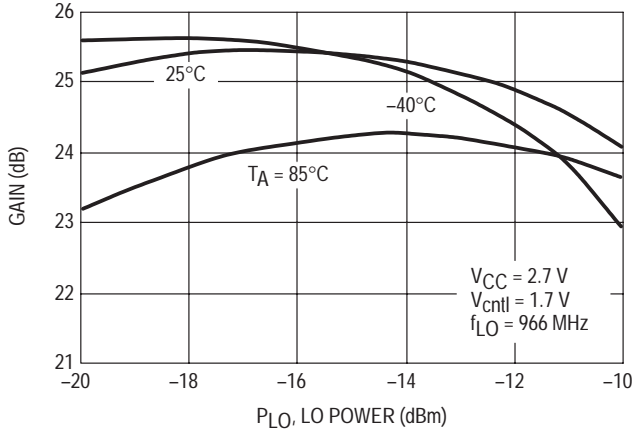


Figure 5. Gain versus LO Power (CDMA Mode)

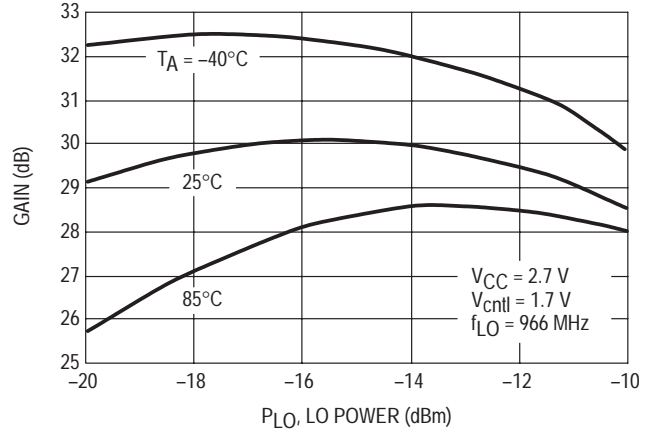


Figure 6. LO Feedthrough versus Control Voltage (FM Mode)

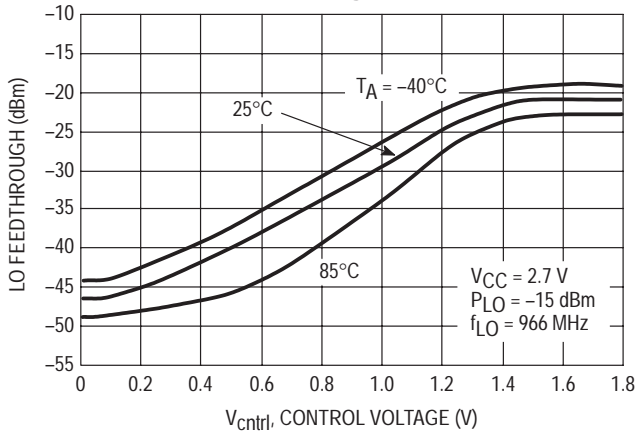


Figure 7. LO Feedthrough versus Control Voltage (CDMA Mode)

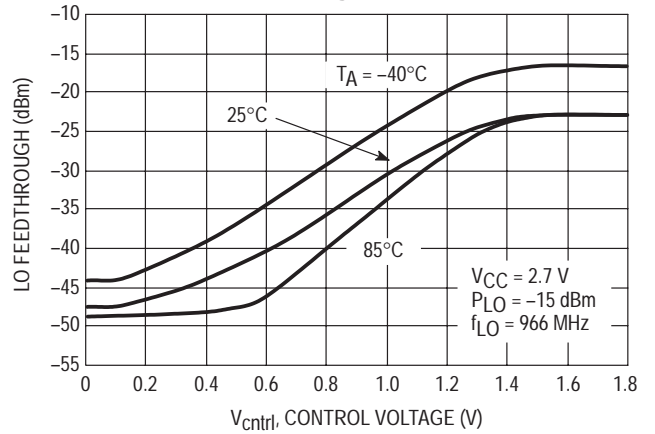


Figure 8. Output Power versus Control Voltage (FM Mode)

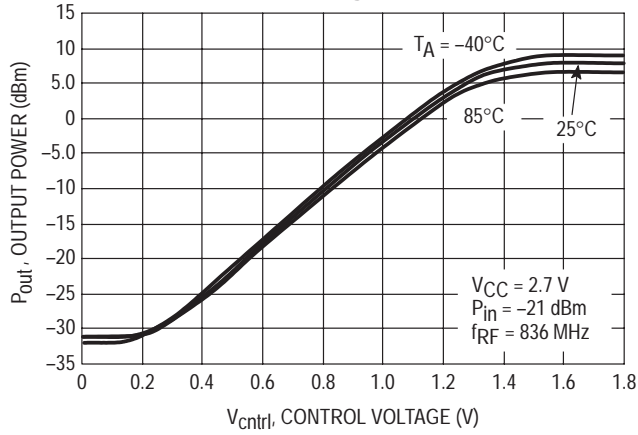


Figure 9. Output Power versus Control Voltage (CDMA Mode)

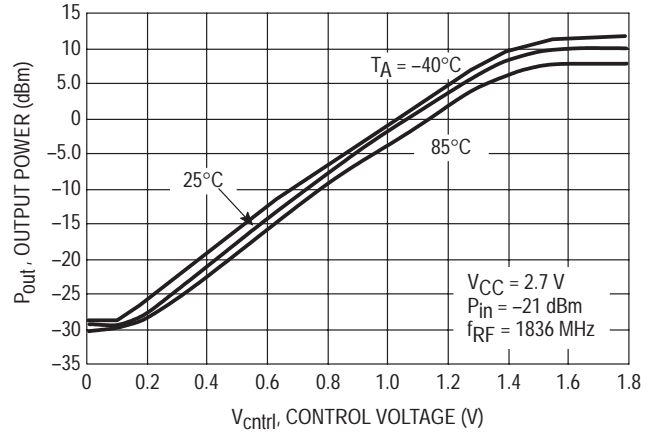


Figure 10. Adjacent Channel Power versus Control Voltage (CDMA Mode)

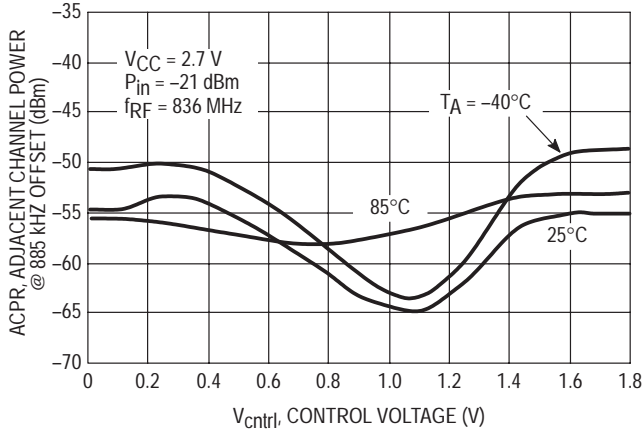
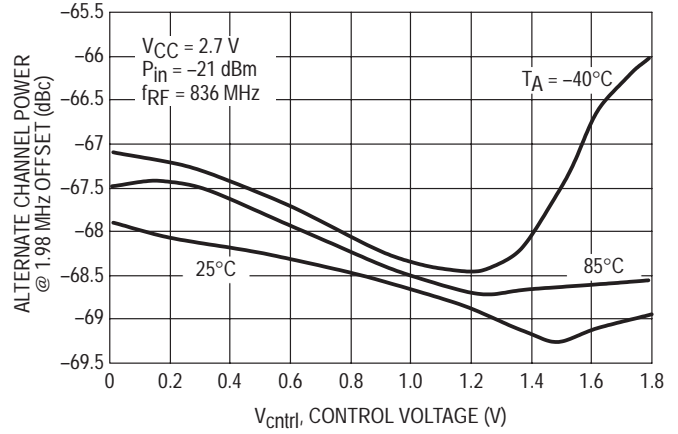


Figure 11. Alternate Channel Power versus Control Voltage (CDMA Mode)



MRFIC0954

APPLICATIONS INFORMATION

Design Philosophy

The MRFIC0954 has three operating states, enable, standby, and disable. These states are controlled by the truth table shown in Table 2. The device is fully operational during the enable state and the bias level can be selected. A high bias current for CDMA or a lower bias current for Analog (or CDMA at lower powers) can be selected via the FM/CDMA pin. In the high current CDMA mode, the quiescent current is increased to maximize the linearity of the device. In the lower current bias, the quiescent current is optimized for efficiency in the Analog mode. This lower bias point is also useful in lower power CDMA operation. The standby mode can be used to reduce current consumption during Voice Activity Factoring. In the standby mode, the LO buffer remains on to prevent VCO pulling and the bandgap reference bias circuit remains on to assure rapid device turn on. Current consumption in standby mode is 10 mA typical. The disable mode is used to turn the MRFIC0954 completely off. Leakage current in this mode is only a few microamps.

The mixer is a double-balanced “Gilbert-cell” design with a balanced LO buffer amplifier. The input and output of the mixer are differential. However, the linearity is high enough to tie one output to V_{CC} and use the other as a single-ended output. Used this way it provides around 7.0 dB of gain and typically draws 20 mA quiescent current in CDMA mode and 16 mA in Analog Mode. An external filter is required between the mixer and RF AGC amplifier to reduce RX band noise.

Figure 1 shows the applications circuit for the MRFIC0954. In this circuit, the IF ports of the mixer have been matched to 50 Ω for testing purposes. In the actual application, the differential IF ports of the mixer would be impedance matched to an IF SAW filter. The differential impedance of the mixer IF ports is 1600 Ω . The RF output of the mixer is configured as a single ended output. DC current to the open collector output of the mixer is provided by inductor, L6 (6.8 nH). Inductor L6 is also part of the matching circuit with C13 (1.6 pF), C14 (1.3 pF) and C15 (100 p).

The RF AGC amplifier is a single-ended cascode design employing the standard “current steering” method of gain control. It’s ground is brought out through pin number 15 so inductance can be added to degenerate the gain for a lower noise floor. With 2.0 to 3.0 nH of external inductance, the maximum gain is around 13 dB. It typically draws 9.0 mA quiescent current in CDMA mode and 3.0 mA in Analog mode. The RF V_{ctrl} signal is buffered with an on-chip OpAmp then preconditioned with temperature compensation and dB/V linearization before being applied to the RF AGC amplifier.

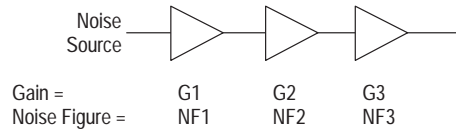
Inductor L3 (6.8 nH) and capacitor C6 (100 pF) are for the interstage match between the RF AGC and the exciter amplifier.

The exciter amplifier is a simple common emitter design. It is grounded directly to the exposed pad which results in 12 dB of gain. It typically draws 24 mA bias current in CDMA mode and 8.0 mA in Analog mode. Inductor L4 (6.8 nH),

capacitor C7 (4.3 pF), and C9 (100 pF) provide the output matching. L4 also provides a DC current path for the open collector output.

Noise Power Considerations

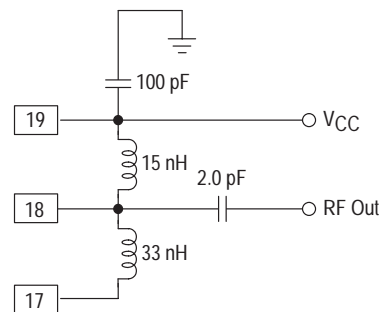
In CDMA systems, the handset is required to dynamically adjust its output power to specific levels. This requires a dynamic range of as much as 90 dB from the transmitter. Another key performance specification in CDMA systems is the output noise power, both in band and out of band. Noise power specifications has caused the noise figure of the transmitter to become an important system consideration. The cascaded noise figure of the transmitter can be analyzed with the same equation used in receiver analysis. The only difference is the noise source is from the transmitter (modulator) instead of the atmosphere.



$$NF_{\text{cascaded}} = NF_1 + \frac{NF_2 - 1}{G_1} + \frac{NF_3 - 1}{G_1 G_2}$$

This equation above shows that the cascaded noise figure is better if the gain is higher and the noise figure is lower for the stages close to the noise source. For this reason, it is advantageous to implement some of the gain control of a CDMA transmitter in the RF section. The MRFIC0954 integrates a RF AGC amplifier after the upmixer to improve the overall noise figure of the transmitter.

If better noise figure from the mixer is required, the mixer RF output can be operated differentially with the addition of a balun. Operating the mixer differentially will provide some noise cancellation and reduce the noise figure by 5.0 dB. Shown below is a lumped element balun that is effective in the cellular transmit band of 824 to 849 MHz.



MRFIC0954

Table 2. Scattering Parameters for Exciter Amplifier
($V_{DD} = 2.7\text{ V}$, $T_A = 25^\circ\text{C}$, RF $V_{ctrl} = 1.8\text{ V}$, $50\ \Omega$ System)

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	$\angle\phi$	S ₂₁	$\angle\phi$	S ₁₂	$\angle\phi$	S ₂₂	$\angle\phi$
800	0.523	-31.46	18.463	-102.56	0.001	153.19	0.341	-26.37
810	0.522	-31.83	18.964	-107.12	0.001	152.15	0.360	-33.06
820	0.519	-31.84	19.412	-111.84	0.001	152.18	0.379	-39.48
830	0.515	-31.96	20.017	-121.57	0.001	143.30	0.413	-52.61
840	0.513	-31.90	20.214	-126.53	0.002	139.87	0.428	-58.96
850	0.512	-31.78	20.330	-131.59	0.001	140.14	0.445	-65.36
860	0.513	-31.62	20.228	-141.98	0.001	143.83	0.468	-77.72
870	0.510	-31.64	19.962	-147.12	0.002	140.02	0.476	-83.97
880	0.510	-31.45	19.593	-152.09	0.002	147.69	0.478	-89.94
890	0.514	-31.41	18.768	-161.40	0.002	139.58	0.486	-100.64
900	0.515	-31.50	18.161	-166.11	0.002	141.12	0.491	-105.67
910	0.514	-31.58	17.585	-170.50	0.002	124.24	0.489	-110.70
920	0.515	-31.83	16.353	-178.79	0.002	125.97	0.485	-119.67
930	0.517	-31.96	15.718	177.30	0.002	128.36	0.489	-124.16
940	0.518	-32.29	15.070	173.39	0.002	125.66	0.484	-128.24
950	0.517	-32.88	13.708	166.70	0.002	112.00	0.473	-135.30
960	0.518	-32.81	13.090	163.84	0.002	117.04	0.468	-138.41

MRFIC0954

Table 3. Scattering Parameters for Upmixer
($V_{DD} = 2.7\text{ V}$, $T_A = 25^\circ\text{C}$, $50\ \Omega$ System)

f (MHz)	IF In+		IF In-		f (MHz)	RF Out (Pin 17)	
	$ S_{11} $	$\angle\phi$	$ S_{11} $	$\angle\phi$		$ S_{11} $	$\angle\phi$
70	0.886	-5.66	0.885	-5.12	800	0.488	-60.15
80	0.883	-5.79	0.882	-5.29	810	0.487	-60.56
90	0.884	-6.15	0.881	-5.73	820	0.487	-61.04
100	0.879	-6.26	0.878	-5.74	830	0.488	-61.82
110	0.881	-6.74	0.881	-6.19	840	0.490	-62.20
120	0.877	-7.20	0.878	-6.43	850	0.487	-62.85
130	0.880	-7.23	0.879	-6.64	860	0.491	-63.72
140	0.876	-7.89	0.876	-7.20	870	0.492	-64.03
150	0.876	-8.11	0.875	-7.28	880	0.493	-64.38
160	0.878	-8.51	0.877	-7.57	890	0.497	-65.56
170	0.879	-8.84	0.879	-8.07	900	0.501	-65.98
180	0.877	-9.28	0.880	-8.26	910	0.503	-66.50
190	0.876	-9.81	0.878	-8.81	920	0.504	-68.66
200	0.876	-10.15	0.877	-9.21	930	0.504	-69.70
210	0.875	-10.52	0.876	-9.44	940	0.502	-69.91
220	0.877	-10.83	0.880	-9.78	950	0.503	-71.15
230	0.877	-11.58	0.877	-10.41	960	0.502	-70.74
240	0.878	-11.59	0.877	-10.41			
250	0.881	-12.29	0.879	-10.85			

f (MHz)	LO In		f (MHz)	LO In		f (MHz)	LO In	
	$ S_{11} $	$\angle\phi$		$ S_{11} $	$\angle\phi$		$ S_{11} $	$\angle\phi$
600	0.820	-18.93	810	0.802	-24.40	1020	0.785	-30.28
610	0.819	-19.00	820	0.800	-24.55	1030	0.784	-30.09
620	0.817	-19.35	830	0.802	-24.75	1040	0.786	-30.63
630	0.815	-19.60	840	0.804	-25.22	1050	0.786	-30.91
640	0.820	-19.87	850	0.804	-25.13	1060	0.784	-31.10
650	0.814	-20.06	860	0.802	-25.86	1070	0.780	-31.60
660	0.813	-20.49	870	0.799	-26.14	1080	0.783	-31.85
670	0.816	-20.61	880	0.801	-26.36	1090	0.782	-31.99
680	0.815	-20.82	890	0.797	-26.72	1100	0.775	-32.54



MOTOROLA

1.9 GHz GaAs Low Noise Amplifier

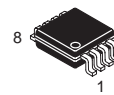
Designed primarily for use in wireless Personal Communication Systems (PCS) applications such as Digital European Cordless Telephone (DECT), Japan's Personal Handy System (PHS) and the emerging North American systems as a preamp for discrete or integrated downmixers. The MRFIC1808DM is a two-stage low noise amplifier in a low-cost Micro-8 package. The amplifier can be matched to optimize gain or noise figure with simple off-chip input matching. The design employs a novel stacked MESFET design which reuses bias current for the highest gain at minimal current. A CMOS compatible Rx Enable pin allows for very low standby current while the system is in transmit mode.

- Usable Frequency Range = 1.7 to 2.1 GHz
- 18 dB Typ Gain
- 1.6 dB Typ Noise Figure
- Simple Off-chip Matching for Maximum Gain/Noise Figure Flexibility
- High Reverse Isolation = 32 dB (Typ)
- Single Bias Supply = 2.7 to 4.5 V
- Low Standby Current = 8 μ A (Typ)
- Low Cost Surface Mount Plastic Package
- Device Marking = M1808

MRFIC1808

1.9 GHz GaAs LOW NOISE AMPLIFIER

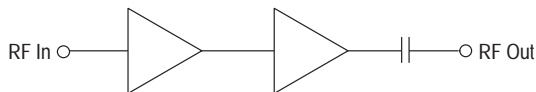
SEMICONDUCTOR TECHNICAL DATA



(Scale 2:1)

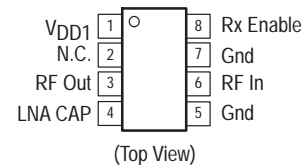
DM SUFFIX
PLASTIC PACKAGE
CASE 846A
(Micro-8, Tape & Reel Only)

Simplified Block Diagram



This device contains 5 active transistors.

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC1808DMR2	T _A = -30 to 85°C	Micro-8

MRFIC1808

MAXIMUM RATINGS ($T_A = 25^\circ\text{C}$, unless otherwise noted)

Rating	Symbol	Value	Unit
Supply Voltage	V_{DD}	5.5	Vdc
RF Input Power	P_{RF}	3.0	dBm
Enable Voltage	Rx Enable	5.5	Vdc
Storage Temperature Range	T_{stg}	-65 to 150	$^\circ\text{C}$
Operating Ambient Temperature	T_A	-30 to 85	$^\circ\text{C}$

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions or Electrical Characteristics tables.
 2. Meets Human Body Model (HBM) ≤ 500 V and Machine Model (MM) ≤ 200 V.
 3. ESD data available upon request.

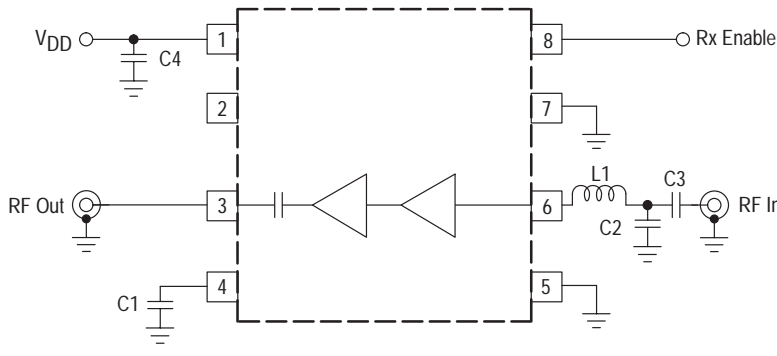
RECOMMENDED OPERATING CONDITIONS

Parameter	Symbol	Min	Typ	Max	Unit
RF Frequency	f_{RF}	1.7	-	2.1	GHz
Supply Voltage	V_{DD}	2.7	-	4.5	Vdc
Rx Enable Voltage, ON	Rx Enable	2.7	-	V_{DD}	Vdc
Rx Enable Voltage, OFF	Rx Enable	0	-	0.2	Vdc

ELECTRICAL CHARACTERISTICS ($V_{DD} = 3.0$ V, $T_A = 25^\circ\text{C}$, $RF = -30$ dBm @ 1.9 GHz, Rx Enable = 3.0 V, unless otherwise noted. Tested in Circuit Shown in Figure 1)

Characteristic	Symbol	Min	Typ	Max	Unit
RF Gain	-	16	18	-	dB
SSB Noise Figure	-	-	1.6	-	dB
RF Output 3rd Order Intercept Point	-	-	13	-	dBm
Output 1 dB Gain Compression	-	-3.0	1.0	-	dBm
Reverse Isolation (s_{12})	-	-	-34	-	dB
Input Return Loss	-	-	-12	-	dB
Output Return Loss	-	-	-15	-	dB
Supply Current, Rx Mode	-	-	5.0	7.5	mA
Supply Current, Standby Mode (Rx Enable = 0 V)	-	-	-	50	μA

Figure 1. Applications Circuit Configuration



C1	1.4 pF
C2	1.4 pF
C3, C4	22 pF
L1	4.7 nH

MRFIC1808

TYPICAL CHARACTERISTICS

Figure 2. Supply Current versus Voltage

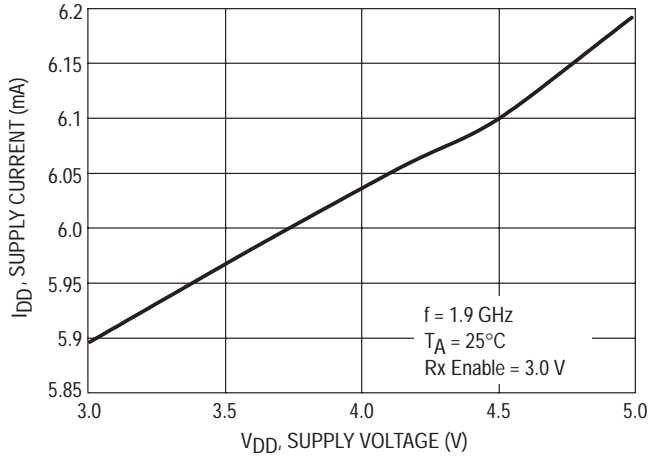


Figure 3. Output Power versus Input Power

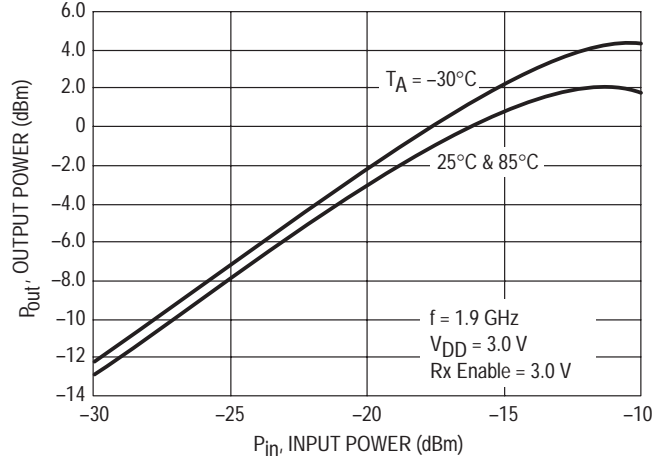


Figure 4. Output Power versus Input Power

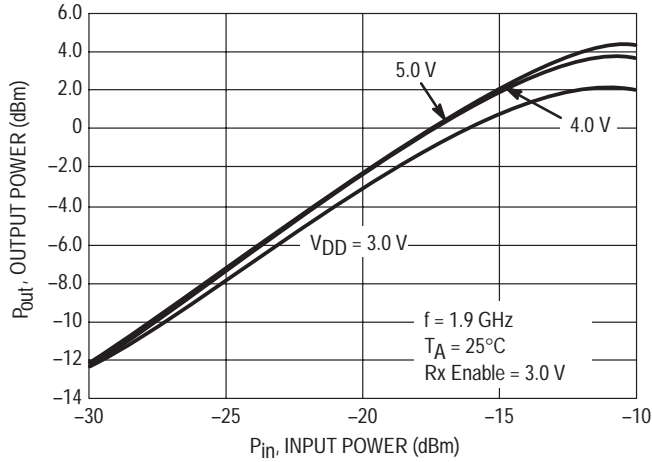


Figure 5. Gain versus Frequency

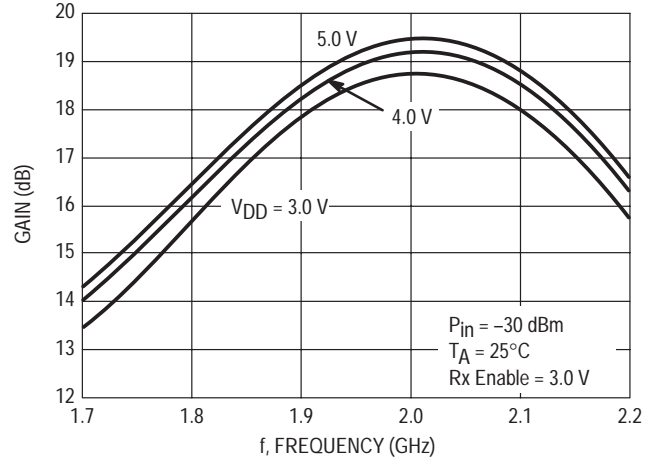


Figure 6. Gain versus Frequency

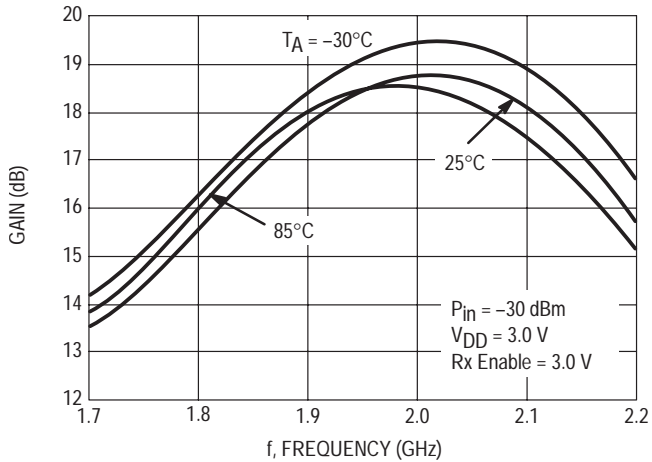
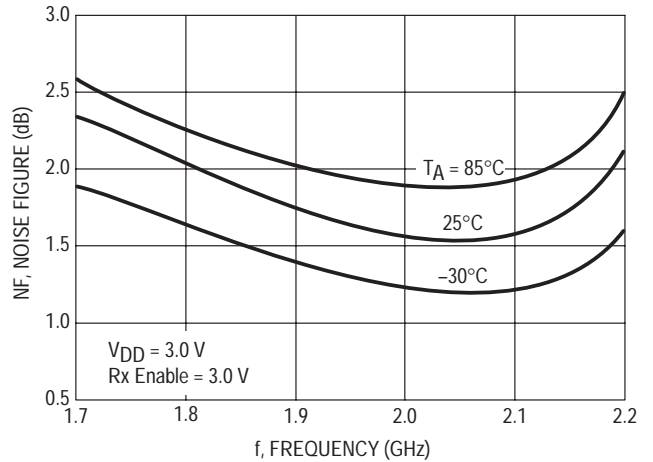


Figure 7. Noise Figure versus Frequency



MRFIC1808

TYPICAL CHARACTERISTICS

Figure 8. Reverse Isolation versus Frequency

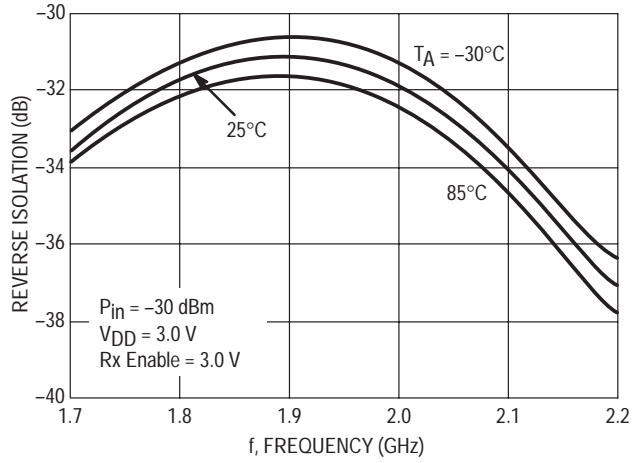
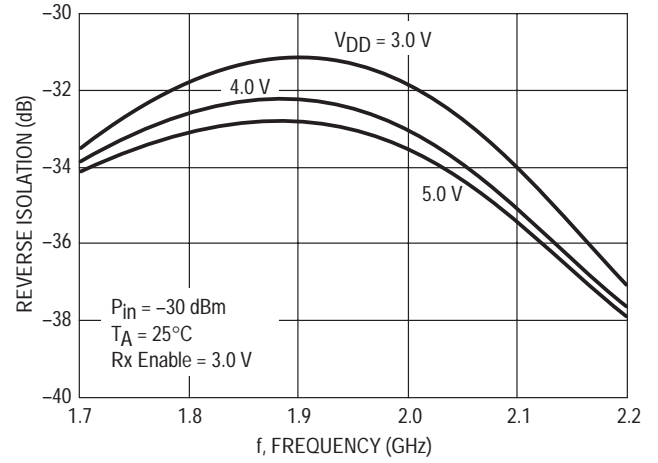


Figure 9. Reverse Isolation versus Frequency



MRFIC1808

Table 1. Scattering Parameters
($V_{DD} = 3.0\text{ V}$, $T_A = 25^\circ\text{C}$, Rx Enable = 3.0 V, 50 Ω System)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	ϕ	S ₂₁	ϕ	S ₁₂	ϕ	S ₂₂	ϕ
1500	0.907	-42	2.91	153	0.012	87	0.793	-60
1530	0.913	-43	3.11	148	0.012	85	0.765	-62
1560	0.920	-44	3.32	144	0.013	83	0.735	-64
1590	0.927	-45	3.55	139	0.013	80	0.701	-66
1620	0.935	-46	3.78	135	0.013	76	0.665	-67
1650	0.943	-47	4.02	130	0.013	73	0.627	-69
1680	0.951	-48	4.26	125	0.013	70	0.586	-70
1710	0.959	-49	4.49	119	0.012	67	0.544	-70
1740	0.967	-50	4.72	114	0.012	63	0.500	-70
1770	0.975	-52	4.94	109	0.012	59	0.458	-70
1800	0.982	-53	5.17	104	0.011	56	0.418	-68
1830	0.988	-55	5.38	98	0.011	52	0.382	-65
1860	0.993	-56	5.58	93	0.011	48	0.351	-60
1890	0.997	-58	5.76	87	0.010	44	0.329	-54
1920	0.999	-59	5.92	82	0.009	40	0.317	-48
1950	1.002	-61	6.07	76	0.008	35	0.317	-40
1980	1.004	-62	6.19	71	0.008	30	0.327	-34
2010	1.004	-64	6.29	65	0.007	25	0.346	-28
2040	1.003	-65	6.37	60	0.006	19	0.371	-24
2070	1.002	-67	6.43	55	0.005	11	0.401	-21
2100	0.999	-68	6.50	50	0.004	2	0.433	-20
2130	0.996	-70	6.55	45	0.004	-10	0.467	-19
2160	0.994	-71	6.61	40	0.003	-29	0.499	-19
2190	0.991	-73	6.67	35	0.003	-52	0.530	-19
2220	0.989	-74	6.70	31	0.003	-80	0.560	-20
2250	0.984	-76	6.70	26	0.003	-100	0.589	-21
2280	0.981	-77	6.66	21	0.004	-113	0.615	-22
2310	0.975	-79	6.59	16	0.005	-122	0.639	-23
2340	0.968	-80	6.51	13	0.006	-130	0.661	-25
2370	0.960	-82	6.48	9	0.007	-135	0.681	-26
2400	0.953	-83	6.47	5	0.008	-140	0.698	-28
2430	0.944	-84	6.48	2	0.009	-145	0.714	-30
2460	0.937	-86	6.50	-2	0.011	-149	0.727	-31
2490	0.929	-87	6.52	-7	0.012	-154	0.739	-33
2520	0.922	-88	6.49	-11	0.013	-158	0.750	-34
2550	0.915	-90	6.43	-15	0.014	-161	0.758	-36
2580	0.908	-91	6.33	-19	0.015	-163	0.766	-38

MRFIC1808

Table 2. Scattering Parameters
($V_{DD} = 4.0\text{ V}$, $T_A = 25^\circ\text{C}$, Rx Enable = 3.0 V, 50 Ω System)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	ϕ	S ₂₁	ϕ	S ₁₂	ϕ	S ₂₂	ϕ
1500	0.893	-42	3.20	151	0.012	87	0.797	-60
1530	0.899	-43	3.42	147	0.012	85	0.770	-62
1560	0.906	-44	3.65	143	0.012	82	0.740	-64
1590	0.914	-45	3.90	138	0.012	80	0.707	-65
1620	0.921	-46	4.15	134	0.013	77	0.671	-67
1650	0.929	-47	4.41	129	0.013	73	0.633	-68
1680	0.936	-48	4.67	124	0.013	70	0.593	-70
1710	0.945	-49	4.93	119	0.012	67	0.551	-70
1740	0.953	-50	5.18	113	0.012	63	0.507	-71
1770	0.960	-52	5.43	108	0.012	60	0.465	-70
1800	0.967	-53	5.66	103	0.011	57	0.424	-68
1830	0.973	-55	5.89	97	0.011	53	0.387	-66
1860	0.979	-56	6.11	92	0.011	50	0.355	-61
1890	0.982	-58	6.32	87	0.010	46	0.330	-56
1920	0.985	-59	6.51	81	0.009	43	0.317	-49
1950	0.987	-61	6.68	75	0.008	39	0.314	-42
1980	0.988	-62	6.81	70	0.008	32	0.322	-35
2010	0.989	-64	6.92	65	0.007	26	0.339	-29
2040	0.988	-65	7.02	60	0.006	20	0.364	-25
2070	0.986	-67	7.09	54	0.005	13	0.394	-22
2100	0.984	-68	7.17	49	0.005	4	0.425	-20
2130	0.980	-70	7.23	44	0.004	-7	0.459	-19
2160	0.978	-71	7.30	40	0.003	-21	0.491	-18
2190	0.975	-73	7.35	35	0.003	-39	0.524	-19
2220	0.972	-74	7.39	30	0.002	-69	0.554	-19
2250	0.968	-76	7.38	25	0.003	-93	0.584	-20
2280	0.964	-77	7.34	20	0.004	-109	0.611	-21
2310	0.958	-79	7.26	16	0.004	-118	0.635	-23
2340	0.950	-80	7.18	12	0.005	-126	0.658	-24
2370	0.942	-82	7.14	8	0.007	-133	0.678	-26
2400	0.934	-83	7.14	4	0.008	-138	0.695	-28
2430	0.927	-84	7.15	1	0.009	-145	0.712	-29
2460	0.920	-85	7.16	-3	0.010	-150	0.726	-31
2490	0.912	-87	7.17	-8	0.011	-154	0.738	-33
2520	0.905	-88	7.14	-12	0.012	-158	0.749	-34
2550	0.897	-89	7.07	-16	0.013	-161	0.758	-36
2580	0.891	-91	6.95	-20	0.014	-163	0.766	-38

MRFIC1808

Table 3. Scattering Parameters

($V_{DD} = 5.0\text{ V}$, $T_A = 25^\circ\text{C}$, Rx Enable = 3.0 V, 50 Ω System)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	ϕ	S ₂₁	ϕ	S ₁₂	ϕ	S ₂₂	ϕ
1500	0.876	-42	3.50	150	0.012	87	0.799	-59
1530	0.883	-43	3.73	146	0.012	85	0.773	-61
1560	0.891	-44	3.98	141	0.012	83	0.744	-63
1590	0.898	-45	4.25	137	0.012	80	0.712	-65
1620	0.906	-46	4.52	132	0.012	77	0.677	-67
1650	0.914	-47	4.80	127	0.012	74	0.640	-68
1680	0.921	-48	5.08	122	0.012	71	0.600	-69
1710	0.928	-49	5.36	117	0.012	67	0.559	-70
1740	0.936	-51	5.63	112	0.012	64	0.517	-70
1770	0.944	-52	5.90	107	0.012	60	0.475	-70
1800	0.950	-53	6.16	102	0.011	57	0.435	-69
1830	0.956	-55	6.41	96	0.011	54	0.397	-66
1860	0.961	-56	6.66	91	0.010	50	0.365	-62
1890	0.965	-58	6.89	85	0.010	47	0.339	-57
1920	0.967	-59	7.10	80	0.009	43	0.323	-51
1950	0.968	-61	7.29	74	0.009	39	0.318	-44
1980	0.969	-62	7.44	69	0.008	35	0.323	-37
2010	0.970	-64	7.56	64	0.007	29	0.338	-31
2040	0.969	-66	7.66	58	0.006	24	0.361	-26
2070	0.966	-67	7.75	53	0.006	18	0.389	-23
2100	0.963	-69	7.84	48	0.005	10	0.420	-21
2130	0.960	-70	7.91	43	0.004	0	0.453	-19
2160	0.957	-72	7.98	38	0.003	-15	0.485	-19
2190	0.954	-73	8.04	34	0.003	-34	0.517	-19
2220	0.951	-75	8.08	29	0.002	-59	0.547	-20
2250	0.946	-76	8.07	24	0.003	-83	0.576	-21
2280	0.942	-78	8.02	19	0.003	-104	0.603	-22
2310	0.936	-79	7.93	14	0.004	-116	0.629	-23
2340	0.928	-81	7.84	10	0.005	-125	0.652	-24
2370	0.920	-82	7.80	7	0.006	-132	0.672	-26
2400	0.912	-83	7.79	3	0.007	-138	0.690	-28
2430	0.904	-84	7.79	-1	0.008	-143	0.707	-29
2460	0.896	-86	7.81	-5	0.009	-148	0.720	-31
2490	0.889	-87	7.81	-9	0.010	-152	0.733	-33
2520	0.882	-88	7.78	-13	0.011	-155	0.744	-34
2550	0.874	-89	7.69	-17	0.012	-158	0.754	-36
2580	0.869	-91	7.56	-21	0.013	-161	0.762	-38

The MRFIC Line 1.9 GHz GaAs Upconverter

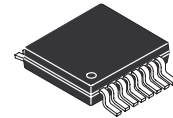
Designed primarily for use in wireless Personal Communication Systems (PCS) applications such as Digital European Cordless Telephone (DECT), Japan's Personal Handy System (PHS) and the emerging North American systems. The MRFIC1813 is also applicable to 2.4 GHz ISM equipment. The device combines a balanced upmixer and a transmit exciter amplifier in a low-cost TSSOP-16 package. Minimal off-chip matching is required while allowing for maximum flexibility and efficiency. The mixer is optimized for low-side injection and provides more than 12 dB of conversion gain with over 0 dBm output at 1 dB gain compression. Image filtering is implemented off-chip to allow maximum flexibility. A CMOS compatible ENABLE pin allows standby operation where the current drain is less than 250 μ A.

Together with other devices from the MRFIC180X or the MRFIC240X series, this GaAs IC family offers the complete transmit and receive functions, less LO and filters, needed for a typical 1.8 GHz cordless telephone or 2.4 GHz ISM band equipment.

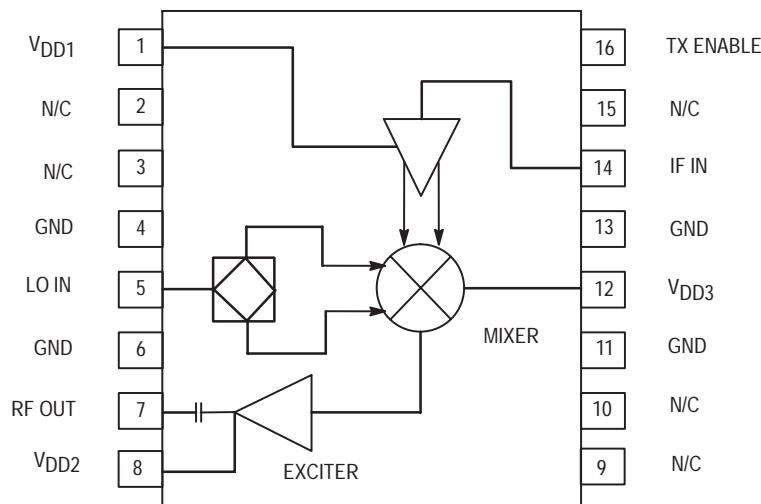
- Usable Frequency Range = 1.7 to 2.5 GHz
- 15 dB Typ IF to RF Conversion Gain
- 3 dBm Power Output Typ, 0 dBm Minimum at 1 dB Gain Compression
- Simple Off-chip Matching for Maximum Flexibility
- Low Power Consumption = 75 mW (Typ)
- Single Bias Supply = 2.7 to 4.5 Volts
- Low LO Power Requirement = - 5 dBm (Typ)
- Low Cost Surface Mount Plastic Package
- Order MRFIC1813R2 for Tape and Reel.
R2 Suffix = 2,500 Units per 16 mm, 13 inch Reel.
- Device Marking = M1813

MRFIC1813

1.9 GHz UPMIXER AND EXCITER AMPLIFIER



CASE 948C-03
(TSSOP-16)



Pin Connections and Functional Block Diagram

MAXIMUM RATINGS ($T_A = 25^\circ\text{C}$ unless otherwise noted)

Ratings	Symbol	Limit	Unit
Supply Voltage	$V_{DD1}, V_{DD2}, V_{DD3}$	5.5	Vdc
IF Input Power	P_{IF}	3	dBm
LO Input Power	P_{LO}	3	dBm
Enable Voltage	TX ENABLE	5.5	Vdc
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Ambient Temperature	T_A	-30 to +85	$^\circ\text{C}$

RECOMMENDED OPERATING RANGES

Parameter	Symbol	Value	Unit
RF Output Frequency	f_{RF}	1.7 to 2.5	GHz
LO Input Frequency	f_{LO}	1.5 to 2.4	GHz
IF Input Frequency	f_{IF}	70 to 350	MHz
Supply Voltage	V_{DD}	2.7 to 4.5	Vdc
TX Enable Voltage, ON	TX ENABLE	2.7 to V_{DD}	Vdc
TX Enable Voltage, OFF	TX ENABLE	0 to 0.2	Vdc

ELECTRICAL CHARACTERISTICS ($V_{DD1,2,3}, TX\ ENABLE = 3\text{ V}, T_A = 25^\circ\text{C}, f_{LO} = 1.65\text{ GHz @ } -5\text{ dBm}, f_{IF} = 250\text{ MHz @ } -15\text{ dBm}$)

Characteristic	Min	Typ	Max	Unit
IF to RF Small Signal Conversion Gain ($P_{RF} = -35\text{ dBm}$)	12	15	—	dB
RF Output 1 dB Gain Compression	0	3	—	dBm
RF Output 3rd Order Intercept	—	11	—	dBm
LO Feedthrough to RF Port	—	-15	-10	dBm
Noise Figure	—	11	—	dB
Lower Sideband Output Power at RF Port	—	-10	-6	dBm
Supply Current TX Mode	—	25	35	mA
Supply Current Standby Mode (TX ENABLE = 0 V, LO Off)	—	100	250	μA
TX Enable Current	—	3	—	μA

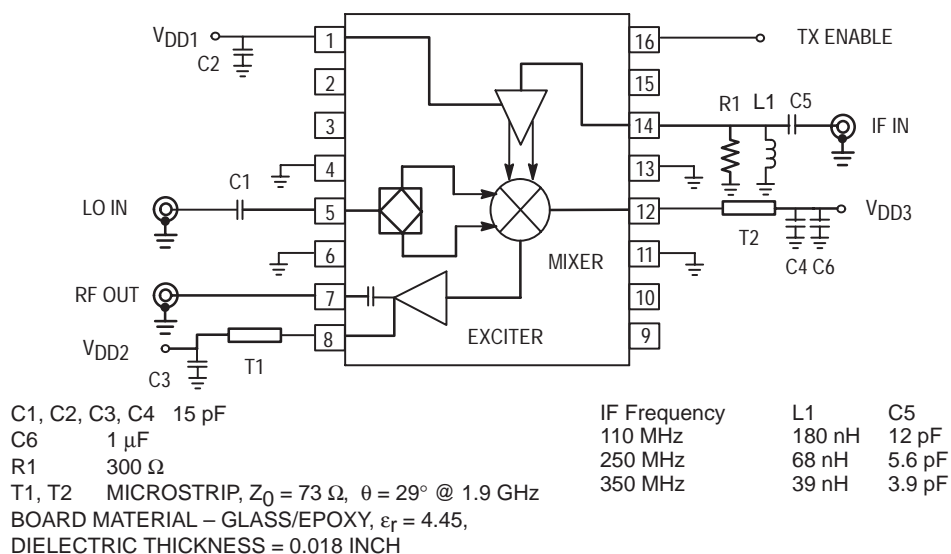


Figure 1. Applications Circuit Configuration

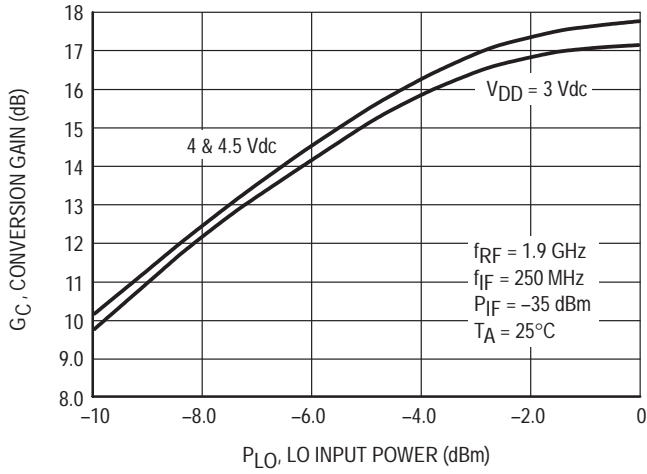


Figure 2. Conversion Gain versus LO Power

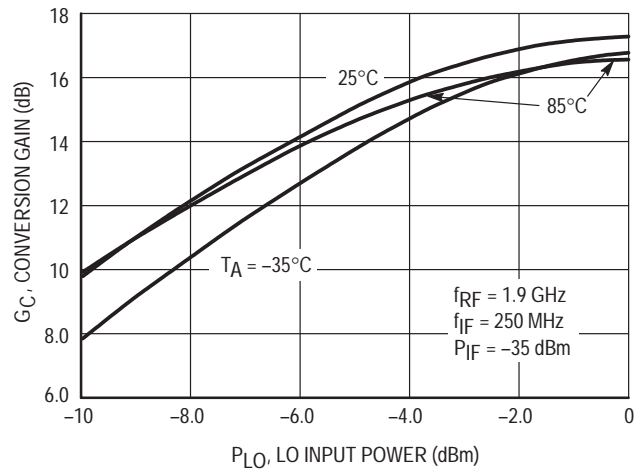


Figure 3. Conversion Gain versus LO Power

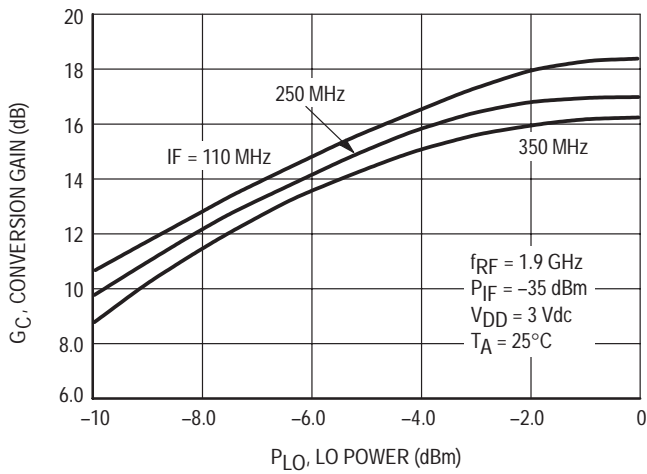


Figure 4. Conversion Gain versus LO Power

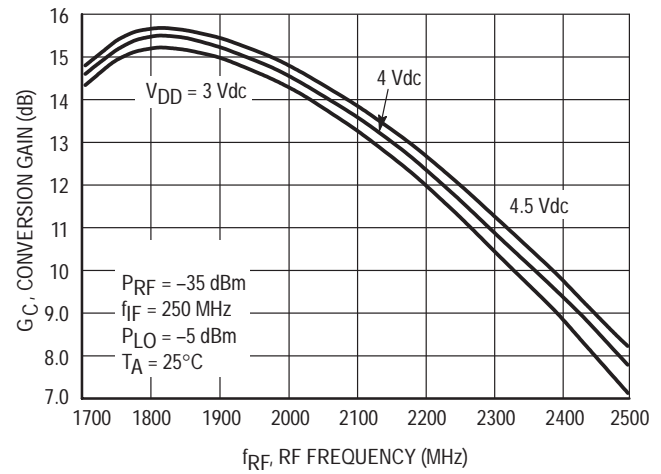


Figure 5. Conversion Gain versus RF Frequency

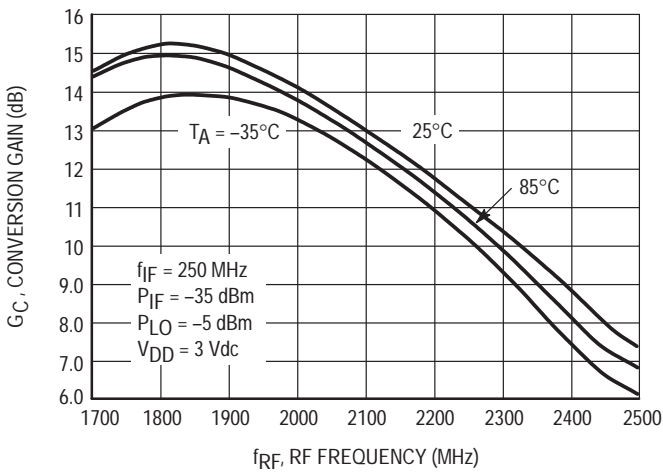


Figure 6. Conversion Gain versus RF Frequency

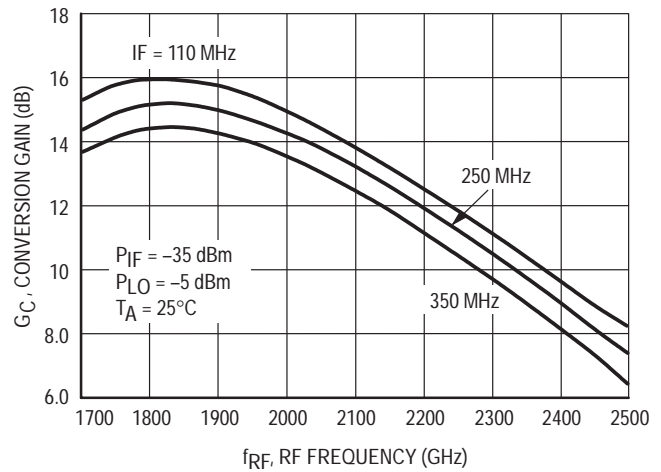


Figure 7. Conversion Gain versus RF Frequency

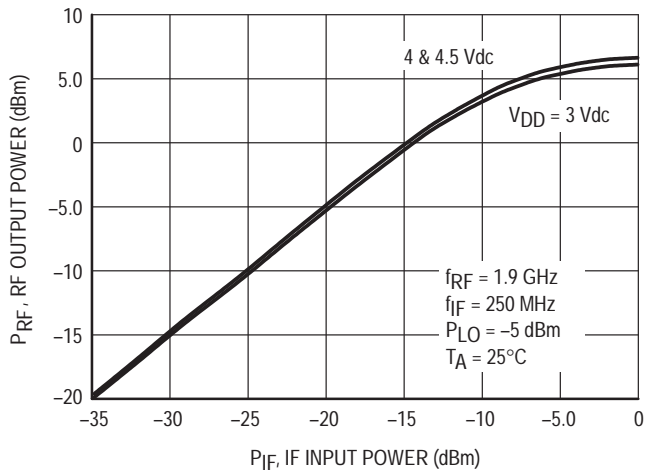


Figure 8. RF Output versus Input Power

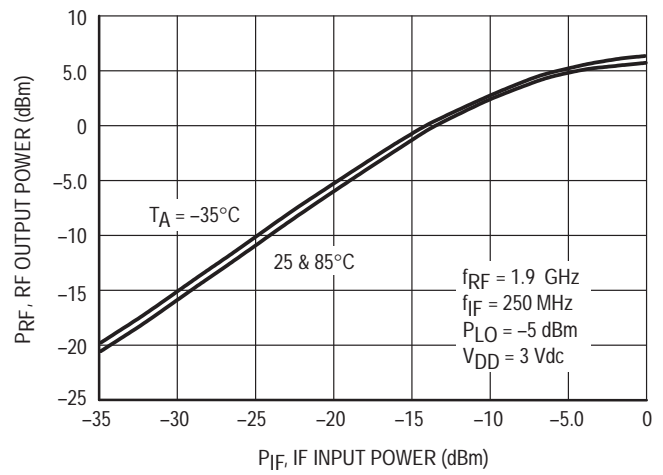


Figure 9. RF Output Power versus IF Input Power

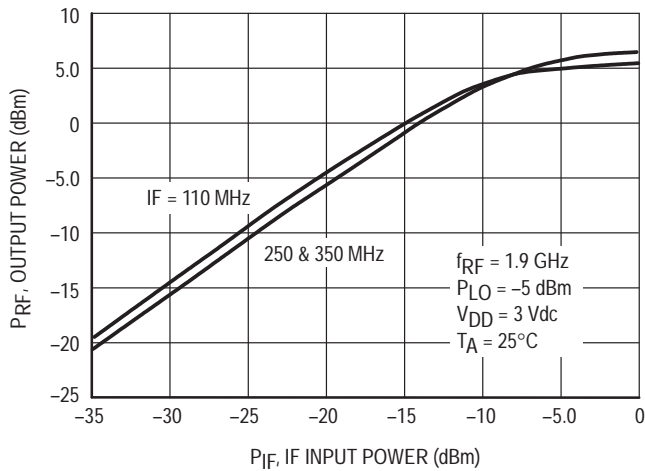


Figure 10. RF Output versus IF Input Power

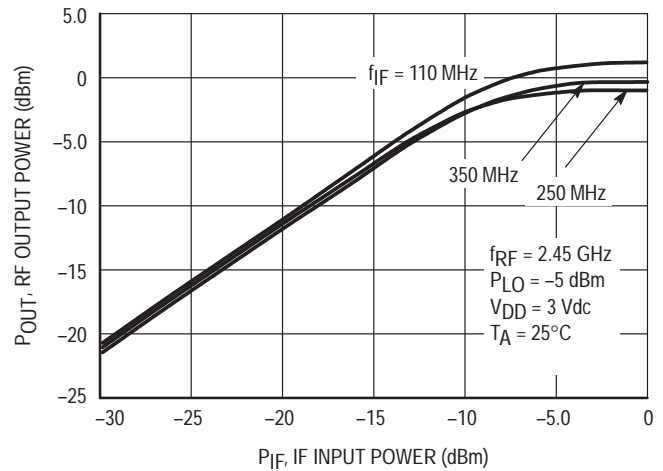


Figure 11. Output Power versus IF Input Power

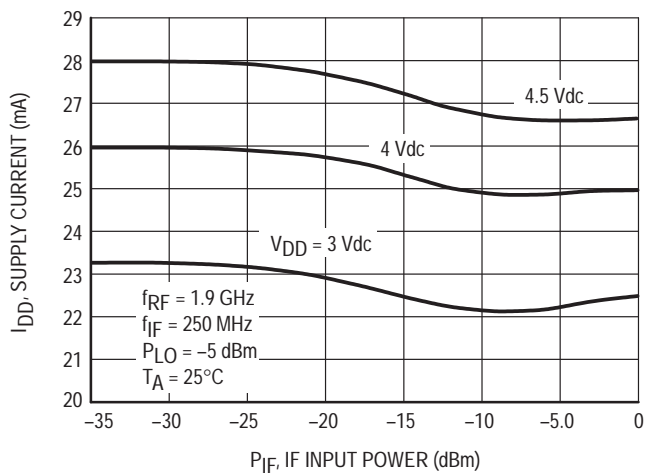


Figure 12. Supply Current versus IF Input Power

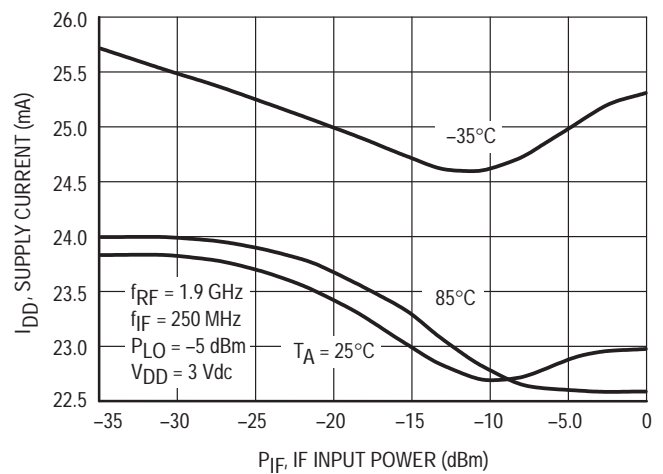


Figure 13. Supply Current versus IF Input Power

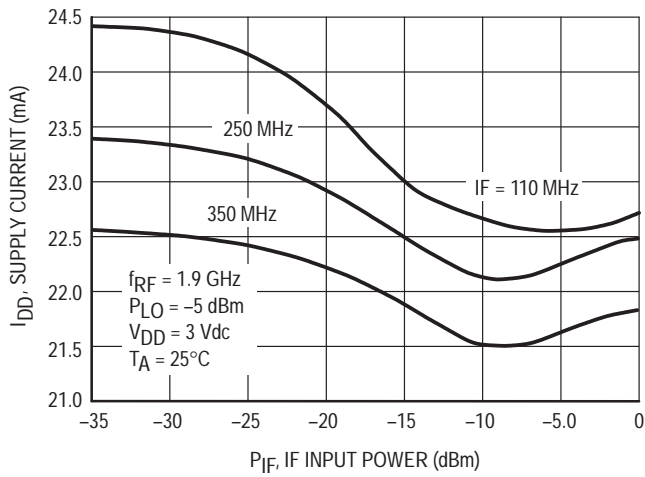


Figure 14. Supply Current versus IF Input Power

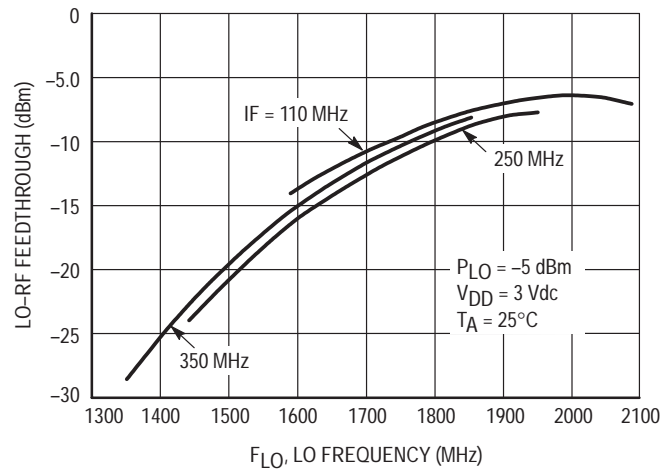


Figure 15. LO to RF Feedthrough versus LO Frequency

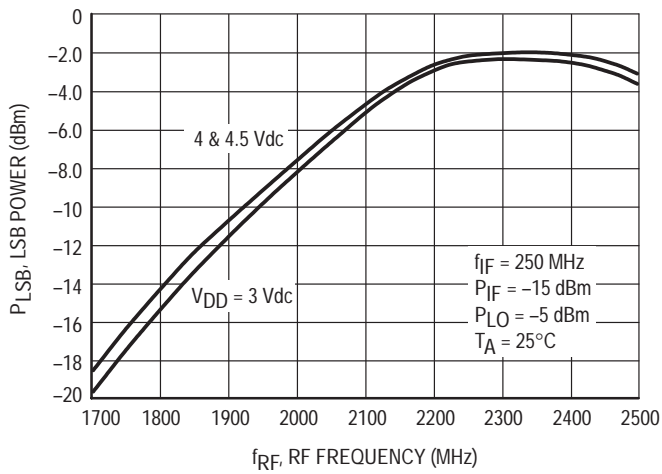


Figure 16. Lower Side Band Power versus RF Frequency

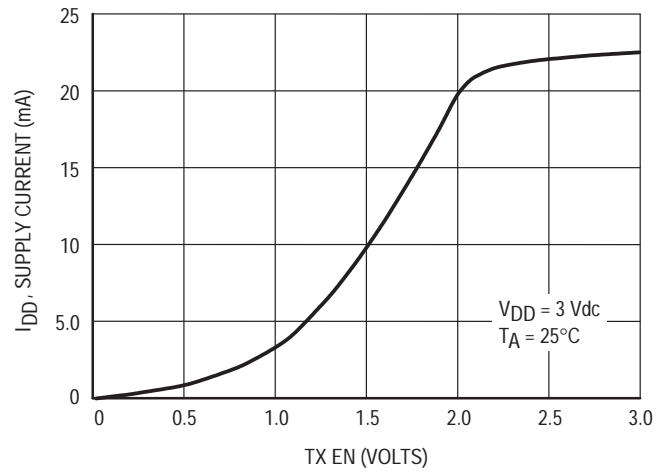


Figure 17. Supply Current versus Transmit Enable Voltage

f (MHz)	IF Input		LO Input		RF Output (1)	
	R	jX	R	jX	R	jX
70	8.3	-452.4				
100	7.3	-318.5				
150	7.1	-211.3				
200	6.6	-156.4				
250	6.5	-123.1				
300	6.1	-100.7				
350	5.7	-84.2				
1100			62.5	3.1		
1200			58.1	4.3		
1300			53.7	4.7		
1400			50.2	4.2		
1500			47.3	3.9		
1600			44.4	3.2		
1700			42.0	1.6	30.4	33.6
1800			40.6	0.5	42.6	16.9
1900			39.6	-0.7	49.1	2.3
2000			38.7	-2.2	40.6	14.2
2100			38.2	-3.6	33.8	17.7
2200			38.4	-5.1	33.3	15.7
2300			38.9	-6.5	32.9	13.7
2400			39.5	-7.8	29.6	13.2
2500					27.4	11.9

(1) Includes T1 shown in Figure 1.

Table 1. Port Impedances versus Frequency
(V_{D1}, V_{D2}, V_{D3}, TX EN = 3 Vdc)

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

The MRFIC1813 combines a single-balanced MESFET mixer with an exciter amplifier. It is usable for transmit frequencies from 1.7 to 2.5 GHz and IF frequencies from 70 to 350 MHz. The design is optimized for low-side local oscillator injection in heterodyne transmit applications.

Minimal off-chip matching is required while allowing for flexibility and performance optimization. An active balun is employed at the IF port which gives good balance down to at least 70 MHz. A passive splitter is used at the LO input to complete the single-balanced configuration.

CIRCUIT CONSIDERATIONS

Figure 1 shows the application circuit used to gather the data presented in the characterization curves. As shown in Table 1, the IF port impedance is very high. Three hundred ohms was chosen for R1 to shunt the IF port as a compromise of gain and bandwidth. A 50 Ω resistor can be used and L1 and C5 eliminated to provide a broadband match. The

conversion gain is reduced to about 8 dB. Microstrip inductors T1 and T2 combine with inductance internal to the device to form RF chokes. Some tuning of the RF output can be achieved with T1.

As with all RF devices, circuit layout is important. Controlled impedance lines should be used for all RF and IF interconnects. As shown in Figure 1, power supply bypassing should be used to avoid device instability. Ground vias should be included near all ground connections indicated in the schematic. Off-chip components should be mounted as close to the IC leads as possible.

EVALUATION BOARDS

Evaluation boards are available for RF Monolithic Integrated Circuits by adding a "TF" to the device type. For a complete list of currently available boards and one in development for newly introduced products, please contact your local Motorola Distributor or Sales Office.



MOTOROLA

3.6 V 1800 MHz GaAs Integrated Power Amplifier

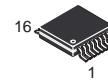
The MRFIC1819 is a single supply, RF power amplifier designed for the 1W DCS1800/PCS1900 handheld radio. The negative power supply is generated inside the chip using RF rectification, which avoids any spurious signal. A built in priority switch is provided to prevent Drain Voltage being applied on the RF lineup if not properly biased by the Negative Voltage. The device is packaged in the TSSOP-16EP package, with exposed backside pad, which allows excellent electrical and thermal performance through a solderable contact.

- Target 3.6 V Characteristics:
 - RF Input Power: 6.0 dBm
 - RF Output Power: 33 dBm Typical
 - Efficiency: 41% Typical
- Single Positive Supply Solution
- Negative Voltage Generator
- Positive Step-Up Voltage Generator
- V_{SS} Check Switch for Gate-Drain Priority

MRFIC1819

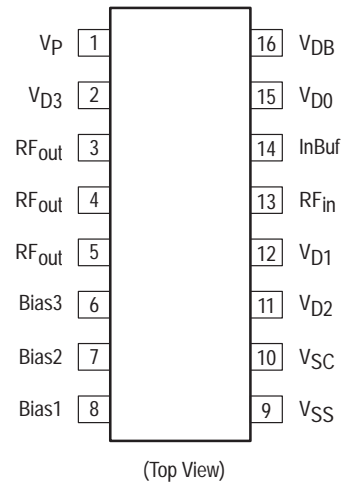
INTEGRATED RF POWER AMPLIFIER DCS1800/PCS1900

SEMICONDUCTOR TECHNICAL DATA

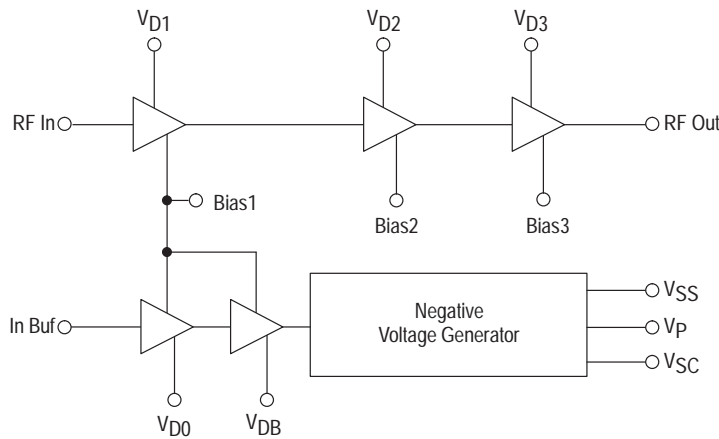


PLASTIC PACKAGE
CASE 948L
(TSSOP-16EP, Tape and Reel Only)

PIN CONNECTIONS



Simplified Block Diagram



This device contains 9 active transistors.

ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC1819R2	T _A = -40 to 85°C	TSSOP-16EP

MRFIC1819

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Supply Voltage	$V_{D1, 2, 3}$	6.0	V
RF Input Power	P_{in}	12	dBm
RF Output Power	P_{out}	36	dBm

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions or Electrical Characteristics tables.
 2. ESD (electrostatic discharge) immunity meets Human Body Model (HBM) ≤ 250 V and Machine Model (MM) ≤ 60 V. This device is rated Moisture Sensitivity Level (MSL) 4. Additional ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Voltage	$V_{D0}, V_{DB}, V_{D1, 2, 3}$	3.0	–	5.0	Vdc
Input Power	P_{in}	5.0	–	10	dBm
Input Frequency	f_{RF}	1700	–	1900	MHz
Operating Case Temperature Range	T_C	–40	–	85	$^{\circ}C$
Storage Temperature Range	T_{stg}	–55	–	150	$^{\circ}C$

ELECTRICAL CHARACTERISTICS ($V_{D0} = V_{DB} = 3.6$ V, $V_{D1, 2, 3} = 3.6$ V, $P_{in} = 6.0$ dBm, Peak measurement at 12.5% duty cycle, 4.6 ms Period, $T_A = 25^{\circ}C$, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	1710	–	1785	MHz
Output Power	P_{out}	32	33	–	dBm
Power Added Efficiency	PAE	35	41	–	%
Output Power (Tuned for PCS Band 1850 to 1910 MHz)	P_{out}	–	33	–	dBm
Power Added Efficiency (Tuned for PCS Band 1850 to 1910 MHz)	PAE	–	41	–	%
Output Power at low voltage ($V_{D0} = V_{DB} = 3.0$ V, $V_{D1, 2, 3} = 3.0$ V)	P_{out}	30.5	31	–	dBm
Harmonic Output	–	–	–	–	dBc
$2f_o$		–	–45	–40	
$3f_o$		–	–35	–30	
Input Return Loss	S11	–	12	–	dB
Output Power Isolation ($P_{in} = 10$ dBm, $V_{D0} = V_{DB} = 3.0$ V, $V_{D1, 2\&3} = 0$ V)	P_{off}	–	–30	–	dBm
Noise Power (In 100 kHz, 1805 to 1880 MHz)		–	–90	–	dBm
Negative Voltage ($P_{in} = 6.0$ dBm, $V_{D0} = V_{DB} = 3.0$ V)	V_{SS}	–4.85	–	–	V
Negative Voltage Setting Time ($P_{in} = 6.0$ dBm, $V_{D0} = V_{DB}$ stepped from 0 to 3.0 V)	T_s	–	0.7	–	μs
Positive Voltage ($P_{in} = 6.0$ dBm, $V_{D0} = V_{DB} = 3.0$ V)	V_P	5.7	6.6	–	V
Stability–Spurious Output ($P_{out} = 0$ to 33 dBm, Load VSWR 6:1 all phase angles, source VSWR = 3:1, at any phase angle, Adjust $V_{D1, 2\&3}$ for specified power)	P_{spur}	–	–	–60	dBc
Load Mismatch Stress ($P_{out} = 3$ to 33 dBm, Load VSWR = 10:1 all phase angles, 5 seconds, Adjust $V_{D1, 2\&3}$ for specified power)		No Degradation in Output Power Before & After Test			

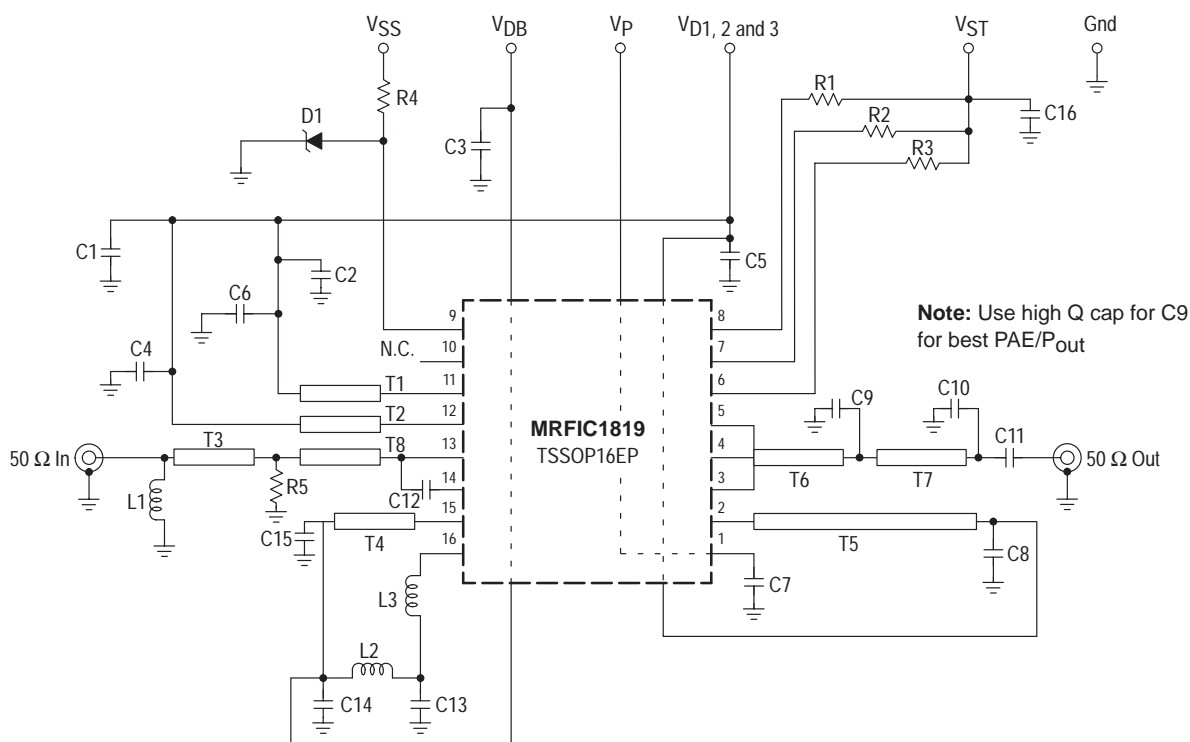
MRFIC1819

Table 1. Optimum Loads Derived from Circuit Characterization

f MHz	Z _{in} OHMS		Z _{OL} [*] OHMS	
	R	jX	R	jX
1710	14.51	-66.87	5.88	3.30
1720	14.67	-67.40	5.86	3.20
1730	14.82	-68.07	5.79	3.10
1740	15.08	-68.73	5.74	2.93
1750	15.30	-69.29	5.67	2.75
1760	15.55	-69.80	5.59	2.58
1770	15.80	-70.30	5.53	2.46
1780	16.00	-70.89	5.44	2.28
1790	16.16	-71.20	5.42	2.25

Z_{in} represents the input impedance of the device.
Z_{OL}^{*} represents the conjugate of the optimum output load to present to the device.

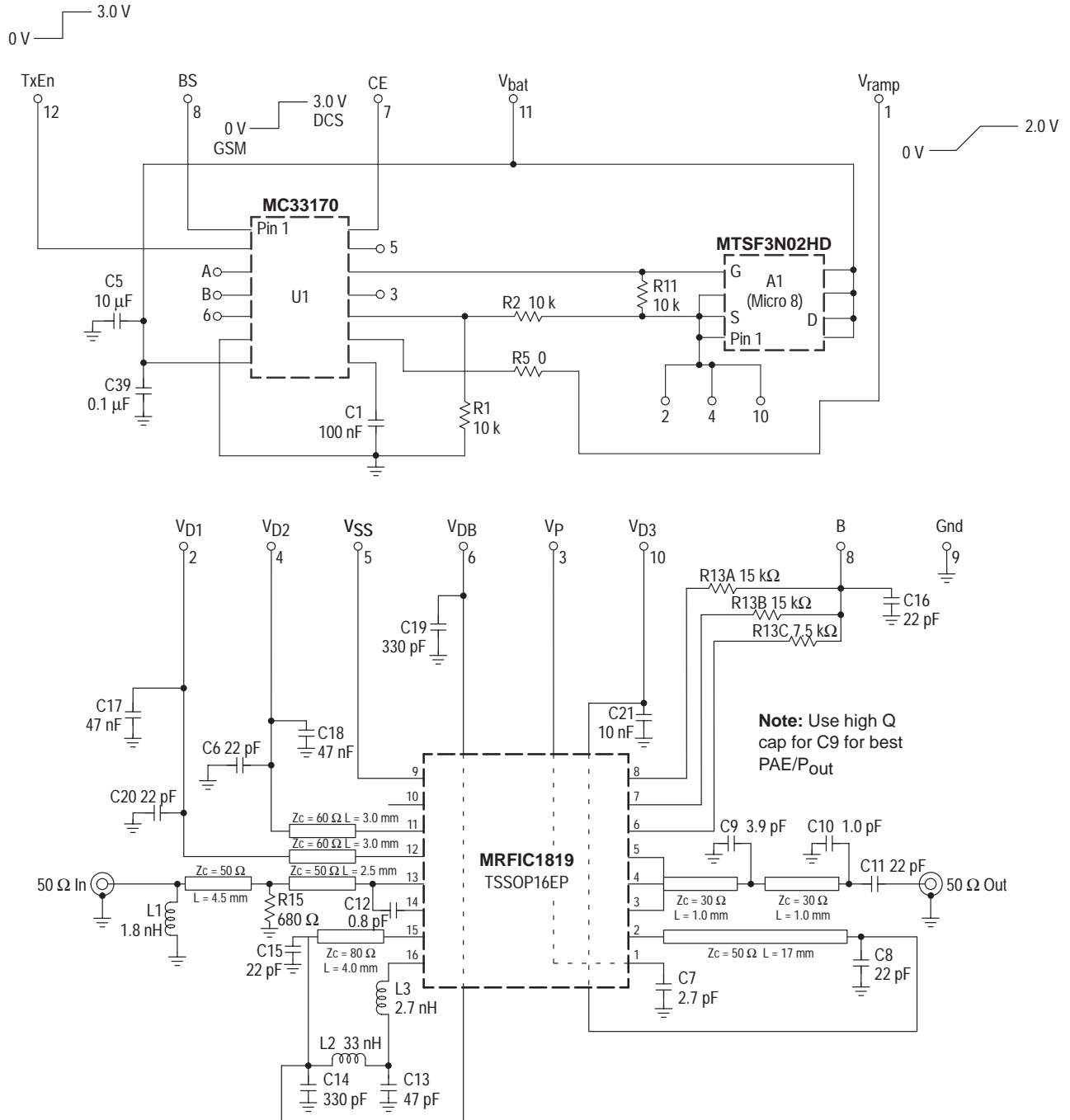
Figure 1. Reference Circuit



C1,C2	47 nF	R4	1.0 kΩ
C3,C14	330 pF	R5	680 Ω
C4,C6,C8,C11, C15,C16	22 pF	L1	1.8 nH
C5	10 nF	L2	33 nH
C7	2.7 pF	L3	2.7 nH
C9	3.9 pF AVX Accu-F	D1	Zener 5.1 V MMSZ4689T1
C10	1.0 pF	T1, T2	60 Ω Microstrip Line, L = 3.0 mm
C12	0.8 pF	T3	50 Ω Microstrip Line, L = 4.5 mm
C13	47 pF	T4	80 Ω Microstrip Line, L = 4.0 mm
R1,R2	15 kΩ	T5	50 Ω Microstrip Line, L = 17 mm
R3	7.5 kΩ	T6,T7	30 Ω Microstrip Line, L = 1.0 mm
		T8	50 Ω Microstrip Line, L = 2.5 mm

MRFIC1819

Figure 2. 3.6 V DCS Application Circuit



MRFIC1819

Figure 3. 3.6 V GSM & DCS IPA Dual-Band Application Circuit with Companion Chip & NMOS Switch

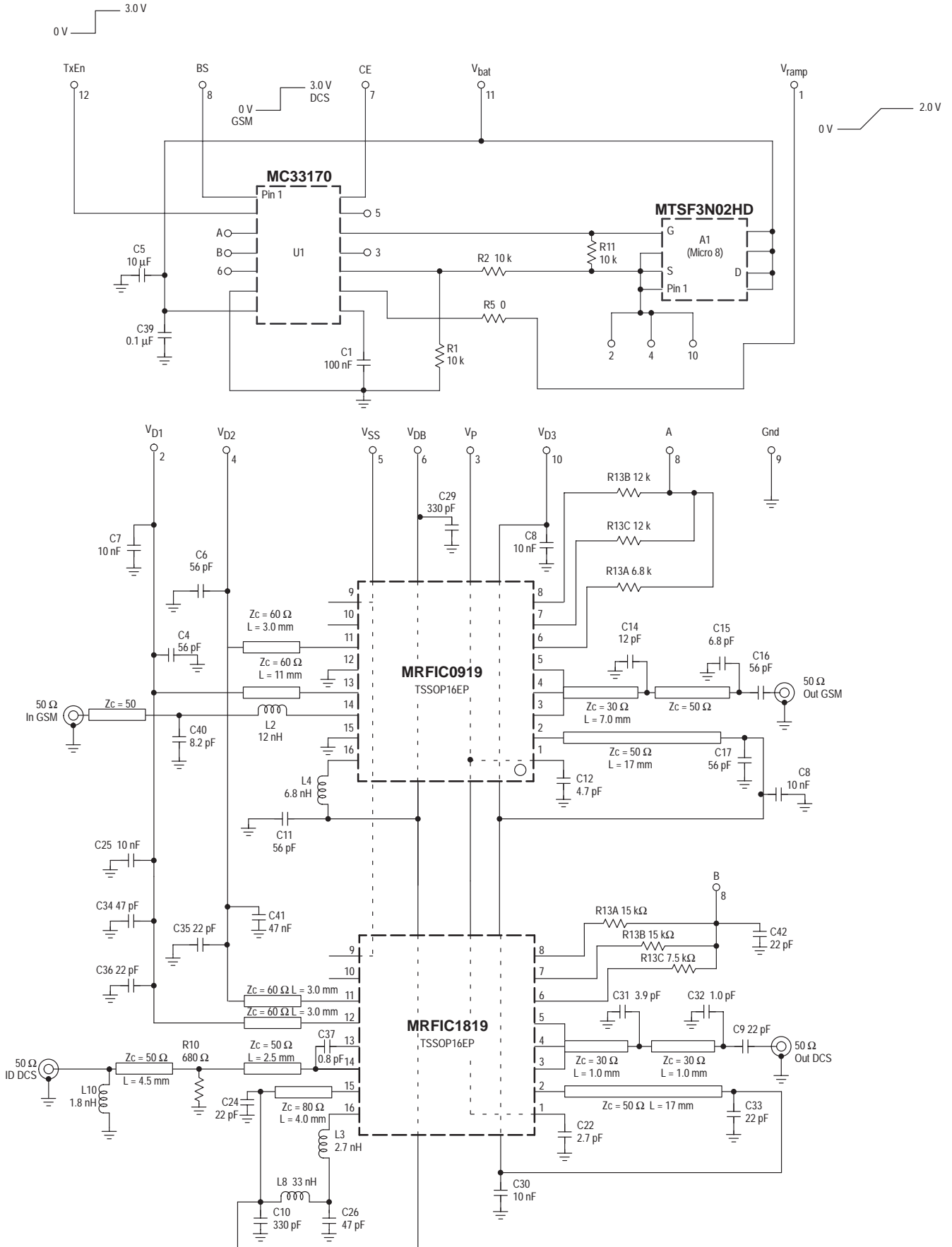


Figure 4. Output Power versus Frequency

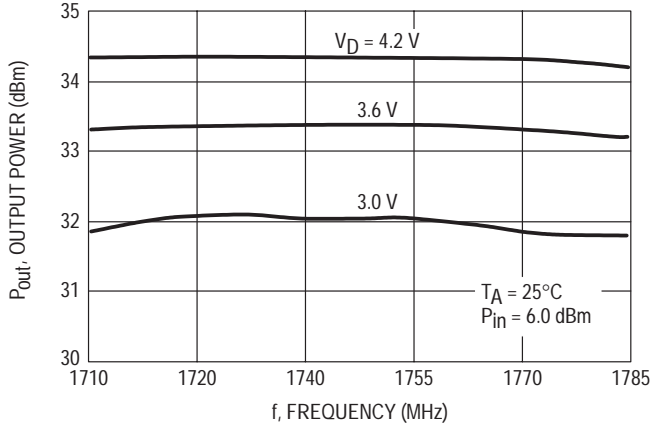


Figure 5. Power Added Efficiency versus Frequency

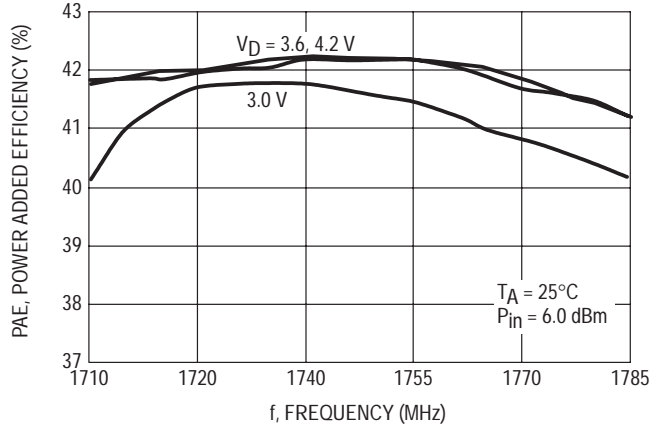


Figure 6. Output Power versus Frequency

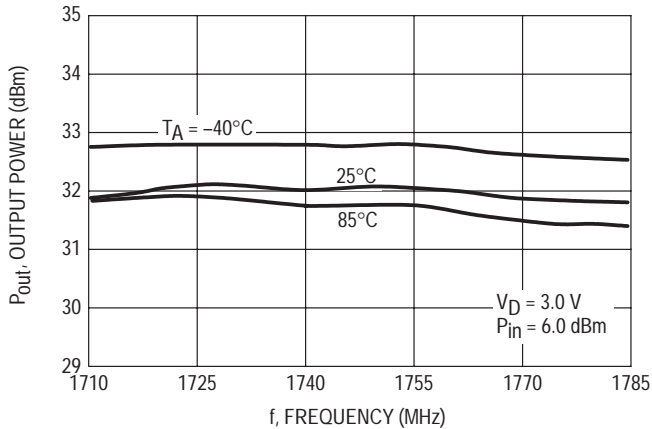


Figure 7. Output Power versus Frequency

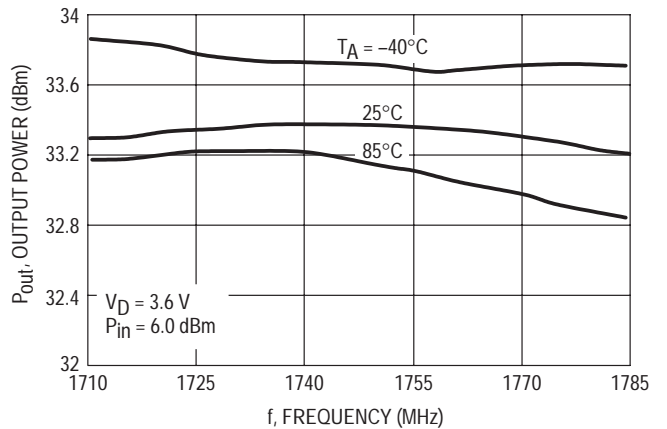


Figure 8. Output Power versus Frequency

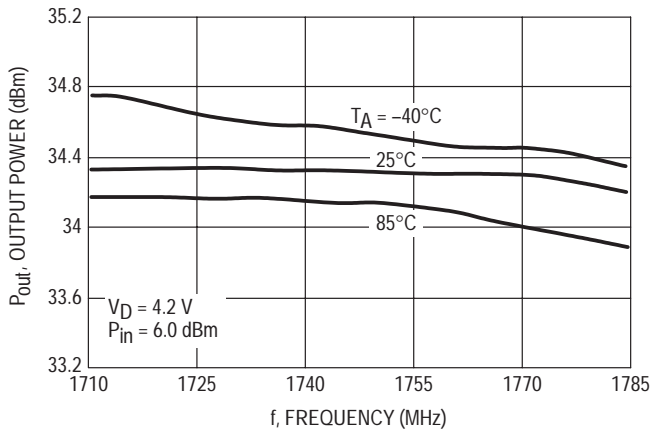


Figure 9. Power Added Efficiency versus Frequency

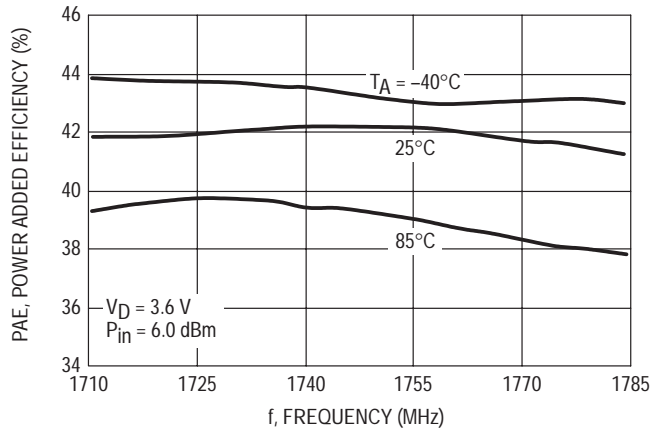


Figure 10. Output Power versus Drain Voltage

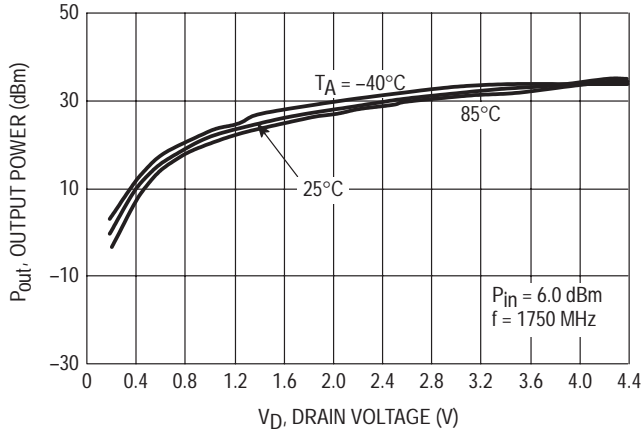


Figure 11. Power Added Efficiency versus Drain Voltage

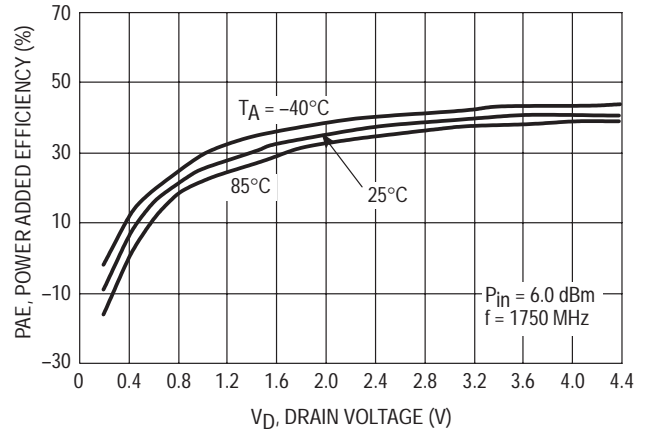


Figure 12. Positive Voltage Generator Output versus Drain Voltage

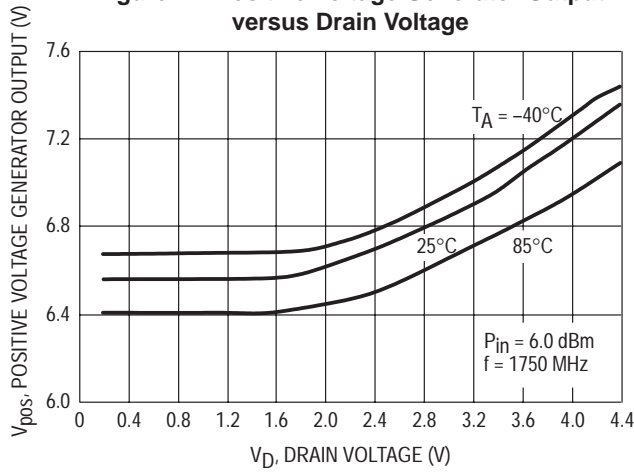
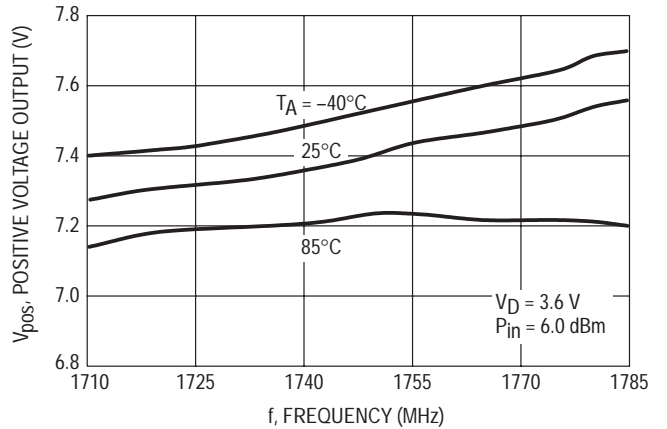


Figure 13. Positive Voltage Output versus Frequency



MRFIC1819

APPLICATIONS INFORMATION

Design Philosophy

The MRFIC1819 is a high performance three stage GaAs IPA (Integrated Power Amplifier) designed for DCS/PCS handheld radios (1710–1785 MHz DCS frequency band, 1850–1910 MHz PCS frequency band). With a 3.6 V battery supply, it delivers typically 33 dBm of Output Power with 41% Power Added Efficiency.

It features an internal Negative Voltage Generator based on RF rectification of the input carrier after its amplification by two dedicated buffer stages (see Internal Block Diagram). This method eliminates spurs found on the Output signal when using dc/dc converter type negative voltage generators, either on or off chip. The buffer also generates a step-up positive voltage which can be used to drive a N–MOS drain switch.

The RF input power is split **externally** (different from MRFIC0919) to the 3 stage RF line-up (Q1, Q2 and Q3) and the Buffer amplifier (Q0, QB). This arrangement allows separate operation of Voltage Generation and Power Amplification for maximum flexibility.

External Circuit Considerations

The MRFIC1819 can be tuned by changing the values and/or positions of the appropriate external components (see Figure 1: Reference Circuit). While tuning the RF line-up, it is recommended to apply external negative supply in order to prevent any damage to the power amplifier stages. Poor tuning on the input may not provide enough RF power to operate the negative voltage generator properly.

Input matching is a shunt–L, series–L high-pass structure and should be optimized at the rated RF Input power (e.g. 6.0 dBm). However, broadband matching is easier with a parallel 680 Ω resistor. This part can be removed to get operation to a lower input power (e.g. 5.0 dBm). Since the Input line feeds both 1st stage and buffer, Input matching should be iterated with Buffer and Q1 drain matching. Note that a dc blocking capacitor is included on chip.

RF input signal is fed to buffer amplifier using C12 capacitor (Figure 1). The value of this capacitor determines the power split between RF line-up and buffer amplifier. C12 has been tuned to get the best trade-off between RF gain and negative voltage on Pin 9.

First stage buffer amplifier is tuned with a short 80 Ω microstrip line which may be replaced by a chip inductor (T4 on Figure 1). Second stage buffer amplifier is supplied and matched through a discrete chip inductor. Those two elements are tuned to get the maximum output from voltage generator. The overall typical buffer current is about 50 mA; however, the negative generator needs a settling time of 2.0 μ sec (see burst mode paragraph). During this transient period of time, both stages are biased to IDSS which is about 200 mA each.

The step-up positive voltage available at Pin 1 is both decoupled and maximised by a small shunt capacitor. This positive voltage which is approximately twice the buffer drain voltage can be used to drive a NMOS drain switch for best performances.

Q1 drain is supplied and matched through a printed microstrip line that could be replaced by a discrete chip inductor as well. Its length (or equivalent inductor value) is tuned by sliding the RF decoupling capacitor along to get the maximum gain on the first stage.

Q2 is supplied through a printed microstrip line that contributes also to the interstage matching in order to provide optimum drive to the final stage.

The line length for Q1 and Q2 is small, so replacing it with a discrete inductor is not practical.

Q3 drain is fed via a printed line that must handle the high supply current of that stage (2.0 Amp peak) without significant voltage drop. This line can be buried in an inner layer to save PCB space or be a discrete RF choke.

Output matching is accomplished with a two stages low-pass network. Easy implementation is achieved with shunt capacitors mounted along a 2.0 mm 30 Ω microstrip transmission line. Value and position are chosen to reach a load line of 5.5 Ω while conjugating the device output parasitics. The network must also properly terminate the second and third harmonic to optimize efficiency and reduce harmonic level. Use of high Q capacitor for the first output matching capacitor circuit is recommended in order to get the best Output Power and Efficiency performance.

NOTE: The choice of output matching capacitors type and supplier will affect H2 and H3 level and efficiency, because of series resonant frequency.

Biasing Considerations

The internally generated negative voltage is clamped by an external Zener diode in order to eliminate variation linked to Input power or Buffer supply. This negative voltage is used by three independent bias circuits to set the proper quiescent current of all stages. Each bias circuitry is equivalent to a current source sinking its value from the bias pin. When the bias pins are set to 3.0 V, nominal quiescent current and operating point of each RF stage are selected.

Q1 and Buffer share the Bias1 (0.25 mA) while Q2 and Q3 have dedicated Bias2 (0.25 mA) and Bias3 (0.5 mA) respectively. It is also possible to reference those bias pins to Gnd by changing series resistors R1, R2, R3 (Figure 1) that drops the 3.0 V.

If those pins are left opened, the corresponding stages are pinched-off. Thus the bias pins can be used as a mean to select the MRFIC1819 or the MRFIC0919 in a dual band configuration. The MRFIC0919 is the partner device to the MRFIC1819 and is designed for GSM900 applications.

Table 2. Pin Function Description

Pin	Symbol	Description
1	V _P	Positive voltage output
2	V _{D3}	Third stage drain supply
3	RF Out	RF output
4	RF Out	RF output
5	RF Out	RF output
6	Bias3	Third stage bias
7	Bias2	Second stage bias
8	Bias1	Buffer and first stage bias
9	V _{SS}	Negative voltage output
10	V _{SC}	Negative voltage check
11	V _{D2}	Second stage drain supply
12	V _{D1}	First stage drain supply
13	RF In	RF input
14	In Buf	Buffer RF input
15	V _{D0}	First buffer stage drain supply
16	V _{DB}	Buffer stage drain supply

V_{SC} is an open drain internal FET switch which is biased through the negative voltage. Consequently, this pin is high impedance when negative voltage is okay and low impedance (about 40 Ω) when negative voltage is missing.

Operation Procedure

The MRFIC1819 is a standard MESFET GaAs Power Amplifier, presence of a negative voltage to bias the RF line-up is essential in order to avoid any damage to the parts. Due to the fact that the negative voltage is generated through rectification of the RF input signal, a minimum input power level is needed for correct operation of the demoboard. The following procedure will guaranty safe operation for doing the RF measurements.

Note: make sure that Bias1 (Pin 8 of demoboard Figure 3) is connected 3.0 V or will have equivalent potential for nominal biasing of Buffer stage.

6. Apply RF input power (RF In) > 6.0 dBm.
7. Apply V_{DB} = 3.0 to 5.0 V.
8. Check that V_{SS} reaches approximately -5.1 V (settling of the negative voltage) (Pin 9).
9. Apply V_{D1,2&3} = 3.0 to 5.5 V.
10. Measure RF output power and relevant parameters.

Proceed in the reverse order to switch off the Power Amplifier.

For linear operation, an external negative voltage will have to be supplied to the V_{SS} pin to maintain initial quiescent operating conditions of the FET amplifiers since the RF input will not provide sufficient voltage to operate the negative voltage generator. When using an external negative voltage supply, an input to the buffer (Pin 14) and supply voltages to V_{DB} (Pin 16) and V_{D0} (Pin 15), would no longer be required.

Control Considerations

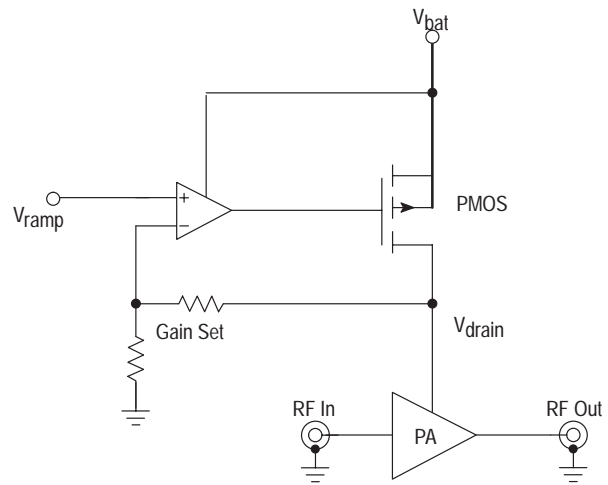
MRFIC01819 application uses the drain control technique developed for our previous range of GaAs IPAs (refer to application note AN1599). This method relies on the fact that for an RF amplifier operating in saturation mode, the RF output power is proportional to the square of the Amplifier drain voltage: P_{out}(Watt)=k*V_D(Volt)*V_D(Volt).

In the proposed application circuit (see Figure 2), a PMOS FET is used to switch the IPA drain and vary the drain supply voltage from 0 to battery voltage. As the PMOS FET has a non linear behavior, an OpAmp is included in the application. This OpAmp is linearizing the PMOS by sensing its drain output and gives a true linear relationship between the Control voltage and the RF output voltage.

The obtained power control transfer function is so linear and repeatable than it can be used to predict the output power within a dynamic range of 25 to 30 dB over frequency and temperature. This so called “open-loop” arrangement eliminates the need for coupler and detector required for the classical but complex closed-loop control and consequently reduces the Insertion Loss from Power Amplifier to the Antenna.

The block diagram (Figure 14) shows the principle of operation as implemented in the application circuit of Figure 2. The OpAmp is connected as an inverter to compensate the negative gain of the PMOS switch.

Figure 14. Drain Control through PMOS Switch



NOTE: The positive voltage generated by the Buffer stage can be used to supply the OpAmp and make it possible to drive a NMOS switch as a voltage follower. Doing so, the main advantage is to have a lower R_{dson} switch and better intrinsic linearity.

In Figure 15, the plot illustrates the “open-loop” performance regarding temperature stability. The measured datas are displayed in a log-log scale in order to have a good representation of both the dynamic and the linearity of control. The variation of P_{out} across the frequency band are also very small (less than 1.0 dB ripple) and are kept to that small amount when controlling P_{out} through the Drain voltage.

MRFIC1819

Figure 15. Temperature Stability of the Open Loop Control

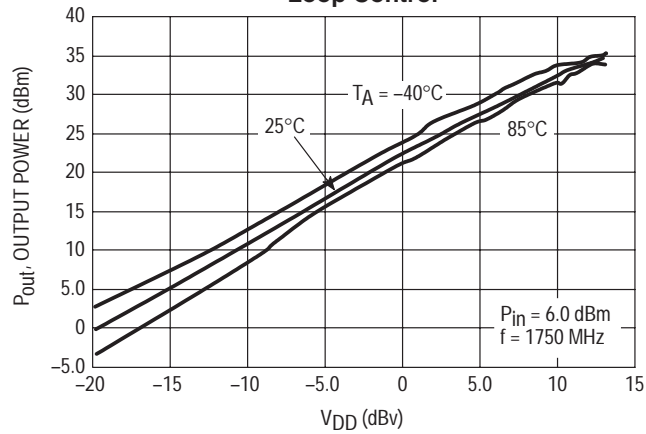
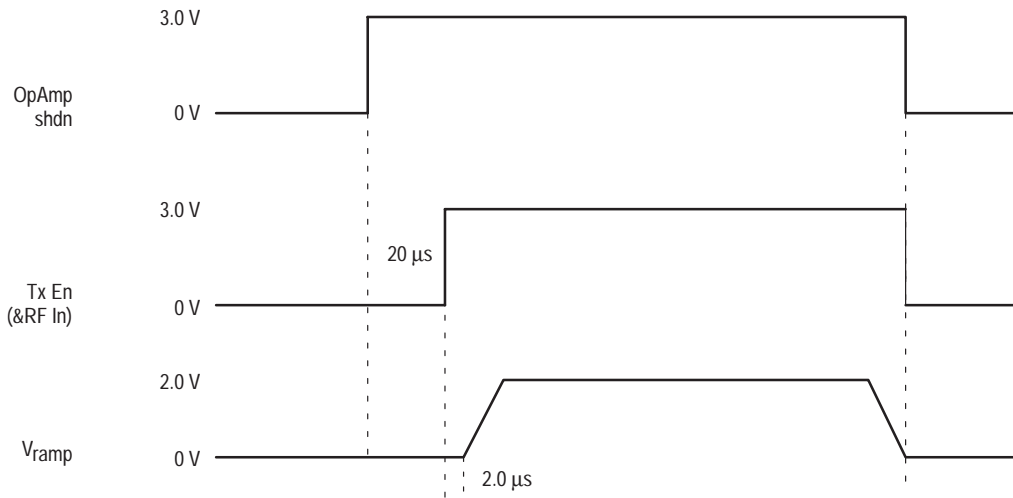


Figure 16. Timing Guide



Burst mode

Use Figure 18 as a guide line to perform burst mode measurements with the complete application circuit of Figure 2. Notice that the V_{SC} pin is connected to V_{ramp} (through a resistor) and acts as a pull down when negative voltage is missing so that drain voltage is not applied to the RF line-up.

- Bursting the OpAmp with its Pin 8 (shdn) is not mandatory during a call as the OpAmp current consumption is very small (1.0 to 2mA). This pin is mainly used for the idle mode of the radio. In any case, the wake-up time of the OpAmp is very short.

- V_{ramp} can be applied soon after Tx EN since the internal negative voltage generator settles in less than 2.0 µs.

- Tx EN signal can be used to switch the input power (using a driver or attenuator) in order to provide higher isolation for on/off burst dynamic.

References (Motorola application notes)

AN1599 – Power Control with the MRFIC0913 GaAs Integrated Power Amplifier and MC33169 Support IC.

AN1602 – 3.6 V and 4.8 V GSM/DCS1800 Dual Band PA Application with DECT capability Using Standard Motorola RFIC's.

Advance Information

1.9 GHz CDMA Upmixer/Exciter

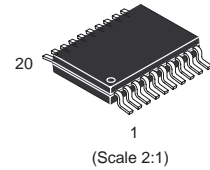
The MRFIC1854A is an integrated upmixer and exciter amplifier designed specifically for PCS CDMA digital cellular radios. The exciter amplifier incorporates a temperature compensated linear gain control and selectable bias to reduce power consumption. The design utilizes Motorola's RF BiCMOS1 process to yield superior performance in a cost effective monolithic device.

- Total Supply Current CDMA Mode = 55 mA Typical
- 65 dB Dynamic Range Gain Control
- Upmixer Output IP3 = 6.0 dBm Typical
- Exciter Output IP3 = 22 dBm Typical
- Supply Voltage Range = 2.7 to 3.6 V
- Adjacent Channel Power (ACPR) @ 1.25 MHz Offset
($P_{out} = 3.0$ dBm) = -58 dBc Typical

MRFIC1854A

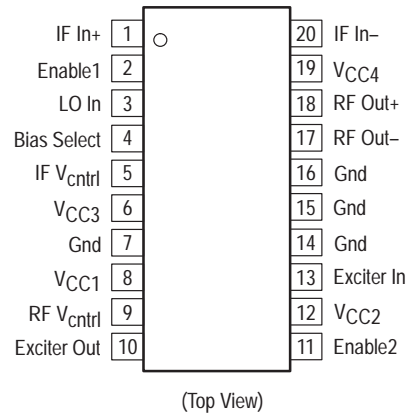
1.9 GHz CDMA UPMIXER/EXCITER

SEMICONDUCTOR TECHNICAL DATA

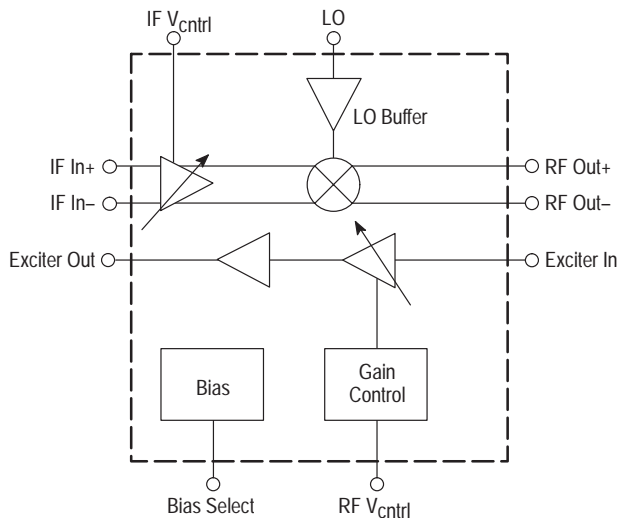


PLASTIC PACKAGE
CASE 948M
(TSSOP-20EP, Tape & Reel Only)

PIN CONNECTIONS



Simplified Block Diagram



This device contains 305 active transistors.

ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC1854AR2	T _A = -40 to 85°C	TSSOP-20EP

MRFIC1854A

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Supply Voltage	V_{CC}	5.0	V
IF Input	IF In+, IF In-	10	dBm
LO Input	LO	10	dBm
Operating Temperature	T_A	-40 to 85	°C
Storage Temperature	T_{stg}	-65 to 150	°C

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions and Electrical Characteristics tables or Pin Descriptions section.
 2. Meets Human Body Model (HBM) ≤ 50 V and Machine Model (MM) ≤ 40 V. This device is rated Moisture Sensitivity Level (MSL) 4. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Voltage	V_{CC}	2.7	-	3.6	V
RF Frequency Range	f_{RF}	1700	-	2000	MHz
IF Frequency Range	f_{IF}	70	-	250	MHz
LO Frequency Range	f_{LO}	1500	-	2100	MHz
Gain Control Voltage Range	IF V_{ctrl} , RF V_{ctrl}	0.1	-	1.7	V

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ V, $P_{LO} = -13$ dBm @ 2010 MHz, $P_{IF} = -27$ dBm (differential) @ 130 MHz, $V_{Enable1} = V_{Enable2} = 2.4$ V, $T_A = -40$ to 85°C , Test Circuit in Figure 1, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

CASCADE PERFORMANCE (Filter included between RF Out and Exciter input. Filter insertion loss is 4.0 dB)

Output Power $V_{ctrl} = 1.7$ V $V_{ctrl} = 1.3$ V	P_{out}	3.0 2.0	5.0 3.8	- -	dBm
Dynamic Range ($V_{ctrl} = 0.1$ to 1.7 V)	DR	50	65	-	dB
Adjacent Channel Power @ 1.25 MHz Offset High Current (Bias Select = 0.4 V, $P_{out} = 3.0$ dBm (set by V_{ctrl}))	ACPR	-52	-58	-	dBc
Supply Current High Current (Bias Select = 0.4 V) Low Current (Bias Select = 2.4 V)	I_{CC}	- -	55 35	80 50	mA

MIXER SECTION

Conversion Gain	G_C	-	16	-	dB
Noise Figure	NF	-	12	-	dB
Output Third Order Intercept Point	OIP3	-	6.0	-	dBm
IF AGC Dynamic Range	DR_{IF}	25	38	-	dB

EXCITER SECTION

Gain (No Attenuation)	G	-	24	-	dB
Noise Figure	NF	-	5.0	-	dB
Output Third Order Intercept Point	OIP3	-	22	-	dBm
RF AGC Dynamic Range	DR_{RF}	25	38	-	dB

MRFIC1854A

PIN FUNCTION DESCRIPTION

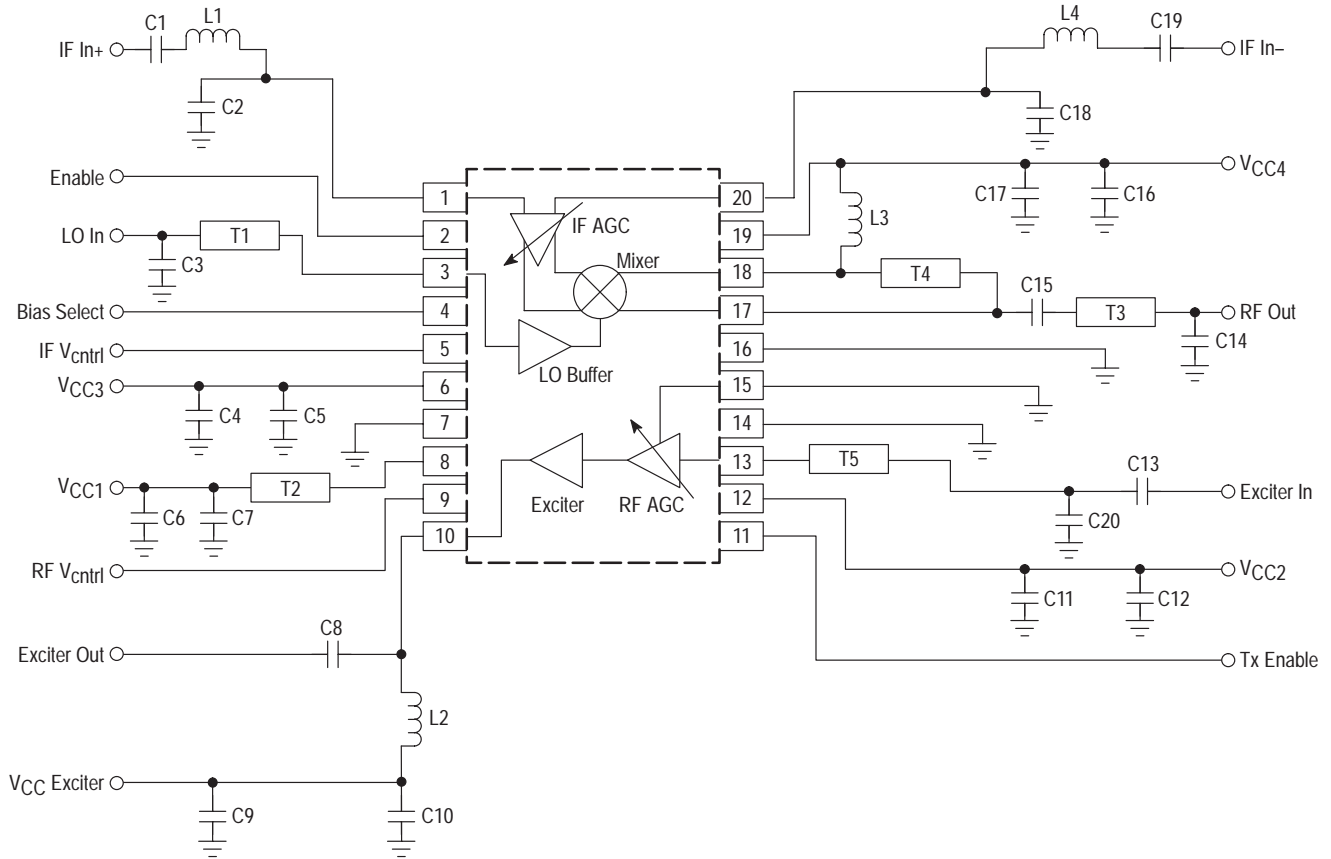
Pin	Function	Description	Voltage On (V)	Voltage Off (V)
1	IF In+	Mixer IF input pin. Input impedance is 500 Ω .	-33 dBm (Typ)	
2	Enable 1 (See Table 2)	Enable pin. A logic "High" (>2.4 V) enables entire chip and "Low" (<0.4 V) disables chip .	2.4 to 3.6	0 to 0.4
3	LO In	Mixer LO input pin.	-13 dBm (Typ)	
4	Bias Select	Bias select pin. Logic "Low" (<0.4 V) selects higher current bias for increased linearity and output power. "High" (>2.4 V) selects lower bias for reduced current consumption.		
5	IF AGC Control Voltage	IF AGC gain control pin. A 30 dB dynamic range can be achieved by adjusting voltage from 0.1 V (low gain) to 1.7 V (high gain).	0.1 to 1.7	
6	VCC3	Supply Voltage.	2.7 to 3.6	
7	Gnd	Ground connection.	-	
8	VCC1	Supply Voltage	2.7 to 3.6	
9	RF AGC Control Voltage	RF AGC control pin. A 30 dB dynamic range can be achieved by adjusting voltage from 0.1 V (low gain) to 1.7 V (high gain).	0.1 to 1.7	
10	Exciter Out	RF exciter amplifier output pin.	-	
11	Enable 2 (See Table 2)	Tx Enable pin. A logic "High" (>2.4 V) enables Tx path and "Low" (<0.4 V) disables Tx path except LO Buffer .	2.4 to 3.6	0 to 0.4
12	VCC2	Supply Voltage	2.7 to 3.6	
13	Exciter In	RF exciter amplifier input pin.	-	
14	Gnd	Ground connection.	-	
15	Gnd	Ground connection.	-	
16	Gnd	Ground connection.	-	
17	RF Out-	Mixer RF output pin.		
18	RF Out+	Mixer RF output pin.		
19	VCC4	Supply Voltage	2.7 to 3.6	
20	IF In-	Mixer IF input pin. Input impedance is 500 Ω .	-33 dBm (Typ)	

Table 1. Enable Truth Table

Enable 1	Enable 2	Mode
0	0	Disabled
0	1	Not Applicable
1	0	Standby Mode: Disables mixer/exciter, except LO buffer
1	1	Tx Enabled

MRFIC1854A

Figure 1. Application Circuit



C1, C19	1.0 nF	L1, L4	220 nH
C2, C18	4.7 pF	L2	10 nH
C3	1.7 pF	L3	18 nH
C4, C6, C9, C12, C16	10 nF	T1	50 Ω Microstrip, L = 670 mils
C5, C8, C10, C11, C13, C15, C17	30 pF	T2	50 Ω Microstrip, L = 150 mils
C7	47 pF	T3	50 Ω Microstrip, L = 400 mils
C14	3.6 pF	T4	50 Ω Stripline, L = $\lambda/2$ @ 1880 MHz
C20	1.0 pF	T5	50 Ω Microstrip, L = 350 mils

- NOTES:** 1. IF ports matched to 50 Ω for testing purposes.
 2. Microstrip line and C7 form part of RF AGC/Exciter interstage match.
 3. Er = 4.45 and board thickness = 18 mils.

Figure 2. Gain versus Frequency (Low Current Mode)

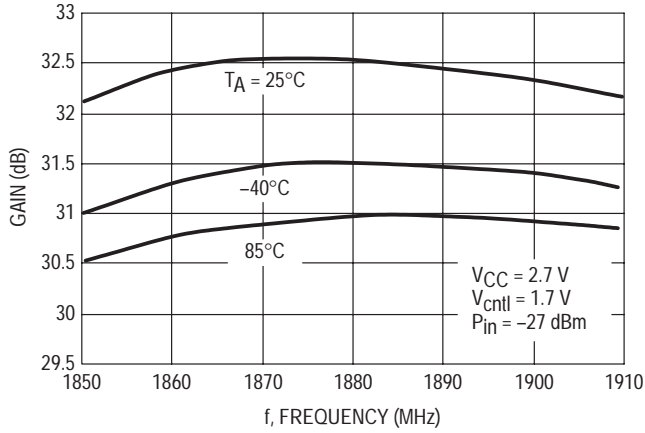


Figure 3. Gain versus Frequency (High Current Mode)

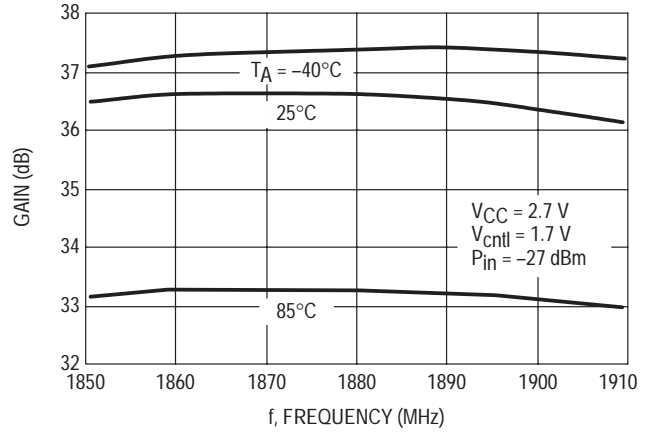


Figure 4. Gain versus LO Power (Low Current Mode)

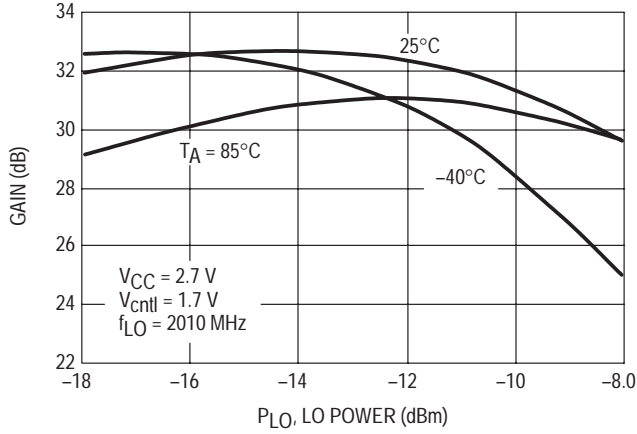


Figure 5. Gain versus LO Power (High Current Mode)

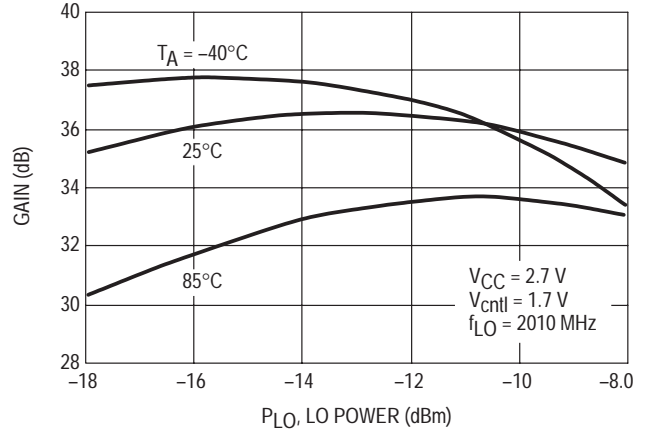


Figure 6. LO Feedthrough versus Control Voltage (Low Current Mode)

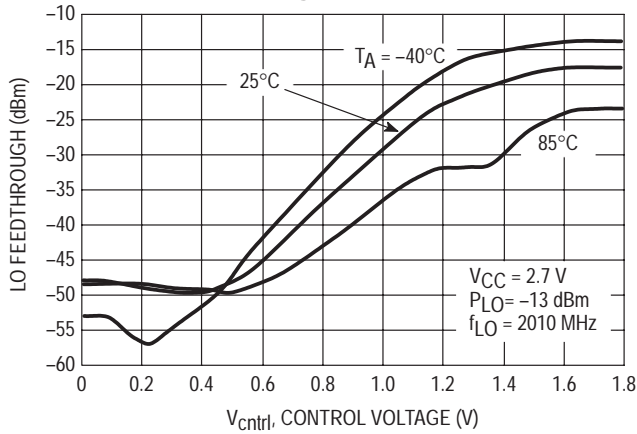
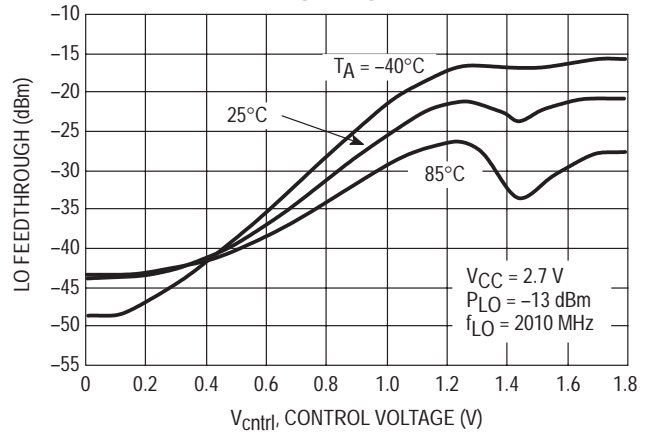


Figure 7. LO Feedthrough versus Control Voltage (High Current Mode)



MRFIC1854A

Figure 8. Output Power versus Control Voltage (Low Current Mode)

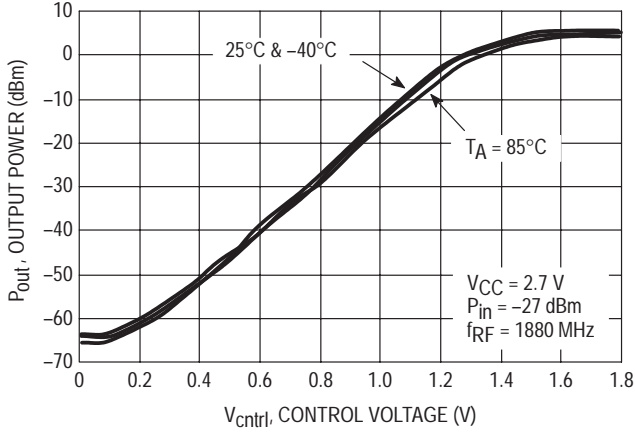


Figure 9. Output Power versus Control Voltage (High Current Mode)

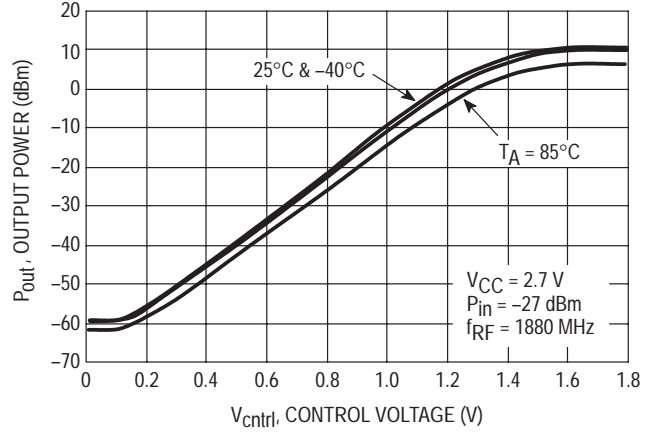
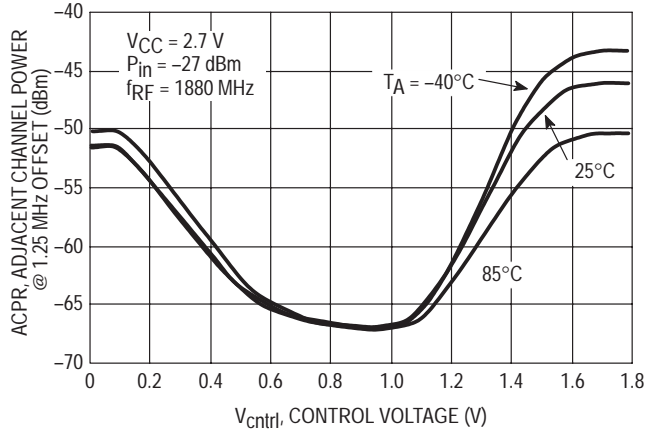


Figure 10. Adjacent Channel Power versus Control Voltage (High Current Mode)



MRFIC1854A

APPLICATION INFORMATION

Design Philosophy

The MRFIC1854A has three operating states, enable, standby, and disable. These states are controlled by the truth table shown in Table 2. The device is fully operational during the enable state and the bias level can be selected. A high bias current for maximum power CDMA or a lower bias current for CDMA at lower powers can be selected via the Bias Select pin. In the high current CDMA mode, the quiescent current is increased to maximize the linearity of the device. In the lower current bias state, the quiescent current is reduced to save current during lower power CDMA operation. The standby mode can be used to reduce current consumption during Voice Activity Factoring. In the standby mode, the LO buffer remains on to prevent VCO pulling and the bandgap reference bias circuit remains on to assure rapid device turn on. Current consumption in standby mode is 10 mA typical. The disable mode is used to turn the MRFIC1854A completely off. Leakage current in this mode is only a few microamps.

The mixer is a double-balanced "Gilbert-cell" design with a balanced LO buffer amplifier. The input and output of the mixer are differential. The IF AGC is a differential amplifier that uses the "current steering" method for gain control. The IF AGC/mixer combination has 16 dB of gain and typically draws 20 mA quiescent current in the CDMA mode. An external filter is required between the mixer and RF AGC amplifier to reduce RX band noise.

Figure 1 shows the applications circuit for the MRFIC1854A. In this circuit, the IF ports of the IF AGC have been matched to 50 Ω for testing purposes. In the actual application, the differential IF ports of the mixer would be impedance matched to an IF SAW filter. The differential impedance of the IF ports is 1600 ohms. The RF output of the mixer is configured as a differential output. A stripline balun is used to convert the RF output to single ended. DC current to the open collector output of the mixer is provided by inductor, L3 (18 nH) and transmission line, T4. Transmission lines T3 and T4, and capacitors C15 (30 pF) and C14 (3.6 pF) form the balun/output match for the mixer.

The RF AGC amplifier is a single-ended cascode design employing the standard "current steering" method of gain control. It's ground is brought out through pin number 15 so inductance can be added to degenerate the gain for a lower noise floor. The maximum gain is around 13 dB. It typically

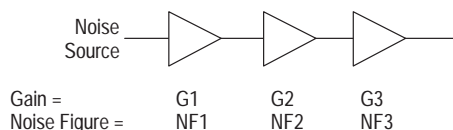
draws 9.0 mA quiescent current in CDMA mode. The RF V_{ctrl} signal is buffered with an on-chip OpAmp then preconditioned with temperature compensation and dB/V linearization before being applied to the RF AGC amplifier.

Transmission line T2 and capacitor C7 (47 pF) are for the interstage match between the RF AGC and the exciter amplifier.

The exciter amplifier is a simple common emitter design. It is grounded directly to the exposed pad which results in 12 dB of gain. It typically draws 24 mA bias current in CDMA. Inductor L2 (10 nH), capacitor C8 (30 pF), and C10 (30 pF) provide the output matching. L2 also provides a DC current path for the open collector output.

Noise Power Considerations

In CDMA systems, the handset is required to dynamically adjust its output power to specific levels. This requires a dynamic range of as much as 90 dB from the transmitter. Another key performance specification in CDMA systems is the output noise power, both in band and out of band. Noise power specifications has caused the noise figure of the transmitter to become an important system consideration. The cascaded noise figure of the transmitter can be analyzed with the same equation used in receiver analysis. The only difference is the noise source is from the transmitter (modulator) instead of the atmosphere.



$$NF_{\text{cascaded}} = NF_1 + \frac{NF_2 - 1}{G_1} + \frac{NF_3 - 1}{G_1 G_2}$$

This equation above shows that the cascaded noise figure is better if the gain is higher and the noise figure is lower for the stages close to the noise source. For this reason, it is advantageous to implement some of the gain control of a CDMA transmitter in the RF section. The MRFIC1854A integrates a RF AGC amplifier after the upmixer to improve the overall noise figure of the transmitter.

MRFIC1854A

Table 2. Scattering Parameters for Exciter Amplifier
($V_{DD} = 2.7$ V, $T_A = 25^\circ\text{C}$, RF $V_{ctrl} = 1.8$ V, $50\ \Omega$ System)

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	∠φ	S ₂₁	∠φ	S ₁₂	∠φ	S ₂₂	∠φ
1700	0.319	-121.64	15.566	84.09	0.00476	-139.21	0.219	-12.29
1725	0.315	-123.78	16.291	76.55	0.00415	-126.71	0.222	-24.12
1750	0.310	-126.93	16.975	68.23	0.00406	-143.61	0.223	-35.58
1775	0.309	-130.34	17.590	56.64	0.00336	-143.09	0.237	-51.49
1800	0.304	-132.64	17.834	47.84	0.00406	-144.41	0.248	-64.80
1825	0.294	-137.08	17.944	35.98	0.00268	-141.85	0.271	-82.53
1850	0.286	-139.92	17.871	26.91	0.00411	-127.38	0.278	-94.74
1875	0.274	-141.87	17.591	17.93	0.00286	-132.49	0.298	-104.71
1900	0.261	-143.08	17.141	9.25	0.00351	-136.62	0.308	-114.83
1925	0.249	-145.61	16.374	-1.69	0.00447	-139.69	0.324	-128.42
1950	0.242	-146.86	15.738	-9.57	0.00322	-153.09	0.335	-137.57
1975	0.233	-148.86	15.046	-17.01	0.00411	-139.41	0.346	-146.12
2000	0.225	-149.74	14.132	-26.57	0.00490	-139.12	0.350	-155.24

MRFIC1854A

Table 3. Scattering Parameters for Upmixer
($V_{DD} = 2.7\text{ V}$, $T_A = 25^\circ\text{C}$, IF $V_{\text{ctrl}} = 1.8\text{ V}$, $50\ \Omega$ System)

f (MHz)	IF In+		IF In-		f (MHz)	RF Out (Pin 17)	
	$ S_{11} $	$\angle\phi$	$ S_{11} $	$\angle\phi$		$ S_{11} $	$\angle\phi$
70	0.830	-2.07	0.832	-2.24	1700	0.815	-55.16
80	0.828	-2.73	0.830	-2.71	1725	0.814	-55.65
90	0.826	-3.01	0.828	-2.95	1750	0.814	-56.29
100	0.826	-3.21	0.827	-3.22	1775	0.817	-56.98
110	0.822	-3.57	0.825	-3.67	1800	0.820	-57.45
120	0.821	-3.74	0.823	-3.93	1825	0.823	-58.68
130	0.821	-3.93	0.823	-4.08	1850	0.825	-59.57
140	0.818	-4.25	0.820	-4.42	1875	0.826	-60.85
150	0.818	-4.54	0.821	-4.57	1900	0.825	-62.07
160	0.818	-4.61	0.820	-4.76	1925	0.815	-63.81
170	0.817	-4.85	0.819	-5.06	1950	0.807	-64.79
180	0.815	-5.12	0.819	-5.29	1975	0.794	-65.64
190	0.815	-5.26	0.819	-5.50	2000	0.782	-66.58
200	0.813	-5.45	0.816	-5.76			
210	0.815	-5.71	0.818	-6.15			
220	0.812	-5.82	0.816	-6.13			
230	0.811	-6.38	0.817	-6.54			
240	0.812	-6.54	0.814	-6.72			
250	0.810	-6.76	0.815	-6.98			

f (MHz)	LO In		f (MHz)	LO In		f (MHz)	LO In	
	$ S_{11} $	$\angle\phi$		$ S_{11} $	$\angle\phi$		$ S_{11} $	$\angle\phi$
1500	0.708	-47.83	1725	0.677	-54.36	1950	0.624	-58.20
1525	0.704	-48.38	1750	0.670	-55.34	1975	0.623	-59.40
1550	0.702	-49.02	1775	0.654	-56.33	2000	0.612	-60.59
1575	0.696	-49.55	1800	0.641	-56.34	2025	0.605	-61.04
1600	0.694	-50.11	1825	0.636	-56.65	2050	0.599	-61.70
1625	0.691	-50.83	1850	0.631	-56.59	2075	0.592	-62.19
1650	0.688	-51.47	1875	0.630	-57.04	2100	0.588	-62.99
1675	0.691	-52.18	1900	0.626	-57.38			
1700	0.681	-53.42	1925	0.622	-57.84			

Advance Information

Dual-Band/Dual-Mode pHEMT GaAs IPA

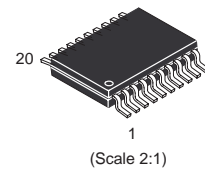
The MRFIC1856 is designed for dual-band subscriber equipment applications at 3.6 V in the cellular (800 MHz) and PCS (1900 MHz) bands. The device incorporates two pHEMT GaAs amplifier chains in one package, allowing the most flexibility and highest performance while reducing board space. Target applications include dual-band/dual-mode handsets for TDMA/AMPS and PCS TDMA cellular phones.

- Designed to Operate in Frequency Ranges of:
 - 824 to 849 MHz TDMA/AMPS
 - 1850 to 1910 MHz PCS TDMA
- 3.6 V Operation
- 30 dBm Output Power PCS TDMA
- 31 dBm Output Power TDMA Cellular
- 31 dBm Output Power AMPS

MRFIC1856

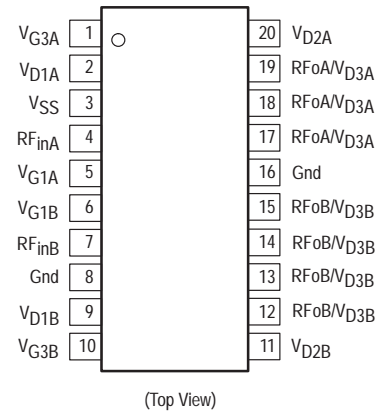
DUAL-BAND/DUAL-MODE GaAs INTEGRATED POWER AMPLIFIER

SEMICONDUCTOR TECHNICAL DATA

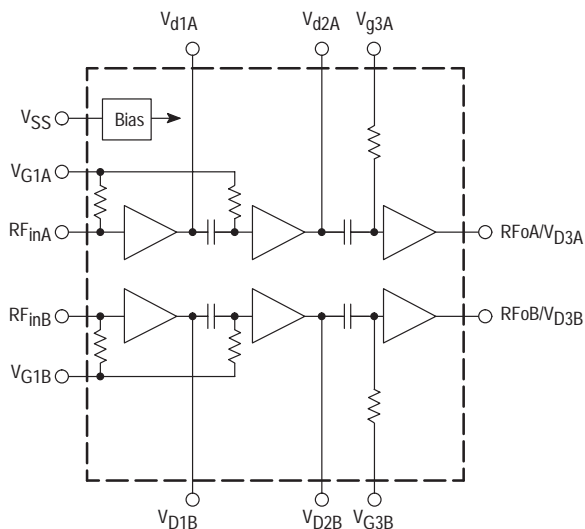


PLASTIC PACKAGE
CASE 948M
(TSSOP-20EP, Tape & Reel Only)

PIN CONNECTIONS



Simplified Block Diagram



This device contains 8 active transistors.

ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC1856R2	T _C = -35 to 85°C	TSSOP-20EP

MRFIC1856

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Supply Voltage	V_D	4.8	Vdc
RF Input Power	P_{in}	15	dBm
Gate Voltage	V_g	-6 to -0.3	Vdc
Storage Temperature Range	T_{stg}	-65 to 150	°C
Operating Case Temperature	T_C	-35 to 85	°C
Thermal Resistance, Junction to Case	$R_{\theta JC}$	15	°C/W

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables.
 2. ESD (electrostatic discharge) immunity meets Human Body Model (HBM) ≤ 100 V and Machine Model (MM) < 50 V. Additional ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristics	Symbol	Limit	Unit
Frequency Range – TDMA/AMPS	f_{RF}	824 to 849	MHz
Frequency Range – PCS TDMA	f_{RF}	1850 to 1910	MHz
Supply Voltage Range	$V_{D1,2,3A}, V_{D1,2,3B}$	3.0 to 4.8	Vdc
Negative Supply Voltage	V_G	-4.5 to -2.5	Vdc

ELECTRICAL CHARACTERISTICS ($V_{D1,2,3A} = 3.6$ V, $T_A = 25^\circ\text{C}$, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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TDMA CELLULAR PERFORMANCE ($P_{out} = 31$ dBm, $f = 840$ MHz)

Quiescent Supply Current	I_{DQ}	-	-	300	mA
Negative Supply Current	I_{SS}	-	-	3.0	mA
Efficiency	PAE	40	45	-	%
Gain	G_P	29	-	-	
Adj Channel Power (± 30 kHz)	ACP	-	-	-29	dBc
Alt Channel Power (± 60 kHz)	ALT	-	-	-48	dBc
Rx Band Noise (30 kHz BW)	-	-	-92	-	dBm
Harmonic Output Power	-	-	-	-	dBc
$2f_o$	-	-	-	-34	
$3f_o$	-	-	-	-40	
Spurious Output, 10:1 VSWR, all angles on output	-	-	-	-60	dBc

AMPS PERFORMANCE ($P_{out} = 31$ dBm, $f = 840$ MHz)

Quiescent Supply Current	I_{DQ}	-	-	300	mA
Negative Supply Current	I_{SS}	-	-	3.0	mA
Efficiency ($P_{out} = 31$ dBm)	PAE	-	48	-	%
Gain	G_P	30	-	-	
Harmonic Output Power	-	-	-	-	dBc
$2f_o$	-	-	-	-34	
$3f_o$	-	-	-	-40	
Rx Band Noise (30 kHz BW)	-	-	-92	-	dBm
Spurious Output, 10:1 VSWR, all angles on output	-	-	-	-60	dBc

PCS TDMA PERFORMANCE ($P_{out} = 30$ dBm, $f = 1.88$ GHz)

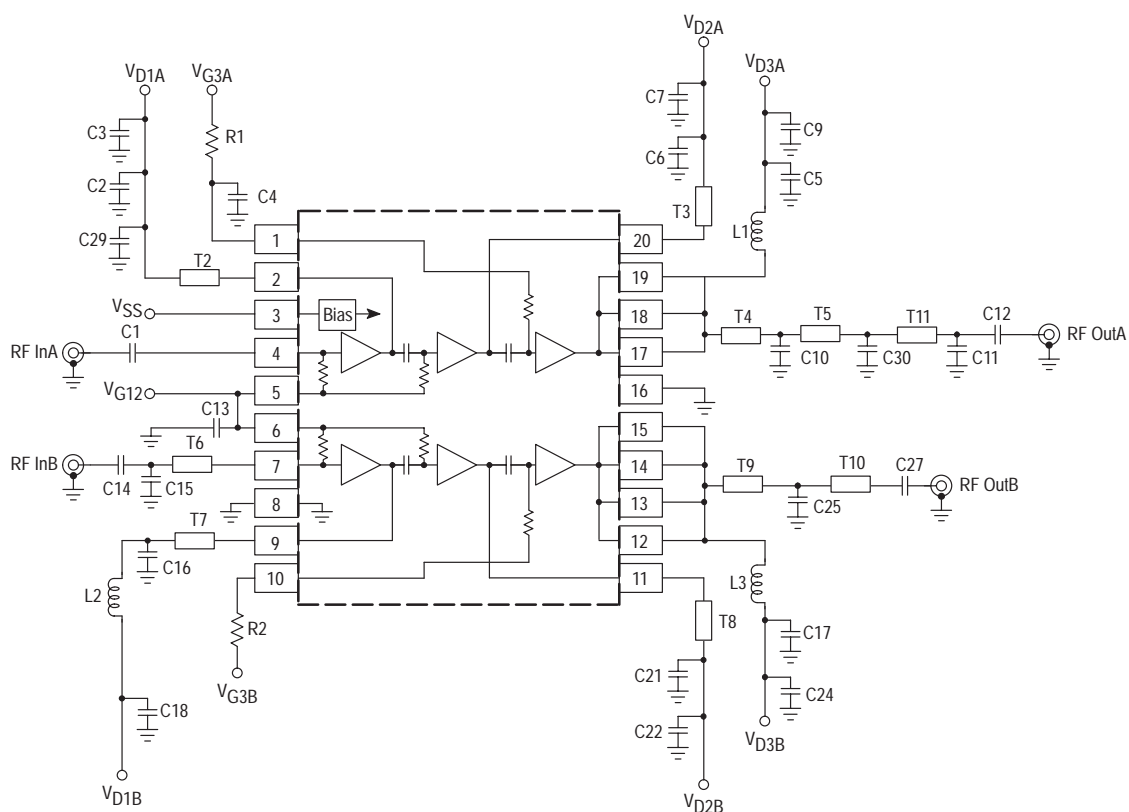
Quiescent Supply Current	-	-	-	300	mA
Negative Supply Current	-	-	-	3.0	mA
Efficiency	-	30	35	-	%
Gain	-	28	-	-	

MRFIC1856

ELECTRICAL CHARACTERISTICS (continued) ($V_{D1,2,3A} = 3.6\text{ V}$, $T_A = 25^\circ\text{C}$, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
PCS TDMA PERFORMANCE (continued) ($P_{\text{Out}} = 30\text{ dBm}$, $f = 1.88\text{ GHz}$)					
Adj Channel Power ($\pm 30\text{ kHz}$)	–	–	–	–29	dBc
Alt Channel Power ($\pm 60\text{ kHz}$)	–	–	–	–48	dBc
Rx Band Noise (30 kHz BW)	–	–	–94	–	dBm
Harmonic Output Power	–	–	–	–	dBc
$2f_o$	–	–	–	–40	
$3f_o$	–	–	–	–40	
Spurious Output, 10:1 VSWR, all angles on output	–	–	–	–60	dBc

Figure 1. 3.6 V Applications Circuit

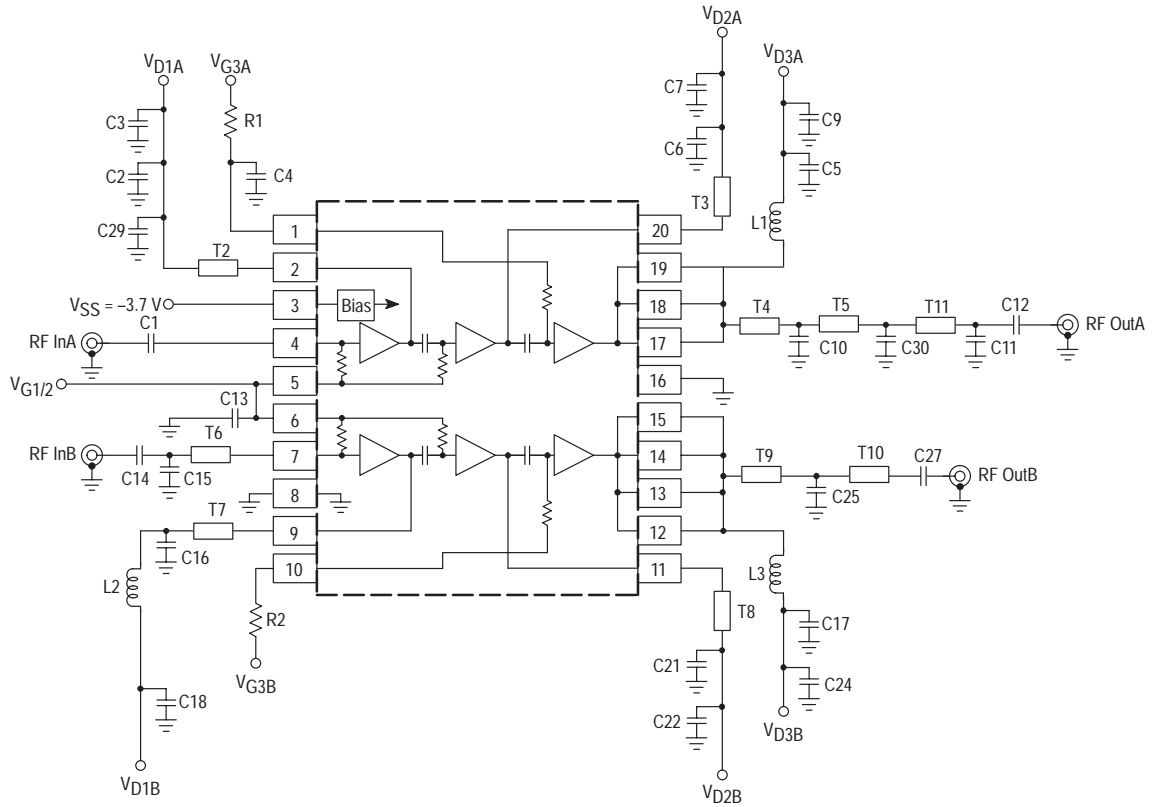


C1,C2,C5,C12,C17, 100 pF	C16	6.2 pF	T2	50 Ω , Microstrip, L = 128 mils
C28 3.9 nF	C25	4.7 pF	T3	50 Ω , Microstrip, L = 50 mils
C3,C4,C6,C13,C21 1000 pF	C27	10 pF	T4	50 Ω , Microstrip, L = 60 mils
C7,C18 10 μF	C29	3.9 pF	T5	90 Ω , Microstrip, L = 88 mils
C9,C22,C24 20 μF	L1,L2,L3	15 nH	T6	90 Ω , Microstrip, L = 600 mils
C10 12 pF	R1	50 Ω	T7	63 Ω , Microstrip, L = 133 mils
C11 5.1 pF	R2	100 Ω	T8	50 Ω , Microstrip, L = 133 mils
C14 22 pF			T9	50 Ω , Microstrip, L = 10 mils
C15,C30 1.3 pF			T10	50 Ω , Microstrip, L = 330 mils
			T11	50 Ω , Microstrip, L = 145 mils

NOTE: C29 added for 2nd harm trap.

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Figure 2. 4.8 V Applications Circuit



C1,C2,C5,C12,C17, 100 pF	C16	6.8 pF	T2	50 Ω, Microstrip, L = 128 mils
C28 3.9 nF	C25	4.3 pF	T3	50 Ω, Microstrip, L = 50 mils
C3,C4,C6,C13,C21 1000 pF	C27	10 pF	T4	50 Ω, Microstrip, L = 60 mils
C7,C18 10 μF	C29	3.9 pF	T5	90 Ω, Microstrip, L = 88 mils
C9,C22,C24 20 μF	L1,L2,L3	15 nH	T6	90 Ω, Microstrip, L = 600 mils
C10 12 pF	R1	50 Ω	T7	63 Ω, Microstrip, L = 133 mils
C11 5.1 pF	R2	100 Ω	T8	50 Ω, Microstrip, L = 133 mils
C14 22 pF			T9	50 Ω, Microstrip, L = 10 mils
C15,C30 1.3 pF			T10	50 Ω, Microstrip, L = 330 mils
			T11	50 Ω, Microstrip, L = 145 mils

TDMA PERFORMANCE

Figure 3. Gain versus Frequency

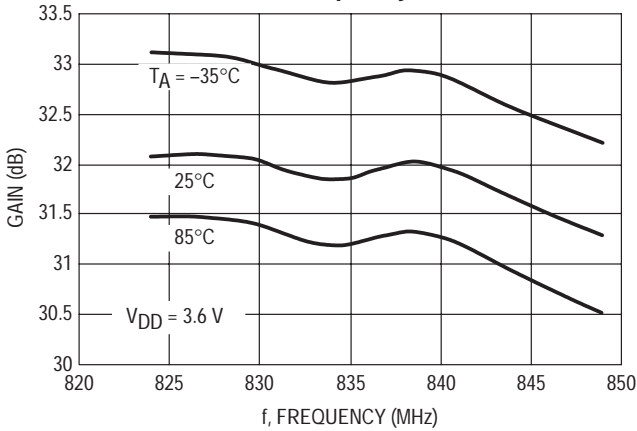


Figure 4. Gain versus Frequency

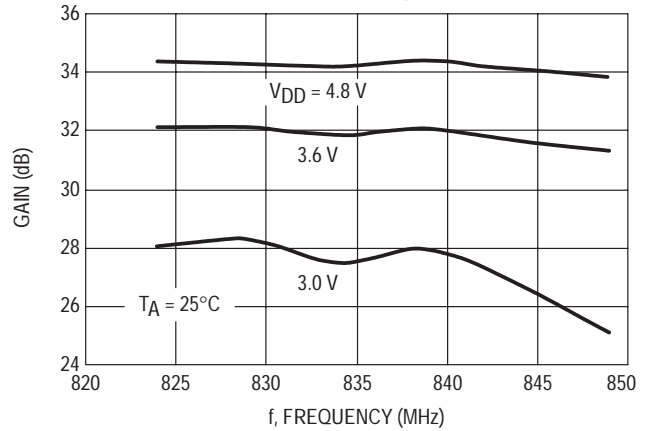


Figure 5. Output Power versus Input Power

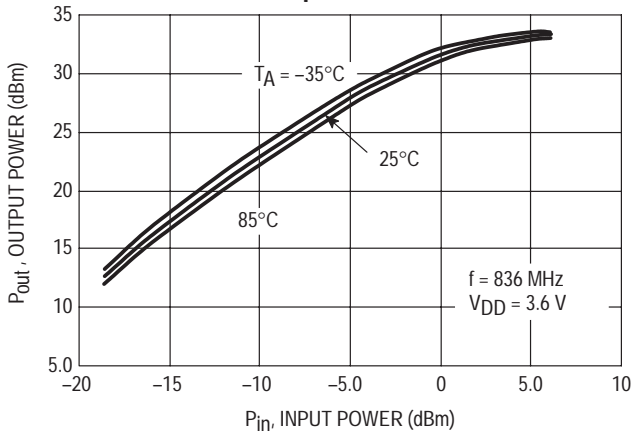


Figure 6. Output Power versus Input Power

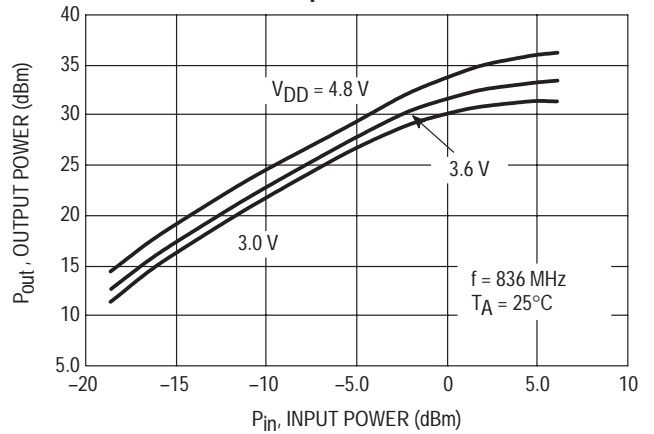


Figure 7. Adjacent Channel Power versus Output Power

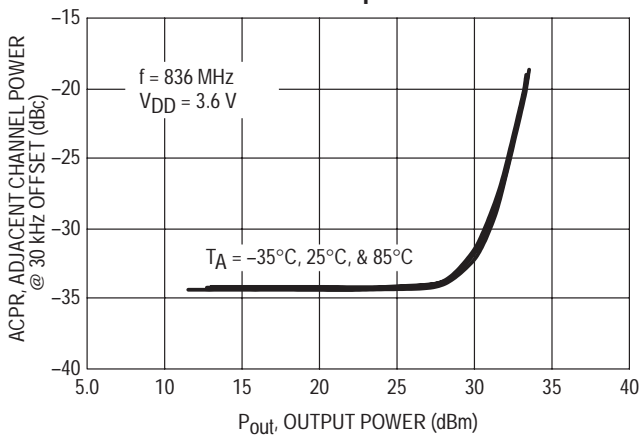
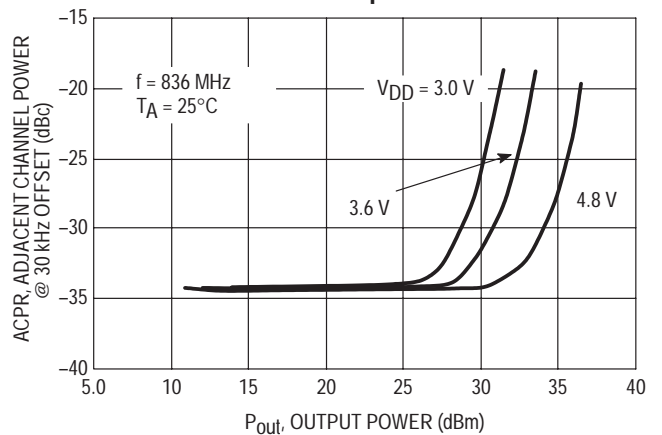


Figure 8. Adjacent Channel Power versus Output Power



TDMA PERFORMANCE

Figure 9. Alternate Channel Power versus Output Power

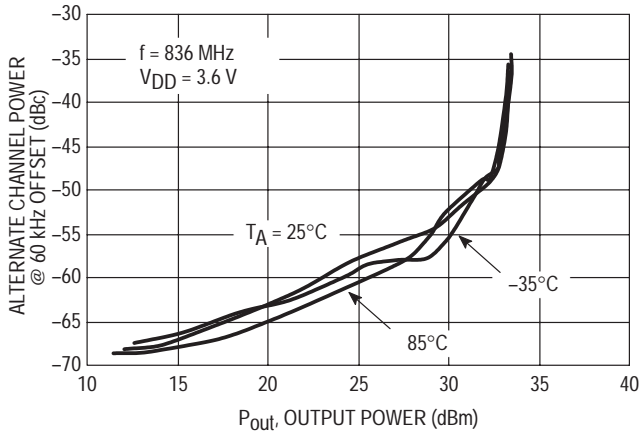


Figure 10. Alternate Channel Power versus Output Power

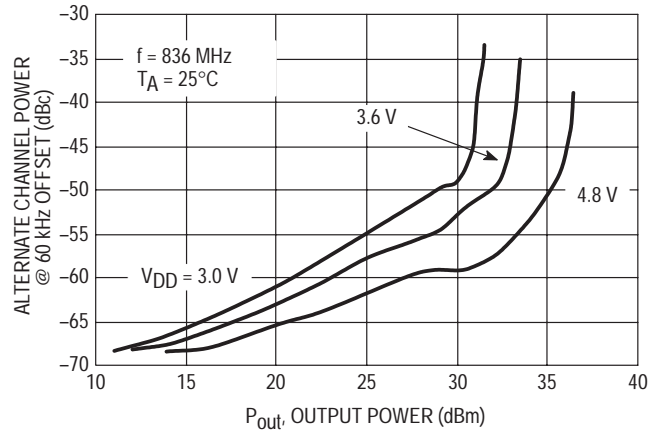


Figure 11. Gain versus Frequency

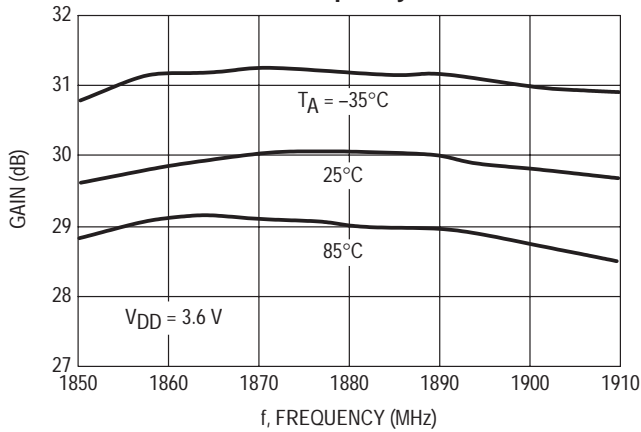


Figure 12. Gain versus Frequency

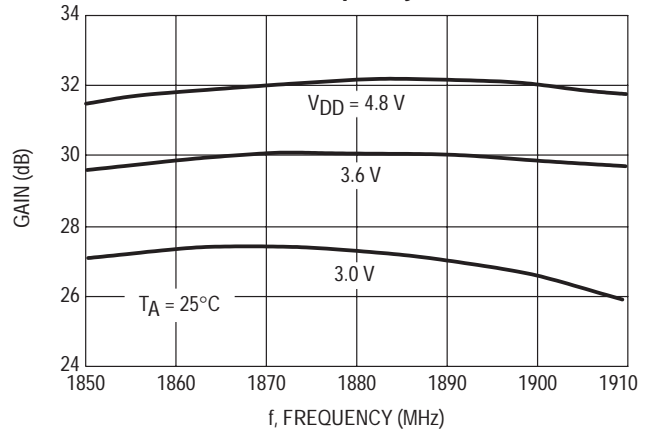


Figure 13. Output Power versus Input Power

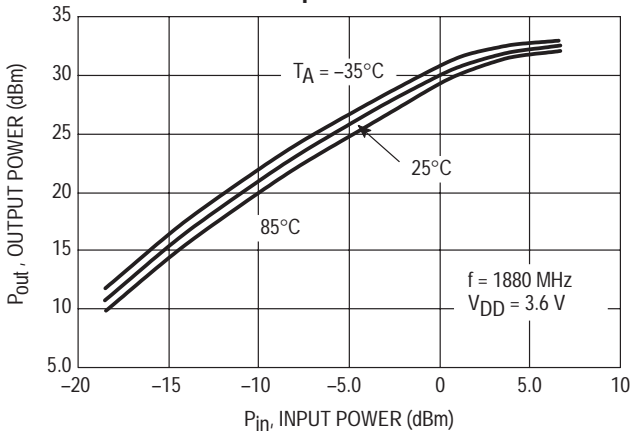
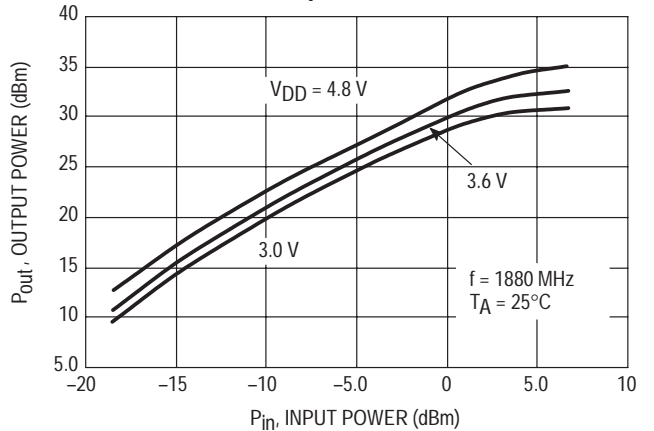


Figure 14. Output Power versus Input Power



TDMA PERFORMANCE

Figure 15. Adjacent Channel Power versus Output Power

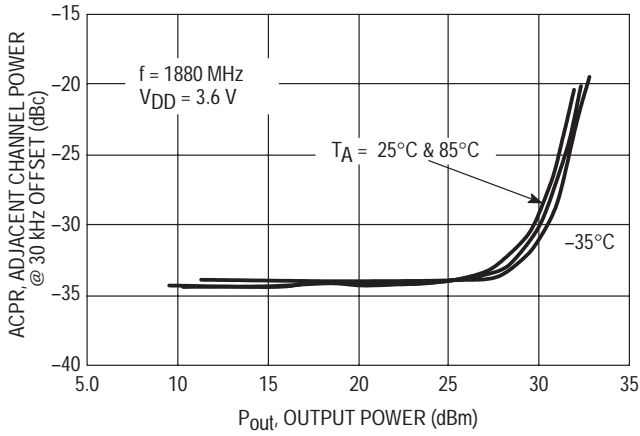


Figure 16. Adjacent Channel Power versus Output Power

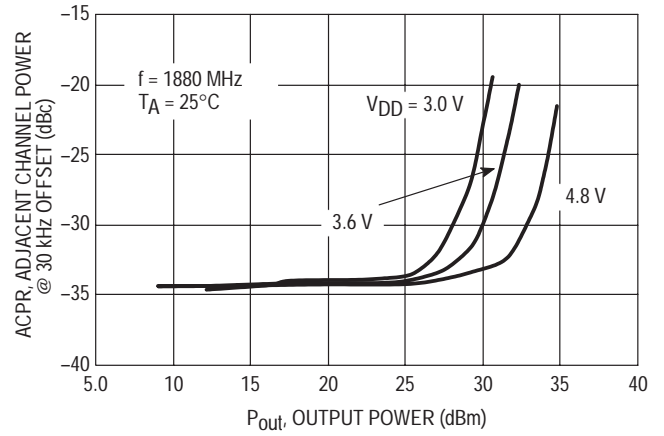


Figure 17. Alternate Channel Power versus Output Power

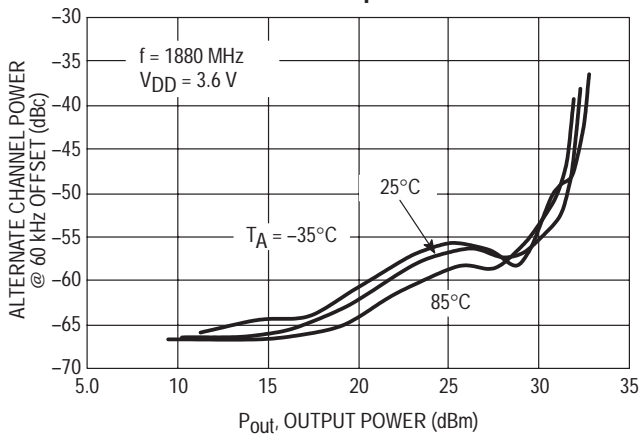
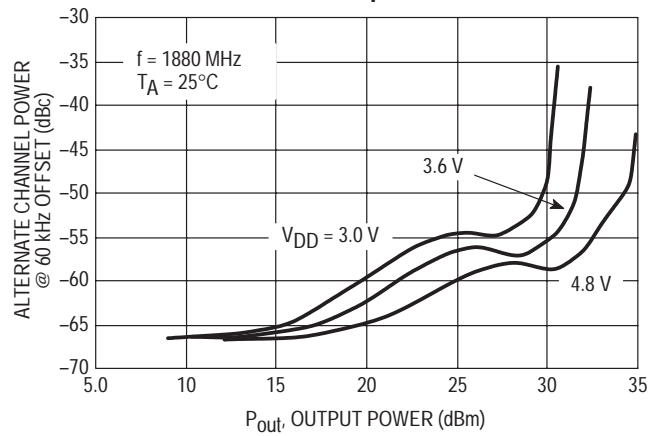


Figure 18. Alternate Channel Power versus Output Power





MOTOROLA

Dual-Band/GSM 3.6 V Integrated Power Amplifier

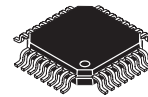
The MRFIC1859 is a dual-band, single supply RF Power Amplifier for GSM900/DCS1800 hand held radios. The on-chip spur free voltage generator reduces the number of external components by eliminating the need for a negative voltage supply. The device output power can be controlled open loop without the use of directional coupler and detection diode. The MRFIC1859 is General Packet Radio Service (GPRS) compatible. The device is packaged in a TQFP-32EP with exposed backside pad allowing excellent electrical and thermal performance through a solderable contact.

- Single Positive Supply Solution
- Input/Output External Matching
- High Power and Efficiency
- Typical 3.6 V Characteristics:
 - $P_{out} = 36.2 \text{ dBm}$, PAE = 53% for GSM
 - $P_{out} = 34 \text{ dBm}$, PAE = 43% for DCS
- Crosstalk Harmonic Leakage of -27 dBm Typical (GSM)

MRFIC1859

DUAL-BAND GSM 3.6 V IPA

SEMICONDUCTOR TECHNICAL DATA



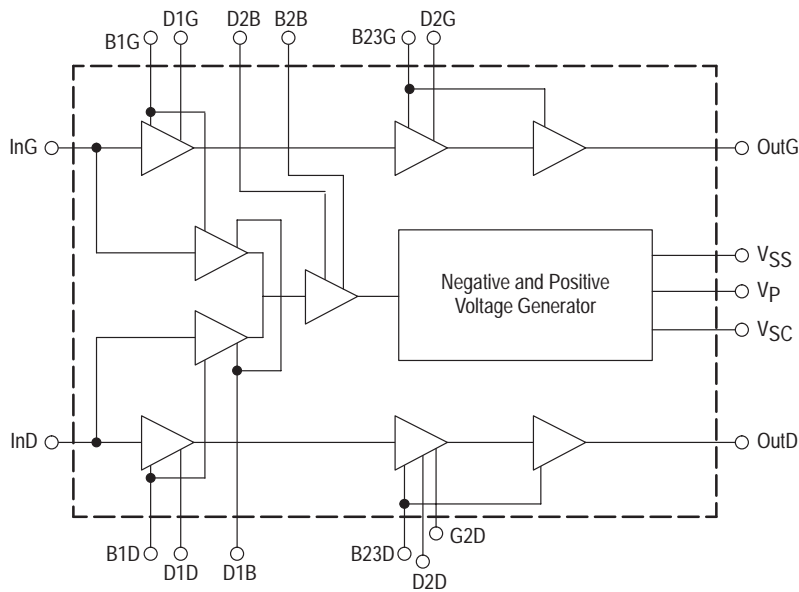
32 1
(Scale 2:1)

PLASTIC PACKAGE
CASE 873E
(TQFP-32EP)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MRFIC1859R2	$T_C = -35 \text{ to } 100^\circ\text{C}$	TQFP-32EP

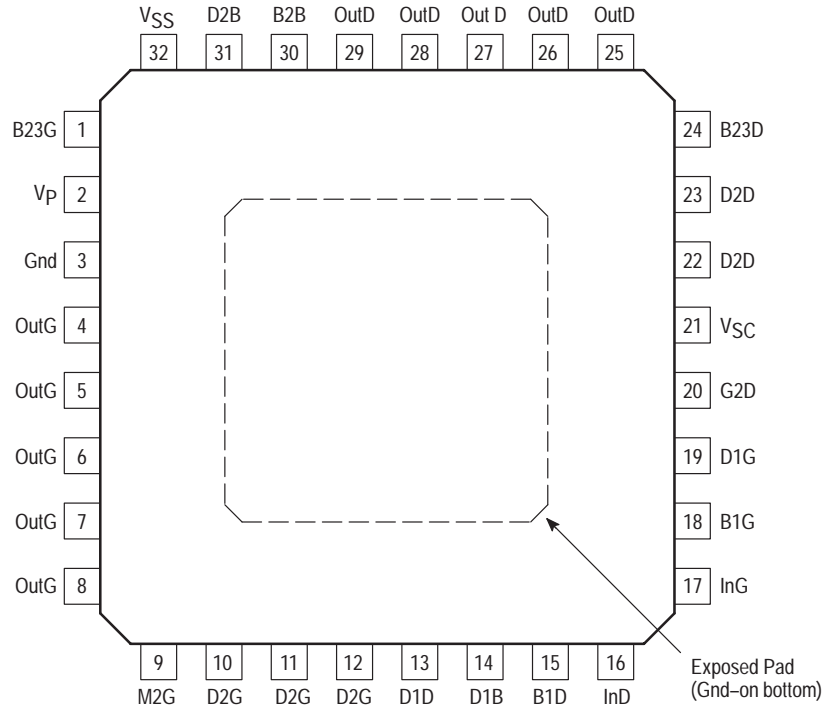
Simplified Block Diagram



This device contains 21 active transistors.

MRFIC1859

PIN CONNECTIONS



MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Supply Voltage	$V_{D1B,D2B}$ $V_{D1G,D2G,D3G,D1D,D2D,D3D}$	6.0	V
RF Input Power	InG, InD	12	dBm
RF Output Power			dBm
GSM Section	OutG	38	
DCS Section	OutD	36	
Operating Case Temperature Range	T_C	-35 to 100	°C
Storage Temperature Range	T_{stg}	-55 to 150	°C
Thermal Resistance, Junction to Case	$R_{\theta JC}$	15	°C/W

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions or Electrical Characteristics tables.
2. Meets Human Body Model (HBM) ≤ 100 V and Machine Model (MM) ≤ 60 V. Additional ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Supply	$V_{D1B,D2B}$ $V_{D1G,D2G,D3G,D1D,D2D,D3D}$	2.8	–	5.5	V
Input Power GSM	InG	3.0	–	10	dBm
Input Power DCS	InD	5.0	–	12	dBm

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ELECTRICAL CHARACTERISTICS ($V_{D1B}, D2B = 3.6$ V, $V_{D1G}, D2G, D3G = 3.6$ V or $V_{D1D}, D2D, D3D = 3.6$ V, Peak measurement at 12.5% duty cycle, 4.6 ms period, $T_A = 25^\circ\text{C}$, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
GSM SECTION ($P_{in} = 3.0$ dBm)					
Frequency Range	BW	880	–	915	MHz
Output Power	P_{out}	35	36.2	–	dBm
Power Added Efficiency	PAE	45	53	–	%
Output Power @ Low Voltage ($V_{D1G}, D2G, D3G = 3.0$ V)	P_{out}	33.5	34.7	–	dBm
Harmonic Output					dBc
$2f_o$		–	–35	–30	
$\geq 3f_o$		–	–60	–45	
Second Harmonic Leakage at DCS Output (Crosstalk isolation)		–	–25	–20	dBm
Input Return Loss	$ S_{11} $	–	12	–	dB
Output Power Isolation with Buffer On ($P_{in} = 3.0$ dBm, $V_{D1B}, D2B = 3.6$ V, $V_{D1G}, D2G, D3G = 0$ V)	P_{on}	–	–8.0	–3.0	dBm
Output Power Isolation ($P_{in} = 3.0$ dBm, $V_{D1B}, D2B = 0$ V, $V_{D1G}, D2G, D3G = 0$ V)	P_{off}	–	–42	–	dBm
Noise Power in Rx Band 925 to 960 MHz (100 kHz measurement bandwidth)	NP				dBm
925 to 935 MHz			–90	–67	
935 to 960 MHz			–90	–79	
Negative Voltage ($P_{in} = 2.0$ dBm, $V_{D1B}, D2B = 3.0$ V)	V_{SS}	–	–	–4.85	V
Negative Voltage Settling time ($P_{in} = 3.0$ dBm, $V_{D1B}, D2B$ stepped from 0 to 3.0 V)	T_S	–	0.7	2.0	μs
Stability–Spurious Output ($P_{out} = 5.0$ to 35 dBm, Load VSWR = 6:1 all Phase Angle, Source VSWR = 3:1, at any phase angle Adjust $V_{D1G}, D2G, D3G$ for specified power)	P_{spur}	–	–	–60	dBc
Load Mismatch Stress ($P_{out} = 5.0$ to 35 dBm, Load VSWR = 10:1 all phase angles, 5 seconds, Adjust $V_{D1G}, D2G, D3G$ for specified power)		No Degradation in Output Power Before and After Test			
Positive Voltage ($P_{in} = 3.0$ dBm, $V_{D1B} = V_{D2B} = 3.0$ V)	V_P	6	10	–	V
DCS SECTION ($P_{in} = 5.0$ dBm)					
Frequency Range	BW	1710	–	1785	MHz
Output Power	P_{out}	33	34	–	dBm
Power Added Efficiency	PAE	35	43	–	%
Output Power @ Low Voltage ($V_{D1D}, D2D, D3D = 3.0$ V)	P_{out}	31.5	32.4	–	dBm
Harmonic Output					dBc
$2f_o$		–	–40	–35	
$\geq 3f_o$		–	–35	–30	
Input Return Loss	$ S_{11} $	–	12	–	dB
Output Power Isolation with Buffer On ($P_{in} = 5.0$ dBm, $V_{D1B}, D2B = 3.6$ V, $V_{D1D}, D2D, D3D = 0$ V)	P_{on}	–	–8.0	–2.0	dBm
Output Power Isolation ($P_{in} = 5.0$ dBm, $V_{D1B}, D2B = 0$ V, $V_{D1D}, D2D, D3D = 0$ V)	P_{off}	–	–36	–	dBm
Noise Power in Rx Band 1805 to 1880 MHz (100 kHz measurement bandwidth)	NP	–	–85	–71	dBm
Negative Voltage ($P_{in} = 5.0$ dBm, $V_{D1B}, D2B = 3.0$ V)	V_{SS}	–	–	–4.85	V
Negative Voltage Settling time ($P_{in} = 5.0$ dBm, $V_{D1B}, D2B$ stepped from 0 to 3.0 V)	T_S	–	0.7	2.0	μs
Stability–Spurious Output ($P_{out} = 3.0$ to 33 dBm, Load VSWR = 6:1 all Phase Angle, Source VSWR = 3:1, at any phase angle Adjust $V_{D1D}, D2D, D3D$ for specified power)	P_{spur}	–	–	–60	dBc

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ELECTRICAL CHARACTERISTICS (continued) ($V_{D1B}, D2B = 3.6\text{ V}$, $V_{D1G}, D2G, D3G = 3.6\text{ V}$ or $V_{D1D}, D2D, D3D = 3.6\text{ V}$, Peak measurement at 12.5% duty cycle, 4.6 ms period, $T_A = 25^\circ\text{C}$, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
DCS SECTION (continued) ($P_{in} = 5.0\text{ dBm}$)					
Load Mismatch Stress ($P_{out} = 3.0$ to 33 dBm , Load VSWR = 10:1 all phase angles, 5 seconds, Adjust $V_{D1D}, D2D, D3D$ for specified power)		No Degradation in Output Power Before and After Test			
Positive Voltage ($P_{in} = 5.0\text{ dBm}$, $V_{D1B} = V_{D2B} = 3.0\text{ V}$)	Vp	6	10	–	V

PIN FUNCTION DESCRIPTION

Pin No.	Symbol	I/O	Description	Functionality
1	B23G	I	GSM Bias for 2nd and 3rd stage	Bias pin of GSM second and third stages. Biasing circuit is made of an internal resistor connected to RF transistor gate, and in series with a current source, connected to V_{SS} (Pin 32). An external resistor allows to tune biasing point for best gain (Class AB). To switch off GSM line-up, setting this pin (and Pin 18) to high impedance, which will apply V_{SS} (-5.0 V) to the gates, i.e., a voltage two times lower than FET threshold voltage.
2	Vp	O	Positive voltage	A buffer amplifier is designed to produce the required negative voltage, based on RF signal amplification and rectification. Also a positive voltage is generated in the same way, with rectification and a voltage doubler. This voltage supplies an op amp in order to drive a NMOS as drain switch. Refer to application schematic, with MC33170 and MTSF3N02 (products of On Semiconductor).
3	Gnd		Ground	
4,5,6,7,8	OutG	O	GSM output	RF output and power supply for output GSM stage. Supply voltage is provided through those five pins. An external matching network is required to provide optimum load impedance.
9		N.C.		
10,11,12	D2G	I	GSM 2nd stage drain	Power supply for GSM second stage, and inter-stage matching. Wire bonds and pins form the required inductor for optimum inter-matching tuning. Make note that decoupling capacitor on those pins needs to be placed as close as possible to the pins. Refer to application schematic for component value.
13	D1D	I	DCS 1st stage drain	Power supply for DCS first stage, and inter-staging matching. This pin associated with a printed line ($80\ \Omega$) forms the required inductor for a proper match.
14	D1B	I	Buffer 1st stage drain	Power supply for buffer amplifier first stage, and inter-staging matching. This pin, associated with a printed line ($80\ \Omega$) forms the required inductor for a proper match.
15	B1D	I	DCS 1st stage Bias	Same function as Pin 18 for DCS amplifier.
16	InD	I	DCS RF Input	RF input for DCS amplifier. A series inductor or line and a parallel inductor are required for a proper matching to $50\ \Omega$ and maximum gain. See application circuit.
17	InG	I	GSM RF Input	RF input for GSM amplifier. An inductor and a capacitor are required for a proper matching to $50\ \Omega$ and maximum gain. See application circuit.
18	B1G	I	GSM 1st stage Bias	Bias pin of GSM first stage and associated buffer stage. Biasing circuit is made of an internal resistor connected to RF transistor gate, and in series with a current source, connected to V_{SS} (Pin 32). An external resistor allows to tune biasing point for best gain (Class AB). See comments on Pin 1.
19	D1G	I	GSM 1st stage drain	Power supply for GSM first stage, and inter-stage matching. This pin, associated with a printed line ($80\ \Omega$) form the required inductor for a proper match.
20	G2D	I	DCS 2nd stage gate	Access to DCS 2nd stage gate. A shunt capacitor connected to this pin contributes to the inter-stage matching between 1st and 2nd DCS stages.
21	VSC	O	Check for Negative voltage	An opened drain transistor connected to this pin, with V_{SS} as gate voltage, gives a checking signal for negative voltage generation. Used in application circuit to forbid on state to the NMOS Drain switch when V_{SS} is not working. Prevents IC degradation when bias is not present. This pin is not used with MC33170 which has its own protection circuit.

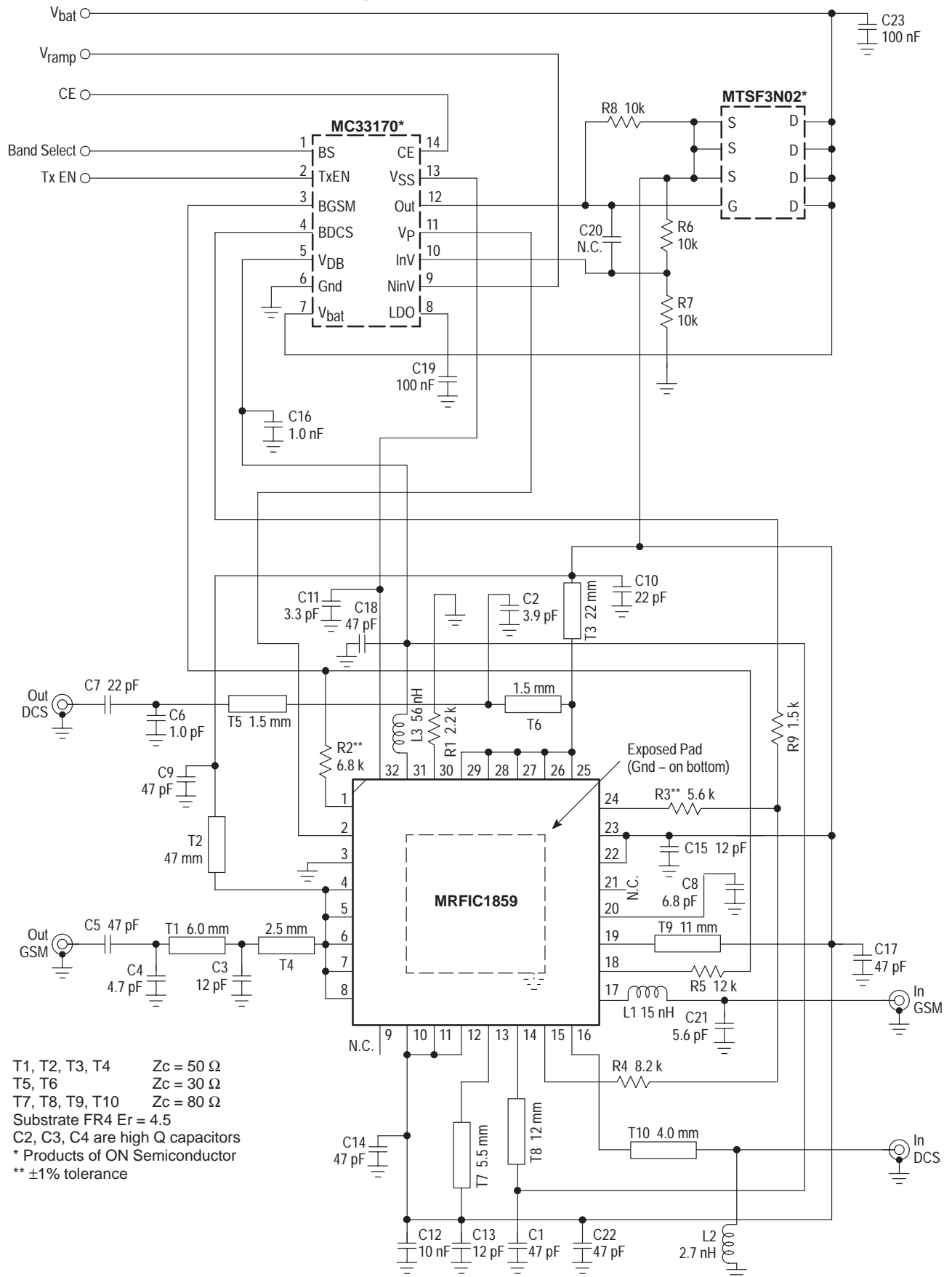
MRFIC1859

PIN FUNCTION DESCRIPTION (continued)

Pin No.	Symbol	I/O	Description	Functionality
22,23	D2D	I	DCS 2nd stage drain	Power supply for DCS driver stage, and inter-staging matching. These pins form the required inductor for a proper match.
24	B23D	I	DCS Bias for 2nd and 3rd stage	Same as Pin 1 for DCS amplifier.
25,26,27, 28,29	OutD	O	DCS RF Output	RF output and power supply for output DCS stage. Supply voltage is provided through those five pins. An external matching network is required to provide optimum load impedance.
30	B2B	I	Buffer 2nd state Bias	Like Pins 1, 15, and 18, this is a bias pin. Pin 30 is used to bias 2nd stage of buffer amplifier.
31	D2B	I	Buffer 2nd stage Drain	Drain supply and matching of buffer amplifier to maximize V_{SS} and V_p voltages.
32	V_{SS}	O	Negative Voltage	A buffer amplifier is designed to produce the required negative voltage, based on RF signal amplification with a two stages wide band amplifier and rectification of the resulting signal. An external zener diode is used to regulate this voltage and provide to the gates a stabilized biasing voltage. V_{SS} is also used to switch off the unused amplifier. Refer to Bias Pins 1, 18 and 15, 24.
Exposed Pad	Gnd	I	Main Gnd	The bottom pad of the TQFP-32EP package is used for electrical/RF grounding and thermal dissipation. The PCB pattern where it fits has to be tailored for good ground and thermal continuity (with many ground via holes).

MRFIC1859

Figure 1. Application Schematic



MRFIC1859

GSM TYPICAL CHARACTERISTICS

Figure 2. Output Power versus Frequency

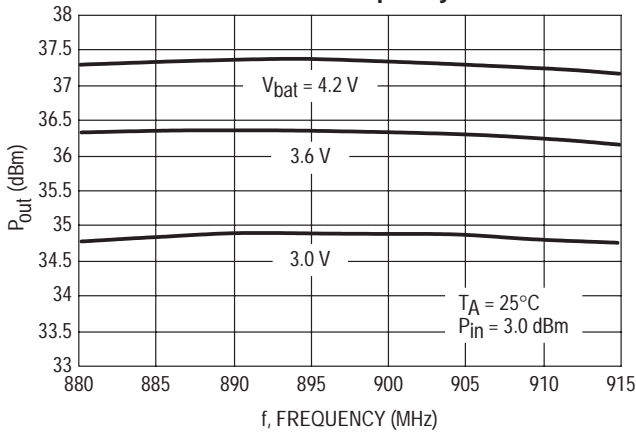


Figure 3. Power Added Efficiency versus Frequency

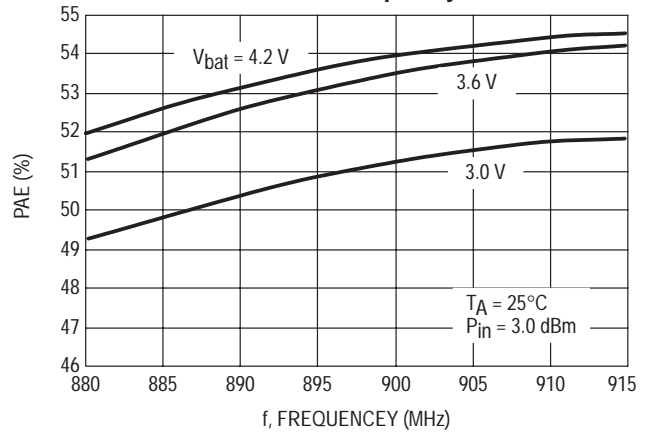


Figure 4. Output Power versus Frequency

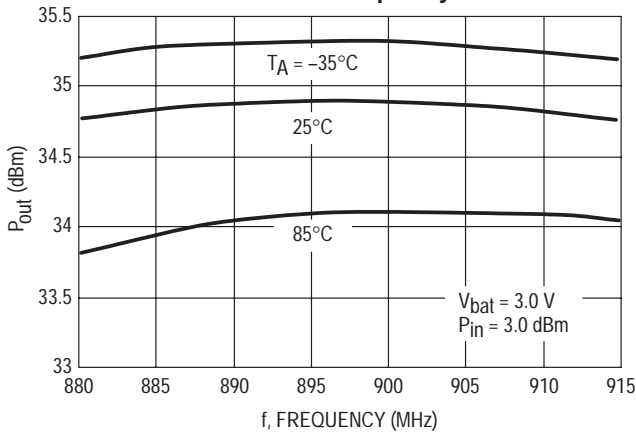


Figure 5. Output Power versus Frequency

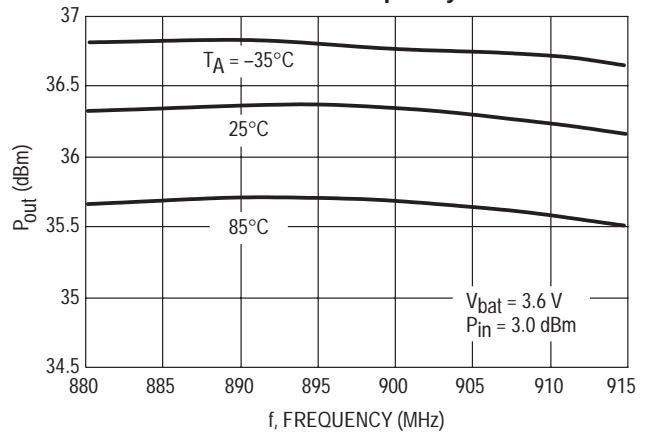


Figure 6. Output Power versus Frequency

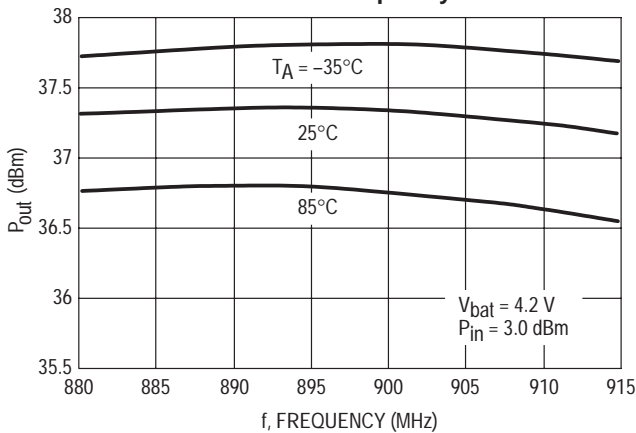
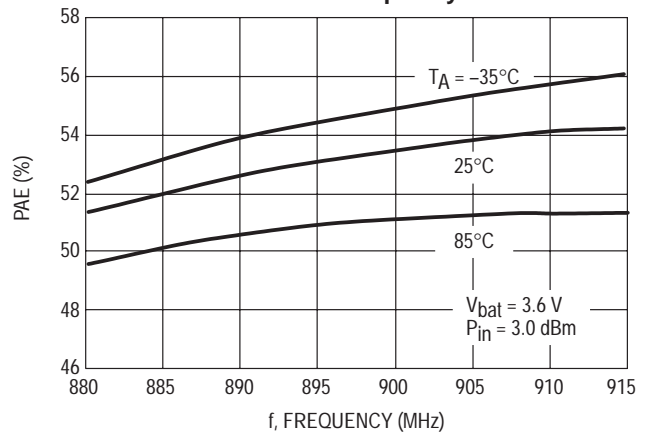


Figure 7. Power Added Efficiency versus Frequency



MRFIC1859

GSM TYPICAL CHARACTERISTICS

Figure 8. Second Harmonics versus Frequency

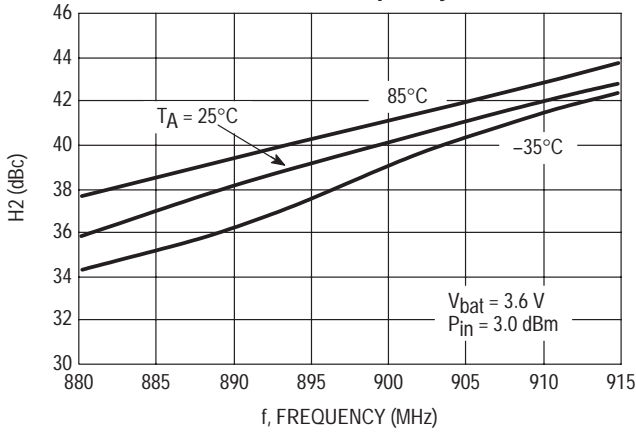


Figure 9. Third Harmonics versus Frequency

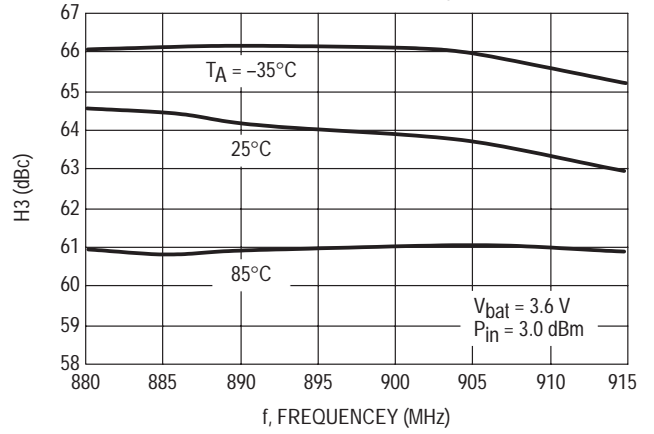


Figure 10. Positive Voltage Generator Output versus Frequency

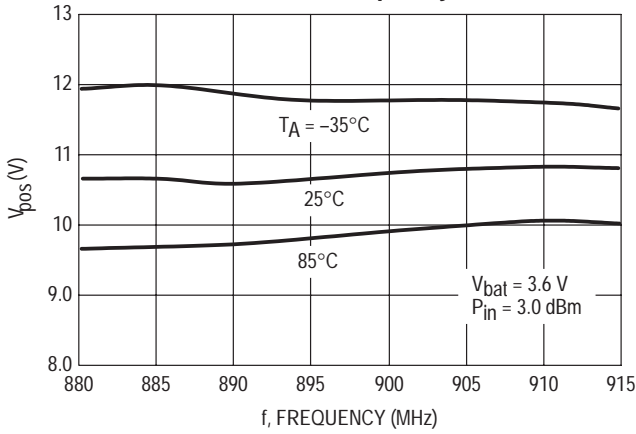


Figure 11. Crosstalk versus Frequency

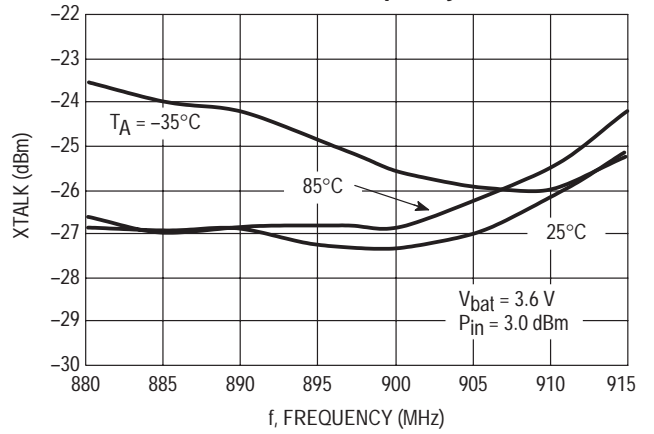


Figure 12. Output Power versus Vramp

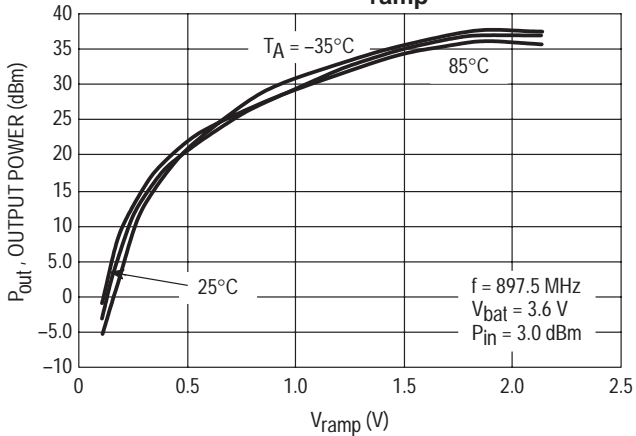
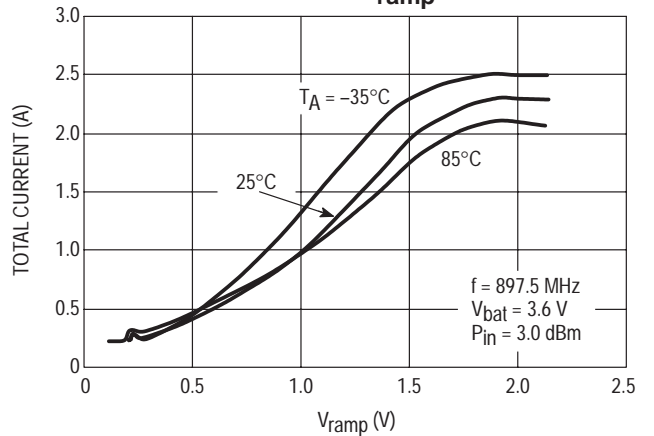


Figure 13. Total Current versus Vramp



MRFIC1859

DCS TYPICAL CHARACTERISTICS

Figure 14. Output Power versus Frequency

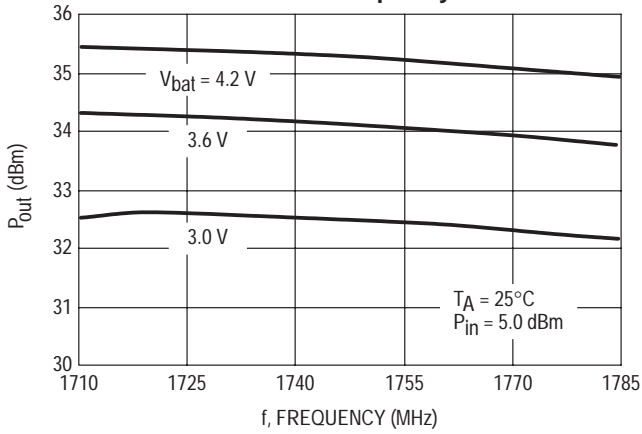


Figure 15. Power Added Efficiency versus Frequency

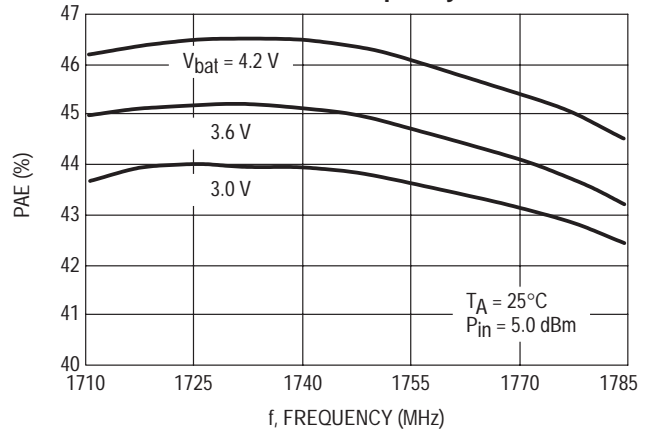


Figure 16. Output Power versus Frequency

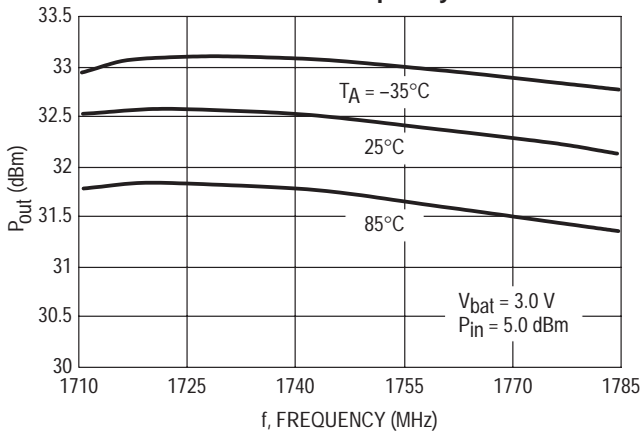


Figure 17. Output Power versus Frequency

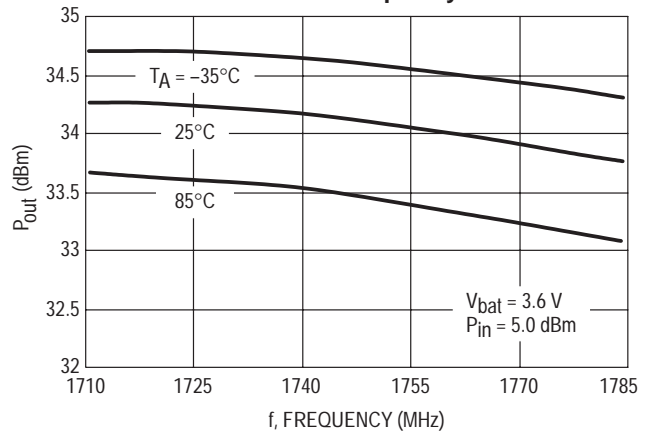


Figure 18. Output Power versus Frequency

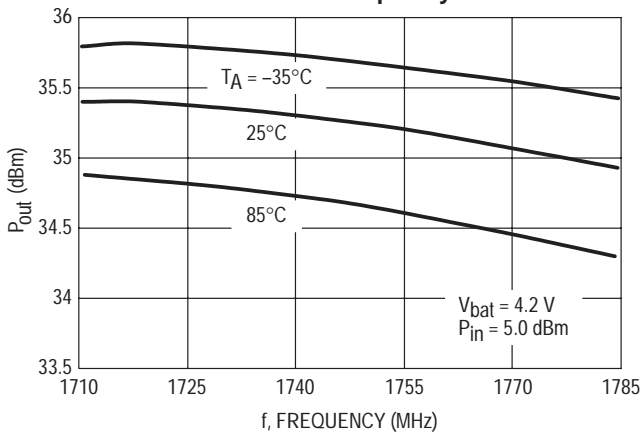
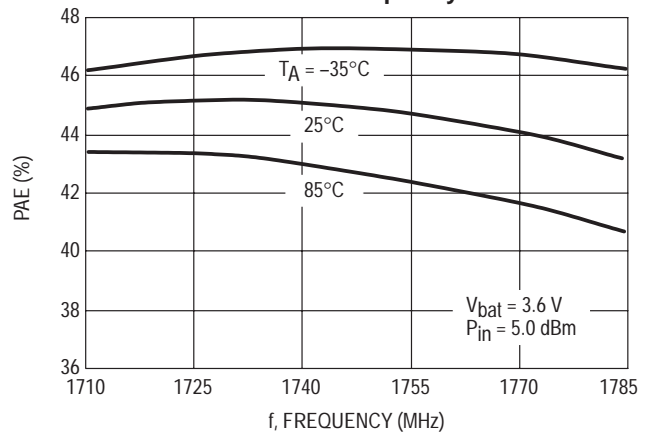


Figure 19. Power Added Efficiency versus Frequency



MRFIC1859

DCS TYPICAL CHARACTERISTICS

Figure 20. Second Harmonics versus Frequency

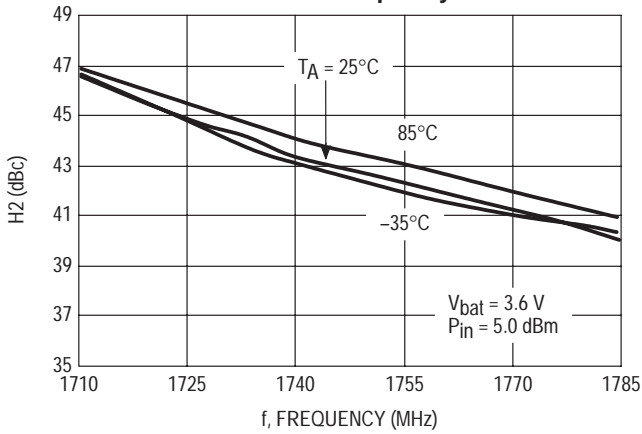


Figure 21. Third Harmonics versus Frequency

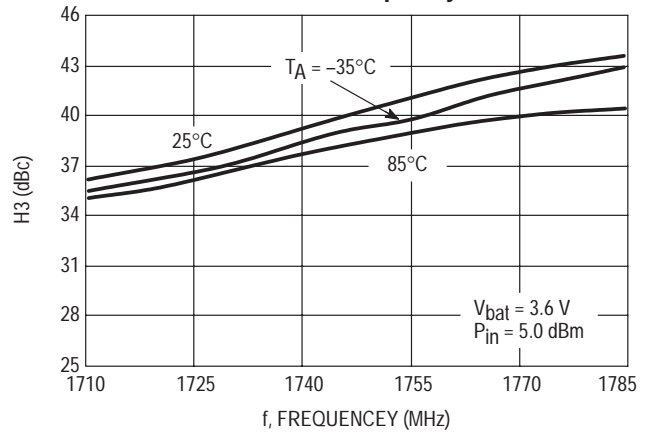


Figure 22. Positive Voltage Generator Output versus Frequency

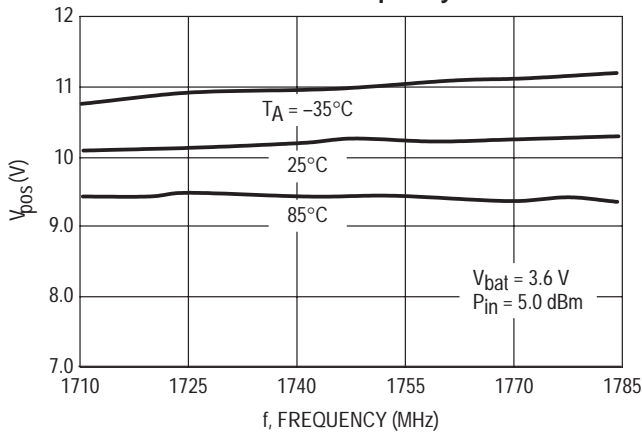


Figure 23. Output Power versus V_{ramp}

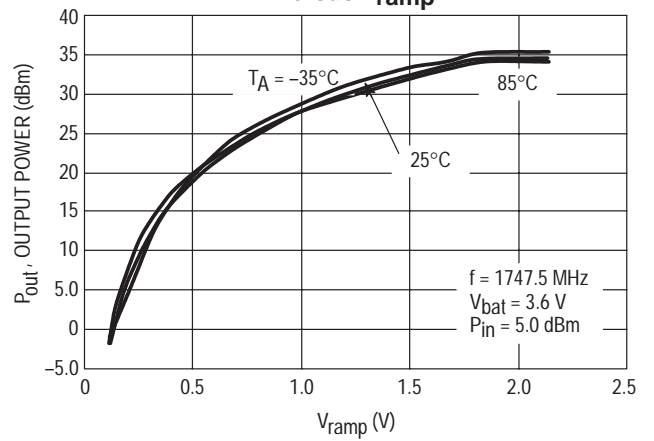
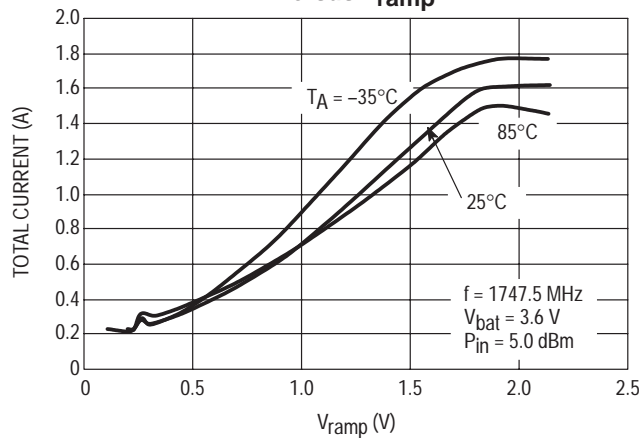


Figure 24. Total Current versus V_{ramp}



MRFIC1859

APPLICATIONS INFORMATION

Design Philosophy

The MRFIC1859 is a dual-band single supply RF integrated power amplifier designed for use in GSM900/DCS1800 handheld radios under 3.6 V operation. With matching circuit modifications, it is also applicable for use in triple band GSM900/DCS1800/PCS1900 equipment. Typical performances in GSM/DCS at 3.6 V are: GSM: 35.8 dBm with 53% PAE and, DCS: 34 dBm with 43% PAE.

It features a large band (900 to 1800 MHz) internal Negative Voltage Generator based on RF rectification of the input carrier after its amplification by two dedicated buffer stages (See Simplified Block Diagram). This method eliminates spurs found on the output signal when using dc/dc converter type negative voltage generators, either on or off chip. The buffer generates also a step-up positive voltage, which can be used to drive a NMOS drain switch.

External Circuit Considerations

The MRFIC1859 can be tuned by changing the values and/or positions of the appropriate external components (see Figure 1: Application Schematic). While tuning the RF line-up, it is recommended to apply external negative supply in order to prevent any damage to the power amplifier stages. Poor tuning on the input may not provide enough RF power to operate the negative voltage generator properly.

Input matching is a shunt-C, series-L, low pass structure for GSM and a shunt-L, series-L high pass structure for DCS. It should be optimized at the rated input power (e.g. 3.0 dBm in GSM, 5.0 dBm in DCS). Since the input lines feed both 1st stages and 1st stage buffers, input matching should be iterated with buffer and Q1 drain matching. Note that dc blocking capacitors are included on chip.

First stage buffer amplifier is tuned with a short 80 Ω microstrip line which may be replaced by a chip inductor. Second stage buffer amplifier is supplied and matched through a discrete chip inductor. Those two elements are tuned to get the maximum output from voltage generator. The overall typical buffer current (DB1 + DB2) is about 60 mA in GSM and 100 mA in DCS. However, the negative generator needs a settling time of 1.0 μ s (see burst mode paragraph). During this transient period of time, both stages are biased to IDSS, which is about 200 mA each.

The step-up positive voltage available at Pin 2, which is approximately 10 V in each band, can be used to drive a NMOS drain switch for best performances.

Q1 drains are supplied and matched through 80 Ω printed microstrip lines that could be replaced by discrete chip inductors as well. Their lengths (or equivalent inductor values) are tuned by sliding the RF decoupling capacitors along to get the maximum gain on the first stages.

Q2 drains are supplied through 60 Ω printed microstrip lines that contribute also to the interstage matching in order to optimum drive to the final stages.

The line length for Q2G and Q2D is small, so replacing it with discrete inductors is not practical.

Q3 stages are fed via 50 Ω printed microstrip lines that must handle the high supply current of that stages (2.0 Amp peak) without significant voltage drop. This line can be buried in an inner layer to save PCB space or be a discrete RF choke.

Output matching is accomplished in both bands with two stages low pass networks. Easy implementation is achieved

with shunt capacitors mounted along a 50 Ω microstrip transmission line. Value and position are chosen to reach a load line of 2.0 Ω while conjugating the device output parasitics. The networks must also properly terminate the second and third harmonic level. Use of high-Q capacitors for the first output matching capacitor circuits is recommended in order to get the best output power and efficiency performances.

Note: the choice of output matching capacitor type and supplier will affect H2 and H3 level and efficiency, because of series resonant frequency.

Tuning Methodology

The following section gives the user some guidelines and hints to tune and optimize the MRFIC1859 operation inside their own radio PCB. First of all, one must keep in mind that negative and positive voltage generation is based on RF carrier rectification. This means that RF input signal must always be present when running the part as a standalone solution. Therefore, in order to ease the tuning phase, it is recommended to apply the negative voltage externally in order to avoid any damage to the large RF MESFET transistors. This is particularly true if one uses the complete application with MC33170 (product of On Semiconductor) as control IC to do the optimization. In that case, both negative and positive voltage should be provided externally.

The RF decoupling capacitors have been selected as 47 pF for GSM band (C17, C14, C22, C9, C1, and C8) and 22 pF or 12 pF for DCS band (C10, C15, and C13). But those can be optimized depending on their size and source, for example 12 pF were used at some places for DCS to provide better decoupling of the harmonics too, thus providing some extra performance.

The recommended tuning procedure consists of several steps that need to be performed in sequential order. Several iterations can be performed if appropriate. Due to low interaction between line-ups, each band can be tuned independently.

- Optimize the buffer operation using D1B (T8 line) and D2B matching (L3 inductor). Simultaneously, tune GSM or DCS input matching using L1, C21 or L2, T10, respectively. Check the margin on P_{in} to generate V_{SS} and V_P (those voltages should still meet their specification with a 5.0 dB reduction in P_{in}). A small shunt capacitor can be placed on V_P to maximize that voltage.
- Optimize RF line up linear gain using D1G, D2G matching (T9 line) or D1D, D2D, G2D matching (T7 line, C8) for GSM or DCS line-up, respectively. The goal is to maximize and center small signal gain. P_{in} has to be reduced for this exercise, hence the negative voltage needs to be applied externally. A broad band measurement is helpful to visualize the frequency response. Linear gain should peak at around 40 dB for GSM and 32 dB for DCS. The input matching has to be checked again and eventually refined during this step.
- Optimize output matching using T4, C3, T1, C4 and T2 for GSM or T6, C2, T5, C6, T3 for DCS, respectively. Those elements set the P_{out} /PAE trade-off and harmonics rejection performance.

MRFIC1859

- Finally, one can iterate some of the above steps to fine tune RF behavior and also to find the best configuration for Cross-Talk and Harmonics content reduction. For example, D2B inductor L3 and V_{SS} decoupling capacitor C11 have a small influence on the GSM second harmonic leaking through the DCS output.

The nominal impedance seen from the IPA package pins have been measured on the demoboard (after removing the MRFIC1859) and are listed in the following table. They can be taken as a starting point for the optimization. Also this gives the equivalent lumped element if one uses a lumped element instead of microstrip line.

Impedance on the different GSM I/Os: (expressed in Ω at 900 MHz)

- $InG = 16.2 + j83.5$
- $OutG = 1.9 - j2.3$
- D2G = close to 0 since decoupled as short as possible
- $D1G = 1 + j19.8$ (3.5 nH)
- $D1B = 1.2 + j28.7$ (5.0 nH)
- D2B = infinite since 56 nH behaves as choke

Impedance on the different DCS I/Os: (expressed in Ω at 1750 MHz)

- $InD = 12.5 + j36.5$
- $OutD = 3.6 - j4.4$
- D2D = close to 0 since decoupled as short as possible
- $G2D = 0.9 + j6.8$ (0.64 nH)
- $D1D = 1.1 + j20.8$ (1.9 nH)
- $D1B = 8.8 + j84.7$ (7.6 nH)
- D2B = infinite since 56 nH behaves as choke

One should note that except for RF_{in}/RF_{out} impedance, all others should be "in theory" pure reactive shunt elements. The fact that their resistive part is not zero is linked to the finite quality factor of the equivalent inductor and also to the limited accuracy of the measurement (when close to the Smith chart border).

Control Considerations

The MRFIC1859 application uses drain control technique developed for our generations of GaAs IPAs. This method relies on the fact that for an RF power amplifier operating in saturation mode, the RF output power is proportional to the square of the Amplifier drain voltage: $P_{out} \text{ (Watt)} = k * V_D \text{ (V)} * V_D \text{ (V)}$.

A dedicated control IC MC33170 has been designed to manage all those control, biasing and band selection functions. When the emitting order is sent ($TxEn = \text{High}$), the MC33170 activates the power supply V_{Dbuf} of the negative voltage generator NVG ($V_{Dbuf} = V_{bat}$), involving the presence of V_{neg} as well as a positive V_P of about 9.0 V. Once V_{neg} detected and regulated at -5.0 V, the MC33170 enables a N-channel MOSFET to be driven.

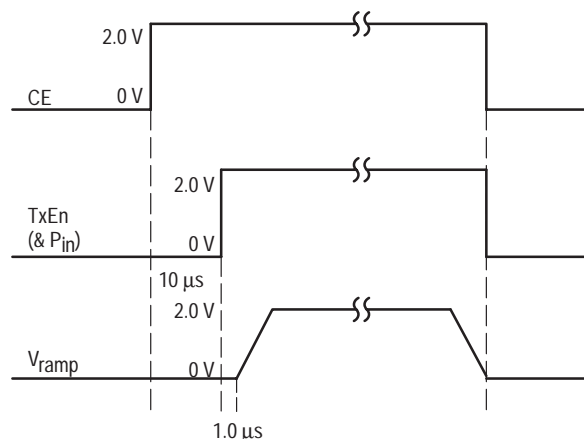
The NMOS is used as a ballast transistor whose drain-source resistance is controlled by V_{ramp} . This allows to supply the PA with a voltage from 0 V ($V_{ramp} = 0$ V) to V_{bat} ($V_{ramp} = 2.0$ V) and hence to control the output power. Such a way of control provides an excellent predictability of the RF output power (since the output voltage is proportional to the drain voltage) and eliminates the need for a power or current detection loop.

The band selection is achieved by setting the BS pin of the MC33170 to 0 V (GSM) or 1.0 V (DCS), hence biasing the GSM or DCS transistors through BiasGSM and BiasDCS pins.

Burst Mode

In order to perform burst mode measurements, the following time can be used as a guideline.

Figure 25.



- First the MC33170 must be awakened through CE to activate its Low Drop Out Regulator. The BS pin has also to be set according to the selected frequency band.
- Then TxEn is set high which supply the buffer stages and activates the Negative and Positive Voltage Generation. TxEn signal can be used to switch the input power (using a driver or attenuator) in order to provide higher isolation for on/off burst dynamic.
- V_{ramp} (Pin 1) can be applied soon after TxEn since the internal negative voltage generator settles in less than 1.0 μ s.

References (Motorola Application Notes)

- AN1599 – Power Control with the MRFIC0913 GaAs Integrated Power Amplifier and MC33169 Support IC.
- AN1697 – GSM900/DCS1800 Dual-Band 3.6 V Power Amplifier Solution with Open Loop Control Scheme.



Product Preview

Dual-Band GSM GPRS 3.6 V Integrated Power Amplifier

The MRFIC1869 is a dual-band single supply RF Power Amplifier for GSM900/DCS1800 hand held radios. The device is packaged in a MLF-32 with exposed backside pad allowing excellent electrical and thermal performance through a solderable contact.

- Single Supply Enhancement Mode pHEMT Technology
- Internal Input Matching
- High Power and Efficiency
- Typical 3.6 V Characteristics:
 - $P_{out} = 35.8 \text{ dBm}$, PAE = 55% for GSM
 - $P_{out} = 34 \text{ dBm}$, PAE = 45% for DCS
- Tri-Band Capability¹

MRFIC1869

DUAL-BAND GSM GPRS 3.6 V IPA

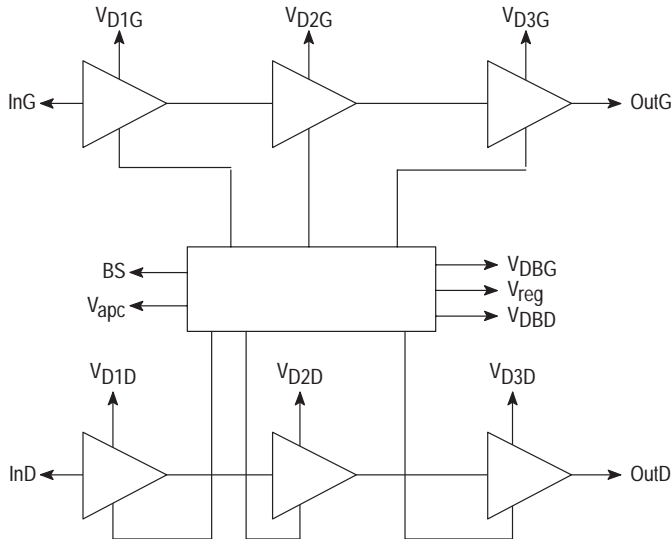
SEMICONDUCTOR TECHNICAL DATA

PLASTIC PACKAGE
CASE TBD
(MLF-32, 5x5)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MRFIC1869	$T_C = -35 \text{ to } 100^\circ\text{C}$	MLF-32

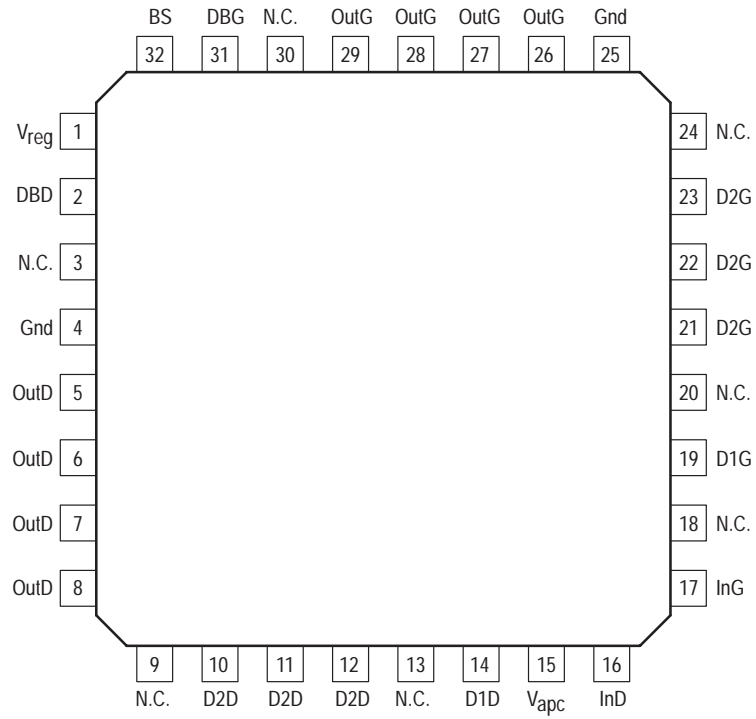
Simplified Block Diagram



1. This product can be used in a tri-band application with a specific DCS1800/PCS1900 matching network. This matching network results in a degradation of Pout, PAE and input power as noted in the Electrical Characteristics table.

MRFIC1869

PIN CONNECTIONS





Product Preview

Dual-Band CDMA Upconverter

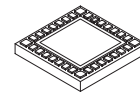
The MRFIC1884 is an integrated upmixer, RF AGC amplifier and driver amplifier designed for dual-band, tri-mode CDMA/AMPS/PCS CDMA cellular radios. The device incorporates a temperature compensated linear gain control and an active bias control that reduces supply current at lower output power. The design utilizes Motorola's RF BiCMOS process and is packaged in a small cost effective BCC32++ package.

- Designed for Dual-Band, Tri-Mode Operation
 - Total Supply Current CDMA/PCS CDMA Mode = 60 mA (Typ)
 - Total Supply Current AMPS Mode = 42 mA (Typ)
- High Output Power
 - 6.0 dBm for CDMA
 - 6.0 dBm for PCS CDMA
 - 11 dBm for AMPS
- Supply Voltage Range: 2.7 to 3.2 V

MRFIC1884

DUAL-BAND CDMA UPCONVERTER

SEMICONDUCTOR TECHNICAL DATA



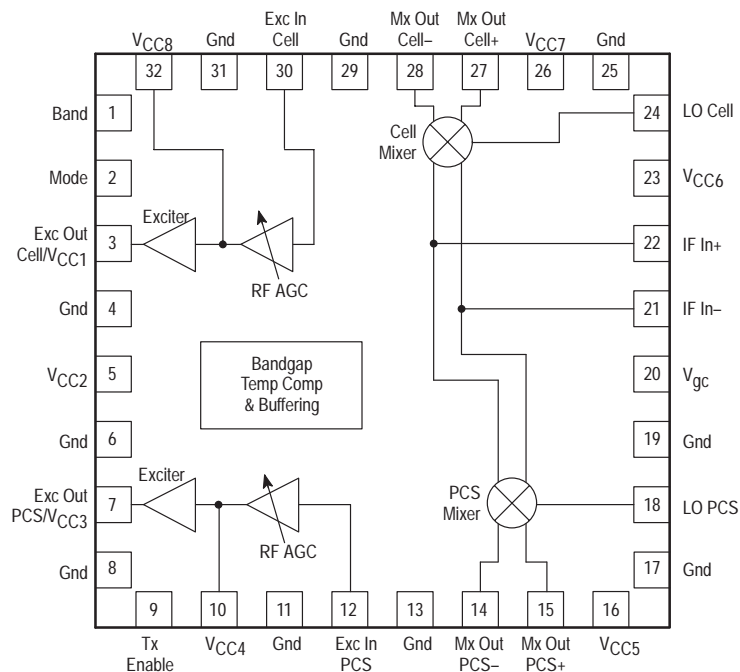
(Scale 2:1)

PLASTIC PACKAGE
CASE 1261A
(BCC32++)

ORDERING INFORMATION

Device	Operating Temp Range	Package
MRFIC1884R2	T _A = -40 to 85°C	BCC32++

Simplified Block Diagram and Pin Connections



MRFIC1884

PIN FUNCTION DESCRIPTION

Pin	Function	Description	Voltage On (V)	Voltage Off (V)
1	Band	Band Selection pin. A logic "High" (>2.4 V) selects PCS band and "Low" (<0.4 V) selects Cellular band.	2.4 to 3.2	0 to 0.4
2	Mode	Mode selection pin. A logic "High" (>2.4 V) selects CDMA band and "Low" (<0.4 V) selects AMPS band.	2.4 to 3.2	0 to 0.4
3	Exciter Out (Cellular)/ VCC1	Cellular band RF Exciter output pin.	2.7 to 3.2	
4	Gnd	Ground connection.	–	
5	VCC2	Supply Voltage.	2.7 to 3.2	
6	Gnd	Ground connection.	–	
7	Exciter Out (PCS)/ VCC3	PCS band RF Exciter output pin.	2.7 to 3.2	
8	Gnd	Ground connection.	–	
9	Tx Enable	Tx Enable pin. A logic "High" (>2.4 V) enables Tx path and "Low" (<0.4 V) disables Tx path except LO Buffer and bandgap reference (will disable the entire chip complete with Band selection pin and Mode selection pin, refer to Table ?).	2.4 to 3.2	0 to 0.4
10	VCC4	Supply Voltage.	2.7 to 3.2	
11	Gnd	Ground connection.	–	
12	Exciter In (PCS)	PCS band RF Exciter input pin.	–	
13	Gnd	Ground connection.	–	
14	Mixer Out– (PCS)	PCS band Mixer RF output pin.	2.7 to 3.2	
15	Mixer Out+ (PCS)	PCS band Mixer RF output pin.	2.7 to 3.2	
16	VCC5	Supply Voltage.	2.7 to 3.2	
17	Gnd	Ground connection.	–	
18	LO (PCS)	PCS band Mixer LO input pin.	–12 dBm (Typ)	
19	Gnd	Ground connection.	–	
20	V _{gc}	RF AGC control pin. A 30 dB dynamic range can be achieved by adjusting voltage from 0.1 V (low gain) to 1.7 V (high gain).	0.1 to 1.7	
21	IF In–	Mixer IF input pin.	–23 dBm (Typ)	
22	IF In+	Mixer IF input pin.	–23 dBm (Typ)	
23	VCC6	Supply Voltage.	2.7 to 3.2	
24	LO (Cellular)	Cellular band Mixer LO input pin.	–13 dBm (Typ)	
25	Gnd	Ground connection.	–	
26	VCC7	Supply Voltage.	2.7 to 3.2	
27	Mixer Out+ (Cellular)	Cellular band Mixer RF output pin.	2.7 to 3.2	
28	Mixer Out– (Cellular)	Cellular band Mixer RF output pin.	2.7 to 3.2	
29	Gnd	Ground connection.	–	
30	Exciter In (Cellular)	Cellular band RF Exciter input pin.	–	
31	Gnd	Ground connection.	–	
32	VCC8	Supply Voltage.	2.7 to 3.2	

Chapter Three

RF/IF Subsystem ICs

Section One	3.1–0
RF/IF Subsystem ICs – Selector Guide	
Section Two	3.2–0
RF/IF Subsystem ICs – Data Sheets	

Section One Selector Guide

RF/IF Subsystems

Table of Contents

	Page
Cordless Phone Subsystems	3.1-2
Tranceivers	3.1-2
Miscellaneous Functions	3.1-3
ADCs/DACs	3.1-3
Encoders/Decoders	3.1-3
Packages	3.1-4

RF/IF Subsystems

Cordless Phone Subsystem ICs

Device	V _{CC}	I _{CC} (Typ)	Dual Conversion Receiver	Universal Dual PLL	Compa n d e r a n d A u d i o I n t e r f a c e	CVSD Compatible	Low Battery Detect	Notes	Suffix/ Case No.
MC13110A	2.7 to 5.5 V	Active Mode 8.5 mA Inactive Mode 15 μA	✓	✓	✓	–	✓	CT-0	FB/848B FTA/932
MC13111A	2.7 to 5.5 V	Active Mode 8.5 mA Inactive Mode 15 μA	✓	✓	✓	–	✓	CT-0	FB/848B, FTA/932
MC13145	2.7 to 6.5 V	Active Mode 27 mA Inactive Mode 10 μA	✓	–	–	✓	–	Receiver with coilless demod CT-900	FTA/932
MC13146	2.7 to 6.5 V	Active Mode 18 mA Inactive Mode 10 μA	–	–	–	✓	–	Transmitter with VCO CT-900	FTA/977

Tranceivers

Device	V _{CC}	I _{CC}	GSM Receiver	TDMA/iDEN Receiver	Fractional-N PLL	Direct Launch GSM Transmitter	System Applicability	Case No./ Pkg Type
MC13760(46a)★	2.65 to 2.9 4.78 to 5.22 (Charge Pumps)	Transmit 20 mA Receive 30 mA	✓	✓	✓	✓	GSM/DCS, TDMA, iDEN, AMPS	1285/ BGA-104

(46)To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

Miscellaneous Functions

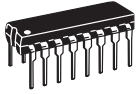
ADCs/DACs

Device	Function	I/O Format	Resolution	Number of Analog Channels	On-Chip Oscillator	Other Features	Suffix/ Case No.
MC144110	DAC	Serial	6 Bits	6	-	Emitter-Follower Outputs	DW/751D
MC144111				4			DW/751G

Encoders/Decoders

Device	Function	Number of Address Lines	Maximum Number of Address Codes	Number of Data Bits	Operation	Suffix/ Case No.
MC145026	Encoder	Depends on Decoder	Depends on Decoder	Depends on Decoder	Simplex	P/648, D/751B
MC145027	Decoder	5	243	4	Simplex	P/648, DW/751G
MC145028		9	19,683	0	Simplex	

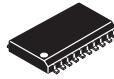
RF/IF Subsystems Packages



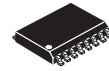
CASE 648
P SUFFIX
(DIP-16)



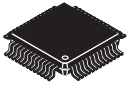
CASE 751B
D SUFFIX
(SO-16)



CASE 751D
DW SUFFIX
(SO-20L)



CASE 751G
DW SUFFIX
(SO-16W)



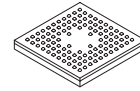
CASE 848B
FB SUFFIX
(QFP-52)



CASE 932
FTA SUFFIX
(LQFP-48)



CASE 977
FTA SUFFIX
(LQFP-24)



CASE 1285
(BGA-104)

Section Two

RF/IF Subsystems – Data Sheets

Device Number	Page Number	Device Number	Page Number
Cordless Phone Subsystems		Miscellaneous Functions	
MC13110A	3.2-16	ADCs/DACs	
MC13111A	3.2-16	MC144110	3.2-257
MC13145	3.2-91	MC144111	3.2-257
MC13146	3.2-108		
MC33411A	3.2-216	Encoders/Decoders	
Receivers		MC145026	3.2-263
MC3356	3.2-3	MC145027	3.2-263
MC13135	3.2-79	MC145028	3.2-263
MC13150	3.2-122		
MC13156	3.2-154		
MC13158	3.2-172		
Transceivers			
MC13760	3.2-211		
IF			
MC13055	3.2-9		
MC13155	3.2-139		
Transmitters			
MC13176	3.2-194		

Wideband FSK Receiver

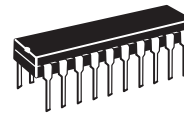
The MC3356 includes Oscillator, Mixer, Limiting IF Amplifier, Quadrature Detector, Audio Buffer, Squelch, Meter Drive, Squelch Status output, and Data Shaper comparator. The MC3356 is designed for use in digital data communications equipment.

- Data Rates up to 500 kilobaud
- Excellent Sensitivity: -3 dB Limiting Sensitivity
 $30 \mu\text{Vrms}$ @ 100 MHz
- Highly Versatile, Full Function Device, yet Few External Parts are Required
- Down Converter Can be Used Independently — Similar to NE602

MC3356

WIDEBAND FSK RECEIVER

SEMICONDUCTOR TECHNICAL DATA



P SUFFIX
PLASTIC PACKAGE
CASE 738

DW SUFFIX
PLASTIC PACKAGE
CASE 751D
(SO-20L)

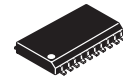
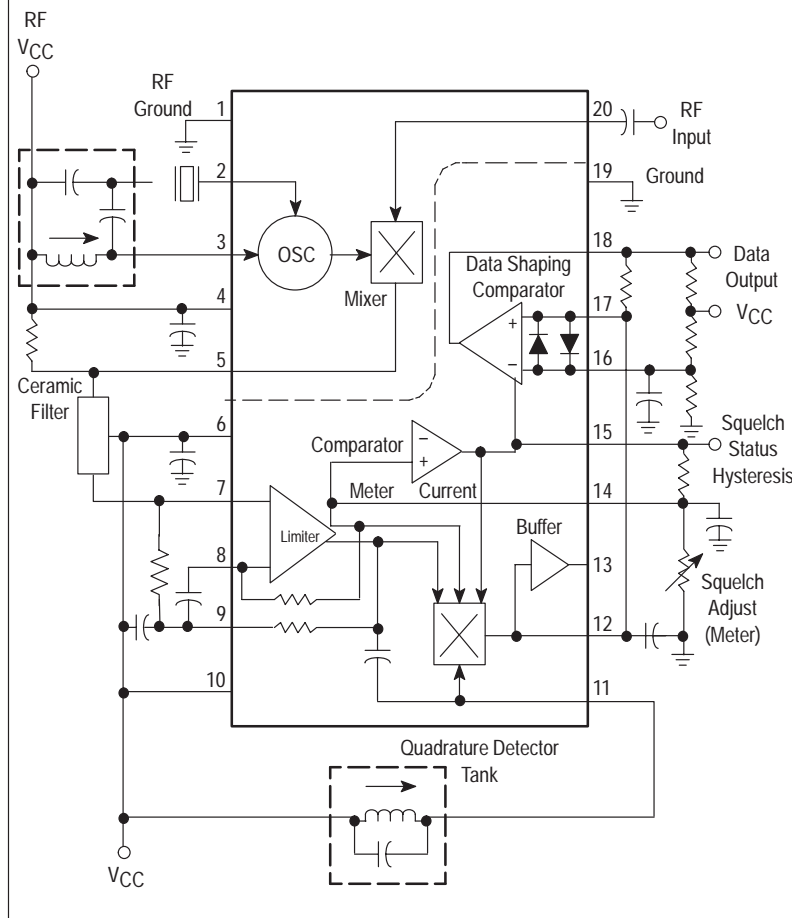
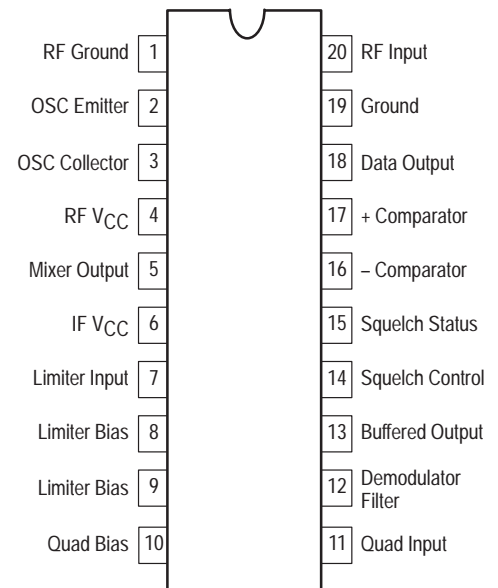


Figure 1. Representative Block Diagram



PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC3356DW	$T_A = -40$ to $+85^\circ\text{C}$	SO-20L
MC3356P		Plastic DIP

MAXIMUM RATINGS

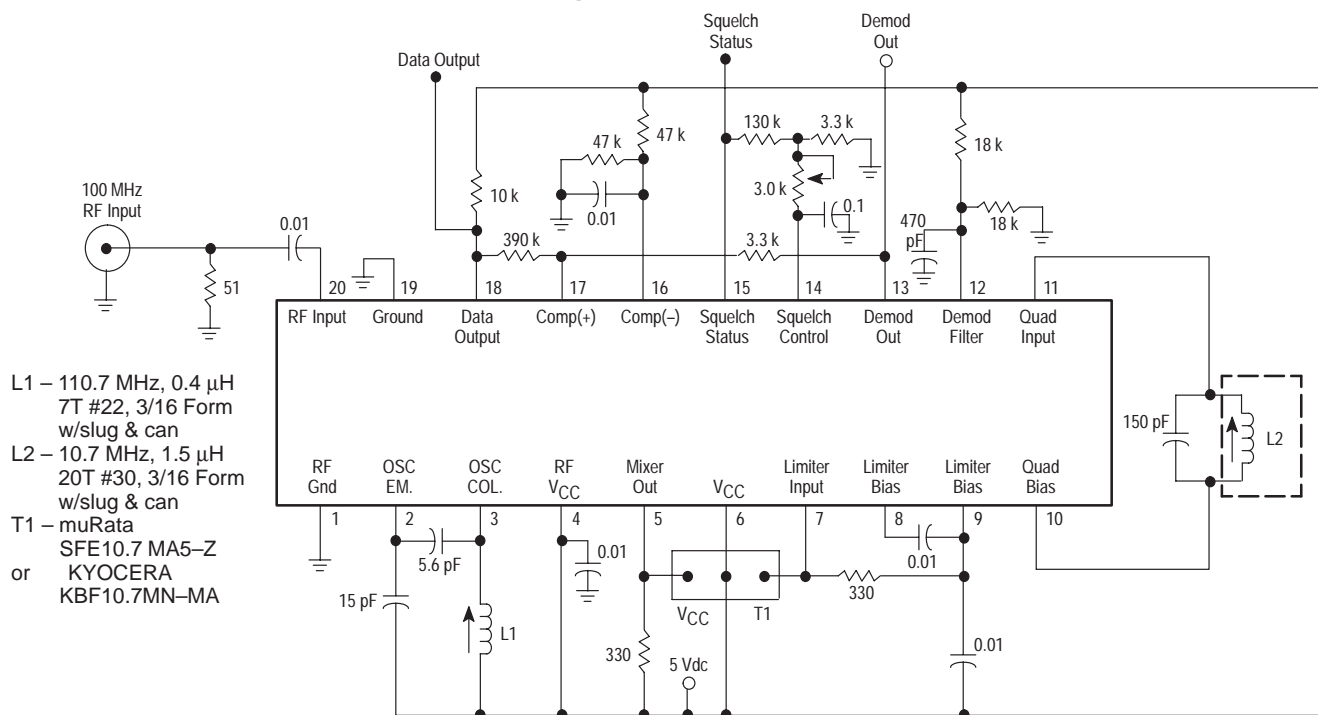
Rating	Symbol	Value	Unit
Power Supply Voltage	V _{CC(max)}	15	Vdc
Operating Power Supply Voltage Range (Pins 6, 10)	V _{CC}	3.0 to 9.0	Vdc
Operating RF Supply Voltage Range (Pin 4)	RF V _{CC}	3.0 to 12.0	Vdc
Junction Temperature	T _J	150	°C
Operating Ambient Temperature Range	T _A	- 40 to + 85	°C
Storage Temperature Range	T _{stg}	- 65 to + 150	°C
Power Dissipation, Package Rating	P _D	1.25	W

ELECTRICAL CHARACTERISTICS (V_{CC} = 5.0 Vdc, f₀ = 100 MHz, f_{osc} = 110.7 MHz, Δf = ±75 kHz, f_{mod} = 1.0 kHz, 50 Ω source, T_A = 25°C, test circuit of Figure 2, unless otherwise noted.)

Characteristics	Min	Typ	Max	Unit
Drain Current Total, RF V _{CC} and V _{CC}	-	20	25	mAdc
Input for - 3 dB limiting	-	30	-	μVrms
Input for 50 dB quieting ($\frac{S+N}{N}$)	-	60	-	μVrms
Mixer Voltage Gain, Pin 20 to Pin 5	2.5	-	-	
Mixer Input Resistance, 100 MHz	-	260	-	Ω
Mixer Input Capacitance, 100 MHz	-	5.0	-	pF
Mixer/Oscillator Frequency Range (Note 1)	-	0.2 to 150	-	MHz
IF/Quadrature Detector Frequency Range (Note 1)	-	0.2 to 50	-	MHz
AM Rejection (30% AM, RF V _{in} = 1.0 mVrms)	-	50	-	dB
Demodulator Output, Pin 13	-	0.5	-	Vrms
Meter Drive	-	7.0	-	μA/dB
Squelch Threshold	-	0.8	-	Vdc

NOTE: 1. Not taken in Test Circuit of Figure 2; new component values required.

Figure 2. Test Circuit



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 3. Output Components of Signal, Noise, and Distortion

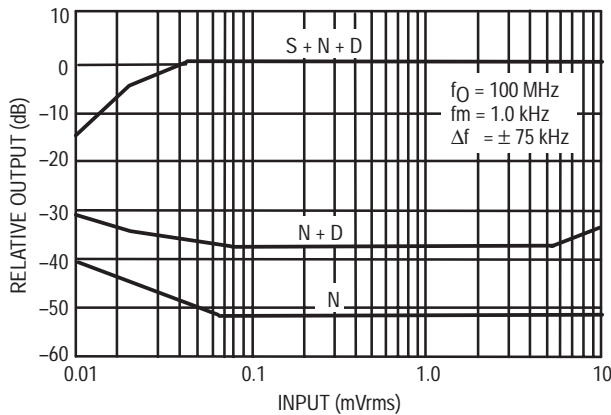
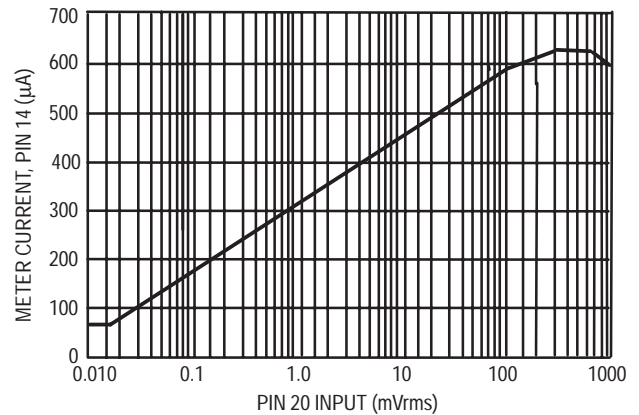


Figure 4. Meter Current versus Signal Input



GENERAL DESCRIPTION

This device is intended for single and double conversion VHF receiver systems, primarily for FSK data transmission up to 500 K baud (250 kHz). It contains an oscillator, mixer, limiting IF, quadrature detector, signal strength meter drive, and data shaping amplifier.

The oscillator is a common base Colpitts type which can be crystal controlled, as shown in Figure 1, or L-C controlled as shown in the other figures. At higher V_{CC} , it has been operated as high as 200 MHz. A mixer/oscillator voltage gain of 2 up to approximately 150 MHz, is readily achievable.

The mixer functions well from an input signal of 10 μVrms , below which the squelch is unpredictable, up to about 10 mVrms, before any evidence of overload. Operation up to 1.0 Vrms input is permitted, but non-linearity of the meter output is incurred, and some oscillator pulling is suspected. The AM rejection above 10 mVrms is degraded.

The limiting IF is a high frequency type, capable of being operated up to 50 MHz. It is expected to be used at 10.7 MHz in most cases, due to the availability of standard ceramic resonators. The quadrature detector is internally coupled to the IF, and a 5.0 pF quadrature capacitor is internally provided. The -3dB limiting sensitivity of the IF itself is approximately 50 μV (at Pin 7), and the IF can accept signals up to 1.0 Vrms without distortion or change of detector quiescent dc level.

The IF is unusual in that each of the last 5 stages of the 6 state limiter contains a signal strength sensitive, current sinking device. These are parallel connected and buffered to produce a signal strength meter drive which is fairly linear for IF input signals of 10 μV to 100 mVrms (see Figure 4).

A simple squelch arrangement is provided whereby the meter current flowing through the meter load resistance flips a comparator at about 0.8 Vdc above ground. The signal strength at which this occurs can be adjusted by changing the meter load resistor. The comparator (+) input and output are available to permit control of hysteresis. Good positive

action can be obtained for IF input signals of above 30 μVrms . The 130 k Ω resistor shown in the test circuit provides a small amount of hysteresis. Its connection between the 3.3 k resistor to ground and the 3.0 k pot, permits adjustment of squelch level without changing the amount of hysteresis.

The squelch is internally connected to both the quadrature detector and the data shaper. The quadrature detector output, when squelched, goes to a dc level approximately equal to the zero signal level unsquelched. The squelch causes the data shaper to produce a high (V_{CC}) output.

The data shaper is a complete "floating" comparator, with back to back diodes across its inputs. The output of the quadrature detector can be fed directly to either input of this amplifier to produce an output that is either at V_{CC} or V_{EE} , depending upon the received frequency. The impedance of the biasing can be varied to produce an amplifier which "follows" frequency detuning to some degree, to prevent data pulse width changes.

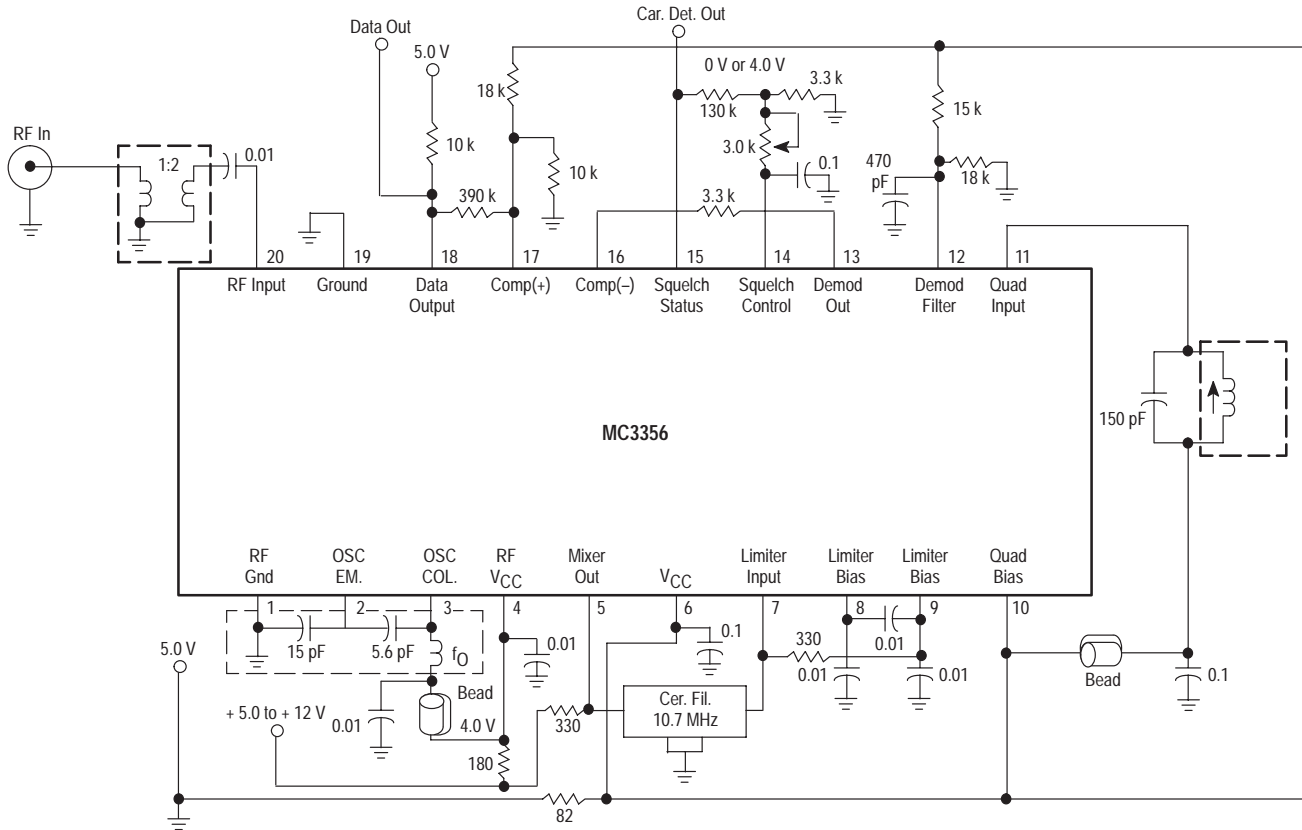
When the data shaper is driven directly from the demodulator output, Pin 13, there may be distortion at Pin 13 due to the diodes, but this is not important in the data application. A useful note in relating high/low input frequency to logic state: low IF frequency corresponds to low demodulator output. If the oscillator is above the incoming RF frequency, then high RF frequency will produce a logic low (input to (+) input of Data Shaper as shown in Figures 1 and 2).

APPLICATION NOTES

The MC3356 is a high frequency/high gain receiver that requires following certain layout techniques in designing a stable circuit configuration. The objective is to minimize or eliminate, if possible, any unwanted feedback.

MC3356

Figure 5. Application with Fixed Bias on Data Shaper



APPLICATION NOTES (continued)

Shielding, which includes the placement of input and output components, is important in minimizing electrostatic or electromagnetic coupling. The MC3356 has its pin connections such that the circuit designer can place the critical input and output circuits on opposite ends of the chip. Shielding is normally required for inductors in tuned circuits.

The MC3356 has a separate V_{CC} and ground for the RF and IF sections which allows good external circuit isolation by minimizing common ground paths.

Note that the circuits of Figures 1 and 2 have RF, Oscillator, and IF circuits predominantly referenced to the plus supply rails. Figure 5, on the other hand, shows a suitable means of ground referencing. The two methods produce identical results when carefully executed. It is important to treat Pin 19 as a ground node for either approach. The RF input should be "grounded" to Pin 1 and then the input and the mixer/oscillator grounds (or RF V_{CC} bypasses) should be connected by a low inductance path to Pin 19. IF and detector sections should also have their

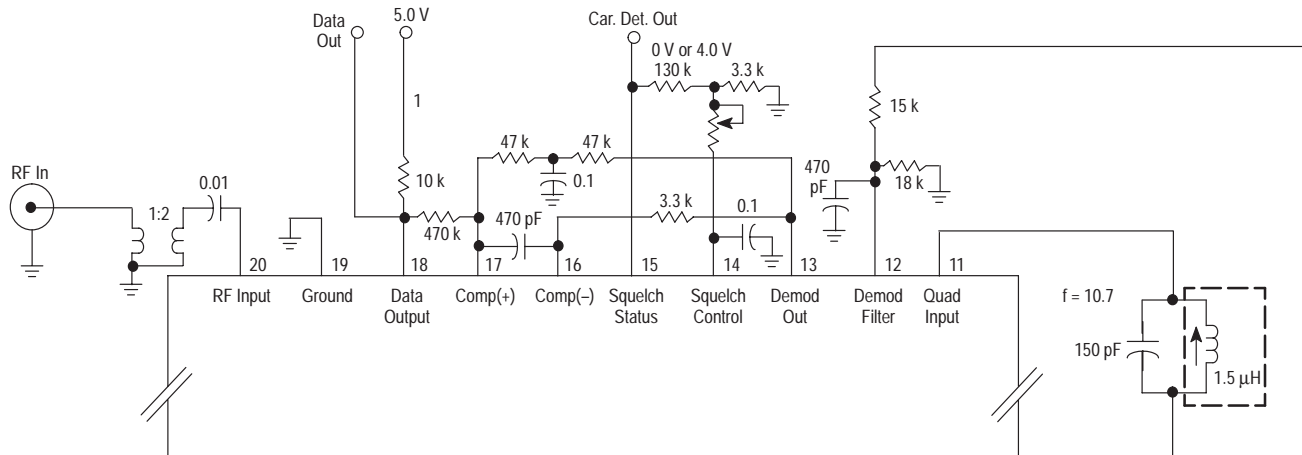
bypasses returned by a **separate** path to Pin 19. V_{CC} and RF V_{CC} can be decoupled to minimize feedback, although the configuration of Figure 2 shows a successful implementation on a common 5.0 V supply. Once again, the message is: define a supply node and a ground node and return each section to those nodes by separate, low impedance paths.

The test circuit of Figure 2 has a 3 dB limiting level of 30 μ V which can be lowered 6 db by a 1:2 untuned transformer at the input as shown in Figures 5 and 6. For applications that require additional sensitivity, an RF amplifier can be added, but with no greater than 20 db gain. This will give a 2.0 to 2.5 μ V sensitivity and any additional gain will reduce receiver dynamic range without improving its sensitivity. Although the test circuit operates at 5.0 V, the mixer/oscillator optimum performance is at 8.0 V to 12 V. A minimum of 8.0 V is recommended in high frequency applications (above 150 MHz), or in PLL applications where the oscillator drives a prescaler.

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 6. Application with Self-Adjusting Bias on Data Shaper

**APPLICATION NOTES (continued)**

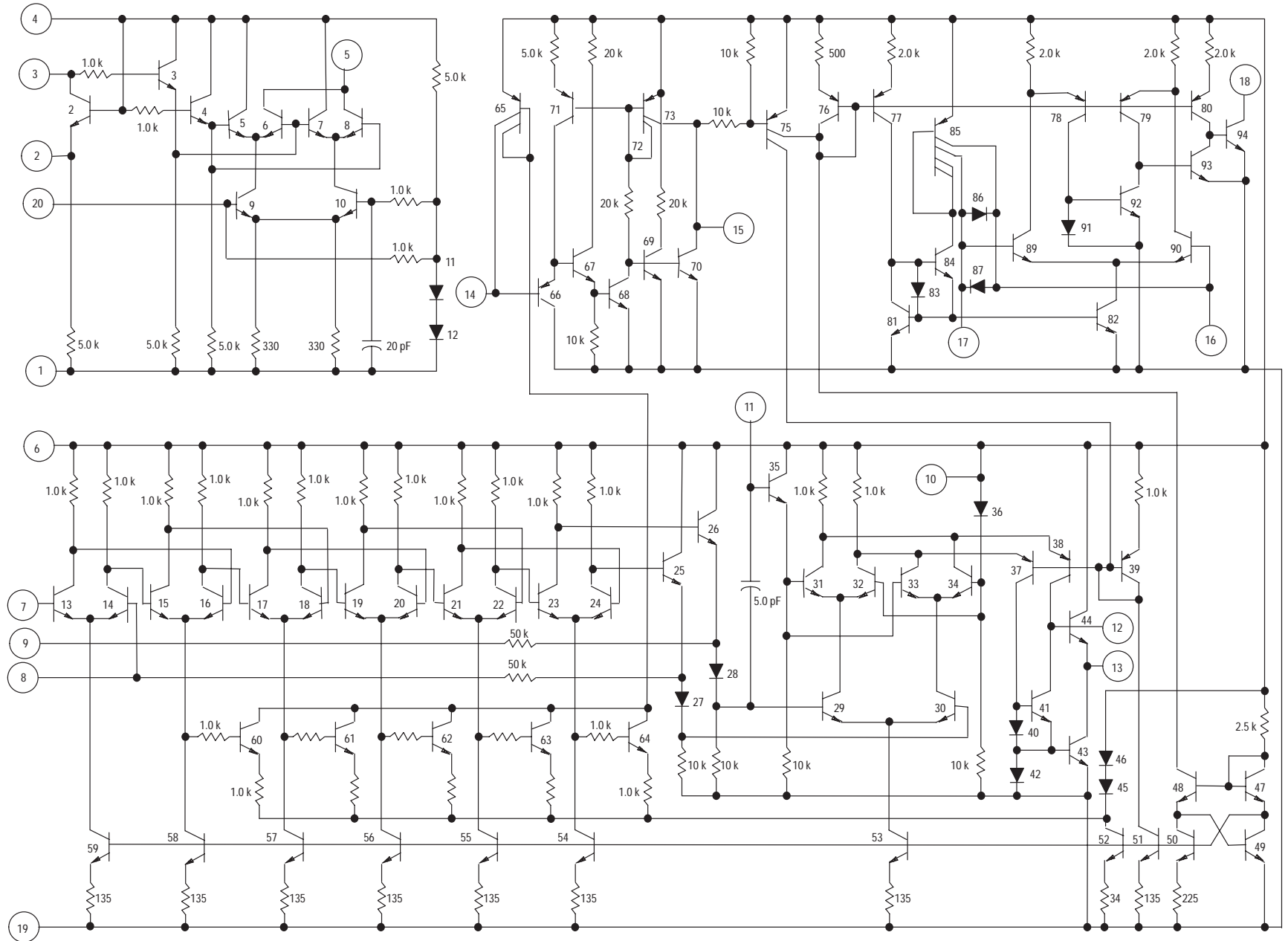
Depending on the external circuit, inverted or noninverted data is available at Pin 18. Inverted data makes the higher frequency in the FSK signal a “one” when the local oscillator is above the incoming RF. Figure 5 schematic shows the comparator with hysteresis. In this circuit the dc reference voltage at Pin 17 is about the same as the demodulated output voltage (Pin 13) when no signal is present. This type circuit is preferred for systems where the data rates can drop to zero. Some systems have a low frequency limit on the data rate, such as systems using the MC3850 ACIA that has a start or stop bit. This defines the low frequency limit that can appear in the data stream.

Figure 5 circuit can then be changed to a circuit configuration as shown in Figure 6. In Figure 6 the reference voltage for the comparator is derived from the demodulator output through a low pass circuit where τ is much lower than the lowest frequency data rate. This and similar circuits will compensate for small tuning changes (or drift) in the quadrature detector.

Squelch status (Pin 15) goes high (squelch off) when the input signal becomes greater than some preset level set by the resistance between Pin 14 and ground. Hysteresis is added to the circuit externally by the resistance from Pin 14 to Pin 15.

NOT RECOMMENDED FOR NEW DESIGNS

Figure 7. Internal Schematic



NOT RECOMMENDED FOR NEW DESIGNS



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13055

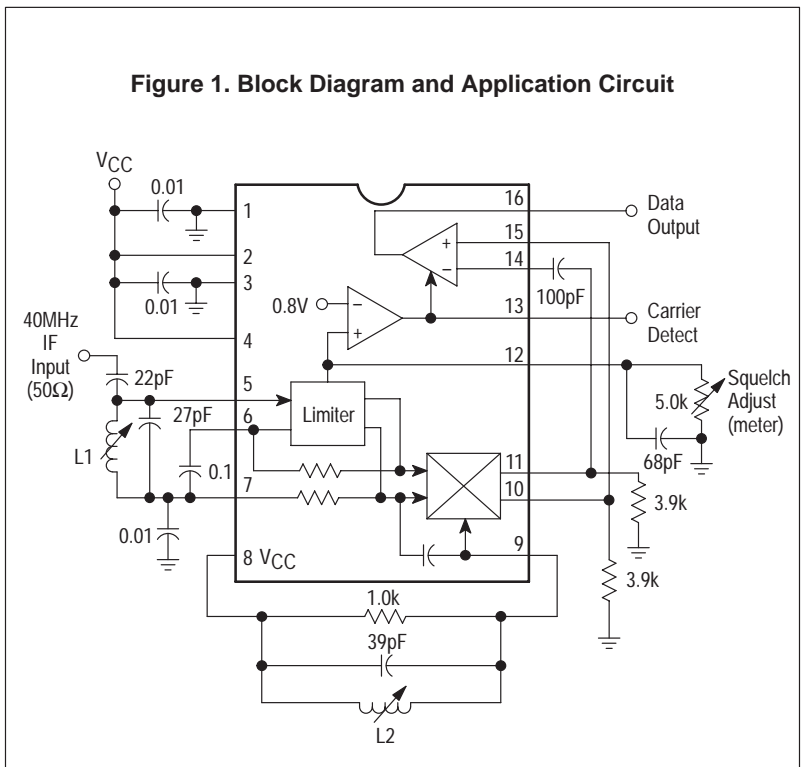
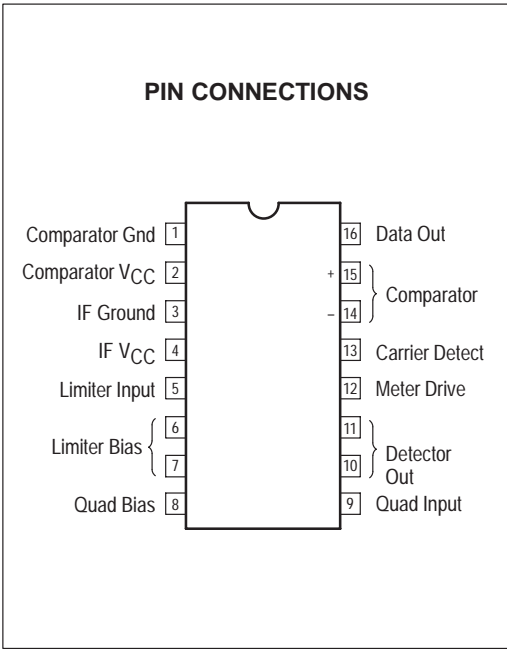
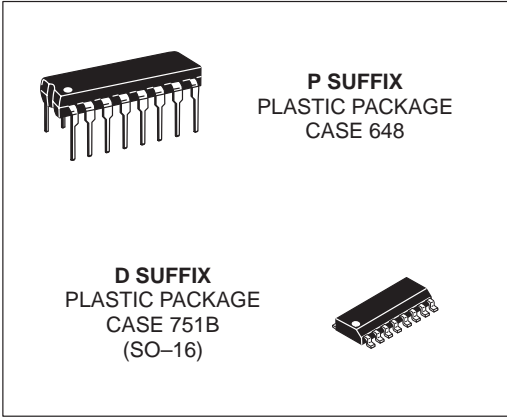
Wideband FSK Receiver

The MC13055 is intended for RF data link systems using carrier frequencies up to 40 MHz and FSK (frequency shift keying) data rates up to 2.0 M Baud (1.0 MHz). This design is similar to the MC3356, except that it does not include the oscillator/mixer. The IF bandwidth has been increased and the detector output has been revised to a balanced configuration. The received signal strength metering circuit has been retained, as has the versatile data slicer/comparator.

- Input Sensitivity 20 μ V @ 40 MHz
- Signal Strength Indicator Linear Over 3 Decades
- Available in Surface Mount Package
- Easy Application, Few Peripheral Components

WIDEBAND FSK RECEIVER

SEMICONDUCTOR TECHNICAL DATA



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13055D	T _A = - 40 to +85°C	SO-16
MC13055P		Plastic DIP

MC13055

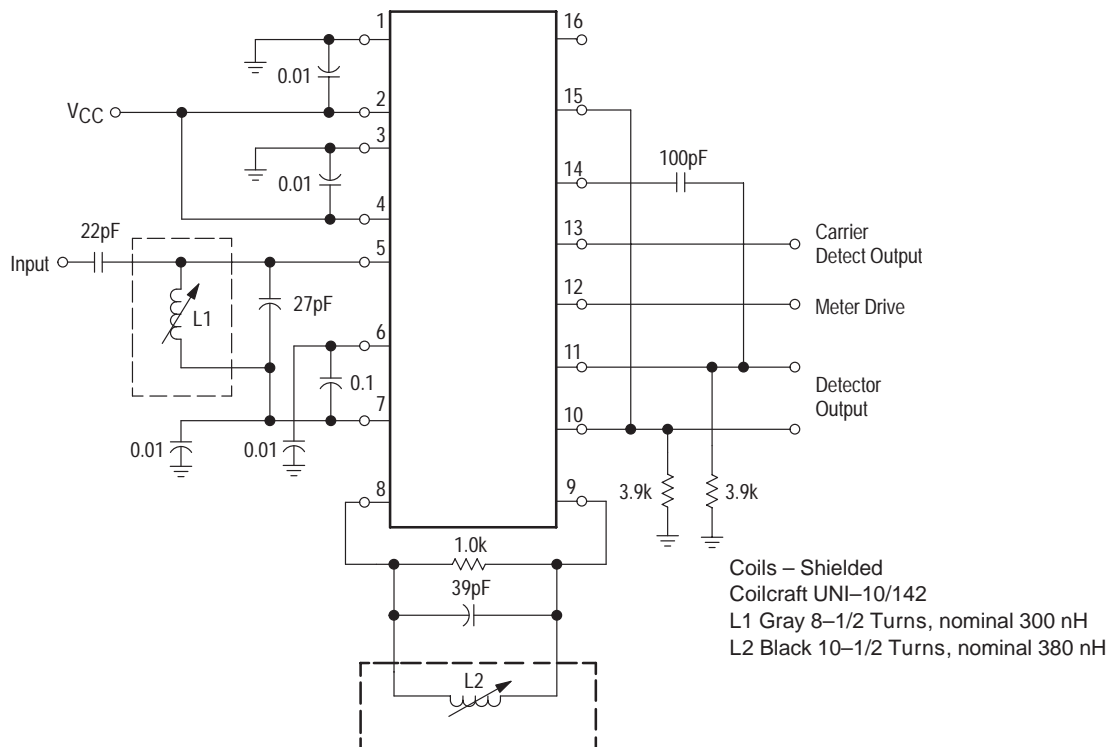
MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Power Supply Voltage	$V_{CC(max)}$	15	Vdc
Operating Supply Voltage Range	V2, V4	3.0 to 12	Vdc
Junction Temperature	T_J	150	°C
Operating Ambient Temperature Range	T_A	-40 to +85	°C
Storage Temperature Range	T_{stg}	-65 to +150	°C
Power Dissipation, Package Rating	P_D	1.25	W

ELECTRICAL CHARACTERISTICS ($V_{CC} = 5.0$ Vdc, $f_0 = 40$ MHz, $f_{mod} = 1.0$ MHz, $\Delta f = \pm 1.0$ MHz, $T_A = 25^\circ\text{C}$, test circuit of Figure 2.)

Characteristic	Conditions	Min	Typ	Max	Unit	
Total Drain Current	I2 + I4	-	20	25	mA	
Data Comparator Pull-Down Current	I16	-	10	-	mA	
Meter Drive Slope versus Input	I12	4.5	7.0	9.0	$\mu\text{A/dB}$	
Carrier Detect Pull-Down Current	I13	-	1.3	-	mA	
Carrier Detect Pull-Up Current	I13	-	500	-	μA	
Carrier Detect Threshold Voltage	V12	690	800	1010	mV	
DC Output Current	I10, I11	-	430	-	μA	
Recovered Signal	V10 - V11	-	350	-	mVrms	
Sensitivity for 20 dB S + N/N, BW = 5.0 MHz	VIN	-	20	-	μVrms	
S + N/N at $V_{in} = 50 \mu\text{V}$	V10 - V11	-	30	-	dB	
Input Impedance @ 40 MHz	R_{in}	Pin 5, Ground	-	4.2	-	k Ω
	C_{in}		-	4.5	-	pF
Quadrature Coil Loading	R_{in}	Pin 9 to 8	-	7.6	-	k Ω
	C_{in}		-	5.2	-	pF

Figure 2. Test Circuit



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 3. Overall Gain, Noise, AM Rejection

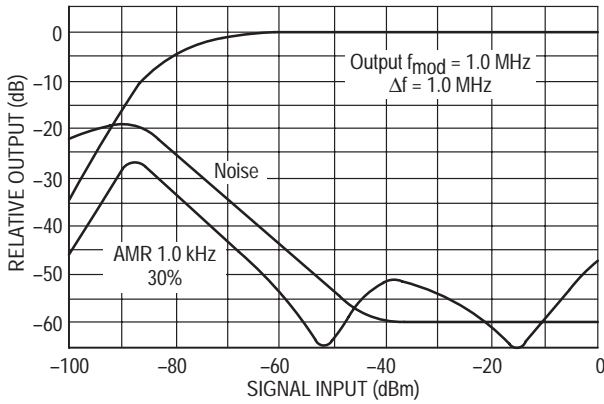


Figure 4. Meter Current versus Signal

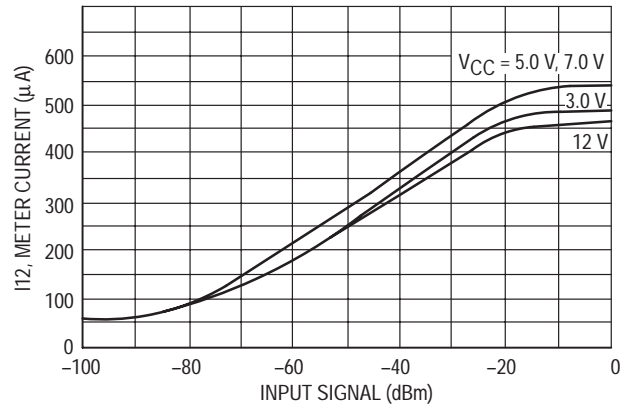


Figure 5. Untuned Input: Limiting Sensitivity versus Frequency

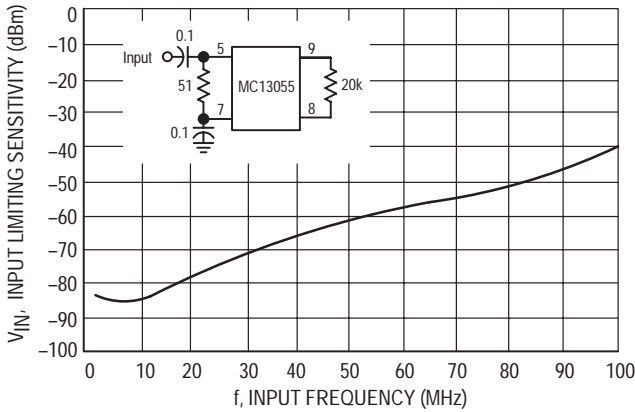


Figure 6. Untuned Input: Meter Current versus Frequency

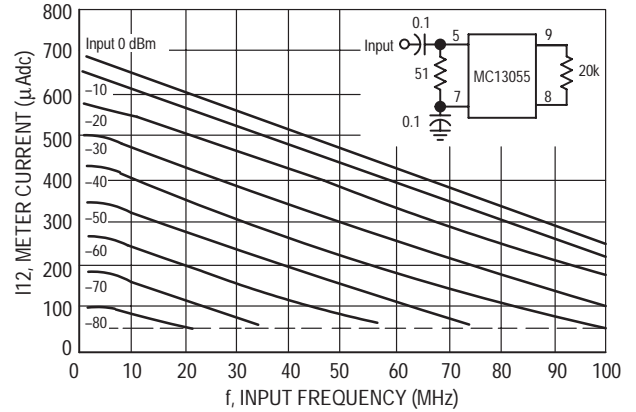


Figure 7. Limiting Sensitivity and Detuning versus Supply Voltage

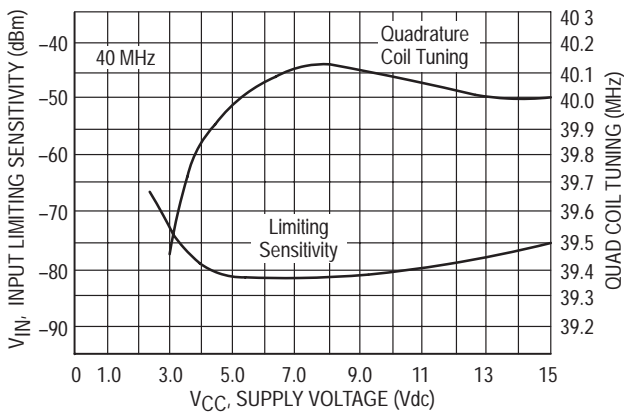
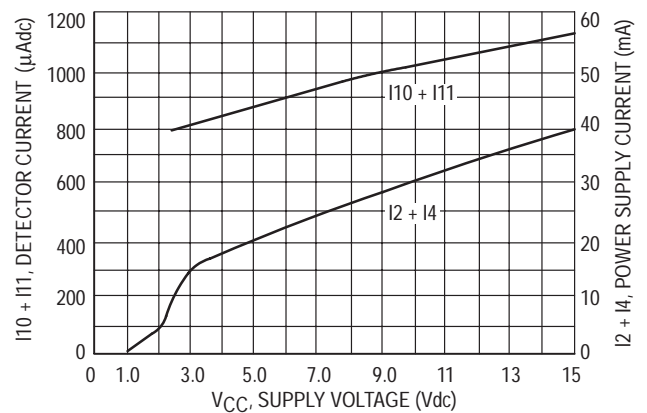


Figure 8. Detector Current and Power Supply Current versus Supply Voltage



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 9. Recovered Audio versus Temperature

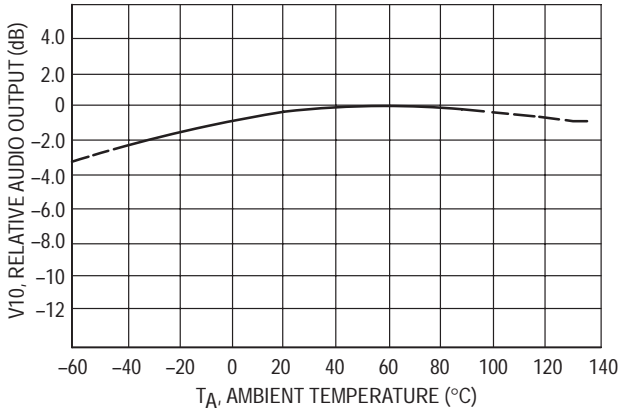


Figure 10. Carrier Detect Threshold versus Temperature

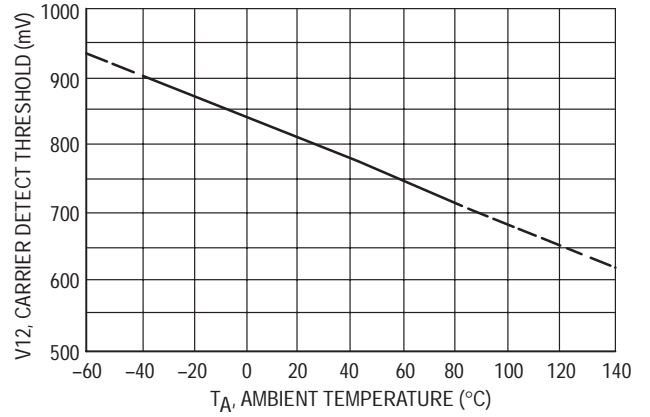


Figure 11. Meter Current versus Temperature

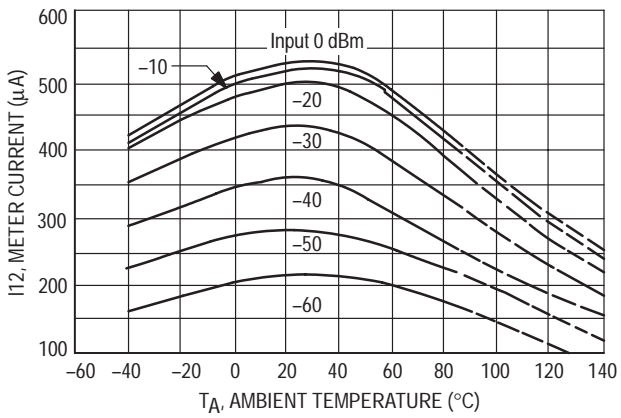


Figure 12. Input Limiting versus Temperature

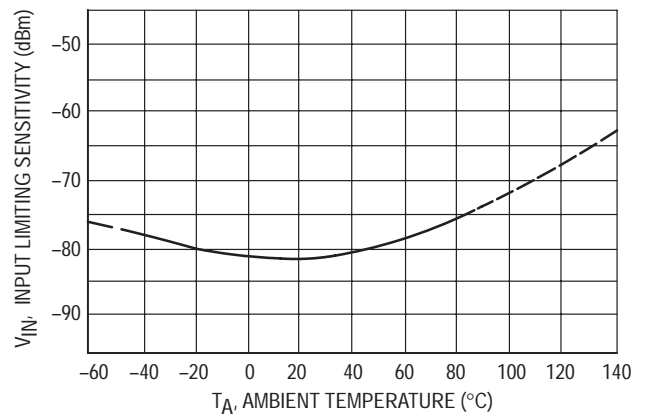
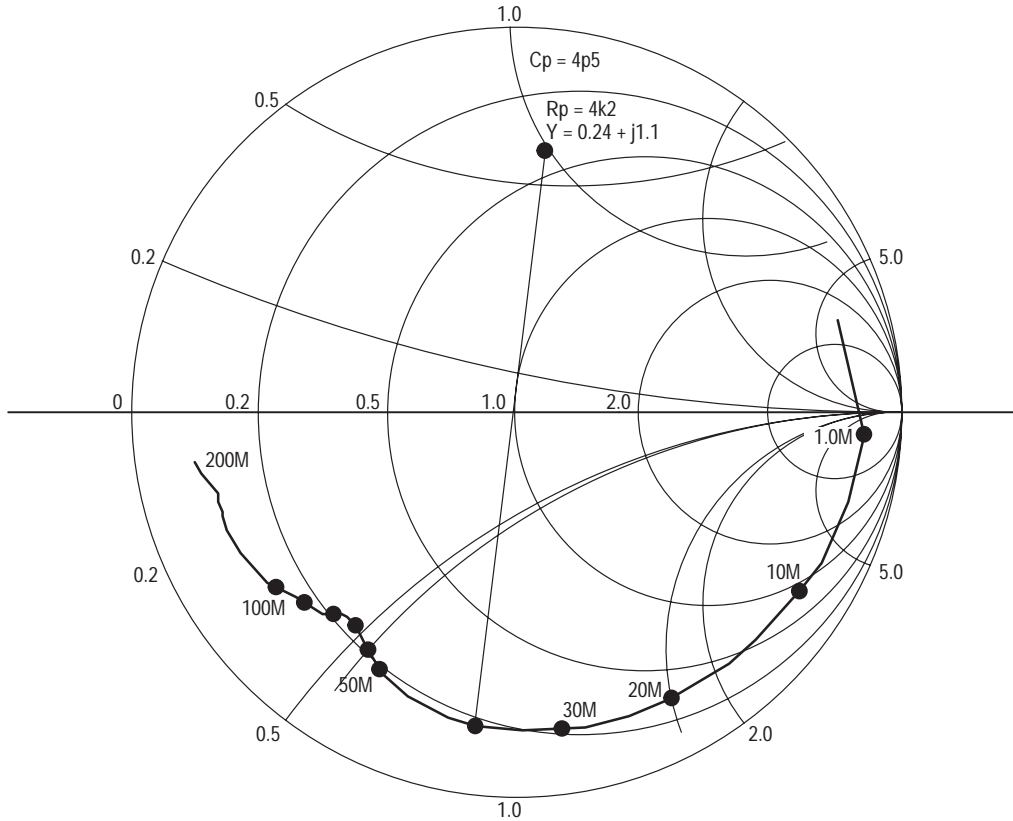


Figure 13. Input Impedance, Pin 5

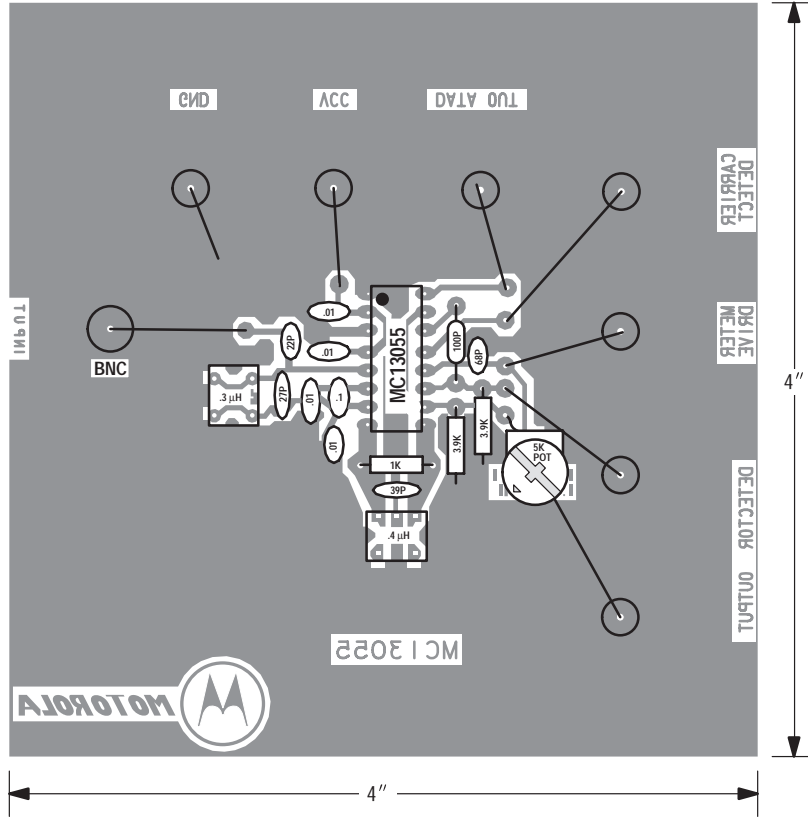


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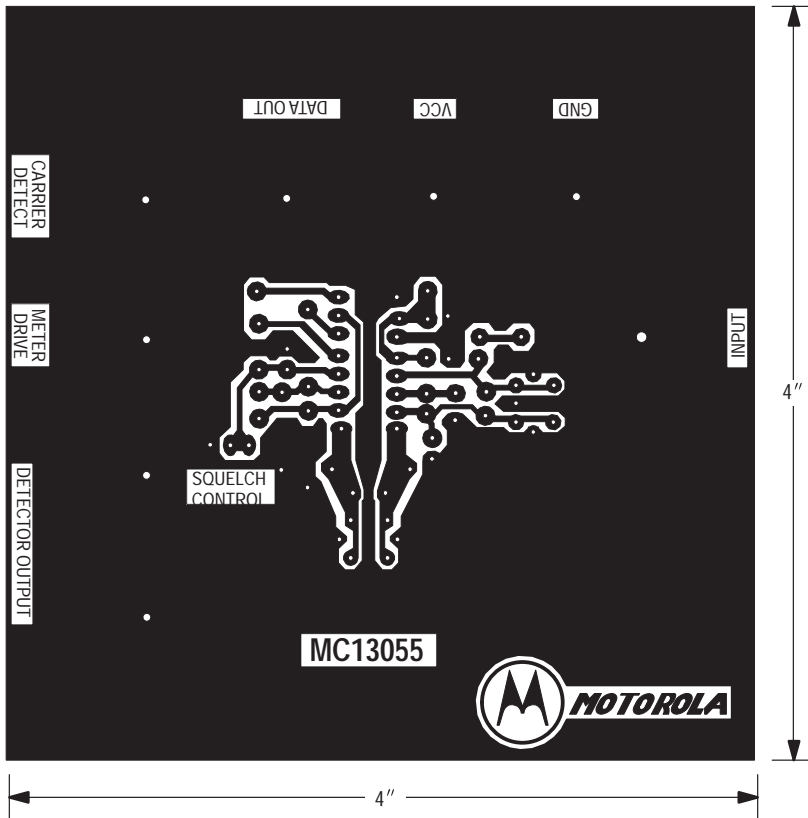
NOT RECOMMENDED FOR NEW DESIGNS

MC13055

Figure 14. Test Fixture
(Component Layout)



(Circuit Side View)

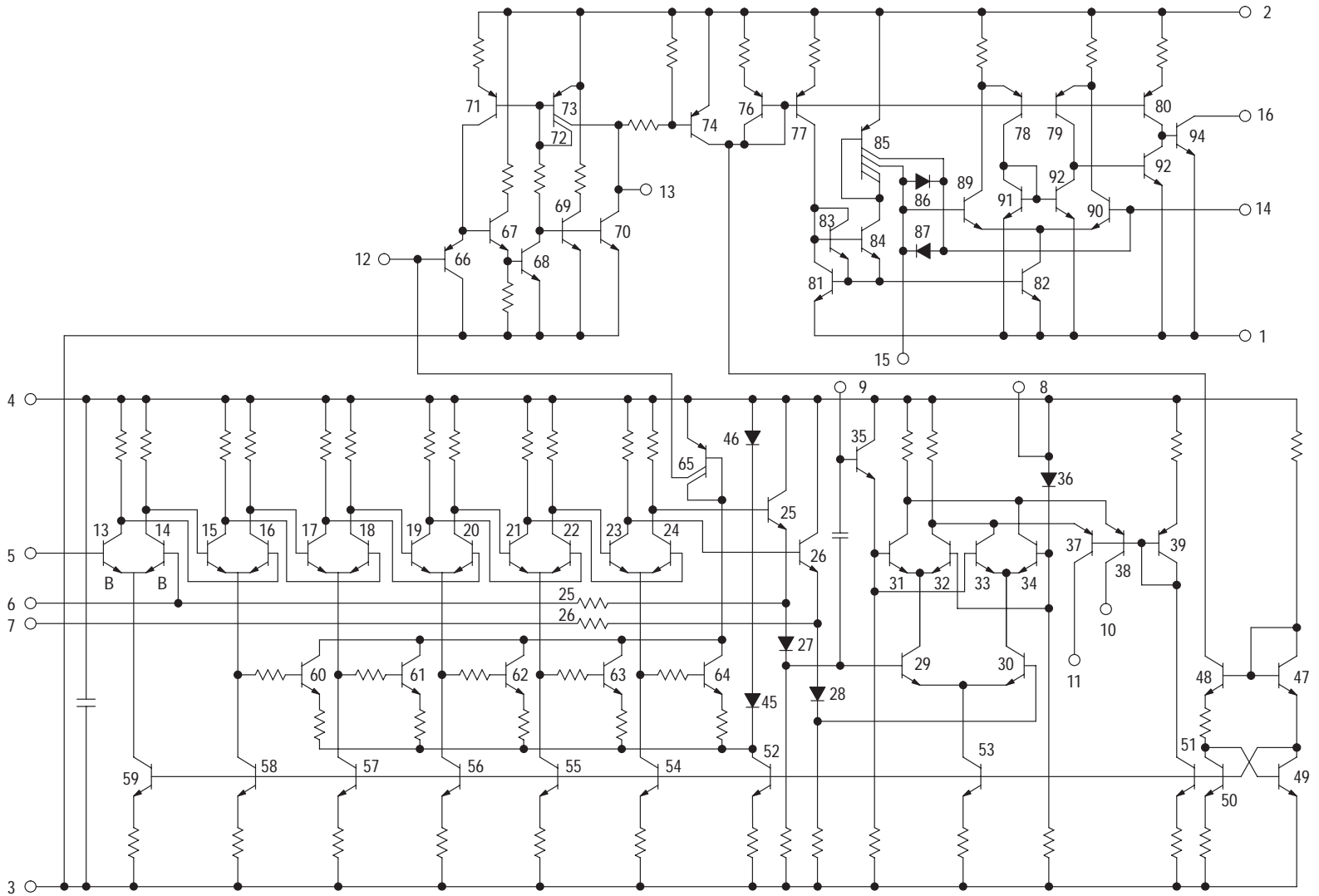


NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 15. Internal Schematic



MC13055
3-2-14

MOTOROLA WIRELESS RF, IF AND TRANSMITTER DEVICE DATA

MC13055

NOT RECOMMENDED FOR NEW DESIGNS

MC13055

GENERAL DESCRIPTION

The MC13055 is an extended frequency range FM IF, quadrature detector, signal strength detector and data shaper. It is intended primarily for FSK data systems. The design is very similar to MC3356 except that the oscillator/mixer has been removed, and the frequency capability of the IF has been raised about 2:1. The detector output configuration has been changed to a balanced, open-collector type to permit symmetrical drive of the data shaper (comparator). Meter drive and squelch features have been retained.

The limiting IF is a high frequency type, capable of being operated up to 100 MHz. It is expected to be used at 40 MHz in most cases. The quadrature detector is internally coupled to the IF, and a 2.0 pF quadrature capacitor is internally provided. The 20 dB quieting sensitivity is approximately 20 μ V, tuned input, and the IF can accept signals up to 220 mVrms without distortion or change of detector quiescent DC level.

The IF is unusual in that each of the last 5 stages of the 6 stage limiter contains a signal strength sensitive, current sinking device. These are parallel connected and buffered

to produce a signal strength meter drive which is fairly linear for IF input signals of 20 μ V to 20 mVrms (see Figure 4).

A simple squelch arrangement is provided whereby the meter current flowing through the meter load resistance flips a comparator at about 0.8 Vdc above ground. The signal strength at which this occurs can be adjusted by changing the meter load resistor. The comparator (+) input and output are available to permit control of hysteresis. Good positive action can be obtained for IF input signals of above 20 μ Vrms. A resistor (R) from Pin 13 to Pin 12 will provide V_{CC}/R of feedback current. This current can be correlated to an amount of signal strength hysteresis by using Figure 4.

The squelch is internally connected to the data shaper. Squelch causes the data shaper to produce a high (V_{CC}) output.

The data shaper is a complete "floating" comparator, with diodes across its inputs. The outputs of the quadrature detector can be fed directly to either or preferably both inputs of the comparator to produce a squared output swinging from V_{CC} to ground in inverted or noninverted form.

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS



MOTOROLA

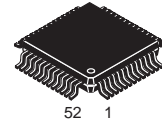
Universal Cordless Telephone Subsystem IC

The MC13110A and MC13111A integrates several of the functions required for a cordless telephone into a single integrated circuit. This significantly reduces component count, board space requirements, external adjustments, and lowers overall costs. It is designed for use in both the handset and the base.

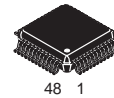
- Fully Programmable in all Power Modes
- Dual Conversion FM Receiver
 - Complete Dual Conversion Receiver – Antenna Input to Audio Out
 - 80 MHz Maximum Carrier Frequency
 - RSSI Output
 - Carrier Detect Output with Programmable Threshold
 - Comparator for Data Recovery
 - Operates with Either a Quad Coil or Ceramic Discriminator
- Compander
 - Expander Includes Mute, Digital Volume Control, Speaker Driver, Programmable Low Pass Filter, and Gain Block
 - Compressor Includes Mute, Programmable Low Pass Filter, Limiter, and Gain Block
- MC13110A only: Frequency Inversion Scrambler
 - Function Controlled via MPU Interface
 - Programmable Carrier Modulation Frequency
- Dual Universal Programmable PLL
 - Supports New 25 Channel U.S. Standard with No External Switches
 - Universal Design for Domestic and Foreign Cordless Telephone Standards
 - Digitally Controlled Via a Serial Interface Port
 - Receive Side Includes 1st LO VCO, Phase Detector, and 14–Bit Programmable Counter and 2nd LO with 12–Bit Counter
 - Transmit Section Contains Phase Detector and 14–Bit Counter
 - MPU Clock Outputs Eliminates Need for MPU Crystal
- Low Battery Detect
 - Provides Two Levels of Monitoring with Separate Outputs
 - Separate, Adjustable Trip Points
- 2.7 to 5.5 V Operation (15 μ A Current Consumption in Inactive Mode)
- AN1575: Refer to this Application Note for a List of the “Worldwide Cordless Telephone Frequencies

MC13110A MC13111A

UNIVERSAL NARROWBAND FM RECEIVER INTEGRATED CIRCUIT



FB SUFFIX
PLASTIC PACKAGE
CASE 848B
(QFP–52)

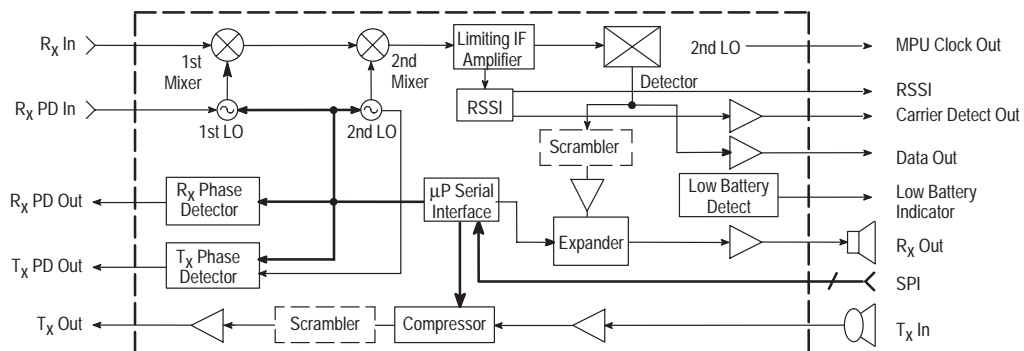


FTA SUFFIX
PLASTIC PACKAGE
CASE 932
(LQFP–48)

ORDERING INFORMATION

Device	Tested Operating Temperature Range	Package
MC13110AFB	$T_A = -40^\circ$ to 85°C	QFP–52
MC13110AFTA		LQFP–48
MC13111AFB		QFP–52
MC13111AFTA		LQFP–48

Simplified Block Diagram



NOTE:

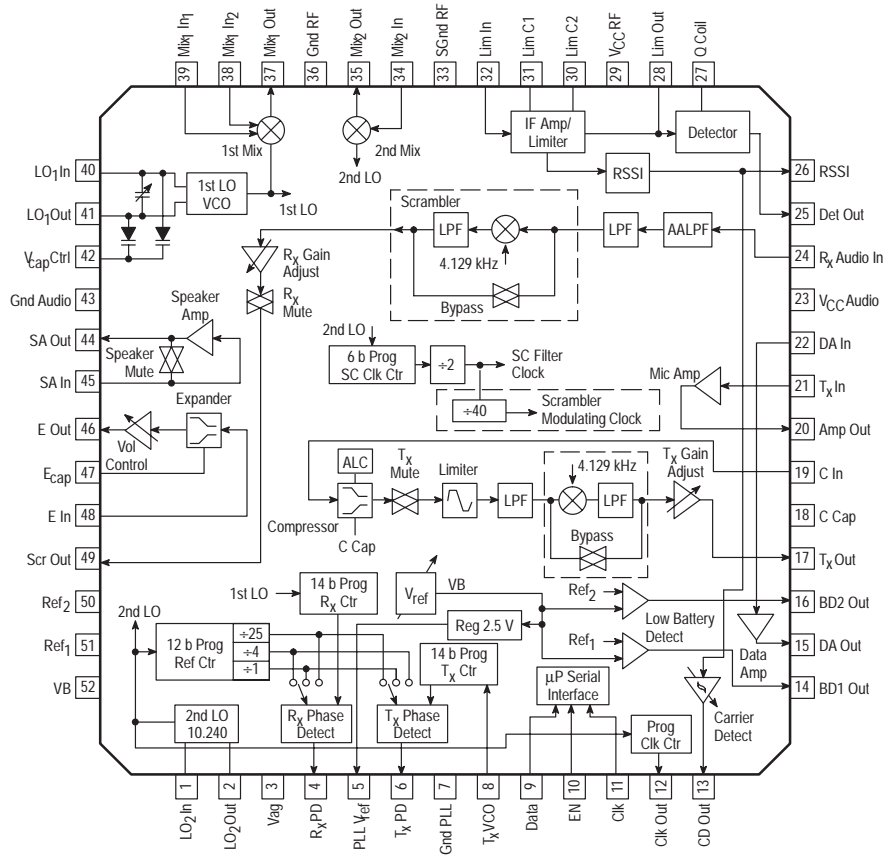
[] = MC13110A Only

This device contains 8262 active transistors.

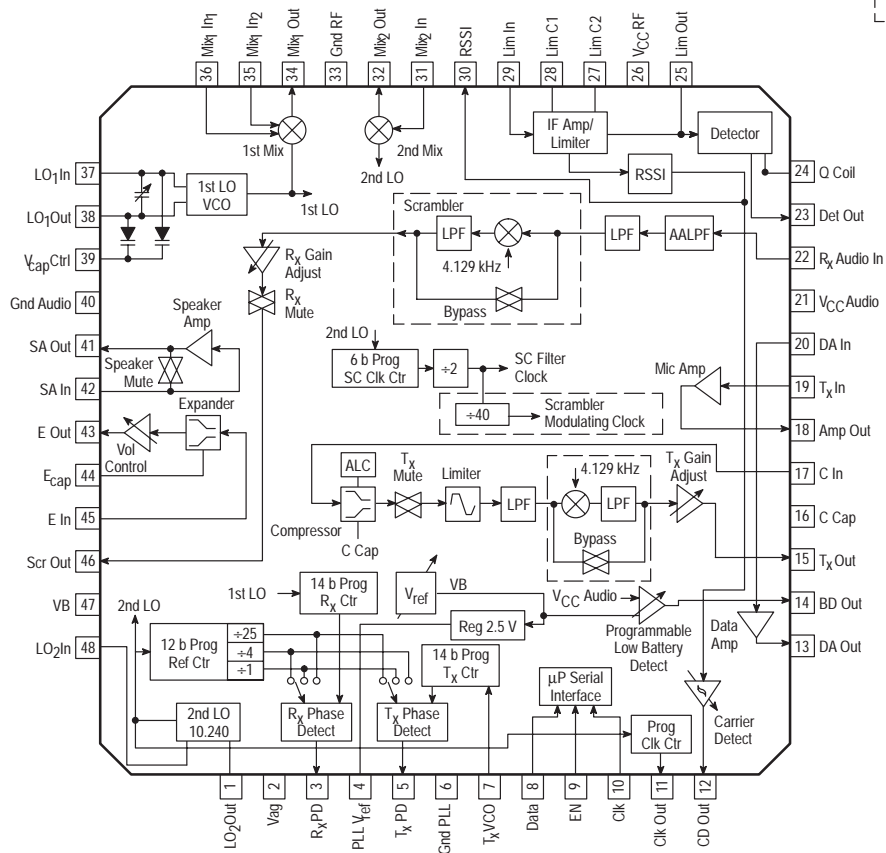
MC13110A MC13111A

PIN CONNECTIONS

QFP-52



LQFP-48



NOTE:

□ = MC13110A Only

MC13110A MC13111A

MAXIMUM RATINGS

Characteristic	Symbol	Value	Unit
Power Supply Voltage	V_{CC}	-0.5 to 6.0	Vdc
Junction Temperature	T_J	-65 to 150	°C
Maximum Power Dissipation, $T_A = 25^\circ\text{C}$	P_D	70	mW

- NOTES:**
1. Maximum Ratings are those values beyond which damage to the device may occur.
 2. Functional operation should be restricted to the limits in the Recommended Operating Conditions and Electrical Characteristics tables or Pin Descriptions section.
 3. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Voltage	V_{CC}	2.7	3.6	5.5	Vdc
Operating Ambient Temperature	T_A	-40	-	85	°C
Input Voltage Low (Data, Clk, EN)	V_{IL}	-	-	0.3	V
Input Voltage High (Data, Clk, EN)	V_{IH}	PLL $V_{ref} - 0.3$	-	-	V
Bandgap Reference Voltage	V_B	-	1.5	-	V

NOTE: 4. All limits are not necessarily functional concurrently.

DC ELECTRICAL CHARACTERISTICS ($V_{CC} = 3.6\text{ V}$, $T_A = 25^\circ\text{C}$, unless otherwise specified, $IP3 = 0$; Test Circuit Figure 1.)

Characteristic	Symbol	Figure	Min	Typ	Max	Unit
Static Current		1				
Active Mode	$ACT I_{CC}$		5.5	8.5	10.5	mA
Receive Mode	$R_x I_{CC}$		3.1	4.1	5.3	mA
Standby Mode	$STD I_{CC}$		-	465	560	μA
Inactive Mode	$INACT I_{CC}$		-	15	30	μA
Current Increase When $IP3 = 1$ (Active and Receive Modes)	I_{IP3}	1	-	1.4	1.8	mA

MC13110A MC13111A

ELECTRICAL CHARACTERISTICS ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or R_X Mode, unless otherwise specified;
Test Circuit Figure 1.)

Characteristic	Figure	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
FM RECEIVER ($f_{RF} = 46.77\text{ MHz}$ [USA Ch 21], $f_{dev} = \pm 3.0\text{ kHz}$, $f_{mod} = 1.0\text{ kHz}$, $V_{cap\ ctrl} = 1.2\text{ V}$)								
Input Sensitivity (for 12 dB SINAD at Det Out Using C–Message Weighting Filter) 50 Ω Termination, Generator Referred Single–Ended, Matched Input, Generator Referred Differential, Matched Input, Generator Referred	68, 69	Mix ₁ In ₁ /In ₂	Det Out	V_{SIN}	–	2.2	–	μVrms dBm
					–	–100	–	
					–	0.4	–	
–	–	–	–	–	0.4	–	–	–
First and Second Mixer Voltage Gain Total ($V_{in} = 1.0\text{ mVrms}$, with CF ₁ and CF ₂ Load)	1	Mix ₁ In ₁ or In ₂	Mix ₂ Out	MX _{gainT}	24	29	–	dB
Isolation of First Mixer Output and Second Mixer Input ($V_{in} = 1.0\text{ mVrms}$, with CFI Removed)	–	Mix ₁ In ₁ or In ₂	Mix ₂ In	Mix–Iso	–	60	–	dB
Total Harmonic Distortion ($V_{in} = 3.16\text{ mVrms}$)	1	Mix ₁ In ₁ or In ₂	Det Out	THD	–	1.4	2.0	%
Recovered Audio ($V_{in} = 3.16\text{ mVrms}$)	1	Mix ₁ In ₁ or In ₂	Det Out	AFO	80	112	150	mVrms
AM Rejection Ratio ($V_{in} = 3.16\text{ mVrms}$, 30% AM, @ 1.0 kHz)	1	Mix ₁ In ₁ or In ₂	Det Out	AMR	30	48	–	dB
Signal to Noise Ratio ($V_{in} = 3.16\text{ mVrms}$, No Modulation)	–	Mix ₁ In ₁ or In ₂	Det Out	SNR	–	48	–	dB

FIRST MIXER (No Modulation, $f_{in} = \text{USA Ch21}$, 46.77 MHz, 50 Ω Termination at Inputs)

Input Impedance Single–Ended	16	–	Mix ₁ In ₁ or In ₂	RPS ₁	–	1.6	–	k Ω pF
				CPS ₁	–	3.7	–	
Differential	16	–	Mix ₁ In ₁ /In ₂	RPD ₁	–	1.6	–	k Ω pF
				CPD ₁	–	1.8	–	
Output Impedance	14	–	Mix ₁ Out	RP ₁ Out	–	300	–	Ω
				CP ₁ Out	–	3.7	–	pF
Voltage Conversion Gain ($V_{in} = 1.0\text{ mVrms}$, with CF ₁ Filter as Load)	17, 18	Mix ₁ In ₁ or In ₂	Mix ₁ Out	MX _{gain1}	–	12	–	dB
1.0 dB Voltage Compression Level (Input Referred) IP3 Bit Set to 0	19, 21	Mix ₁ In ₁ or In ₂	Mix ₁ Out	V_O Mix ₁ 1 dB	–	20	–	mVrms dBm
					–	–21	–	
IP3 Bit Set to 1	20, 21				–	56	–	
					–	–12	–	
Third Order Intercept (Input Referred) [Note 5] IP3 Bit Set to 0	19, 21	Mix ₁ In ₁ or In ₂	Mix ₁ Out	TOI _{mix1}	–	64	–	mVrms dBm
					–	–11	–	
IP3 Bit Set to 1	20, 21				–	178	–	
					–	–2.0	–	
–3.0 dB IF Bandwidth	22	Mix ₁ In ₁ or In ₂	Mix ₁ Out	Mix ₁ BW	–	13	–	MHz

NOTE: 5. Third order intercept calculated for input levels 10 dB below 1.0 dB compression point.

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ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or R_X Mode, unless otherwise specified; Test Circuit Figure 1.)

Characteristic	Figure	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
SECOND MIXER (No Modulation, $f_{in} = 10.7\text{ MHz}$, $50\ \Omega$ Termination at Inputs)								
Input Impedance	24	Mix ₂ In	Mix ₂ In	R _{P2} In C _{P2} In	– –	2.8 3.6	– –	k Ω pF
Output Impedance	24	–	Mix ₂ Out	R _{P2} Out C _{P2} Out	– –	1.5 6.1	– –	k Ω pF
Voltage Conversion Gain ($V_{in} = 1.0\text{ mV}_{rms}$, with CF ₂ Filter as Load)	26, 27	Mix ₂ In	Mix ₂ Out	MX _{gain2}	–	20	–	dB
1.0 dB Voltage Compression Level (Input Referred) IP3 Bit Set 0	28, 30	Mix ₂ In	Mix ₂ Out	V _O Mix ₂ 1 dB	–	32	–	mV _{rms} dBm
					–	–17	–	
IP3 Bit Set 1	29, 30				–	45	–	
					–	–14	–	
Third Order Intercept (Input Referred) [Note 6] IP3 Bit Set 0	28, 30	Mix ₂ In	Mix ₂ Out	TOI _{mix2}	–	136	–	mV _{rms} dBm
					–	–4.3	–	
IP3 Bit Set 1	29, 30				–	158	–	
					–	–3.0	–	
–3.0 dB IF Bandwidth	31	Mix ₂ In	Mix ₂ Out	Mix ₂ BW	–	2.5	–	MHz
LIMITER/DEMULATOR ($f_{in} = 455\text{ kHz}$, $f_{dev} = \pm 3.0\text{ kHz}$, $f_{mod} = 1.0\text{ kHz}$)								
Input Impedance	49	Lim In	Lim In	R _{PLim} C _{PLim}	– –	1.5 16	– –	k Ω pF
Detector Output Impedance	–	–	Det Out	R _O	–	1.1	–	k Ω
IF –3.0 dB Limiting Sensitivity	1	Lim In	Det Out	IF Sens	–	71	100	μV_{rms}
Demodulator Bandwidth	–	Lim In	Det Out	BW	–	20	–	kHz
RSSI/CARRIER DETECT (No Modulation)								
RSSI Output Dynamic Range	56	Mix ₁ In	RSSI	RSSI	–	80	–	dB
DC Voltage Range	56	Mix ₁ In	RSSI	DC RSSI	–	0.2 to 1.5	–	V _{dc}
Carrier Detect Threshold CD Threshold Adjust = (10100) (Threshold Relative to Mix ₁ In Level)	57	Mix ₁ In	CD Out	V _T	–	15	–	μV_{rms}
Hysteresis, CD = (10100) (Threshold Relative to Mix ₁ In Level)	57	Mix ₁ In	CD Out	Hys	–	2.0	–	dB
Output High Voltage CD = (00000), RSSI = 0.2 V	1	RSSI	CD Out	V _{OH}	$V_{CC} - 0.1$	3.6	–	V
Output Low Voltage CD = (11111), RSSI = 0.9 V	1	RSSI	CD Out	V _{OL}	–	0.02	0.4	V
Carrier Detect Threshold Adjustment Range (Programmable through MPU Interface)	125	–	–	V _T Range	–	–20 to 11	–	dB
Carrier Detect Threshold – Number of Programmable Levels	125	–	–	V _{Tn}	–	32	–	–

NOTE: 6. Third order intercept calculated for input levels 10 dB below 1.0 dB compression point.

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ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or R_X Mode, unless otherwise specified; Test Circuit Figure 1.)

Characteristic	Figure	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
R_X AUDIO PATH ($f_{in} = 1.0\text{ kHz}$, Active Mode, scrambler bypassed)								
Absolute Gain ($V_{in} = -20\text{ dBV}$)	1, 72	R_X Audio In	SA Out	G	-4.0	0	4.0	dB
Gain Tracking (Referenced to E Out for $V_{in} = -20\text{ dBV}$) $V_{in} = -30\text{ dBV}$ $V_{in} = -40\text{ dBV}$	1, 76	E In	E Out	G_t	-21 -42	-20 -40	-19 -38	dB
Total Harmonic Distortion ($V_{in} = -20\text{ dBV}$)	1, 76	R_X Audio In	SA Out	THD	-	0.7	1.0	%
Maximum Input Voltage ($V_{CC} = 2.7\text{ V}$)	76	R_X Audio In	-	-	-	-11.5	-	dBV
Maximum Output Voltage (Increase input voltage until output voltage THD = 5.0%, then measure output voltage)	1	E In	E Out	V_{Omax}	-2.0	0	-	dBV
Input Impedance	-	R_X Audio In E In	-	Z_{in}	- -	600 7.5	- -	k Ω
Attack Time $E_{cap} = 0.5\text{ }\mu\text{F}$, $R_{filt} = 40\text{ k}$ (See Appendix B)	-	E In	E Out	t_a	-	3.0	-	ms
Release Time $E_{cap} = 0.5\text{ }\mu\text{F}$, $R_{filt} = 40\text{ k}$ (See Appendix B)	-	E In	E Out	t_r	-	13.5	-	ms
Compressor to Expander Crosstalk $V_{in} = -10\text{ dBV}$, $V(E\text{ In}) = \text{AC Gnd}$	1	C In	E Out	C_T	-	-90	-70	dB
R_X Muting (Δ Gain) $V_{in} = -20\text{ dBV}$, R_X Gain Adj = (01111)	1	R_X Audio In	E Out	M_e	-	-84	-60	dB
R_X High Frequency Corner R_X Path, $V_{R_X\text{ Audio In}} = -20\text{ dBV}$	1	R_X Audio In	Scr Out	$R_X f_{ch}$	3.779	3.879	3.979	kHz
Low Pass Filter Passband Ripple ($V_{in} = -20\text{ dBV}$)	1, 73	R_X Audio In	Scr Out	Ripple	-	0.4	0.6	dB
R_X Gain Adjust Range (Programmable through MPU Interface)	124	R_X Audio In	Scr Out	R_X Range	-	-9.0 to 10	-	dB
R_X Gain Adjust Steps – Number of Programmable Levels	124	R_X Audio In	Scr Out	$R_X n$	-	20	-	dB
Audio Path Noise, C–Message Weighting (Input AC–Grounded)	70	R_X Audio In	Scr Out E Out SA Out	EN	- - -	-85 <-95 <-95	- - -	dBV
Volume Control Adjust Range	122	E In	E Out	$V_{ctrlRange}$	-	-14 to 16	-	dB
Volume Control – Number of Programmable Levels	122	E In	E Out	V_{cn}	-	16	-	-
SPEAKER AMP/SP MUTE (Active Mode)								
Maximum Output Swing $R_L = \text{No Load}$, $V_{in} = 3.4\text{ Vpp}$ $R_L = 130\text{ }\Omega$, $V_{in} = 2.8\text{ Vpp}$ $R_L = 620\text{ }\Omega$, $V_{in} = 4.0\text{ Vpp}$	1, 79	SA In	SA Out	V_{Omax}	2.8 2.0 -	3.2 2.6 3.4	- - -	Vpp
Speaker Amp Muting $V_{in} = -20\text{ dBV}$, $R_L = 130\text{ }\Omega$	1	SA In	SA Out	M_{sp}	-	-92	-60	dB

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ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or R_X Mode, unless otherwise specified; Test Circuit Figure 1.)

Characteristic	Figure	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
DATA AMP COMPARATOR								
Hysteresis	1	DA In	DA Out	Hys	30	42	50	mV
Threshold Voltage	–	DA In	DA Out	V_T	–	$V_{CC} - 0.7$	–	V
Input Impedance	1	–	DA In	Z_I	200	250	280	k Ω
Output Impedance	–	–	DA Out	Z_O	–	100	–	k Ω
Output High Voltage $V_{in} = V_{CC} - 1.0\text{ V}$, $I_{OH} = 0\text{ mA}$	1	DA In	DA Out	V_{OH}	$V_{CC} - 0.1$	3.6	–	V
Output Low Voltage $V_{in} = V_{CC} - 0.4\text{ V}$, $I_{OL} = 0\text{ mA}$	1	DA In	DA Out	V_{OL}	–	0.1	0.4	V
Maximum Frequency	–	DA In	DA Out	F_{max}	–	10	–	kHz
MIC AMP ($f_{in} = 1.0\text{ kHz}$, External resistors set to gain of 1, Active Mode)								
Open Loop Gain	–	T_X In	Amp Out	AVOL	–	100,000	–	V/V
Gain Bandwidth	–	T_X In	Amp Out	GBW	–	100	–	kHz
Maximum Output Swing ($R_L = 10\text{ k}\Omega$)	–	T_X In	Amp Out	V_{Omax}	–	3.2	–	V _{pp}
T_X AUDIO PATH ($f_{in} = 1.0\text{ kHz}$, T_X Gain Adj = (01111); ALC, Limiter, and Mutes Disabled; Active Mode, scrambler bypassed)								
Absolute Gain ($V_{in} = -10\text{ dBV}$)	1, 83	T_X In	T_X Out	G	-4.0	0	4.0	dB
Gain Tracking (Referenced to T_X Out for $V_{in} = -10\text{ dBV}$) $V_{in} = -30\text{ dBV}$ $V_{in} = -40\text{ dBV}$	1, 87	T_X In	T_X Out	G_t	-11 -17	-10 -15	-9.0 -13	dB
Total Harmonic Distortion ($V_{in} = -10\text{ dBV}$)	1, 87	T_X In	T_X Out	THD	–	0.8	1.8	%
Maximum Output Voltage (Increase input voltage until output voltage THD = 5.0%, then measure output voltage. T_X Gain Adjust = 8 dB)	1	T_X In	T_X Out	V_{Omax}	-2.0	0	–	dBV
Input Impedance	–	–	C In	Z_{in}	–	10	–	k Ω
Attack Time ($C_{cap} = 0.5\text{ }\mu\text{F}$, $R_{filt} = 40\text{ k}$ (See Appendix B))	–	C In	T_X Out	t_a	–	3.0	–	ms
Release Time ($C_{cap} = 0.5\text{ }\mu\text{F}$, $R_{filt} = 40\text{ k}$ (See Appendix B))	–	C In	T_X Out	t_r	–	13.5	–	ms
Expander to Compressor Crosstalk ($V_{in} = -20\text{ dBV}$, Speaker Amp No Load, $V(C\text{ In}) = AC\text{ Gnd}$)	1	E In	T_X Out	C_T	–	-60	-40	dB
T_X Muting ($V_{in} = -10\text{ dBV}$)	1	T_X In	T_X Out	M_C	–	-88	-60	dB
ALC Output Level (ALC enabled) $V_{in} = -10\text{ dBV}$ $V_{in} = -2.5\text{ dBV}$	1, 87, 90	T_X In	T_X Out	ALC _{out}	-15 -13	-13 -11	-8.0 -6.0	dBV
ALC Slope (ALC enabled) $V_{in} = -10\text{ dBV}$ $V_{in} = -2.5\text{ dBV}$	1	T_X In	T_X Out	Slope	0.1	0.25	0.4	dB/dB
ALC Input Dynamic Range	–	C In	T_X Out	DR	–	-16 to -2.5	–	dBV
Limiter Output Level ($V_{in} = -2.5\text{ dBV}$, Limiter enabled)	1	T_X In	T_X Out	V_{lim}	-10	-8.0	–	dBV
T_X High Frequency Corner [Note 7] ($V_{T_X\text{ In}} = -10\text{ dBV}$, Mic Amp = Unity Gain)	1	T_X In	T_X Out	$T_X\text{ }f_c$	3.6	3.7	3.8	kHz

NOTE: 7. The filter specification is based on a 10.24 MHz 2nd LO, and a switched-capacitor (SC) filter counter divider ratio of 31. If other 2nd LO frequencies and/or SC filter counter divider ratios are used, the filter corner frequency will be proportional to the resulting SC filter clock frequency.

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ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or R_X Mode, unless otherwise specified; Test Circuit Figure 1.)

Characteristic	Figure	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
T_X AUDIO PATH ($f_{in} = 1.0\text{ kHz}$, T_X Gain Adj = (01111); ALC, Limiter, and Mutes Disabled; Active Mode, scrambler bypassed)								
Low Pass Filter Passband Ripple ($V_{in} = -10\text{ dBV}$)	1, 84	T_X In	T_X Out	Ripple	–	0.7	1.2	dB
Maximum Compressor Gain ($V_{in} = -70\text{ dBV}$)	–	C In	T_X Out	AV_{max}	–	23	–	dB
T_X Gain Adjust Range (Programmable through MPU Interface)	124	C In	T_X Out	T_X Range	–	–9.0 to 10	–	dB
T_X Gain Adjust Steps – Number of Programmable Levels	124	C In	T_X Out	T_X n	–	20	–	–

R_X AND T_X SCRAMBLER (2nd LO = 10.24 MHz, T_X Gain Adj = (01111), R_X Gain Adj = (01111), Volume Control = (0 dB Default Levels), SCF Clock Divider = 31. Total is divide by 62 for SCF clock frequency of 165.16 kHz)

R_X High Frequency Corner (Note 8) R_X Path, $f = 479\text{ Hz}$, V_{R_X} Audio In = -20 dBV	–	R_X Audio In	Scr Out	R_X f_{ch}	3.55	3.65	3.75	kHz
T_X High Frequency Corner (Note 8) T_X Path, $f = 300\text{ Hz}$, V_{T_X} In = -10 dBV , Mic Amp = Unity Gain	–	T_X In	T_X Out	T_X f_{ch}	3.829	3.879	3.929	kHz
Absolute Gain R_X : $V_{in} = -20\text{ dBV}$ T_X : $V_{in} = -10\text{ dBV}$, Limiter disabled	– –	R_X Audio In T_X In	E Out T_X Out	AV	–4.0 –4.0	0.4 –1.0	4.0 4.0	dB
Pass Band Ripple $R_X + T_X$ Path – $1.0\text{ }\mu\text{F}$ from T_X Out to R_X Audio In, f_{in} = low corner frequency to high corner frequency	–	C In	E Out	Ripple	–	1.9	2.5	dB
Scrambler Modulation Frequency R_X : 100 mV (-20 dBV) T_X : 316 mV (-10 dBV)	– –	R_X Audio In C In	E Out T_X Out	f_{mod}	4.119	4.129	4.139	kHz
Group Delay $R_X + T_X$ Path – $1.0\text{ }\mu\text{F}$ from T_X Out to R_X Audio In, $f_{in} = 1.0\text{ kHz}$ f_{in} = low corner frequency to high corner frequency	– –	C In C In	E Out E Out	GD GD	– –	1.0 4.0	– –	ms
Carrier Breakthrough $R_X + T_X$ Path – $1.0\text{ }\mu\text{F}$ from T_X Out to R_X Audio In	–	C In	E Out	CBT	–	–60	–	dB
Baseband Breakthrough $R_X + T_X$ Path – $1.0\text{ }\mu\text{F}$ from T_X Out to R_X Audio In, $f_{in} = 1.0\text{ kHz}$, $f_{meas} = 3.192\text{ kHz}$	–	C In	E Out	BBT	–	–50	–	dB

LOW BATTERY DETECT

Average Threshold Voltage Before Electronic Adjustment ($V_{ref_Adj} = (0111)$)	1, 130	Ref ₁ Ref ₂	BD ₁ Out BD ₂ Out	VT_i	1.38	1.48	1.58	V
Average Threshold Voltage After Electronic Adjustment ($V_{ref_Adj} = (\text{adjusted value})$)	1	Ref ₁ Ref ₂	BD ₁ Out BD ₂ Out	VT_f	1.475	1.5	1.525	V
Hysteresis	–	Ref ₁ Ref ₂	BD ₁ Out BD ₂ Out	Hys	–	4.0	–	mV
Input Current ($V_{in} = 1.0$ and 2.0 V)	1	–	Ref ₁ Ref ₂	I_{in}	–50	–	50	nA
Output High Voltage ($V_{in} = 2.0\text{ V}$)	1	Ref ₁ Ref ₂	BD ₁ Out BD ₂ Out	V_{OH}	$V_{CC} - 0.1$	3.6	–	V

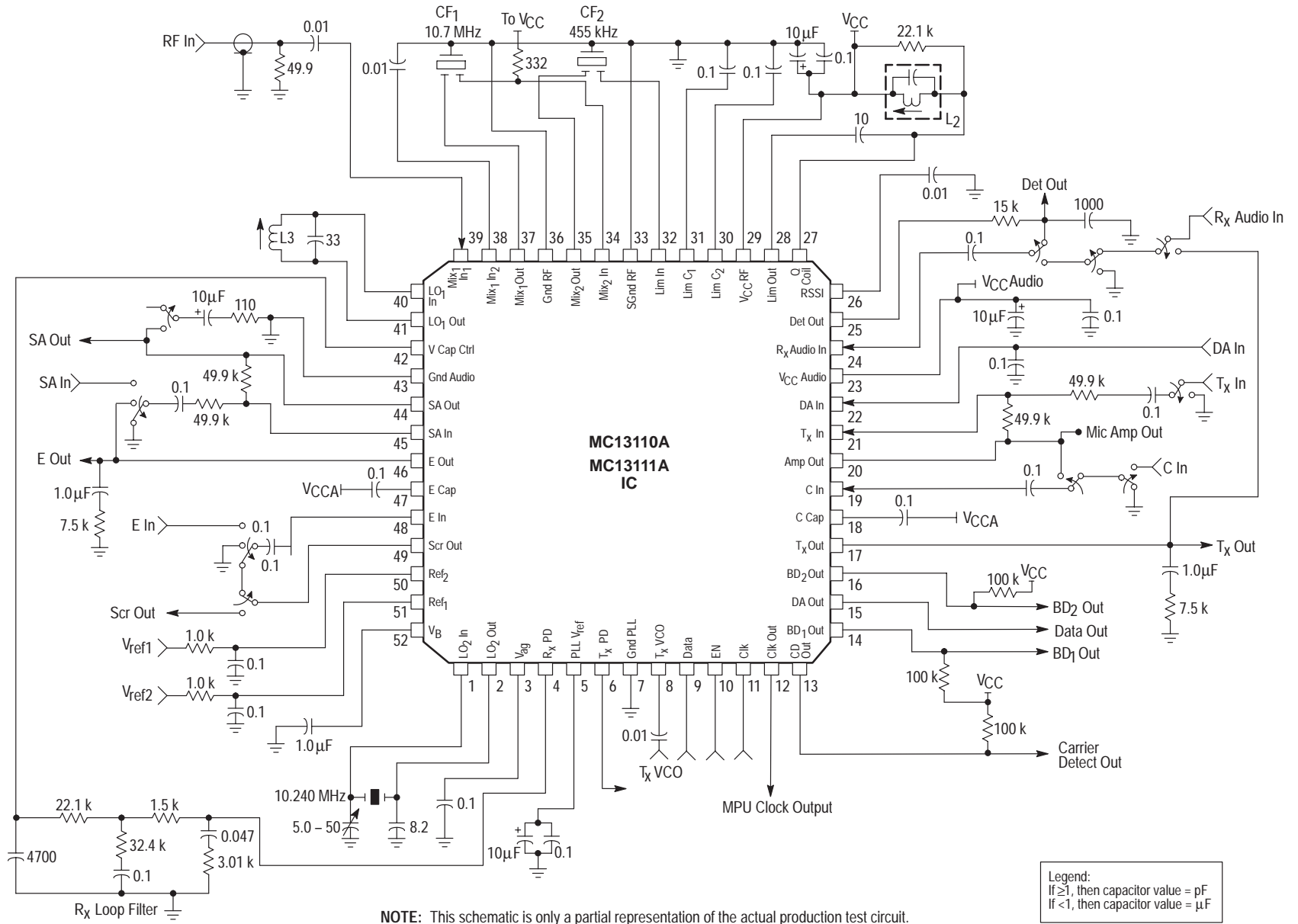
NOTE: 8. The filter specification is based on a 10.24 MHz 2nd LO, and a switch-capacitor (SC) filter counter divider ratio of 31. If other 2nd LO frequencies and/or SC filter counter divider ratios are used, the filter corner frequency will be proportional to the resulting SC filter clock frequency.

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ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or R_X Mode, unless otherwise specified; Test Circuit Figure 1.)

Characteristic	Figure	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
LOW BATTERY DETECT								
Output Low Voltage ($V_{in} = 1.0\text{ V}$)	1	Ref ₁ Ref ₂	BD ₁ Out BD ₂ Out	V_{OL}	–	0.2	0.4	V
BATTERY DETECT INTERNAL THRESHOLD								
After Electronic Adjustment of V_B Voltage BD Select = (111) BD Select = (110) BD Select = (101) BD Select = (100) BD Select = (011) BD Select = (010) BD Select = (001)	1, 127	V_{CC} Audio	BD ₂ Out	IBS ₇ IBS ₆ IBS ₅ IBS ₄ IBS ₃ IBS ₂ IBS ₁	3.381 3.298 3.217 3.134 2.970 2.886 2.802	3.455 3.370 3.287 3.202 3.034 2.948 2.862	3.529 3.442 3.357 3.270 3.098 3.010 2.922	V
PLL PHASE DETECTOR								
Output Source Current ($V_{PD} = \text{Gnd} + 0.5\text{ V}$ to PLL $V_{ref} - 0.5\text{ V}$)	–	–	R_X PD T_X PD	I_{OH}	–	1.0	–	mA
Output Sink Current ($V_{PD} = \text{Gnd} + 0.5\text{ V}$ to PLL $V_{ref} - 0.5\text{ V}$)	–	–	R_X PD T_X PD	I_{OL}	–	1.0	–	mA
PLL LOOP CHARACTERISTICS								
Maximum 2nd LO Frequency (No Crystal)	–	LO ₂ In	–	f_{2ext}	–	12	–	MHz
Maximum 2nd LO Frequency (With Crystal)	–	–	LO ₂ In LO ₂ Out	f_{2ext}	–	12	–	MHz
Maximum T_X VCO (Input Frequency), $V_{in} = 200\text{ mVpp}$	–	–	T_X VCO	f_{txmax}	–	80	–	MHz
PLL VOLTAGE REGULATOR								
Regulated Output Level ($I_L = 0\text{ mA}$, after V_{ref} Adjustment)	1	–	PLL V_{ref}	V_O	2.4	2.5	2.6	V
Line Regulation ($I_L = 0\text{ mA}$, $V_{CC} = 3.0$ to 5.5 V)	1	V_{CC} Audio	PLL V_{ref}	$V_{RegLine}$	–	11.8	40	mV
Load Regulation ($I_L = 1.0\text{ mA}$)	1	V_{CC} Audio	PLL V_{ref}	$V_{RegLoad}$	–20	–1.4	–	mV
MICROPROCESSOR SERIAL INTERFACE								
Input Current Low ($V_{in} = 0.3\text{ V}$, Standby Mode)	1	–	Data, Clk, EN	I_{IL}	–5.0	0.4	–	μA
Input Current High ($V_{in} = 3.3\text{ V}$, Standby Mode)	1	–	Data, Clk, EN	I_{IH}	–	1.6	5.0	μA
Hysteresis Voltage	–	–	Data, Clk, EN	V_{hys}	–	1.0	–	V
Maximum Clock Frequency	–	Data, EN, Clk	–	–	–	2.0	–	MHz
Input Capacitance	–	Data, Clk, EN	–	C_{in}	–	8.0	–	pF
EN to Clk Setup Time	106	–	EN, Clk	t_{suEC}	–	200	–	ns
Data to Clk Setup Time	105	–	Data, Clk	t_{suDC}	–	100	–	ns
Hold Time	105	–	Data, Clk	t_h	–	90	–	ns
Recovery Time	106	–	EN, Clk	t_{rec}	–	90	–	ns
Input Pulse Width	–	–	EN, Clk	t_w	–	100	–	ns
MPU Interface Power-Up Delay (90% of PLL V_{ref} to Data, Clk, EN)	108	–	–	t_{puMPU}	–	100	–	μs

Figure 1. Production Test Circuit (52 Pin QFP)



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PIN FUNCTION DESCRIPTION

Pin		Symbol/ Type	Equivalent Internal Circuit (52 Pin QFP)	Description
LQFP-48	QFP-52			
48 1	1 2	LO ₂ In LO ₂ Out		<p>These pins form the PLL reference oscillator when connected to an external parallel-resonant crystal (10.24 MHz typical). The reference oscillator is also the second Local Oscillator (LO₂) for the RF receiver. "LO₂ In" may also serve as an input for an externally generated reference signal which is typically ac-coupled.</p> <p>When the IC is set to the inactive mode, LO₂ In is internally pulled low to disable the oscillator. The input capacitance to ground at each pin (LO₂ In/ LO₂ Out) is 3.0 pF.</p>
2	3	V _{ag}		V _{ag} is the internal reference voltage for the switched capacitor filter section. This pin must be decoupled with a 0.1 μF capacitor.
3	4	R _X PD (Output)		<p>This pin is a tri-state voltage output of the R_X and T_X Phase Detector. It is either "high", "low", or "high impedance," depending on the phase difference of the phase detector input signals. During lock, very narrow pulses with a frequency equal to the reference frequency are present. This pin drives the external R_X and T_X PLL loop filters. R_X and T_X PD outputs can sink or source 1.0 mA.</p>
5	6	T _X PD (Output)		
4	5	PLL V _{ref}		<p>PLL V_{ref} is a PLL voltage regulator output pin. An internal voltage regulator provides a stable power supply voltage for the R_X and T_X PLL's and can also be used as a regulated supply voltage for other IC's. It can source up to 1.0 mA externally. Proper supply filtering is a must on this pin. PLL V_{ref} is pulled up to V_{CC} audio for the standby and inactive modes (Note 1).</p>
6	7	Gnd PLL		Ground pin for digital PLL section of IC.
7	8	T _X VCO (Input)		<p>T_X VCO is the transmit divide counter input which is driven by an ac-coupled external transmit loop VCO. The minimum signal level is 200 mVpp @ 60.0 MHz. This pin also functions as the test mode input for the counter tests.</p>

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PIN FUNCTION DESCRIPTION (continued)

Pin		Symbol/ Type	Equivalent Internal Circuit (52 Pin QFP)	Description
LQFP-48	QFP-52			
8 9 10	9 10 11	Data EN Clk (Input)		Microprocessor serial interface input pins are for programming various counters and control functions. The switching thresholds are referenced to PLL V_{ref} and Gnd PLL. The inputs operate up to V_{CC} . These pins have $1.0 \mu\text{A}$ internal pull-down currents.
11	12	Clk Out (Output)		The microprocessor clock output is derived from the 2nd LO crystal oscillator and a programmable divider with divide ratios of 2 to 312.5. It can be used to drive a microprocessor and thereby reduce the number of crystals required in the system design. The driver has an internal resistor in series with the output which can be combined with an external capacitor to form a low pass filter to reduce radiated noise on the PCB. This output also functions as the output for the counter test modes. The Clk Out can be disabled via the MPU interface.
12	13	CD Out (I/O)		Dual function pin; 1) Carrier detect output (open collector with external $100 \text{ k}\Omega$ pull-up resistor. 2) Hardware interrupt input which can be used to "wake-up" from the Inactive Mode.
-	14	BD ₁ Out		Low battery detect output #1 is an open collector with external pull-up resistor.
14	16	BD ₂ Out (Output)		Low battery detect output #2 is an open collector with external pull-up resistor.
13	15	DA Out (Output)		Data amplifier output (open collector with internal $100 \text{ k}\Omega$ pull-up resistor).
15	17	T _x Out (Output)		T _x Out is the T _x path audio output. Internally this pin has a low-pass filter circuitry with -3 dB bandwidth of 4.0 kHz. T _x gain and mute are programmable through the MPU interface. This pin is sensitive to load capacitance.

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PIN FUNCTION DESCRIPTION (continued)

Pin		Symbol/ Type	Equivalent Internal Circuit (52 Pin QFP)	Description
LQFP-48	QFP-52			
16	18	C Cap		C Cap is the compressor rectifier filter capacitor pin. It is recommended that an external filter capacitor to V_{CC} audio be used. A practical capacitor range is 0.1 to 1.0 μF . 0.47 μF is the recommended value.
17	19	C In (Input)		C In is the compressor input. This pin is internally biased and has an input impedance of 12.5 k. C In must be ac-coupled.
18	20	Amp Out (Output)		Microphone amplifier output. The gain is set with external resistors. The feedback resistor should be less than 200 k Ω .
19	21	T _x In (Input)		T _x In is the T _x path input to the microphone amplifier (Mic Amp). An external resistor is connected to this pin to set the Mic Amp gain and input impedance. T _x In must be ac-coupled, too.
20	22	DA In (Input)		The data amplifier input (DA In) resistance is 250 k Ω and must be ac-coupled. Hysteresis is internally provided.
21	23	V _{CC} Audio		V _{CC} audio is the supply for the audio section. It is necessary to adequately filter this pin.
22	24	R _x Audio In (Input)		The R _x audio input resistance is 600 k Ω and must be ac-coupled.
23	25	Det Out (Output)		Det Out is the audio output from the FM detector. This pin is dc-coupled from the FM detector and has an output impedance of 1100 Ω .

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PIN FUNCTION DESCRIPTION (continued)

Pin		Symbol/ Type	Equivalent Internal Circuit (52 Pin QFP)	Description
LQFP-48	QFP-52			
30	26	RSSI		RSSI is the receive signal strength indicator. This pin must be filtered through a capacitor to ground. The capacitance value range should be 0.01 to 0.1 μ F. This is also the input to the Carrier Detect comparator. An external R to ground shifts the RSSI voltage.
24	27	Q Coil		A quad coil or ceramic discriminator connects this pin as part of the FM demodulator circuit. DC-couple this pin to V_{CC} RF through the quad coil or the external resistor.
26	29	V_{CC} RF		V_{CC} supply for RF receiver section (1st LO, mixer, limiter, demodulator). Proper supply filtering is needed on this pin too.
25	28	Lim Out		A quad coil or ceramic discriminator are connected to these pins as part of the FM demodulator circuit. A coupling capacitor connects this pin to the quad coil or ceramic discriminator as part of the FM demodulator circuit. This pin can drive coupling capacitors up to 47 pF with no deterioration in performance.
27 28	30 31	Lim C ₂ Lim C ₁		IF amplifier/limiter capacitor pins. These decoupling capacitors should be 0.1 μ F. They determine the IF limiter gain and low frequency bandwidth.
29	32	Lim In (Input)		Signal input for IF amplifier/limiter. Signals should be ac-coupled to this pin. The input impedance is 1.5 k Ω at 455 kHz.
-	33	SGnd RF		This pin is not connected internally but should be grounded to reduce potential coupling between pins.
31	34	Mix ₂ In (Input)		Mix ₂ In is the second mixer input. Signals are to be ac-coupled to this pin, which is biased internally to V_{CC} RF. The input impedance is 2.8 k Ω at 455 kHz. The input impedance can be reduced by connecting an external resistor to V_{CC} RF.

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PIN FUNCTION DESCRIPTION (continued)

Pin		Symbol/ Type	Equivalent Internal Circuit (52 Pin QFP)	Description
LQFP-48	QFP-52			
32	35	Mix ₂ Out (Output)		Mix ₂ Out is the second mixer output. The second mixer has a 3 dB bandwidth of 2.5 MHz and an output impedance of 1.5 kΩ. The output current drive is 50 μA.
33	36	Gnd RF		Ground pin for RF section of the IC.
34	37	Mix ₁ Out (Output)		The first mixer has a 3 dB IF bandwidth of 13 MHz and an output impedance of 300 Ω. The output current drive is 300 μA and can be programmed for 1.0 mA.
35	38	Mix ₁ In ₂ (Input)		Signals should be ac-coupled to this pin, which is biased internally to V _{CC} - 1.6 V. The single-ended and differential input impedance are about 1.6 and 1.8 kΩ at 46 MHz, respectively.
36	39	Mix ₁ In ₁ (Input)		
37 38	40 41	LO ₁ In LO ₁ Out		Tank Elements, an internal varactor and capacitor matrix for 1st LO multivibrator oscillator are connected to these pins. The oscillator is useable up to 80 MHz.
39	42	V _{cap} Ctrl		
40	43	Gnd Audio		Ground for audio section of the IC.
41	44	SA Out (Output)		The speaker amplifier gain is set with an external feedback resistor. It should be less than 200 kΩ. The speaker amplifier can be muted through the MPU interface.
42	45	SA In (Input)		

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PIN FUNCTION DESCRIPTION (continued)

Pin		Symbol/ Type	Equivalent Internal Circuit (52 Pin QFP)	Description
LQFP-48	QFP-52			
43	46	E Out (Output)		The output level of the expander output is determined by the volume control. Volume control is programmable through the MPU interface.
44	47	E Cap		E Cap is the expander rectifier filter capacitor pin. Connect an external filter capacitor between V _{CC} audio and E Cap. The recommended capacitance range is 0.1 to 1.0 μF. 0.47 μF is the suggested value.
45	48	E In (Input)		The expander input pin is internally biased and has input impedance of 30 kΩ.
46	49	Scr Out (Output)		Scr Out is the R _x audio output. An internal low pass filter has a -3 dB bandwidth of 4.0 kHz.
-	50	Ref ₂		Reference voltage input for Low Battery Detect #2.
-	51	Ref ₁		Reference voltage input for Low Battery Detect #1.
47	52	V _B		V _B is the internal half supply analog ground reference. This pin must be filtered with a capacitor to ground. A typical capacitor range of 0.5 to 10 μF is desired to reduce crosstalk and noise. It is important to keep this capacitor value equal to the PLL V _{ref} capacitor due to logic timing (Note 9).

NOTE: 9. A capacitor range of 0.5 to 10 μF is recommended. The capacitor value should be the same used on the V_B pin (Pin 52). An additional high quality parallel capacitor of 0.01 μF is essential to filter out spikes originating from the PLL logic circuitry.

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DEVICE DESCRIPTION AND APPLICATION INFORMATION

The following text, graphics, tables and schematics are provided to the user as a source of valuable technical information about the Universal Cordless Telephone IC. This information originates from thorough evaluation of the device performance for the US and French applications. This data was obtained by using units from typical wafer lots. It is important to note that the forgoing data and information was from a limited number of units. By no means is the user to assume that the data following is a guaranteed parametric. Only the minimum and maximum limits identified in the electrical characteristics tables found earlier in this spec are guaranteed.

General Circuit Description

The MC13110A and MC13111A are a low power dual conversion narrowband FM receiver designed for applications up to 80 MHz carrier frequency. This device is primarily designated to be used for the 49 MHz cordless phone (CT-0), but has other applications such as low data rate narrowband data links and as a backend device for 900 MHz systems where baseband analog processing is required. This device contains a first and second mixer, limiter, demodulator, extended range receive signal strength (RSSI), receive and transmit baseband processing, dual programmable PLL, low battery detect, and serial interface for microprocessor control. The FM receiver can also be used with either a quadrature coil or ceramic resonator. Refer to the Pin Function Description table for the simplified internal circuit schematic and description of this device.

DC Current and Battery Detect

Figures 3 through 6 are the current consumption for Inactive, Standby, Receive, and Active modes versus supply voltages. Figures 7 and 8 show the typical behavior of current consumption in relation to temperature. The relationship of additional current draw due to IP3 bit set to <1> and supply voltage are shown in Figures 9 and 10.

For the Low Battery Detect, the user has the option to operate the IC in the programmable or non-programmable modes. Note that the 48 pin package can only be used in the programmable mode. Figure 127 describes this operation (refer to the Serial Interface section under Clock Divider Register).

In the programmable mode several different internal threshold levels are available (Figure 2). The bits are set through the SCF Clock Divider Register as shown in Figures 108 and 125. The reference for the internal divider network is V_{CC} Audio. The voltages on the internal divider network are compared to the Internal Reference Voltage, VB, generated by an internal source. Since the internal comparator used is non-inverting, a high at V_{CC} Audio will yield a high at the

battery detect output, and vice versa for V_{CC} Audio set to a low level. For the 52 pin package option, the Ref 1 and Ref 2 pins need to be tied to V_{CC} when used in the programmable mode. It is essential to keep the external reference pins above Gnd to prevent any possible power-on reset to be activated.

When considering the non-programmable mode (bits set to <000>) for the 52 pin package, the Ref 1 and Ref 2 pins become the comparators reference. An internal switch is activated when the non-programmable mode is chosen connecting Ref 1 and Ref 2. Here, two external precision resistor dividers are used to set independent thresholds for two battery detect hysteresis comparators. The voltages on Ref 1 and Ref 2 are again compared to the internally generated 1.5 V reference voltage (VB).

The Low Battery Detect threshold tolerance can be improved by adjusting a trim-pot in the external resistor divider (user designed). The initial tolerance of the internal reference voltage (VB) is $\pm 6.0\%$. Alternately, the tolerance of the internal reference voltage can be improved to $\pm 1.5\%$ through MPU serial interface programming (refer to the Serial Interface section, Figure 130). The internal reference can be measured directly at the "VB" pin. During final test of the telephone, the VB internal reference voltage is measured. Then, the internal reference voltage value is adjusted electronically through the MPU serial interface to achieve the desired accuracy level. The voltage reference register value should be stored in ROM during final test so that it can be reloaded each time the combo IC is powered up. The Low Battery Detect outputs are open collector. The battery detect levels will depend on the accuracy of the VB voltage. Figure 12 indicates that the VB voltage is fairly flat over temperature.

Figure 2. Internal Low Battery Detect Levels (with VB = 1.5 V)

Battery Detect Select	Ramping Up (V)	Ramping Down (V)	Average (V)	Hysteresis (mV)
0	–	–	–	–
1	2.867	2.861	2.864	4.0
2	2.953	2.947	2.950	6.0
3	3.039	3.031	3.035	8.0
4	3.207	3.199	3.204	8.0
5	3.291	3.285	3.288	6.0
6	3.375	3.367	3.371	8.0
7	3.461	3.453	3.457	8.0

NOTE: 10. Battery Detect Select 0 is the non-programmable operating mode.

DC CURRENT

Figure 3. Current versus Supply Voltage Inactive Mode

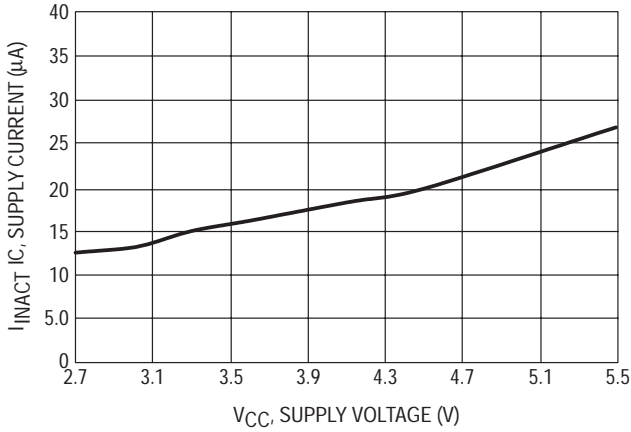


Figure 4. Current versus Supply Voltage Standby Mode, MCU Clock Output – On at 2.048 MHz

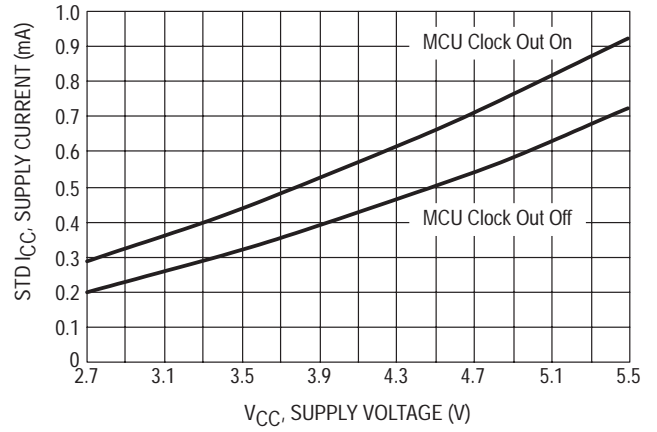


Figure 5. Current versus Supply Voltage Receive Mode

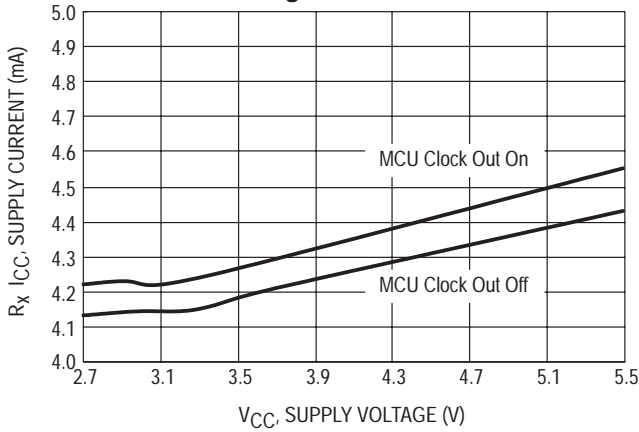


Figure 6. Current versus Supply Voltage Active Mode

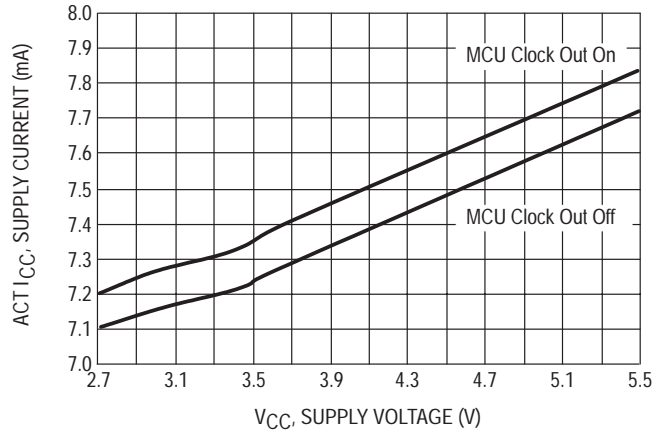


Figure 7. Current versus Temperature Normalized to 25°C

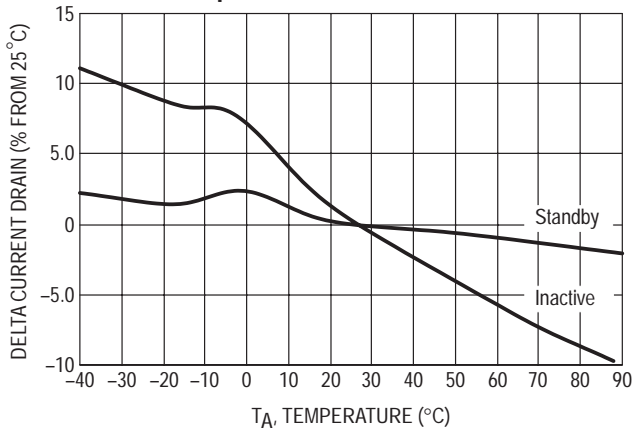
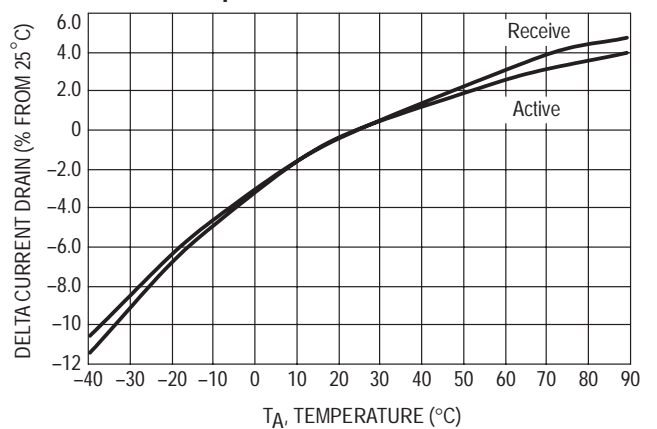


Figure 8. Current versus Temperature Normalized to 25°C



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DC CURRENT

Figure 9. Additional Supply Current Consumption versus Supply Voltage, IP3 = <1>

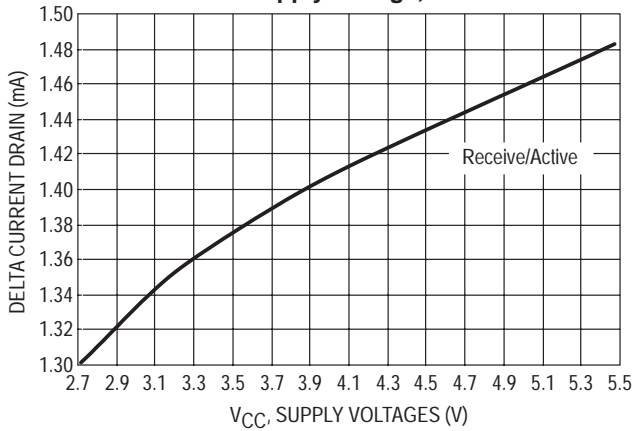


Figure 10. Additional IP3 Supply Current Consumption versus Temperature Normalized to 25°C

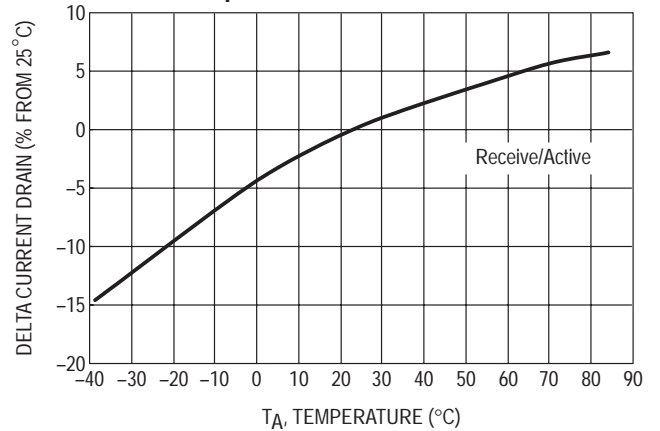


Figure 11. Current Standby Mode versus MCU Clock Output

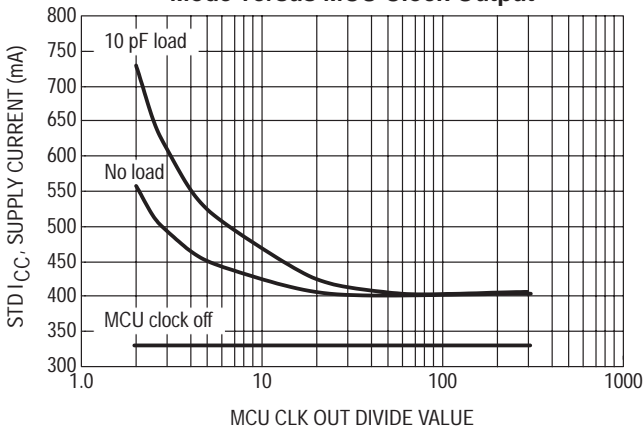
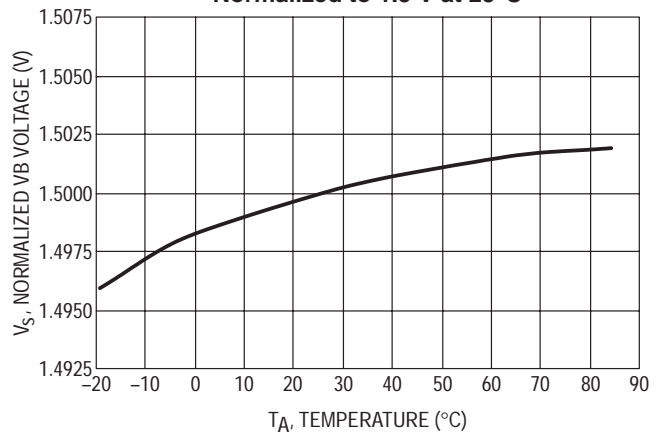


Figure 12. VB Voltage versus Temperature Normalized to 1.5 V at 25°C



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FIRST AND SECOND MIXER

Mixer Description

The 1st and 2nd mixers are similar in design. Both are double balanced to suppress the LO and the input frequencies to give only the sum and difference frequencies at the mixer output. Typically the LO is suppressed better than -50 dB for the first mixer and better than -40 dB for the second mixer. The gain of the 1st mixer has a -3.0 dB corner at approximately 13 MHz and is used at a 10.7 MHz IF. It has an output impedance of 300Ω and matches to a typical 10.7 MHz ceramic filter with a source and load impedance of 330Ω . A series resistor may be used to raise the impedance for use with crystal filters. They typically have an input impedance much greater than 330Ω .

First Mixer

Figures 17 through 20 show the first mixer transfer curves for the voltage conversion gain, output level, and intermodulation. Notice that there is approximately 10 dB linearity improvement when the "IP3 Increase" bit is set to $\langle 1 \rangle$. The "IP3 Increase" bit is a programmable bit as shown in the Serial Programmable Interface section under the R_X Counter Latch Register. The IP3 = $\langle 1 \rangle$ option will increase the supply current demand by 1.3 mA.

Figure 13. First Mixer Input and Output Impedance Schematic

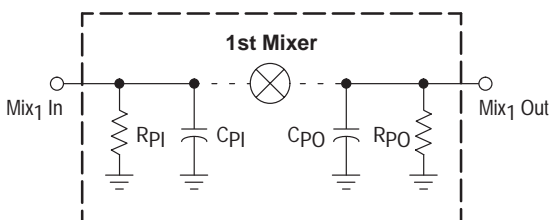


Figure 14. First Mixer Output Impedance

Unit	Output Impedance
B IP3 = $\langle 0 \rangle$ (Set Low)	$304 \Omega // 3.7 \text{ pF}$
B IP3 = $\langle 1 \rangle$ (Set High)	$300 \Omega // 4.0 \text{ pF}$

Figures 13, 14, and 16 represent the input and output impedance for the first mixer. Notice that the input single-ended and differential impedances are basically the same. The output impedance as described in Figure 14 will be used to match to a ceramic or crystal filter's input impedance. A typical ceramic filter input impedance is 330Ω while crystal filter input impedance is usually 1500Ω . Exact impedance matching to ceramic filters are not critical, however, more attention needs to be given to the filter characteristics of a crystal filter. Crystal filters are much narrower. It is important to accurately match to these filters to guaranty a reasonable response.

To find the IF bandwidth response of the first mixer refer to Figure 22. The -3.0 dB bandwidth point is approximately 13 MHz. Figure 15 is a summary of the first mixer feedthrough parameters.

Figure 15. First Mixer Feedthrough Parameters

Parameter	(dBm)
1st LO Feedthrough @ Mix ₁ In ₁	-70.0
1st LO Feedthrough @ Mix ₁ Out	-55.5
RF Feedthrough @ Mix ₁ Out with -30 dBm	-61.0

Figure 16. First Mixer Input Impedance over Input Frequency

Unit	US Center Channels		France Center Channels	
	49 MHz	46 MHz	41 MHz	26 MHz
Single-Ended	$1550 \Omega // 3.7 \text{ pF}$	$1560 \Omega // 3.7 \text{ pF}$	$1570 \Omega // 3.8 \text{ pF}$	$1650 \Omega // 3.7 \text{ pF}$
Differential	$1600 \Omega // 1.8 \text{ pF}$	$1610 \Omega // 1.8 \text{ pF}$	$1670 \Omega // 1.8 \text{ pF}$	$1710 \Omega // 1.8 \text{ pF}$

NOTE: 11. Single-Ended data is from measured results. Differential data is from simulated results.

FIRST MIXER

Figure 17. First Mixer Voltage Conversion Gain, IP3_bit = 0

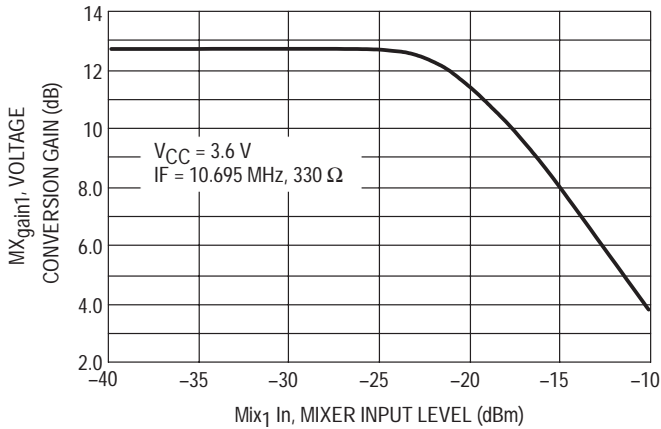


Figure 18. First Mixer Voltage Conversion Gain, IP3_bit = 1

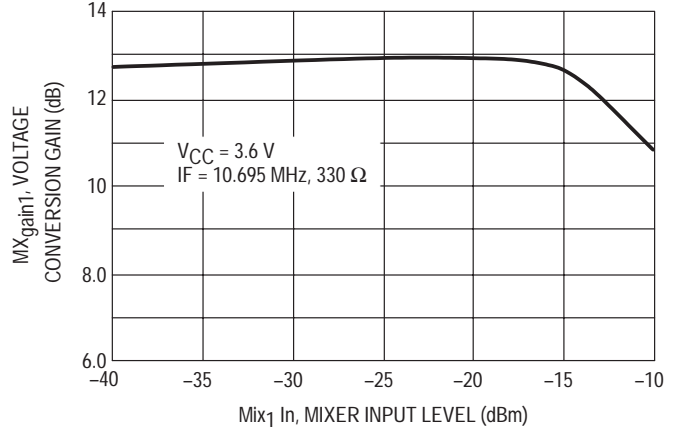


Figure 19. First Mixer Output Level and Intermodulation, IP3_bit = 0

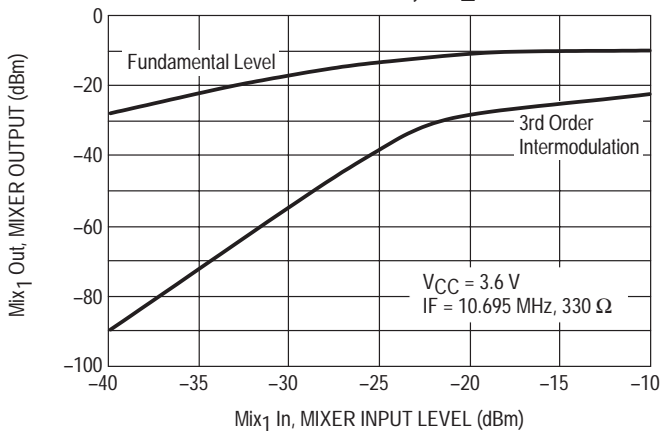


Figure 20. First Mixer Output Level and Intermodulation, IP3_bit = 1

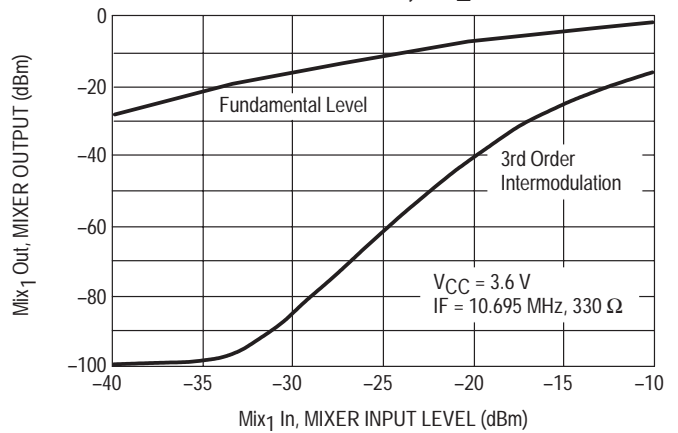


Figure 21. First Mixer Compression versus Supply Voltage

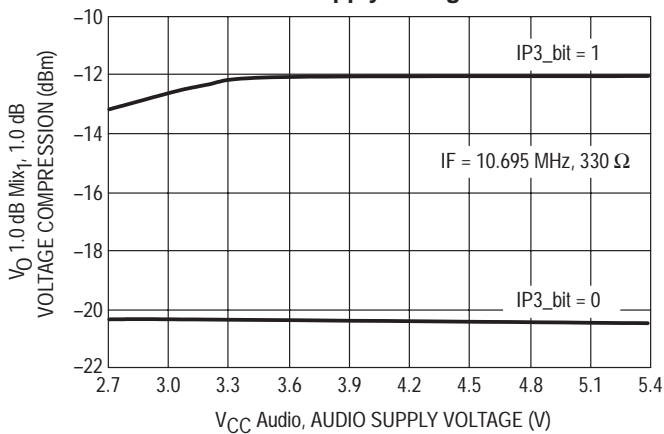
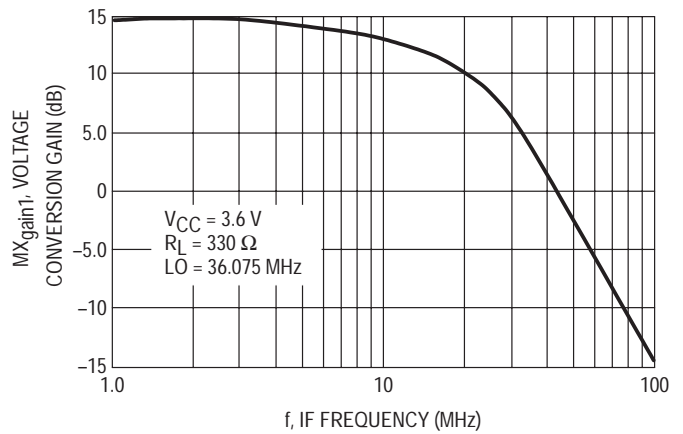


Figure 22. First IF Bandwidth



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Second Mixer

Figures 26 through 29 represents the second mixer transfer characteristics for the voltage conversion gain, output level, and intermodulation. There is a slight improvement in gain when the “IP3 bit” is set to <1> for the second mixer. (Note: This is the same programmable bit discussed earlier in the section.)

Figure 23. Second Mixer Input and Output Impedance Schematic

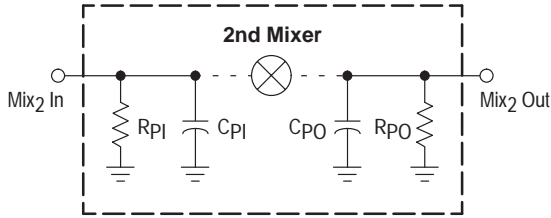


Figure 24. Second Mixer Input and Output Impedances

Unit	Input Impedance $R_{P1} // C_{P1}$	Output Impedance $R_{P0} // C_{P0}$
IP3 = <0> (Set Low)	2817 Ω // 3.6 pF	1493 Ω // 6.1 pF
IP3 = <1> (Set High)	2817 Ω // 3.6 pF	1435 Ω // 6.2 pF

The 2nd mixer input impedance is typically 2.8 k Ω . It requires an external 360 Ω parallel resistor for use with a standard 330 Ω , 10.7 MHz ceramic filter. The second mixer output impedance is 1.5 k Ω making it suitable to match standard 455 kHz ceramic filters.

The IF bandwidth response of the second mixer is shown in Figure 31. The -3.0 dB corner is 2.5 MHz. The feedthrough parameters are summarized in Figure 25.

Figure 25. Second Mixer Feedthrough Parameters

Parameter	(dBm)
2nd LO Feedthrough @ Mix ₂ Out	-42.9
IF Feedthrough @ Mix ₂ Out with -30 dBm	-61.7

SECOND MIXER

Figure 26. Second Mixer Conversion Gain, IP3_bit = 0

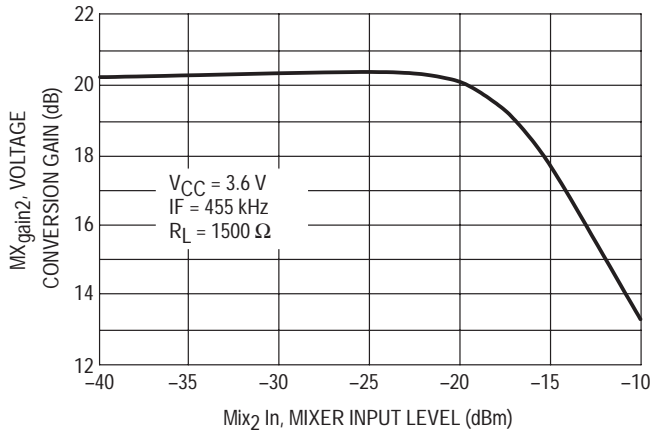


Figure 27. Second Mixer Conversion Gain, IP3_bit = 1

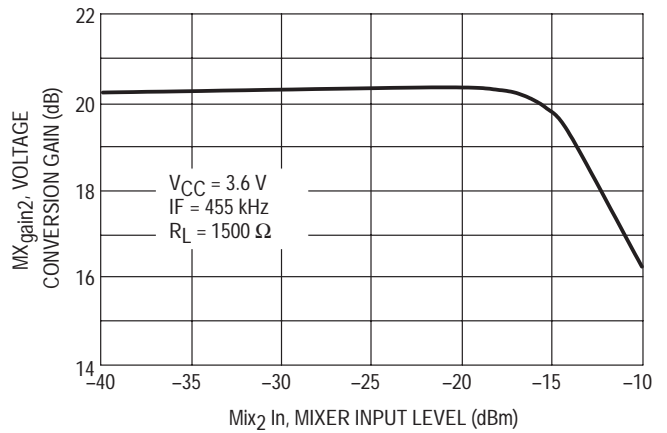


Figure 28. Second Mixer Output Level and Intermodulation, IP3_bit = 0

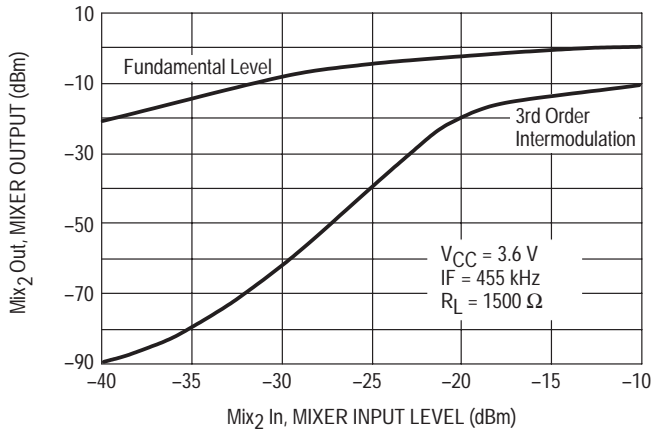


Figure 29. Second Mixer Output Level and Intermodulation, IP3_bit = 1

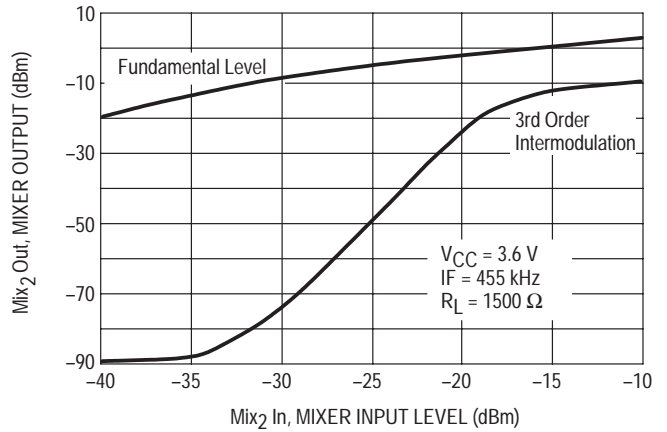


Figure 30. Second Mixer Compression versus Supply Voltage

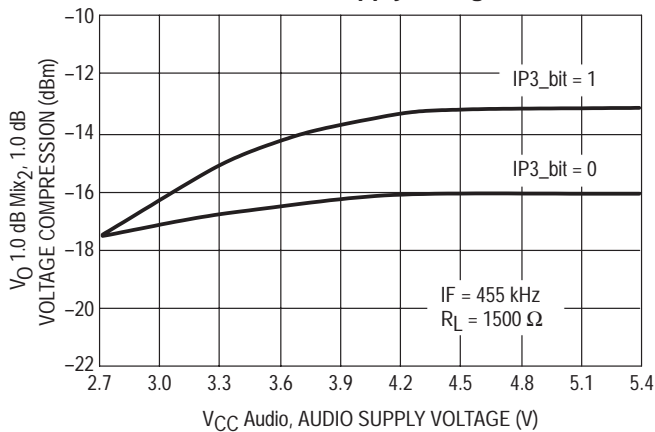
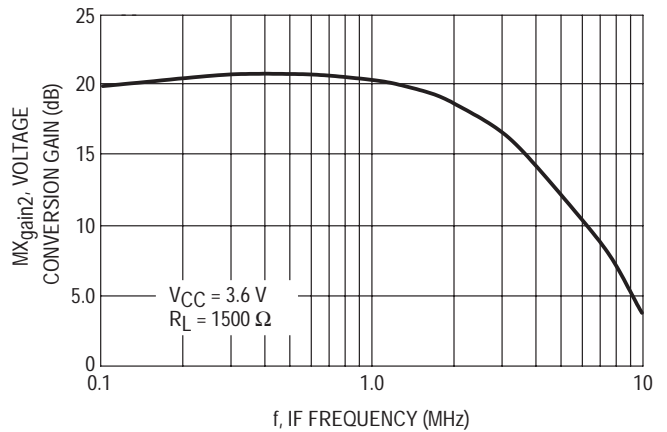


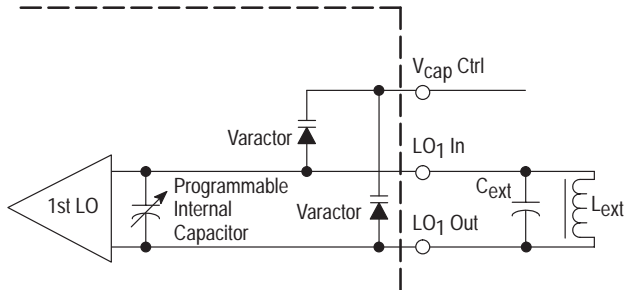
Figure 31. Second IF Bandwidth



First Local Oscillator

The 1st LO is a multi-vibrator oscillator. The tank circuit is composed of a parallel external capacitance and inductance, internal programmable capacitor matrix, and internal varactor. The local oscillator requires a voltage controlled input to the internal varactor and an external loop filter driven by on-board phase-lock control loop (PLL). The 1st LO internal component values have a tolerance of ±15%. A typical dc bias level on the LO Input and LO Output is 0.45 Vdc. The temperature coefficient of the varactor is +0.08%/°C. The curve in Figure 33 is the varactor control voltage range as it relates to varactor capacitance. It represents the expected internal capacitance for a given control voltage ($V_{capCtrl}$) of the MC13110A and MC13111A. Figure 32 shows a representative schematic of the first LO function.

Figure 32. First Local Oscillator Schematic



To select the proper L_{ext} and C_{ext} we can do the following analysis. From Figure 34 it is observed that an inductor will have a significant affect on first LO performance, especially over frequency. The overall minimum Q required for first LO to function as it relates to the LO frequency is also given in Figure 34.

Choose an inductor value, say 470 nH. From Figure 34, the minimum operating Q is approximately 25. From the following equation:

$$Q_{Coil} = R_p / X_{Coil}$$

where: R_p = parallel equivalent impedance (Figure 35).

C_{ext} can be determined as follows:

$$f_{LO} = \frac{1}{2\pi\sqrt{L_{ext}C_{ext}}}$$

where: L_{ext} = external inductance, C_{ext} = external capacitance.

Figure 34 clearly indicates that for lower coil values, higher quality factors (Q) are required for the first LO to function properly. Also, lower LO frequencies need higher Q's. In Figure 35 the internal programmable capacitor selection relative to the first LO frequency and the parallel impedance is shown. This information will help the user to decide what inductor (L_{ext}) to choose for best performance in terms of Q.

Refer to the Auxiliary Register in the Serial Interface Section for further discussion on LO programmability.

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FIRST LOCAL OSCILLATOR

Figure 33. First LO Varicap Capacitance versus Control Voltage

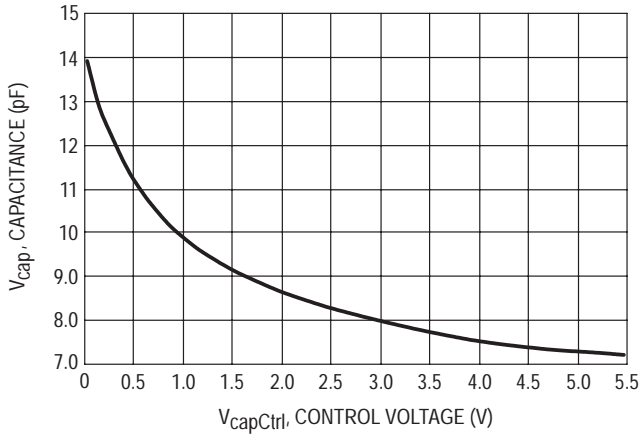


Figure 34. First LO Minimum Required Overall Q Value versus Inductor Value

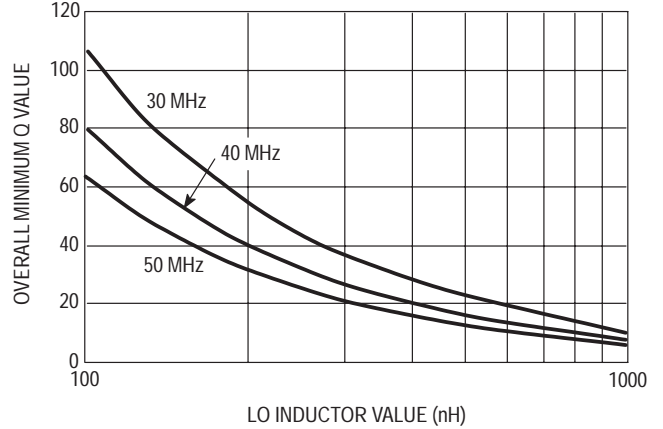


Figure 35. Representative Parallel Impedance versus Capacitor Select

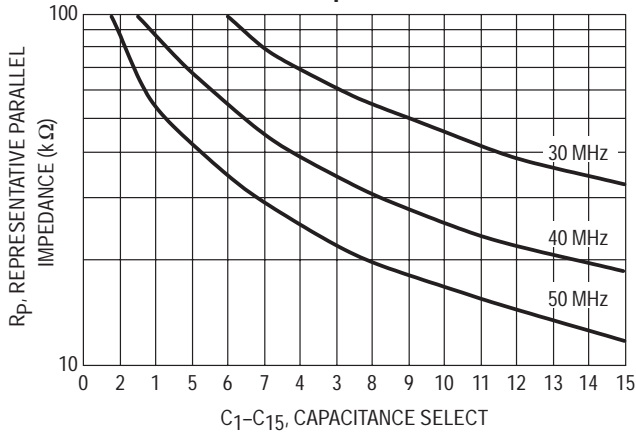


Figure 36. Varicap Value at V_{CV} = 1.0 V Over Temperature

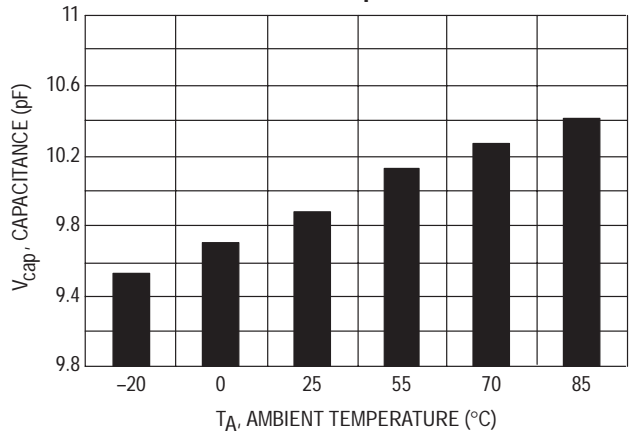


Figure 37. Control Voltage versus Channel Number, U.S. Handset Application

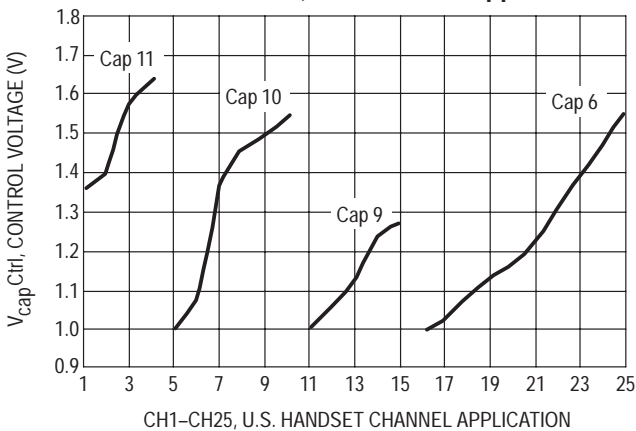
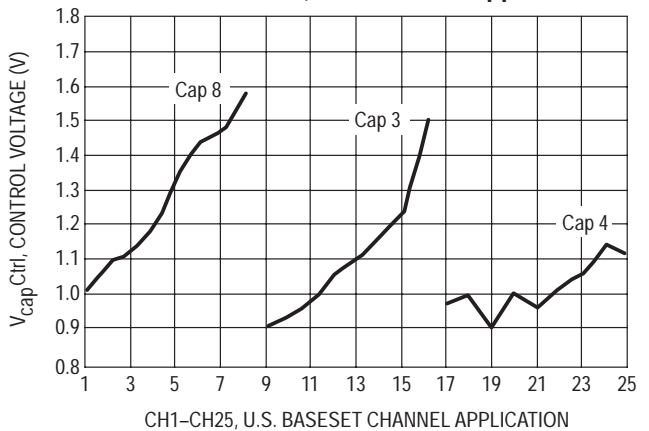


Figure 38. Control Voltage versus Channel Number, U.S. Baseband Application



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Second Local Oscillator

The 2nd LO is a CMOS oscillator. It is used as the PLL reference oscillator and local oscillator for the second frequency conversion in the RF receiver. It is designed to utilize an external parallel resonant crystal. See schematic in Figure 39.

Figure 39. Second Local Oscillator Schematic

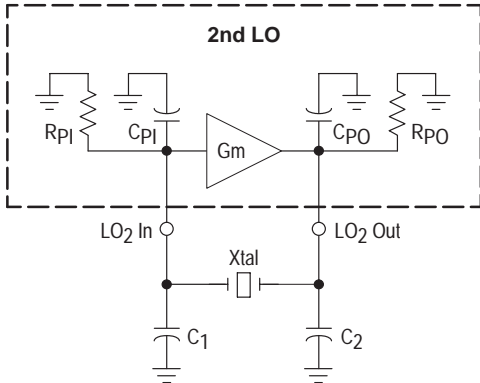


Figure 40. Second Local Oscillator Input and Output Impedance

Input Impedance ($R_{PI} // C_{PI}$)	11.6 k Ω // 2.9 pF
Output Impedance ($R_{PO} // C_{PO}$)	9.6 k Ω // 2.7 pF

Figure 41 shows a typical gain/phase response of the second local oscillator. Load capacitance (C_L), equivalent series resistance (ESR), and even supply voltage will have an effect on the 2nd LO response as shown in Figures 45 and 46. Except for the standby mode open loop gain is fairly constant as supply voltage increases from 2.5 V. This is due to the regulated voltage of 2.5 V on PLL V_{ref} . From the graphs it can be seen that optimum performance is achieved when $C1$ equals $C2$ ($C1/C2 = 1$).

Figure 46 represents the ESR versus crystal load capacitance for the 2nd LO. This relationship was defined by using a 6.0 dB minimum loop gain margin at 3.6 V. This is considered the minimum gain margin to guarantee oscillator start-up.

Oscillator start-up is also significantly affected by the crystal load capacitance selection. In Figures 42 and 43 the relationship between crystal load capacitance, supply voltage, and external load capacitance ratio ($C2/C1$), can be seen. The lower the load capacitance the better the performance.

Given the desired crystal load capacitance, $C1$ and $C2$ can be determined from Figure 47. It is also interesting to point out that current consumption increases when $C1 \neq C2$, as shown in Figure 44.

Be careful not to overdrive the crystal. This could cause a noise problem. An external series resistor on the crystal output can be added to reduce the drive level, if necessary.

SECOND LOCAL OSCILLATOR

Figure 41. Second LO Gain/Phase @ -10 dBm

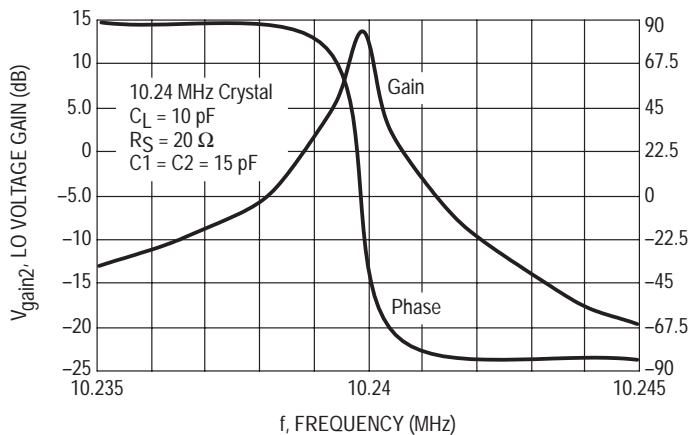
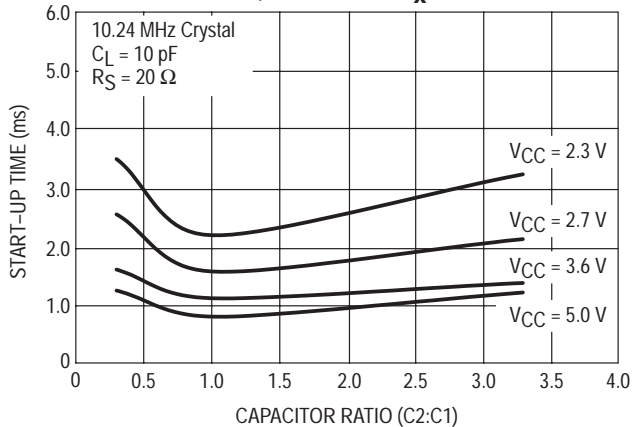


Figure 42. Start-Up Time versus Capacitor Ratio, Inactive to Rx Mode



SECOND LOCAL OSCILLATOR

Figure 43. Start-Up Time versus Capacitor Ratio, Inactive to Rx Mode

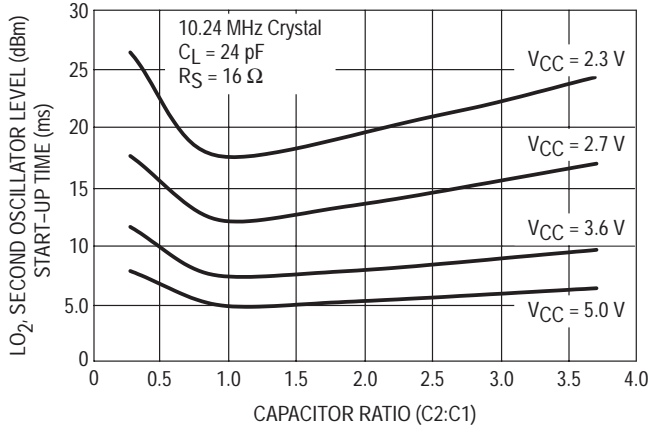


Figure 44. Second LO Current Consumption versus Capacitor Ratio

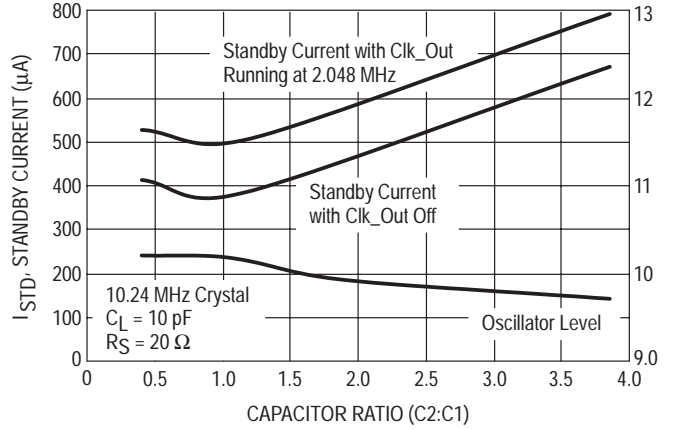


Figure 45. Maximum Open Loop Gain versus Capacitor Ratio

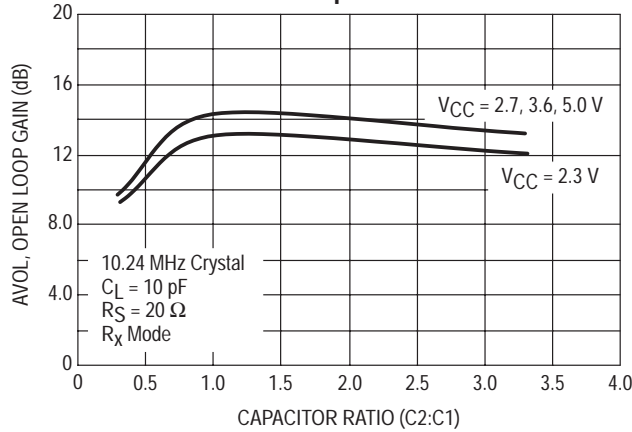


Figure 46. Maximum Allowable Equivalent Series Resistance (ESR) versus Crystal Load Capacitance

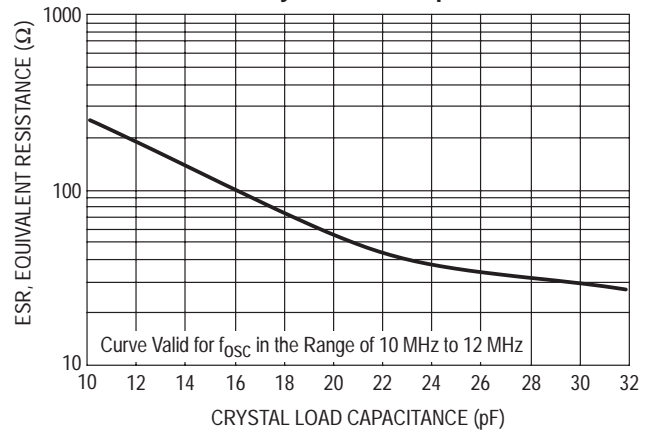
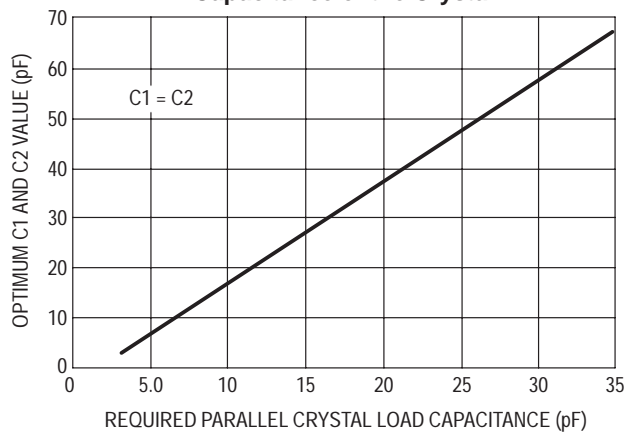


Figure 47. Optimum Value for C1 and C2 versus Equivalent Required Parallel Capacitance of the Crystal



IF Limiter and Demodulator

The limiting IF amplifier typically has about 110 dB of gain; the frequency response starts rolling off at 1.0 MHz. Decoupling capacitors should be placed close to Pins 31 and 32 to ensure low noise and stable operation. The IF input impedance is 1.5 kΩ. This is a suitable match to 455 kHz ceramic filters.

Figure 48. IF Limiter Schematic

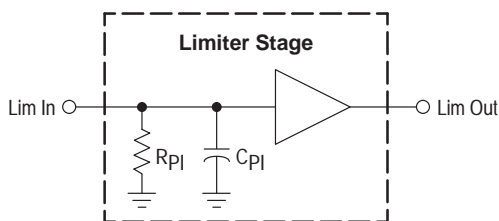
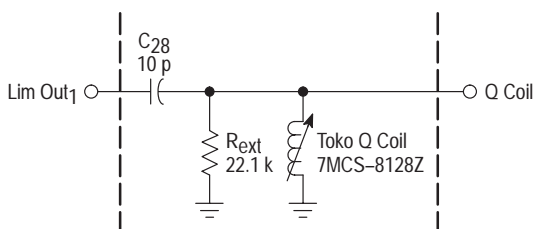


Figure 49. Limiter Input Impedance

Unit	Input Impedance (R _{PI})	Input Impedance (C _{PI})
Lim In	1538 Ω	15.7 pF

Figure 50. Quadrature Detector Demodulator Schematic



The quadrature detector is coupled to the IF with an external capacitor between Pins 27 and 28. Thus, the recovered signal level output is increased for a given bandwidth by increasing the capacitor. The external quadrature component may be either a LCR resonant circuit, which may be adjustable, or a ceramic resonator which is usually fixed tuned. (More on ceramic resonators later.)

The bandwidth performance of the detector is controlled by the loaded Q of the LC tank circuit (Figure 50). The following equation defines the components which set the detector circuit's bandwidth:

$$(1) R_T = Q X_L,$$

where R_T is the equivalent shunt resistance across the LC tank. X_L is the reactance of the quadrature inductor at the IF frequency ($X_L = 2\pi f L$).

The 455 kHz IF center frequency is calculated by:

$$(2) f_c = [2\pi (L C_p)^{1/2}]^{-1}$$

where L is the parallel tank inductor. C_p is the equivalent parallel capacitance of the parallel resonant tank circuit.

The following is a design example for a detector at 455 kHz and a specific loaded Q:

The loaded Q of the quadrature detector is chosen somewhat less than the Q of the IF bandpass for margin. For an IF frequency of 455 kHz and an IF bandpass of 20 kHz,

the IF bandpass Q is approximately 23; the loaded Q of the quadrature tank is chosen slightly lower at 15.

Example:

Let the total external C = 180 pF. (Note: the capacitance is the typical capacitance for the quad coil.) Since the external capacitance is much greater than the internal device and PCB parasitic capacitance, the parasitic capacitance may be neglected.

Rewrite equation (2) and solve for L:

$$L = (0.159)^2 / (C f_c^2)$$

$L = 678 \mu\text{H}$; Thus, a standard value is chosen:

$L = 680 \mu\text{H}$ (surface mount inductor)

The value of the total damping resistor to obtain the required loaded Q of 15 can be calculated from equation (1):

$$R_T = Q(2\pi f L)$$

$$R_T = 15(2\pi)(0.455)(680) = 29.5 \text{ k}\Omega$$

The internal resistance, R_{int} at the quadrature tank Pin 27 is approximately 100 kΩ and is considered in determining the external resistance, R_{ext} which is calculated from:

$$R_{ext} = ((R_T)(R_{int})) / (R_{int} - R_T)$$

$R_{ext} = 41.8 \text{ k}\Omega$; Thus, choose a standard value:

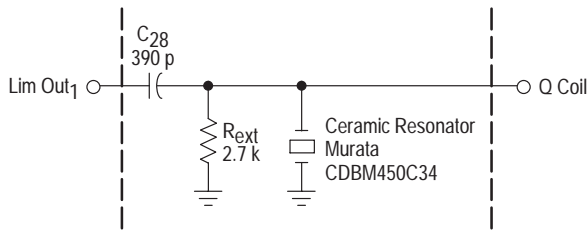
$R_{ext} = 39 \text{ k}\Omega$

In Figure 50, the R_{ext} is chosen to be 22.1 kΩ. An adjustable quadrature coil is selected. This tank circuit represents one popular network used to match to the 455 kHz carrier frequency. The output of the detector is represented as a "S-curve" as shown in Figure 52. The goal is to tune the inductor in the area that is most linear on the "S-curve" (minimum distortion) to optimize the performance in terms of dc output level. The slope of the curve can also be adjusted by choosing higher or lower values of R_{ext} . This will have an affect on the audio output level and bandwidth. As R_{ext} is increased the detector output slope will decrease. The maximum audio output swing and distortion will be reduced and the bandwidth increased. Of course, just the opposite is true for smaller R_{ext} .

A ceramic discriminator is recommended for the quadrature circuit in applications where fixed tuning is desired. The ceramic discriminator and a 5.6 kΩ resistor are placed from Pin 27 to V_{CC} . A 22 pF capacitor is placed from Pin 28 to 27 to properly drive the discriminator. MuRata Erie has designed a resonator for this part (CDBM455C48 for USA & A/P regions and CDBM450C48 for Europe). This resonator has been designed specifically for the MC13110/111 family. Figure 51 shows the schematic used to generate the "S-curve" and waveform shown in Figure 54 and 55.

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Figure 51. Ceramic Resonator Demodulator Schematic with Murata CDBM450C48



(CDBM455C48 US; CDBM450C48 France)

The “S-curve” for the ceramic discriminator shown in Figure 54 is centered around 450 kHz. It is for the French application. The same resonator is also used for the US application and is centered around 455 kHz. Clearly, the “S-curves” for the resonator and quad coil have very similar limiter outputs. As discussed previously, the slope of the “S-curve” centered around the center frequency can be controlled by the parallel resistor, R_{ext} . Distortion, bandwidth, and audio output level will be affected.

IF LIMITER AND DEMODULATION

Figure 52. S-Curve of Limiter Discriminator with Quadrature Coil

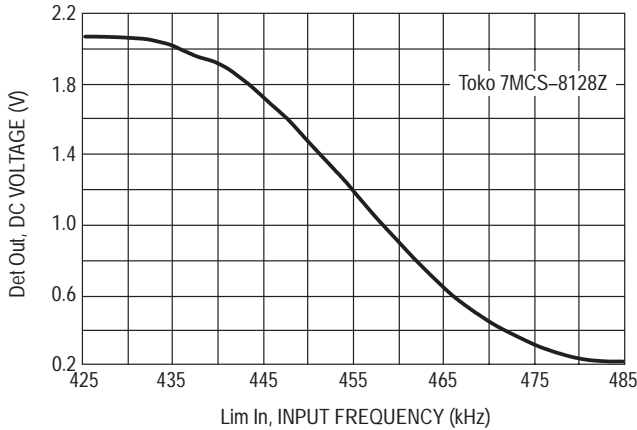


Figure 53. Typical Limiter Output Waveform with Quadrature Coil

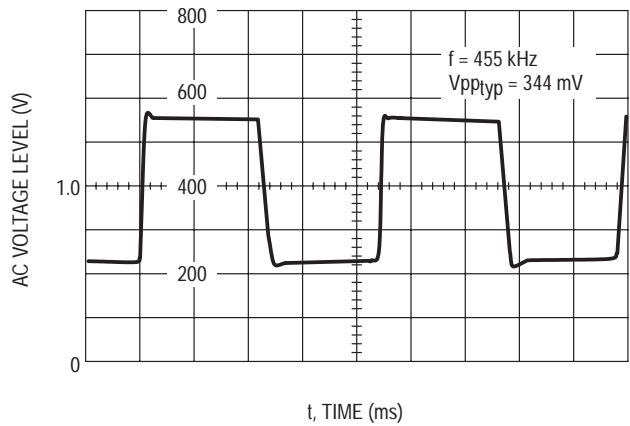


Figure 54. S-Curve of Limiter Discriminator with Ceramic Resonator

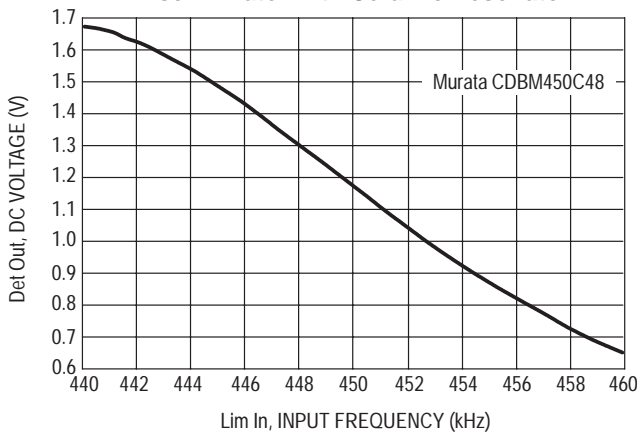
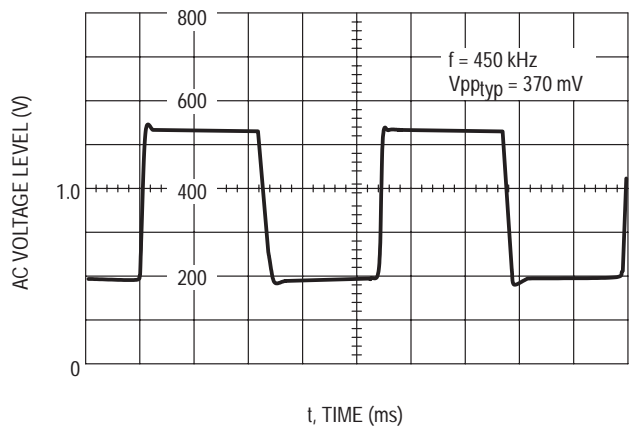


Figure 55. Typical Limiter Output Waveform with Ceramic Resonator



RSSI and Carrier Detect

The Received Signal Strength Indicator (RSSI) indicates the strength of the IF level. The output is proportional to the logarithm of the IF input signal magnitude. RSSI dynamic range is typically 80 dB. A 187 kΩ resistor to ground is provided internally to the IC. This internal resistor converts the RSSI current to a voltage level at the “RSSI” pin. To improve the RSSI accuracy over temperature an internal compensated reference is used. Figure 56 shows the RSSI versus RF input. The slope of the curve is 16.5 mV/dB.

The Carrier Detect Output (CD Out) is an open-collector transistor output. An external pull-up resistor of 100 kΩ will be required to bias this device. To form a carrier detect filter a capacitor needs to be connected from the RSSI pin to ground. The carrier detect threshold is programmable through the MPU interface (see “Carrier Detect Threshold Programming” in the serial interface section). The range can be scaled by connecting additional external resistance from

the RSSI pin to ground in parallel with the capacitor. From Figure 57, the affect of an external resistor at RSSI on the carrier detect level can be noticed. Since there is hysteresis in the carrier detect comparator, one trip level can be found when the input signal is increased while the another one can be found when the signal is decreased.

Figure 58 represents the RSSI ripple in relation to the RF input for different filtering capacitors at RSSI. Clearly, the higher the capacitor, the less the ripple. However, at low carrier detect thresholds, the ripple might supersede the hysteresis of the carrier detect. The carrier detect output may appear to be unstable. Using a large capacitor will help to stabilize the RSSI level, but RSSI charge time will be affected. Figure 59 shows this relationship.

The user must decide on a compromise between the RSSI ripple and RSSI start-up time. Choose a 0.01 μf capacitor as a starting point. For low carrier detect threshold settings, a 0.047 μf capacitor is recommended.

RSSI AND CARRIER DETECT

Figure 56. Typical RSSI Voltage Level versus RF Input

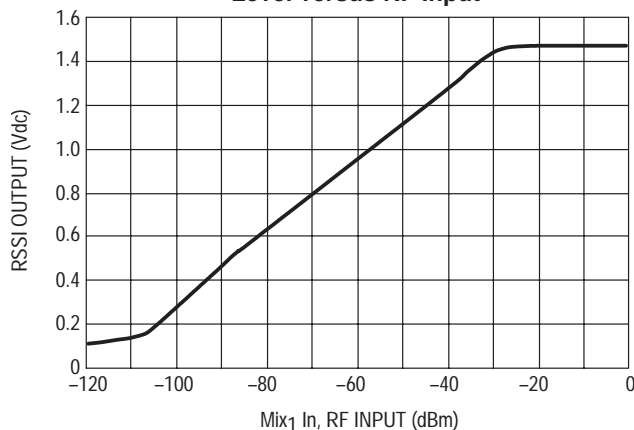


Figure 57. Carrier Detect Threshold versus External RSSI Resistor

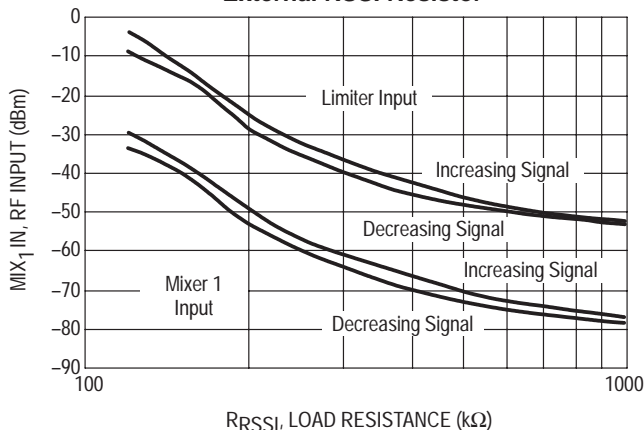


Figure 58. RSSI Ripple versus RF Input Level for Different RSSI Capacitors

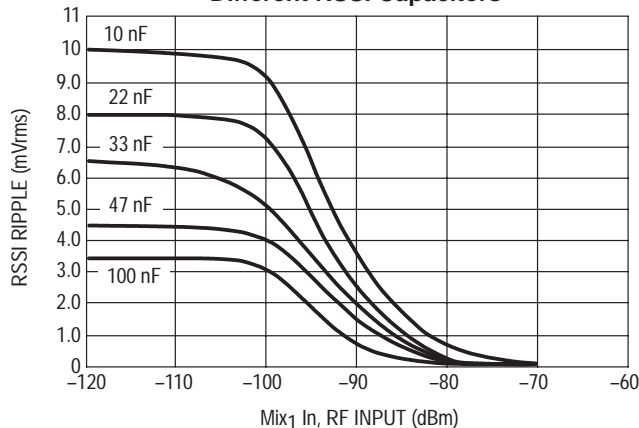
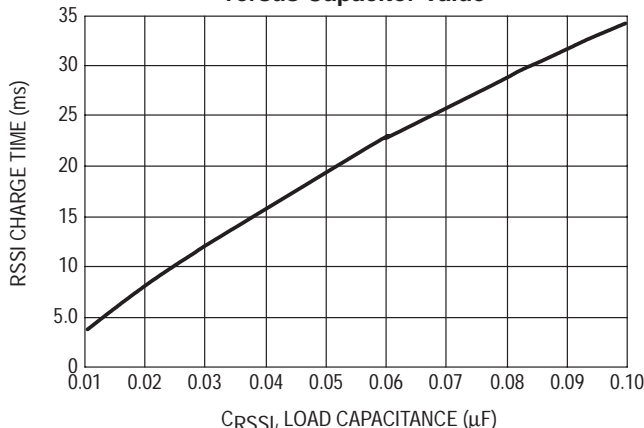


Figure 59. RSSI Charge Time versus Capacitor Value



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RF System Performance

The sensitivity of the IC is typically 0.4 μ Vrms matched (single ended or differential) with no preamp. To achieve suitable system performance, a preamp and passive duplexer may be used. In production final test, each section of the IC is separately tested to guarantee its system performance in the specific application. The preamp and duplexer (differential, matched input) yields typically -115 dBm @ 12 dB SINAD sensitivity performance under full duplex operation. See Figure 45 and 48.

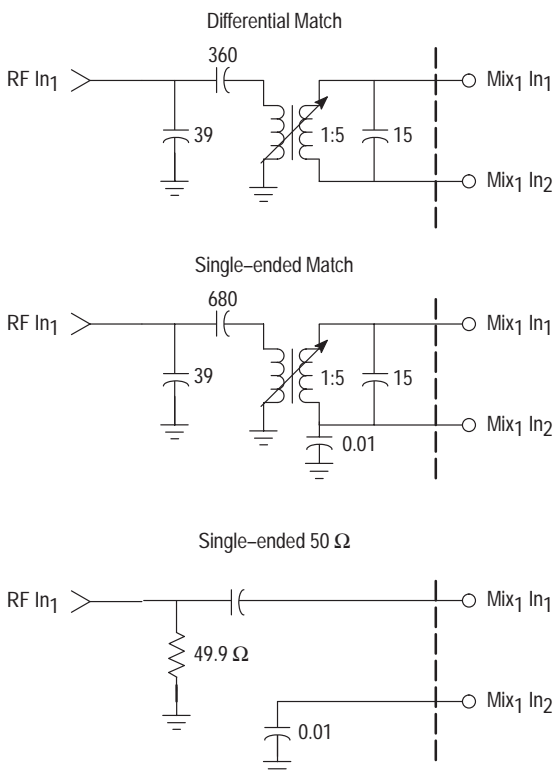
The duplexer is important to achieve full duplex operation without significant “de-sensing” of the receiver by the transmitter. The combination of the duplexer and preamp circuit should attenuate the transmitter power to the receiver by over 60 dB. This will improve the receiver system noise figure without giving up too much IMD performance.

The duplexer may be a two piece unit offered by Shimida, Sansui, or Toko products (designed for 25 channel CT-0 cordless phone). The duplexer frequency response at the receiver port has a notch at the transmitter frequency band of about 35 to 40 dB with a 2.0 to 3.0 dB insertion loss at the receiver frequency band.

The preamp circuit utilizes a tuned transformer at the output side of the amplifier. This transformer is designed to bandpass filter at the receiver input frequency while rejecting the transmitter frequency. The tuned preamp also improves the noise performance by reducing the bandwidth of the pass band and by reducing the second stage contribution of the 1st mixer. The preamp is biased such that it yields suitable noise figure and gain.

The following matching networks have been used to obtain 12 dB SINAD sensitivity numbers:

Figure 60. Matching Input Networks



The exact impedance looking into the RF In1 pin is displayed in the following table along with the sensitivity levels.

Figure 61. 12 dB SINAD Sensitivity Levels, US Handset Application Channel 21

	Sensitivity (dBm)	Input Impedance (dBm)
Differential matched	-115.3	50.2 \pm 0.1j
Single-ended match	-114.8	50.2 \pm 0.1j
Single-ended 50 Ω	-100.1	50.2 \pm 0.1j

The graphs in Figures 64 to 69 are performance results based on Evaluation Board Schematic (Figure 137). This evaluation board did not use a duplexer or preamp stage. Figure 62 is a summary of the RF performance and Figure 63 contains the French RF Performance Summary.

Figure 62. RF Performance Summary for US Applications

MC13110A/MC13111A (fdev = 3.0 kHz, fmod = 1.0 kHz, 50 Ω)			
Parameter	Handset	Basetest	Unit
Sensitivity at 12 dB SINAD	-100.1	-100.1	dBm
Recovered Audio	132	132	mVrms
SINAD @ -30 dBm	41.8	41.4	dB
THD @ -30 dBm	0.8	0.8	%
S/N @ -30 dBm	78.2	78.5	dB
AMRR @ -30 dBm	73.4	72.2	dB
RSSI range	>80	>80	dB

Figure 63. RF Performance Summary for US French Applications

MC13110A/MC13111A (fdev = 1.5 kHz, fmod = 1.0 kHz, 50 Ω)			
Parameter	Handset	Basetest	Unit
Sensitivity at 12 dB SINAD	-91	-90.8	dBm
Recovered Audio	89.8	90	mVrms
SINAD @ -30 dBm	42.1	44.3	dB
THD @ -30 dBm	0.8	0.8	%
S/N @ -30 dBm	75.7	75.1	dB
AMRR @ -30 dBm	56	84.7	dB
RSSI range	>80	>80	dB

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RF SYSTEM PERFORMANCE

Figure 64. Typical Receiver Performance Parameters U.S. Handset Application Channel 21

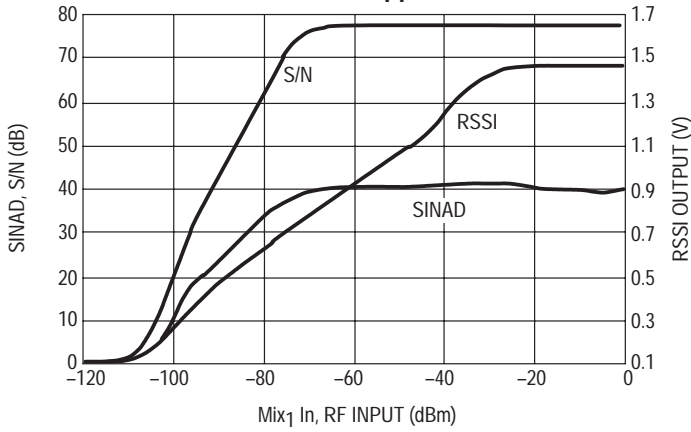


Figure 65. Typical Performance Parameters Over U.S. Handset Channel Frequencies

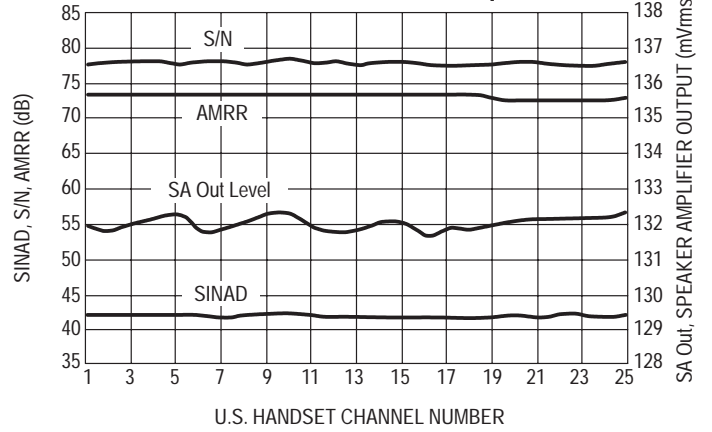


Figure 66. Typical Performance Parameters Over U.S. Baseband Channel Frequencies

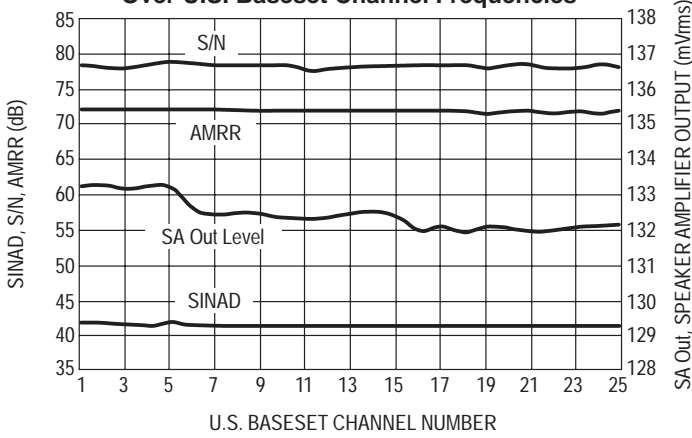


Figure 67. Typical Receiver Performance for US Handset Application Channel 21

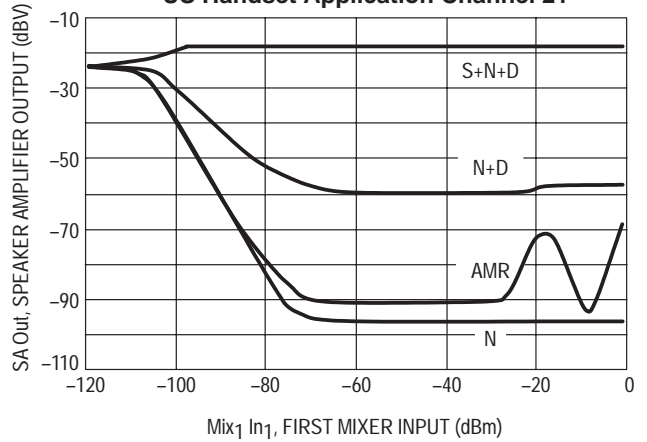


Figure 68. 12 dB SINAD Sensitivity Over US Handset Application Channels

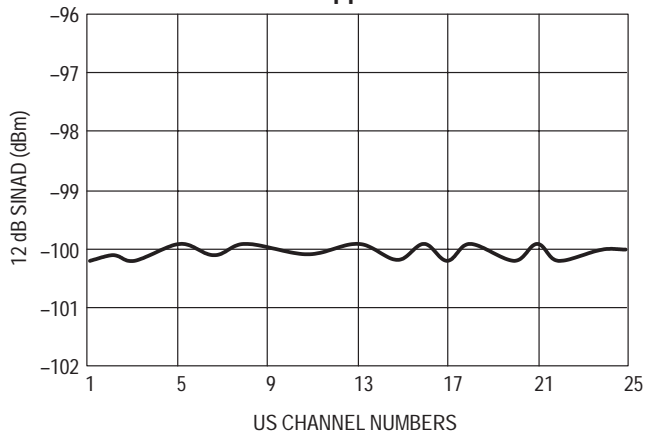
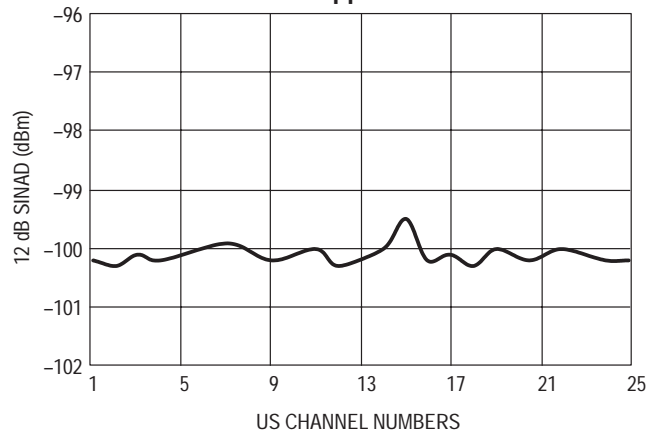


Figure 69. 12 dB SINAD Sensitivity Over US Baseband Application Channels



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Receive Audio Path

The R_X Audio signal path begins at “Rx Audio In” and goes through the IC to “E Out”. The “R_X Audio In”, “Scr Out”, and “E In” pins are all ac-coupled. This signal path consists of filters; programmable R_X gain adjust, R_X mute, and volume control, and finally the expander. The typical maximum output voltage at “E Out” should be approximately 0 dBV @ THD = 5.0% .

Figures 71 to 73 represent the receive audio path filter response. The filter response attenuation is very sharp above 3900 Hz, which is the cutoff frequency. Inband (audio), out-of-band, and ripple characteristics are also shown in these graphs.

The group delay (Figure 75) has a peak around 6.5 kHz. This spike is formed by rapid change in the phase at the frequency. In practice this does not cause a problem since the signal is attenuated by at least 50 dB.

The output capability at “Scr Out” and “E Out” are shown in Figures 76, 77, and 78. The results were obtained by increasing the input level for 2.0% distortion at the outputs.

In Figure 70, noise data for the R_X audio path is shown. At Scr Out, the noise level clearly rises when the scrambler is

enabled. However, assuming a nominal output level of –20 dBV (100 mVrms) at the 0 dB gain setting, the noise floor is more than 56 dB below the audio signal. However, the noise data at E Out and SA Out is much more improved.

Speaker Amp

The Speaker Amp is an inverting rail-to-rail operational amplifier. The noninverting input is connected to the internal VB reference. External resistors and capacitors are used to set the gain and frequency response. The “SA In” input pin must be ac-coupled. The typical output voltage at “SA Out” is 2.6 V_{pp} with a 130 Ω load. The speaker amp response is shown in Figures 79 and 80.

Data Amp Comparator

The data amp comparator is an inverting hysteresis comparator. Its open collector output has an internal 100 kΩ pull-up resistor. A band pass filter is connected between the “Det Out” pin and the “DA In” pin with component values as shown in the Application Circuit schematic. The “DA In” input signal needs to be ac-coupled, too.

Figure 70. R_X Path Noise Data

Receive Scrambler	Receive Gain (dB)	Volume (dB)	SCR_Out (dBV)	E_Out (dBV)	SA_Out (dBV)
off/on	muted	muted	< –95	< –95	< –95
off	–9.0	–14	–92	< –95	< –95
off	0	0	–85	< –95	< –95
off	1.0	16	–76	< –95	< –95
on (MC13110A)	–9.0	–14	–85	< –95	< –95
on (MC13110A)	0	0	–77	< –95	< –95
on (MC13110A)	10	16	–66	< –95	< –95

R_X AUDIO

Figure 71. R_X Audio Wideband Frequency Response

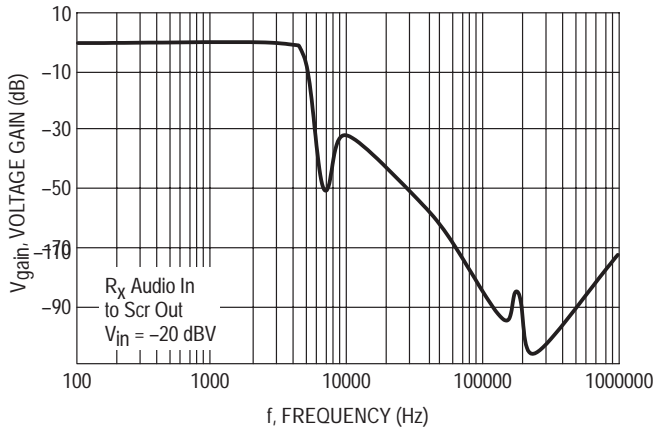


Figure 72. R_X Audio Inband Frequency Response

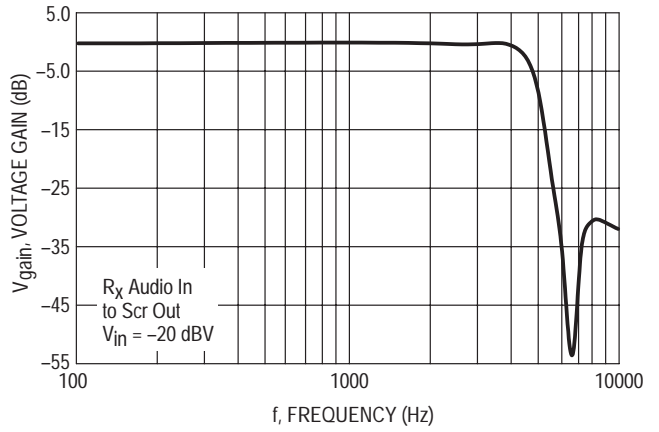


Figure 73. R_X Audio Ripple Response

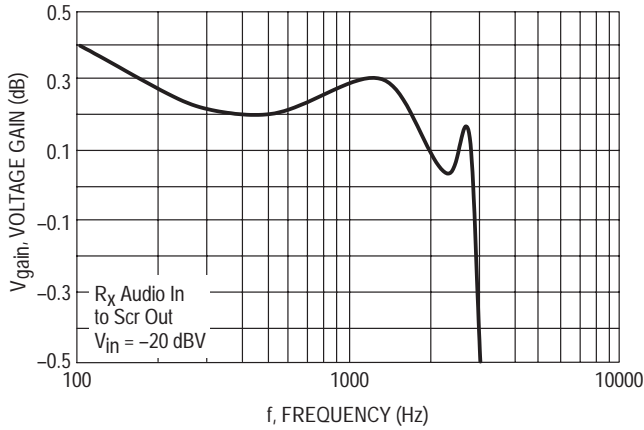


Figure 74. R_X Audio Inband Phase Response

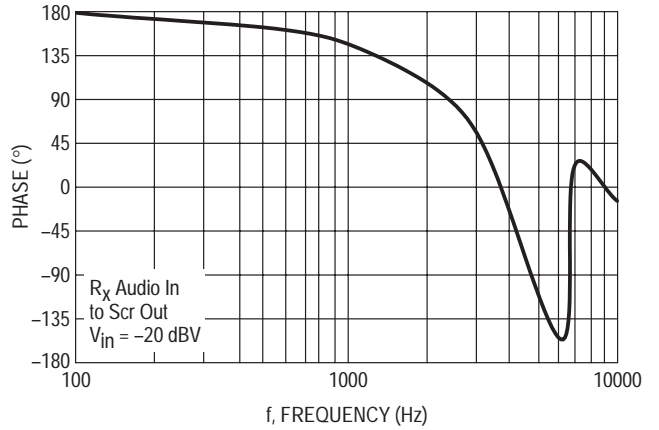


Figure 75. R_X Audio Inband Group Delay

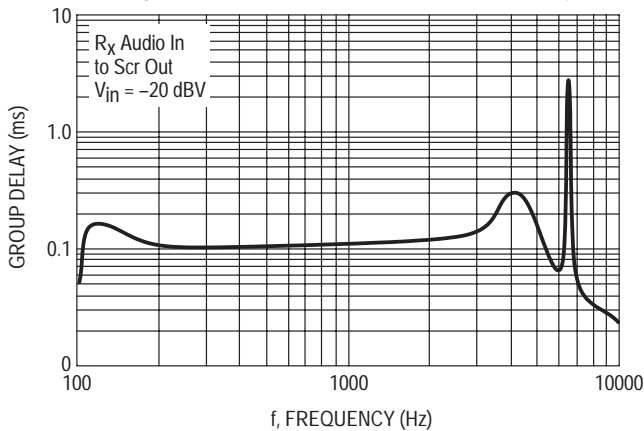
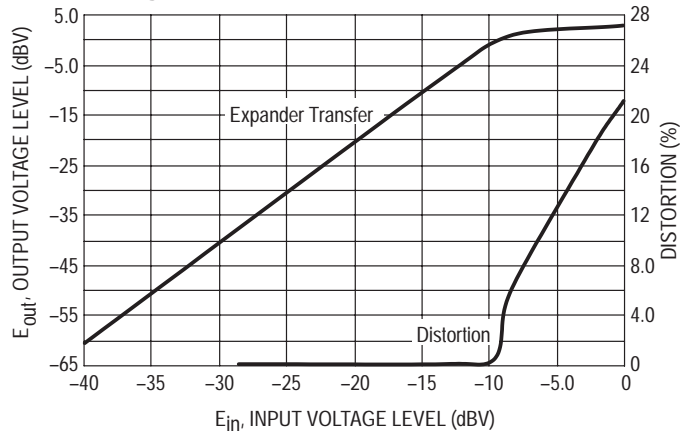


Figure 76. R_X Audio Expander Response



R_X AUDIO

Figure 77. R_X Audio Maximum Output Voltage versus Gain Control Setting

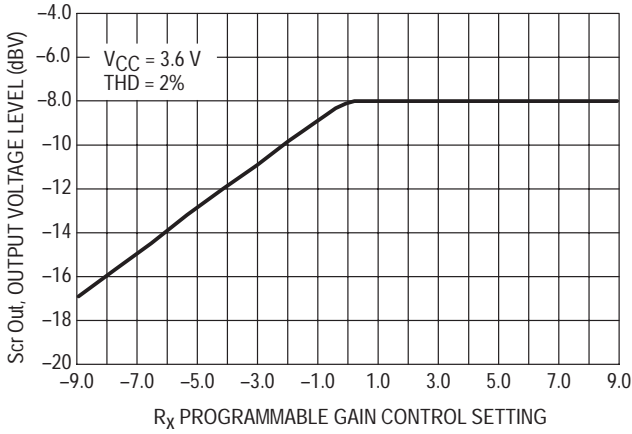


Figure 78. R_X Audio Maximum Output Voltage versus Volume Setting

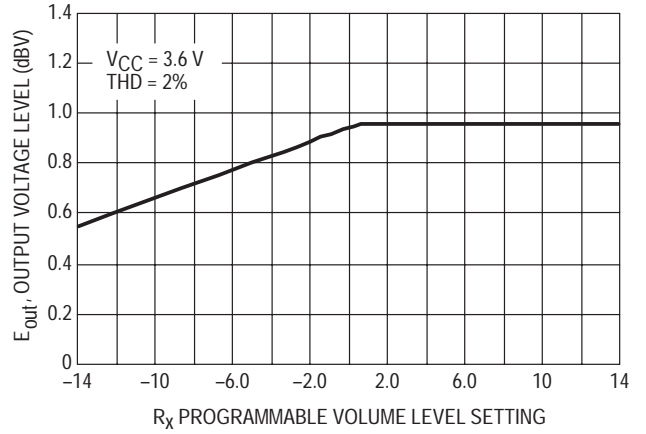


Figure 79. R_X Audio Speaker Amplifier Drive

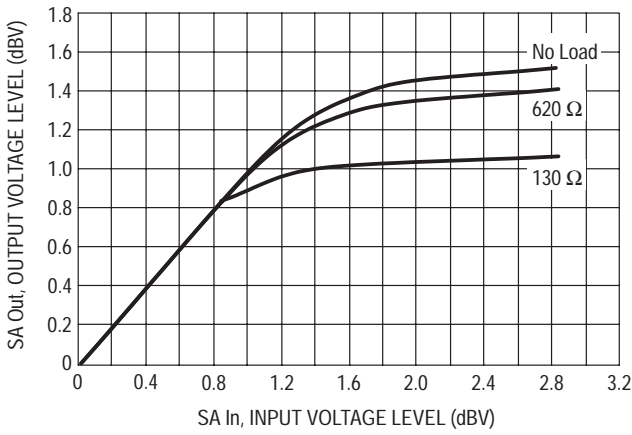
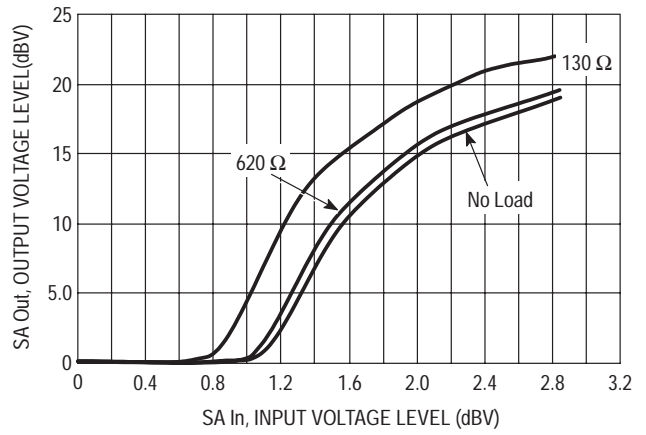


Figure 80. R_X Audio Speaker Amplifier Distortion



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Transmit Audio Path

This portion of the audio path goes from “C In” to “T_X Out”. The “C In” pin will be ac-coupled. The audio transmit signal path includes automatic level control (ALC) (also referred to as the Compressor), T_X mute, limiter, filters, and T_X gain adjust. The ALC provides “soft” limiting to the output signal swing as the input voltage slowly increases. With this technique the gain is slightly lowered to help reduce distortion of the audio signal. The limiter section provides hard limiting due to rapidly changing signal levels, or transients. This is accomplished by clipping the signal peaks. The ALC, T_X mute, and limiter functions can be enabled or disabled via the MPU serial interface. The T_X gain adjust can also be remotely controlled to set different desired signal levels. The typical maximum output voltage at “T_X Out” should be approximately 0 dBV @ THD = 5.0%.

Figures 82 to 86 represent the transmit audio path filter response. The filter response attenuation, again, is very definite above 3800 Hz. This is the filter cutoff frequency. Inband (audio), wideband, and ripple characteristics are also shown in these graphs.

The compressor transfer characteristics, shown in Figure 87, has three different slopes. A typical compressor slope can be found between -55 and -15 dBV. Here the slope is 2.0. At an input level above -15 dBV the automatic level control (ALC) function is activated and prevents hard clipping of the output. The slope below -55 dBV input level is one. This is where the compressor curve ends. Above 5.0 dBV the output actually begins to decrease and distort. This is due to supply voltage limitations.

In Figure 88 the ALC function is off. Here the compressor curve continues to increase above -15 dBV up to -4.0 dBV.

The limiter begins to clip the output signal at this level and distortion is rapidly rising. Similarly, Figure 68 (ALC and Limiter Off) shows to compressor transfer curve extending all the way up to the maximum output. Finally, Figure 90 through 93 show the T_X Out signal versus several combinations of ALC and Limiter selected.

Figure 81 is the noise data measured for the MC13110A/13111A. This data is for 0 dB gain setting and -20 dBV (100 mVrms) audio levels.

Figure 81. T_X Path Noise Data

Transmit Scrambler	Transmit Gain (dB)	Amp_Out (dBV)	T _X _Out (dBV)
off/on	muted	muted	< -95
off	-9.0	< -95	-83
off	0	< -95	-74
off	10	< -95	-64
on (MC13110A)	-9.0	< -95	-82
on (MC13110A)	0	< -95	-73
on (MC13110A)	10	< -95	-63

Mic Amp

Like the Speaker Amp the Mic Amp is also an inverting rail-to-rail operational amplifier. The noninverting input terminal is connected to the internal VB reference. External resistors and capacitors are used to set the gain and frequency response. The “T_X In” input is ac-coupled.

T_X AUDIO

Figure 82. T_X Audio Wideband Frequency Response

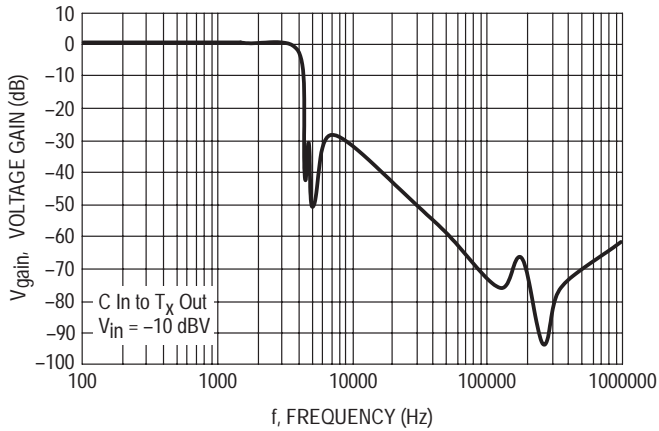


Figure 83. T_X Audio Inband Frequency Response

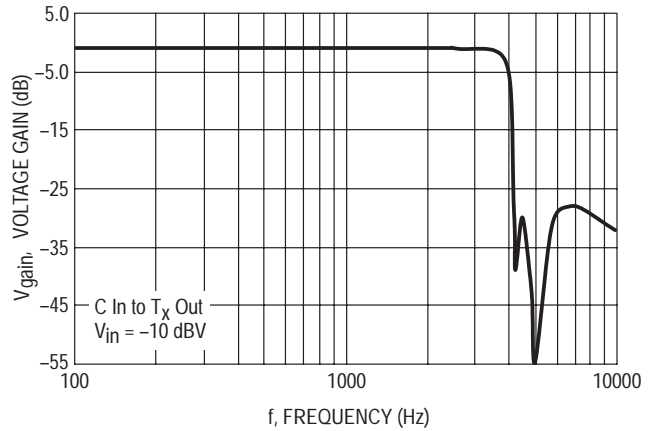


Figure 84. T_X Audio Ripple Response

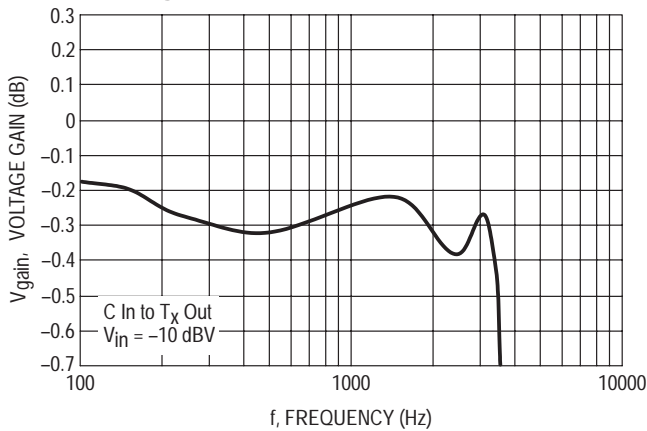


Figure 85. T_X Audio Inband Phase Response

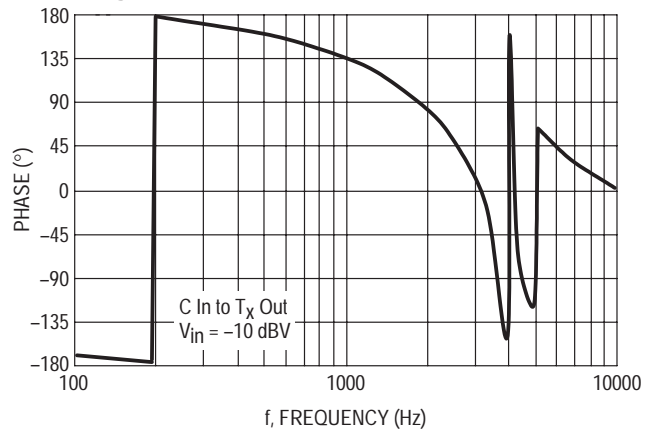


Figure 86. T_X Audio Inband Group Delay

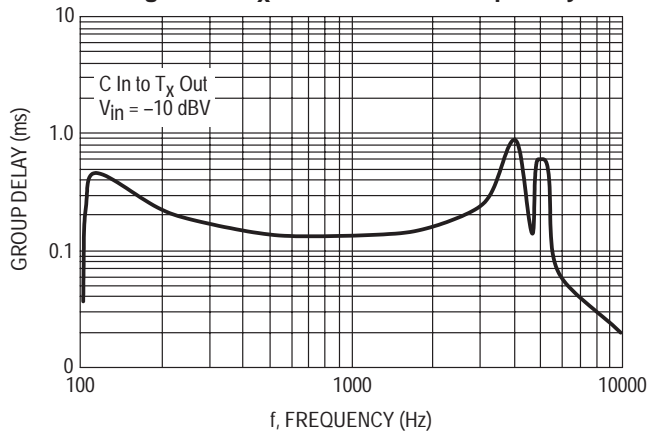
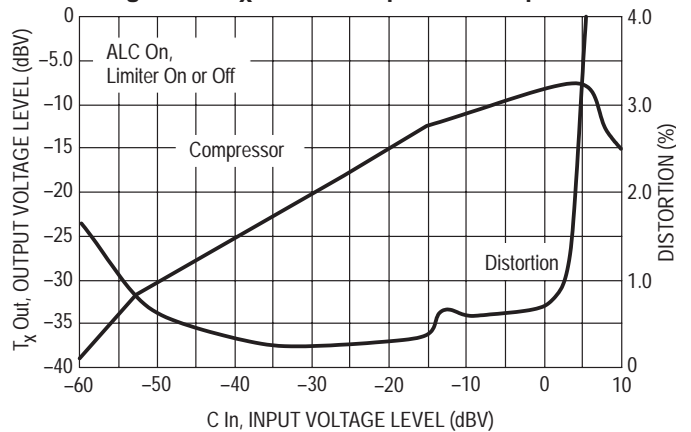


Figure 87. T_X Audio Compressor Response



T_X AUDIO

Figure 88. T_X Audio Compressor Response

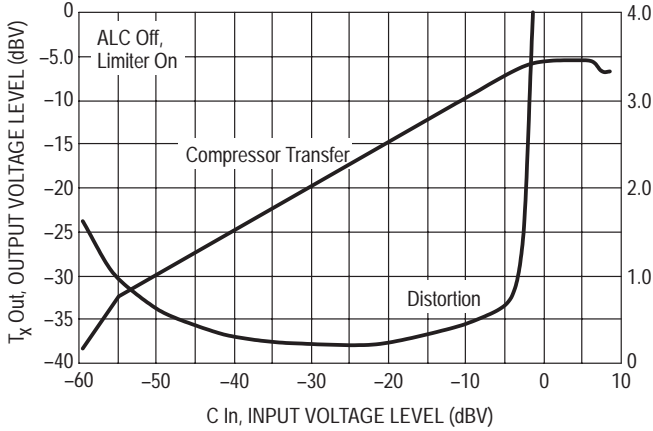


Figure 89. T_X Audio Compressor Response

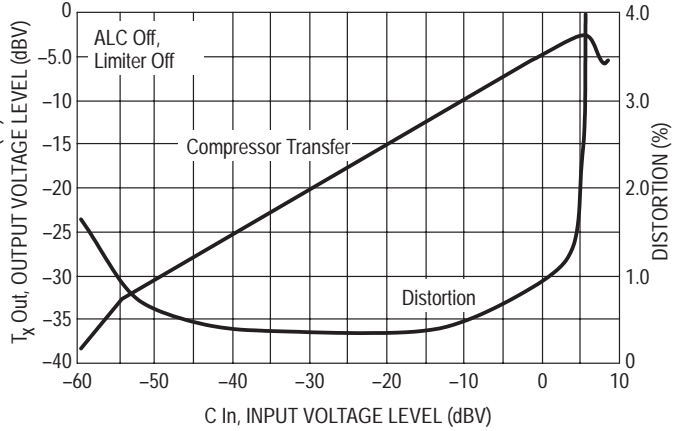


Figure 90. T_X Audio Maximum Output Voltage versus Gain Control Setting

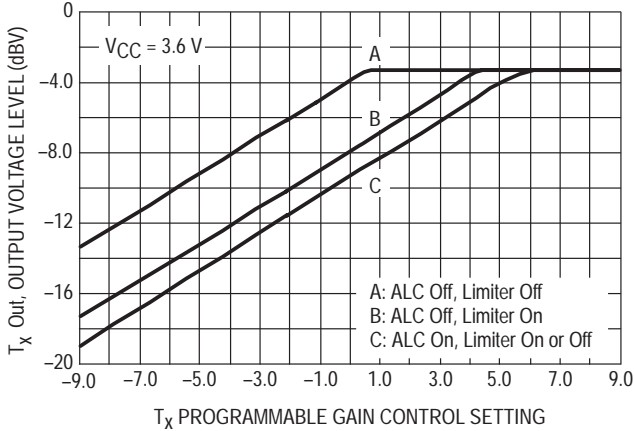


Figure 91. T_X Output Audio Response

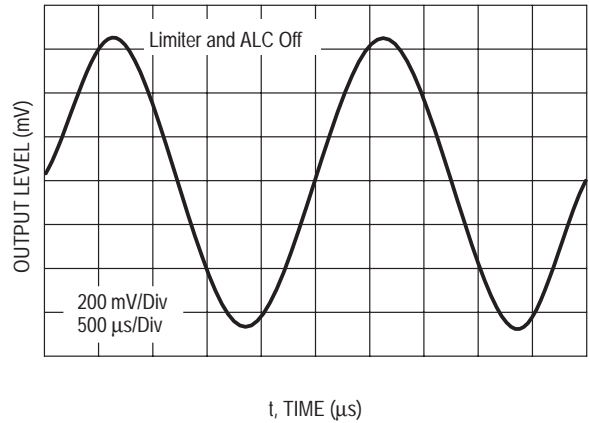


Figure 92. T_X Output Audio Response

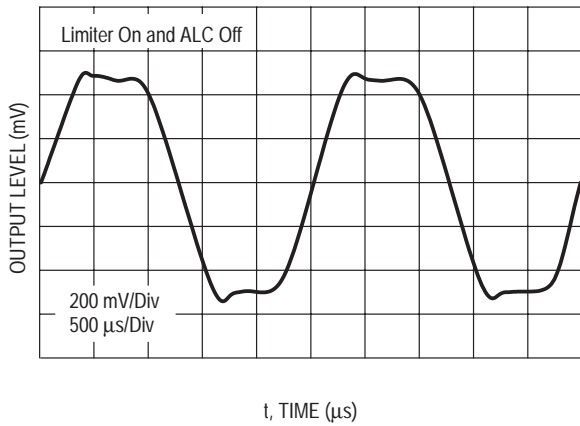
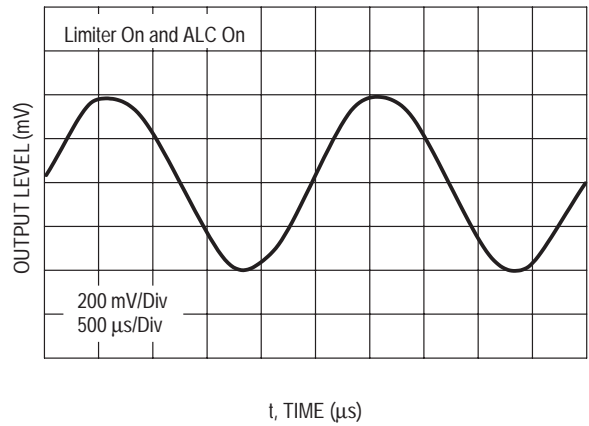


Figure 93. T_X Audio Output Response



MC13110A MC13111A

PLL SYNTHESIZER SECTION

PLL Frequency Synthesizer General Description

Figure 95 shows a simplified block diagram of the programmable universal dual phase locked loop (PLL) designed into the MC13110A and MC13111A IC. This dual PLL is fully programmable through the MCU serial interface and supports most country channel frequencies including USA (25 ch), Spain, Australia, Korea, New Zealand, U.K., Netherlands, France, and China (see channel frequency tables in AN1575, "Worldwide Cordless Telephone Frequencies").

The 2nd local oscillator and reference divider provide the reference frequency signal for the R_X and T_X PLL loops. The programmed divider value for the reference divider is selected based on the crystal frequency and the desired R_X and T_X reference frequency values. For the U.K., additional divide by 25 and divide by 4 blocks are provided to allow for generation of the 1.0 kHz and 6.2 kHz reference frequencies.

The 14-bit R_X counter is programmed for the desired first local oscillator frequency. The 14-bit T_X counter is programmed for the desired transmit channel frequency. All counters power-up to a set default state for USA channel #21 using a 10.24 MHz reference frequency crystal (see power-up default latch register state in the Serial Programmable Interface section).

To extend the sensitivity of the 1st LO for U.S. 25 channel operation, internal fixed capacitors can be connected to the tank circuit through microprocessor programmable control. When designing the external PLL loop filters, it is recommended that the T_X and R_X phase detectors be considered as current drive type outputs. The loop filter control voltage must be 0.5 V away from either the positive or negative supply rail.

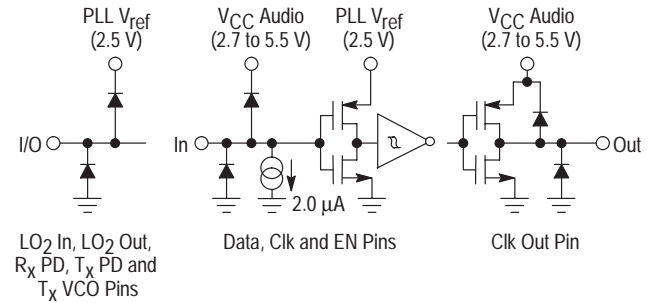
PLL I/O Pin Configurations

The 2nd LO, R_X and T_X PLL's, and MPU serial interface are powered by the internal voltage regulator at the "PLL V_{ref} " pin. The "PLL V_{ref} " pin is the output of a voltage regulator which is powered from the "VCC Audio" power supply pin. It is regulated by an internal bandgap voltage reference. Therefore, the maximum input and output levels for most of the PLL I/O pins (LO2 In, LO2 Out, R_X PD, T_X PD, T_X VCO) is the regulated voltage at the "PLL V_{ref} " pin. The ESD protection diodes on these pins are also connected to "PLL V_{ref} ".

Internal level shift buffers are provided for the pins (Data, Clk, EN, Clk Out) which connect directly to the

microprocessor. The maximum input and output levels for these pins is V_{CC} . Figure 94 shows a simplified schematic of the I/O pins.

Figure 94. PLL I/O Pin Simplified Schematics

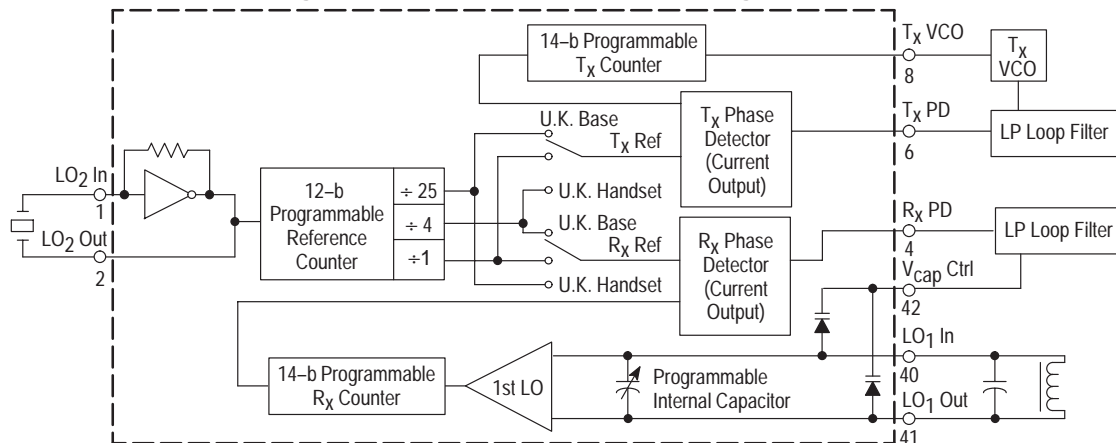


PLL Loop Control Voltage Range

The control voltage for the T_X and R_X loop filters is set by the phase detector outputs which drive the external loop filters. The phase detectors are best considered to have a current mode type output. The output can have three states; ground, high impedance, and positive supply, which in this case is the voltage at "PLL V_{ref} ". When the loop is locked the phase detector outputs are at high impedance. An exception of this state is for narrow current pulses, referenced to either the positive or negative supply rails. If the loop voltages get within 0.5 V of either rail the linear current output starts to degrade. The phase detector current source was not designed to operate at the supply rails. VCO tuning range will also be limited by this voltage range.

The maximum loop control voltage is the "PLL V_{ref} " voltage which is 2.5 V. If a higher loop control voltage range is desired, the "PLL V_{ref} " pin can be pulled to a higher voltage. It can be tied directly to the V_{CC} voltage (with suitable filter capacitors connected close to each pin). When this is done, the internal voltage regulator is automatically disabled. This is commonly used in the telephone base set where an external 5.0 V regulated voltage is available. It is important to remember, that if "PLL V_{ref} " is tied to V_{CC} and V_{CC} is not a regulated voltage, the PLL loop parameters and lock-up time will vary with supply voltage variation. The phase detector gain constant, K_{pd} , will not be affected if the "PLL V_{ref} " is tied to V_{CC} .

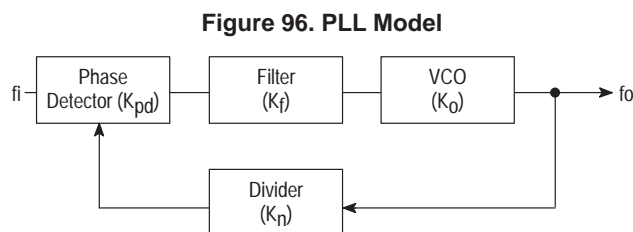
Figure 95. Dual PLL Simplified Block Diagram



Loop Filter Characteristics

Lets consider the following discussion on loop filters. The fundamental loop characteristics, such as capture range, loop bandwidth, lock-up time, and transient response are controlled externally by loop filtering.

Figure 96 is the general model for a Phase Lock Loop (PLL).



Where:

- K_{pd} = Phase Detector Gain Constant
- K_f = Loop Filter Transfer Function
- K_o = VCO Gain Constant
- K_n = Divide Ratio (1/N)
- f_i = Input frequency
- f_o = Output frequency
- f_o/N = Feedback frequency divided by N

From control theory the loop transfer function can be represented as follows:

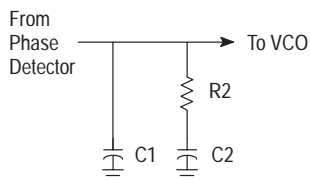
$$A = K_{pd} K_f K_o K_n \text{ Open loop gain}$$

K_{pd} can be either expressed as being 2.5 V/4.0 π or 1.0 mA/2.0 π for the CT-0 circuits. More details about performance of different type PLL loops, refer to Motorola application note AN535.

The loop filter can take the form of a simple low pass filter. A current output, type 2 filter will be used in this discussion since it has the advantage of improved step response, velocity, and acceleration.

The type 2 low pass filter discussed here is represented as follows:

Figure 97. Loop Filter with Additional Integrating Element

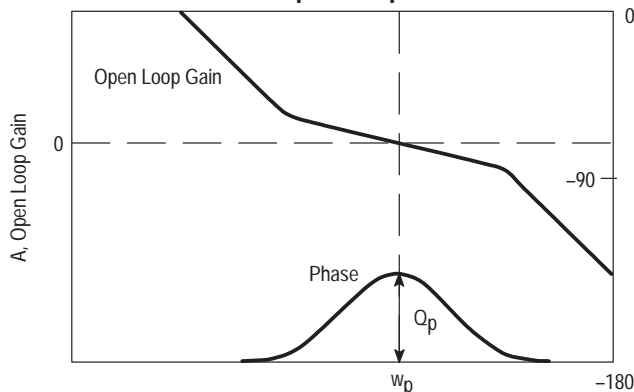


From Figure 97, capacitor C1 forms an additional integrator, providing the type 2 response, and filters the discrete current steps from the phase detector output. The function of the additional components R2 and C2 is to create a pole and a zero (together with C1) around the 0 dB point of the open loop gain. This will create sufficient phase margin for stable loop operation.

In Figure 98, the open loop gain and the phase is displayed in the form of a Bode plot. Since there are two integrating functions in the loop, originating from the loopfilter and the VCO gain, the open loop gain response follows a

second order slope (-40 dB/dec) creating a phase of -180 degrees at the lower and higher frequencies. The filter characteristic needs to be determined such that it is adding a pole and a zero around the 0 dB point to guarantee sufficient phase margin in this design (Q_p in Figure 98).

Figure 98. Bode Plot of Gain and Phase in Open Loop Condition



The open loop gain including the filter response can be expressed as:

$$A_{openloop} = \frac{K_{pd}K_o(1 + jw(R2C2))}{jwK_n \left(jw \left(1 + jw \left(\frac{R2C1C2}{C1 + C2} \right) \right) \right)} \quad (1)$$

The two time constants creating the pole and the zero in the Bode plot can now be defined as:

$$T1 = \frac{R2C1C2}{C1 + C2} \quad T2 = R2C2 \quad (2)$$

By substituting equation (2) into (1), it follows:

$$A_{openloop} = \left(\frac{K_{pd}K_oT1}{w^2C1K_nT2} \right) \left(\frac{1 + jwT2}{1 + jwT1} \right) \quad (3)$$

The phase margin (phase + 180) is thus determined by:

$$Q_p = \arctan(wT2) - \arctan(wT1) \quad (4)$$

At $w=w_p$, the derivative of the phase margin may be set to zero in order to assure maximum phase margin occurs at w_p (see also Figure 98). This provides an expression for w_p :

$$\frac{dQ_p}{dw} = 0 = \frac{T2}{1 + (wT2)^2} - \frac{T1}{1 + (wT1)^2} \quad (5)$$

$$w = w_p = \frac{1}{\sqrt{T2T1}} \quad (6)$$

Or rewritten:

$$T1 = \frac{1}{w_p^2 T2} \quad (7)$$

By substituting into equation (4), solve for T2:

$$T2 = \frac{\tan\left(\frac{Q_p}{2} + \frac{\pi}{4}\right)}{w_p} \quad (8)$$

By choosing a value for w_p and Q_p , T1 and T2 can be calculated. The choice of Q_p determines the stability of the loop. In general, choosing a phase margin of 45 degrees is a good choice to start calculations. Choosing lower phase margins will provide somewhat faster lock-times, but also generate higher overshoots on the control line to the VCO. This will present a less stable system. Larger values of phase margin provide a more stable system, but also increase lock-times. The practical range for phase margin is 30 degrees up to 70 degrees.

The selection of w_p is strongly related to the desired lock-time. Since it is quite complicated to accurately calculate lock time, a good first order approach is:

$$T_{lock} \approx \frac{3}{w_p} \quad (9)$$

Equation (9) only provides an order of magnitude for lock time. It does not clearly define what the exact frequency difference is from the desired frequency and it does not show the effect of phase margin. It assumes, however, that the phase detector steps up to the desired control voltage without hesitation. In practice, such step response approach is not really valid. The two input frequencies are not locked. Their phase maybe momentarily zero and force the phase detector into a high impedance mode. Hence, the lock times may be found to be somewhat higher.

In general, w_p should be chosen far below the reference frequency in order for the filter to provide sufficient attenuation at that frequency. In some applications, the reference frequency might represent the spacing between channels. Any feedthrough to the VCO that shows up as a spur might affect adjacent channel rejection. In theory, with the loop in lock, there is no signal coming from the phase detector. But in practice leakage currents will be supplied to both the VCO and the phase detector. The external capacitors may show some leakage, too. Hence, the lower w_p , the better the reference frequency is filtered, but the longer it takes for the loop to lock.

As shown in Figure 98, the open loop gain at w_p is 1 (or 0 dB), and thus the absolute value of the complex open loop gain as shown in equation (3) solves C1:

$$C1 = \left(\frac{K_{pd}K_oT1}{w^2K_nT2}\right) \sqrt{\frac{(1 + w_pT2)^2}{(1 + w_pT1)^2}} \quad (10)$$

With C1 known, and equation (2) solve C2 and R2:

$$C2 = C1\left(\frac{T2}{T1} - 1\right) \quad (11)$$

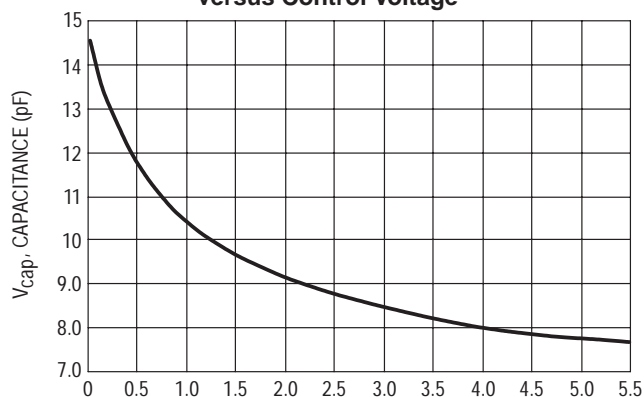
$$R2 = \frac{T2}{C2} \quad (12)$$

The VCO gain is dependent on the selection of the external inductor and the frequency required. The free running frequency of the VCO is determined by:

$$f = \frac{1}{2\pi\sqrt{LC_T}} \quad (13)$$

In which L represents the external inductor value and C_T represents the total capacitance (including internal capacitance) in parallel with the inductor. The VCO gain can be easily calculated via the internal varicap transfer curve shown below.

Figure 99. Varicap Capacitance versus Control Voltage



As can be derived from Figure 99, the varicap capacitance changes 1.3 pF over the voltage range from 1.0 V to 2.0 V:

$$\Delta Cvar = \frac{1.3 \text{ pF}}{V} \quad (14)$$

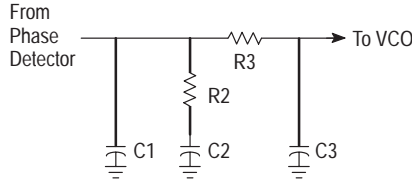
Combining (13) with (14) the VCO gain can be determined by:

$$K_o = \frac{1}{jw} \left\{ \frac{1}{2\pi\sqrt{L\left(C_T + \frac{\Delta Cvar}{2}\right)}} - \frac{1}{2\pi\sqrt{L\left(C_T + \frac{\Delta Cvar}{2}\right)}} \right\} \quad (15)$$

Although the basic loopfilter previously described provides adequate performance for most applications, an extra pole may be added for additional reference frequency filtering. Given that the channel spacing in a CT-0 telephone set is based on the reference frequency, and any feedthrough to

the first LO may effect parameters like adjacent channel rejection and intermodulation. Figure 100 shows a loopfilter architecture incorporating an additional pole.

Figure 100. Loop Filter with Additional Integrating Element



For the additional pole formed by R3 and C3 to be efficient, the cut-off frequency must be much lower than the reference frequency. However, it must also be higher than ω_p in order not to compromise phase margin too much. The following equations were derived in a similar manner as for the basic filter previously described.

Similarly, it can be shown:

$$A_{\text{openloop}} = -\frac{K_{pd}K_o}{K_n\omega^2((C1 + C2 + C3) - \omega^2C1C2C3R2R3)} + \frac{1 + j\omega T2}{1 + j\omega T1} \quad (16)$$

In which:

$$T1 = \frac{(C1 + C2)T2 + (C1C2)T3}{C1 + C2 + C3 - \omega^2C1T2T3} \quad (17)$$

$$T2 = R2C2 \quad (18) \quad T3 = R3C3 \quad (19)$$

From T1 it can be derived that:

$$C2 = \frac{(T1 + T2)C3 - C1(T2 + T3 - T1 + \omega^2T1T2T3)}{T3 - T1} \quad (20)$$

In analogy with (10), by forcing the loopgain to 1 (0 dB) at ω_p , we obtain:

$$C1(T1 + T2) + C2T3 + C3T2 = \left(\frac{K_{pd}K_o}{K_n\omega_p^2}\right) \sqrt{\frac{1 + (\omega_p T2)^2}{1 + (\omega_p T1)^2}} \quad (21)$$

Solving for C1:

$$C1 = \frac{(T2 - T1)T3C3 - (T3 - T1)T2C3 + (T3 - T1)\left(\frac{K_{pd}K_o T1}{\omega_p^2 K_n}\right) \sqrt{\frac{1 + (\omega_p T2)^2}{1 + (\omega_p T1)^2}}}{(T3 - T1)T2 + (T3 - T1)T3 - (T2 + T3 - T1 + \omega_p^2 T1 T2 T3)T3} \quad (22)$$

By selecting ω_p via (9), the additional time constant expressed as T3, can be set to:

$$T3 = \frac{1}{K\omega_p} \quad (23)$$

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The K-factor shown determines how far the additional pole frequency will be separated from ω_p . Selecting too small of a K-factor, the equations may provide negative capacitance or resistor values. Too large of a K-factor may not provide the maximum attenuation.

By selecting R3 to be 100 k Ω , C3 becomes known and C1 and C2 can be solved from the equations. By using equations (8) and (7), time constants T2 and T1 can be derived by selecting a phase margin. Finally, R2 follows from T2 and C2.

The following pages, the loopfilter components are determined for both handset and basaset the US application based on the equations described. Choose K to be approximately five times ω_p ($5\omega_p$).

In an application, ω_p is chosen to be 20 times less than the reference frequency of 5.0 kHz and the phase margin has

been set to 45 degrees. This provides a lock time according to (9) of about 2.0 ms (order of magnitude). With the adjacent channels spaced at least 15 kHz away, reference feedthrough at ω_p will not be directly disastrous but still, the additional pole may be added in the loopfilter design for added safety.

In an application, ω_p is chosen to be 20 times less than the reference frequency of 5.0 kHz and the phase margin has been set to 45 degrees. This provides a lock time according to (9) of about 2.0 ms (order of magnitude). With the adjacent channels spaced at least 15 kHz away, reference feedthrough at ω_p will not be directly disastrous but still, the additional pole may be added in the loopfilter design for added safety.

Figure 101. Open Loop Response Handset US with Selected Values

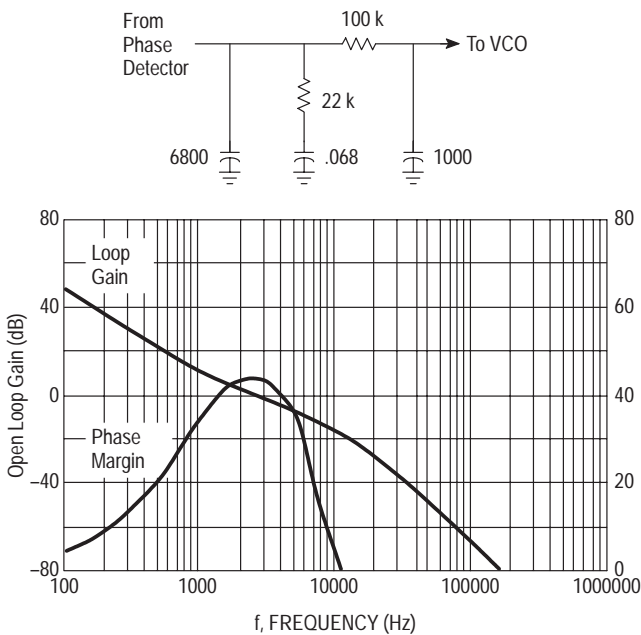


Figure 102. Open Loop Response Basaset US with Selected Values

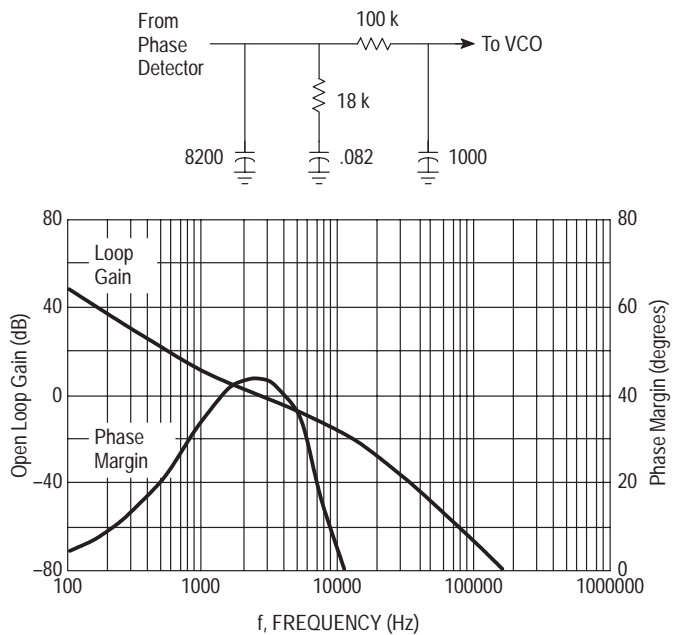


Figure 103. Handset US

Conditions		
L = 470 μ H	$F_{ref} = 5.0$ kHz	
RF = 46.77 MHz	$Q_p = 45$ degrees	
VCO center = 36.075 MHz	$\omega_p = \omega_{ref} / 20$ radians	
Results	Equations	Select
$K_{pd} = 159.2$ μ A/rad	(14), (15)	
$K_{VCO} = 3.56$ Mrad/V	(8)	
T2 = 1540 μ s	(7)	
T1 = 264 μ s	with K = 7	
T3 = 91 μ s		
C1 = 7.6 nF	(21)	C1 = 6.8 nF
C2 = 70.9 nF	(20)	C2 = 68 nF
R2 = 21.7 k Ω	(18)	R2 = 22 k Ω
R3 = 100 k Ω	choose:	R3 = 100 k Ω
C3 = 909.5 pF	(19)	C3 = 1 nF

Figure 104. Basaset US

Conditions		
L = 470 μ H	$F_{ref} = 5.0$ kHz	
RF = 49.83 MHz	$Q_p = 45$ degrees	
VCO center = 39.135 MHz	$\omega_p = \omega_{ref} / 20$ radians	
Results	Equations	Select
$K_{pd} = 159.2$ μ A/rad	(14), (15)	
$K_{VCO} = 4.54$ Mrad/V	(8)	
T2 = 1540 μ s	(7)	
T1 = 264 μ s	with K = 7	
T3 = 91 μ s		
C1 = 9.1 nF	(21)	C1 = 8.2 nF
C2 = 83.5 nF	(20)	C2 = 82 nF
R2 = 18.4 k Ω	(18)	R2 = 18 k Ω
R3 = 100 k Ω	choose:	R3 = 100 k Ω
C3 = 909.5 pF	(19)	C3 = 1 nF

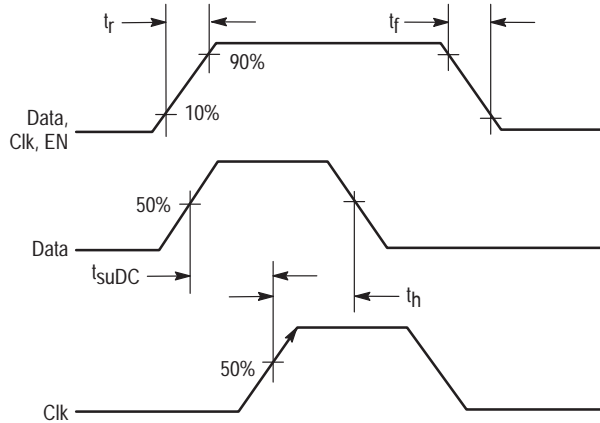
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SERIAL PROGRAMMABLE INTERFACE

Microprocessor Serial Interface

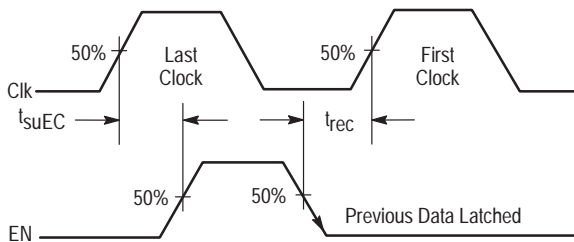
The Data, Clock, and Enable (“Data”, “Clk”, and “EN” respectively) pins provide a MPU serial interface for programming the reference counters, the transmit and receive channel divide counters, the switched capacitor filter clock counter, and various other control functions. The “Data” and “Clk” pins are used to load data into the MC13111A shift register (Figure 109). Figure 105 shows the timing required on the “Data” and “Clk” pins. Data is clocked into the shift register on positive clock transitions.

Figure 105. Data and Clock Timing Requirement



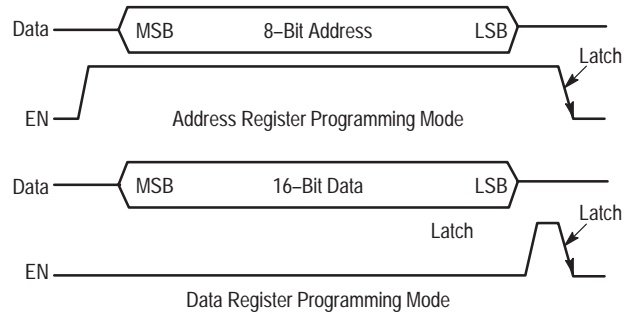
After data is loaded into the shift register, the data is latched into the appropriate latch register using the “EN” pin. This is done in two steps. First, an 8-bit address is loaded into the shift register and latched into the 8-bit address latch register. Then, up to 16-bits of data is loaded into the shift register and latched into the data latch register. It is specified by the address that was previously loaded. Figure 106 shows the timing required on the EN pin. Latching occurs on the negative EN transition.

Figure 106. Enable Timing Requirement



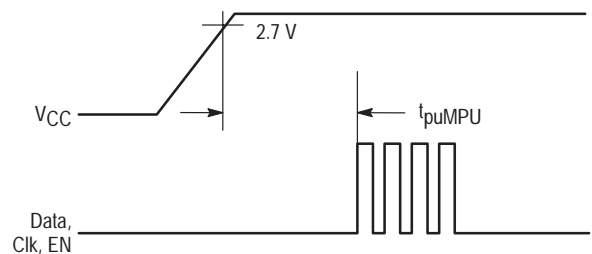
The state of the “EN” pin when clocking data into the shift register determines whether the data is latched into the address register or a data register. Figure 107 shows the address and data programming diagrams. In the data programming mode, there must not be any clock transitions when “EN” is high. The clock can be in a high state (default high) or a low state (default low) but must not have any transitions during the “EN” high state. The convention in these figures is that latch bits to the left are loaded into the shift register first. A minimum of four “Clk” rising edge transition must occur before a negative “EN” transition will latch data or an address into a register.

Figure 107. Microprocessor Interface Programming Mode Diagrams



The MPU serial interface is fully operational within 100 μ s after the power supply has reached its minimum level during power-up (see Figure 108). The MPU Interface shift registers and data latches are operational in all four power saving modes; Inactive, Standby, R_x , and Active Modes. Data can be loaded into the shift registers and latched into the latch registers in any of the operating modes.

Figure 108. Microprocessor Serial Interface Power-Up Delay



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Data Registers

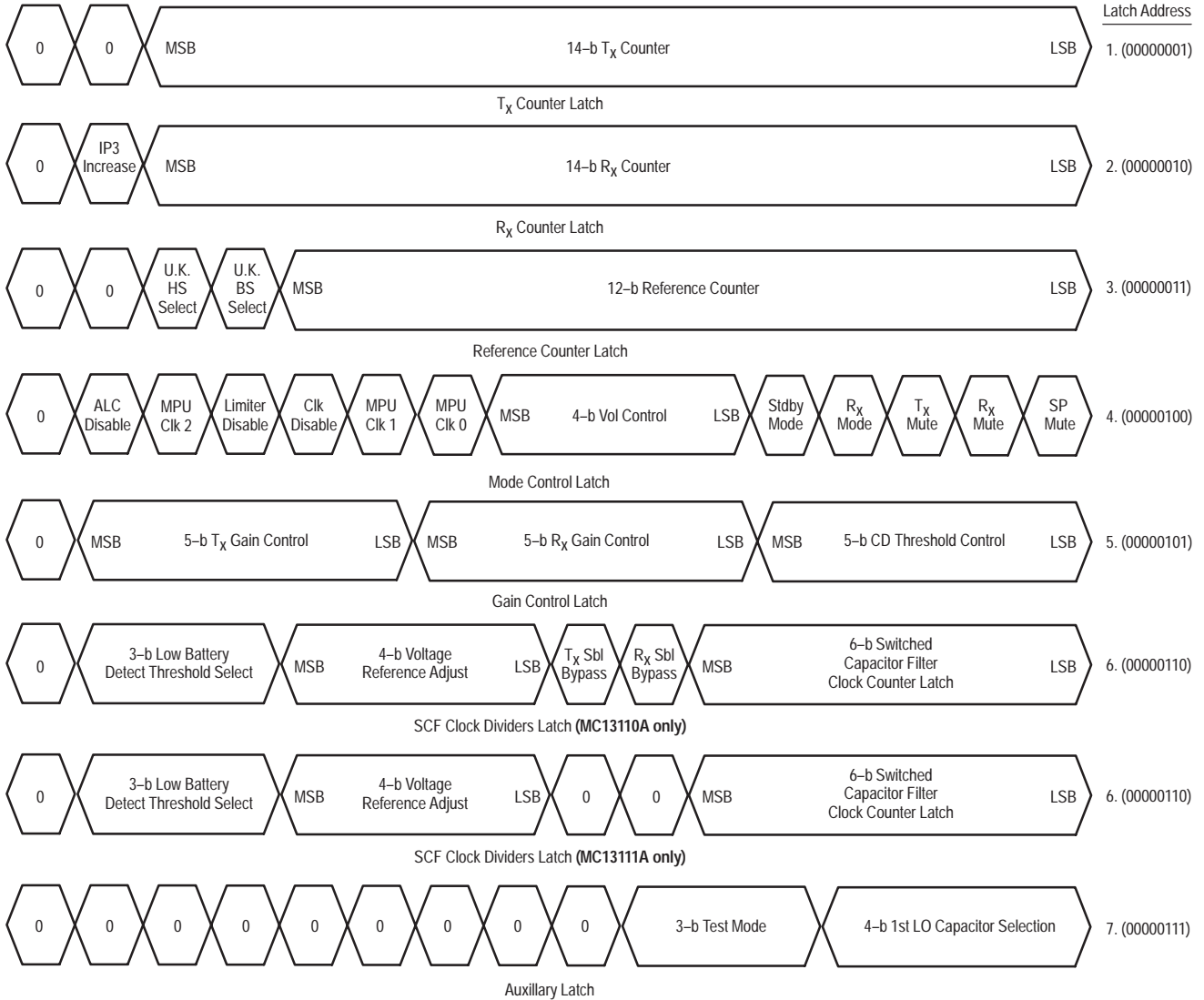
Figure 109 shows the data latch registers and addresses which are used to select each of each registers. Latch bits to the left (MSB) are loaded into the shift register first. The LSB bit must always be the last bit loaded into the shift register. Bits preceding the register must be "0's" as shown.

Power-Up Defaults for Data Registers

When the IC is first powered up, all latch registers are initialized to a defined state. The device is initially placed in the

R_X mode with all mutes active. The reference counter is set to generate a 5.0 kHz reference frequency from a 10.24 MHz crystal. The switched capacitor filter clock counter is set properly for operation with a 10.24 MHz crystal. The T_X and R_X counter registers are set for USA handset channel frequency, number 21 (Channel 6 for previous FCC 10 Channel Band). Figure 110 shows the initial power-up states for all latch registers.

Figure 109. Microprocessor Interface Data Latch Registers



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Figure 110. Latch Register Power-Up Defaults

Register	Count	MSB								LSB							
		15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
T _X	9966	–	–	1	0	0	1	1	0	1	1	1	0	1	1	1	0
R _X	7215	–	–	0	1	1	1	0	0	0	0	1	0	1	1	1	1
Ref	2048	–	–	0	0	1	0	0	0	0	0	0	0	0	0	0	0
Mode	N/A	–	0	0	0	0	1	1	0	1	1	1	0	1	1	1	1
Gain	N/A	–	0	1	1	1	1	0	1	1	1	1	1	0	1	0	0
SCF (MC13110A)	31	–	0	0	0	0	1	1	1	0	0	0	1	1	1	1	1
SCF (MC13111A)	31	–	0	0	0	0	1	1	1	–	–	0	1	1	1	1	1
Aux	N/A	–	–	–	–	–	–	–	–	–	0	0	0	0	0	0	0

NOTE: 12. Bits 6 and 7 in the SCF latch register are "Don't Cares" for the MC13111A since this part does not have a scrambler.

T_X and R_X Counter Registers

The 14 bit T_X and R_X counter registers are used to select the transmit and receive channel frequencies. In the R_X counter there is an "IP3 Increase" bit that allows the ability to trade off increased receiver mixer performance versus reduced power consumption. With "IP3 increase" = <1>, there is about a 10 dB improvement in 1 dB compression and 3rd order intercept for both the 1st and 2nd mixers. However, there is also an increase in power supply current of 1.3 mA. The power-up default for the MC13111A is "IP3 Increase" = <0>. The register bits are shown in Figure 111.

Reference Counter Register

Reference Counter

Figure 113 shows how the reference frequencies for the R_X and T_X loops are generated. All countries except the U.K. require that the T_X and R_X reference frequencies be identical.

In this case, set "U.K. Base Select" and "U.K. Handset Select" bits to "0". Then the fixed divider is set to "1" and the T_X and R_X reference frequencies will be equal to the crystal oscillator frequency divided by the programmable reference counter value.

The U.K. is a special case which requires a different reference frequency value for T_X and R_X. For U.K. base operation, set "U.K. Base Select" to "1". For U.K. handset operation, set "U.K. Handset Select" to "1". The Netherlands is also a special case. A 2.5 kHz reference frequency is used for both the T_X and R_X reference and the total divider value required is 4096. This is larger than the maximum divide value available from the 12-bit reference divider (4095). In this case, set "U.K. Base Select" to "1" and set "U.K. Handset Select" to "1". This will give a fixed divide by 4 for both the T_X and R_X reference. Then set the reference divider to 1024 to get a total divider of 4096.

Figure 111. R_X and T_X Counter Register Latch Bits

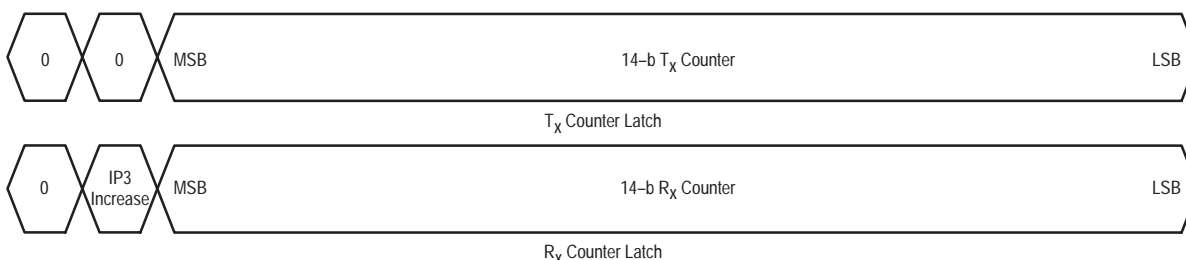
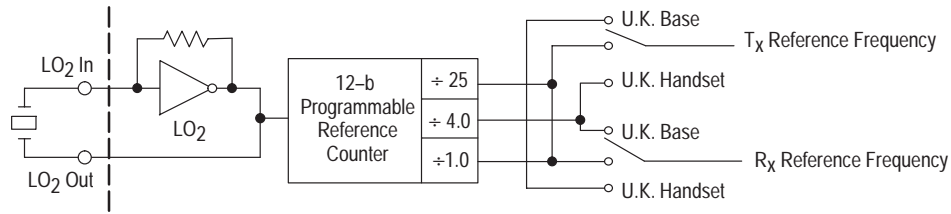


Figure 112. Reference Counter Register



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Figure 113. Reference Counter Register Programming Mode



U.K. Handset Select	U.K. Base Select	T _x Divider Value	R _x Divider Value	Application
0	0	1	1	All but U.K. and Netherlands
0	1	25	4	U.K. Base Set
1	0	4	25	U.K. Hand Set
1	1	4	4	Netherlands Base and Hand Set

Figure 114. Reference Frequency and Divider Values

MC13110A							
MC13111A							
Crystal Frequency	Reference Divider Value	U.K. Base/Handset Divider	Reference Frequency	SC Filter Clock Divider	SC Filter Clock Frequency	Scrambler Modulation Divider	Scrambler Modulation Frequency
10.24 MHz	2048	1	5.0 kHz	31	165.16 kHz	40	4.129 kHz
10.24 MHz	1024	4	5.0 kHz	31	165.16 kHz	40	4.129 kHz
11.15 MHz	2230	1	5.0 kHz	34	163.97 kHz	40	4.099 kHz
12.00 MHz	2400	1	5.0 kHz	36	166.67 kHz	40	4.167 kHz
11.15 MHz	1784	1	6.25 kHz	34	163.97 kHz	40	4.099 kHz
11.15 MHz	446	4	6.25 kHz	34	163.97 kHz	40	4.099 kHz
11.15 MHz	446	25	1.0 kHz	34	163.97 kHz	40	4.099 kHz

Figure 115. Mode Control Register



Reference Frequency Selection

The “LO₂ In” and “LO₂ Out” pins form a reference oscillator when connected to an external parallel-resonant crystal. The reference oscillator is also the second local oscillator for the RF Receiver. Figure 114 shows the relationship between different crystal frequencies and reference frequencies for cordless phone applications in various countries. “LO₂ In” may also serve as an input for an externally generated reference signal which is ac-coupled. The switched capacitor filter 6-bit programmable counter must be programmed for the crystal frequency that is selected since this clock is derived from the crystal frequency and must be held constant regardless of the crystal that is selected. The actual switched capacitor clock divider ratio is twice the programmed divider ratio due to the a fixed divide by 2.0 after the programmable counter. The scrambler mixer modulation frequency is the switched capacitor clock divided by 40 for the MC13110A.

Mode Control Register

The power saving modes; mutes, disables, volume control, and microprocessor clock output frequency are all

set by the Mode Control Register. Operation of the Control Register is explained in Figures 115 through 119.

Figure 116. Mute and Disable Control Bit Descriptions

ALC Disable	1	Automatic Level Control Disabled
	0	Normal Operation
T _x Limiter Disable	1	T _x Limiter Disabled
	0	Normal Operation
Clock Disable (MC13110A/111A)	1	MPU Clock Output Disabled
	0	Normal Operation
T _x Mute	1	Transmit Channel Muted
	0	Normal Operation
R _x Mute	1	Receive Channel Muted
	0	Normal Operation
SP Mute	1	Speaker Amp Muted
	0	Normal Operation

MC13110A MC13111A

Power Saving Operating Modes

When the MC13110A or MC13111A are used in a handset, it is important to conserve power in order to prolong battery life. There are five modes of operation for the MC13110A/MC13111A; Active, R_X, Standby, Interrupt, and Inactive. They are Active, R_X, and Standby. In the Active mode, all circuit blocks are powered. In the R_X mode, all circuitry is powered down except for those circuit sections needed to receive a transmission from the base. In the Standby and Interrupt Modes, all circuitry is powered down except for the circuitry needed to provide the clock output for the microprocessor. In the Inactive Mode, all circuitry is powered down except the MPU serial interface. Latch memory is maintained in all modes. Figure 117 shows the control register bit values for selection of each power saving mode and Figure 118 shows the circuit blocks which are powered in each of these operating modes.

Figure 117. Power Saving Mode Selection

Stdby Mode Bit	R _X Mode Bit	"CD Out/ Hardware Interrupt" Pin	Power Saving Mode
----------------	-------------------------	--	-------------------------

MC13110A/MC13111A

0	0	X	Active
0	1	X	R _X
1	0	X	Standby
1	1	1 or High Impedance	Inactive
1	1	0	Interrupt

MC13110B/MC13111B [Note 14]

0	0	X	Active
0	1	X	R _X
1	X	X	Standby
1	1	0	Interrupt

- NOTES:** 13. "X" is a don't care
14. MPU Clock Out is "Always On"

Figure 118. Circuit Blocks Powered During Power Saving Modes

Circuit Blocks	MC13110A/MC13111A			
	Active	R _X	Standby	Inactive
"PLL V _{ref} " Regulated Voltage	X	X	X ¹	X ^{1, 2}
MPU Serial Interface	X	X	X	X ²
2nd LO Oscillator	X	X	X	
MPU Clock Output	X	X	X	
RF Receiver and 1st LO VCO	X	X		
R _X PLL	X	X		
Carrier Detect	X	X		
Data Amp	X	X		
Low Battery Detect	X	X		
T _X PLL	X			
R _X and T _X Audio Paths	X			

NOTE: 15. In Standby and Inactive Modes, "PLL V_{ref}" remains powered but is not regulated. It will fluctuate with V_{CC}.

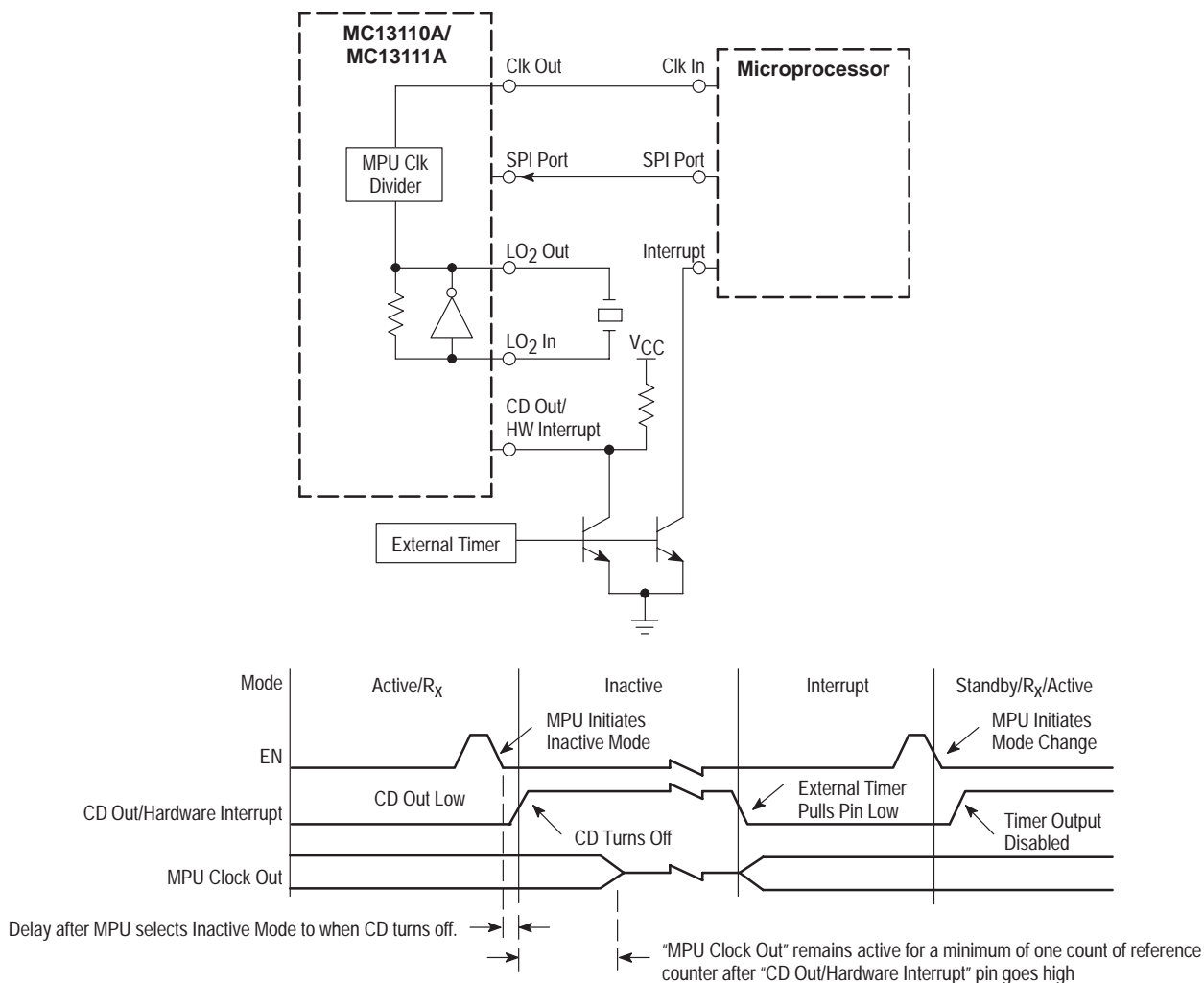
Power Saving Application

In some handset applications it may be desirable to power down all circuitry including the microprocessor (MPU). First put the MC13110A/MC13111A into the Inactive mode. This turns off the MPU Clock Output (see Figure 119) and disables the microprocessor. Once a command is given to switch the IC into an "Inactive" mode, the MPU Clock output will remain active for a minimum of one reference counter cycle (about 200 μs) and up to a maximum of two reference counter cycles (about 400 μs). This is performed in order to give the MPU adequate time to power down.

An external timing circuit should be used to initiate the turn-on sequence. The "CD Out" pin has a dual function. In the Active and R_X modes it performs the carrier detect function. In the Standby and Inactive modes the carrier detect circuit is disabled and the "CD Out" pin is in a "High" state, because of an external pull-up resistor. In the Inactive mode, the "CD Out" pin is the input for the hardware interrupt function. When the "CD Out" pin is pulled "low", by the external timing circuit, the IC switches from the Inactive to the Interrupt mode. Thereby turning on the MPU Clock Output. The MPU can then resume control of the IC. The "CD Out" pin must remain low until the MPU changes the operating mode from Interrupt to Standby, Active, or R_X modes.

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Figure 119. Power Saving Application



MPU "Clk Out" Divider Programming

The "Clk Out" signal is derived from the second local oscillator. It can be used to drive a microprocessor (MPU) clock input. This will eliminate the need for a separate crystal to drive the MPU, thus reducing system cost. Figure 120 shows the relationship between the second LO crystal frequency and the

clock output for each divide value. Figure 121 shows the "Clk Out" register bit values. With a 10.24 MHz crystal, the divide by 312.5 gives the same clock frequency as a clock crystal and allows the MPU to display the time on a LCD display without additional external components.

Figure 120. Clock Output Values

Crystal Frequency	Clock Output Divider							
	2	2.5	3	4	5	20	80	312.5
10.24 MHz	5.120 MHz	4.096 MHz	3.413 MHz	2.560 MHz	2.048 MHz	512 kHz	128 kHz	32.768 kHz
11.15 MHz	5.575 MHz	4.460 MHz	3.717 MHz	2.788 MHz	2.230 MHz	557 kHz	139 kHz	35.680 kHz
12.00 MHz	6.000 MHz	4.800 MHz	4.000 MHz	3.000 MHz	2.400 MHz	600 kHz	150 kHz	38.400 kHz

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Figure 121. Clock Output Divider

MPU Clk Bit #2	MPU Clk Bit #1	MPU Clk Bit #0	Clk Out Divider Value
0	0	0	2
0	0	1	3
0	1	0	4
0	1	1	5
1	0	0	2.5
1	0	1	20
1	1	0	80
1	1	1	312.5

MPU "Clk Out" Power-Up Default Divider Value

The power-up default divider value is "divide by 5". This provides a MPU clock of about 2.0 MHz after initial power-up. The reason for choosing a relatively low clock frequency at initial power-up is because some microprocessors operate using a 3.0 V power supply and have a maximum clock frequency of 2.0 MHz. After initial power-up, the MPU can change the clock divider value and set the clock to the desired operating frequency. Special care was taken in the design of the clock divider to insure that the

transition between one clock divider value and another is "smooth" (i.e. there will be no narrow clock pulses to disturb the MPU).

MPU "Clk Out" Radiated Noise on Circuit Board

The clock line running between the MC13110A or MC13111A and the microprocessor has the potential to radiate noise. Problems in the system can occur, especially if the clock is a square wave digital signal with large high frequency harmonics. In order to minimize the radiated noise, a 1000 Ω resistor is included on-chip in series with the "Clk Out" output driver. A small capacitor or inductor with a capacitor can be connected to the "Clk Out" line on the PCB to form a one or two pole low pass filter. This filter should significantly reduce noise radiated by attenuating the high frequency harmonics on the signal line. The filter can also be used to attenuate the signal level so that it is only as large as required by the MPU clock input. To further reduce radiated noise, the PCB signal trace length should be kept to a minimum.

Volume Control Programming

The volume control adjustable gain block can be programmed in 2 dB gain steps from -14 dB to +16 dB. The power-up default value for the MC13110A and MC13111A is 0 dB. (see Figure 122)

Figure 122. Volume Control

Volume Control Bit #3	Volume Control Bit #2	Volume Control Bit #1	Volume Control Bit #0	Volume Control #	Gain/Attenuation Amount
0	0	0	0	0	-14 dB
0	0	0	1	1	-12 dB
0	0	1	0	2	-10 dB
0	0	1	1	3	-8 dB
0	1	0	0	4	-6 dB
0	1	0	1	5	-4 dB
0	1	1	0	6	-2 dB
0	1	1	1	7	0 dB
1	0	0	0	8	2 dB
1	0	0	1	9	4 dB
1	0	1	0	10	6 dB
1	0	1	1	11	8 dB
1	1	0	0	12	10 dB
1	1	0	1	13	12 dB
1	1	1	0	14	14 dB
1	1	1	1	15	16 dB

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Gain Control Register

The gain control register contains bits which control the T_X Voltage Gain, R_X Voltage Gain, and Carrier Detect threshold. Operation of these latch bits are explained in Figures 123, 124 and 125.

T_X and R_X Gain Programming

The T_X and R_X audio signal paths each have a programmable gain block. If a T_X or R_X voltage gain, other

than the nominal power-up default, is desired, it can be programmed through the MPU interface. Alternately, these programmable gain blocks can be used during final test of the telephone to electronically adjust for gain tolerances in the telephone system (see Figure 124). In this case, the T_X and R_X gain register values should be stored in ROM during final test so that they can be reloaded each time the IC is powered up.

Figure 123. Gain Control Latch Bits

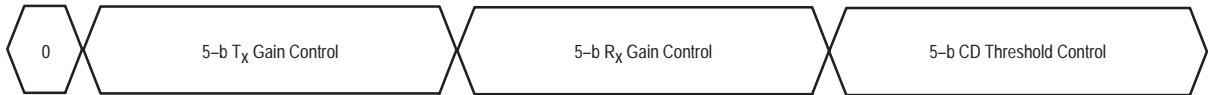


Figure 124. T_X and R_X Gain Control

Gain Control Bit #4	Gain Control Bit #3	Gain Control Bit #2	Gain Control Bit #1	Gain Control Bit #0	Gain Control #	Gain/Attenuation Amount
–	–	–	–	–	<6	–9 dB
0	0	1	1	0	6	–9 dB
0	0	1	1	1	7	–8 dB
0	1	0	0	0	8	–7 dB
0	1	0	0	1	9	–6 dB
0	1	0	1	0	10	–5 dB
0	1	0	1	1	11	–4 dB
0	1	1	0	0	12	–3 dB
0	1	1	0	1	13	–2 dB
0	1	1	1	0	14	–1 dB
0	1	1	1	1	15	0 dB
1	0	0	0	0	16	1 dB
1	0	0	0	1	17	2 dB
1	0	0	1	0	18	3 dB
1	0	0	1	1	19	4 dB
1	0	1	0	0	20	5 dB
1	0	1	0	1	21	6 dB
1	0	1	1	0	22	7 dB
1	0	1	1	1	23	8 dB
1	1	0	0	0	24	9 dB
1	1	0	0	1	25	10 dB
–	–	–	–	–	>25	10 dB

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Carrier Detect Threshold Programming

The "CD Out" pin gives an indication to the microprocessor if a carrier signal is present on the selected channel. The nominal value and tolerance of the carrier detect threshold is given in the carrier detect specification section of this document. If a different carrier detect threshold value is desired, it can be programmed through the MPU interface as shown in Figure 125 below. Alternately, the carrier detect threshold can be electronically adjusted during final test of the telephone to reduce the tolerance of the carrier detect

threshold. This is done by measuring the threshold and then by adjusting the threshold through the MPU interface. In this case, it is necessary to store the carrier detect register value in ROM so that the CD register can be reloaded each time the combo IC is powered up. If a preamp is used before the first mixer it may be desirable to scale the carrier detect range by connecting an external resistor from the "RSSI" pin to ground. The internal resistor is 187 kΩ.

Figure 125. Carrier Detect Threshold Control

CD Bit #4	CD Bit #3	CD Bit #2	CD Bit #1	CD Bit #0	CD Control #	Carrier Detect Threshold
0	0	0	0	0	0	-20 dB
0	0	0	0	1	1	-19 dB
0	0	0	1	0	2	-18 dB
0	0	0	1	1	3	-17 dB
0	0	1	0	0	4	-16 dB
0	0	1	0	1	5	-15 dB
0	0	1	1	0	6	-14 dB
0	0	1	1	1	7	-13 dB
0	1	0	0	0	8	-12 dB
0	1	0	0	1	9	-11 dB
0	1	0	1	0	10	-10 dB
0	1	0	1	1	11	-9 dB
0	1	1	0	0	12	-8 dB
0	1	1	0	1	13	-7 dB
0	1	1	1	0	14	-6 dB
0	1	1	1	1	15	-5 dB
1	0	0	0	0	16	-4 dB
1	0	0	0	1	17	-3 dB
1	0	0	1	0	18	-2 dB
1	0	0	1	1	19	-1 dB
1	0	1	0	0	20	0 dB
1	0	1	0	1	21	1 dB
1	0	1	1	0	22	2 dB
1	0	1	1	1	23	3 dB
1	1	0	0	0	24	4 dB
1	1	0	0	1	25	5 dB
1	1	0	1	0	26	6 dB
1	1	0	1	1	27	7 dB
1	1	1	0	0	28	8 dB
1	1	1	0	1	29	9 dB
1	1	1	1	0	30	10 dB
1	1	1	1	1	31	11 dB

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Clock Divider/Voltage Adjust Register

This register controls the divider value for the programmable switched capacitor filter clock divider, the low battery detect threshold select, the voltage reference adjust, and the scrambler bypass mode (MC13110A only). Operation is explained in Figures 126 through 133. Figure 128 describes the operation of the Tx and Rx Audio bits. Note the power-up default bit is set to <0>, which is the scrambler bypass mode.

Low Battery Detect

The low battery detect circuit can be operated in programmable and non-programmable threshold modes.

The non-programmable threshold mode is only available in the 52 QFP package. In this mode, there are two low battery detect comparators and the threshold values are set by external resistor dividers which are connected to the REF1 and REF2 pins. In the programmable threshold mode, several different threshold levels may be selected through the “Low Battery Detect Threshold Register” as shown in Figure 127. The power-on default value for this register is <0,0,0> and is the non-programmable mode. Figure 129 shows equivalent schematics for the programmable and non-programmable operating modes.

Figure 126. Clock Divider/Voltage Adjust Latch Bits

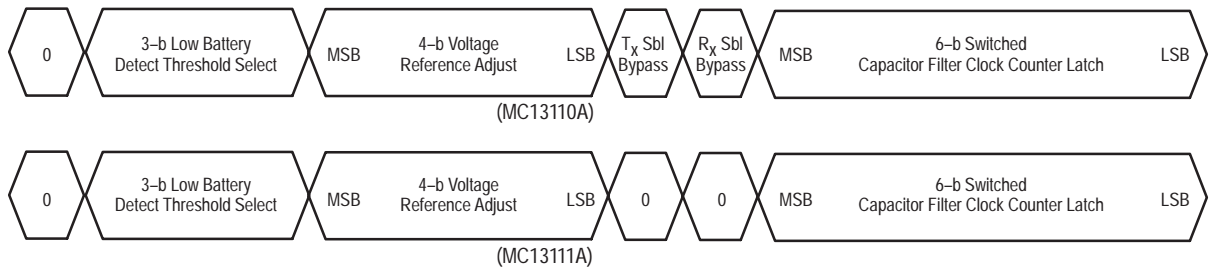


Figure 127. Low Battery Detect Threshold Selection

Low Battery Detect Threshold Select Bit #2	Low Battery Detect Threshold Select Bit #1	Low Battery Detect Threshold Select Bit #0	Select #	Operating Mode	Nominal Low Battery Detect Threshold Value (V)
0	0	0	0	Non-Programmable	N/A
0	0	1	1	Programmable	2.850
0	1	0	2	Programmable	2.938
0	1	1	3	Programmable	3.025
1	0	0	4	Programmable	3.200
1	0	1	5	Programmable	3.288
1	1	0	6	Programmable	3.375
1	1	1	7	Programmable	3.463

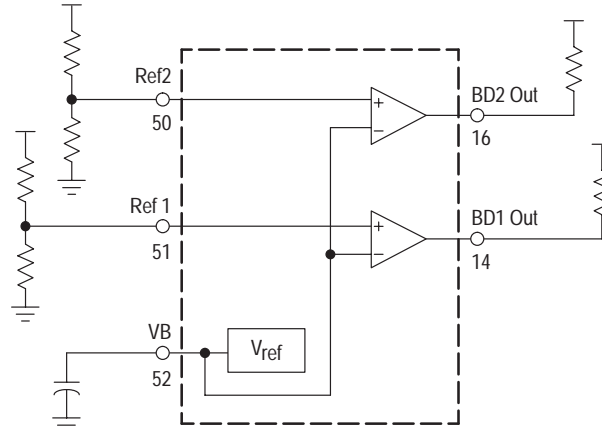
NOTE: 17. Nominal Threshold Value is before electronic adjustment.

Figure 128. MC13110A Bypass Mode Bit Description (MC13110A Only)

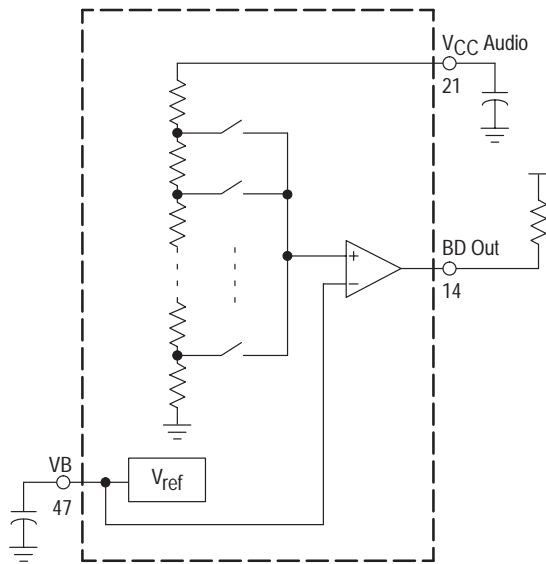
T _x Scrambler Bypass	1	T _x Scrambler Post-Mixer LPF and Mixer Bypassed
	0	Normal Operation with T _x Scrambler
R _x Scrambler Bypass	1	R _x Scrambler Post-Mixer LPF and Mixer Bypassed
	0	Normal Operation R _x Scrambler

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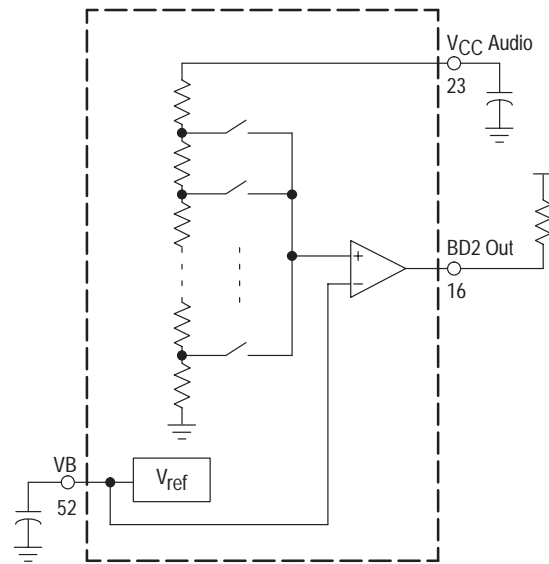
Figure 129. Low Battery Detect Equivalent Schematics



Non-Programmable Threshold Mode: 52-QFP Package



Programmable Threshold Mode: 48-LQFP Package



Programmable Threshold Mode: 52-QFP Package

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Voltage Reference Adjustment

An internal 1.5 V bandgap voltage reference provides the voltage reference for the “BD₁ Out” and “BD₂ Out” low battery detect circuits, the “PLL V_{ref}” voltage regulator, the “V_B” reference, and all internal analog ground references. The initial tolerance of the bandgap voltage reference is ±6%. The tolerance of the internal reference voltage can be improved to ±1.5% through MPU serial interface programming. During final test of the telephone, the battery detect threshold is measured. Then, the internal reference voltage value is adjusted electronically through the MPU serial interface to achieve the desired accuracy level. The voltage reference register value should be stored in ROM during final test so that it can be reloaded each time the MC13110A or MC13111A is powered up (see Figure 130).

Figure 130. Bandgap Voltage Reference Adjustment

V _{ref} Adj. Bit #3	V _{ref} Adj. Bit #2	V _{ref} Adj. Bit #1	V _{ref} Adj. Bit #0	V _{ref} Adj. #	V _{ref} Adj. Amount
0	0	0	0	0	-9.0%
0	0	0	1	1	-7.8%
0	0	1	0	2	-6.6%
0	0	1	1	3	-5.4%
0	1	0	0	4	-4.2%
0	1	0	1	5	-3.0%
0	1	1	0	6	-1.8%
0	1	1	1	7	-0.6%
1	0	0	0	8	+0.6%
1	0	0	1	9	+1.8%
1	0	1	0	10	+3.0%
1	0	1	1	11	+4.2%
1	1	0	0	12	+5.4%
1	1	0	1	13	+6.6%
1	1	1	0	14	+7.8%
1	1	1	1	15	+9.0%

Switched Capacitor Filter Clock Programming

A block diagram of the switched capacitor filter clock divider is shown in Figure 131. There is a fixed divide by 2 after the programmable divider. The switched capacitor filter clock value is given by the following equation;

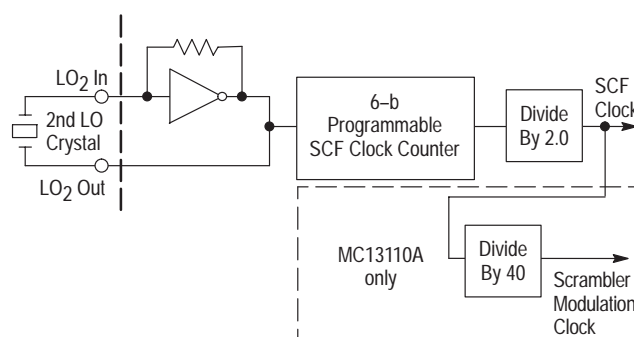
$$(\text{SCF Clock}) = F(2\text{nd LO}) / (\text{SCF Divider Value} * 2).$$

The scrambler modulation clock frequency (SMCF) is proportional to the SCF clock. The following equation defines its value:

$$\text{SMCF} = (\text{SCF Clock})/40$$

The SCF divider should be set to a value which brings the SCF Clock as close to 165.16 kHz as possible. This is based on the 2nd LO frequency which is chosen in Figure 114.

Figure 131. SCF Clock Divider Circuit



Corner Frequency Programming for MC13110A and MC13111A

Four different corner frequencies may be selected by programming the SCF Clock divider as shown in Figures 132 and 133. It is important to note, that all filter corner frequencies will change proportionately with the SCF Clock Frequency and Scrambler Modulation Frequency. The power-up default SCF Clock divider value is 31.

Figure 132. Corner Frequency Programming for 10.240 MHz 2nd LO

MC13110A							
MC13111A							
SCF Clock Divider	Total Divide Value	SCF Clock Freq. (kHz)	R _x Upper Corner Frequency (kHz)	T _x Upper Corner Frequency (kHz)	Scrambler Modulation Frequency (Clk/40) (kHz)	Scrambler Lower Corner Frequency (Hz)	Scrambler Upper Corner Frequency (kHz)
29	58	176.55	4.147	3.955	4.414	267.2	3.902
30	60	170.67	4.008	3.823	4.267	258.3	3.772
31	62	165.16	3.879	3.700	4.129	250.0	3.650
32	64	160.00	3.758	3.584	4.000	242.2	3.536

NOTE: 18. All filter corner frequencies have a tolerance of ±3%.

19. R_x and T_x Upper Corner Frequencies are the same corner frequencies for the MC13110A in scrambler bypass

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Figure 133. Corner Frequency Programming for 11.15 MHz 2nd LO

MC13110A							
MC13111A							
SCF Clock Divider	Total Divide Value	SCF Clock Freq. (kHz)	R _x Upper Corner Frequency (kHz)	T _x Upper Corner Frequency (kHz)	Scrambler Modulation Frequency (Clk/40) (kHz)	Scrambler Lower Corner Frequency (Hz)	Scrambler Upper Corner Frequency (kHz)
32	64	174.22	4.092	3.903	4.355	263.7	3.850
33	66	168.94	3.968	3.785	4.223	255.7	3.733
34	68	163.97	3.851	3.673	4.099	248.2	3.624
35	70	159.29	3.741	3.568	3.982	241.1	3.520

NOTES: 20. All filter corner frequencies have a tolerance of $\pm 3\%$.
 21. R_x and T_x Upper Corner Frequencies are the same corner frequencies for the MC13110A in scrambler bypass

Figure 134. Auxiliary Register Latch Bits



Figure 135. Digital Test Mode Description

TM #	TM 2	TM 1	TM 0	Counter Under Test or Test Mode Option	"T _x VCO" Input Signal	"Clk Out" Output Expected
0	0	0	0	Normal Operation	>200 mVpp	–
1	0	0	1	R _x Counter	0 to 2.5 V	Input Frequency/R _x Counter Value
2	0	1	0	T _x Counter	0 to 2.5 V	Input Frequency/T _x Counter Value
3	0	1	1	Reference Counter + Divide by 4/25	0 to 2.5 V	Input Frequency/Reference Counter Value * 100
4	1	0	0	SC Counter	0 to 2.5 V	Input Frequency/SC Counter Value * 2
5	1	0	1	ALC Gain = 10 Option	N/A	N/A
6	1	1	0	ALC Gain = 25 Option	N/A	N/A

Auxiliary Register

The auxiliary register contains a 4-bit First LO Capacitor Selection latch and a 3-bit Test Mode latch. Operation of these latch bits are explained in Figures 134, 135 and 136.

Test Modes

Test modes are selected through the 3-bit Test Mode Register. In test mode, the "T_x VCO" input pin is multiplexed to the input of the counter under test. The output of the counter under test is multiplexed to the "Clk Out" output pin so that each counter can be individually tested. **Make sure test mode bits are set to "0's" for normal operation.** Test mode operation is described in Figure 135. During normal operation, the "T_x VCO" input can be a minimum of 200 mVpp at 80 MHz and should be AC coupled. Input signals should be standard logic levels of 0 to 2.5 V and a maximum frequency of 16 MHz.

First Local Oscillator Programmable Capacitor Selection

There is a very large frequency difference between the minimum and maximum channel frequencies in the 25 Channel U.S. standard. The internal varactor adjustment

range is not large enough to accommodate this large frequency span. An internal capacitor with 15 programmable capacitor values can be used to cover the 25 channel frequency span without the need to add external capacitors and switches. The programmable internal capacitor can also be used to eliminate the need to use an external variable capacitor to adjust the 1st LO center frequency during telephone assembly. Figure 32 shows the schematic of the 1st LO tank circuit. Figure 136 shows the register control bit values.

The internal programmable capacitor is composed of a matrix bank of capacitors that are switched in as desired. Programmable capacitor values between about 0 and 16 pF can be selected in steps of approximately 1.1 pF. The internal parallel resistance values in the table can be used to calculate the quality factor (Q) of the oscillator if the Q of the external inductor is known. The temperature coefficient of the varactor is 0.08%/°C. The temperature coefficient of the internal programmable capacitor is negligible. Tolerance on the varactor and programmable capacitor values is $\pm 15\%$.

MC13110A MC13111A

Figure 136. First Local Oscillator Internal Capacitor Selection

1st LO Cap. Bit 3	1st LO Cap. Bit 2	1st LO Cap. Bit 1	1st LO Cap. Bit 0	1st LO Cap. Select	Internal Programmable Capacitor Value (pF)	Varactor Value over 0.3 to 2.5 V (pF)	Equivalent Internal Parallel Resistance at 40 MHz (kΩ)	Equivalent Internal Parallel Resistance at 51 MHz (kΩ)
0	0	0	0	0	0.0	9.7 to 5.8	1200	736
0	0	1	0	2	0.6	9.7 to 5.8	79.3	48.8
0	0	0	1	1	1.7	9.7 to 5.8	131	80.8
0	1	0	1	5	2.8	9.7 to 5.8	31.4	19.3
0	1	1	0	6	3.9	9.7 to 5.8	33.8	20.8
0	1	1	1	7	4.9	9.7 to 5.8	66.6	41
0	1	0	0	4	6.0	9.7 to 5.8	49.9	30.7
0	0	1	1	3	7.1	9.7 to 5.8	40.7	25.1
1	0	0	0	8	8.2	9.7 to 5.8	27.1	16.7
1	0	0	1	9	9.4	9.7 to 5.8	21.6	13.3
1	0	1	0	10	10.5	9.7 to 5.8	20.5	12.6
1	0	1	1	11	11.6	9.7 to 5.8	18.6	11.5
1	1	0	0	12	12.7	9.7 to 5.8	17.2	10.6
1	1	0	1	13	13.8	9.7 to 5.8	15.8	9.7
1	1	1	0	14	14.9	9.7 to 5.8	15.3	9.4
1	1	1	1	15	16.0	9.7 to 5.8	14.2	8.7

MC13110A MC13111A

OTHER APPLICATIONS INFORMATION

PCB Board Lay-Out Considerations

The ideal printed circuit board (PCB) lay out would be double-sided with a full ground plane on one side. The ground plane would be divided into separate sections to prevent any audio signal from feeding into the first local oscillator via the ground plane. Leaded components, can likewise, be inserted on the ground plane side to improve shielding and isolation from the circuit side of the PCB. The opposite side of the PCB is typically the circuit side. It has the interconnect traces and surface mount components. In cases where cost allows, it may be beneficial to use multi-layer boards to further improve isolation of components and sensitive sections (i.e. RF and audio). For the CT-0 band, it is also permissible to use single-sided PC layouts, but with continuous full ground fill in and around the components.

The proper placement of certain components specified in the application circuit may be very critical. In a lay-out design, these components should be placed before the other less critical components are inserted. It is also imperative that all RF paths be kept as short as possible. Finally, the MC13110A and MC13111A ground pins should be tied to ground at the pins and VCC pins should have adequate decoupling to ground as close to the IC as possible. In mixed mode systems where digital and RF/Analog circuitry are present, the VCC and VEE buses need to be ac-decoupled and isolated from each other. The design must also take great caution to avoid interference with low level analog circuits. The receiver can be particularly susceptible to interference as they respond to signals of only a few microvolts. Again, be sure to keep the dc supply lines for the digital and analog portions separate. Avoid ground paths carrying common digital and analog currents, as well.

Component Selection

The evaluation circuit schematics specify particular components that were used to achieve the results shown in the typical curves and tables, but alternate components should give similar results. The MC13110A and MC13111A IC are capable of matching the sensitivity, IMD, adjacent channel rejection, and other performance criteria of a multi-chip analog cordless telephone system. For the most part, the same external components are used as in the multi-chip solution.

VB and PLL V_{ref}

VB is an internally generated bandgap voltage. It functions as an ac reference point for the operational amplifiers in the audio section as well as for the battery detect circuitry. This pin needs to be sufficiently filtered to reduce noise and prevent crosstalk between R_x audio to T_x audio signal paths. A practical capacitor range to choose that will minimize crosstalk and noise relative to start up time is 0.5 μ F to 10 μ F. The start time for a 0.5 μ F capacitor is approximately 5.0 ms, while a 10 μ F capacitor is about 10 ms.

The "PLL V_{ref}" pin is the internal supply voltage for the R_x and T_x PLL's. It is regulated to a nominal 2.5 V. The "VCC Audio" pin is the supply voltage for the internal voltage regulator. Two capacitors with 10 μ F and 0.01 μ F values must be connected to the "PLL V_{ref}" pin to filter and stabilize this regulated voltage. The "PLL V_{ref}" pin may be used to power other IC's as long as the total external load current does not exceed 1.0 mA. The tolerance of the regulated voltage is initially \pm 8.0%, but is improved to \pm 4.0% after the internal Bandgap voltage reference is adjusted electronically through the MPU serial interface. The voltage regulator is turned off in the Standby and Inactive modes to reduce current drain. In these modes, the "PLL V_{ref}" pin is internally connected to the "VCC Audio" pin (i.e., the power supply voltage is maintained but is now unregulated).

It is important to note that the momentary drop in voltage below 2.5 V during this transition may affect initial PLL lock times and also may trigger the reset. To prevent this, the PLL V_{ref} capacitor described above should be kept the same or larger than the VB capacitor, say 10 μ F as shown in the evaluation and application diagrams.

DC Coupling

Choosing the right coupling capacitors for the compander is also critical. The coupling capacitors will have an effect on the audio distortion, especially at lower audio frequencies. A useful capacitor range for the compander timing capacitors is 0.1 μ F to 1.0 μ F. It is advised to keep the compander capacitors the same value in both the handset and baserset applications.

All other dc coupling capacitors in the audio section will form high pass filters. The designer should choose the overall cut off frequency (-3.0 dB) to be around 200 Hz. Designing for lower cut off frequencies may add unnecessary cost and capacitor size to the design, while selecting too high of a cut off frequency may affect audio quality. It is not necessary or advised to design each audio coupling capacitors for the same cut off frequency. Design for the overall system cut off frequency. (Note: Do not expect the application, evaluation, nor production test schematics to necessarily be the correct capacitor selections.) The goals of these boards may be different than the systems approach a designer must consider.

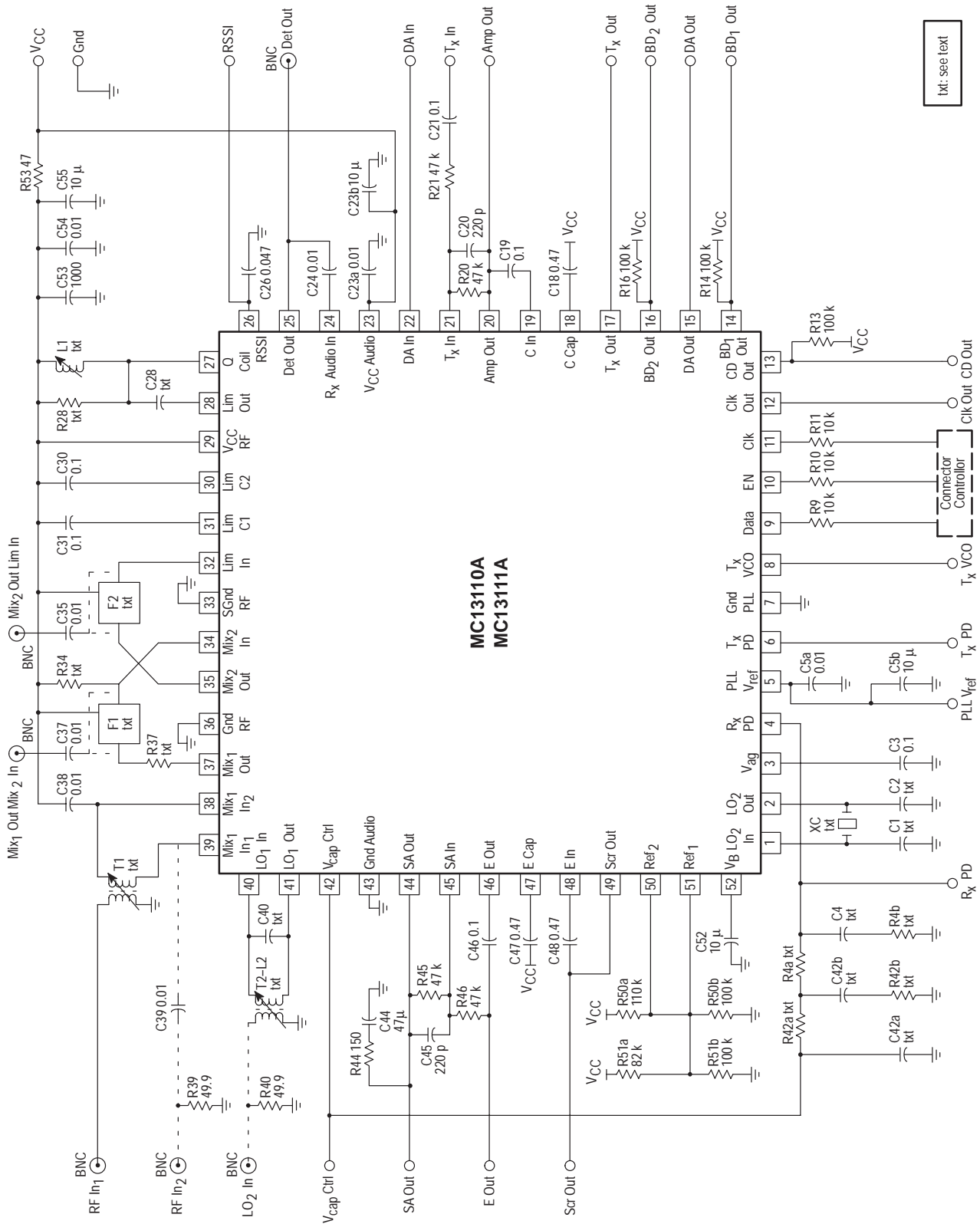
For the supply pins (VCC Audio and VCC RF) choose a 10 μ F in parallel with a high quality 0.01 μ F capacitor. Separation of these two supply planes is essential, too. This is to prevent interference between the RF and audio sections. It is always a good design practice to add additional coupling on each supply plane to ground as well.

The IF limiter capacitors are recommended to be 0.1 μ F. Smaller values lower the gain of the limiter stage. The -3.0 dB limiting sensitivity and SINAD may be adversely affected.

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APPENDIX A

Figure 138. Evaluation Board Schematic



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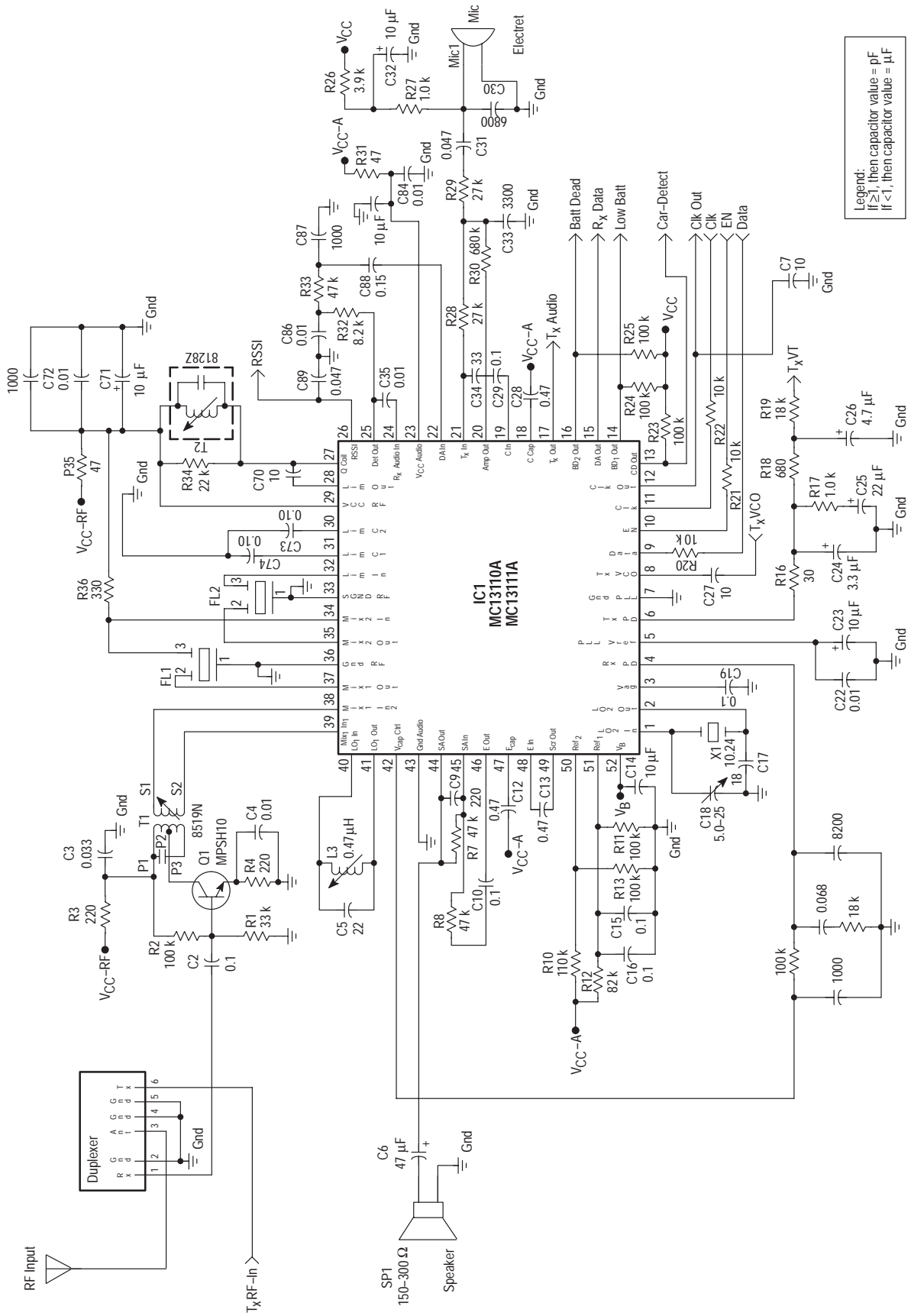
MC13110A MC13111A

APPENDIX A

Figure 138. Evaluation Board Bill of Materials for U.S. and French Application

Comp. Number	USA Application Handset		French Application Base		
	RF (50 Ω)	RF Matched	RF Crystal (50 Ω)	RF Ceramic (50 Ω)	RF Matched
INPUT MATCHING					
T1	n.m.	Toko 1:5 292GNS-765A0	n.m.	n.m.	Toko 1:5 292GNS-765A0
C38	0.01	n.m.	0.01	0.01	n.m.
C39	0.01	n.m.	0.01	0.01	n.m.
10.7 MHz FILTER					
F1	Ceramic	Ceramic	Crystal	Ceramic	Ceramic
R37	0	0	1.2 k	0	0
R34	360	360	3.01 k	360	360
450 kHz FILTER					
F2	4 Element Murata E	4 Element Murata E	4 Element Murata G	4 Element Murata G	4 Element Murata G
DEMODULATOR					
L1	Q Coil Toko 7MCS-8128Z	Q Coil Toko 7MCS-8128Z	Ceramic Murata CDBM 450C34	Ceramic Murata CDBM 450C34	Ceramic Murata CDBM 450C34
R28	22.1 k	22.1 k	2.7 k	2.7 k	2.7 k
C28	10 p	10 p	390 p	390 p	390 p
OSCILLATOR					
Xtal	10.24 C1 = 10 p	10.24 C1 = 10 p	11.15 C1 = 18 p	11.15 C1 = 18 p	11.15 C1 = 18 p
C2	18 p	18 p	33 p	33 p	33 p
C1	5-25 p	5-25 p	15 p + 5-25 p	15 p + 5-25 p	15 p + 5-25 p
FIRST LO					
L2	0.47 Toko T1370	0.47 Toko T1370	0.22 Toko T1368	0.22 Toko T1368	0.22 Toko T1368
C40 HS/BS	HS: 27 pF BS: 22 pF	HS: 27 pF BS: 22 pF	BS: 100 p HS: 68 pF	BS: 100 p HS: 68 pF	BS: 100 p HS: 68 pF
LOOP FILTER HANDSET/BASESET					
R4a	HS: 0 BS: 0	HS: 0 BS: 0	HS: 0 BS: 0	HS: 0 BS: 0	HS: 0 BS: 0
R4b	HS: 0 BS: 0	HS: 0 BS: 0	HS: 0 BS: 0	HS: 0 BS: 0	HS: 0 BS: 0
C4	HS: 6800 BS: 8200	HS: 6800 BS: 8200	HS: 8600 BS: 6800	HS: 8600 BS: 6800	HS: 8600 BS: 6800
R42a	HS: 100 k BS: 100 k	HS: 100 k BS: 100 k	HS: 100 k BS: 100 k	HS: 100 k BS: 100 k	HS: 100 k BS: 100 k
R42b	HS: 22 k BS: 18 k	HS: 22 k BS: 18 k	HS: 18 k BS: 22 k	HS: 18 k BS: 22 k	HS: 18 k BS: 22 k
C42a	HS: 1000 BS: 1000	HS: 1000 BS: 1000	HS: 1000 BS: 1000	HS: 1000 BS: 1000	HS: 1000 BS: 1000
C42b	HS: 0.068 BS: 0.082	HS: 0.068 BS: 0.082	HS: 0.082 BS: 0.068	HS: 0.082 BS: 0.068	HS: 0.082 BS: 0.068

Figure 140. Basic Cordless Telephone Transceiver Application Circuit

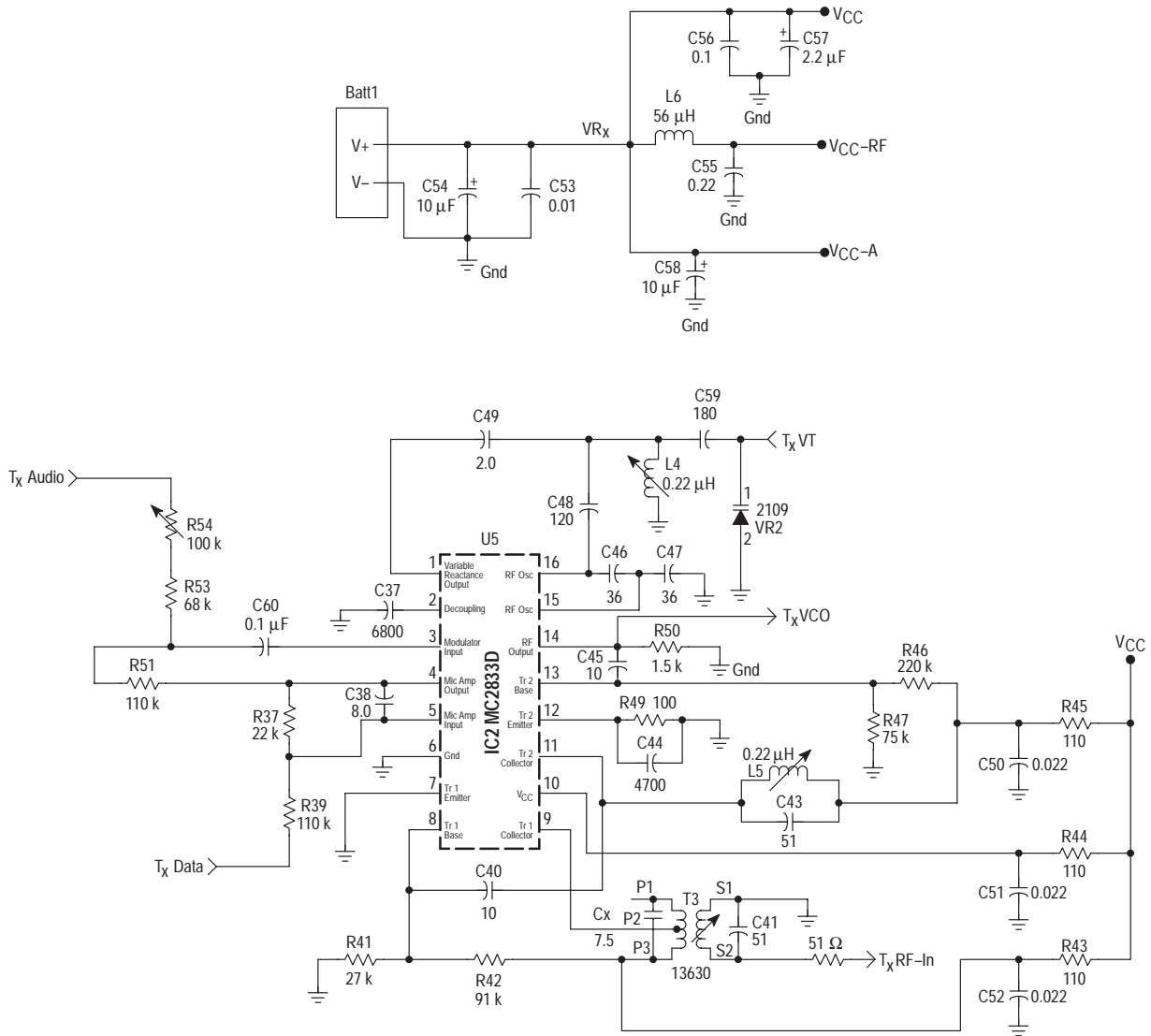


Legend:
 If ≥ 1 , then capacitor value = pF
 If < 1 , then capacitor value = μ F

MC13110A MC13111A

APPENDIX B

Figure 140. Basic Cordless Telephone Transceiver Application Circuit (continued)



MC13110A MC13111A

APPENDIX C – MEASUREMENT OF COMPANDER ATTACK/DECAY TIME

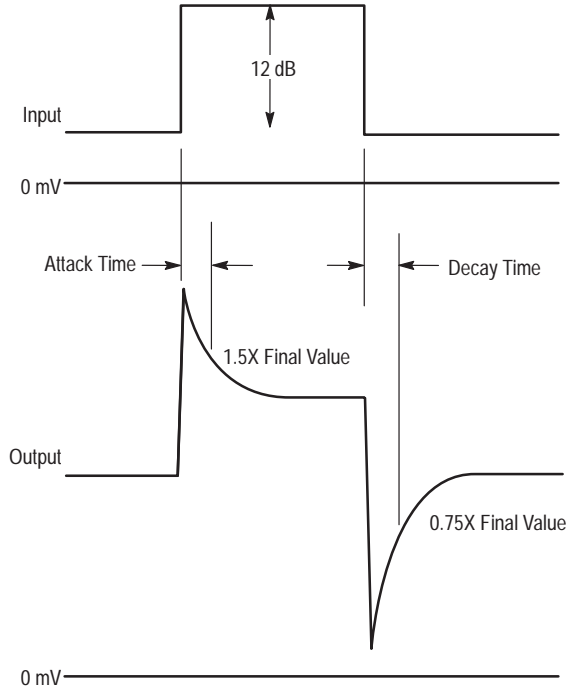
This measurement definition is based on EIA/CCITT recommendations.

Compressor Attack Time

For a 12 dB step up at the input, attack time is defined as the time for the output to settle to 1.5X of the final steady state value.

Compressor Decay Time

For a 12 dB step down at the input, decay time is defined as the time for the input to settle to 0.75X of the final steady state value.

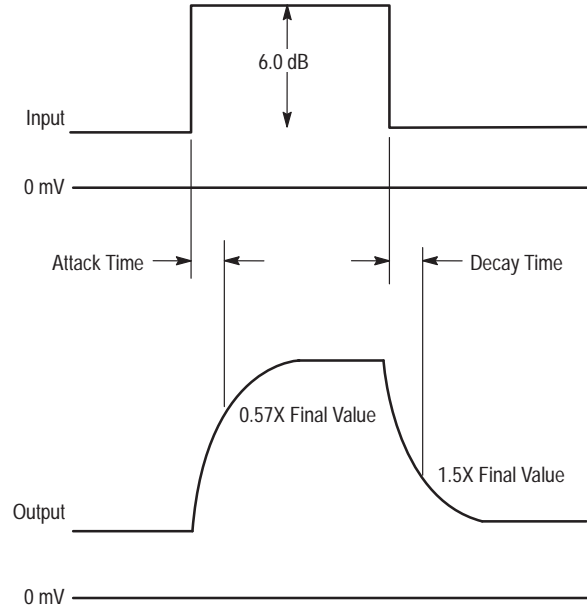


Expander Attack

For a 6.0 dB step up at the input, attack time is defined as the time for the output to settle to 0.57X of the final steady state value.

Expander Decay

For a 6.0 dB step down at the input, decay time is defined as the time for the output to settle to 1.5X of the final steady state value.





MOTOROLA

FM Communications Receivers

The MC13135/MC13136 are the second generation of single chip, dual conversion FM communications receivers developed by Motorola. Major improvements in signal handling, RSSI and first oscillator operation have been made. In addition, recovered audio distortion and audio drive have improved. Using Motorola's MOSAIC™ 1.5 process, these receivers offer low noise, high gain and stability over a wide operating voltage range.

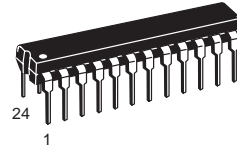
Both the MC13135 and MC13136 include a Colpitts oscillator, VCO tuning diode, low noise first and second mixer and LO, high gain limiting IF, and RSSI. The MC13135 is designed for use with an LC quadrature detector and has an uncommitted op amp that can be used either for an RSSI buffer or as a data comparator. The MC13136 can be used with either a ceramic discriminator or an LC quad coil and the op amp is internally connected for a voltage buffered RSSI output.

These devices can be used as stand-alone VHF receivers or as the lower IF of a triple conversion system. Applications include cordless telephones, short range data links, walkie-talkies, low cost land mobile, amateur radio receivers, baby monitors and scanners.

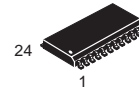
- Complete Dual Conversion FM Receiver – Antenna to Audio Output
- Input Frequency Range – 200 MHz
- Voltage Buffered RSSI with 70 dB of Usable Range
- Low Voltage Operation – 2.0 to 6.0 Vdc (2 Cell NiCad Supply)
- Low Current Drain – 3.5 mA Typ
- Low Impedance Audio Output < 25 Ω
- VHF Colpitts First LO for Crystal or VCO Operation
- Isolated Tuning Diode
- Buffered First LO Output to Drive CMOS PLL Synthesizer

MC13135 MC13136

DUAL CONVERSION NARROWBAND FM RECEIVERS



P SUFFIX
PLASTIC PACKAGE
CASE 724

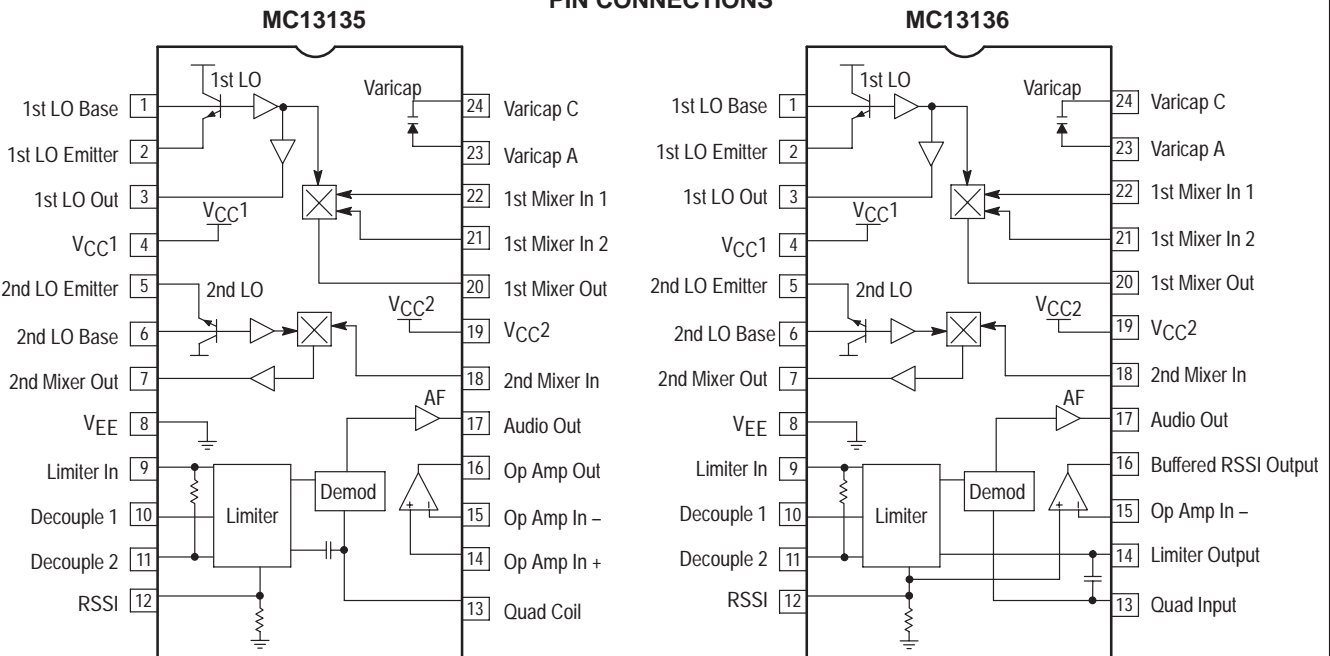


DW SUFFIX
PLASTIC PACKAGE
CASE 751E
(SO-24L)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13135P	T _A = -40° to +85°C	Plastic DIP
MC13135DW		SO-24L
MC13136DW		SO-24L

PIN CONNECTIONS



Each device contains 142 active transistors.

NOT RECOMMENDED FOR NEW DESIGNS

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MC13135 MC13136

MAXIMUM RATINGS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage	4, 19	V _{CC} (max)	6.5	Vdc
RF Input Voltage	22	RF _{in}	1.0	Vrms
Junction Temperature	–	T _J	+150	°C
Storage Temperature Range	–	T _{stg}	– 65 to +150	°C

RECOMMENDED OPERATING CONDITIONS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage	4, 19	V _{CC}	2.0 to 6.0	Vdc
Maximum 1st IF	–	f _{IF1}	21	MHz
Maximum 2nd IF	–	f _{IF2}	3.0	MHz
Ambient Temperature Range	–	T _A	– 40 to + 85	°C

ELECTRICAL CHARACTERISTICS (T_A=25°C, V_{CC}=4.0Vdc, f₀=49.7 MHz, f_{MOD}=1.0kHz, Deviation=±3.0kHz, f_{1stLO}=39MHz, f_{2ndLO}=10.245 MHz, IF1 = 10.7 MHz, IF2 = 455 kHz, unless otherwise noted. All measurements performed in the test circuit of Figure 1.)

Characteristic	Condition	Symbol	Min	Typ	Max	Unit
Total Drain Current	No Input Signal	I _{CC}	–	4.0	6.0	mAdc
Sensitivity (Input for 12 dB SINAD)	Matched Input	V _{SIN}	–	1.0	–	μVrms
Recovered Audio MC13135 MC13136	V _{RF} = 1.0 mV	A _{FO}	170 215	220 265	300 365	mVrms
Limiter Output Level (Pin 14, MC13136)		V _{LIM}	–	130	–	mVrms
1st Mixer Conversion Gain	V _{RF} = – 40 dBm	MX _{gain1}	–	12	–	dB
2nd Mixer Conversion Gain	V _{RF} = – 40 dBm	MX _{gain2}	–	13	–	dB
First LO Buffered Output	–	V _{LO}	–	100	–	mVrms
Total Harmonic Distortion	V _{RF} = – 30 dBm	THD	–	1.2	3.0	%
Demodulator Bandwidth	–	BW	–	50	–	kHz
RSSI Dynamic Range	–	RSSI	–	70	–	dB
First Mixer 3rd Order Intercept (Input)	Matched Unmatched	TOI _{Mix1}	– –	–17 –11	– –	dBm
Second Mixer 3rd Order Intercept (RF Input)	Matched Input	TOI _{Mix2}	–	–27	–	dBm
First LO Buffer Output Resistance	–	R _{LO}	–	–	–	Ω
First Mixer Parallel Input Resistance	–	R	–	722	–	Ω
First Mixer Parallel Input Capacitance	–	C	–	3.3	–	pF
First Mixer Output Impedance	–	Z _O	–	330	–	Ω
Second Mixer Input Impedance	–	Z _I	–	4.0	–	kΩ
Second Mixer Output Impedance	–	Z _O	–	1.8	–	kΩ
Detector Output Impedance	–	Z _O	–	25	–	Ω

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NOT RECOMMENDED FOR NEW DESIGNS

MC13135 MC13136

TEST CIRCUIT INFORMATION

Although the MC13136 can be operated with a ceramic discriminator, the recovered audio measurements for both the MC13135 and MC13136 are made with an LC quadrature detector. The typical recovered audio will depend on the external circuit; either the Q of the quad coil, or the RC matching network for the ceramic discriminator. On the MC13136, an external capacitor between Pins 13 and 14 can be used with a quad coil for slightly higher recovered audio. See Figures 10 through 13 for additional information.

Since adding a matching circuit to the RF input increases the signal level to the mixer, the third order intercept (TOI) point is better with an unmatched input (50 Ω from Pin 21 to Pin 22). Typical values for both have been included in the Electrical Characterization Table. TOI measurements were taken at the pins with a high impedance probe/spectrum analyzer system. The first mixer input impedance was measured at the pin with a network analyzer.

Figure 1a. MC13135 Test Circuit

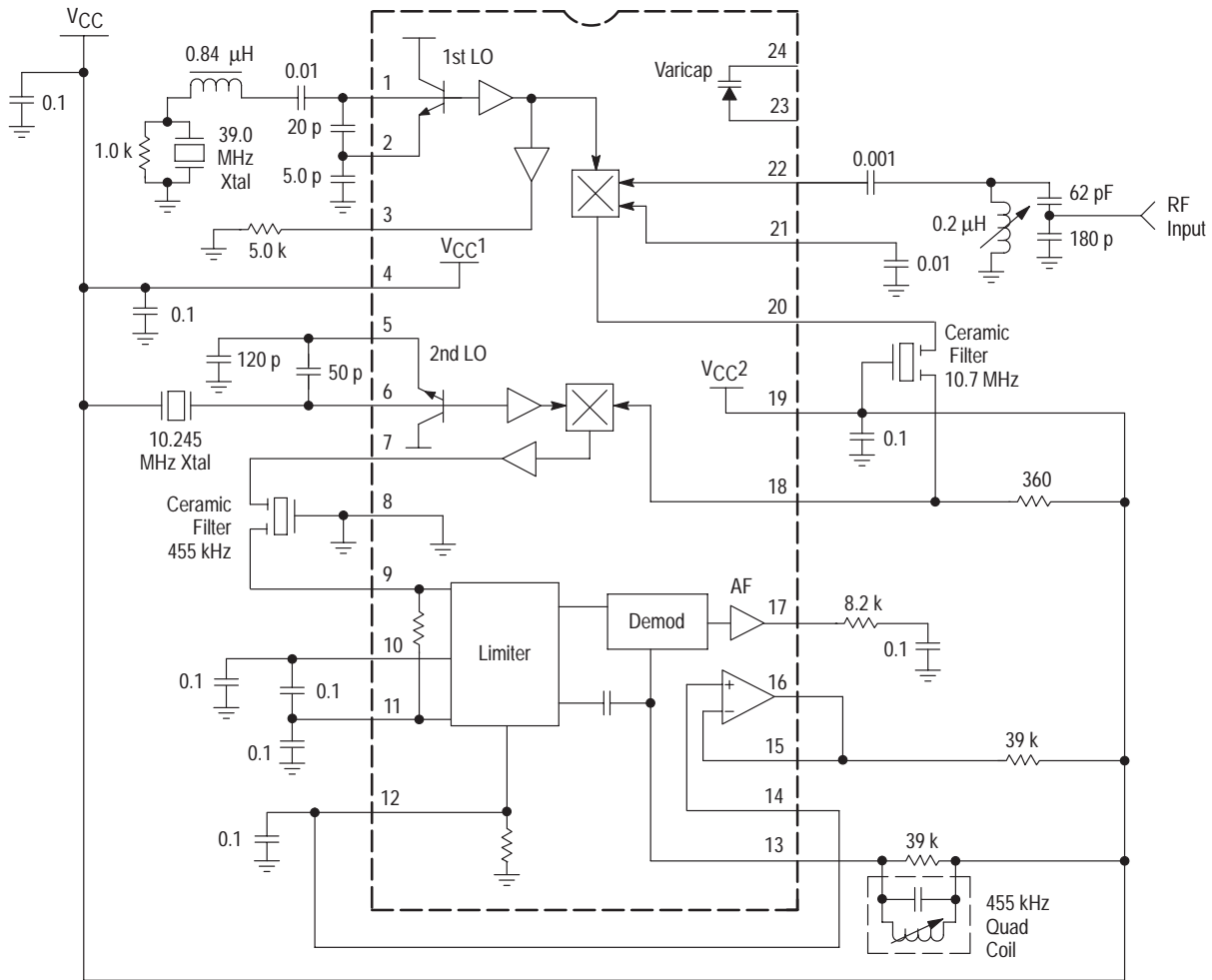
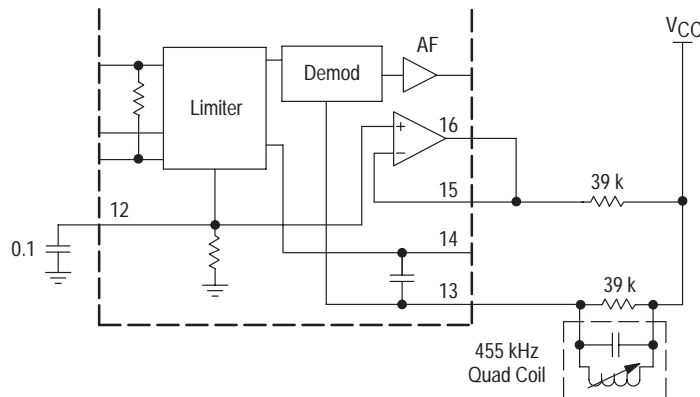


Figure 1b. MC13136 Quad Detector Test Circuit



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NOT RECOMMENDED FOR NEW DESIGNS

Figure 2. Supply Current versus Supply Voltage

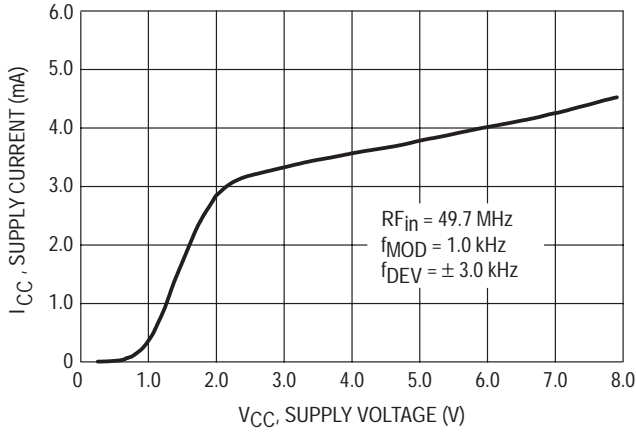


Figure 3. RSSI Output versus RF Input

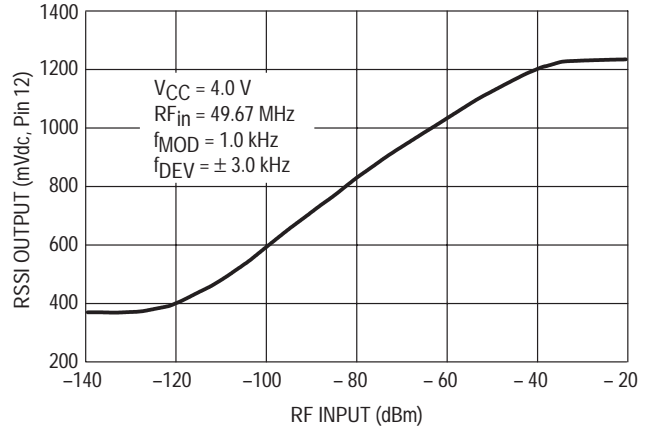


Figure 4. Varactor Capacitance, Resistance versus Bias Voltage

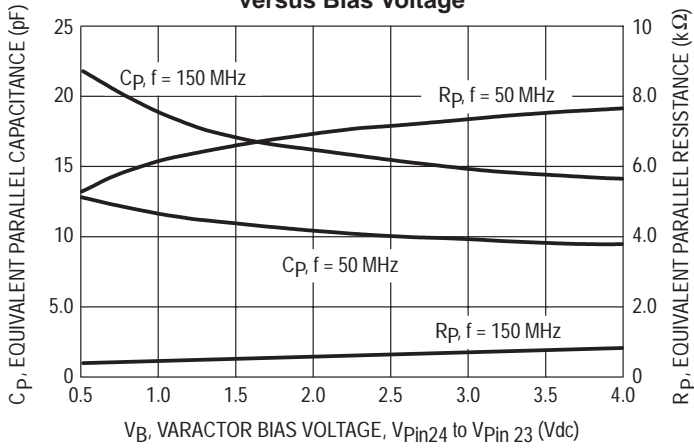


Figure 5. Oscillator Frequency versus Varactor Bias

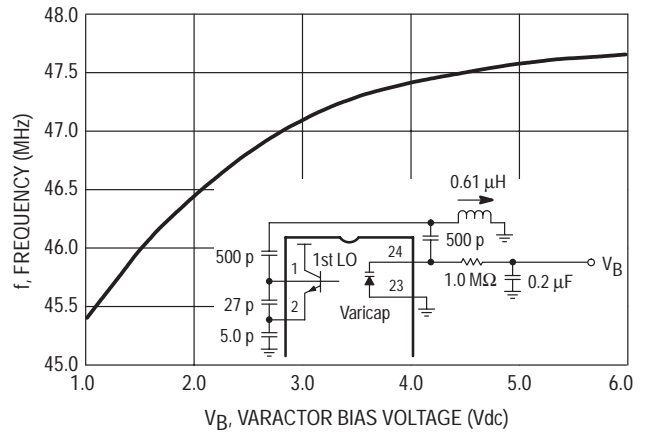


Figure 6. Signal Levels versus RF Input

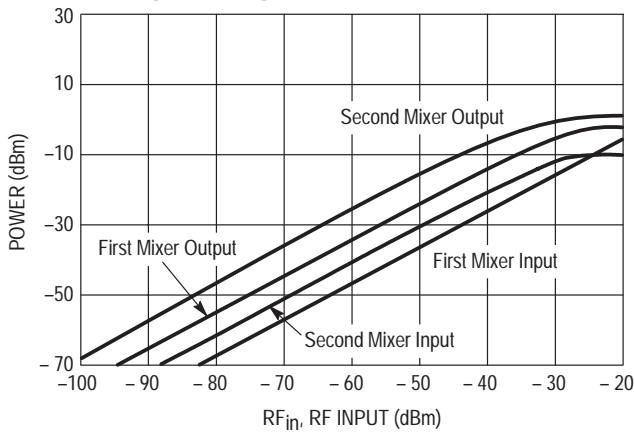
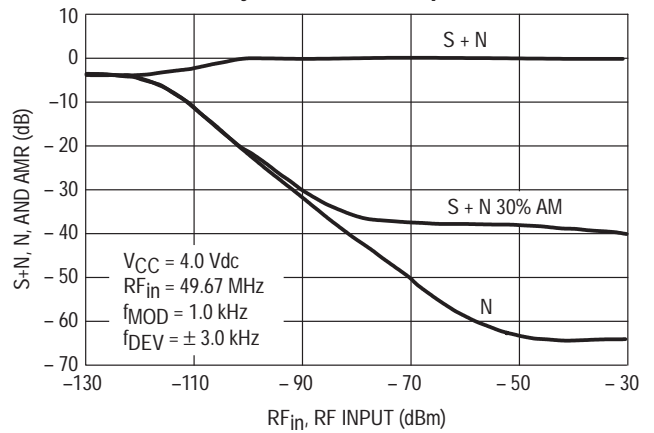


Figure 7. Signal + Noise, Noise, and AM Rejection versus Input Power



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Figure 8. Op Amp Gain and Phase versus Frequency

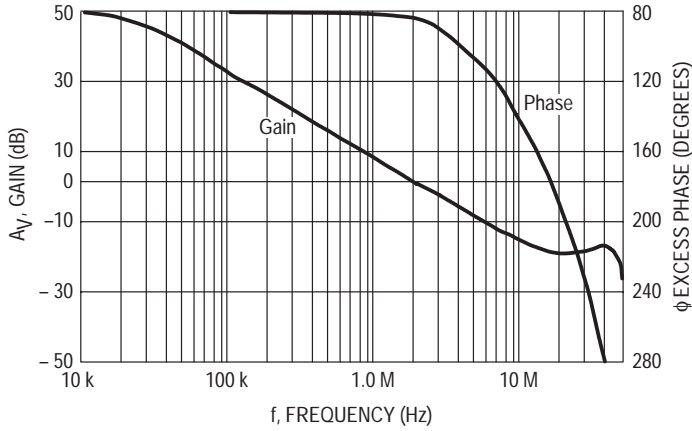


Figure 9. First Mixer Third Order Intermodulation (Unmatched Input)

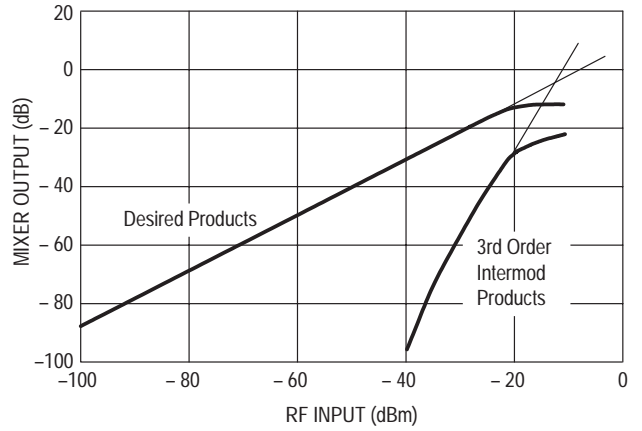


Figure 10. Recovered Audio versus Deviation for MC13135

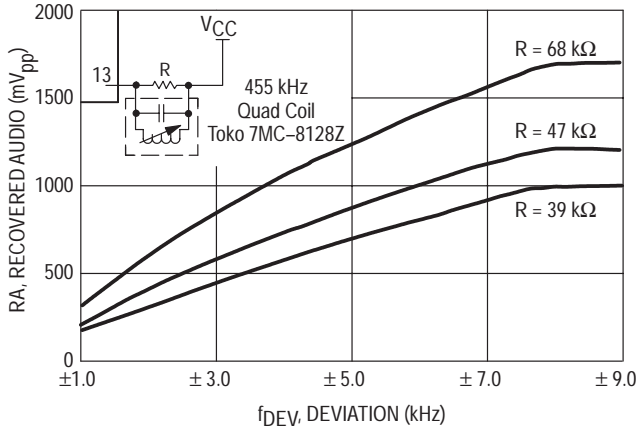


Figure 11. Distortion versus Deviation for MC13135

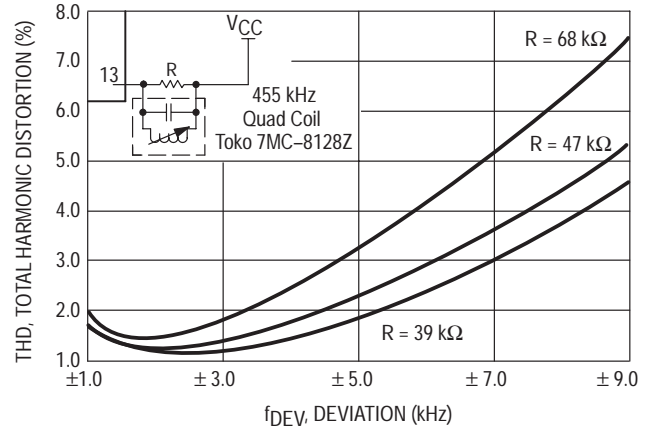


Figure 12. Recovered Audio versus Deviation for MC13136

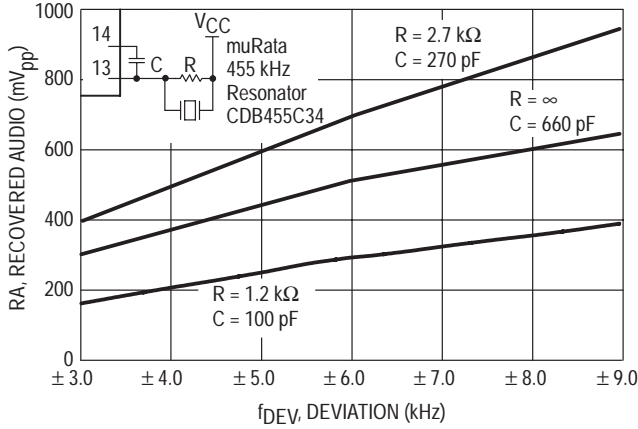
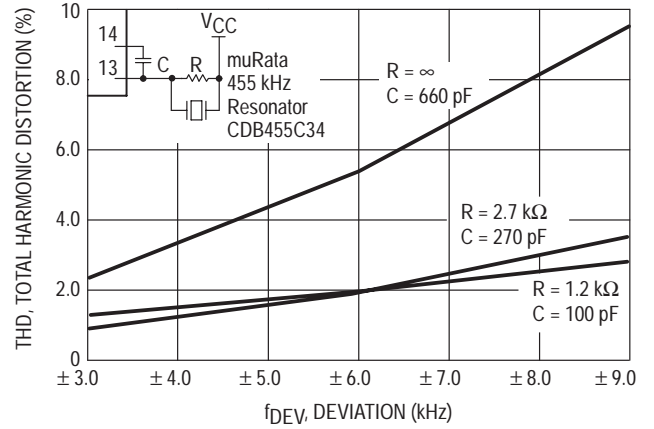


Figure 13. Distortion versus Deviation for MC13136



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13135 MC13136

CIRCUIT DESCRIPTION

The MC13135/13136 are complete dual conversion receivers. They include two local oscillators, two mixers, a limiting IF amplifier and detector, and an op amp. Both provide a voltage buffered RSSI with 70 dB of usable range, isolated tuning diode and buffered LO output for PLL operation, and a separate V_{CC} pin for the first mixer and LO. Improvements have been made in the temperature performance of both the recovered audio and the RSSI.

V_{CC}

Two separate V_{CC} lines enable the first LO and mixer to continue running while the rest of the circuit is powered down. They also isolate the RF from the rest of the internal circuit.

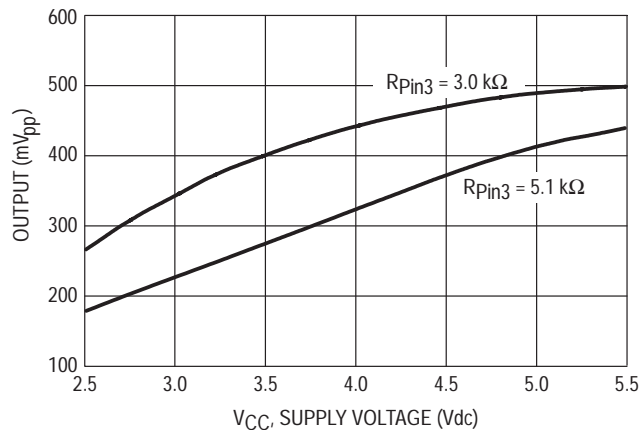
Local Oscillators

The local oscillators are grounded collector Colpitts, which can be easily crystal-controlled or VCO controlled with the on-board varactor and external PLL. The first LO transistor is internally biased, but the emitter is pinned-out and I_Q can be increased for high frequency or VCO operation. The collector is not pinned out, so for crystal operation, the LO is generally limited to 3rd overtone crystal frequencies; typically around 60 MHz. For higher frequency operation, the LO can be provided externally as shown in Figure 16.

Buffer

An amplifier on the 1st LO output converts the single-ended LO output to a differential signal to drive the mixer. Capacitive coupling between the LO and the amplifier minimizes the effects of the change in oscillator current on the mixer. Buffered LO output is pinned-out at Pin 3 for use with a PLL, with a typical output voltage of 320 mV_{pp} at $V_{CC} = 4.0$ V and with a 5.1 k resistor from Pin 3 to ground. As seen in Figure 14, the buffered LO output varies with the supply voltage and a smaller external resistor may be needed for low voltage operation. The LO buffer operates up to 60 MHz, typically. Above 60 MHz, the output at Pin 3 rolls off at approximately 6.0 dB per octave. Since most PLLs require about 200 mV_{pp} drive, an external amplifier may be required.

Figure 14. Buffered LO Output Voltage versus Supply Voltage



Mixers

The first and second mixer are of similar design. Both are double balanced to suppress the LO and input frequencies to give only the sum and difference frequencies out. This configuration typically provides 40 to 60 dB of LO suppression. New design techniques provide improved mixer linearity and third order intercept without increased noise. The gain on the output of the 1st mixer starts to roll off at about 20 MHz, so this receiver could be used with a 21 MHz first IF. It is designed for use with a ceramic filter, with an output impedance of 330 Ω . A series resistor can be used to raise the impedance for use with a crystal filter, which typically has an input impedance of 4.0 k Ω . The second mixer input impedance is approximately 4.0 k Ω ; it requires an external 360 Ω parallel resistor for use with a standard ceramic filter.

Limiting IF Amplifier and Detector

The limiter has approximately 110 dB of gain, which starts rolling off at 2.0 MHz. Although not designed for wideband operation, the bandwidth of the audio frequency amplifier has been widened to 50 kHz, which gives less phase shift and enables the receiver to run at higher data rates. However, care should be taken not to exceed the bandwidth allowed by local regulations.

The MC13135 is designed for use with an LC quadrature detector, and does not have sufficient drive to be used with a ceramic discriminator. The MC13136 was designed to use a ceramic discriminator, but can also be run with an LC quad coil, as mentioned in the Test Circuit Information section. The data shown in Figures 12 and 13 was taken using a muRata CDB455C34 ceramic discriminator which has been specially matched to the MC13136. Both the choice of discriminators and the external matching circuit will affect the distortion and recovered audio.

RSSI/Op Amp

The Received Signal Strength Indicator (RSSI) on the MC13135/13136 has about 70 dB of range. The resistor needed to translate the RSSI current to a voltage output has been included on the internal circuit, which gives it a tighter tolerance. A temperature compensated reference current also improves the RSSI accuracy over temperature. On the MC13136, the op amp on board is connected to the output to provide a voltage buffered RSSI. On the MC13135, the op amp is not connected internally and can be used for the RSSI or as a data slicer (see Figure 17c).

MC13135 MC13136

Figure 15. PLL Controlled Narrowband FM Receiver at 46/49 MHz

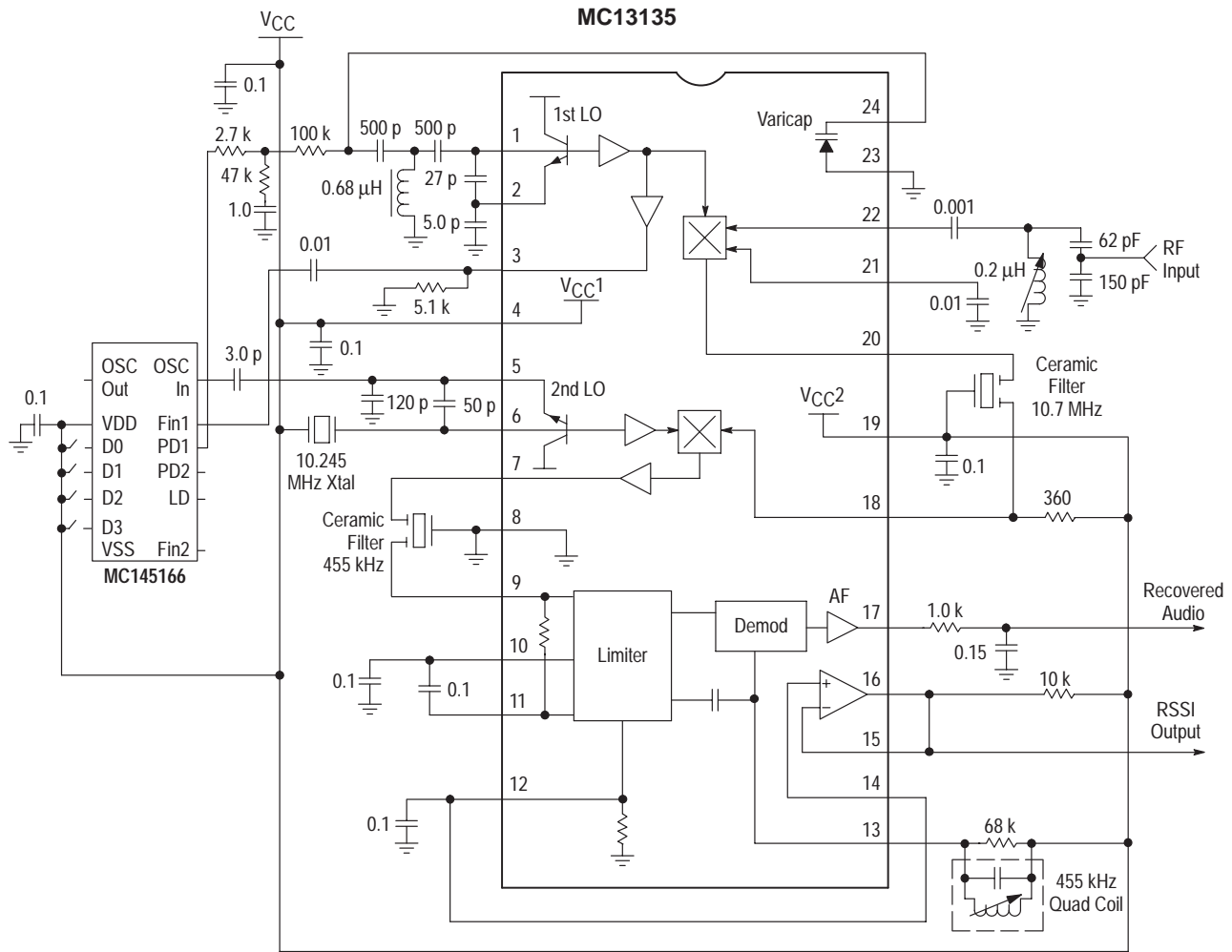
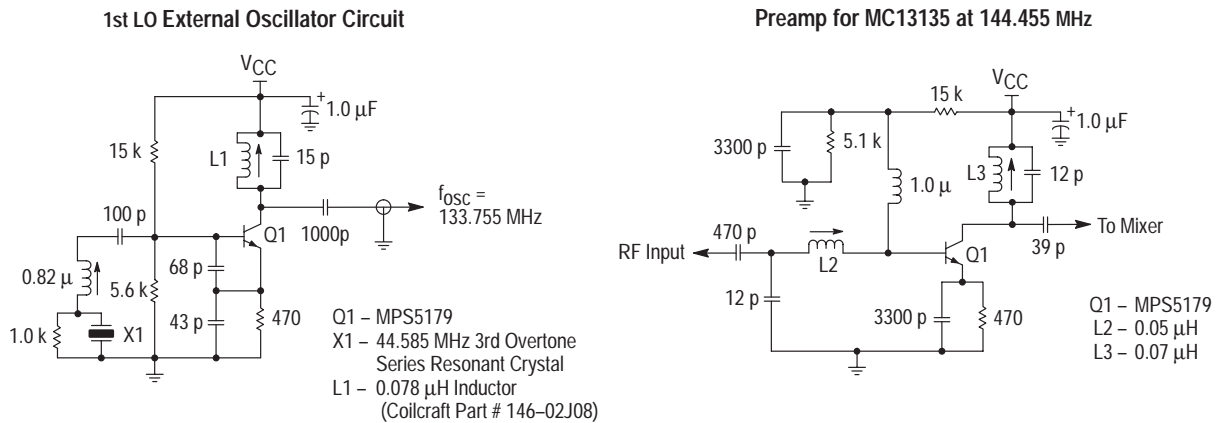


Figure 16. 144 MHz Single Channel Application Circuit



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13135 MC13136

Figure 17a. Single Channel Narrowband FM Receiver at 49.7 MHz

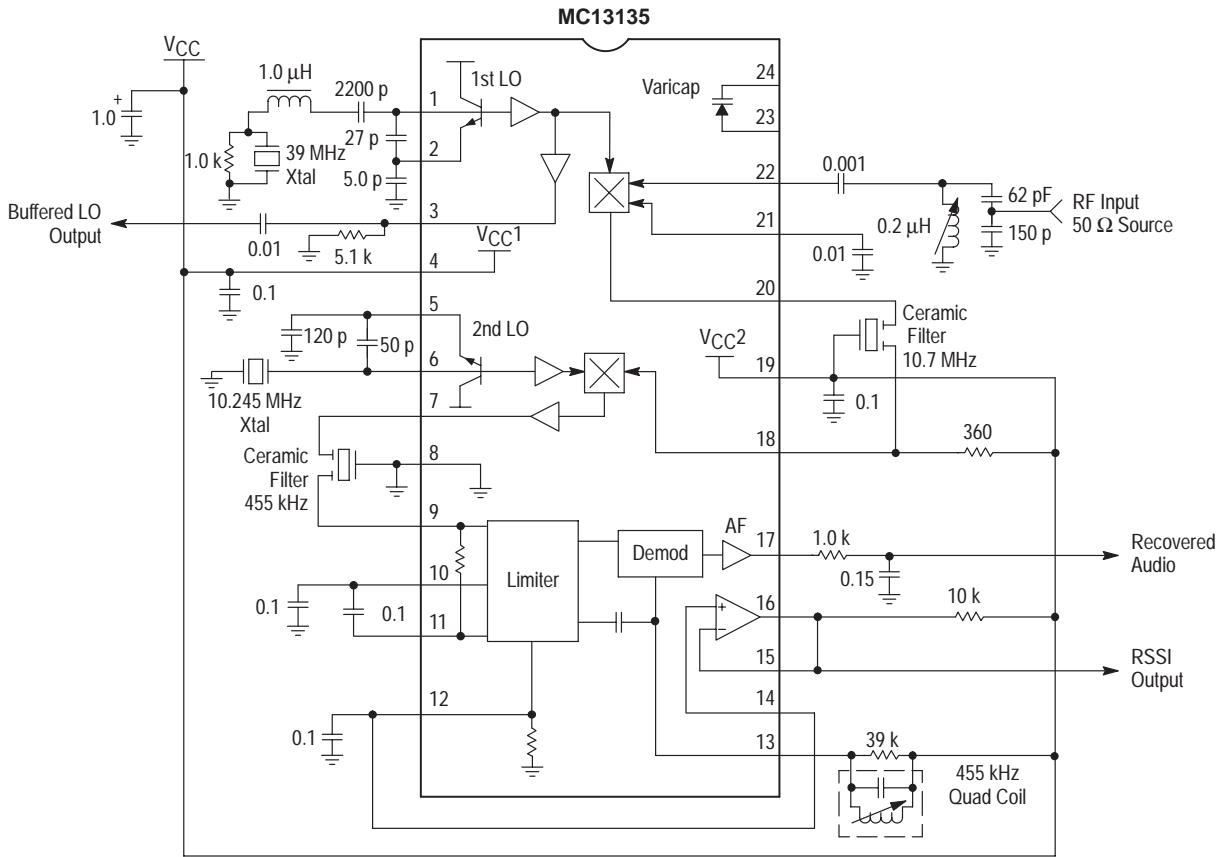
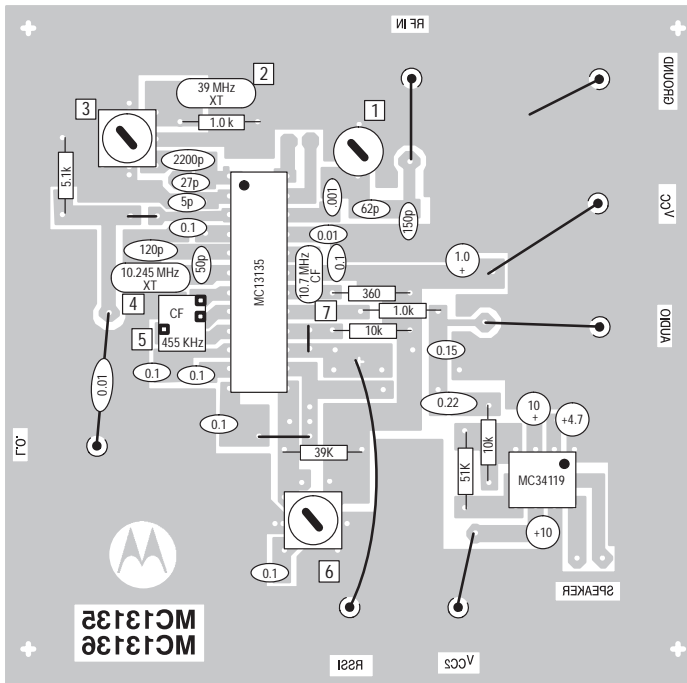
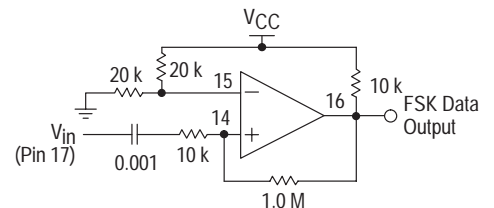


Figure 17b. PC Board Component View



- NOTES:**
- 0.2 μ H tunable (unshielded) inductor
 - 39 MHz Series mode resonant 3rd Overtone Crystal
 - 1.5 μ H tunable (shielded) inductor
 - 10.245 MHz Fundamental mode crystal, 32 pF load
 - 455 kHz ceramic filter, muRata CFU 455B or equivalent
 - Quadrature coil, Toko 7MC-8128Z (7mm) or Toko RMC-2A6597HM (10mm)
 - 10.7 MHz ceramic filter, muRata SFE10.7MJ-A or equivalent

Figure 17c. Optional Data Slicer Circuit (Using Internal Op Amp)



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13135 MC13136

Figure 18. PC Board Solder Side View

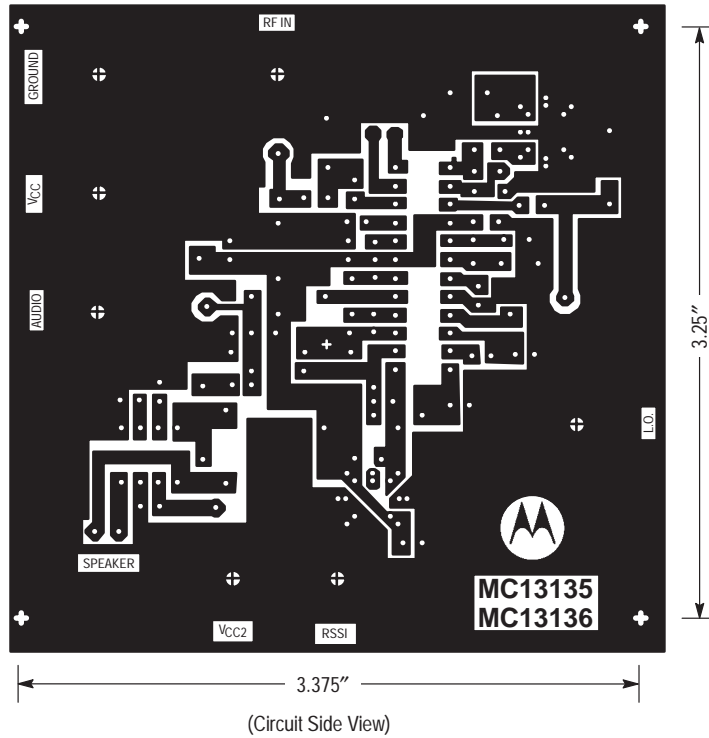
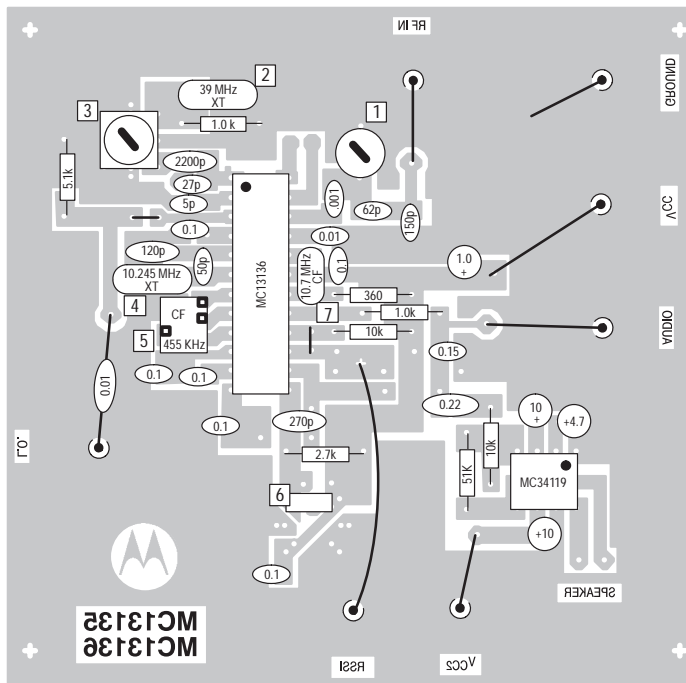


Figure 19. PC Board Component View



- NOTES:**
1. 0.2 μ H tunable (unshielded) inductor
 2. 39 MHz Series mode resonant 3rd Overtone Crystal
 3. 1.5 μ H tunable (shielded) inductor
 4. 10.245 MHz Fundamental mode crystal, 32 pF load
 5. 455 kHz ceramic filter, muRata CFU 455B or equivalent
 6. Ceramic discriminator, muRata CDB455C34 or equivalent
 7. 10.7 MHz ceramic filter, muRata SFE10.7MJ-A or equivalent

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13135 MC13136

Figure 20a. Single Channel Narrowband FM Receiver at 49.7 MHz

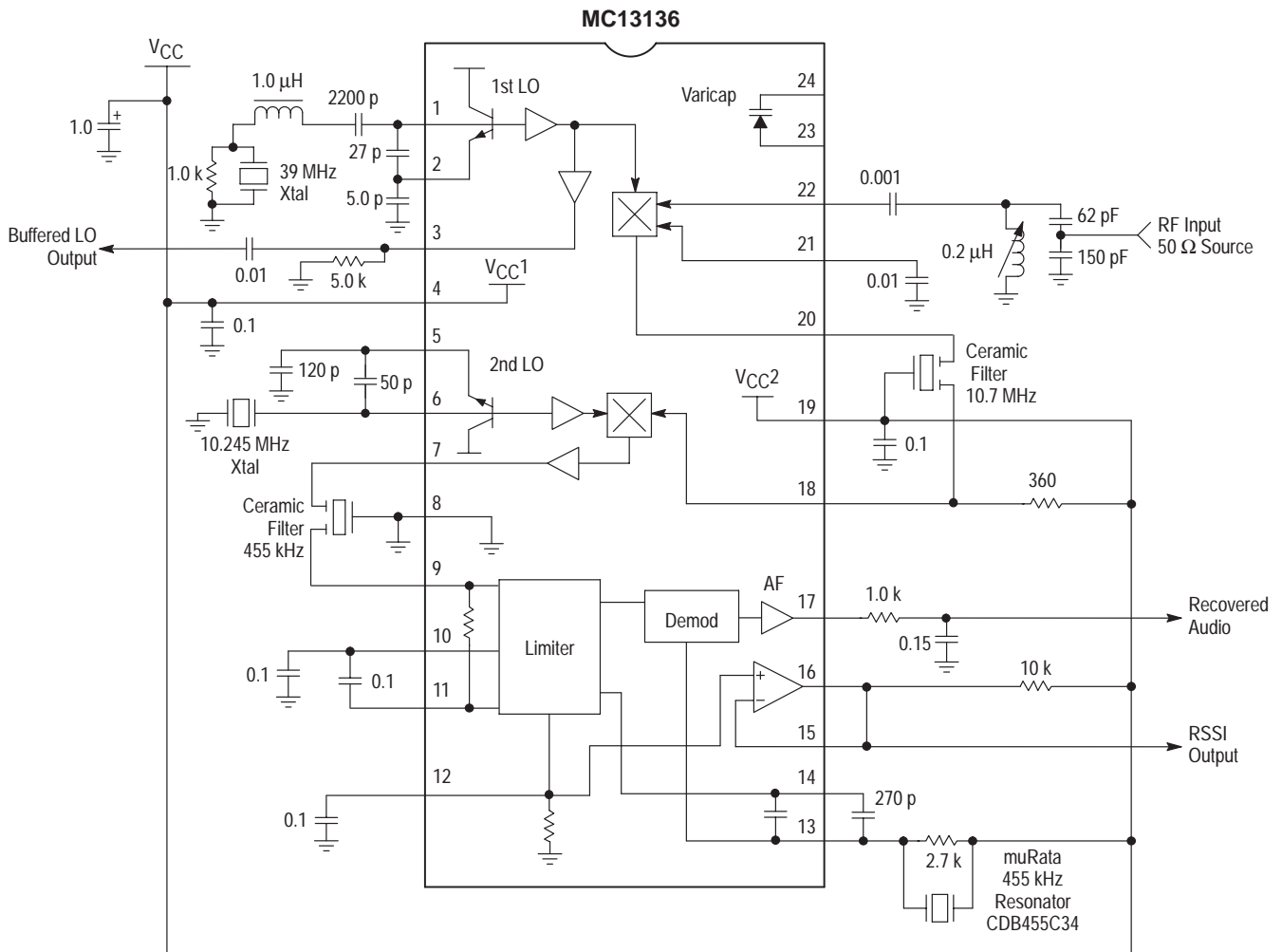
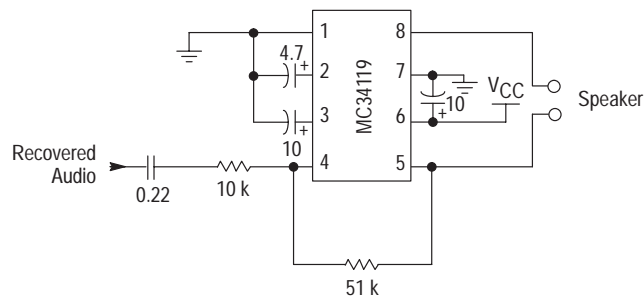


Figure 20b. Optional Audio Amplifier Circuit

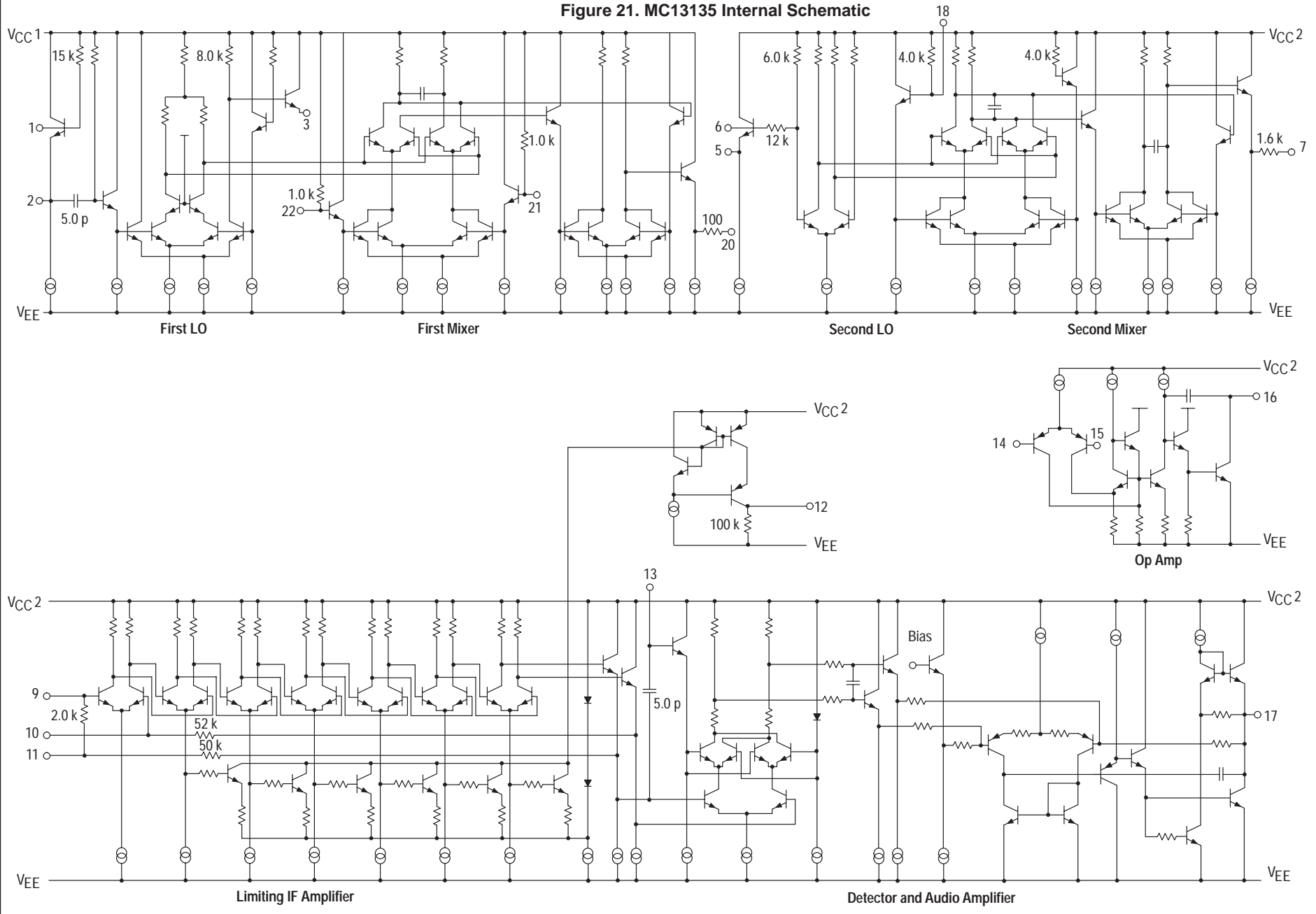


NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 21. MC13135 Internal Schematic



MOTOROLA WIRELESS RF, IF AND TRANSMITTER DEVICE DATA

MC13135 MC13136
3-2-89

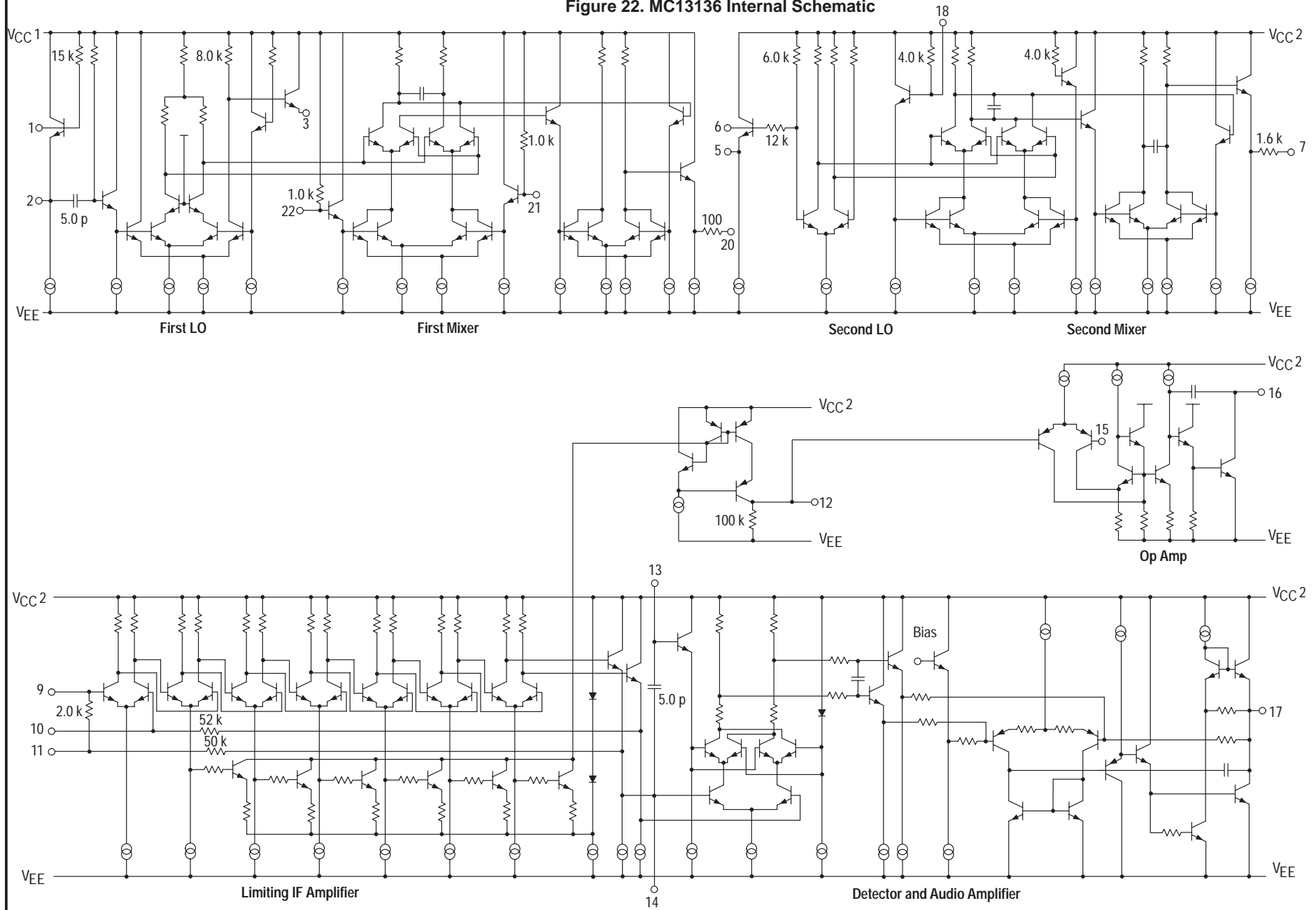
MC13135 MC13136

This device contains 142 active transistors.

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 22. MC13136 Internal Schematic



MC13135 MC13136
3.2-90

MOTOROLA WIRELESS RF, IF AND TRANSMITTER DEVICE DATA

MC13135 MC13136

This device contains 142 active transistors.

NOT RECOMMENDED FOR NEW DESIGNS



MOTOROLA

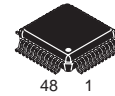
MC13145

Low Power Integrated Receiver for ISM Band Applications

The MC13145 is a dual conversion integrated RF receiver intended for ISM band applications. It features a Low Noise Amplifier (LNA), two 50 Ω linear Mixers with linearity control, Voltage Controlled Oscillator (VCO), second LO amplifier, divide by 64/65 dual modulus Prescaler, split IF Amplifier and Limiter, RSSI output, Coillless FM/FSK Demodulator and power down control. Together with the transmit chip (MC13146) and the baseband chip (MC33410 or MC33411A/B), a complete 900 MHz cordless phone system can be implemented. This device may be used in applications up to 1.8 GHz.

- Low (<1.8 dB @ 900 MHz) Noise Figure LNA with 14 dB Gain
- Externally Programmable Mixer linearity: IIP3 = 10(nom.) to 17 dBm (Mixer1); IIP3 = 10 (nom.) to 17 dBm (Mixer2)
- 50 Ω Mixer Input Impedance and Open Collector Output (Mixer 1 and Mixer 2); 50 Ω Second LO (LO2) Input Impedance
- Low Power 64/65 Dual Modulus Prescaler (MC12053 type)
- Split IF for Improved Filtering and Extended RSSI Range
- Internal 330 Ω Terminations for 10.7 MHz Filters
- Linear Coillless FM/FSK Demodulator with Externally Programmable Bandwidth, Center Frequency and Audio level
- 2.7 to 6.5 V Operation, Low Current Drain (<27 mA, Typ @ 3.6 V) with Power Down Mode (<10 μA, Typ)
- 2.4 GHz RF, 1.0 GHz IF1 and 50 MHz IF2 Bandwidth

**UHF WIDEBAND
RECEIVER SUBSYSTEM
(LNA, Mixer, VCO, Prescaler,
IF Subsystem,
Coillless Detector)**

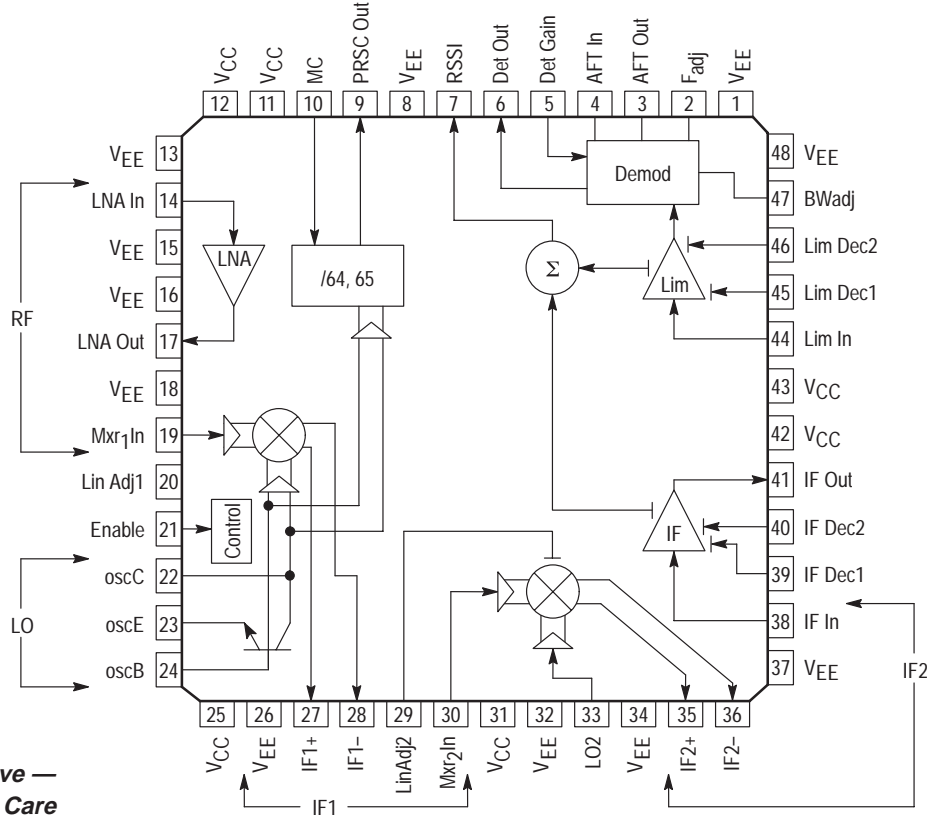


FTA SUFFIX
PLASTIC PACKAGE
CASE 932
(LQFP-48)

ORDERING INFORMATION

Device	Temperature Range	Package
MC13145FTA	T _A = -20 to 70°C	LQFP-48

PIN CONNECTIONS AND FUNCTIONAL BLOCK DIAGRAM



**ESD Sensitive —
Handle with Care**

This device contains 626 active transistors.

MC13145

OVERALL RECEIVER SPECIFICATIONS

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Power Supply Voltage	$V_{CC(max)}$	7.0	Vdc
Junction Temperature	$T_J(max)$	150	°C
Storage Temperature Range	T_{stg}	-65 to 150	°C
Maximum Input Signal	P_{in}	5.0	dBm

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions, Electrical Characteristics tables or Pin Descriptions section.
2. Meets Human Body Model (HBM) ≤ 250 V and Machine Model (MM) ≤ 25 V. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Rating	Symbol	Min	Typ	Max	Unit
Power Supply Voltage ($T_A = 25^\circ\text{C}$)	V_{CC} V_{EE}	2.7 0	- 0	6.5 0	Vdc
Input Frequency (LNA In, Mxr ₁ In)	f_{in}	100	-	1800	MHz
Ambient Temperature Range	T_A	-20	-	70	°C
Input Signal Level (with minor performance degradation)	P_{in}	-	-10	-	dBm

RECEIVER DC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$; $V_{CC} = 3.6$ Vdc; No Input Signal, unless otherwise noted)

Characteristics	Symbol	Min	Typ	Max	Unit
Total Supply Current (Enable = V_{CC})	I_{total}	24	27	34	mA
Power Down Current (Enable = V_{EE})	I_{total}	-	10	50	μA

RECEIVER AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$; $V_{CC} = 3.6$ Vdc; RF In = 1.0 GHz; 1st LO Freq = 1070.7 MHz; 2nd LO Freq = 60 MHz; $f_{mod} = 1.0$ kHz; $f_{dev} = \pm 40$ kHz; IF filter bandwidth = 280 kHz, unless otherwise noted. See Figure 1 Test Circuit)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
SINAD @ -110 dBm LNA Input	LNA In	Det Out	SINAD	12	20	-	dB
12 dB SINAD Sensitivity (Apps Circuit with C-message filter at DetOut)	LNA In	Det Out	SINAD _{12dB}	-	-115	-	dBm
30 dB SINAD Sensitivity (No IF filter distortion within ± 40 kHz)	LNA In	Det Out	SINAD _{30dB}	-	-100	-	dBm
SINAD Variation with IF Offset of ± 40 kHz (No IF filter distortion within ± 40 kHz)	LNA In	Det Out	-	-	5.0	-	dB
Noise Figure: LNA, 1st Mixer & 2nd Mixer	LNA In	IF Out	NF	-	3.5	5.0	dB
Power Gain: LNA, 1st Mixer & 2nd Mixer	LNA In	IF Out	G	15	19	25	dB
RSSI Dynamic Range	IF In	RSSI	-	-	80	-	dB
RSSI Current	IF In	RSSI	-	-	-	-	μA
-10 dBm @ IF Input				35	40	55	
-20 dBm @ IF Input				-	35	-	
-30 dBm @ IF Input				-	30	-	
-40 dBm @ IF Input				-	25	-	
-50 dBm @ IF Input				15	20	37	
-60 dBm @ IF Input				-	15	-	
-70 dBm @ IF Input				-	10	-	
-80 dBm @ IF Input				-	5.0	-	
-90 dBm @ IF Input				-	1.0	7.0	
Input 1.0 dB Compression Point (Measured at IF output)			P_{in1dB}	-	-18	-	dBm

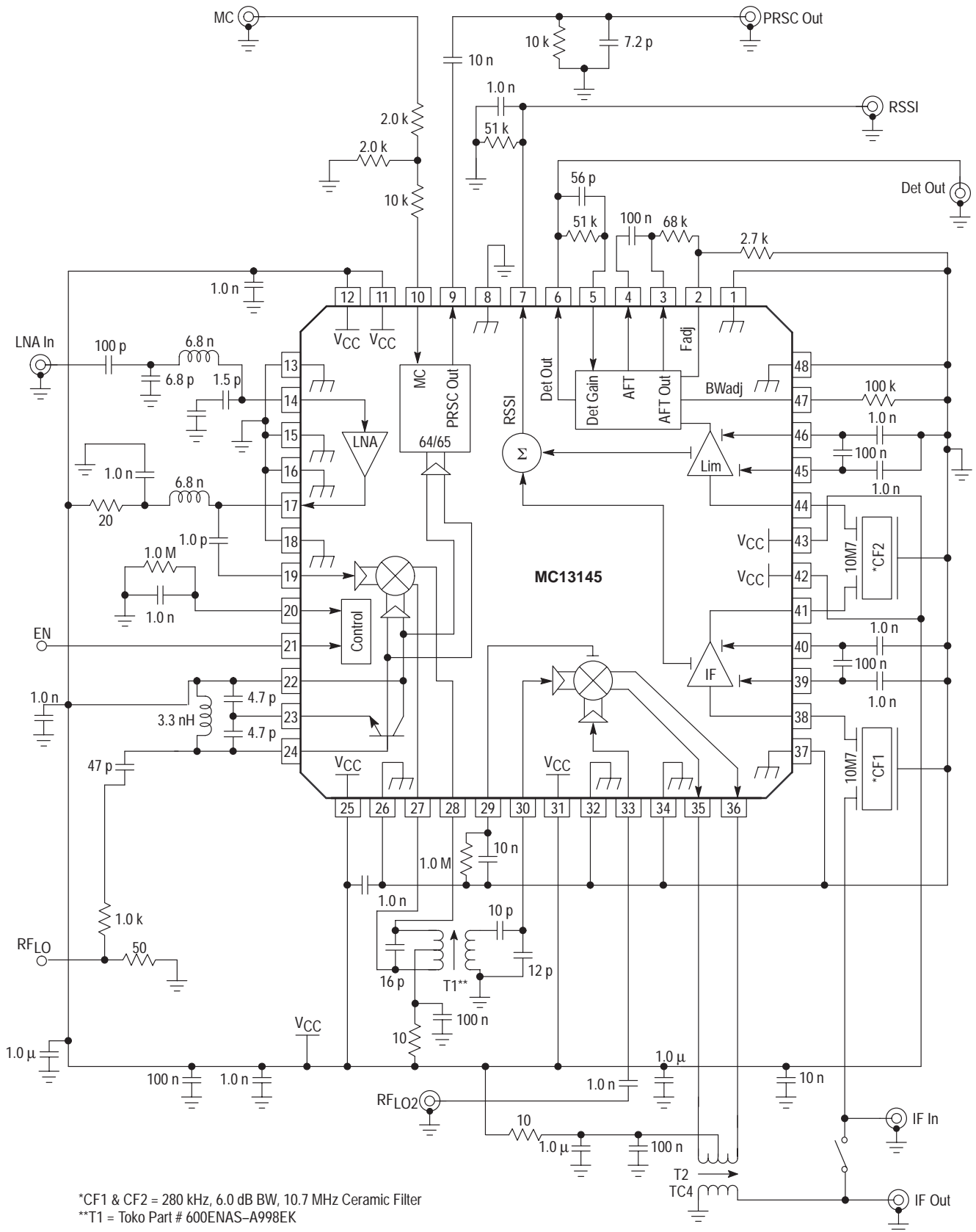
MC13145

RECEIVER AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$; $V_{CC} = 3.6\text{ Vdc}$; RF In = 1.0 GHz; 1st LO Freq = 1070.7 MHz; 2nd LO Freq = 60 MHz; $f_{\text{mod}} = 1.0\text{ kHz}$; $f_{\text{dev}} = \pm 40\text{ kHz}$; IF filter bandwidth = 280 kHz, unless otherwise noted. See Figure 1 Test Circuit)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
Input 3rd Order Intercept Point (Measured at IF output)			IIP3	–	–8.0	–	dBm
Demodulator Output Swing (50 k \parallel 56 pF Load)	IF In	Det Out	V_{out}	0.8	1.0	1.2	V_{pp}
Demodulator Bandwidth ($\pm 1.0\text{ dB}$ bandwidth)		Det Out	BW	–	100	–	kHz
Prescaler Output Level (10 k Ω //8.0 pF load) Prescaler 64 Frequency = 16.72968 MHz Prescaler 65 Frequency = 16.4723 MHz		PRSC _{out}	V_{out}	0.4 0.4	0.51 0.51	0.6 0.6	V_{pp}
MC Current Input (High)		MC	I_{ih}	70	100	130	μA
MC Current Input (Low)		MC	I_{il}	–130	–100	–70	μA
Input high voltage		Enable	V_{ih}	V_{CC} –0.4	–	V_{CC}	V
Input low voltage		Enable	V_{il}	0	–	0.4	V
Input Current		Enable	I_{in}	–50	–	50	μA
PLL Setup Time [Note 1]	MC	PRSC _{out}	T_{PLL}	–	10	–	nS
SNR @ –30 dBm Signal Input (<40 kHz deviation;with C–Message Filter)				–	50	–	dB
Total Harmonic Distortion (<40 kHz deviation;with C–Message Filter)				–	1.0	–	%
Spurious Response SINAD (RF In: –50 dBm)				–	12	–	dB

MC13145

Figure 1. Test Circuit



*CF1 & CF2 = 280 kHz, 6.0 dB BW, 10.7 MHz Ceramic Filter
 **T1 = Toko Part # 600ENAS-A998EK

MC13145

CIRCUIT DESCRIPTION

General

The MC13145 is a low power dual conversion wideband FM receiver incorporating a split IF. This device is designated for use as the receiver in analog and digital FM systems such as 900 Mhz ISM Band Cordless phones and wideband data links with data rates up to 150kbps. It contains a 1st and 2nd mixer, 1st and 2nd local oscillator, Received Signal Strength Indicator (RSSI), IF amplifier, limiting IF, a unique coilless quadrature detector, and a device enable function.

Current Regulation/Enable

The MC13145 is designed for battery powered portable applications. Supply current is typically 27 mA at 3.6 Vdc.

Temperature compensating, voltage independent current regulators are controlled by the Enable Pin where "high" powers up and "low" powers down the entire circuit.

Low Noise Amplifier (LNA)

The LNA is a cascoded common emitter amplifier configuration. Under very large RF input signals, the DC base current of the common emitter and cascode transistors can become very significant. To maintain linear operation of the LNA, adequate dc current source is needed to establish the $2V_{be}$ reference at the base of the RF cascoded transistor and to provide the base voltage on the common emitter transistor. A sensing circuit, together with a current mirror guarantees that there is always sufficient dc base current available for the cascode transistor under all power levels.

1st and 2nd Mixer

Each mixer is a double-balanced class AB four quadrant multiplier which may be externally biased for high mixer dynamic range. Mixer input third order intercept point of up to 17 dBm is achieved with only 7.0 mA of additional supply current. The 1st mixer has a single-ended input at 50Ω and operates at 1.0 GHz with -3.0 dB of power gain at approximately 100 mVrms LO drive level. The mixers have open collector differential outputs to provide excellent mixer dynamic range and linearity.

1st Local Oscillator

The 1st LO has an on-chip transistor which operates with coaxial transmission line and LC resonant elements up to 1.8 GHz. A VCO output is available for multi-frequency operation under PLL synthesizer control.

RSSI

The received signal strength indicator (RSSI) output is a current proportional to the log of the received signal amplitude. The RSSI current output (Pin 7) is derived by summing the currents from the IF and limiting amplifier stages. An increase in RSSI dynamic range, particularly at higher input signal levels is achieved. The RSSI circuit is designed to provide typically 80 dB of dynamic range with temperature compensation.

Linearity of the RSSI is optimized by using external ceramic bandpass filters which have an insertion loss of 4.0 dB and 330Ω source and load impedance.

IF Amplifier

The first IF amplifier section is composed of three differential stages with the second and third stages

contributing to the RSSI. This section has internal DC feedback and external input decoupling for improved symmetry and stability. The total gain of the IF amplifier block is approximately 40 dB up to 40MHz.

The fixed internal input impedance is 330Ω . When using ceramic filters requiring source and load impedances of 330Ω , no external matching is necessary. Overall RSSI linearity is dependent on having total midband attenuation of 10 dB (4.0 dB insertion loss plus 6.0 dB impedance matching loss) for the filter. The output of the IF amplifier is buffered and the impedance is 330Ω .

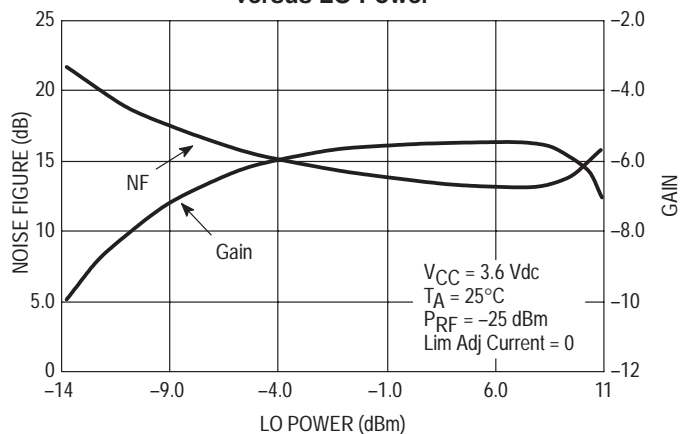
Limiters

The limiter section is similar to the IF amplifier section except that five stages are used with the middle three contributing to the RSSI. The fixed internal input impedance is 330Ω . The total gain of the limiting amplifier section is approximately 84 dB. This IF limiting amplifier section internally drives the coilless quadrature detector section.

Coilless Quadrature Detector

The coilless detector is a unique design which eliminates the conventional tunable quadrature coil in FM receiver systems. The frequency detector implements a phase locked loop with a fully integrated on chip relaxation oscillator which is current controlled and externally adjusted, a bandwidth adjust, and an automatic frequency tuning circuit. The loop filter is external to the chip allowing the user to set the loop dynamics. Two outputs are used: one to deliver the audio signal (detector output) and the other to filter and tune the detector (AFT).

Figure 2. 2nd Mixer NF & Gain versus LO Power



Evaluation PCB

The evaluation PCB is a versatile board which allows the MC13145 to be configured as a dual-conversion receiver, or to characterize individual operating parameters.

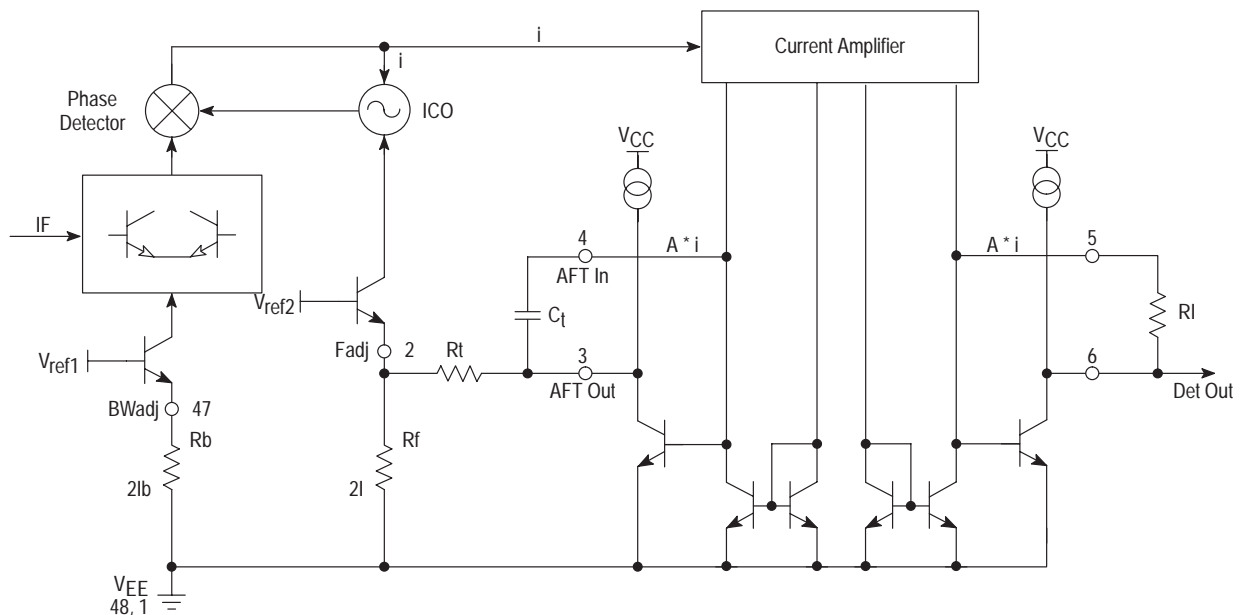
The general purpose schematic and associated parts list for a typical application are given in Figure 15. Please refer to AN1687/D and AN1691/D for additional details and applications for the device.

MC13145

PIN FUNCTION DESCRIPTION

Pin	Symbol/Type	Description	Description
47	BWadj	See Figure 3.	COILLESS DETECTOR Bandwidth Adjust The deviation bandwidth of the detector response is determined by the combination of an on-chip capacitor and an external resistor to ground.
2	Fadj		Frequency Adjust The free running frequency of the detector oscillator is defined by the combination of an on-chip capacitor and an external resistor, Radj from frequency adjust pin to ground.
1, 48	VEE		VEE, Negative Supply These pins are VEE supply for the coilless detector circuit.
3	AFT Out		AFT Out The AFT is low pass filtered with a corner frequency below the audio bandwidth allowing the error to be added to the center frequency adjust signal at Fadj, Pin 2. The low frequency high pass corner is set by the external capacitor, Ct from AFT out (Pin 3) to AFT in (Pin 4) and external resistor, Rt from AFT out to Fadj (Pin 2).
4	AFT In		AFT In The AFT in is used to set the buffer transfer function.
5	Det Gain		Detector Gain The AFT buffer is used to set the buffer transfer function.
6	Det Out		Detector Output Set gain and output level of detector with resistor to Det Out Pin.

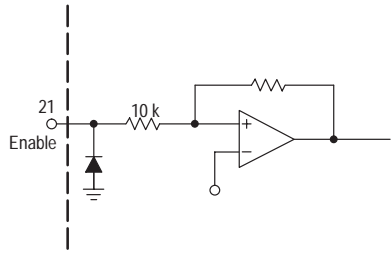
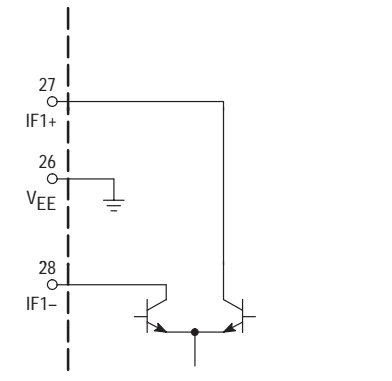
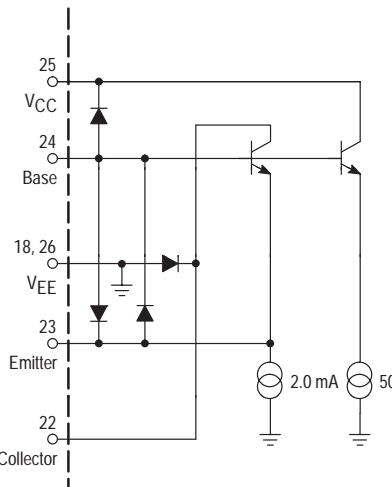
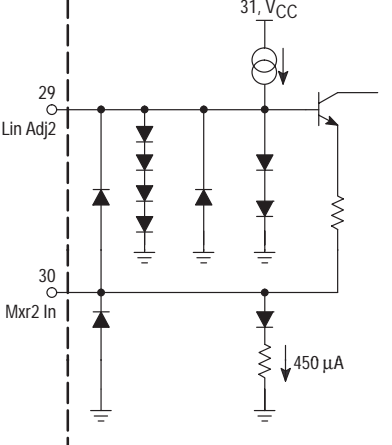
Figure 3. Coilless Detector Internal Circuit



MC13145

Pin	Symbol/Type	Description	Description	
8	V _{EE}		V_{EE}, Negative Supply Voltage	
9	PRSCout		Prescaler Output The prescaler output provides typically 500 mVpp drive to the fin pin of a PLL synthesizer. Conjugately matching the interface will increase the drive delivered to the PLL input.	
10	MC		Dual Modulus Control Current Input This requires a current input of typically 200 μApp.	
11, 12	V _{CC}		V_{CC}, Positive Supply V _{CC} pin is taken to the incoming positive battery or regulated dc voltage through a low impedance trace on the PCB. It decoupled to V _{EE} ground at the pin of the IC.	
14	LNA In		LNA In The input is the base of the common emitter transistor. Minimum external matching is required to optimize the input return loss and gain.	
13, 15, & 16	V _{EE}		V_{EE}, Negative Supply V _{EE} pin is taken to an ample dc ground plane through a low impedance path. The path should be kept as short as possible. A minimum two sided PCB is recommended so that ground returns can be easily made through via holes.	
17	LNAout		LNA Out The output is from the collector of the cascode transistor amplifier. The output may be conjugately matched with a shunt L (needed to dc bias the open collector), and series L and C network.	
19	Mxr ₁ In			1st Mixer Input The mixer input impedance is broadband 50 Ω for applications up to 2.4 GHz. It easily interfaces with a RF ceramic filter.
20	Lin Adj1			1st Mixer Linearity Control The mixer linearity control circuit accepts approximately 0 to 300 μA control current to set the dynamic range of the mixer. An Input Third Order Intercept Point, IIP3 of 17 dBm may be achieved at 300 μA of control current.

MC13145

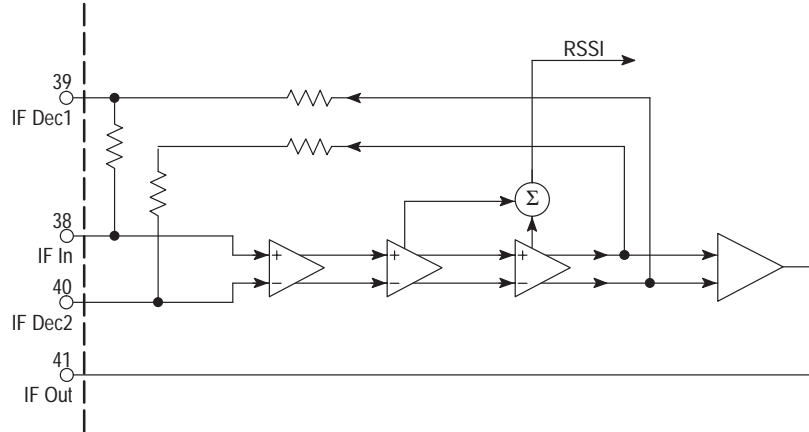
Pin	Symbol/Type	Description	Description	
21	Enable		<p>Enable Enable the receiver by pulling the pin up to V_{CC}.</p>	
26	V_{EE}		<p>V_{EE}, Negative Supply V_{EE} supply for the mixer IF output.</p>	
27	IF1+		<p>1st Mixer Outputs The Mixer is a differential open collector output configuration which is designed to use over a wide frequency range. The differential output of the mixer has back to back diodes across them to limit the output voltage swing and to prevent pulling of the VCO. Differential to single-ended circuit configuration and matching options are shown in the Test Circuit. Additional mixer gain can be achieved by matching the outputs for the desired passband Q.</p>	
28	IF1-			
22	Collector		<p>On-board VCO Transistor The transistor has the emitter, base, collector, V_{CC}, and V_{EE} pins available. Internal biasing which is compensated for stability over temperature is provided. It is recommended that the base pin is pulled up to V_{CC} through an RFC chosen for the particular oscillator center frequency .</p>	
23	Emitter		<p>V_{CC}, Positive Supply Voltage A V_{CC} pin is provided for the VCO. The operating supply voltage range is from 2.7 Vdc to 6.5 Vdc.</p>	
24	Base		<p>V_{EE}, Negative Supply Voltage</p>	
25	V_{CC}		<p>2nd Mixer Linearity Control The mixer linearity control circuit accepts approximately 0 to 400 μA control current to set the dynamic range of the mixer. An Input Third Order Intercept Point, IIP3 of 17 dBm may be achieved at 400 μA of control current. IIP3 default with no external bias is 10 dBm.</p>	
18, 26	V_{EE}			<p>2nd Mixer Input The mixer input impedance is broadband 50 Ω.</p>
29	Lin Adj2			
30	Mxr2 In			
31	V_{CC}			

MC13145

Pin	Symbol/Type	Description	Description
32, 34	V _{EE}		V_{EE}, Negative Supply Voltage
33	LO2		2nd Local Oscillator The 2nd LO input impedance is broadband 50 Ω; it is driven from an external 50 Ω source. Typical level is -15 to -10 dBm.
35	IF2+		2nd Mixer Outputs The Mixer is a differential open collector configuration.
36	IF2-		
37	V _{EE}	See Figure 4.	V_{EE}, Negative Supply Voltage
38	IF In		IF Amplifier Input IF amplifier input source impedance is 330 Ω. The three stage amplifier has 40 dB of gain with 3.0 dB bandwidth of 40 MHz.
39, 40	IF Dec1, IF Dec2		IF Decoupling These pins are decoupled to V _{CC} to provide stable operation of the limiting IF amplifier.
41	IF Out		IF Amplifier Output IF amplifier output load impedance is 330 Ω.
42	V _{CC}		V_{CC}, Positive Supply Voltage
7	RSSI		RSSI The RSSI circuitry in the 2nd & 3rd amplifier stages outputs a current when the output of the previous stage enters limiting. The net result is a RSSI current which represents the logarithm of the IF input voltage. An external resistor to ground is used to provide a voltage output.

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Figure 4. IF Amplifier Functional Diagram



Pin	Symbol/Type	Description	Description
43	V _{CC}	See Figure 5.	V_{CC}, Positive Supply Voltage
44	Lim In		Limiting Amplifier Input Limiting amplifier input source impedance is 330 Ω. This amplifier has 84 dB of gain with 3.0 dB bandwidth of 40 MHz; this enables the IF and limiting amplifiers chain to hard limit on noise.
45, 46	Lim Dec1, Lim Dec2		If Decoupling These pins are decoupled to V _{CC} to provide stable operation of the 2nd IF limiting amplifier.
7	RSSI		RSSI The RSSI circuitry in the 2nd, 3rd, & 4th amplifier stages outputs a current when the output of the previous stage enters limiting. The net result is a RSSI current which represents the logarithm of the IF input voltage. An external resistor to ground is used to provide a voltage output.

Figure 5. Limiter Amplifier Functional Diagram

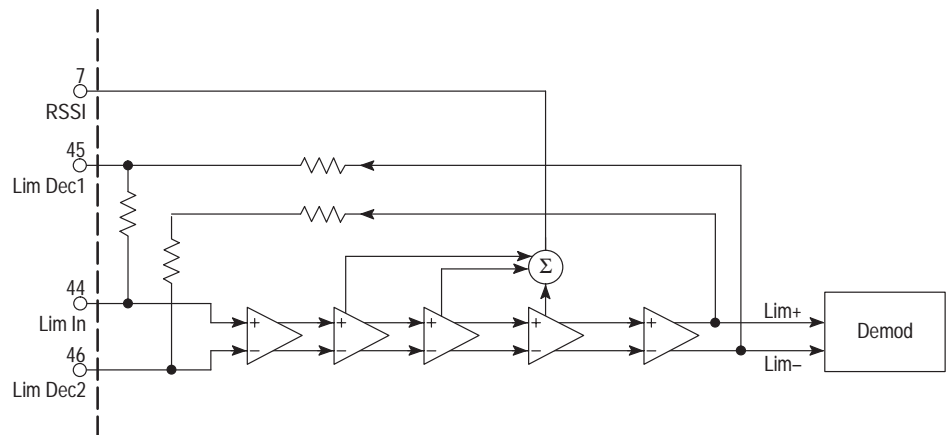


Figure 6. 2nd Mixer Gain versus LO Drive

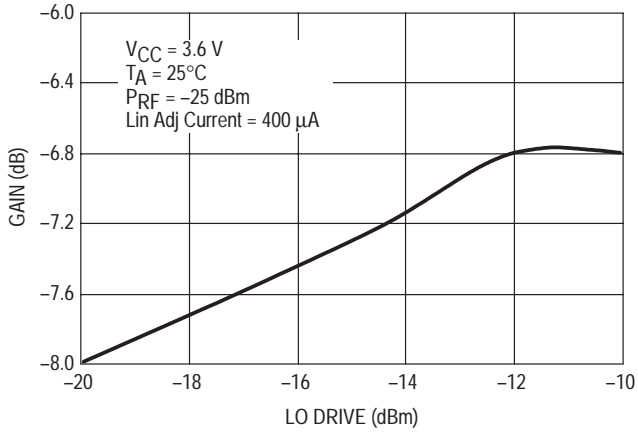


Figure 7. 2nd Mixer P1dB versus LO Drive

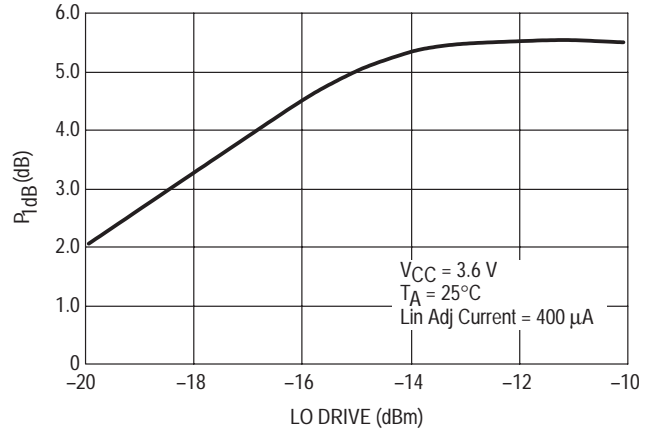


Figure 8. 2nd Mixer IP3/P1dB versus Lin Adj Current

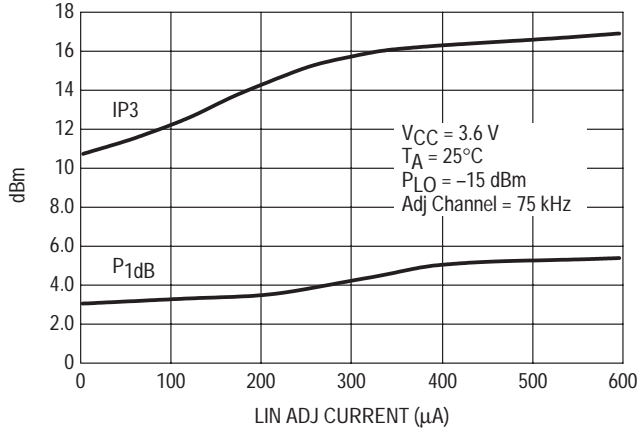


Figure 9. 2nd Mixer Gain versus Lin Adj Current

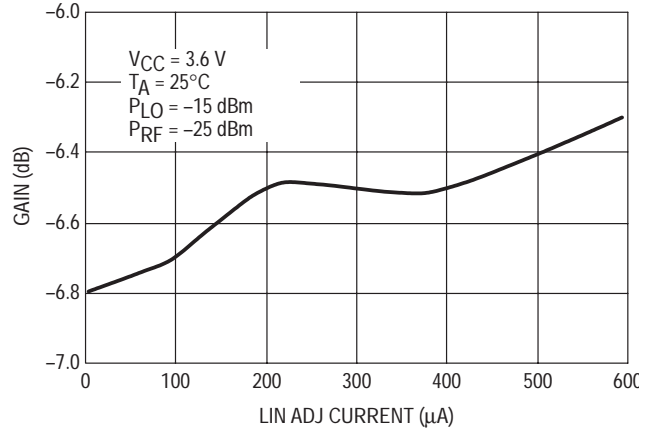
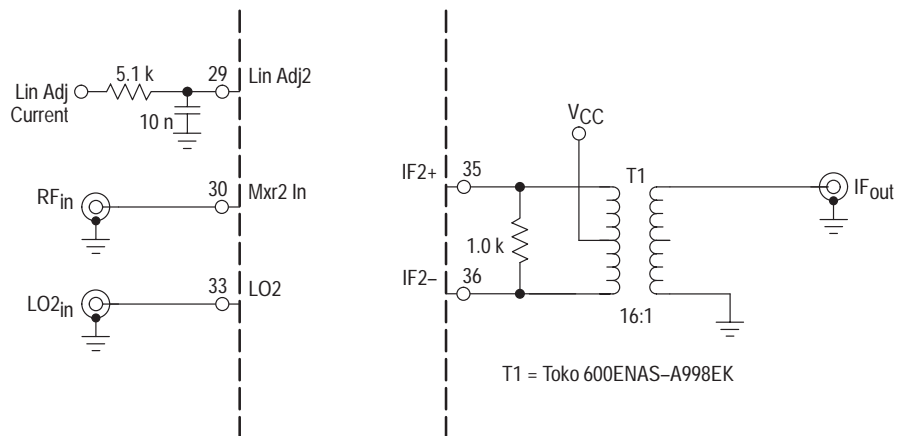


Figure 10. Test Circuit for Figures 6 thru 9.



Input Matching / Components

It is desirable to use a RF ceramic or SAW filter before the mixer to provide image frequency rejection. The filter is selected based on cost, size and performance tradeoffs. Typical RF filters have 1.5 to 2.5 dB insertion loss. The evaluation PC board layout accommodates ceramic RF filters which are offered by various suppliers.

Interface matching between the LNA, RF filter and the mixer will be required. The interface matching networks shown in the evaluation circuit are designed for 50 Ω interfaces.

1st Mixer Output & 2nd Mixer Input Interface Matching

In a wideband system the primary sensitivity of the receiver backend may be achieved before the last mixer. The evaluation circuit shows the matching and impedance transformation network between the 1st mixer open collector differential outputs and 2nd mixer single ended 50 ohm input. This adjustable shielded transformer and tapped capacitor transform network does two things: 1) bandpass limits the 1st IF signal with a loaded Q of approximately 40 and 2) provides adequate second image rejection and a low cost alternative to a SAW filter.

However, a SAW filter may be selected as a more costly alternative while providing improved 2nd image rejection and a fixed tuned 1st IF filter.

2nd Mixer & Limiting IF Matching / Filtering

A simple LCR network is needed to interface the 2nd mixer differential outputs to 330 ohm ceramic filters or directly to the 330 ohm IF input. TDK, Toko and Murata offer single 10.7 MHz ceramic filters with various 3.0 dB bandwidths from 110 to 380 kHz. Murata offers a series-parallel resonator pair (part number KMFC545) with a 3.0 dB bandwidth of ± 325 kHz and a maximum insertion loss of 5.0 dB. However, even the series-parallel ceramic filter pair yields only a maximum bandpass of 650 kHz. In some data applications a wider band IF bandpass is necessary.

Local Oscillators – VHF/UHF Applications

The on-chip transistor may be used for HF and VHF local oscillator with higher order overtone crystals. It is recommended that a Butler overtone oscillator configuration is used. The crystal is driven from the emitter and is coupled to the high impedance base through a capacitive tap network. Operation at the desired overtone frequency is ensured by the parallel resonant circuit formed by an inductor and the tap capacitors and parasitic capacitances of the on-chip transistor and PC board. A high tolerance, high Q ceramic or air wound surface mount component may be used if the other components have tight enough tolerances; however, a variable inductor provides an adjustment for gain and frequency of the resonant tank ensuring lock up and start-up of the crystal oscillator. The overtone crystal is chosen with ESR of typically 80 ohms and 120 ohms maximum; if the resistive loss in the crystal is too high the performance of oscillator may be impacted by lower gain margins.

A series LC network to ac ground (which is V_{CC}) is comprised of the inductance of the base lead of the on-chip transistor and PC board traces and tap capacitors. Parasitic oscillations often occur in the 200 to 900 MHz range. A small resistor is placed in series with the base (pin 9) to cancel the

negative resistance associated with this undesired mode of oscillation. Since the base input impedance is so large a small resistor in the range of 27 to 68 ohms has very little effect on the desired Butler mode of oscillation.

The crystal parallel capacitance, C_O , provides a feedback path that is low enough in reactance at frequencies of 5th overtones or higher to cause trouble. C_O has little effect near resonance because of the low impedance of the crystal motional arm ($R_m-L_m-C_m$). As the tunable inductor which forms the resonant tank with the tap capacitors is tuned off the crystal resonant frequency it may be difficult to tell if the oscillation is under crystal control. Frequency jumps may occur as the inductor is tuned. In order to eliminate this behavior an inductor, L_O , is placed in parallel with the crystal. L_O is chosen to be resonant with the crystal parallel capacitance, C_O , at the desired operation frequency. The inductor provides a feedback path at frequencies well below resonance; however, the parallel tank network of the tap capacitors and tunable inductor prevent oscillation at these frequencies.

Coilless Detector

The coilless detector (see Figure 3) is unique and offers cost and performance advantages over the conventional quadrature detector. It consists of a current controlled oscillator (ICO) and a phase detector. The error current, I is also amplified to provide an output, and the output is duplicated and filtered and fed back to the oscillator to provide automatic fine tuning (AFT).

The oscillator free running frequency, f_o is set by R_f and is calculated by the following equation where C is approximately 4.0 pF:

$$f_o = 1/(8 \cdot R_f \cdot C)$$

The demodulator bandwidth is set by R_b and is shown in Figure 14.

The AFT is filtered by C_t and R_t . The low pass pole creates a high pass pole in the overall demodulator frequency response at:

$$A/(2 \cdot \pi \cdot C_t \cdot R_t)$$

where A , the current gain = 10.

Typical coilless detector output level is:

$$V_{out(peak)} = (f_{peak dev}/f_{IF}) \cdot A \cdot i \cdot R_I$$

For example, if peak deviation is 25 kHz, $i = 250 \mu A$ at $f_{IF} = 10.7$ MHz, and R_I is 50 k Ω ; then V_{out} is 292 mVp or 584 mVpp.

The AFT Out pin is capable of voltage swings from about 300 mV to $V_{CC} - 300$ mV. At these extreme values, the AFT circuit can become saturated and very long detector lock-up times may be observed. It is best, therefore, to limit the AFT Out swing from about 500 mV to $V_{CC} - 500$ mV and attempt to center the AFT Out voltage at $V_{CC}/2$ for a detector lock condition.

As an example, for $V_{CC} = 2.7$ V, the ideal AFT Out voltage at lock would be 1.35 V, with an available swing of 0.5 V to 2.2 V (1.7 V total). If the AFT tuning range is to be ± 500 kHz, this corresponds to an adjustment current of $1.0 \text{ MHz}/f_{IF} \cdot i$. From Figure 11, to set f_{IF} at 10.7 MHz, i is approximately 240 μA , and the total adjustment current range is therefore about 22.4 μA over a 1.7 V total swing, or $R_t = 75.9$ k. At lock,

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current equaling $(AFT\ Out - F_{adj})/R_t$ will be flowing into the F_{adj} node. This current then is approximately $(1.35\ V -$

$0.7\ V)/75.9\ k\Omega$ or $8.6\ \mu A$. The F_{adj} resistor, R_f , is therefore equal to $0.7\ V/(240\ \mu A + 8.6\ \mu A)$ or about $2.82\ k\Omega$.

Figure 11. Fadj Current versus IF Frequency

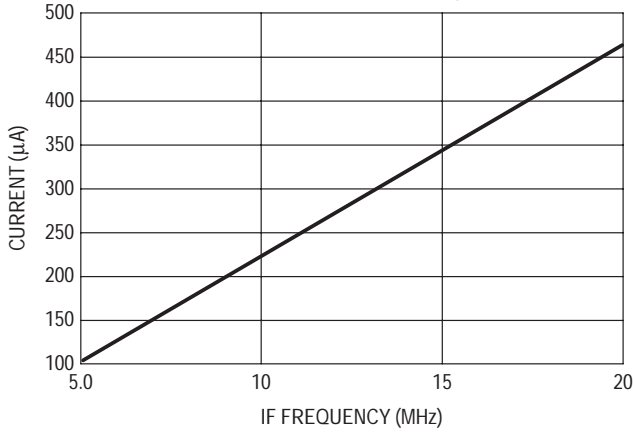


Figure 12. Fadj Resistor versus IF Frequency

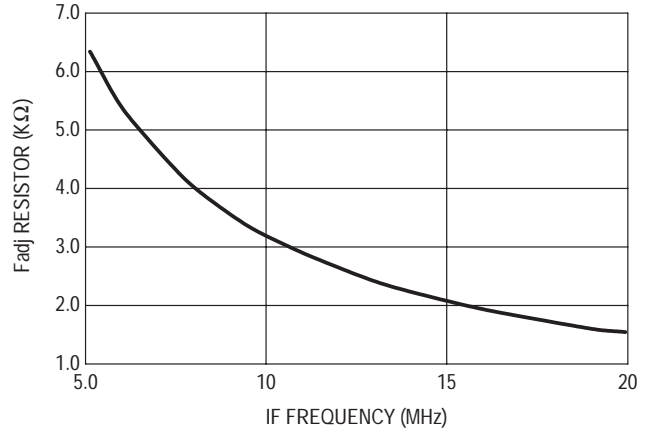


Figure 13. BWadj Resistor versus BWadj Current

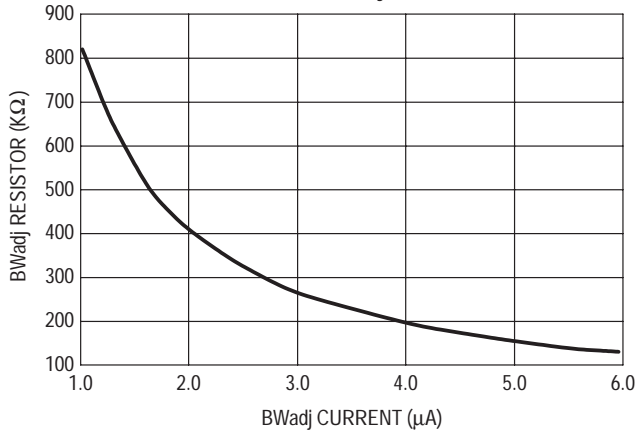
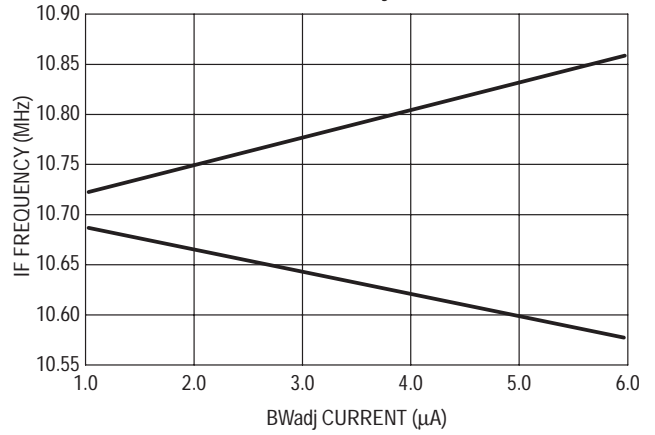


Figure 14. IF Frequency versus BWadj Current

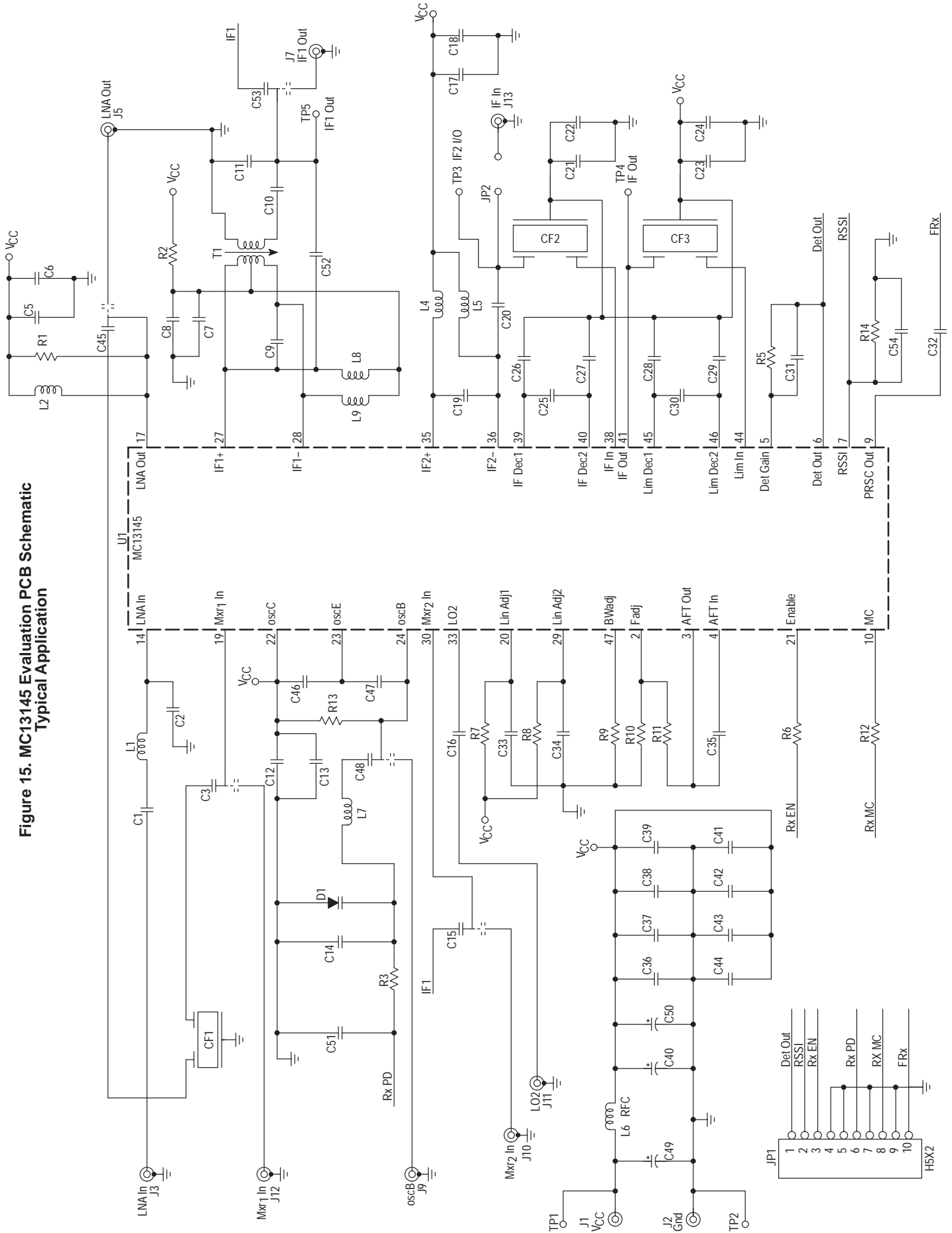


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Table 1. LNA S-Parameters: 3.6 Vdc

Freq (MHz)	S11 Mag	S11 Ang	S21 Mag	S21 Ang	S12 Mag	S12 Ang	S22 mag	S22 Ang
25	0.84	-3.0	10.8	176	0.00005	-27	1.0	-1.2
50	0.84	-71	10.7	171	0.0004	76	1.0	-3.7
100	0.83	-15	10.3	162	0.0006	61	0.99	-4.9
150	0.81	-22	10.	154	0.0011	91	0.99	-7.3
200	0.78	-28	9.6	147	0.001	60	0.99	-9.7
300	0.73	-41	9.0	132	0.002	42	0.99	-15
400	0.66	-50	7.8	116	0.00070	22	0.95	-19
450	0.64	-54	7.4	111	0.0014	39	0.96	-21
500	0.62	-59	7.0	106	0.0009	69	0.96	-23
750	0.51	-77	5.5	80	0.0013	-51	0.94	-33
800	0.49	-80	5.2	75	0.002	-80	0.93	-36
850	0.47	-81	4.9	71	0.004	-120	0.92	-37
900	0.46	-82	4.6	67	0.0057	-130	0.92	-38
950	0.44	-82	4.3	62	0.008	-142	0.91	-40
1000	0.45	-81	3.9	58	0.014	-162	0.95	-41
1250	0.55	-94	3.5	47	0.029	140	0.099	-50
1500	0.48	-120	3.1	24	0.02	63	0.94	-65
1750	0.43	-126	2.5	6.9	0.0066	79	0.93	-74
2000	0.43	-135	2.1	-9.9	0.0099	129	0.92	-85
2250	0.45	-145	1.8	-27	0.017	133	0.91	-96
2500	0.47	-155	1.5	-43	0.021	132	0.89	-106
2750	0.51	-167	1.2	-60	0.03	130	0.88	-118
3000	0.55	-180	1.0	-78	0.039	120	0.85	-129

Figure 15. MC13145 Evaluation PCB Schematic
Typical Application



MC13145

Figure 18. Evaluation PCB Ground Plane

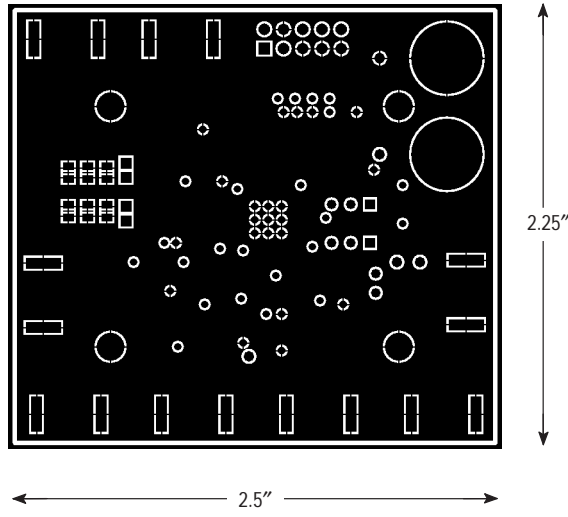
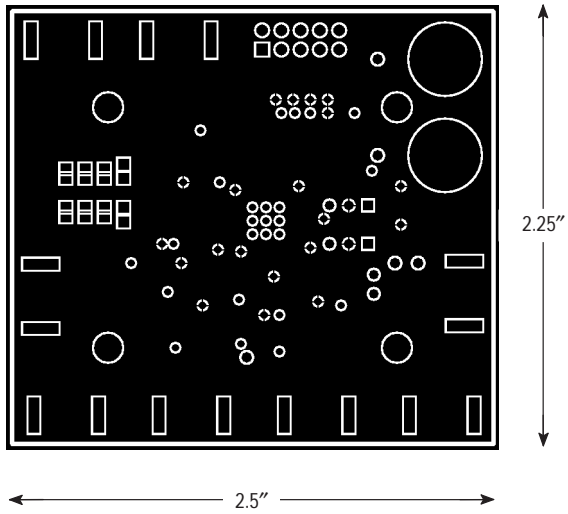


Figure 19. Evaluation PCB Power Plane





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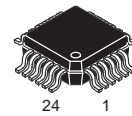
Low Power Integrated Transmitter for ISM Band Applications

The MC13146 is an integrated RF transmitter targeted at ISM band applications. It features a 50 Ω linear Mixer with linearity control, voltage controlled oscillator, divide by 64/65 dual modulus Prescaler and Low Power Amplifier (LPA). Together with the receiver chip (MC13145) and either baseband chip (MC33410 or MC33411A/B), a complete 900 MHz cordless phone system can be implemented. This device may be used in applications up to 1.8 GHz.

- Low Distortion LPA: P_{out_1 dB} Compression Point ≈ 10 dBm
- High Mixer Linearity: IIP3 = 10 dBm
- 50 Ω Mixer Input Impedance
- Differential Open Collector Mixer Output
- Low Power 64/65 Dual Modulus Prescaler (MC12054 type)
- 2.7 to 6.5 V Operation, Low Current Drain (25 mA @ 2.0 GHz)
- Powerdown Mode: <60 μA
- Usable up to 1.8 GHz

LOW POWER DC – 1.8 GHz TRANSMITTER

SEMICONDUCTOR TECHNICAL DATA

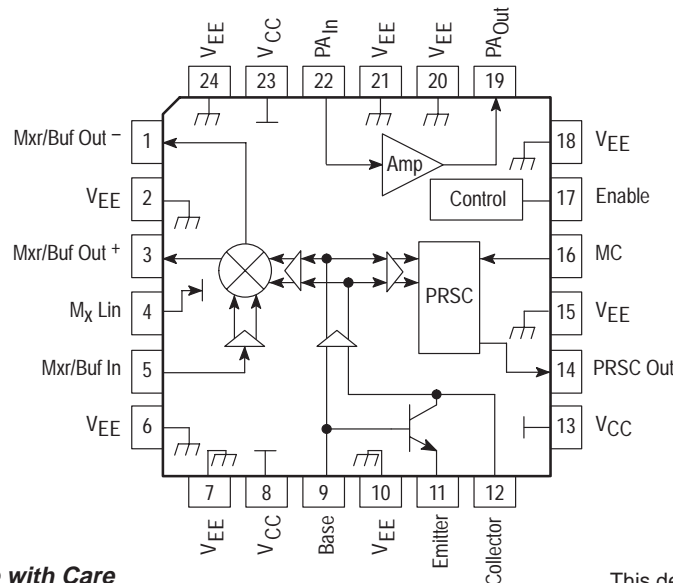


FTA SUFFIX
 PLASTIC PACKAGE
 CASE 977
 (LQFP-24)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13146FTA	T _A = -20 to 70°C	LQFP-24

PIN CONNECTIONS



ESD Sensitive — Handle with Care

This device contains 268 active transistors.

MC13146

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Power Supply Voltage	$V_{CC(max)}$	7.0	Vdc
Junction Temperature	$T_J(max)$	150	°C
Storage Temperature Range	T_{stg}	-65 to 150	°C

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions, Electrical Characteristics tables or Pin Descriptions section.
2. Meets Human Body Model (HBM) ≤ 100 V and Machine Model (MM) ≤ 25 V. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Power Supply Voltage ($T_A = 25^\circ\text{C}$)	V_{CC} V_{EE}	2.7 -	- 0	6.5 -	Vdc Vdc
RF Frequency Range	f_{RF}	1.0	-	2500	MHz
Ambient Temperature Range	T_A	-20	-	70	°C
Maximum Input Signal Level	P_{IF}	-	-10	-	dBm
- with no damage		-	15	-	dBm
- with minor performance degradation		-		-	

TRANSMITTER DC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, $V_{CC} = 3.6$ Vdc, no input signal, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Total Supply Current (Enable = V_{CC})	I_{total}	15	18	21	mA
Power Down Current (Enable = V_{EE})	I_{total}	-	30	100	μA
MC Current Input (High)	I_{ih}	70	100	130	μA
MC Current Input (Low)	I_{il}	-130	-100	-70	μA
Input high voltage	V_{ih}	$V_{CC} - 0.4$	-	-	V
Input low voltage	V_{il}	-	-	0.4	V
Input Current	I_{in}	-50	-	50	μA

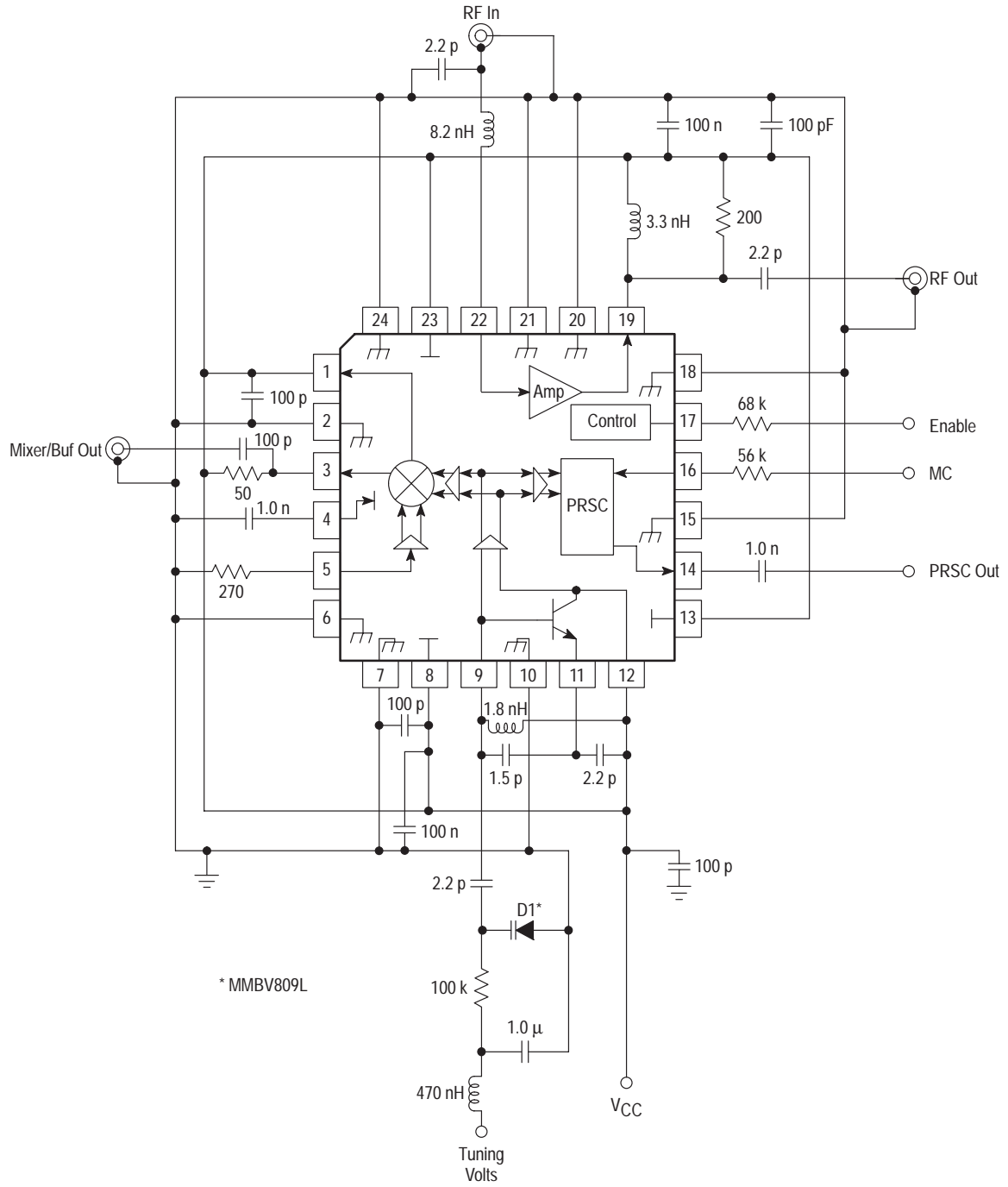
TRANSMITTER AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, $V_{CC} = 3.6$ Vdc, Enable = 3.6 Vdc, per Test Circuit shown in Figure 1, unless otherwise noted)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
Amplifier Output Power (with external matching) @ 950 MHz; $P_{in} = -19$ dBm	PA_{in}	PA_{out}	PA_{PO}	-4.5	-3.3	-2.1	dBm
Amplifier 1.0 dB Compression Point (@ 950 MHz = f_{IF_out})	PA_{in}	PA_{out}	$P_{1dBc.Pt.}$	-	8.0	-	dBm
Amplifier Output Harmonics (with external matching) @ 950 MHz; $P_{in} = -19$ dBm	PA_{in}	PA_{out}					dBc
2nd			$PA - 2f$	-25	-37	-	
3rd			$PA - 3f$	-35	-52	-	
Mixer/Buffer Output (@ 950 MHz = f_{osc} ; Mixer input (Pin 5) pulled through 270 Ω resistor)		Buf_out+	PMx/Buf_out	-19	-18	-17	dBm
PLL Setup Time [Note 1]	MC	$PRSC_{out}$	T_{PLL}	-	10	-	nS
Mixer Input Third Order Intercept Point			IIP3	-	10	-	dBm
VCO Phase Noise (@ 10 kHz offset)		Buf_out+		-	-80	-	dBc/Hz
Prescaler Output Level (10 k \parallel 8.0 pF Load)		$PRSC_{out}$		400	-	600	mVpp

- NOTES:** 1. MC input (50%) to $PRSC_{out}$ rising output (50%) for proper modulus selection.
2. Typical performance parameters indicate the potential of the device under ideal operation conditions.

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Figure 1. Test Circuit



MC13146

PIN FUNCTION DESCRIPTION

Pin	Symbol/Type	Description	Description
1, 3	Mxr/Buf Out-, Mxr/Buf Out+		<p>Mixer/Buffer Outputs The Mixer/Buffer is a differential open collector configuration which designed to use over a wide frequency range for up conversion as well as direct conversion. Differential to single-ended circuit configuration and matching options are discussed in the Circuit Description section. 6.0 dB of additional Mixer gain can be achieved by conjugately matching the outputs at the desired RF frequency.</p>
2	V _{EE}		<p>V_{EE}, Negative Supply This pin is V_{EE} supply for the mixer IF output. In the application PC board this pin is tied to a common V_{EE} trace with other V_{EE} pins.</p>
4	Mx Lin		<p>Mixer Linearity Control The mixer linearity control circuit accepts approximately 0 to 200 μA control current to set the dynamic range of the mixer. An Input Third Order Intercept Point, IIP3 of 17 dBm may be achieved at 200 μA of control current.</p>
5	Mxr/Buf In		<p>Mixer/Buffer Input The mixer input impedance is broadband 50 Ω for applications up to 2.4 GHz.</p>
6, 7, 18, 24	V _{EE}		<p>V_{EE}, Negative Supply These pins are substrate connections on the IC. In the application PC board these pins are tied to a common V_{EE} trace with other V_{EE} pins.</p>
8	V _{CC}		<p>V_{CC}, Supply Voltage Two V_{CC} pins are provided for the Local Oscillator and LO Buffer Amplifier. The operating supply voltage range is from 2.7 Vdc to 6.5 Vdc. In the PCB layout, the V_{CC} trace must be kept as wide as feasible to minimize inductive reactances along the trace. V_{CC} should be decoupled to V_{EE} at the IC pin.</p>
9	Base		<p>On-board VCO Transistor The transistor has the emitter, base, collector, V_{CC} and V_{EE} pins available. Internal biasing which is compensated for stability over temperature is provided. It is recommended that the base pin is pulled up to V_{CC} through an RFC chosen for the particular oscillator center frequency. The application circuit shows a Colpitts oscillator configuration.</p>
10	V _{EE}		
11	Emitter		
12	Collector		

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PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
13	V _{CC}		V_{CC}, Supply Voltage
14	PRSC Out		Prescaler Output The prescaler output provides 500 mVpp drive to the F _{in} Pin of a PLL synthesizer. Conjugately matching the interface will increase the drive delivered to the PLL input.
15	V _{EE}		V_{EE}, Negative Supply
16	MC		Dual Modulus Control Current Input This requires a current input of typically 200 μApp.
17	Enable		Transmitter Enable Enable the transmitter by pulling the pin up to V _{CC} .
19	PA _{out}		PA Out The output is an open collector of the cascode transistor low power amplifier (LPA); it is externally biased. The output may be conjugately matched with a shunt L, and series L and C network.
20, 21	V _{EE}		V_{EE}, Negative Supply V _{EE} pin is taken to an ample dc ground plane through a low impedance path. The path should be kept as short as possible. A two sided PCB is implemented so that ground returns can be easily made through via holes.
22	PA _{in}		PA In The input is the base of the common emitter transistor. Minimum external matching is required to optimize the input return loss and gain.
23	V _{CC}		V_{CC}, Positive Supply V _{CC} pin is taken to the incoming positive battery or regulated dc voltage through a low impedance trace on the PCB. It is decoupled to V _{EE} ground at the pin of the IC.

MC13146

CIRCUIT DESCRIPTION

General

The MC13146 consists of a low power amplifier, a 50 Ω linear mixer with linearity control, divide by 64/65 dual modulus prescaler and LPA. This device is designated for use as the low power transmitter in analog and digital FM systems such as UHF and 800 MHz Special Mobile Radio (SMR), UHF Family Radio Services, PCS and 902 to 928 MHz cordless telephones. It features a mixer linearity control to preset or auto program the mixer dynamic range, an enable function and a wideband mixer output so the IC may be used either as an upconverter or for a direct conversion source. Additional details are covered in the Pin by Pin Description which shows the equivalent internal circuit and external circuit requirements.

Current Regulation/Enable

The device features temperature compensating, voltage independent current regulators which are controlled by the enable function in which "high" powers up the IC.

Mixer: General

The mixer is a double-balanced four quadrant multiplier biased class AB allowing for programmable linearity control via an external current source. An input third order intercept point of 20 dBm has been achieved. The mixer has a 50 Ω single-ended RF input and open collector differential outputs. An onboard Local Oscillator transistor has the emitter, base and collector pinned out to implement a low phase noise VCO in various configurations. Additionally, a buffered prescaler output is provided for operation with a low frequency synthesizer. For direct conversion applications the input of the mixer may be terminated to ground through a 120 to 330 Ω resistor.

Local Oscillator/Voltage Control Oscillator

The on-chip transistor operates with coaxial transmission line or LC resonant elements to over 1.8 GHz. Biasing is done with a temperature/voltage compensated current source in the emitter. A RFC from V_{CC} to the base is recommended.

The transistor can be operated in the classic Colpitts, Clapp, or Hartley configuration. The application circuit (Figure 8) depicts a parallel resonant VCO which can cover the entire 902 to 928 MHz frequency band with phase noise of approximately -80 dBc/Hz at a 10 kHz offset (see Figure 2). For this configuration, the LO will be driven with approximately 100 mV_{rms}, and the frequency of oscillation can be approximated by:

$$F_{osc} = \frac{1}{\left(2\pi \sqrt{\left(\frac{C1 C2}{C1 + C2} \right) \left(\frac{C3 C_v}{C3 + C_v} + 3.6 \text{ pF} \right) (L1 + 1.8 \text{ nH})} \right)}$$

where C_v is the equivalent capacitance of the varactor at the control voltage.

For higher frequency operation, a series tuned oscillator configuration is recommended. Table 1 contains the S-parameters for the VCO transistor in a common collector configuration. This information is useful for designing a VCO at other operating frequencies or for various other oscillator topologies.

The output power (at Mix/Buf Out) can be varied by adjusting the value of R5 as illustrated in Figures 3 and 4. Figure 5 shows the typical operating window for the prescaler.

Figure 2. Typical Tuning Performance

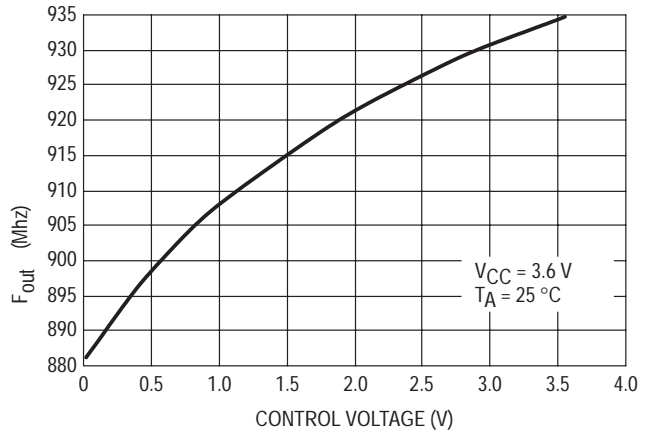


Figure 3. Mixer/Buffer Output versus 1st LO Input

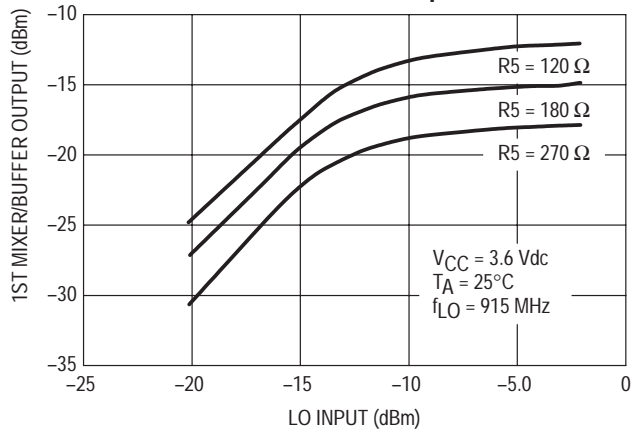


Figure 4. Test Circuit for Figure 3.

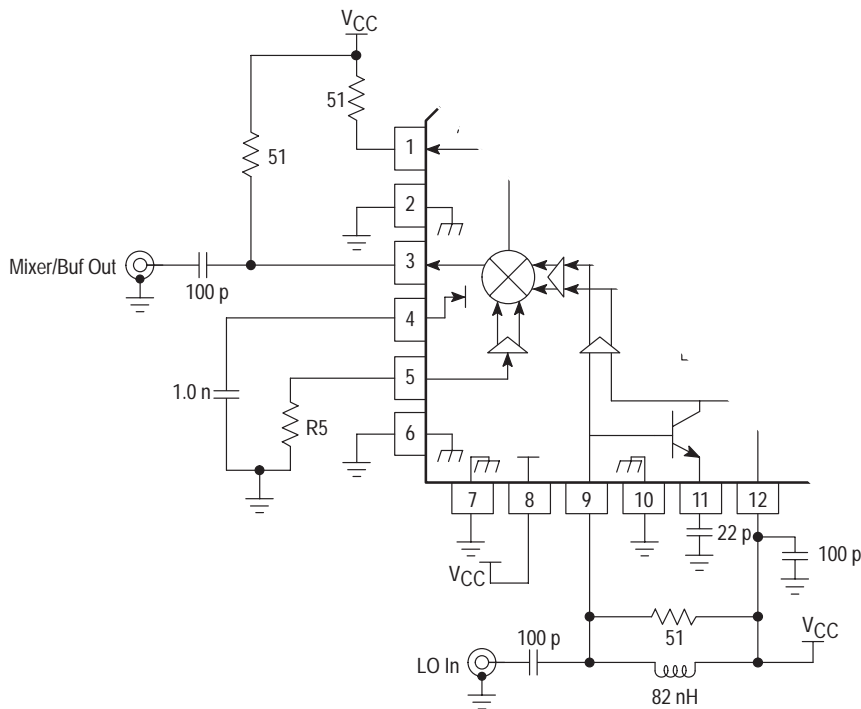
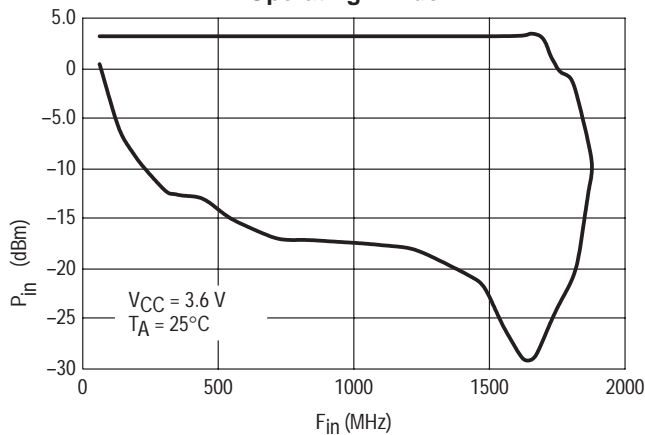


Figure 5. Typical Prescaler Operating Window



Mixer/Buffer Input

The Mixer/Buf In pin is a broadband, 50 Ω input used to drive the IF port of the mixer (see Table 2, S11 parameters). The Mixer/Buf In pin can be used in one of three modes:

11. A IF signal can be applied to this pin and up-converted to the desired RF frequency.
12. A resistor can be connected to ground, controlling the RF output power.
13. A resistor can be connected to V_{CC} , disabling the entire mixer.

The linear gain of the Mixer/Buf when used as a buffer is approximately -5.0 to -8.0 dB.

Mixer/Buffer Outputs

The mixer outputs (Mixer/Buf Out + and Mixer/Buf Out $-$) are balanced, open collector. A shunt resistor of 200 Ω minimum to V_{CC} is recommended for stability.

The outputs can be used as a single-ended driver or connected in a balanced-to-unbalanced configuration. If the single-ended driver configuration is used, the unused output must be tied directly to V_{CC} . For the balanced-to-unbalanced configuration, an additional 3.0 to 6.0 dB of power gain can be achieved. Conjugate matching is easily accomplished to the desired load by the addition of a shunt and series element (see Table 2, S22 parameters).

Low Power Amplifier (LPA)

The LPA is internally biased at low supply current (approximately 2.0 mA emitter current) for optimal low power operation, yielding a 10 dBm 1.0 dB output power compression point. Input and output matching may be achieved at various frequencies using few external components (see Table 3 S-parameters). Typical power gain is 16 dB with the input/output conjugately matched to the source/load impedance. A minimum 200 Ω shunt resistor from the output to V_{CC} is recommended for stability.

Figure 6. I_{CC} versus Temperature

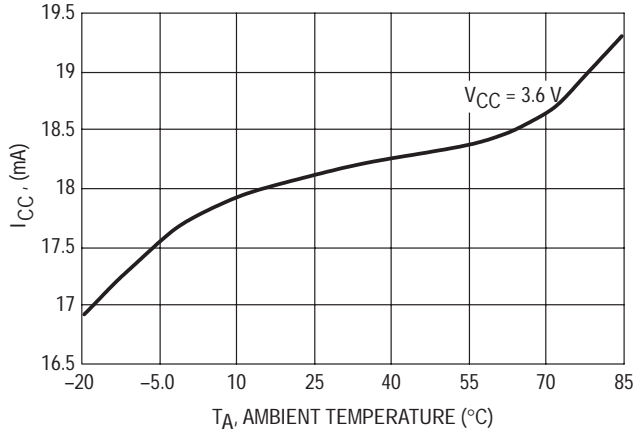
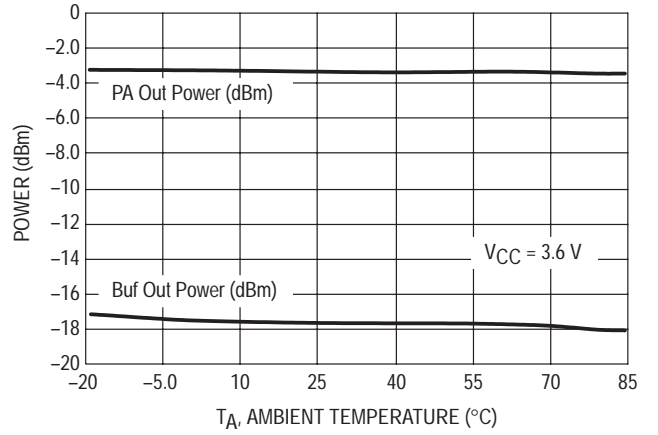
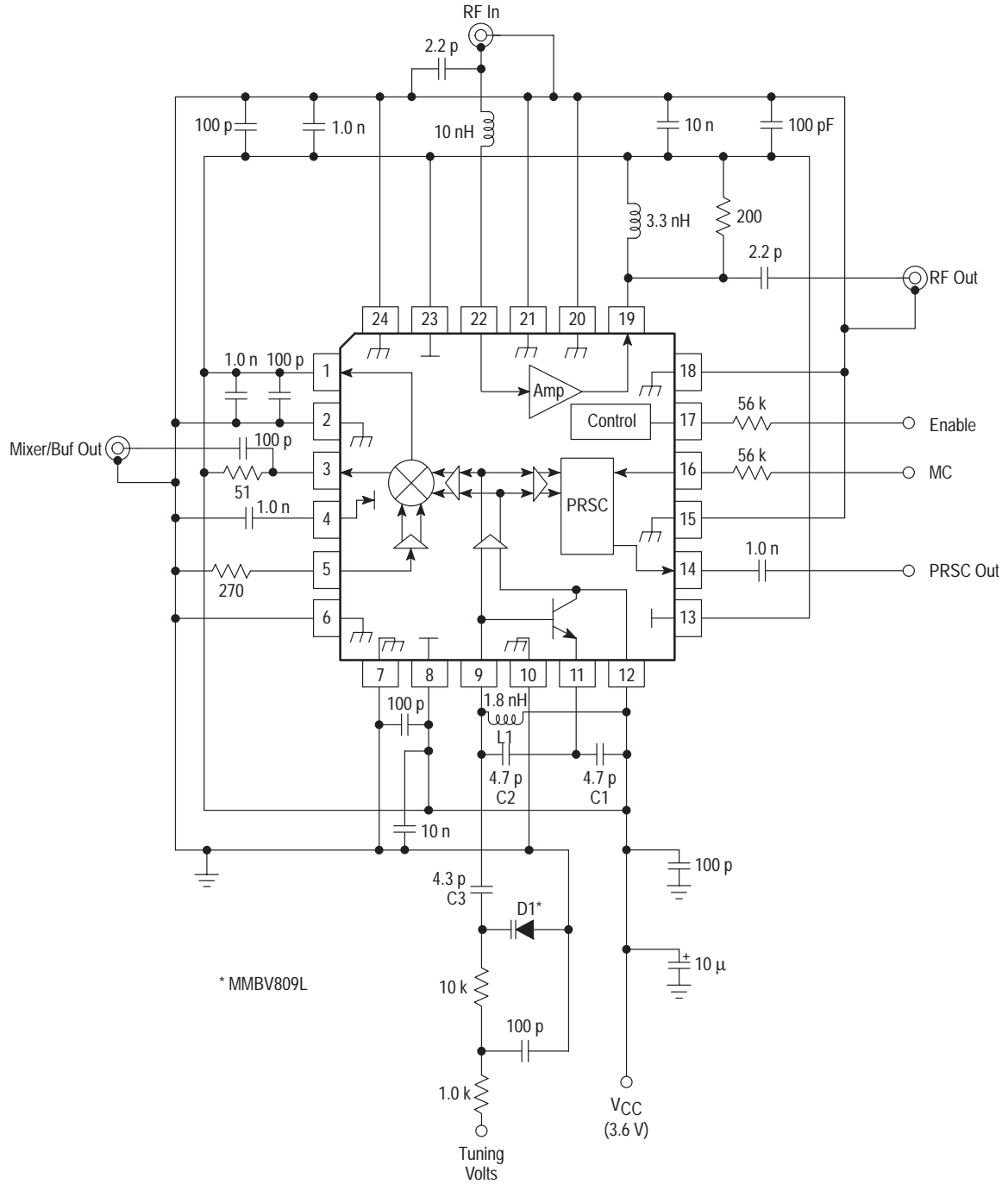


Figure 7. Output Power versus Temperature



MC13146

Figure 8. Applications Circuit



MC13146

Evaluation PCB

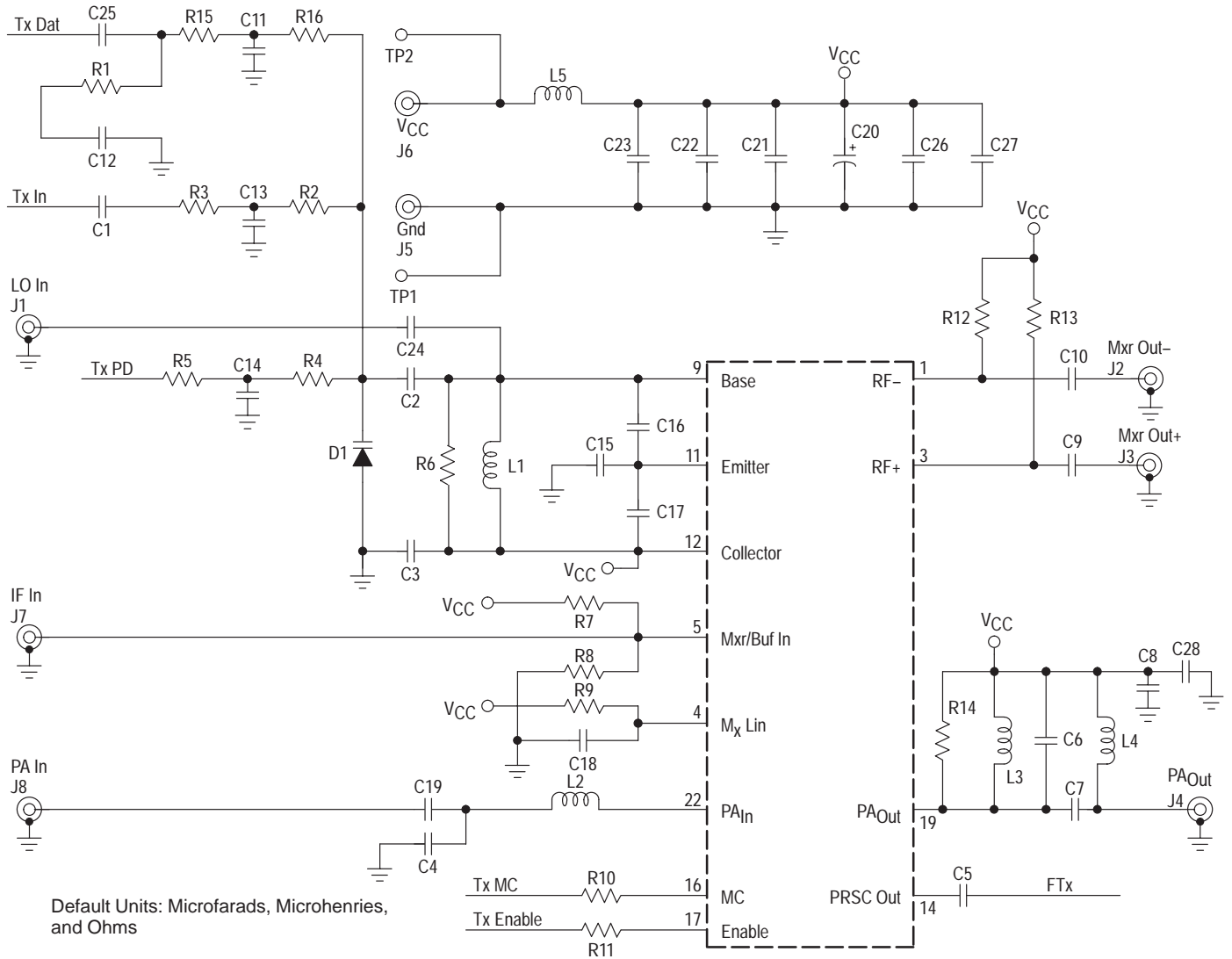
The evaluation PCB is a versatile board which allows the MC13146 to be configured as a basic transmitter, or to characterize individual operating parameters.

The general purpose schematic and associated parts list for the PCB is given in Figure 9. This parts list build-up is

identical to the Test Circuit illustrated in Figure 1, although parameters can vary significantly due to differences in PCB parasitics. Figures 10, 11, and 12 show the actual PCB component, ground and solder sides, respectively.

Please refer to AN1687/D and AN1691/D for additional details and applications for the device.

Figure 9. Evaluation PCB Schematic

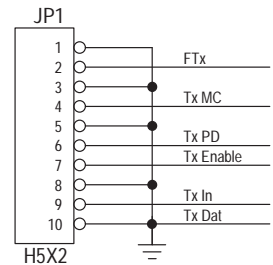


Default Units: Microfarads, Microhenries, and Ohms

R1,R2,R3,R15,R16,
C1,C11,C12,C13,C25,
R6,R7,R9,L4,J1,J2,J7,
C6,C10,C15,C24
R4
R5,R12,C19
R8
R10
R11
R13
R14
C2
C3,C8,C9,C26,C27
C4, C7
C5,C18,C21,C22,C23
C14

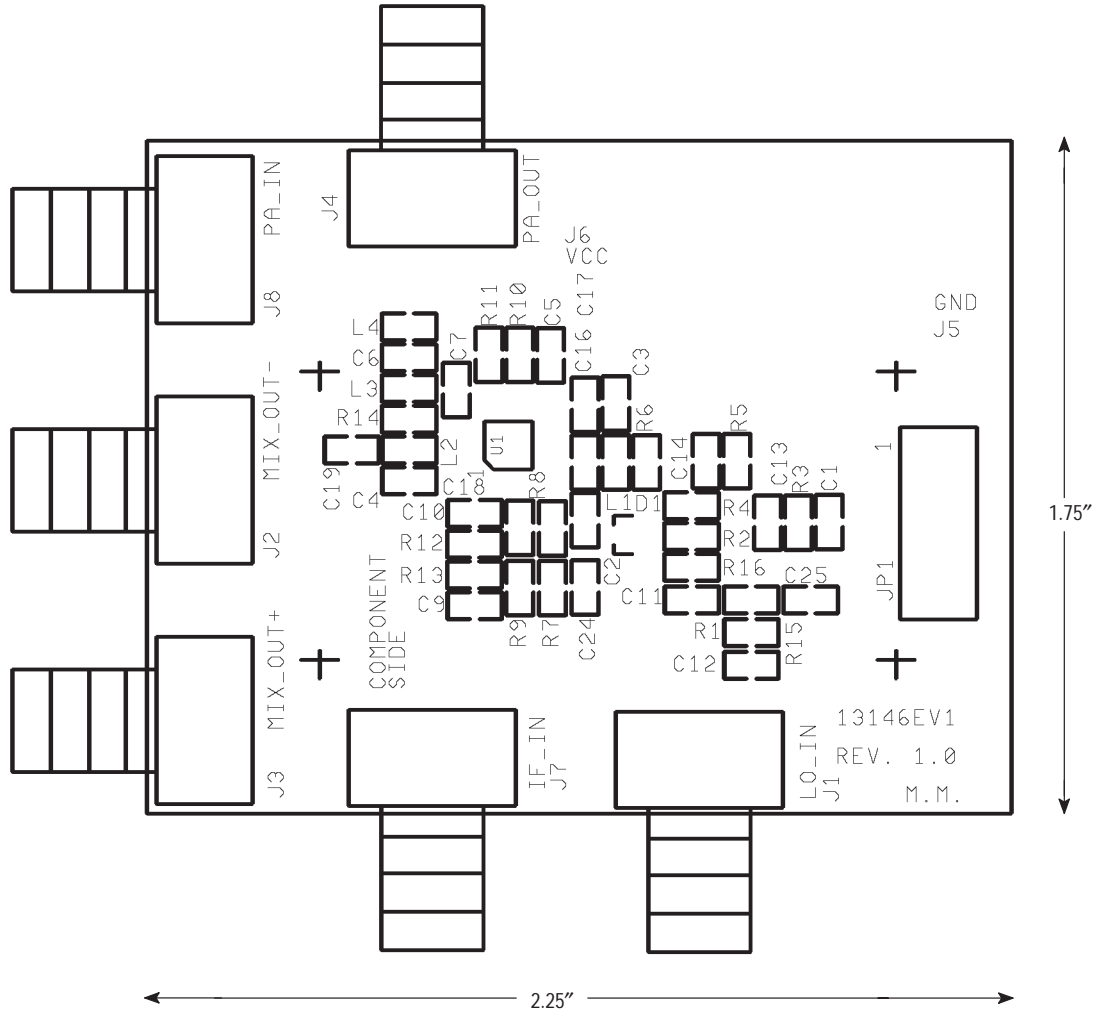
No component
100 k
Short
270
56 k
68 k
51
200
2.2 p
100 p
2.2 p
1.0 n
1.0 μ

C16 1.5 p
C17 2.2 p
C20 10 μ
C28 10 n
L1 1.8 n
L2 8.2 n
L3 3.3 n
L5 RFC
D1 MMBV809LT1
J3,J4,J8 SMA EF Johnson 142-0701-851
J5,J6 Banana Johnson Components 108-0902-001
JP1 Header, 5x2
U1 MC13146FTA



MC13146

Figure 10. MC13146 Evaluation PCB Component Side



MC13146

Figure 11. MC13146 Evaluation PCB Ground Plane

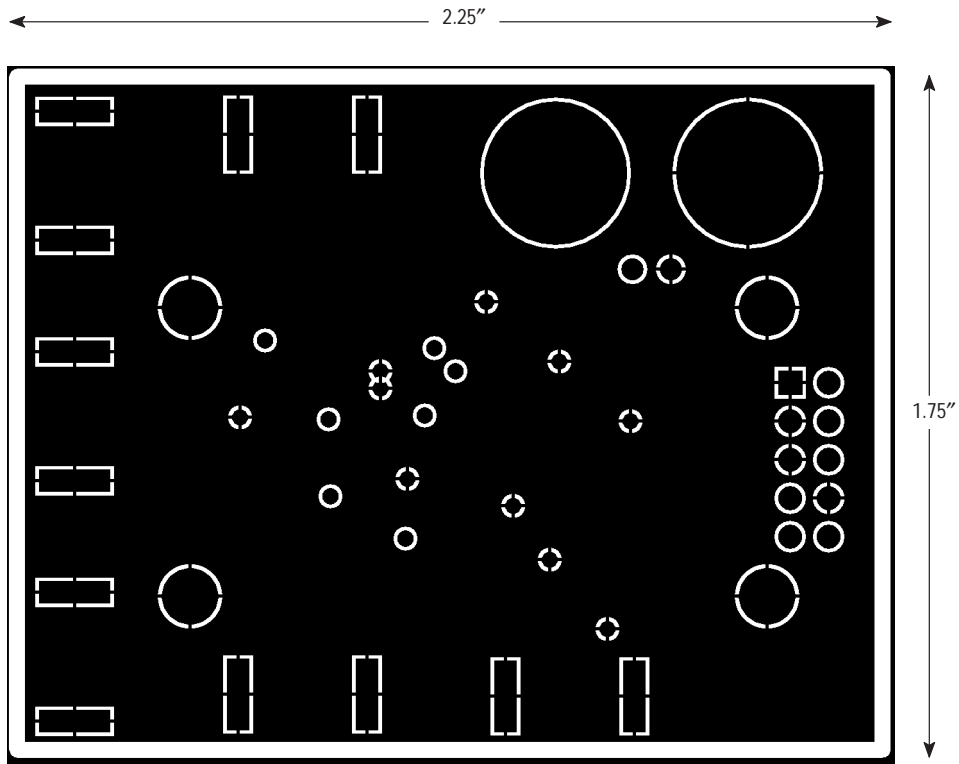
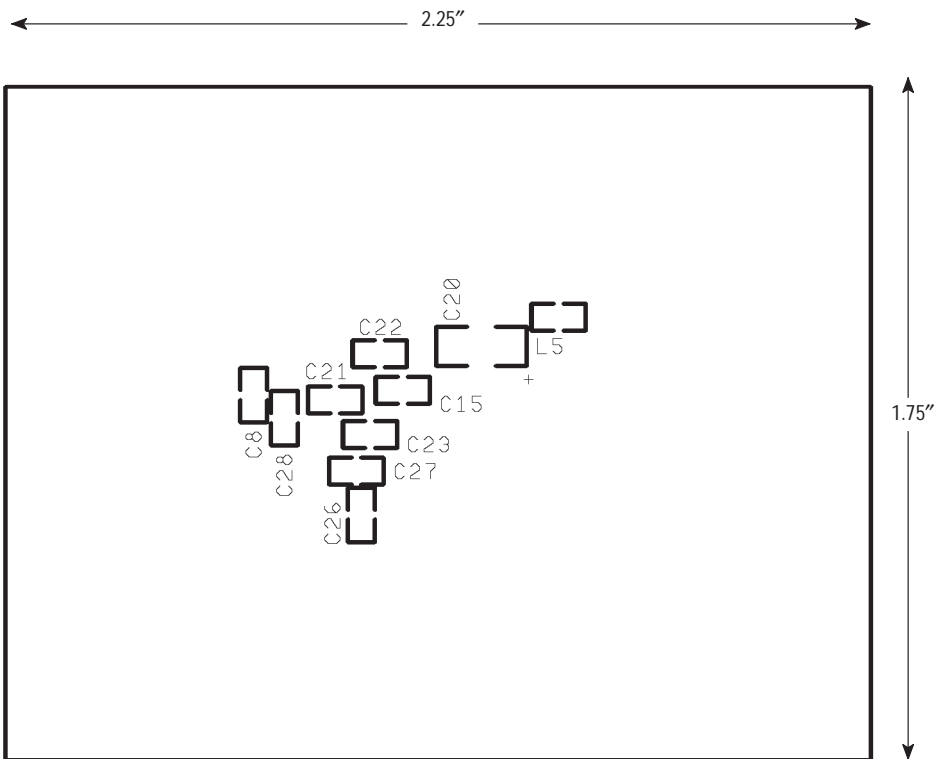


Figure 12. MC13146 Evaluation PCB Solder Side



MC13146

Table 1. VCO Transistor S-Parameters 3.6 Vdc; 50 Ω Load and Source Impedance; Common Collector

Freq (MHz)	S11 Mag	S11 Ang	S21 Mag	S21 Ang	S12 Mag	S12 Ang	S22 Mag	S22 Ang
25	0.99	-1	0.88	0	0.01	44	0.10	-7
50	0.99	-2	0.92	-1	0.02	61	0.09	-9
100	0.98	-5	0.95	-2	0.04	70	0.07	-37
150	0.98	-7	0.97	-3	0.06	73	0.07	-47
200	0.97	-10	1.04	-4	0.07	73	0.06	-86
300	0.95	-14	1.11	-8	0.10	71	0.09	-124
400	0.93	-19	1.23	-12	0.13	67	0.14	-149
450	0.92	-21	1.26	-14	0.15	66	0.15	-155
500	0.91	-23	1.30	-16	0.16	65	0.17	-159
600	0.86	-28	1.35	-20	0.19	61	0.20	-167
750	0.79	-37	1.46	-25	0.24	57	0.26	-172
800	0.79	-39	1.48	-26	0.25	56	0.28	-174
850	0.77	-42	1.48	-28	0.26	54	0.29	-177
900	0.74	-44	1.47	-31	0.28	52	0.28	-179
950	0.67	-49	1.53	-35	0.30	49	0.31	174
1000	0.61	-55	1.59	-38	0.33	47	0.34	171
1250	0.45	-81	1.61	-50	0.41	38	0.38	157
1500	0.35	-159	1.68	-67	0.53	16	0.38	134
1750	0.85	107	1.60	-100	0.57	-15	0.33	97
2000	1.02	76	1.17	-117	0.47	-32	0.18	86
2250	1.25	76	1.13	-125	0.55	-38	0.19	89
2500	1.58	53	0.84	-150	0.56	-64	0.09	57

MC13146

Table 2. Mixer Input/Output S-Parameters: 200 Ω Pull-Up Resistor

Freq (MHz)	S11 Mag	S11 Ang	S21 Mag	S21 Ang	S12 Mag	S12 Ang	S22 Mag	S22 Ang
50	0.11	176.8	0.43	-4.2	0.001	38.7	0.60	-1.9
100	0.11	177.9	0.43	-7.5	0.002	19.8	0.60	-3.5
200	0.11	179.4	0.42	-13.7	0.001	28.3	0.60	-6.7
300	0.10	179.5	0.42	-20.7	0.001	69.8	0.61	-9.9
400	0.10	177.2	0.42	-27.3	0.001	106.3	0.61	-13.2
450	0.11	174.9	0.41	-31.1	0.001	135.2	0.62	-14.8
500	0.10	177.7	0.42	-34.1	0.002	138.2	0.62	-16.6
600	0.09	174.3	0.42	-41.8	0.003	150.5	0.63	-20.0
700	0.09	167.2	0.41	-49.3	0.005	158.7	0.64	-23.5
750	0.08	162.8	0.41	-53.9	0.006	166.0	0.65	-25.2
800	0.08	156.6	0.40	-58.4	0.008	166.5	0.65	-26.9
850	0.06	152.3	0.40	-62.7	0.009	171.2	0.66	-28.7
900	0.05	145.2	0.39	-66.4	0.012	177.6	0.66	-30.3
950	0.04	131.1	0.38	-71.6	0.015	-179.7	0.67	-31.9
1000	0.02	101.1	0.38	-76.7	0.019	178.0	0.68	-33.7
1250	0.08	-41.5	0.27	-96.8	0.042	137.1	0.73	-43.2
1500	0.40	-87.6	0.24	-90.2	0.036	129.9	0.78	-53.3
1750	0.50	-144.1	0.30	-114.0	0.058	142.8	0.86	-63.8
2000	0.51	-173.5	0.22	-133.0	0.174	151.6	0.96	-81.3

Table 3. LPA S-Parameters: 200 Ω Pull-Up Resistor

Freq (MHz)	S11 Mag	S11 Ang	S21 Mag	S21 Ang	S12 Mag	S12 Ang	S22 Mag	S22 Ang
200	0.76	-26.0	9.3	148.1	0.0006	73.3	0.60	-12.4
300	0.71	-37.5	8.5	135.2	0.0011	74.4	0.60	-18.5
400	0.67	-47.2	7.6	124.5	0.0011	79.6	0.61	-24.6
450	0.64	-51.7	7.2	118.6	0.0010	66.0	0.62	-28.3
500	0.62	-55.4	6.9	114.2	0.0011	45.4	0.62	-31.6
600	0.58	-63.7	6.3	105.3	0.0012	16.7	0.64	-38.8
700	0.54	-72.1	5.6	95.2	0.0016	-20.9	0.66	-45.6
750	0.52	-74.6	5.4	91.8	0.0013	-36.9	0.66	-48.5
800	0.51	-77.9	5.2	87.7	0.0023	-50.8	0.67	-52.6
850	0.49	-80.3	5.0	83.8	0.0033	-63.6	0.68	-56.1
900	0.49	-83.5	4.7	79.6	0.0044	-78.7	0.68	-60.3
950	0.48	-85.4	4.5	77.2	0.0060	-90.3	0.68	-63.2
1000	0.48	-88.8	4.3	74.7	0.0082	-97.6	0.68	-65.8
1250	0.51	-102.7	3.7	58.8	0.0249	-136.6	0.73	-74.6
1500	0.48	-119.7	3.3	37.6	0.0273	172.0	0.90	-87.7
1750	0.47	-130.0	2.7	20.5	0.0290	166.5	0.97	-103.7
2000	0.51	-136.7	2.2	-1.1	0.0386	164.1	1.01	-119.1



MC13150

Narrowband FM Coilless Detector IF Subsystem

The MC13150 is a narrowband FM IF subsystem targeted at cellular and other analog applications. Excellent high frequency performance is achieved, with low cost, through use of Motorola's MOSAIC 1.5™ RF bipolar process. The MC13150 has an onboard Colpitts VCO for Crystal controlled second LO in dual conversion receivers. The mixer is a double balanced configuration with excellent third order intercept. It is useful to beyond 200 MHz. The IF amplifier is split to accommodate two low cost cascaded filters. RSSI output is derived by summing the output of both IF sections. The quadrature detector is a unique design eliminating the conventional tunable quadrature coil.

Applications for the MC13150 include cellular, CT-1 900 MHz cordless telephone, data links and other radio systems utilizing narrowband FM modulation.

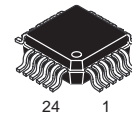
- Linear Coilless Detector
- Adjustable Demodulator Bandwidth
- 2.5 to 6.0 Vdc Operation
- Low Drain Current: < 2.0 mA
- Typical Sensitivity of 2.0 μV for 12 dB SINAD
- IIP3, Input Third Order Intercept Point of 0 dBm
- RSSI Range of Greater Than 100 dB
- Internal 1.4 kΩ Terminations for 455 kHz Filters
- Split IF for Improved Filtering and Extended RSSI Range

ORDERING INFORMATION

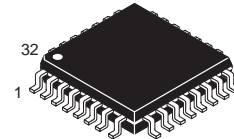
Device	Operating Temperature Range	Package
MC13150FTA	T _A = -40 ° to +85°C	LQFP-24
MC13150FTB		LQFP-32

NARROWBAND FM COILLESS DETECTOR IF SUBSYSTEM FOR CELLULAR AND ANALOG APPLICATIONS

SEMICONDUCTOR TECHNICAL DATA

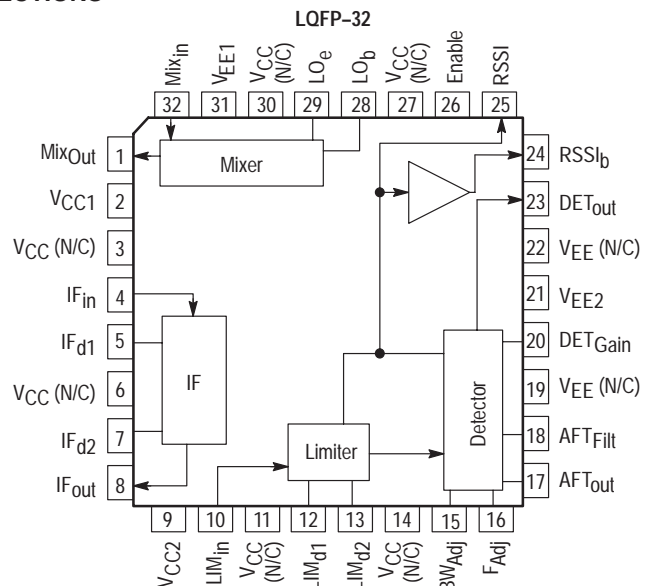
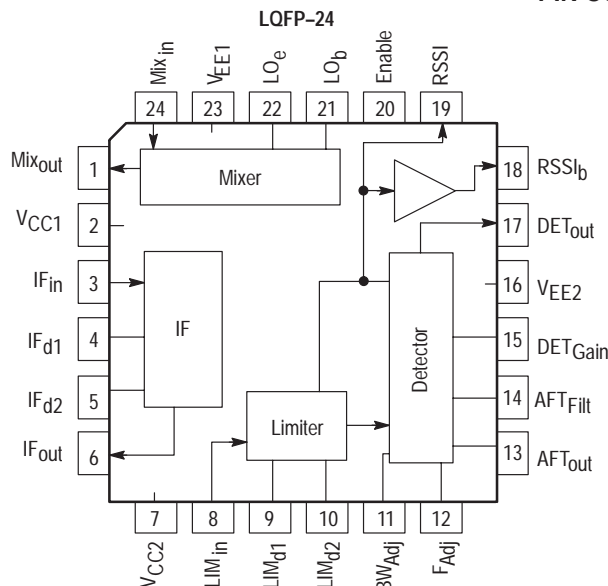


FTA SUFFIX
PLASTIC PACKAGE
CASE 977
(LQFP-24)



FTB SUFFIX
PLASTIC PACKAGE
CASE 873
(LQFP-32)

PIN CONNECTIONS



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13150

MAXIMUM RATINGS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage	2, 9	$V_{CC(max)}$	6.5	Vdc
Junction Temperature	–	T_{Jmax}	+150	°C
Storage Temperature Range	–	T_{stg}	–65 to +150	°C

NOTE: 1. Devices should not be operated at or outside these values. The "Recommended Operating Limits" provide for actual device operation.
2. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage $T_A = 25^\circ\text{C}$ $-40^\circ\text{C} \leq T_A \leq 85^\circ\text{C}$ (See Figure 22)	2, 9 21, 31	V_{CC} V_{EE}	2.5 to 6.0 0	Vdc
Input Frequency	32	f_{in}	10 to 500	MHz
Ambient Temperature Range	–	T_A	–40 to +85	°C
Input Signal Level	32	V_{in}	0	dBm

DC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, $V_{CC1} = V_{CC2} = 3.0$ Vdc, No Input Signal.)

Characteristics	Condition	Pin	Symbol	Min	Typ	Max	Unit
Total Drain Current (See Figure 2)	$V_S = 3.0$ Vdc	2 + 9	I_{TOTAL}	–	1.7	3.0	mA
Supply Current, Power Down (See Figure 3)	–	2 + 9	–	–	40	–	nA

AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, $V_S = 3.0$ Vdc, $f_{RF} = 50$ MHz, $f_{LO} = 50.455$ MHz, LO Level = –10 dBm, see Figure 1 Test Circuit*, unless otherwise specified.)

Characteristics	Condition	Pin	Symbol	Min	Typ	Max	Unit
12 dB SINAD Sensitivity (See Figure 15)	$f_{mod} = 1.0$ kHz; $f_{dev} = \pm 5.0$ kHz	32	–	–	–100	–	dBm
RSSI Dynamic Range (See Figure 7)	–	25	–	–	100	–	dB
Input 1.0 dB Compression Point Input 3rd Order Intercept Point (See Figure 18)	– –	– –	1.0 dB C. Pt. IIP3	– –	–11 –1.0	– –	dBm
Coilless Detector Bandwidth Adjust (See Figure 11)	Measured with No IF Filters	–	ΔBW adj	–	26	–	kHz/ μA

MIXER

Conversion Voltage Gain (See Figure 5)	$P_{in} = -30$ dBm; $PLO = -10$ dBm	32	–	–	10	–	dB
Mixer Input Impedance	Single-Ended	32	–	–	200	–	Ω
Mixer Output Impedance	–	1	–	–	1.5	–	k Ω

LOCAL OSCILLATOR

LO Emitter Current (See Figure 26)	–	29	–	30	63	100	μA
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IF & LIMITING AMPLIFIERS SECTION

IF and Limiter RSSI Slope	Figure 7	25	–	–	0.4	–	$\mu\text{A}/\text{dB}$
IF Gain	Figure 8	4, 8	–	–	42	–	dB
IF Input & Output Impedance	–	4, 8	–	–	1.5	–	k Ω
Limiter Input Impedance	–	10	–	–	1.5	–	k Ω
Limiter Gain	–	–	–	–	96	–	dB

* Figure 1 Test Circuit uses positive (V_{CC}) Ground.

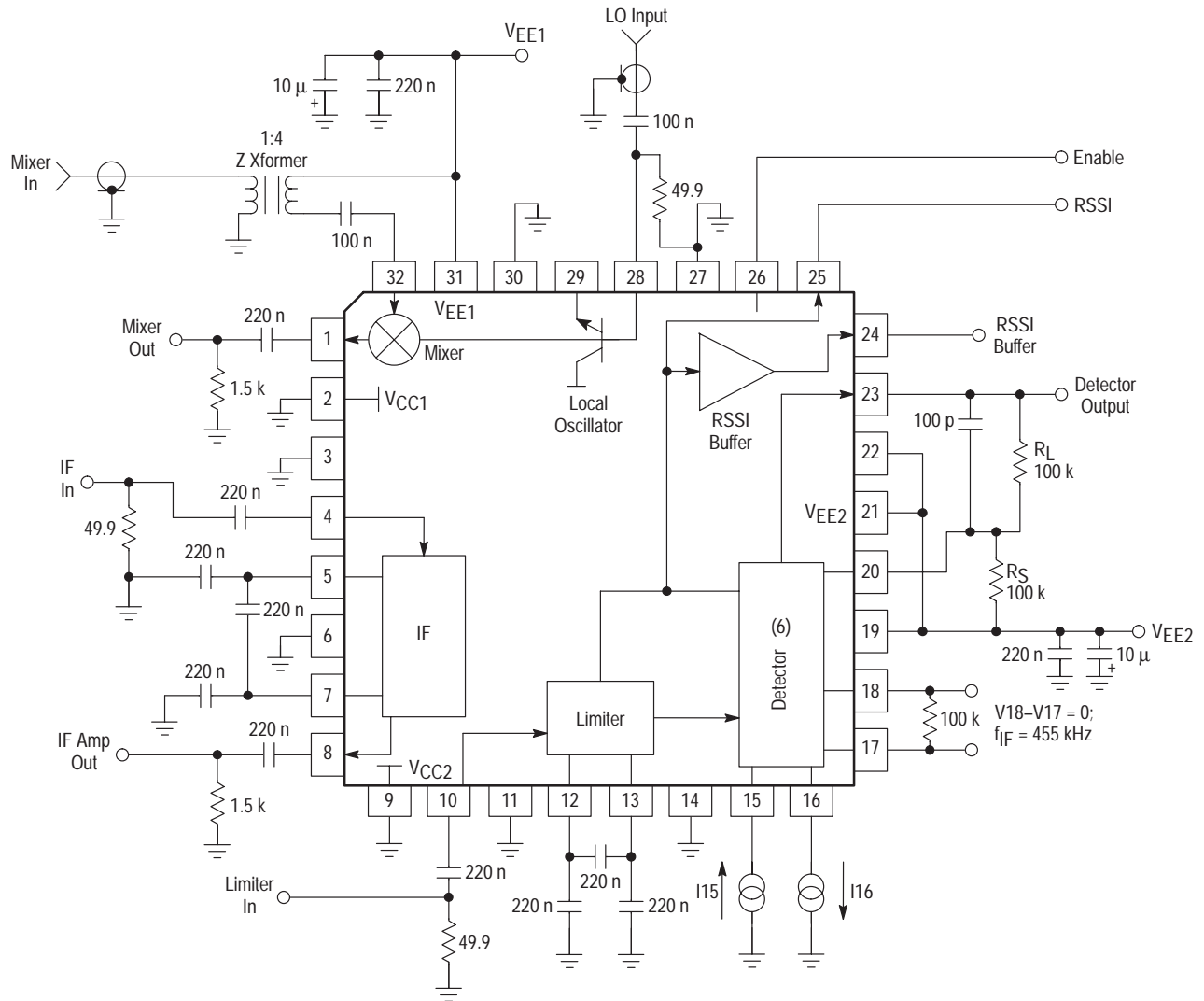
MC13150

AC ELECTRICAL CHARACTERISTICS (continued) ($T_A = 25^\circ\text{C}$, $V_S = 3.0\text{ Vdc}$, $f_{RF} = 50\text{ MHz}$, $f_{LO} = 50.455\text{ MHz}$, LO Level = -10 dBm , see Figure 1 Test Circuit*, unless otherwise specified.)

Characteristics	Condition	Pin	Symbol	Min	Typ	Max	Unit
DETECTOR							
Frequency Adjust Current	Figure 9, $f_{IF} = 455\text{ kHz}$	16	–	41	49	56	μA
Frequency Adjust Voltage	Figure 10, $f_{IF} = 455\text{ kHz}$	16	–	600	650	700	mVdc
Bandwidth Adjust Voltage	Figure 12, $I_{15} = 1.0\ \mu\text{A}$	15	–	–	570	–	mVdc
Detector DC Output Voltage (See Figure 25)	–	23	–	–	1.36	–	Vdc
Recovered Audio Voltage	$f_{dev} = \pm 3.0\text{ kHz}$	23	–	85	122	175	mVrms

* Figure 1 Test Circuit uses positive (V_{CC}) Ground.

Figure 1. Test Circuit



This device contains 292 active transistors.

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MC13150

MC13150 CIRCUIT DESCRIPTION

General

The MC13150 is a very low power single conversion narrowband FM receiver incorporating a split IF. This device is designated for use as the backend in analog narrowband FM systems such as cellular, 900 MHz cordless phones and narrowband data links with data rates up to 9.6 k baud. It contains a mixer, oscillator, extended range received signal strength indicator (RSSI), RSSI buffer, IF amplifier, limiting IF, a unique coilless quadrature detector and a device enable function (see Package Pin Outs/Block Diagram).

Low Current Operation

The MC13150 is designed for battery and portable applications. Supply current is typically 1.7 mA_{DC} at 3.0 V_{DC}. Figure 2 shows the supply current versus supply voltage.

Enable

The enable function is provided for battery powered operation. The enabled pin is pulled down to enable the regulators. Figure 3 shows the supply current versus enable voltage, V_{enable} (relative to V_{CC}) needed to enable the device. Note that the device is fully enabled at $V_{CC} - 1.3$ V_{DC}. Figure 4 shows the relationship of enable current, I_{enable} to enable voltage, V_{enable} .

Mixer

The mixer is a double-balanced four quadrant multiplier and is designed to work up to 500 MHz. It has a single ended input. Figure 5 shows the mixer gain and saturated output response as a function of input signal drive and for -10 dBm LO drive level. This is measured in the application circuit shown in Figure 15 in which a single LC matching network is used. Since the single-ended input impedance of the mixer is 200 Ω , an alternate solution uses a 1:4 impedance transformer to match the mixer to 50 Ω input impedance. The linear voltage gain of the mixer alone is approximately 4.0 dB (plus an additional 6.0 dB for the transformer). Figure 6 shows the mixer gain versus the LO input level for various mixer input levels at 50 MHz RF input.

The buffered output of the mixer is internally loaded, resulting in an output impedance of 1.5 k Ω .

Local Oscillator

The on-chip transistor operates with crystal and LC resonant elements up to 220 MHz. Series resonant, overtone crystals are used to achieve excellent local oscillator stability. 3rd overtone crystals are used through about 65 to 70 MHz. Operation from 70 MHz up to 200 MHz is feasible using the on-chip transistor with a 5th or 7th overtone crystal. To enhance operation using an overtone crystal, the internal transistor's bias is increased by adding an external resistor from Pin 29 (in 32 pin QFP package) to V_{EE} to keep the oscillator on continuously or it may be taken to the enable pin to shut it off when the receiver is disabled. -10 dBm of local oscillator drive is needed to adequately drive the mixer (Figure 6). The oscillator configurations specified above are described in the application section.

RSSI

The received signal strength indicator (RSSI) output is a current proportional to the log of the received signal amplitude. The RSSI current output is derived by summing the currents from the IF and limiting amplifier stages. An external resistor at Pin 25 (in 32 pin QFP package) sets the voltage range or swing of the RSSI output voltage. Linearity of the RSSI is optimized by using external ceramic bandpass filters which have an insertion loss of 4.0 dB. The RSSI circuit is designed to provide 100+ dB of dynamic range with temperature compensation (see Figures 7 and 23 which show the RSSI response of the applications circuit).

RSSI Buffer

The RSSI buffer has limitations in what loads it can drive. It can pull loads well towards the positive and negative supplies, but has problems pulling the load away from the supplies. The load should be biased at half supply to overcome this limitation.

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Figure 2. Supply Current versus Supply Voltage

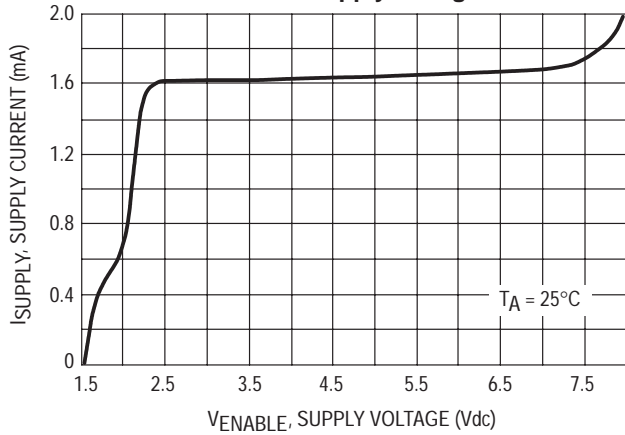


Figure 3. Supply Current versus Enable Voltage

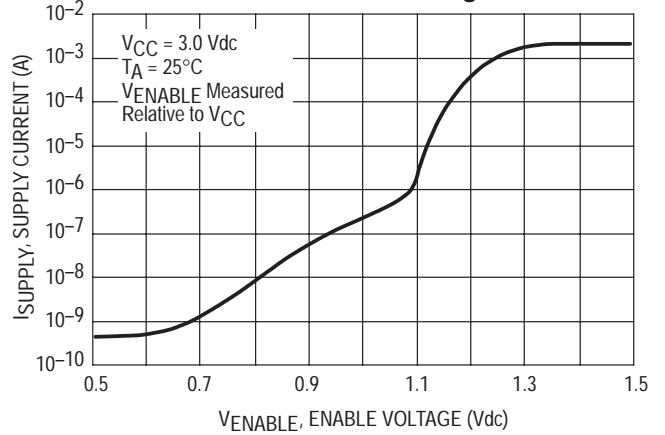


Figure 4. Enable Current versus Enable Voltage

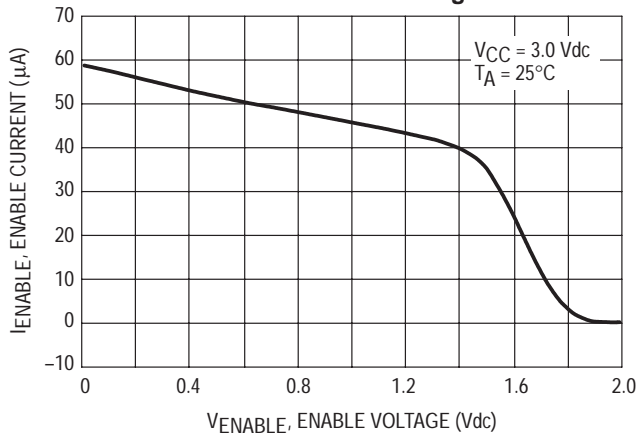


Figure 5. Mixer IF Output Level versus RF Input Level

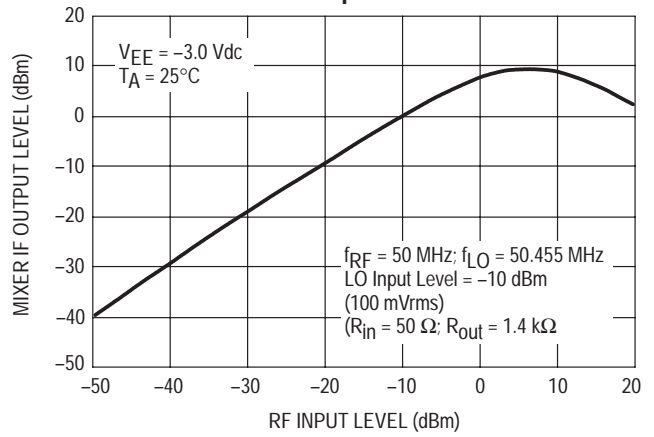


Figure 6. Mixer IF Output Level versus Local Oscillator Input Level

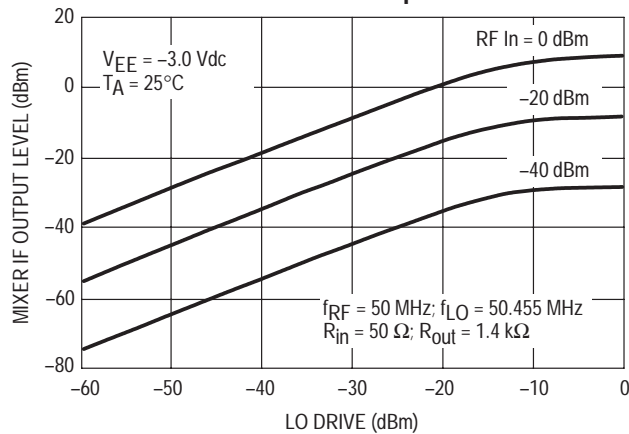
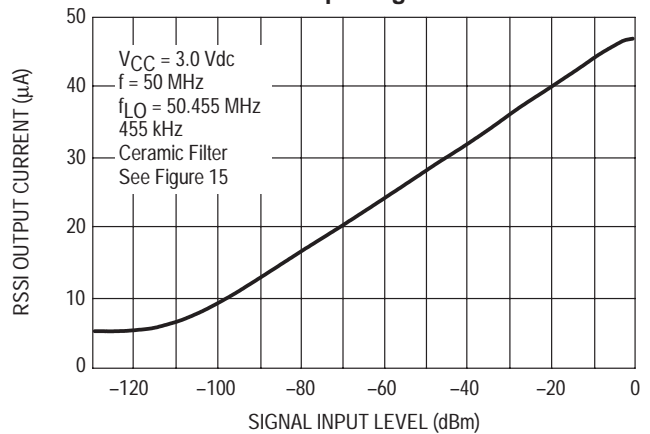


Figure 7. RSSI Output Current versus Input Signal Level



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IF Amplifier

The first IF amplifier section is composed of three differential stages. This section has internal dc feedback and external input decoupling for improved symmetry and stability. The total gain of the IF amplifier block is approximately 42 dB at 455 kHz. Figure 8 shows the gain of the IF amplifier as a function of the IF frequency.

The fixed internal input impedance is 1.5 kΩ; it is designed for applications where a 455 kHz ceramic filter is used and no external output matching is necessary since the filter requires a 1.5 kΩ source and load impedance.

Overall RSSI linearity is dependent on having total midband attenuation of 10 dB (4.0 dB insertion loss plus 6.0 dB impedance matching loss) for the filter. The output of the IF amplifier is buffered and the impedance is 1.5 kΩ.

Limiter

The limiter section is similar to the IF amplifier section except that six stages are used. The fixed internal input impedance is 1.5 kΩ. The total gain of the limiting amplifier section is approximately 96 dB. This IF limiting amplifier section internally drives the quadrature detector section.

Figure 8. IF Amplifier Gain versus IF Frequency

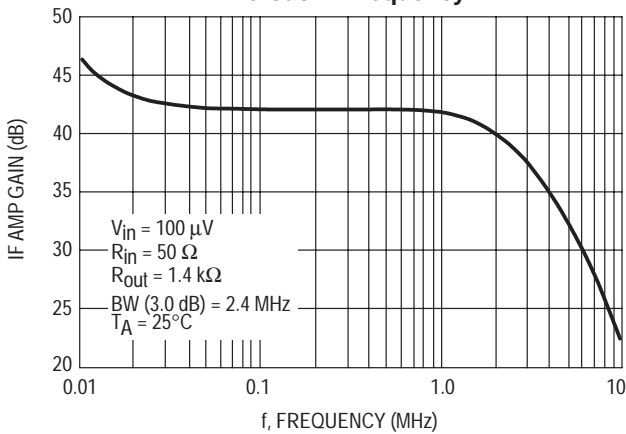


Figure 9. F_{adj} Current versus IF Frequency

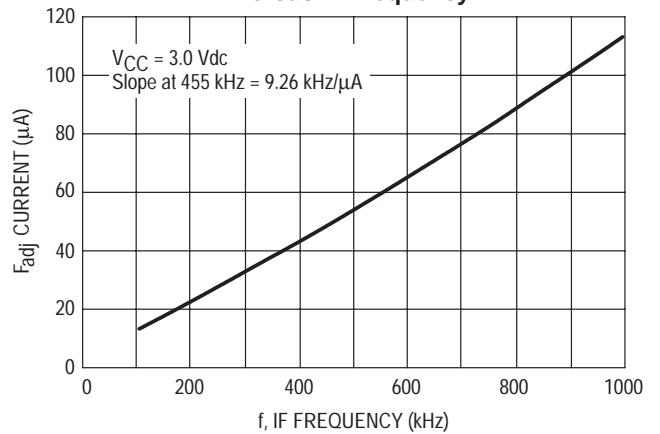


Figure 10. F_{adj} Voltage versus F_{adj} Current

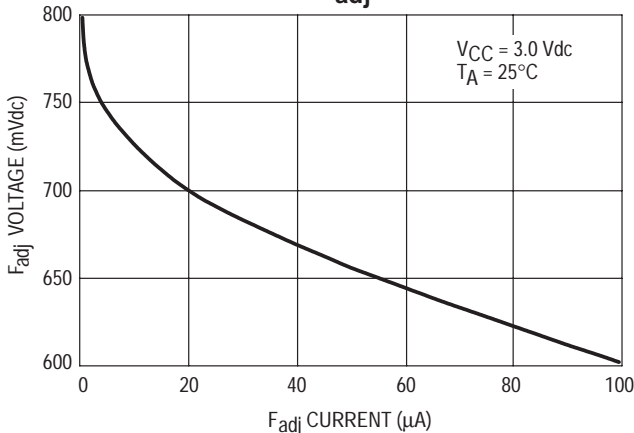
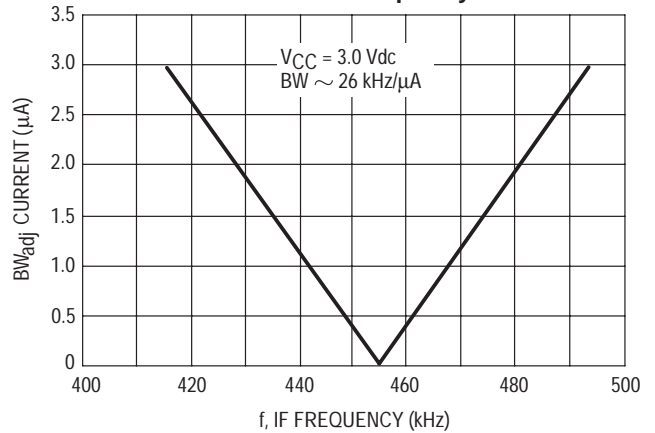


Figure 11. BW_{adj} Current versus IF Frequency



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NOT RECOMMENDED FOR NEW DESIGNS

Coilless Detector

The quadrature detector is similar to a PLL. There is an internal oscillator running at the IF frequency and two detector outputs. One is used to deliver the audio signal and the other one is filtered and used to tune the oscillator.

The oscillator frequency is set by an external resistor at the F_{adj} pin. Figure 9 shows the control current required for a particular frequency; Figure 10 shows the pin voltage at that current. From this the value of R_F is chosen. For example, 455 kHz would require a current of around 50 μA . The pin voltage (Pin 16 in the 32 pin QFP package) is around 655mV giving a resistor of 13.1 k Ω . Choosing 12 k Ω as the nearest standard value gives a current of approximately 55 μA . The 5.0 μA difference can be taken up by the tuning resistor, R_T .

The best nominal frequency for the AFT_{out} pin (Pin 17) would be half supply. A supply voltage of 3.0 Vdc suggests a resistor value of $(1.5 - 0.655)V/5.0 \mu A = 169 k\Omega$. Choosing 150 k Ω would give a tuning current of $3/150 k = 20 \mu A$. From Figure 9 this would give a tuning range of roughly 10 kHz/ μA or ± 100 kHz which should be adequate.

The bandwidth can be adjusted with the help of Figure 11. For example, 1.0 μA would give a bandwidth of ± 13 kHz. The

voltage across the bandwidth resistor, R_B from Figure 12 is $V_{CC} - 2.44 Vdc = 0.56 Vdc$ for $V_{CC} = 3.0 Vdc$, so $R_B = 0.56V/1.0 \mu A = 560 k\Omega$. Actually the locking range will be ± 13 kHz while the audio bandwidth will be approximately ± 8.4 kHz due to an internal filter capacitor. This is verified in Figure 13. For some applications it may be desirable that the audio bandwidth is increased; this is done by reducing R_B . Reducing R_B widens the detector bandwidth and improves the distortion at high input levels at the expense of 12 dB SINAD sensitivity. The low frequency 3.0dB point is set by the tuning circuit such that the product

$$R_T C_T = 0.68/f_{3dB}$$

So, for example, 150 k and 1.0 μF give a 3.0 dB point of 4.5 Hz. The recovered audio is set by R_L to give roughly 50mV per kHz deviation per 100 k of resistance. The dc level can be shifted by R_S from the nominal 0.68 V by the following equation:

$$\text{Detector DC Output} = ((R_L + R_S)/R_S) 0.68 Vdc$$

Thus, $R_S = R_L$ sets the output at $2 \times 0.68 = 1.36 V$; $R_L = 2R_S$ sets the output at $3 \times 0.68 = 2.0 V$.

Figure 12. BW_{adj} Current versus BW_{adj} Voltage

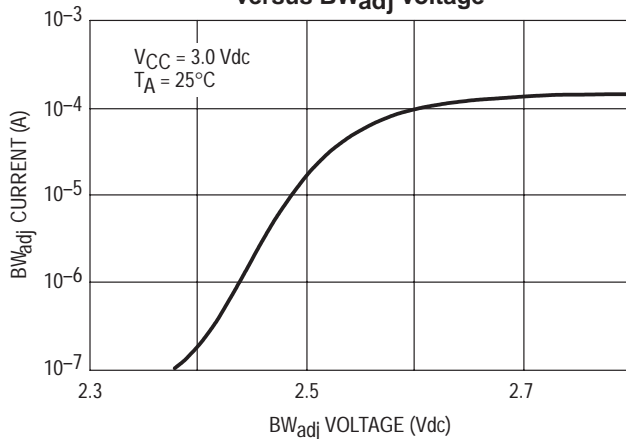
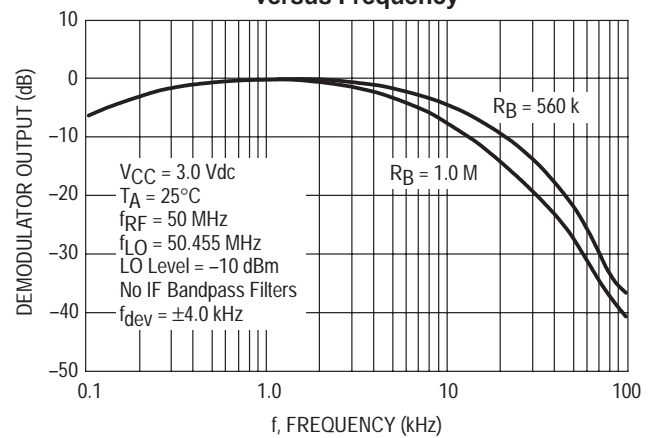


Figure 13. Demodulator Output versus Frequency



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MC13150

APPLICATIONS INFORMATION

Evaluation PC Board

The evaluation PCB is very versatile and is intended to be used across the entire useful frequency range of this device. The center section of the board provides an area for attaching all SMT components to the circuit side and radial leaded components to the component ground side (see Figures 29 and 30). Additionally, the peripheral area surrounding the RF core provides pads to add supporting and interface circuitry as a particular application dictates. There is an area dedicated for a LNA preamp. This evaluation board will be discussed and referenced in this section.

Component Selection

The evaluation PC board is designed to accommodate specific components, while also being versatile enough to use components from various manufacturers and coil types. The applications circuit schematic (Figure 15) specifies particular components that were used to achieve the results shown in the typical curves but equivalent components should give similar results. Component placement views are

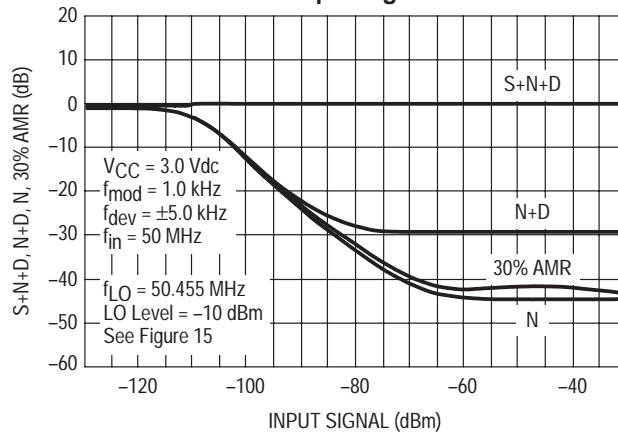
shown in Figures 27 and 28 for the application circuit in Figure 15 and for the 83.616 MHz crystal oscillator circuit in Figure 16.

Input Matching Components

The input matching circuit shown in the application circuit schematic (Figure 15) is a series L, shunt C single L section which is used to match the mixer input to 50 Ω. An alternative input network may use 1:4 surface mount transformers or BALUNs. The 12 dB SINAD sensitivity using the 1:4 impedance transformer is typically -100 dBm for $f_{mod} = 1.0$ kHz and $f_{dev} = \pm 5.0$ kHz at $f_{in} = 50$ MHz and $f_{LO} = 50.455$ MHz (see Figure 14).

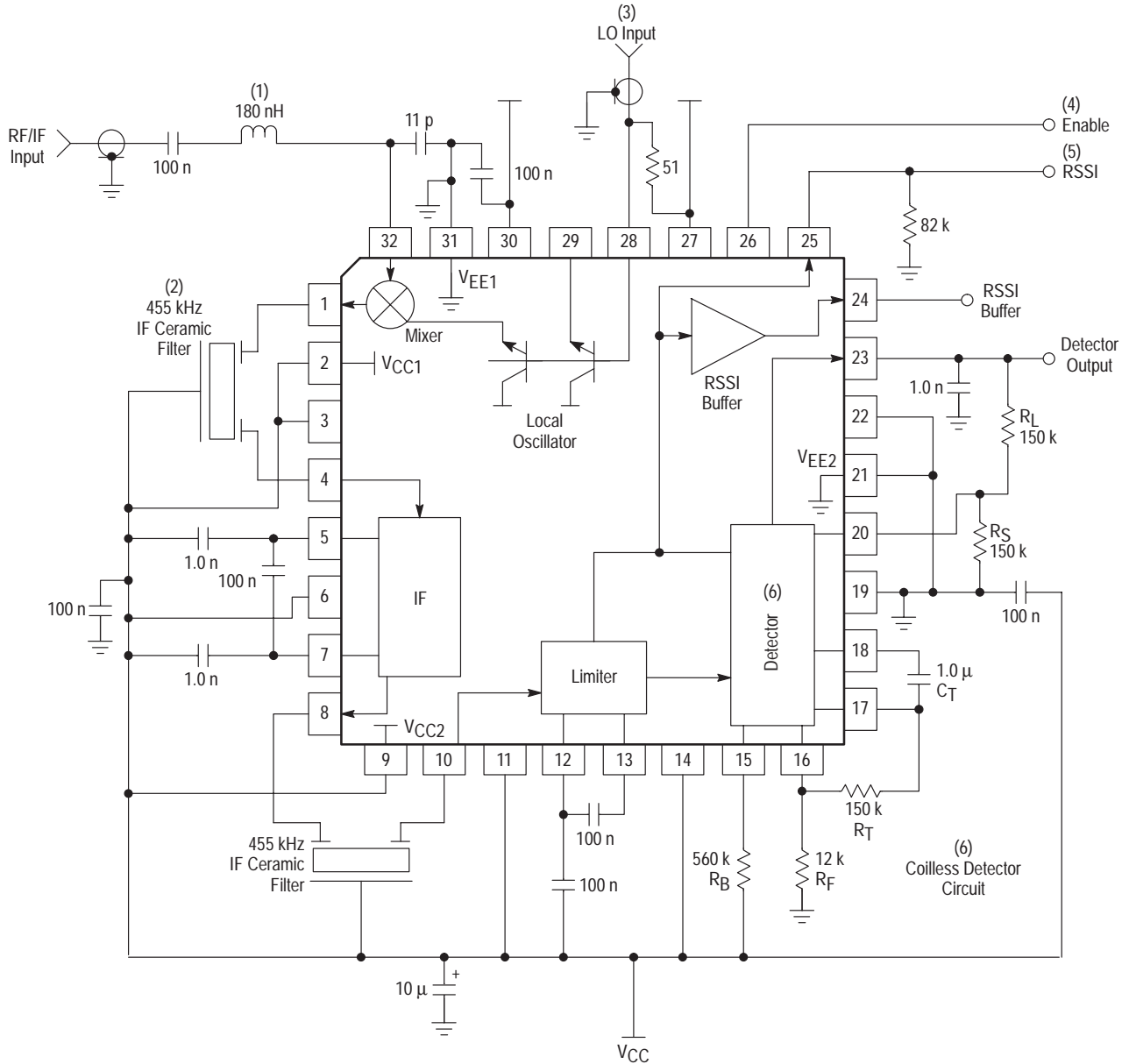
It is desirable to use a SAW filter before the mixer to provide additional selectivity and adjacent channel rejection and improved sensitivity. SAW filters sourced from Toko (Part # SWS083GBWA) and Murata (Part # SAF83.16MA51X) are excellent choices to easily interface with the MC13150 mixer. They are packaged in a 12 pin low profile surface mount ceramic package. The center frequency is 83.161 MHz and the 3.0 dB bandwidth is 30 kHz.

Figure 14. S+N+D, N+D, N, 30% AMR versus Input Signal Level



MC13150

Figure 15. Application Circuit



- NOTES:**
1. Alternate solution is 1:4 impedance transformer (sources include Mini Circuits, Coilcraft and Toko).
 2. 455 kHz ceramic filters (source Murata CFU455 series which are selected for various bandwidths).
 3. For external LO source, a 51 Ω pull-up resistor is used to bias the base of the on-board transistor as shown in Figure 15. Designer may provide local oscillator with 3rd, 5th, or 7th overtone crystal oscillator circuit. The PC board is laid out to accommodate external components needed for a Butler emitter coupled crystal oscillator (see Figure 16).
 4. Enable IC by switching the pin to V_{EE} .
 5. The resistor is chosen to set the range of RSSI voltage output swing.
 6. Details regarding the external components to setup the coilless detector are provided in the application section.

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Local Oscillators

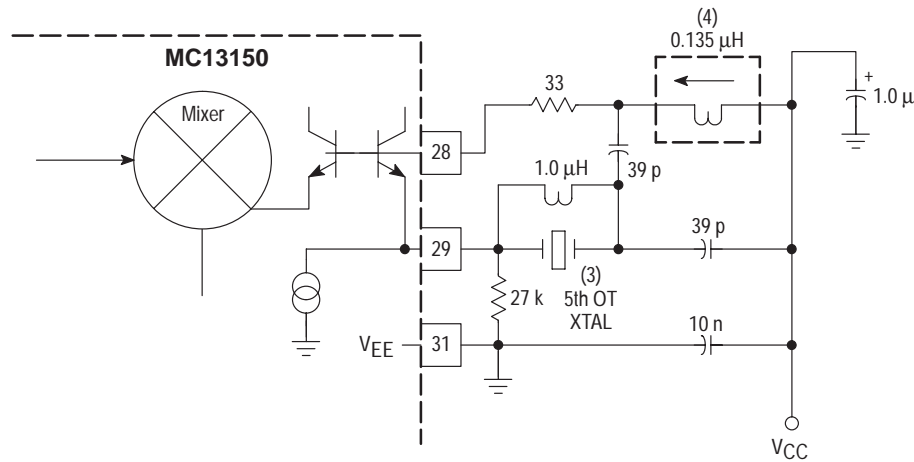
HF & VHF Applications

In the application schematic, an external sourced local oscillator is utilized in which the base is biased via a 51 Ω resistor to V_{CC}. However, the on-chip grounded collector transistor may be used for HF and VHF local oscillators with higher order overtone crystals. Figure 16 shows a 5th overtone oscillator at 83.616 MHz. The circuit uses a Butler overtone oscillator configuration. The amplifier is an emitter follower. The crystal is driven from the emitter and is coupled to the high impedance base through a capacitive tap network. Operation at the desired overtone frequency is ensured by the parallel resonant circuit formed by the variable inductor and the tap capacitors and parasitic capacitances of the on-chip transistor and PC board. The variable inductor specified in the schematic could be replaced with a high tolerance, high Q ceramic or air wound surface mount component if the other components have tight enough tolerances. A variable inductor provides an adjustment for gain and frequency of the resonant tank ensuring lock up and start-up of the crystal oscillator. The overtone crystal is chosen with ESR of typically 80 Ω and 120 Ω maximum; if the resistive loss in the crystal is too high the performance of oscillator may be impacted by lower gain margins.

A series LC network to ac ground (which is V_{CC}) is comprised of the inductance of the base lead of the on-chip transistor and PC board traces and tap capacitors. Parasitic oscillations often occur in the 200 to 800 MHz range. A small resistor is placed in series with the base (Pin 28) to cancel the negative resistance associated with this undesired mode of oscillation. Since the base input impedance is so large, a small resistor in the range of 27 to 68 Ω has very little effect on the desired Butler mode of oscillation.

The crystal parallel capacitance, C_O, provides a feedback path that is low enough in reactance at frequencies of 5th overtones or higher to cause trouble. C_O has little effect near resonance because of the low impedance of the crystal motional arm (R_m-L_m-C_m). As the tunable inductor, which forms the resonant tank with the tap capacitors, is tuned off the crystal resonant frequency, it may be difficult to tell if the oscillation is under crystal control. Frequency jumps may occur as the inductor is tuned. In order to eliminate this behavior an inductor, L_O, is placed in parallel with the crystal. L_O is chosen to resonant with the crystal parallel capacitance, C_O, at the desired operation frequency. The inductor provides a feedback path at frequencies well below resonance; however, the parallel tank network of the tap capacitors and tunable inductor prevent oscillation at these frequencies.

Figure 16. MC13150FTB Overtone Oscillator
 $f_{RF} = 83.16 \text{ MHz}$; $f_{LO} = 83.616 \text{ MHz}$
 5th Overtone Crystal Oscillator



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MC13150

Receiver Design Considerations

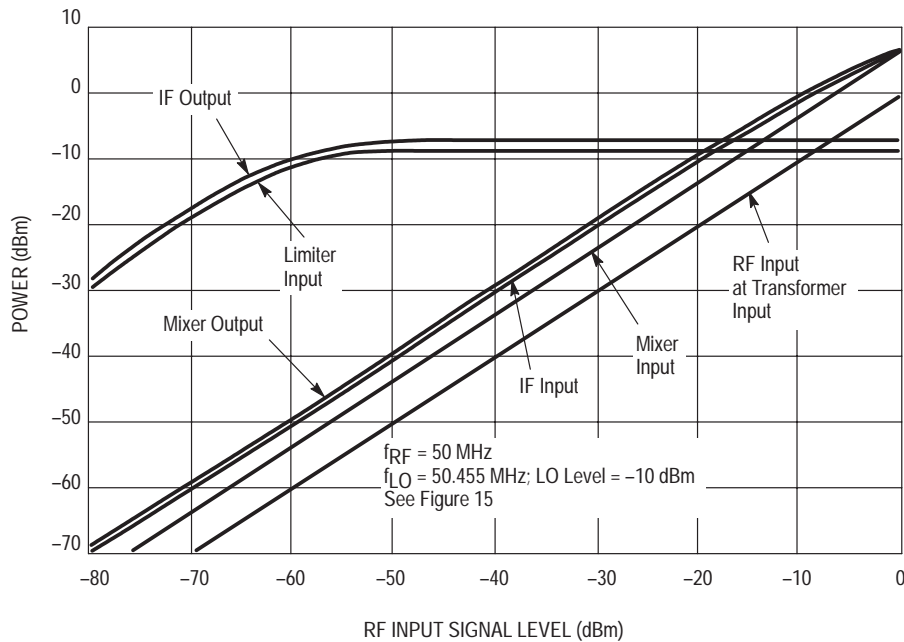
The curves of signal levels at various portions of the application receiver with respect to RF input level are shown in Figure 17. This information helps determine the network topology and gain blocks required ahead of the MC13150 to achieve the desired sensitivity and dynamic range of the receiver system. The PCB is laid out to accommodate a low noise preamp followed by the 83.16 MHz SAW filter. In the

application circuit (Figure 15), the input 1.0 dB compression point is -10 dBm and the input third order intercept (IP3) performance of the system is approximately 0 dBm (see Figure 18).

Typical Performance Over Temperature

Figures 19–26 show the device performance over temperature.

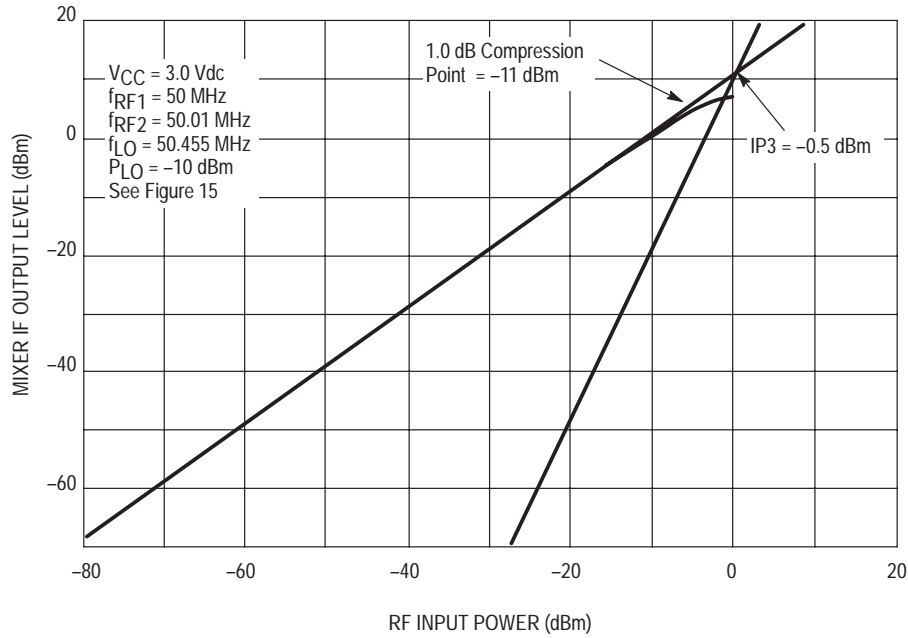
Figure 17. Signal Levels versus RF Input Signal Level



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Figure 18. 1.0 dB Compression Point and Input Third Order Intercept Point versus Input Power



TYPICAL PERFORMANCE OVER TEMPERATURE

Figure 19. Supply Current, I_{VEE1} versus Signal Input Level

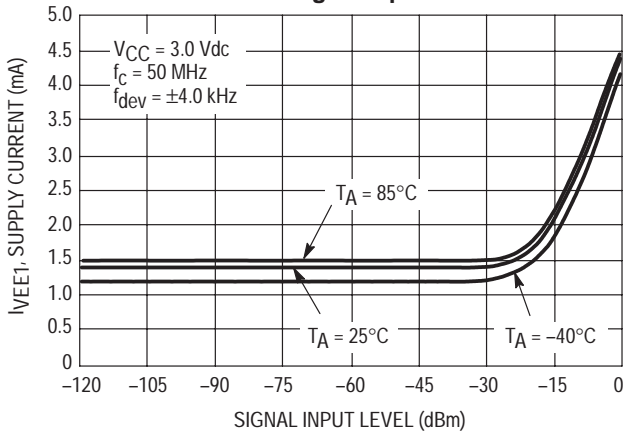
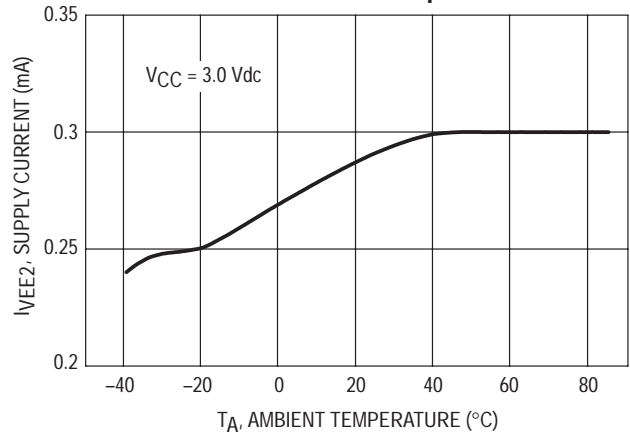


Figure 20. Supply Current, I_{VEE2} versus Ambient Temperature



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MC13150

TYPICAL PERFORMANCE OVER TEMPERATURE

Figure 21. Total Supply Current versus Ambient Temperature

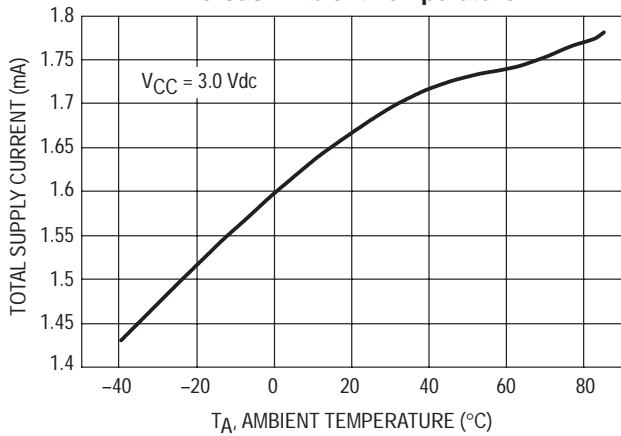


Figure 22. Minimum Supply Voltage versus Ambient Temperature

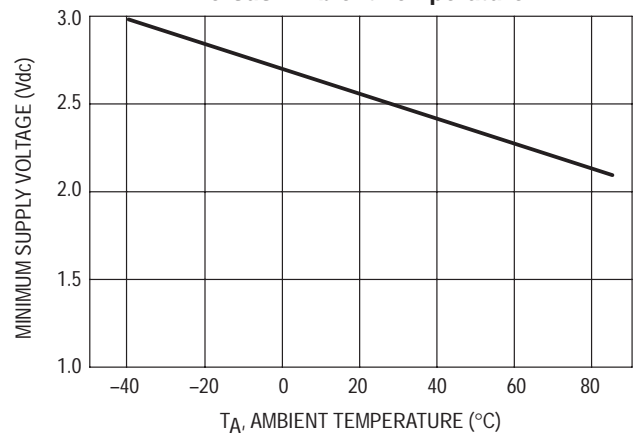


Figure 23. RSSI Current versus Ambient Temperature and Signal Level

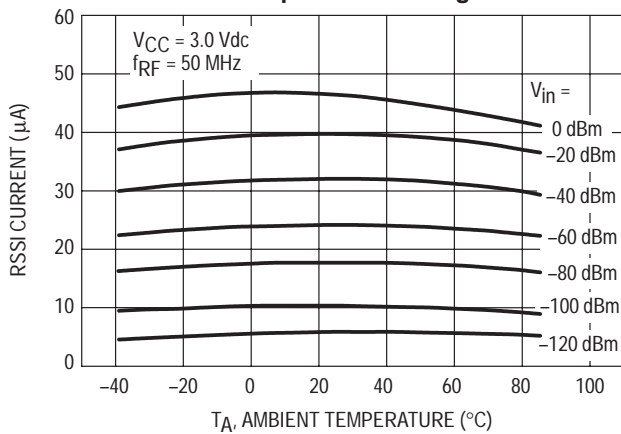


Figure 24. Recovered Audio versus Ambient Temperature

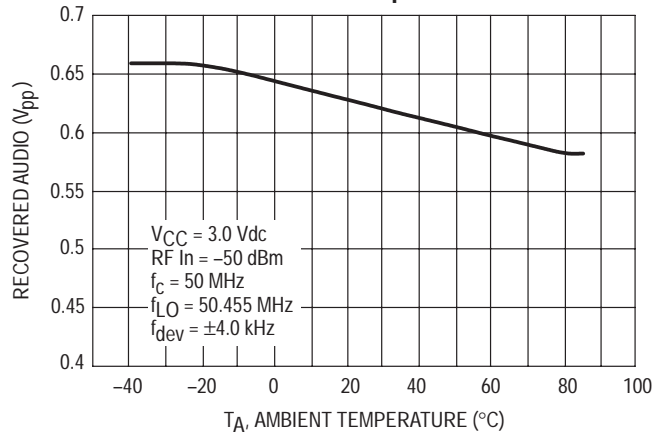


Figure 25. Demod DC Output Voltage versus Ambient Temperature

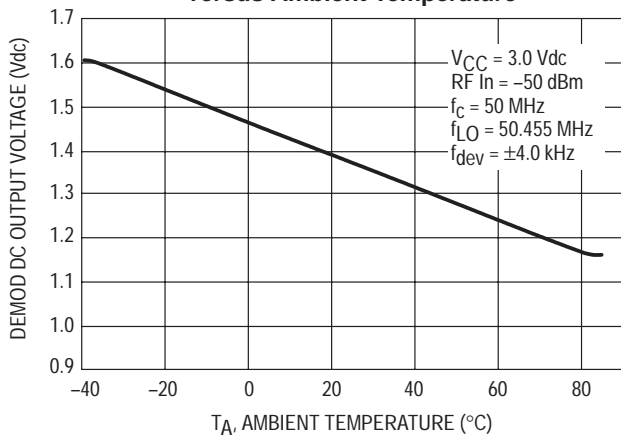
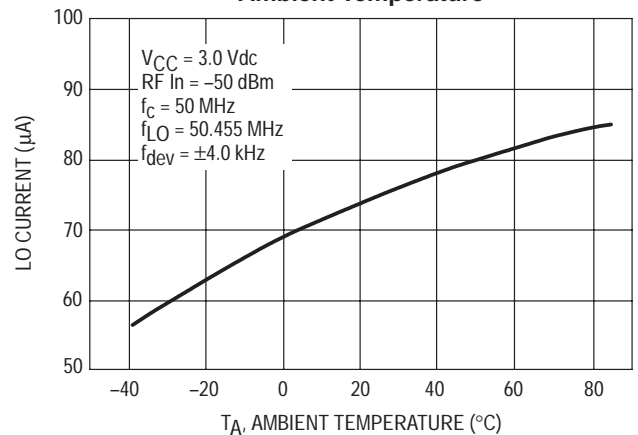


Figure 26. LO Current versus Ambient Temperature



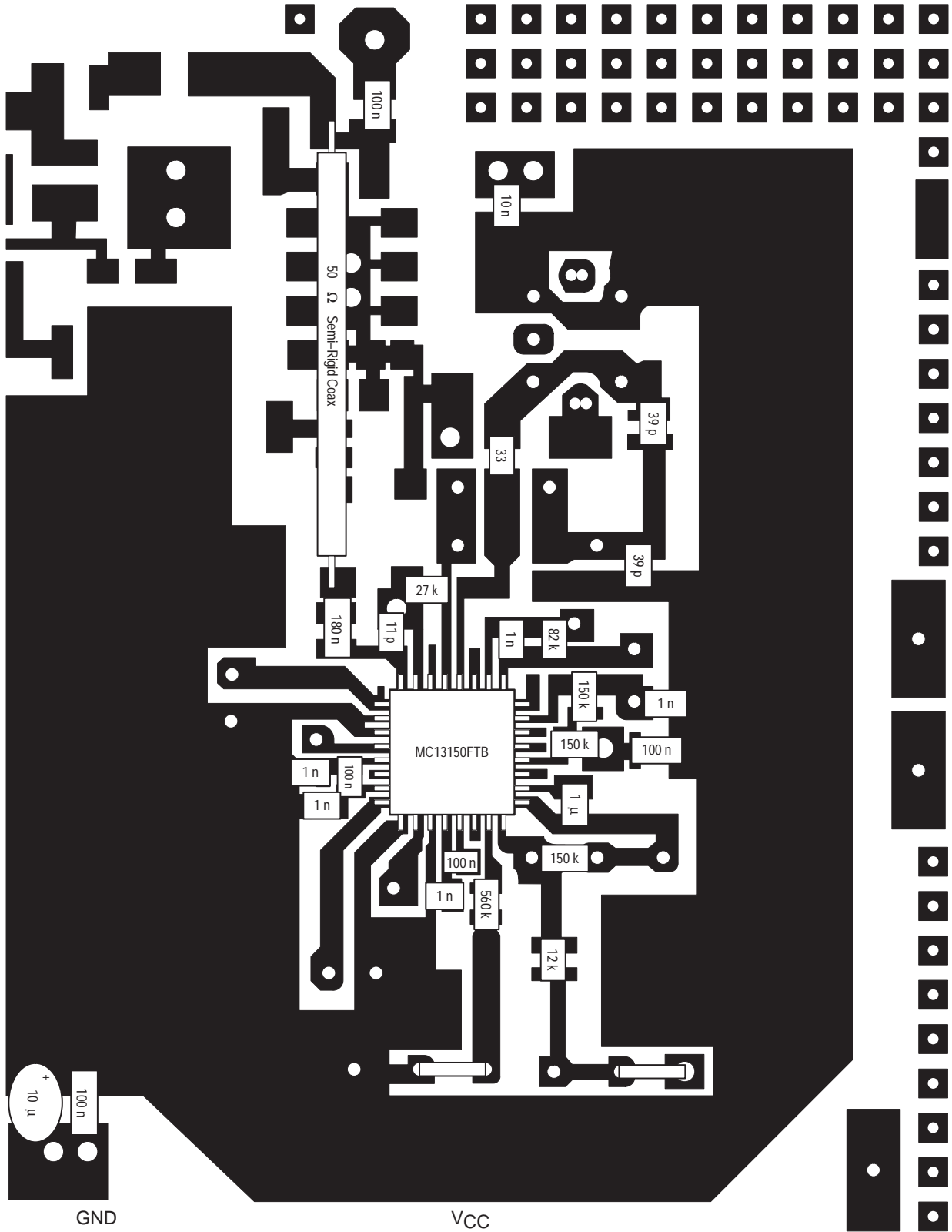
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MC13150

Figure 27. Component Placement View – Circuit Side

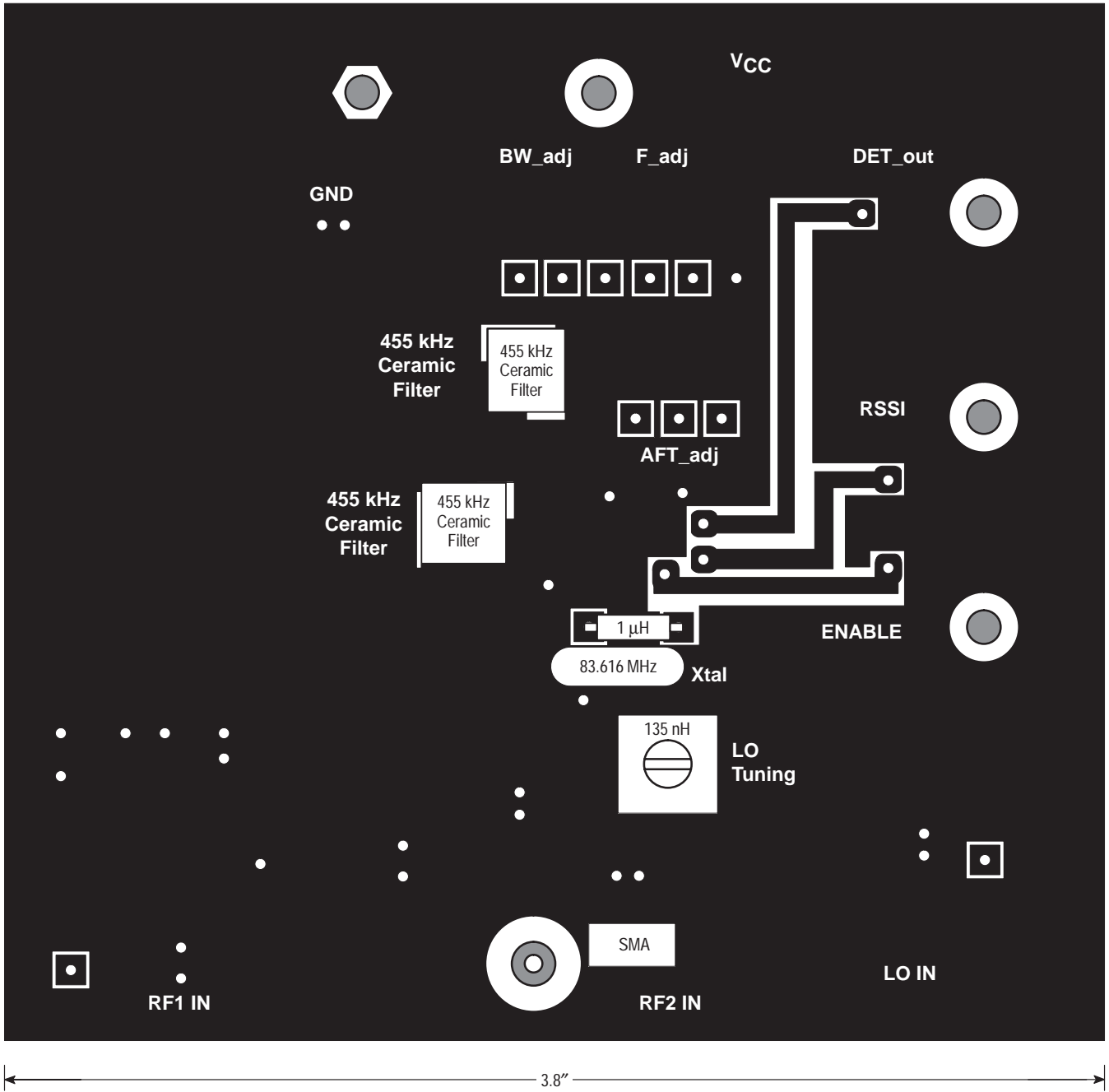
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MC13150

Figure 28. Component Placement View – Ground Side

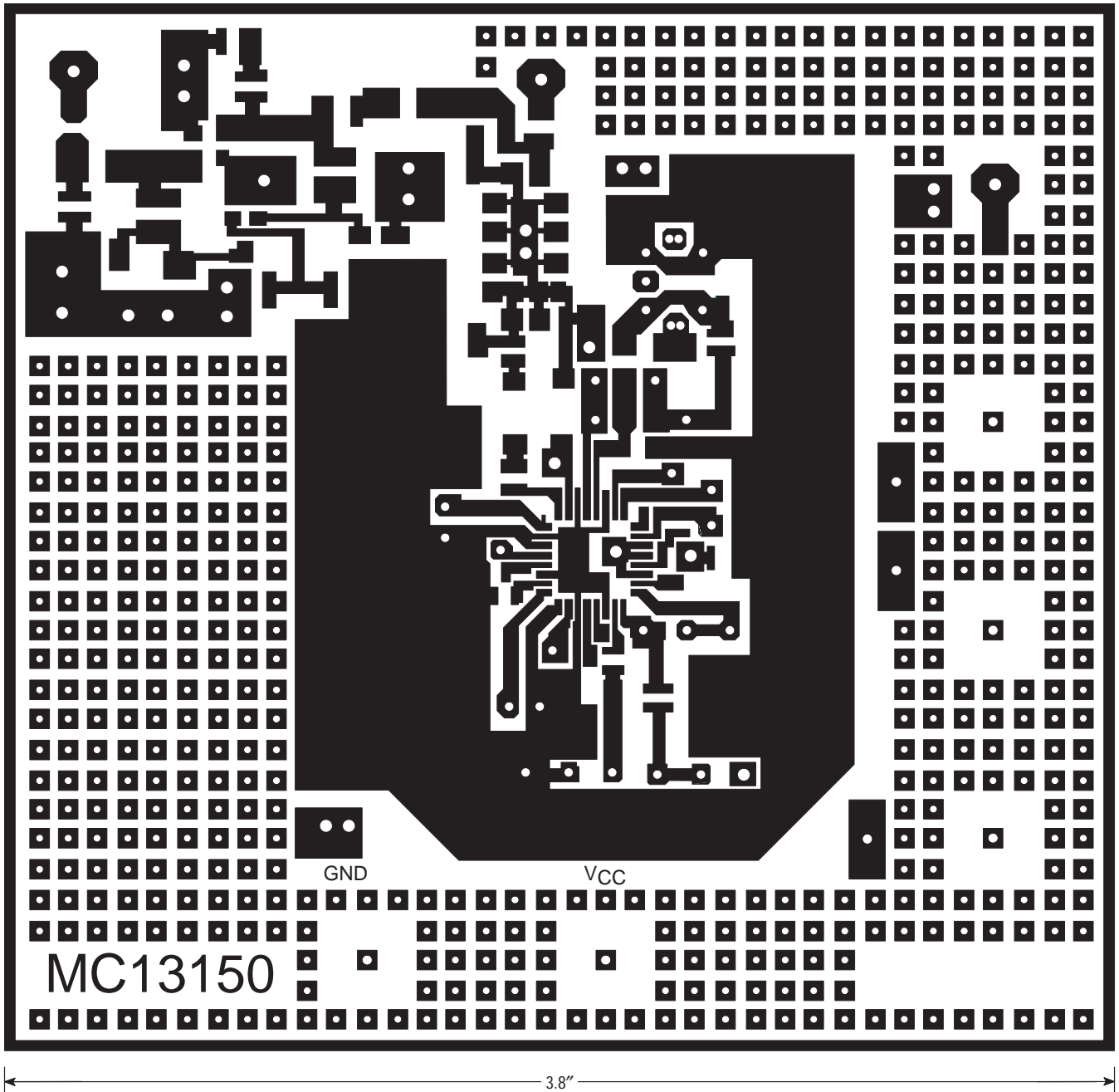


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MC13150

Figure 29. PCB Circuit Side View

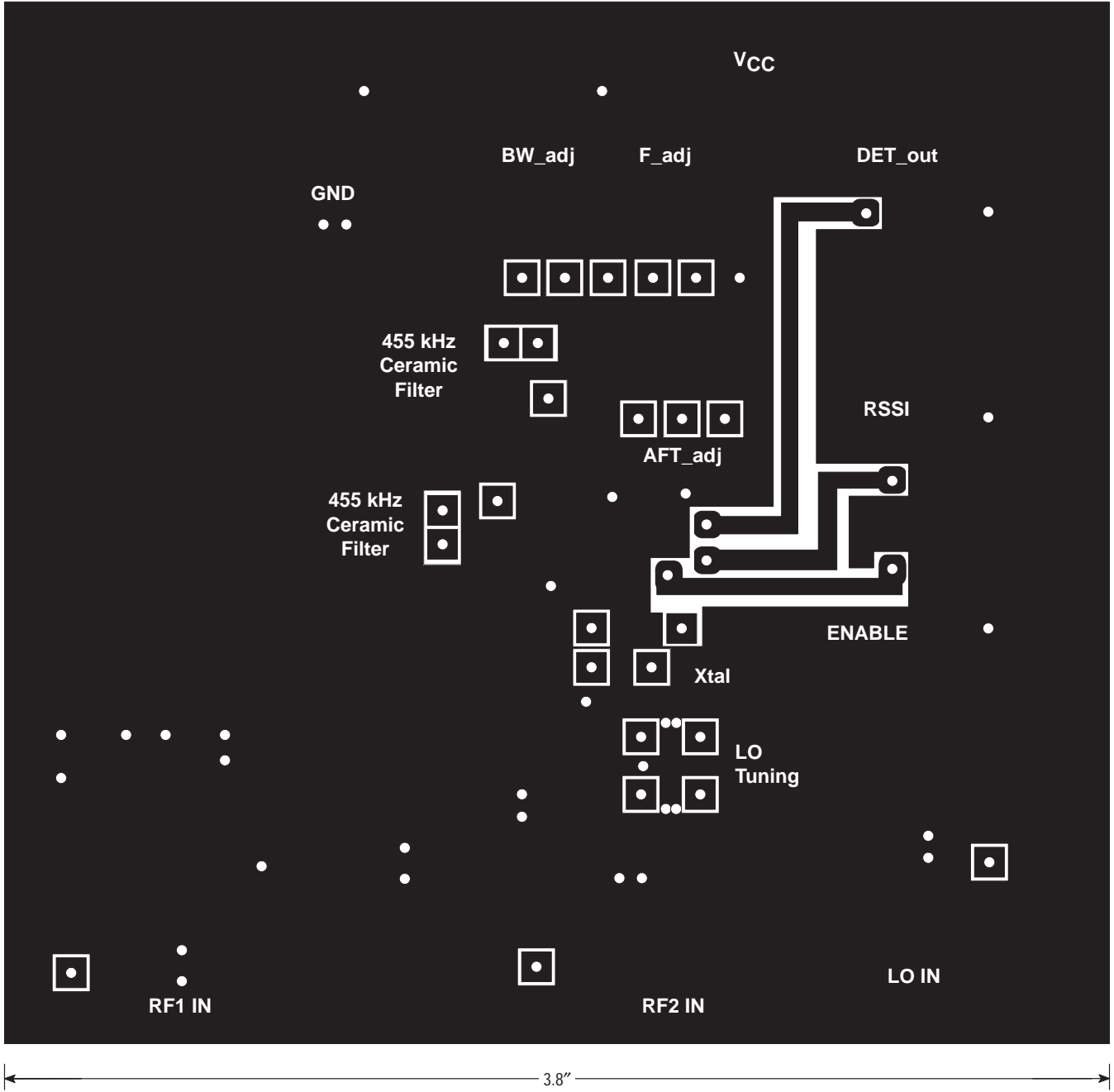


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MC13150

Figure 30. PCB Ground Side View



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Wideband FM IF

The MC13155 is a complete wideband FM detector designed for satellite TV and other wideband data and analog FM applications. This device may be cascaded for higher IF gain and extended Receive Signal Strength Indicator (RSSI) range.

- 12 MHz Video/Baseband Demodulator
- Ideal for Wideband Data and Analog FM Systems
- Limiter Output for Cascade Operation
- Low Drain Current: 7.0 mA
- Low Supply Voltage: 3.0 to 6.0 V
- Operates to 300 MHz

MAXIMUM RATINGS

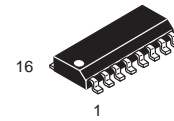
Rating	Pin	Symbol	Value	Unit
Power Supply Voltage	11, 14	V_{EE} (max)	6.5	Vdc
Input Voltage	1, 16	V_{in}	1.0	Vrms
Junction Temperature	—	T_J	+150	°C
Storage Temperature Range	—	T_{stg}	-65 to +150	°C

NOTE: Devices should not be operated at or outside these values. The "Recommended Operating Conditions" provide for actual device operation.

MC13155

WIDEBAND FM IF

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751B
(SO-16)

PIN CONNECTIONS

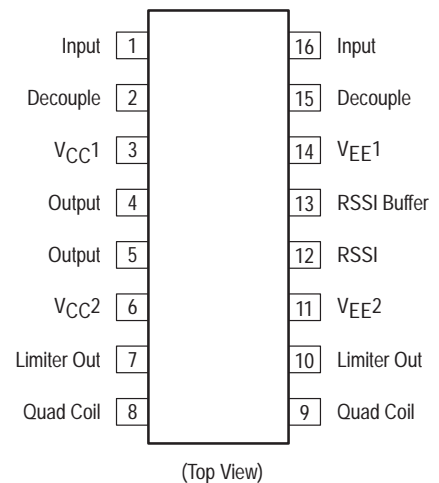
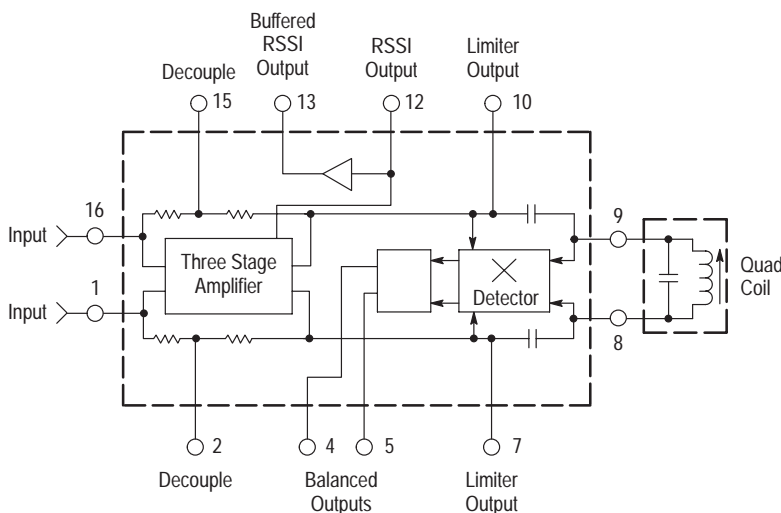


Figure 1. Representative Block Diagram



NOTE: This device requires careful layout and decoupling to ensure stable operation.

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13155D	$T_A = -40$ to $+85^\circ\text{C}$	SO-16

MC13155

RECOMMENDED OPERATING CONDITIONS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage ($T_A = 25^\circ\text{C}$) – $40^\circ\text{C} \leq T_A \leq 85^\circ\text{C}$	11, 14 3, 6	V_{EE} V_{CC}	– 3.0 to – 6.0 Grounded	Vdc
Maximum Input Frequency	1, 16	f_{in}	300	MHz
Ambient Temperature Range	–	T_J	– 40 to + 85	$^\circ\text{C}$

DC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, no input signal.)

Characteristic	Pin	Symbol	Min	Typ	Max	Unit
Drain Current ($V_{EE} = -5.0\text{ Vdc}$)	11	I_{11}	2.0	2.8	4.0	mA
($V_{EE} = -5.0\text{ Vdc}$)	14	I_{14}	3.0	4.3	6.0	
($V_{EE} = -5.0\text{ Vdc}$)	14	I_{14}	3.0	4.3	6.0	
Drain Current Total (see Figure 3) ($V_{EE} = -5.0\text{ Vdc}$)	11, 14	I_{Total}	5.0	7.1	10	mA
($V_{EE} = -6.0\text{ Vdc}$)			5.0	7.5	10.5	
($V_{EE} = -6.0\text{ Vdc}$)			5.0	7.5	10.5	
($V_{EE} = -3.0\text{ Vdc}$)			4.7	6.6	9.5	

AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, $f_{IF} = 70\text{ MHz}$, $V_{EE} = -5.0\text{ Vdc}$ Figure 2, unless otherwise noted.)

Characteristic	Pin	Min	Typ	Max	Unit
Input for – 3 dB Limiting Sensitivity	1, 16	–	1.0	2.0	mVrms
Differential Detector Output Voltage ($V_{in} = 10\text{ mVrms}$) ($f_{dev} = \pm 3.0\text{ MHz}$) ($V_{EE} = -6.0\text{ Vdc}$)	4, 5	470	590	700	mV _{p-p}
($V_{EE} = -5.0\text{ Vdc}$)		450	570	680	
($V_{EE} = -3.0\text{ Vdc}$)		380	500	620	
Detector DC Offset Voltage	4, 5	– 250	–	250	mVdc
RSSI Slope	13	1.4	2.1	2.8	$\mu\text{A/dB}$
RSSI Dynamic Range	13	31	35	39	dB
RSSI Output ($V_{in} = 100\ \mu\text{Vrms}$)	12	–	2.1	–	μA
($V_{in} = 1.0\text{ mVrms}$)		–	2.4	–	
($V_{in} = 10\text{ mVrms}$)		16	24	36	
($V_{in} = 100\text{ mVrms}$)		–	65	–	
($V_{in} = 500\text{ mVrms}$)		–	75	–	
RSSI Buffer Maximum Output Current ($V_{in} = 10\text{ mVrms}$)	13	–	2.3	–	mAdc
Differential Limiter Output ($V_{in} = 1.0\text{ mVrms}$)	7, 10	100	140	–	mVrms
($V_{in} = 10\text{ mVrms}$)		–	180	–	
Demodulator Video 3.0 dB Bandwidth	4, 5	–	12	–	MHz
Input Impedance (Figure 14) @ 70 MHz R_p ($V_{EE} = -5.0\text{ Vdc}$)	1, 16	–	450	–	Ω
C_p ($C_2=C_{15} = 100\text{ p}$)		–	4.8	–	pF
Differential IF Power Gain	1, 7, 10, 16	–	46	–	dB

NOTE: Positive currents are out of the pins of the device.

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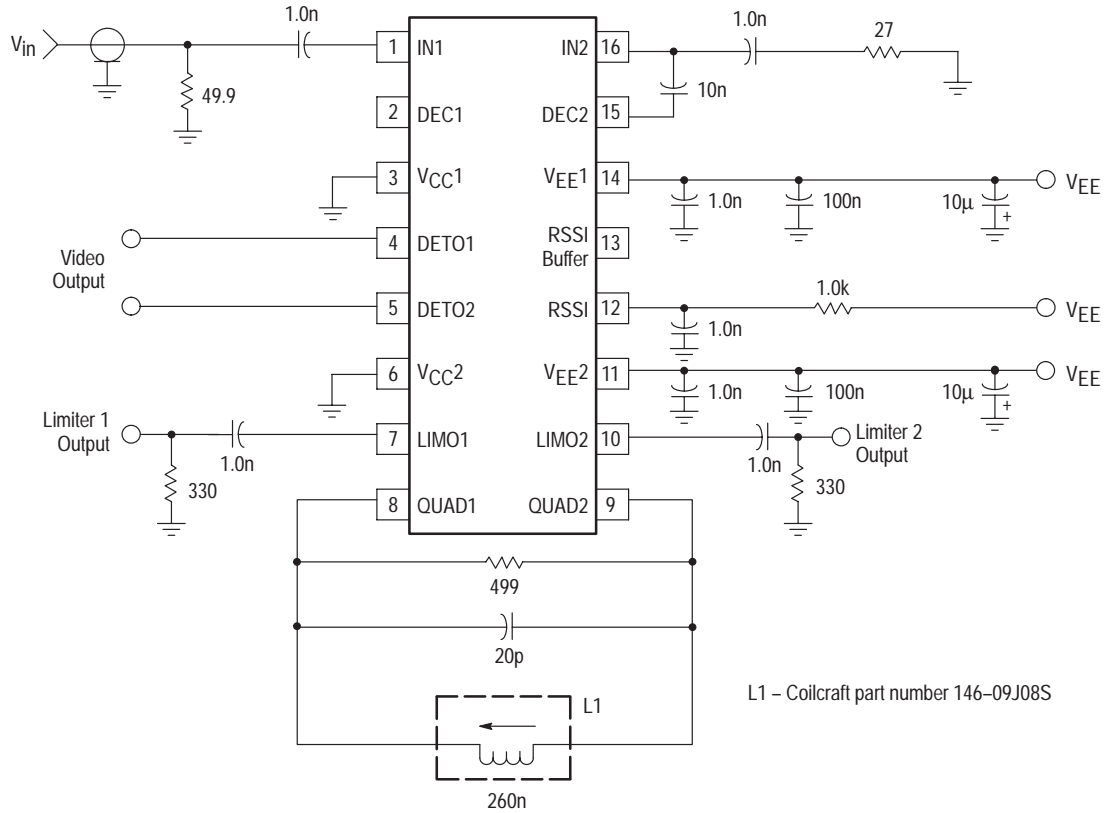
MC13155

CIRCUIT DESCRIPTION

The MC13155 consists of a wideband three-stage limiting amplifier, a wideband quadrature detector which may be operated up to 200 MHz, and a received signal strength

indicator (RSSI) circuit which provides a current output linearly proportional to the IF input signal level for approximately 35 dB range of input level.

Figure 2. Test Circuit



APPLICATIONS INFORMATION

Evaluation PC Board

The evaluation PCB shown in Figures 19 and 20 is very versatile and is designed to cascade two ICs. The center section of the board provides an area for attaching all surface mount components to the circuit side and radial leaded components to the component ground side of the PCB (see Figures 17 and 18). Additionally, the peripheral area surrounding the RF core provides pads to add supporting and interface circuitry as a particular application dictates. This evaluation board will be discussed and referenced in this section.

Limiting Amplifier

Differential input and output ports interfacing the three stage limiting amplifier provide a differential power gain of typically 46 dB and useable frequency range of 300 MHz. The IF gain flatness may be controlled by decoupling of the internal feedback network at Pins 2 and 15.

Scattering parameter (S-parameter) characterization of the IF as a two port linear amplifier is useful to implement maximum stable power gain, input matching, and stability over a desired bandpass response and to ensure stable operation outside the bandpass as well. The MC13155 is unconditionally stable over most of its useful operating frequency range; however, it can be made unconditionally stable over its entire operating range with the proper decoupling of Pins 2 and 15. Relatively small decoupling capacitors of about 100 pF have a significant effect on the wideband response and stability. This is shown in the scattering parameter tables where S-parameters are shown for various values of C2 and C15 and at VEE of -3.0 and -5.0 Vdc.

TYPICAL PERFORMANCE AT TEMPERATURE
(See Figure 2. Test Circuit)

Figure 3. Drain Current versus Supply Voltage

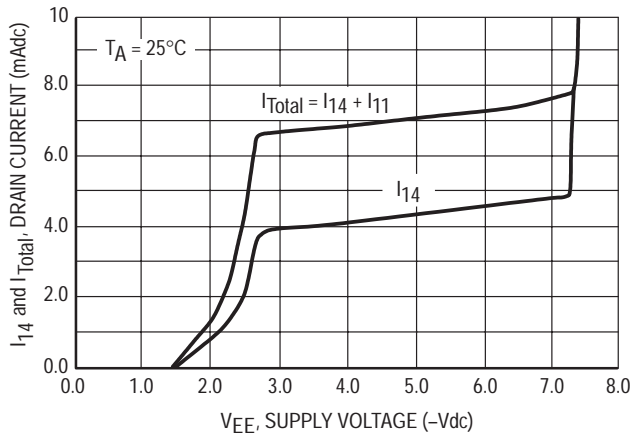


Figure 4. RSSI Output versus Frequency and Input Signal Level

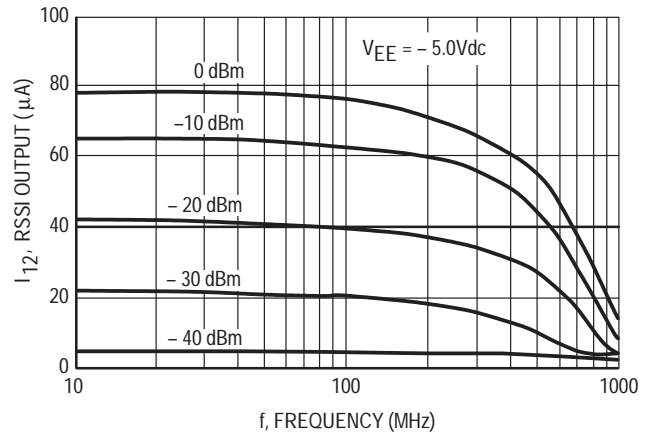


Figure 5. Total Drain Current versus Ambient Temperature and Supply Voltage

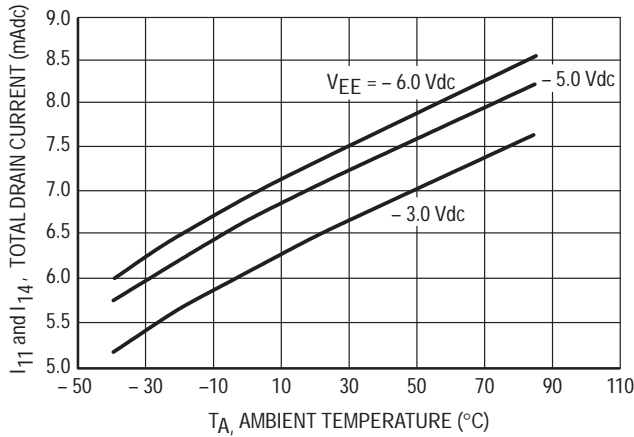


Figure 6. Detector Drain Current and Limiter Drain Current versus Ambient Temperature

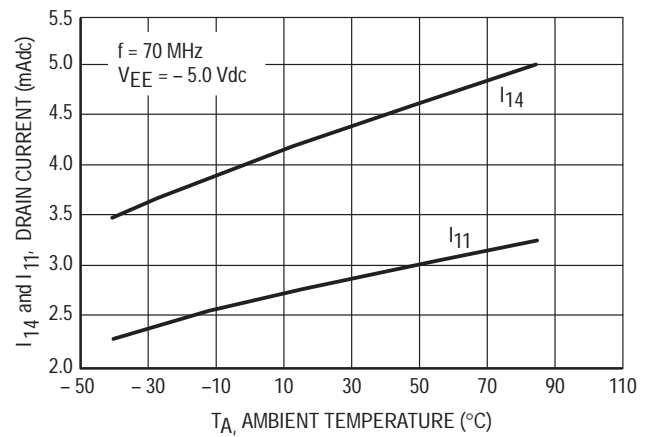


Figure 7. RSSI Output versus Ambient Temperature and Supply Voltage

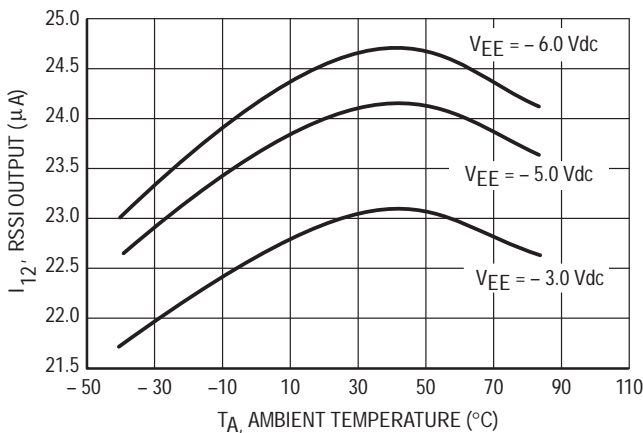
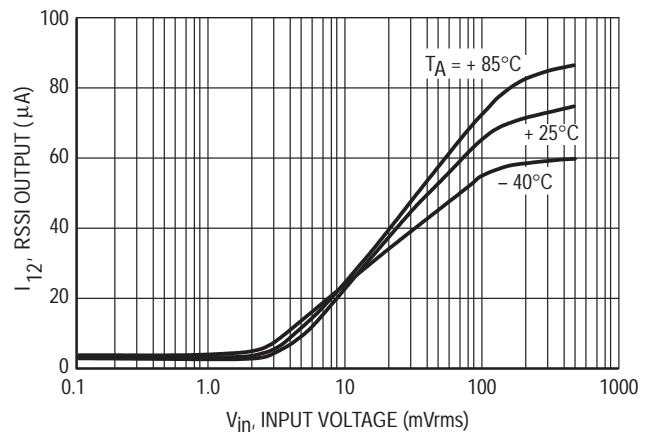


Figure 8. RSSI Output versus Input Signal Voltage (Vin at Temperature)



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Figure 9. Differential Detector Output Voltage versus Ambient Temperature and Supply Voltage

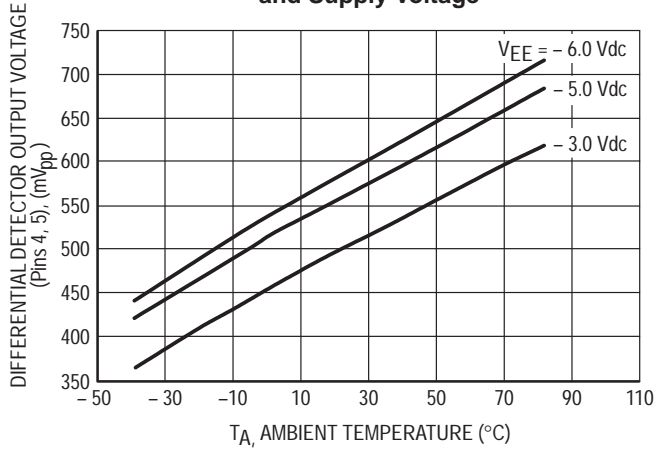


Figure 10. Differential Limiter Output Voltage versus Ambient Temperature (V_{in} = 1 and 10 mVrms)

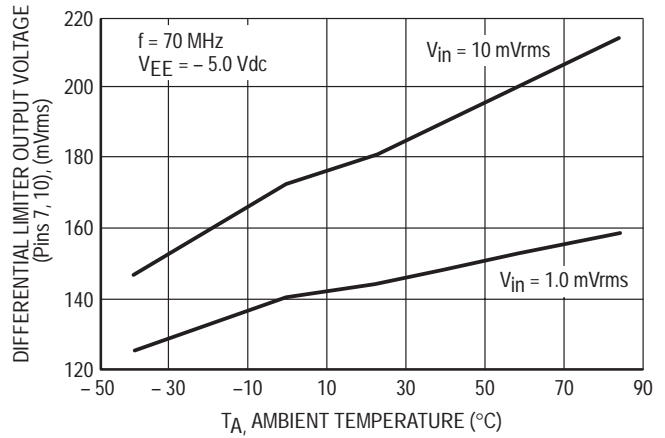


Figure 11A. Differential Detector Output Voltage versus Q of Quadrature LC Tank

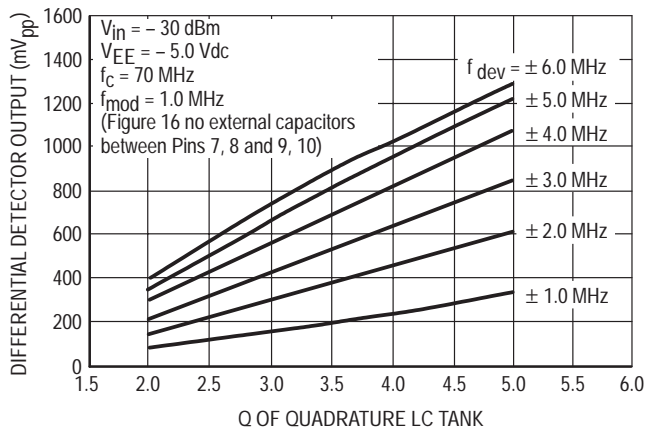


Figure 11B. Differential Detector Output Voltage versus Q of Quadrature LC Tank

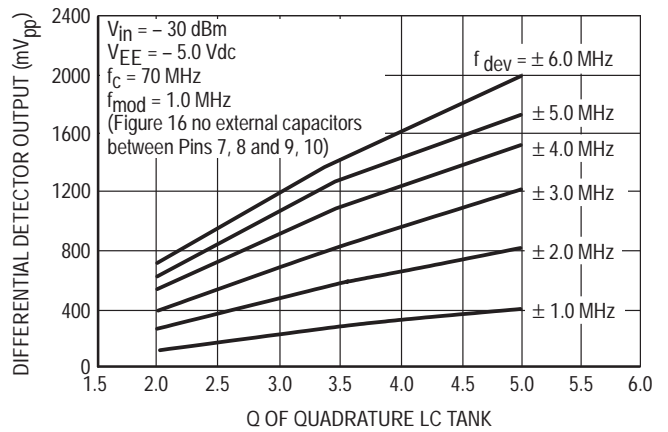


Figure 12. RSSI Output Voltage versus IF Input

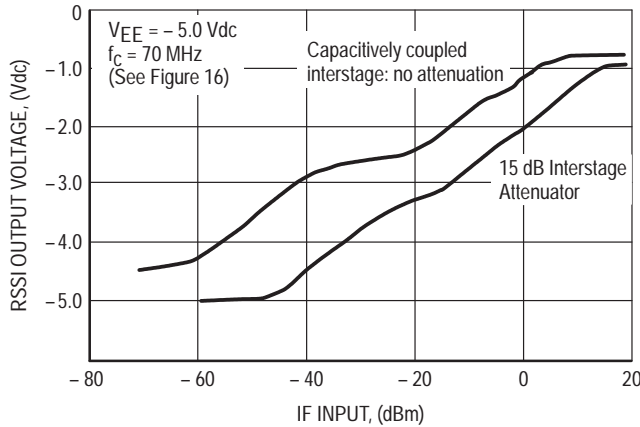
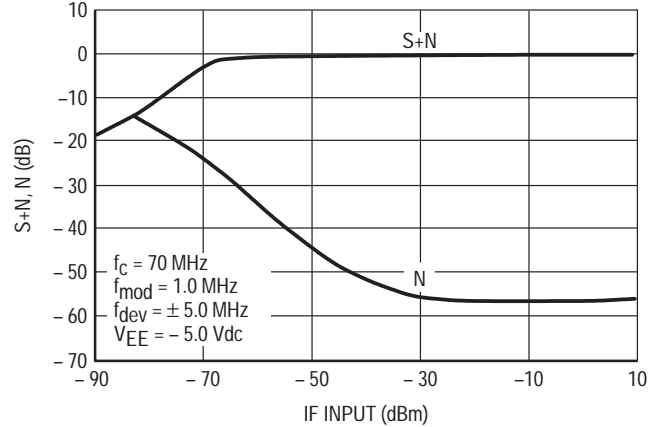


Figure 13. - S+N, N versus IF Input



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NOT RECOMMENDED FOR NEW DESIGNS

MC13155

In the S-parameters measurements, the IF is treated as a two-port linear class A amplifier. The IF amplifier is measured with a single-ended input and output configuration in which the Pins 16 and 7 are terminated in the series combination of a 47 Ω resistor and a 10 nF capacitor to V_{CC} ground (see Figure 14. S-Parameter Test Circuit).

The S-parameters are in polar form as the magnitude (MAG) and angle (ANG). Also listed in the tables are the calculated values for the stability factor (K) and the Maximum

Available Gain (MAG). These terms are related in the following equations:

$$K = (1 - |S_{11}|^2 - |S_{22}|^2 + |\Delta|^2) / (2 |S_{12} S_{21}|)$$

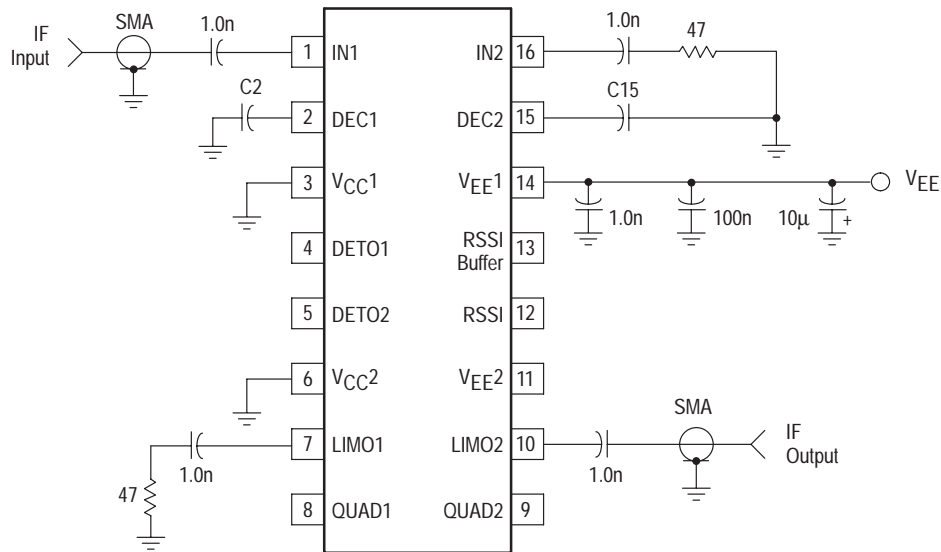
where: $|\Delta| = |S_{11} S_{22} - S_{12} S_{21}|$.

$$\text{MAG} = 10 \log |S_{21}| / |S_{12}| + 10 \log |K - (K^2 - 1)^{1/2}|$$

where: $K > 1$. The necessary and sufficient conditions for unconditional stability are given as $K > 1$:

$$B1 = 1 + |S_{11}|^2 - |S_{22}|^2 - |\Delta|^2 > 0$$

Figure 14. S-Parameter Test Circuit



MC13155

S-Parameters ($V_{EE} = -5.0$ Vdc, $T_A = 25^\circ\text{C}$, C_2 and $C_{15} = 0$ pF)

Frequency	Input S11		Forward S21		Rev S12		Output S22		K	MAG
MHz	MAG	ANG	MAG	ANG	MAG	ANG	MAG	ANG	MAG	dB
1.0	0.94	-13	8.2	143	0.001	7.0	0.87	-22	2.2	32
2.0	0.78	-23	23.5	109	0.001	-40	0.64	-31	4.2	33.5
5.0	0.48	1.0	39.2	51	0.001	-97	0.34	-17	8.7	33.7
7.0	0.59	15	40.3	34	0.001	-41	0.33	-13	10.6	34.6
10	0.75	17	40.9	19	0.001	-82	0.41	-1.0	5.7	36.7
20	0.95	7.0	42.9	-6.0	0.001	-42	0.45	0	1.05	46.4
50	0.98	-10	42.2	-48	0.001	-9.0	0.52	-3.0	0.29	-
70	0.95	-16	39.8	-68	0.001	112	0.54	-16	1.05	46.4
100	0.93	-23	44.2	-93	0.001	80	0.53	-22	0.76	-
150	0.91	-34	39.5	-139	0.001	106	0.50	-34	0.94	-
200	0.87	-47	34.9	-179	0.002	77	0.42	-44	0.97	-
500	0.89	-103	11.1	-58	0.022	57	0.40	-117	0.75	-
700	0.61	-156	3.5	-164	0.03	0	0.52	179	2.6	13.7
900	0.56	162	1.2	92	0.048	-44	0.47	112	4.7	4.5
1000	0.54	131	0.8	42	0.072	-48	0.44	76	5.1	0.4

S-Parameters ($V_{EE} = -5.0$ Vdc, $T_A = 25^\circ\text{C}$, C_2 and $C_{15} = 100$ pF)

Frequency	Input S11		Forward S21		Rev S12		Output S22		K	MAG
MHz	MAG	ANG	MAG	ANG	MAG	ANG	MAG	ANG	MAG	dB
1.0	0.98	-15	11.7	174	0.001	-14	0.84	-27	1.2	37.4
2.0	0.50	-2.0	39.2	85.5	0.001	-108	0.62	-35	6.0	35.5
5.0	0.87	8.0	39.9	19	0.001	100	0.47	-9.0	4.2	39.2
7.0	0.90	5.0	40.4	9.0	0.001	-40	0.45	-8.0	3.1	40.3
10	0.92	3.0	41	1.0	0.001	-40	0.44	-5.0	2.4	41.8
20	0.92	-2.0	42.4	-14	0.001	-87	0.49	-6.0	2.4	41.9
50	0.91	-8.0	41.2	-45	0.001	85	0.50	-5.0	2.3	42
70	0.91	-11	39.1	-63	0.001	76	0.52	-4.0	2.2	41.6
100	0.91	-15	43.4	-84	0.001	85	0.50	-11	1.3	43.6
150	0.90	-22	38.2	-126	0.001	96	0.43	-22	1.4	41.8
200	0.86	-33	35.5	-160	0.002	78	0.43	-21	1.3	39.4
500	0.80	-66	8.3	-9.0	0.012	75	0.57	-63	1.7	23.5
700	0.62	-96	2.9	-95	0.013	50	0.49	-111	6.3	12.5
900	0.56	-120	1.0	-171	0.020	53	0.44	-150	13.3	2.8
1000	0.54	-136	0.69	154	0.034	65	0.44	-179	12.5	-0.8

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13155

S-Parameters ($V_{EE} = -5.0$ Vdc, $T_A = 25^\circ\text{C}$, C_2 and $C_{15} = 680$ pF)

Frequency	Input S11		Forward S21		Rev S12		Output S22		K	MAG
	MHz	MAG	ANG	MAG	ANG	MAG	ANG	MAG	ANG	MAG
1.0	0.74	4.0	53.6	110	0.001	101	0.97	-35	0.58	-
2.0	0.90	3.0	70.8	55	0.001	60	0.68	-34	1.4	45.6
5.0	0.91	0	87.1	21	0.001	-121	0.33	-60	1.1	49
7.0	0.91	0	90.3	11	0.001	-18	0.25	-67	1.2	48.4
10	0.91	-2.0	92.4	2.0	0.001	33	0.14	-67	1.5	47.5
20	0.91	-4.0	95.5	-16	0.001	63	0.12	-15	1.3	48.2
50	0.90	-8.0	89.7	-50	0.001	-43	0.24	26	1.8	46.5
70	0.90	-10	82.6	-70	0.001	92	0.33	21	1.4	47.4
100	0.91	-14	77.12	-93	0.001	23	0.42	-1.0	1.05	49
150	0.94	-20	62.0	-122	0.001	96	0.42	-22	0.54	-
200	0.95	-33	56.9	-148	0.003	146	0.33	-62	0.75	-
500	0.82	-63	12.3	-12	0.007	79	0.44	-67	1.8	26.9
700	0.66	-98	3.8	-107	0.014	84	0.40	-115	4.8	14.6
900	0.56	-122	1.3	177	0.028	78	0.39	-166	8.0	4.7
1000	0.54	-139	0.87	141	0.048	76	0.41	165	7.4	0.96

S-Parameters ($V_{EE} = -3.0$ Vdc, $T_A = 25^\circ\text{C}$, C_2 and $C_{15} = 0$ pF)

Frequency	Input S11		Forward S21		Rev S12		Output S22		K	MAG
	MHz	MAG	ANG	MAG	ANG	MAG	ANG	MAG	ANG	MAG
1.0	0.89	-14	9.3	136	0.001	2.0	0.84	-27	3.2	30.7
2.0	0.76	-22	24.2	105	0.001	-90	0.67	-37	3.5	34.3
5.0	0.52	5.0	35.7	46	0.001	-32	0.40	-13	10.6	33.3
7.0	0.59	12	38.1	34	0.001	-41	0.40	-10	9.1	34.6
10	0.78	15	37.2	16	0.001	-92	0.40	-1.0	5.7	36.3
20	0.95	5.0	38.2	-9.0	0.001	47	0.51	-4.0	0.94	-
50	0.96	-11	39.1	-50	0.001	-103	0.48	-6.0	1.4	43.7
70	0.93	-17	36.8	-71	0.001	-76	0.52	-13	2.2	41.4
100	0.91	-25	34.7	-99	0.001	-152	0.51	-19	3.0	39.0
150	0.86	-37	33.8	-143	0.001	53	0.49	-34	1.7	39.1
200	0.81	-49	27.8	86	0.003	76	0.55	-56	2.4	35.1
500	0.70	-93	6.2	-41	0.015	93	0.40	-110	2.4	19.5
700	0.62	-144	1.9	-133	0.049	56	0.40	-150	3.0	8.25
900	0.39	-176	0.72	125	0.11	-18	0.25	163	5.1	-1.9
1000	0.44	166	0.49	80	0.10	-52	0.33	127	7.5	-4.8

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13155

S-Parameters ($V_{EE} = -3.0$ Vdc, $T_A = 25^\circ\text{C}$, C_2 and $C_{15} = 100$ pF)

Frequency	Input S11		Forward S21		Rev S12		Output S22		K	MAG
MHz	MAG	ANG	MAG	ANG	MAG	ANG	MAG	ANG	MAG	dB
1.0	0.97	-15	11.7	171	0.001	-4.0	0.84	-27	1.4	36.8
2.0	0.53	2.0	37.1	80	0.001	-91	0.57	-31	6.0	34.8
5.0	0.88	7.0	37.7	18	0.001	-9.0	0.48	-7.0	3.4	39.7
7.0	0.90	5.0	37.7	8.0	0.001	-11	0.49	-7.0	2.3	41
10	0.92	2.0	38.3	1.0	0.001	-59	0.51	-9.0	2.0	41.8
20	0.92	-2.0	39.6	-15	0.001	29	0.48	-3.0	1.9	42.5
50	0.91	-8.0	38.5	-46	0.001	-21	0.51	-7.0	2.3	41.4
70	0.91	-11	36.1	-64	0.001	49	0.50	-8.0	2.3	40.8
100	0.91	-15	39.6	-85	0.001	114	0.52	-13	1.7	37.8
150	0.89	-22	34.4	-128	0.001	120	0.48	-23	1.6	40.1
200	0.86	-33	32	-163	0.002	86	0.40	-26	1.7	37.8
500	0.78	-64	7.6	-12	0.013	94	0.46	-71	1.9	22.1
700	0.64	-98	2.3	-102	0.027	58	0.42	-109	4.1	10.1
900	0.54	-122	0.78	179	0.040	38.6	0.35	-147	10.0	-0.14
1000	0.53	-136	0.47	144	0.043	23	0.38	-171	15.4	-4.52

S-Parameters ($V_{EE} = -3.0$ Vdc, $T_A = 25^\circ\text{C}$, C_2 and $C_{15} = 680$ pF)

Frequency	Input S11		Forward S21		Rev S12		Output S22		K	MAG
MHz	MAG	ANG	MAG	ANG	MAG	ANG	MAG	ANG	MAG	dB
1.0	0.81	3.0	37	101	0.001	-19	0.90	-32	1.1	43.5
2.0	0.90	2.0	47.8	52.7	0.001	-82	0.66	-39	0.72	-
5.0	0.91	0	58.9	20	0.001	104	0.37	-56	2.3	44
7.0	0.90	-1	60.3	11	0.001	-76	0.26	-55	2.04	44
10	0.91	-2.0	61.8	3.0	0.001	105	0.18	-52	2.2	43.9
20	0.91	-4.0	63.8	-15	0.001	59	0.11	-13	2.0	44.1
50	0.90	-8.0	60.0	-48	0.001	96	0.22	33	2.3	43.7
70	0.90	-11	56.5	-67	0.001	113	0.29	15	2.3	43.2
100	0.91	-14	52.7	-91	0.001	177	0.36	5.0	2.0	43
150	0.93	-21	44.5	-126	0.001	155	0.35	-17	1.8	42.7
200	0.90	-43	41.2	-162	0.003	144	0.17	-31	1.6	34.1
500	0.79	-65	7.3	-13	0.008	80	0.44	-75	3.0	22
700	0.65	-97	2.3	-107	0.016	86	0.38	-124	7.1	10.2
900	0.56	-122	0.80	174	0.031	73	0.38	-174	12	0.37
1000	0.55	-139	0.52	137	0.50	71	0.41	157	11.3	-3.4

NOT RECOMMENDED FOR NEW DESIGNS

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DC Biasing Considerations

The DC biasing scheme utilizes two V_{CC} connections (Pins 3 and 6) and two V_{EE} connections (Pins 14 and 11). V_{EE1} (Pin 14) is connected internally to the IF and RSSI circuits' negative supply bus while V_{EE2} (Pin 11) is connected internally to the quadrature detector's negative bus. Under positive ground operation, this unique configuration offers the ability to bias the RSSI and IF separately from the quadrature detector. When two ICs are cascaded as shown in the 70 MHz application circuit and provided by the PCB (see Figures 17 and 18), the first MC13155 is used without biasing its quadrature detector, thereby saving approximately 3.0 mA. A total current of 7.0 mA is used to fully bias each IC, thus the total current in the application circuit is approximately 11 mA. Both V_{CC} pins are biased by the same supply. V_{CC1} (Pin 3) is connected internally to the positive bus of the first half of the IF limiting amplifier, while V_{CC2} is internally connected to the positive bus of the RSSI, the quadrature detector circuit, and the second half of the IF limiting amplifier (see Figure 15). This distribution of the V_{CC} enhances the stability of the IC.

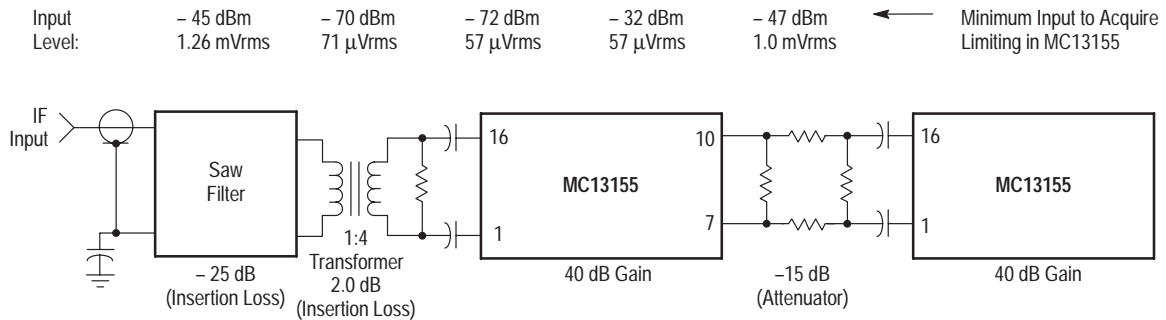
RSSI Circuitry

The RSSI circuitry provides typically 35 dB of linear dynamic range and its output voltage swing is adjusted by

selection of the resistor from Pin 12 to V_{EE} . The RSSI slope is typically $2.1 \mu A/dB$; thus, for a dynamic range of 35 dB, the current output is approximately $74 \mu A$. A 47 k resistor will yield an RSSI output voltage swing of 3.5 Vdc. The RSSI buffer output at Pin 13 is an emitter-follower and needs an external emitter resistor of 10 k to V_{EE} .

In a cascaded configuration (see circuit application in Figure 16), only one of the RSSI Buffer outputs (Pin 13) is used; the RSSI outputs (Pin 12 of each IC) are tied together and the one closest to the V_{EE} supply trace is decoupled to V_{CC} ground. The two pins are connected to V_{EE} through a 47 k resistor. This resistor sources a RSSI current which is proportional to the signal level at the IF input; typically, 1.0 mVrms (-47 dBm) is required to place the MC13155 into limiting. The measured RSSI output voltage response of the application circuit is shown in Figure 12. Since the RSSI current output is dependent upon the input signal level at the IF input, a careful accounting of filter losses, matching and other losses and gains must be made in the entire receiver system. In the block diagram of the application circuit shown below, an accounting of the signal levels at points throughout the system shows how the RSSI response in Figure 12 is justified.

Block Diagram of 70 MHz Video Receiver Application Circuit



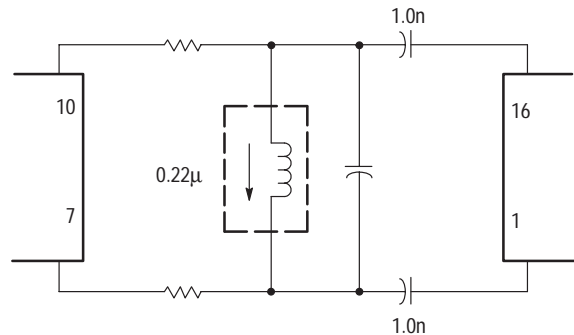
Cascading Stages

The limiting IF output is pinned-out differentially, cascading is easily achieved by AC coupling stage to stage. In the evaluation PCB, AC coupling is shown, however, interstage filtering may be desirable in some applications. In which case, the S-parameters provide a means to implement a low loss interstage match and better receiver sensitivity.

Where a linear response of the RSSI output is desired when cascading the ICs, it is necessary to provide at least 10 dB of interstage loss. Figure 12 shows the RSSI response with and without interstage loss. A 15 dB resistive attenuator is an inexpensive way to linearize the RSSI response. This has its drawbacks since it is a wideband noise source that is dependent upon the source and load impedance and the amount of attenuation that it provides. A better, although more costly, solution would be a bandpass filter designed to the desired center frequency and bandpass response while carefully selecting the insertion loss. A network topology

shown below may be used to provide a bandpass response with the desired insertion loss.

Network Topology



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Quadrature Detector

The quadrature detector is coupled to the IF with internal 2.0 pF capacitors between Pins 7 and 8 and Pins 9 and 10. For wideband data applications, such as FM video and satellite receivers, the drive to the detector can be increased with additional external capacitors between these pins, thus, the recovered video signal level output is increased for a given bandwidth (see Figure 11A and Figure 11B).

The wideband performance of the detector is controlled by the loaded Q of the LC tank circuit. The following equation defines the components which set the detector circuit's bandwidth:

$$Q = R_T / X_L \quad (1)$$

where: R_T is the equivalent shunt resistance across the LC Tank and X_L is the reactance of the quadrature inductor at the IF frequency ($X_L = 2\pi fL$).

The inductor and capacitor are chosen to form a resonant LC Tank with the PCB and parasitic device capacitance at the desired IF center frequency as predicted by:

$$f_c = (2\pi \sqrt{LC_p})^{-1} \quad (2)$$

where: L is the parallel tank inductor and C_p is the equivalent parallel capacitance of the parallel resonant tank circuit.

The following is a design example for a wideband detector at 70 MHz and a loaded Q of 5. The loaded Q of the quadrature detector is chosen somewhat less than the Q of the IF bandpass. For an IF frequency of 70 MHz and an IF bandpass of 10.9 MHz, the IF bandpass Q is approximately 6.4.

Example:

Let the external $C_{ext} = 20$ pF. (The minimum value here should be greater than 15 pF making it greater than the internal device and PCB parasitic capacitance, $C_{int} \approx 3.0$ pF).

$$C_p = C_{int} + C_{ext} = 23 \text{ pF}$$

Rewrite Equation 2 and solve for L:

$$L = (0.159)^2 / (C_p f_c^2)$$

$L = 198$ nH, thus, a standard value is chosen.

$L = 0.22$ μ H (tunable shielded inductor).

The value of the total damping resistor to obtain the required loaded Q of 5 can be calculated by rearranging Equation 1:

$$R_T = Q(2\pi fL)$$

$$R_T = 5 (2\pi)(70)(0.22) = 483.8 \Omega.$$

The internal resistance, R_{int} between the quadrature tank Pins 8 and 9 is approximately 3200 Ω and is considered in determining the external resistance, R_{ext} which is calculated from:

$$R_{ext} = ((R_T)(R_{int})) / (R_{int} - R_T)$$

$R_{ext} = 570$, thus, choose the standard value.

$R_{ext} = 560 \Omega$.

SAW Filter

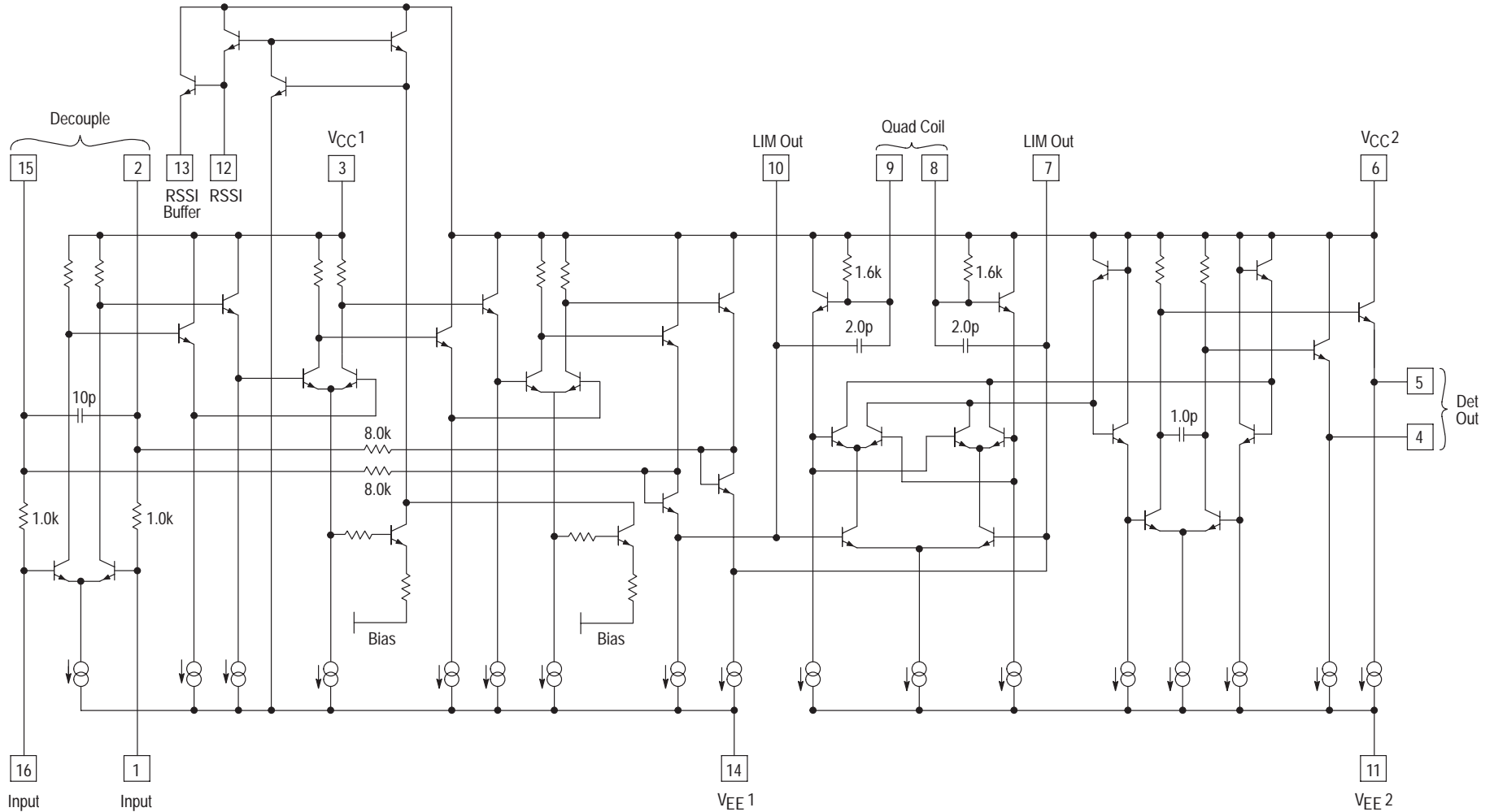
In wideband video data applications, the IF occupied bandwidth may be several MHz wide. A good rule of thumb is to choose the IF frequency about 10 or more times greater than the IF occupied bandwidth. The IF bandpass filter is a SAW filter in video data applications where a very selective response is needed (i.e., very sharp bandpass response). The evaluation PCB is laid out to accommodate two SAW filter package types: 1) A five-leaded plastic SIP package. Recommended part numbers are Siemens X6950M which operates at 70 MHz; 10.4 MHz 3 dB passband, X6951M (X252.8) which operates at 70 MHz; 9.2 MHz 3 dB passband; and X6958M which operates at 70 MHz, 6.3 MHz 3 dB passband, and 2) A four-leaded TO-39 metal can package. Typical insertion loss in a wide bandpass SAW filter is 25 dB.

The above SAW filters require source and load impedances of 50 Ω to assure stable operation. On the PCB board layout, space is provided to add a matching network, such as a 1:4 surface mount transformer between the SAW filter output and the input to the MC13155. A 1:4 transformer, made by Coilcraft and Mini Circuits, provides a suitable interface (see Figures 16, 17 and 18). In the circuit and layout, the SAW filter and the MC13155 are differentially configured with interconnect traces which are equal in length and symmetrical. This balanced feed enhances RF stability, phase linearity, and noise performance.

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MC13155
3-2-150

Figure 15. Simplified Internal Circuit Schematic



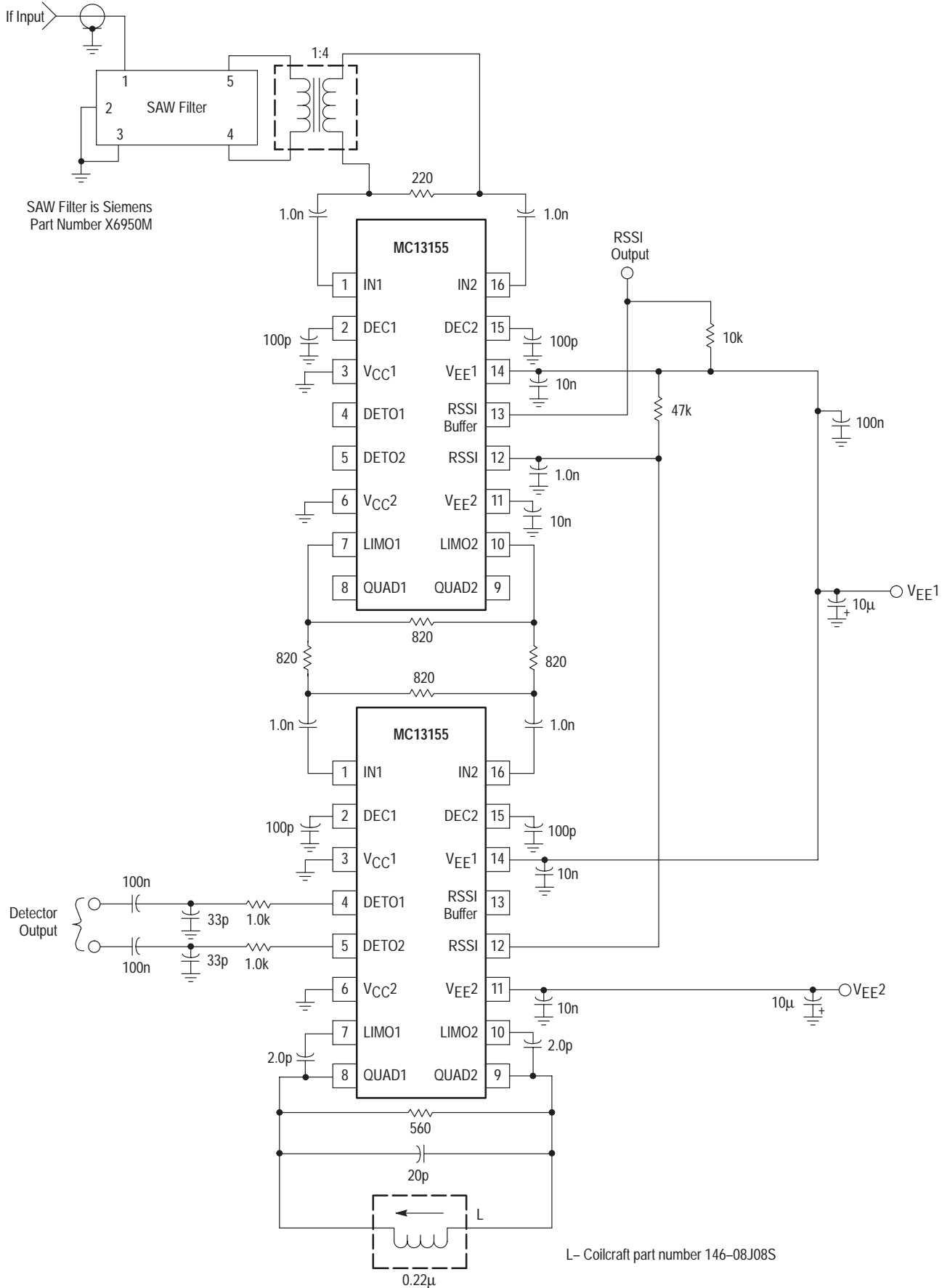
MOTOROLA WIRELESS RF, IF AND TRANSMITTER DEVICE DATA

MC13155

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MC13155

Figure 16. 70 MHz Video Receiver Application Circuit



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MC13155

Figure 19. Circuit Side View

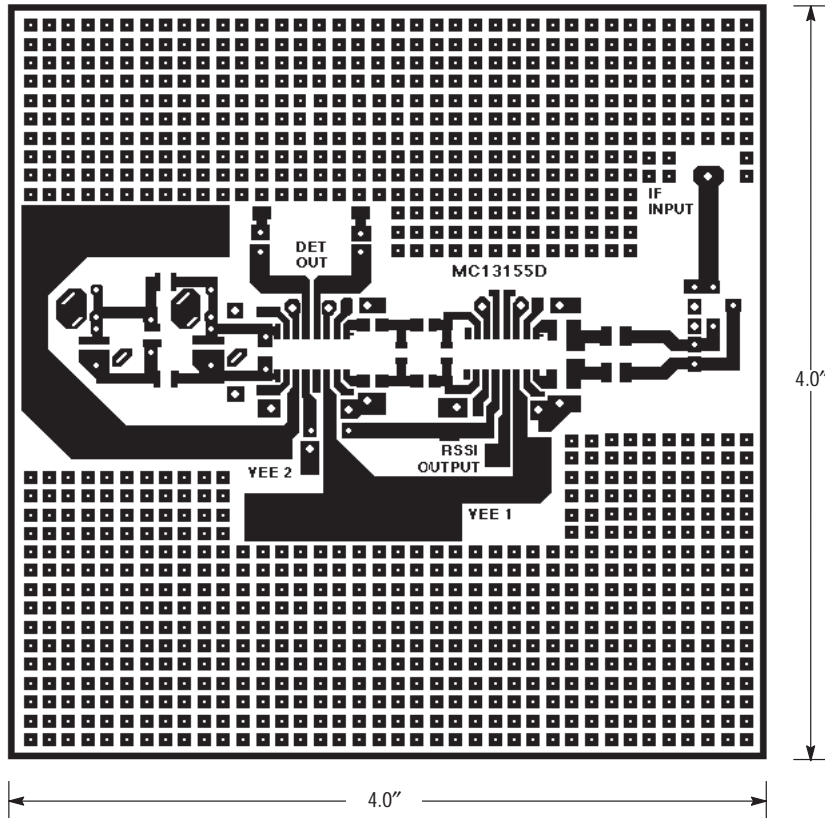
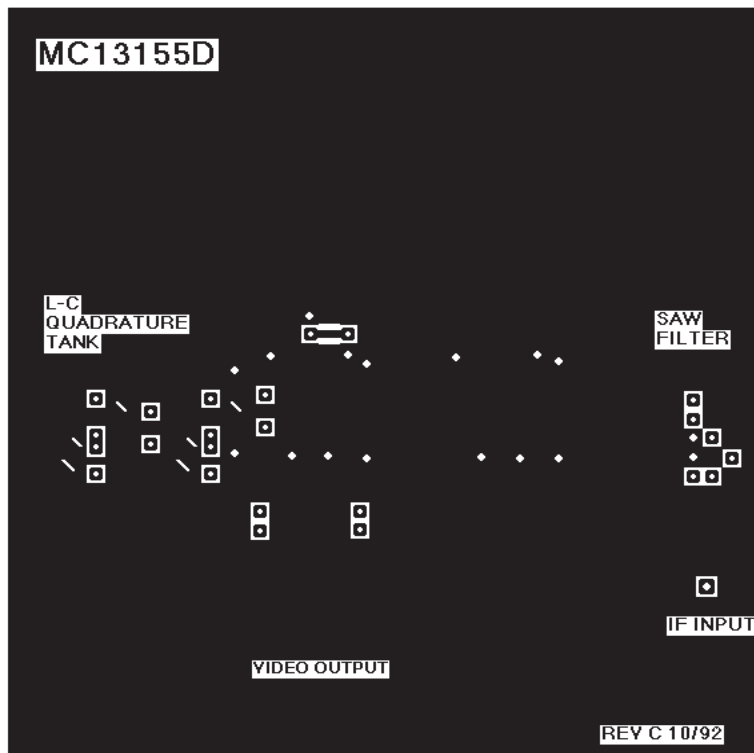


Figure 20. Ground Side View



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MC13156

Wideband FM IF System

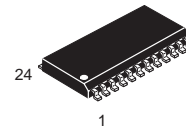
The MC13156 is a wideband FM IF subsystem targeted at high performance data and analog applications. Excellent high frequency performance is achieved at low cost using Motorola's MOSAIC 1.5™ bipolar process. The MC13156 has an onboard grounded collector VCO transistor that may be used with a fundamental or overtone crystal in single channel operation or with a PLL in multichannel operation. The mixer is useful to 500 MHz and may be used in a balanced-differential, or single-ended configuration. The IF amplifier is split to accommodate two low cost cascaded filters. RSSI output is derived by summing the output of both IF sections. A precision data shaper has a hold function to preset the shaper for fast recovery of new data.

Applications for the MC13156 include CT-2, wideband data links and other radio systems utilizing GMSK, FSK or FM modulation.

- 2.0 to 6.0 Vdc Operation
- Typical Sensitivity at 200 MHz of 2.0 μ V for 12 dB SINAD
- RSSI Dynamic Range Typically 80 dB
- High Performance Data Shaper for Enhanced CT-2 Operation
- Internal 330 Ω and 1.4 k Ω Terminations for 10.7 MHz and 455 kHz Filters
- Split IF for Improved Filtering and Extended RSSI Range
- 3rd Order Intercept (Input) of -25 dBm (Input Matched)

WIDEBAND FM IF SYSTEM FOR DIGITAL AND ANALOG APPLICATIONS

SEMICONDUCTOR TECHNICAL DATA



DW SUFFIX
PLASTIC PACKAGE
CASE 751E
(SO-24L)



FB SUFFIX
PLASTIC QFP PACKAGE
CASE 873

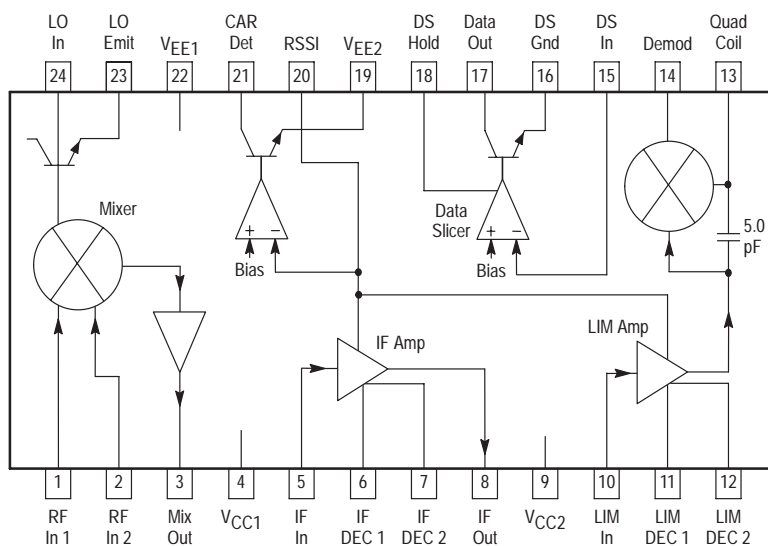
PIN CONNECTIONS

Function	SO-24L	QFP
RF Input 1	1	31
RF Input 2	2	32
Mixer Output	3	1
V _{CC} 1	4	2
IF Amp Input	5	3
IF Amp Decoupling 1	6	4
IF Amp Decoupling 2	7	5
V _{CC} Connect (N/C Internal)	-	6
IF Amp Output	8	7
V _{CC} 2	9	8
Limiter IF Input	10	9
Limiter Decoupling 1	11	10
Limiter Decoupling 2	12	11
V _{CC} Connect (N/C Internal)	-	12, 13, 14
Quad Coil	13	15
Demodulator Output	14	16
Data Slicer Input	15	17
V _{CC} Connect (N/C Internal)	-	18
Data Slicer Ground	16	19
Data Slicer Output	17	20
Data Slicer Hold	18	21
V _{EE} 2	19	22
RSSI Output/Carrier Detect In	20	23
Carrier Detect Output	21	24
V _{EE} 1 and Substrate	22	25
LO Emitter	23	26
LO Base	24	27
V _{CC} Connect (N/C Internal)	-	28, 29, 30

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13156DW	T _A = -40 to +85°C	SO-24L
MC13156FB		QFP

Simplified Block Diagram



NOTE: Pin Numbers shown for SOIC package only. Refer to Pin Assignments Table.

This device contains 197 active transistors.

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13156

MAXIMUM RATINGS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage	16, 19, 22	$V_{EE(max)}$	-6.5	Vdc
Junction Temperature	-	$T_{J(max)}$	150	°C
Storage Temperature Range	-	T_{stg}	-65 to +150	°C

NOTES: 1. Devices should not be operated at or outside these values. The "Recommended Operating Conditions" table provides for actual device operation.
2. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage @ $T_A = 25^\circ\text{C}$ $-40^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$	4, 9 16, 19, 22	V_{CC} V_{EE}	0 (Ground) -2.0 to -6.0	Vdc
Input Frequency	1, 2	f_{in}	500	MHz
Ambient Temperature Range	-	T_A	-40 to +85	°C
Input Signal Level	1, 2	V_{in}	200	mVrms

DC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, $V_{CC1} = V_{CC2} = 0$, no input signal.)

Characteristic	Pin	Symbol	Min	Typ	Max	Unit
Total Drain Current (See Figure 2) $V_{EE} = -2.0$ Vdc $V_{EE} = -3.0$ Vdc $V_{EE} = -5.0$ Vdc $V_{EE} = -6.0$ Vdc	19, 22	I_{Total}	- 3.0 - -	4.8 5.0 5.2 5.4	- 8.0 - -	mA
Drain Current, I_{22} (See Figure 3) $V_{EE} = -2.0$ Vdc $V_{EE} = -3.0$ Vdc $V_{EE} = -5.0$ Vdc $V_{EE} = -6.0$ Vdc	22	I_{22}	- - - -	3.0 3.1 3.3 3.4	- - - -	mA
Drain Current, I_{19} (See Figure 3) $V_{EE} = -2.0$ Vdc $V_{EE} = -3.0$ Vdc $V_{EE} = -5.0$ Vdc $V_{EE} = -6.0$ Vdc	19	I_{19}	- - - -	1.8 1.9 1.9 2.0	- - - -	mA

DATA SLICER (Input Voltage Referenced to $V_{EE} = -3.0$ Vdc, no input signal; See Figure 15.)

Input Threshold Voltage (High V_{in})	15	V_{15}	1.0	1.1	1.2	Vdc
Output Current (Low V_{in}) Data Slicer Enabled (No Hold) $V_{15} > 1.1$ Vdc $V_{18} = 0$ Vdc	17	I_{17}	-	1.7	-	mA

AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$, $V_{EE} = -3.0$ Vdc, $f_{RF} = 130$ MHz, $f_{LO} = 140.7$ MHz, Figure 1 test circuit, unless otherwise specified.)

Characteristic	Pin	Symbol	Min	Typ	Max	Unit
12 dB SINAD Sensitivity (See Figures 17, 25) $f_{in} = 144.45$ MHz; $f_{mod} = 1.0$ kHz; $f_{dev} = \pm 75$ kHz	1, 14	-	-	-100	-	dBm

MIXER

Conversion Gain $P_{in} = -37$ dBm (Figure 4)	1, 3	-	-	22	-	dB
Mixer Input Impedance Single-Ended (Table 1)	1, 2	R_p C_p	- -	1.0 4.0	- -	k Ω pF
Mixer Output Impedance	3	-	-	330	-	Ω

IF AMPLIFIER SECTION

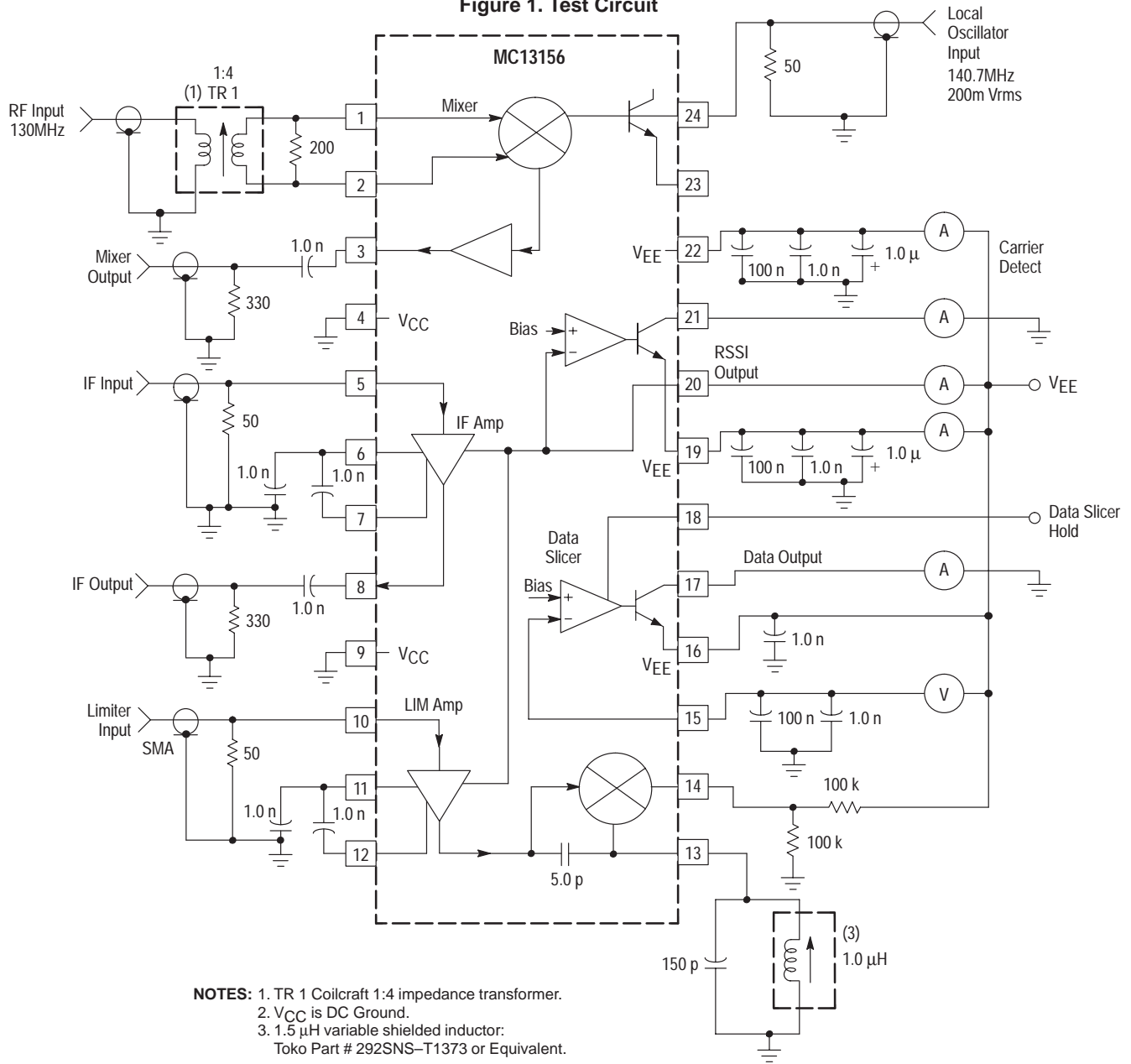
IF RSSI Slope (Figure 6)	20	-	0.2	0.4	0.6	$\mu\text{A/dB}$
IF Gain (Figure 5)	5, 8	-	-	39	-	dB
Input Impedance	5	-	-	1.4	-	k Ω
Output Impedance	8	-	-	290	-	Ω

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AC ELECTRICAL CHARACTERISTICS (continued) ($T_A = 25^\circ\text{C}$, $V_{EE} = -3.0\text{ Vdc}$, $f_{RF} = 130\text{ MHz}$, $f_{LO} = 140.7\text{ MHz}$, Figure 1 test circuit, unless otherwise specified.)

Characteristic	Pin	Symbol	Min	Typ	Max	Unit
LIMITING AMPLIFIER SECTION						
Limiter RSSI Slope (Figure 7)	20	-	0.2	0.4	0.6	$\mu\text{A/dB}$
Limiter Gain	-	-	-	55	-	dB
Input Impedance	10	-	-	1.4	-	$\text{k}\Omega$
CARRIER DETECT						
Output Current – Carrier Detect (High V_{in})	21	-	-	0	-	μA
Output Current – Carrier Detect (Low V_{in})	21	-	-	3.0	-	mA
Input Threshold Voltage – Carrier Detect Input Voltage Referenced to $V_{EE} = -3.0\text{ Vdc}$	20	-	0.9	1.2	1.4	Vdc

Figure 1. Test Circuit



NOTES: 1. TR 1 Coilcraft 1:4 impedance transformer.
 2. V_{CC} is DC Ground.
 3. 1.5 μH variable shielded inductor:
 Toko Part # 292SNS-T1373 or Equivalent.

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Figure 2. Total Drain Current versus Supply Voltage and Temperature

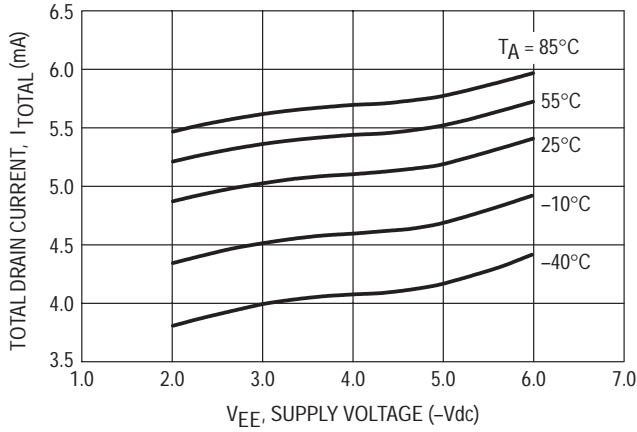


Figure 3. Drain Currents versus Supply Voltage

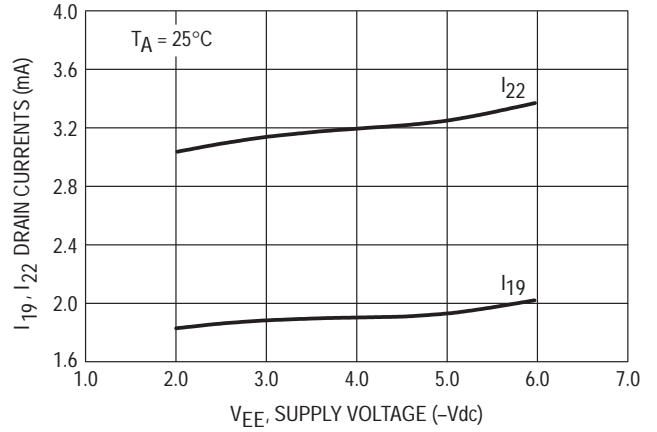


Figure 4. Mixer Gain versus Input Signal Level

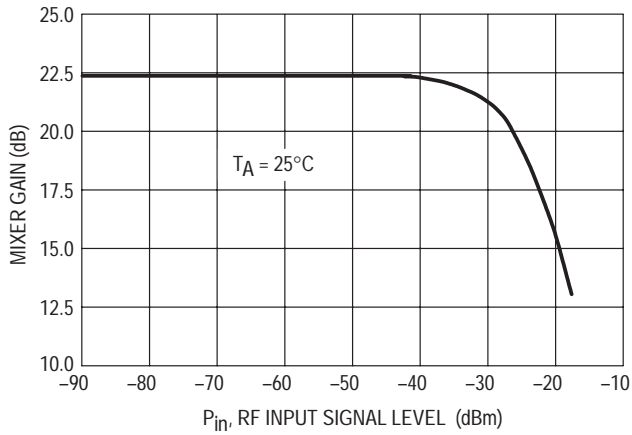


Figure 5. IF Amplifier Gain versus Input Signal Level and Ambient Temperature

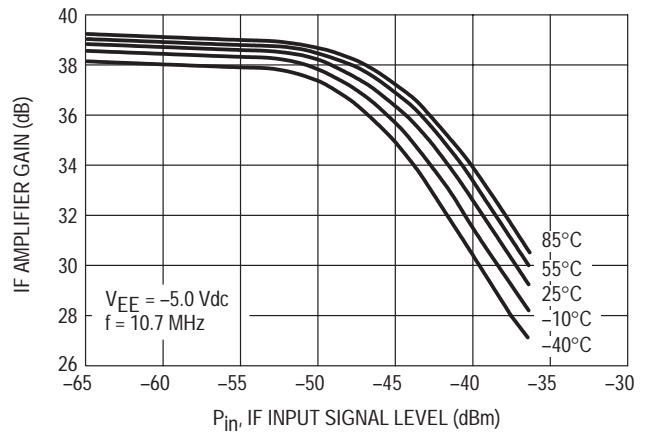


Figure 6. IF Amplifier RSSI Output Current versus Input Signal Level and Ambient Temperature

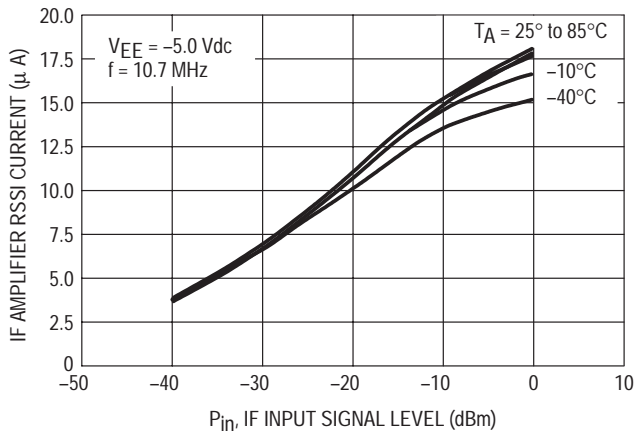
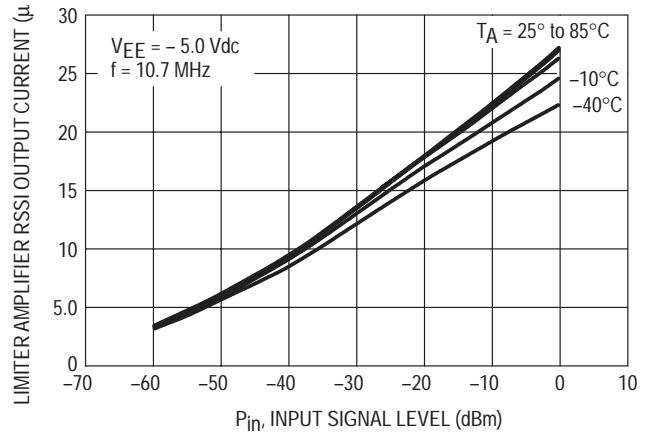


Figure 7. Limiter Amplifier RSSI Output Current versus Input Signal Level and Temperature

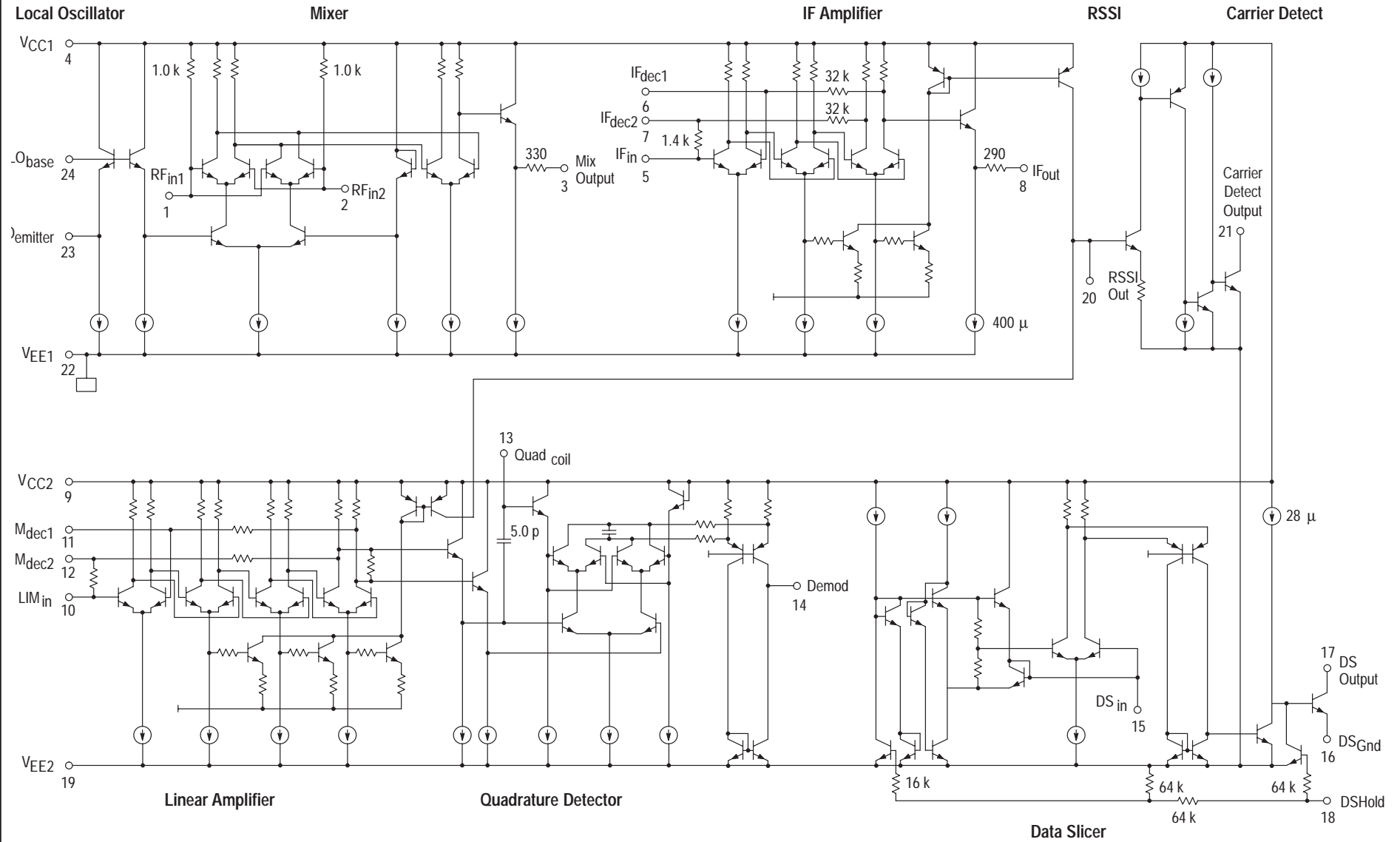


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Figure 8. MC13156DW Internal Circuit Schematic



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MOTOROLA WIRELESS RF, IF AND TRANSMITTER DEVICE DATA

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CIRCUIT DESCRIPTION

General

The MC13156 is a low power single conversion wideband FM receiver incorporating a split IF. This device is designated for use as the backend in digital FM systems such as CT-2 and wideband data links with data rates up to 500 kbaud. It contains a mixer, oscillator, signal strength meter drive, IF amplifier, limiting IF, quadrature detector and a data slicer with a hold function (refer to Figure 8, Simplified Internal Circuit Schematic).

Current Regulation

Temperature compensating voltage independent current regulators are used throughout.

Mixer

The mixer is a double-balanced four quadrant multiplier and is designed to work up to 500 MHz. It can be used in differential or in single-ended mode by connecting the other input to the positive supply rail.

Figure 4 shows the mixer gain and saturated output response as a function of input signal drive. The circuit used to measure this is shown in Figure 1. The linear gain of the mixer is approximately 22 dB. Figure 9 shows the mixer gain versus the IF output frequency with the local oscillator of 150 MHz at 100 mVrms LO drive level. The RF frequency is swept. The sensitivity of the IF output of the mixer is shown in Figure 10 for an RF input drive of 10 mVrms at 140 MHz and IF at 10 MHz.

The single-ended parallel equivalent input impedance of the mixer is $R_p \sim 1.0 \text{ k}\Omega$ and $C_p \sim 4.0 \text{ pF}$ (see Table 1 for details). The buffered output of the mixer is internally loaded resulting in an output impedance of 330Ω .

Local Oscillator

The on-chip transistor operates with crystal and LC resonant elements up to 220 MHz. Series resonant, overtone crystals are used to achieve excellent local oscillator stability. 3rd overtone crystals are used through about 65 to 70 MHz. Operation from 70 MHz up to 180 MHz is feasible using the on-chip transistor with a 5th or 7th overtone crystal. To enhance operation using an overtone crystal, the internal transistor's bias is increased by adding an external resistor from Pin 23 to V_{EE} . -10 dBm of local oscillator drive is needed to adequately drive the mixer (Figure 10).

The oscillator configurations specified above, and two others using an external transistor, are described in the application section:

- 1) A 133 MHz oscillator multiplier using a 3rd overtone crystal, and
- 2) A 307.8 to 309.3 MHz manually tuned, varactor controlled local oscillator.

RSSI

The Received Signal Strength Indicator (RSSI) output is a current proportional to the log of the received signal

amplitude. The RSSI current output is derived by summing the currents from the IF and limiting amplifier stages. An external resistor at Pin 20 sets the voltage range or swing of the RSSI output voltage. Linearity of the RSSI is optimized by using external ceramic or crystal bandpass filters which have an insertion loss of 8.0 dB. The RSSI circuit is designed to provide 70+ dB of dynamic range with temperature compensation (see Figures 6 and 7 which show RSSI responses of the IF and Limiter amplifiers). Variation in the RSSI output current with supply voltage is small (see Figure 11).

Carrier Detect

When the meter current flowing through the meter load resistance reaches 1.2 Vdc above ground, the comparator flips, causing the carrier detect output to go high. Hysteresis can be accomplished by adding a very large resistor for positive feedback between the output and the input of the comparator.

IF Amplifier

The first IF amplifier section is composed of three differential stages with the second and third stages contributing to the RSSI. This section has internal dc feedback and external input decoupling for improved symmetry and stability. The total gain of the IF amplifier block is approximately 39 dB at 10.7 MHz. Figure 5 shows the gain and saturated output response of the IF amplifier over temperature, while Figure 12 shows the IF amplifier gain as a function of the IF frequency.

The fixed internal input impedance is $1.4 \text{ k}\Omega$. It is designed for applications where a 455 kHz ceramic filter is used and no external output matching is necessary since the filter requires a $1.4 \text{ k}\Omega$ source and load impedance.

For 10.7 MHz ceramic filter applications, an external 430Ω resistor must be added in parallel to provide the equivalent load impedance of 330Ω that is required by the filter; however, no external matching is necessary at the input since the mixer output matches the 330Ω source impedance of the filter. For 455 kHz applications, an external $1.1 \text{ k}\Omega$ resistor must be added in series with the mixer output to obtain the required matching impedance of $1.4 \text{ k}\Omega$ of the filter input resistance. Overall RSSI linearity is dependent on having total midband attenuation of 12 dB (6.0 dB insertion loss plus 6.0 dB impedance matching loss) for the filter. The output of the IF amplifier is buffered and the impedance is 290Ω .

Limiter

The limiter section is similar to the IF amplifier section except that four stages are used with the last three contributing to the RSSI. The fixed internal input impedance is $1.4 \text{ k}\Omega$. The total gain of the limiting amplifier section is approximately 55 dB. This IF limiting amplifier section internally drives the quadrature detector section.

Figure 9. Mixer Gain versus IF Frequency

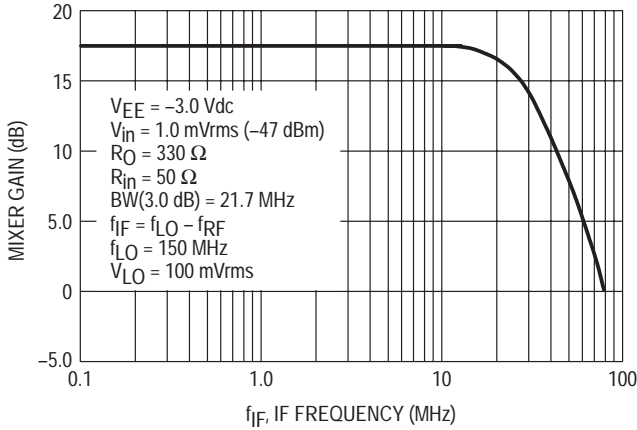


Figure 10. Mixer IF Output Level versus Local Oscillator Input Level

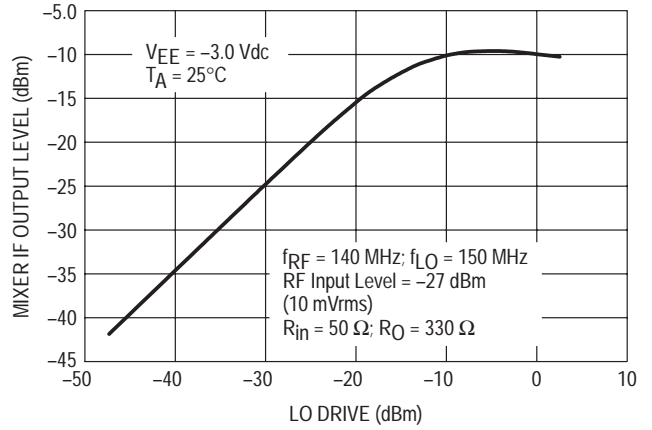


Figure 11. RSSI Output Current versus Supply Voltage and RF Input Signal Level

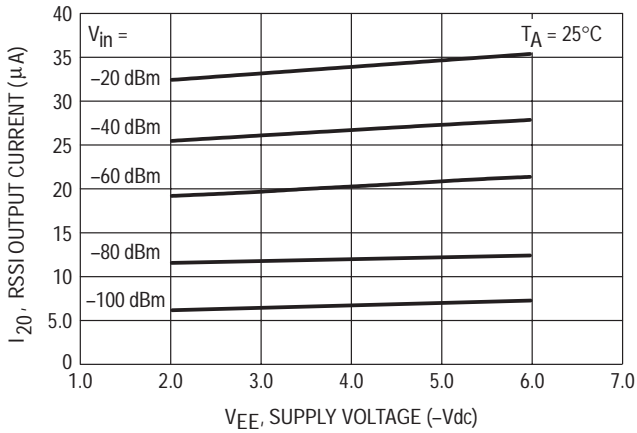


Figure 12. IF Amplifier Gain versus IF Frequency

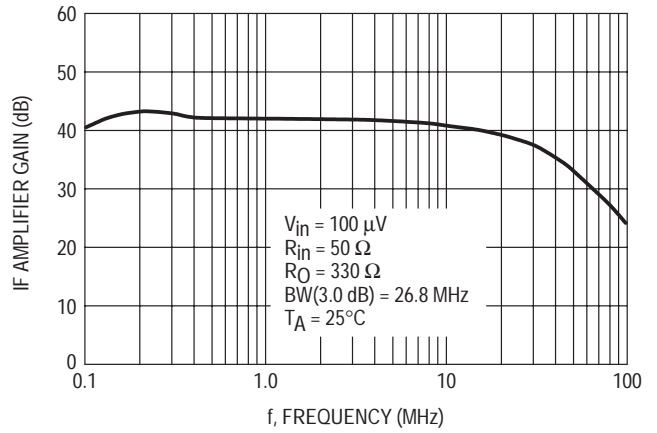
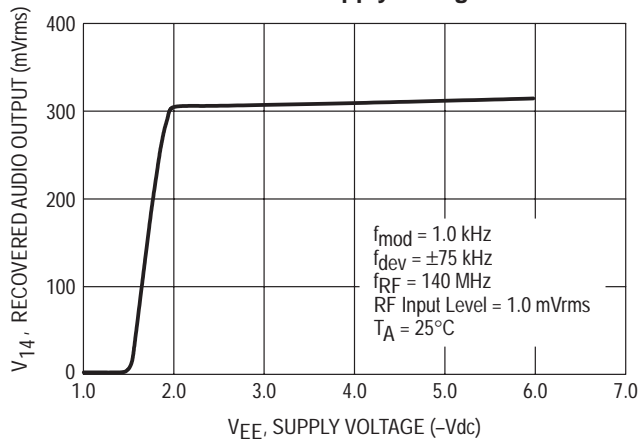


Figure 13. Recovered Audio Output Voltage versus Supply Voltage



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Quadrature Detector

The quadrature detector is a doubly balanced four quadrant multiplier with an internal 5.0 pF quadrature capacitor to couple the IF signal to the external parallel RLC resonant circuit that provides the 90 degree phase shift and drives the quadrature detector. A single pin (Pin 13) provides for the external LC parallel resonant network and the internal connection to the quadrature detector.

The bandwidth of the detector allows for recovery of relatively high data rate modulation. The recovered signal is converted from differential to single ended through a push-pull NPN/PNP output stage. Variation in recovered audio output voltage with supply voltage is very small (see Figure 13). The output drive capability is approximately $\pm 9.0 \mu\text{A}$ for a frequency deviation of $\pm 75 \text{ kHz}$ and 1.0 kHz modulating frequency (see Application Circuit).

Data Slicer

The data slicer input (Pin 15) is self centering around 1.1 V with clamping occurring at $1.1 \pm 0.5 V_{\text{be}}$ Vdc. It is designed to square up the data signal. Figure 14 shows a detailed schematic of the data slicer.

The Voltage Regulator sets up 1.1 Vdc on the base of Q12, the Differential Input Amplifier. There is a potential of $1.0 V_{\text{be}}$ on the base-collector of transistor diode Q11 and $2.0 V_{\text{be}}$ on the base-collector of Q10. This sets up a $1.5 V_{\text{be}}$ ($\sim 1.1 \text{ Vdc}$) on the node between the 36 k Ω resistors which is connected to the base of Q12. The differential output of the data slicer Q12 and Q13 is converted to a single-ended output by the Driver Circuit. Additional circuitry, not shown in Figure 14, tends to keep the data slicer input centered at 1.1 Vdc as input signal levels vary.

The Input Diode Clamp Circuit provides the clamping at $1.0 V_{\text{be}}$ (0.75 Vdc) and $2.0 V_{\text{be}}$ (1.45 Vdc). Transistor diodes Q7 and Q8 are on, thus, providing a $2.0 V_{\text{be}}$ potential at the base of Q1. Also, the voltage regulator circuit provides a potential of $2.0 V_{\text{be}}$ on the base of Q3 and $1.0 V_{\text{be}}$ on the emitter of Q3 and Q2. When the data slicer input (Pin 15) is

pulled up, Q1 turns off; Q2 turns on, thereby clamping the input at $2.0 V_{\text{be}}$. On the other hand, when Pin 15 is pulled down, Q1 turns on; Q2 turns off, thereby clamping the input at $1.0 V_{\text{be}}$.

The recovered data signal from the quadrature detector is ac coupled to the data slicer via an input coupling capacitor. The size of this capacitor and the nature of the data signal determine how faithfully the data slicer shapes up the recovered signal. The time constant is short for large peak to peak voltage swings or when there is a change in dc level at the detector output. For small signal or for continuous bits of the same polarity which drift close to the threshold voltage, the time constant is longer. When centered there is no input current allowed, which is to say, that the input looks high in impedance.

Another unique feature of the data slicer is that it responds to various logic levels applied to the Data Slicer Hold Control pin (Pin 18). Figure 15 illustrates how the input and output currents under "no hold" condition relate to the input voltage. Figure 16 shows how the input current and input voltage relate for both the "no hold" and "hold" condition.

The hold control (Pin18) does three separate tasks:

- 1) With Pin 18 at $1.0 V_{\text{be}}$ or greater, the output is shut off (sets high). Q19 turns on which shunts the base drive from Q20, thereby turning the output off.
- 2) With Pin 18 at $2.0 V_{\text{be}}$ or greater, internal clamping diodes are open circuited and the comparator input is shut off and effectively open circuited. This is accomplished by turning off the current source to emitters of the input differential amplifier, thus, the input differential amplifier is shut off.
- 3) When the input is shut off, it allows the input capacitor to hold its charge during transmit to improve recovery at the beginning of the next receive period. When it is turned on, it allows for very fast charging of the input capacitor for quick recovery of new tuning or data average. The above features are very desirable in a TDD digital FM system.

Figure 14. Data Slicer Circuit

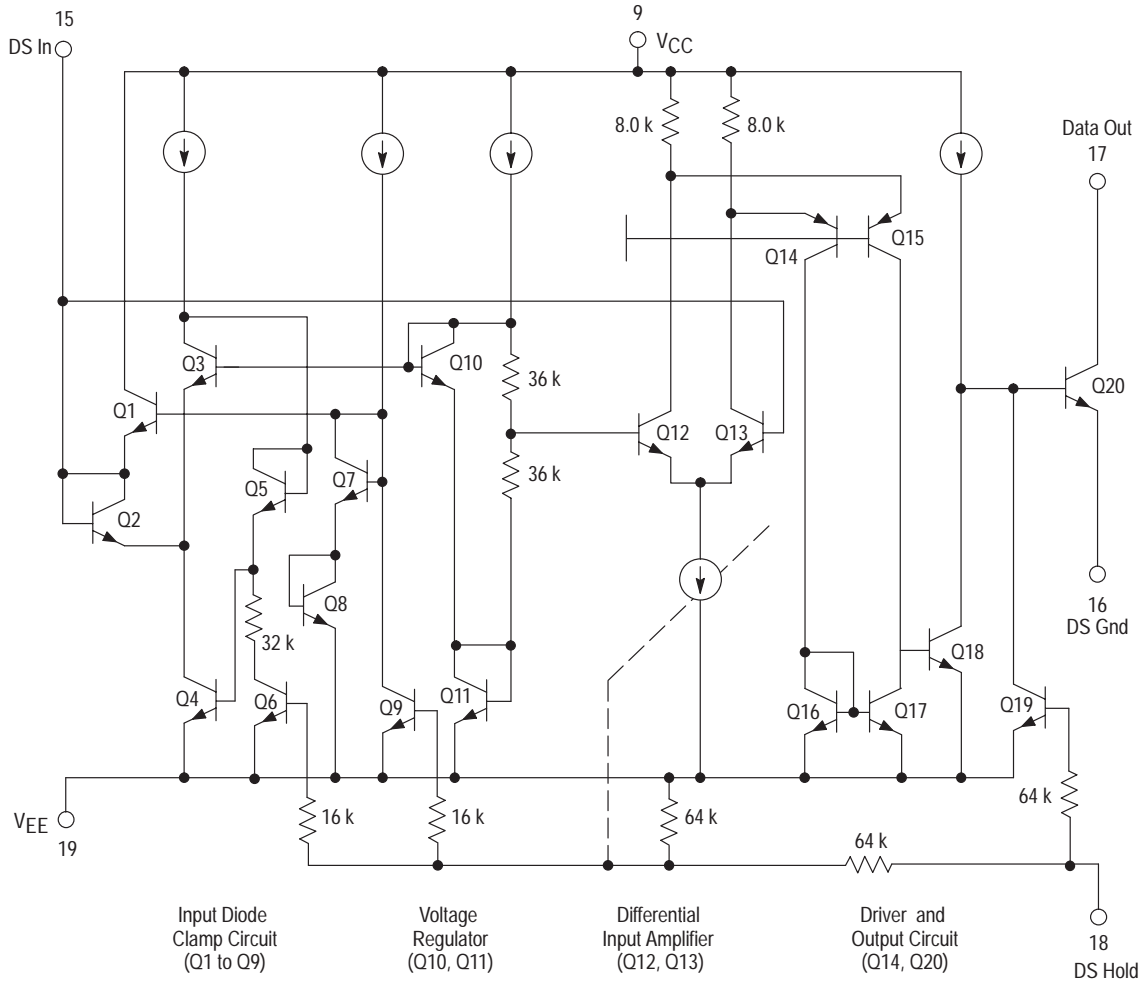


Figure 15. Data Slicer Input/Output Currents versus Input Voltage

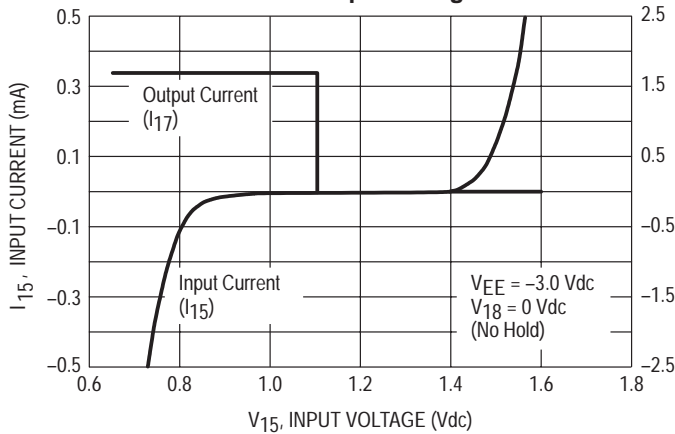
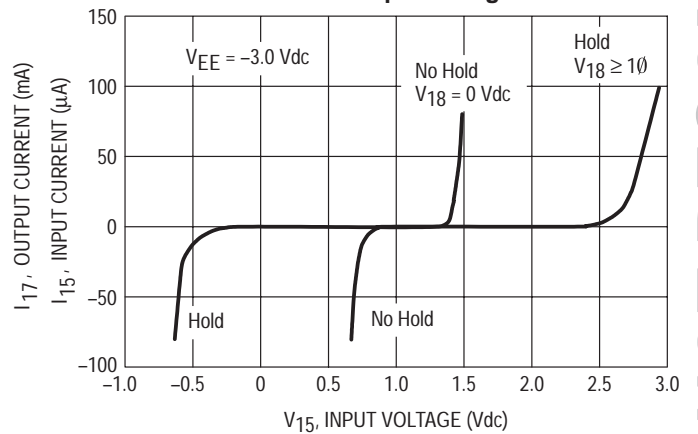


Figure 16. Data Slicer Input Current versus Input Voltage



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Figure 18. MC13156DW Circuit Side Component Placement

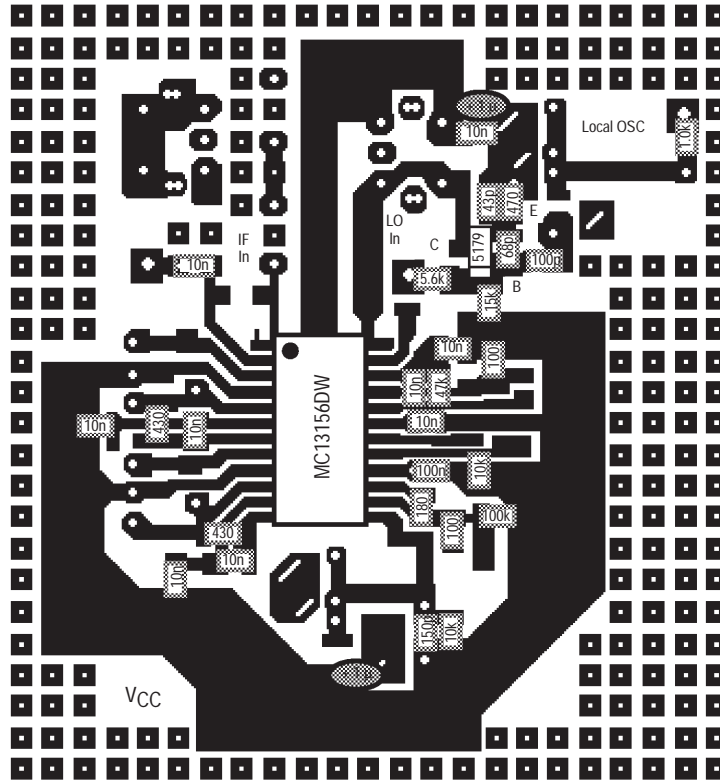
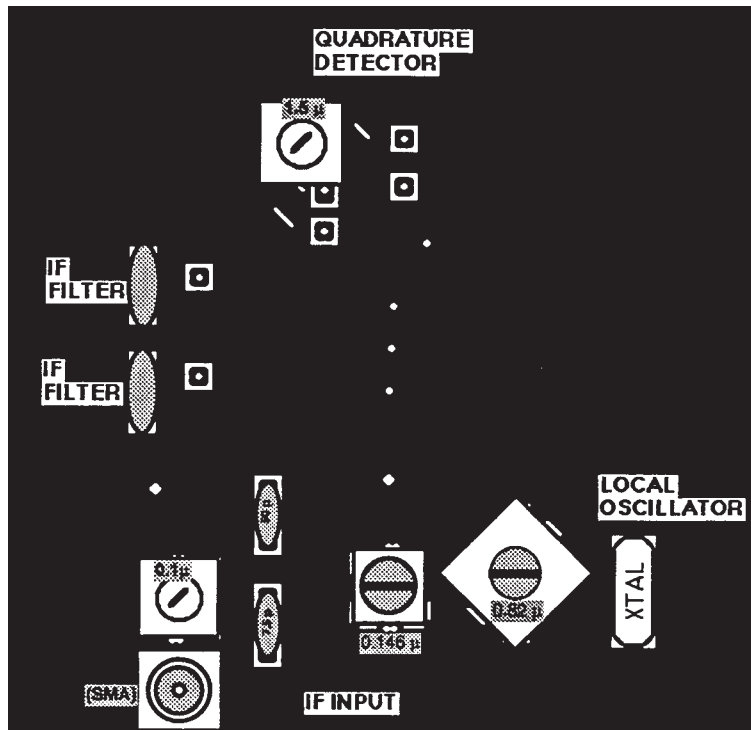


Figure 19. MC13156DW Ground Side Component Placement



Component Selection

The evaluation PC board is designed to accommodate specific components, while also being versatile enough to use components from various manufacturers and coil types. Figures 18 and 19 show the placement for the components specified in the application circuit (Figure 17). The applications circuit schematic specifies particular components that were used to achieve the results shown in the typical curves and tables but equivalent components should give similar results.

Input Matching Networks/Components

The input matching circuit shown in the application circuit schematic is passive high pass network which offers effective image rejection when the local oscillator is below the RF input frequency. Silver mica capacitors are used for their high Q and tight tolerance. The PC board is not dedicated to any particular input matching network topology; space is provided for the designer to breadboard as desired.

Alternate matching networks using 4:1 surface mount transformers or BALUNs provide satisfactory performance. The 12 dB SINAD sensitivity using the above matching networks is typically -100 dBm for $f_{\text{mod}} = 1.0$ kHz and $f_{\text{dev}} = \pm 75$ kHz at $f_{\text{IN}} = 144.45$ MHz and $f_{\text{OSC}} = 133.75$ MHz (see Figure 25).

It is desirable to use a SAW filter before the mixer to provide additional selectivity and adjacent channel rejection and improved sensitivity. The SAW filter should be designed to interface with the mixer input impedance of approximately 1.0 k Ω . Table 1 displays the series equivalent single-ended mixer input impedance.

Local Oscillators

VHF Applications – The local oscillator circuit shown in the application schematic utilizes a third overtone crystal and an RF transistor. Selecting a transistor having good phase noise performance is important; a mandatory criteria is for the

device to have good linearity of beta over several decades of collector current. In other words, if the low current beta is suppressed, it will not offer good 1/f noise performance. A third overtone series resonant crystal having at least 25 ppm tolerance over the operating temperature is recommended. The local oscillator is an impedance inversion third overtone Colpitts network and harmonic generator. In this circuit a 560 to 1.0 k Ω resistor shunts the crystal to ensure that it operates in its overtone mode; thus, a blocking capacitor is needed to eliminate the dc path to ground. The resulting parallel LC network should “free-run” near the crystal frequency if a short to ground is placed across the crystal. To provide sufficient output loading at the collector, a high Q variable inductor is used that is tuned to self resonate at the 3rd harmonic of the overtone crystal frequency.

The on-chip grounded collector transistor may be used for HF and VHF local oscillator with higher order overtone crystals. Figure 20 shows a 5th overtone oscillator at 93.3 MHz and Figure 21 shows a 7th overtone oscillator at 148.3 MHz. Both circuits use a Butler overtone oscillator configuration. The amplifier is an emitter follower. The crystal is driven from the emitter and is coupled to the high impedance base through a capacitive tap network. Operation at the desired overtone frequency is ensured by the parallel resonant circuit formed by the variable inductor and the tap capacitors and parasitic capacitances of the on-chip transistor and PC board. The variable inductor specified in the schematic could be replaced with a high tolerance, high Q ceramic or air wound surface mount component if the other components have good tolerances. A variable inductor provides an adjustment for gain and frequency of the resonant tank ensuring lock up and startup of the crystal oscillator. The overtone crystal is chosen with ESR of typically 80 Ω and 120 Ω maximum; if the resistive loss in the crystal is too high, the performance of the oscillator may be impacted by lower gain margins.

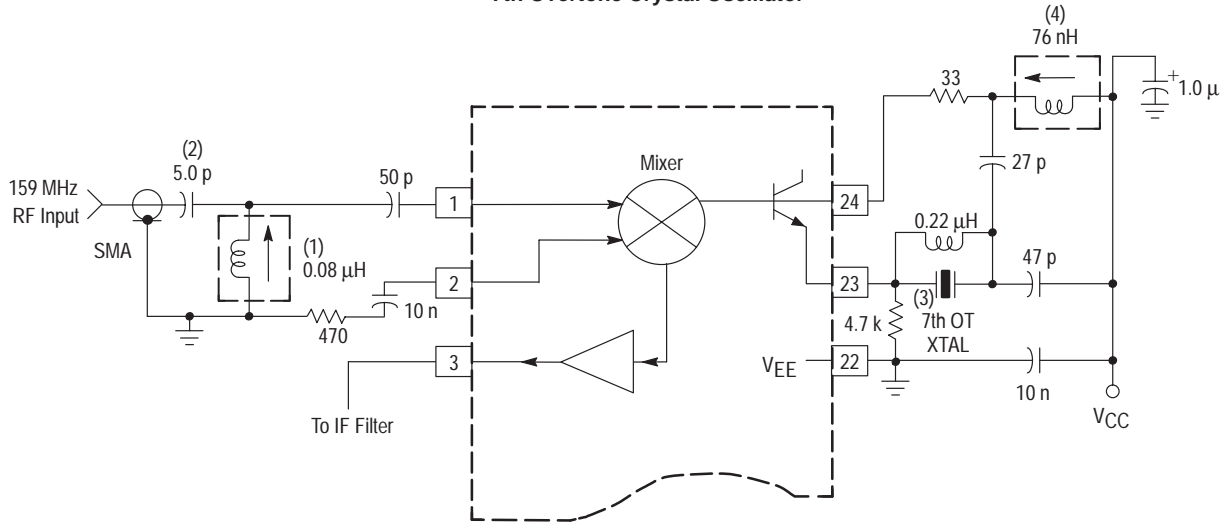
Table 1. Mixer Input Impedance Data

(Single-ended configuration, $V_{\text{CC}} = 3.0$ Vdc, local oscillator drive = 100 mVrms)

Frequency (MHz)	Series Equivalent Complex Impedance ($R + jX$) (Ω)	Parallel Resistance R_p (Ω)	Parallel Capacitance C_p (pF)
90	190 – j380	950	4.7
100	160 – j360	970	4.4
110	130 – j340	1020	4.2
120	110 – j320	1040	4.2
130	97 – j300	1030	4.0
140	82 – j280	1040	4.0
150	71 – j270	1100	4.0
160	59 – j260	1200	3.9
170	52 – j240	1160	3.9
180	44 – j230	1250	3.8
190	38 – j220	1300	3.8

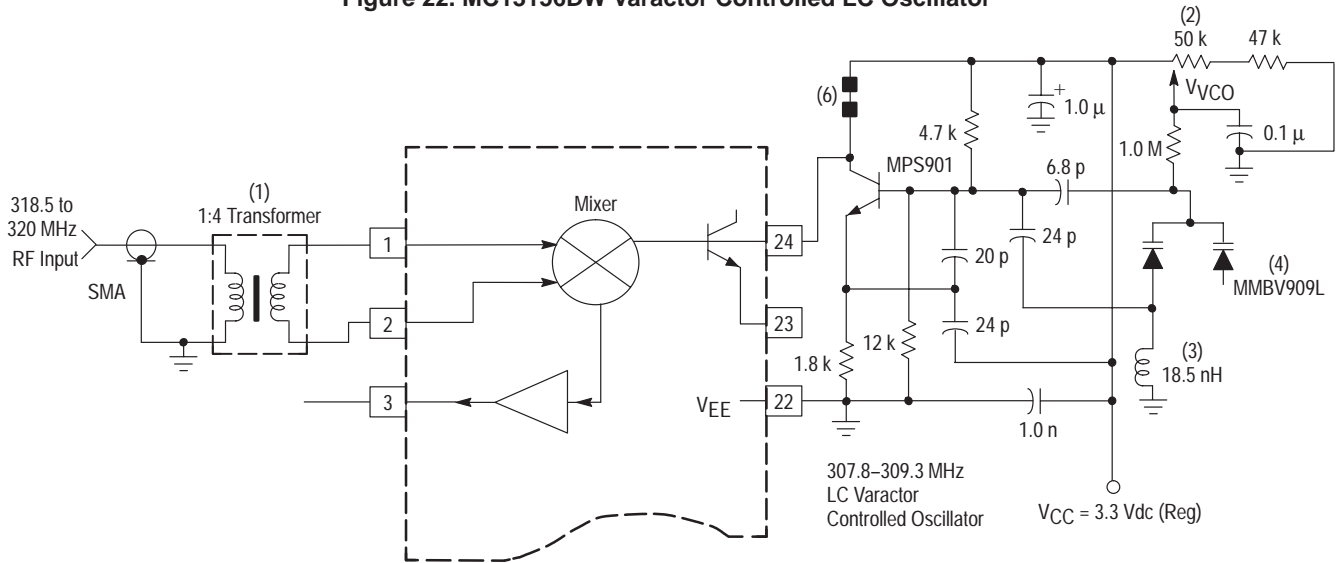
MC13156

Figure 21. MC13156DW Application Circuit
 $f_{RF} = 159 \text{ MHz}$; $f_{LO} = 148.30 \text{ MHz}$
 7th Overtone Crystal Oscillator



- NOTES:**
- 0.08 μH Variable Shielded Inductor: Toko part # 292SNS-T1365Z or equivalent.
 - Capacitors are Silver Mica.
 - 7th Overtone, Series Resonant, 25 PPM Crystal at 148.300 MHz.
 - 76 nH Variable Shielded Inductor: Coilcraft part # 150-03J08S or equivalent.

Figure 22. MC13156DW Varactor Controlled LC Oscillator



- NOTES:**
- 1:4 Impedance Transformer: Mini-Circuits.
 - 50 k Potentiometer, 10 turns.
 - Spring Coil; Coilcraft A05T.
 - Dual Varactor in SOT-23 Package.
 - All other components are surface mount components.
 - Ferrite beads through loop of 24 AWG wire.

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45 MHz Narrowband Receiver

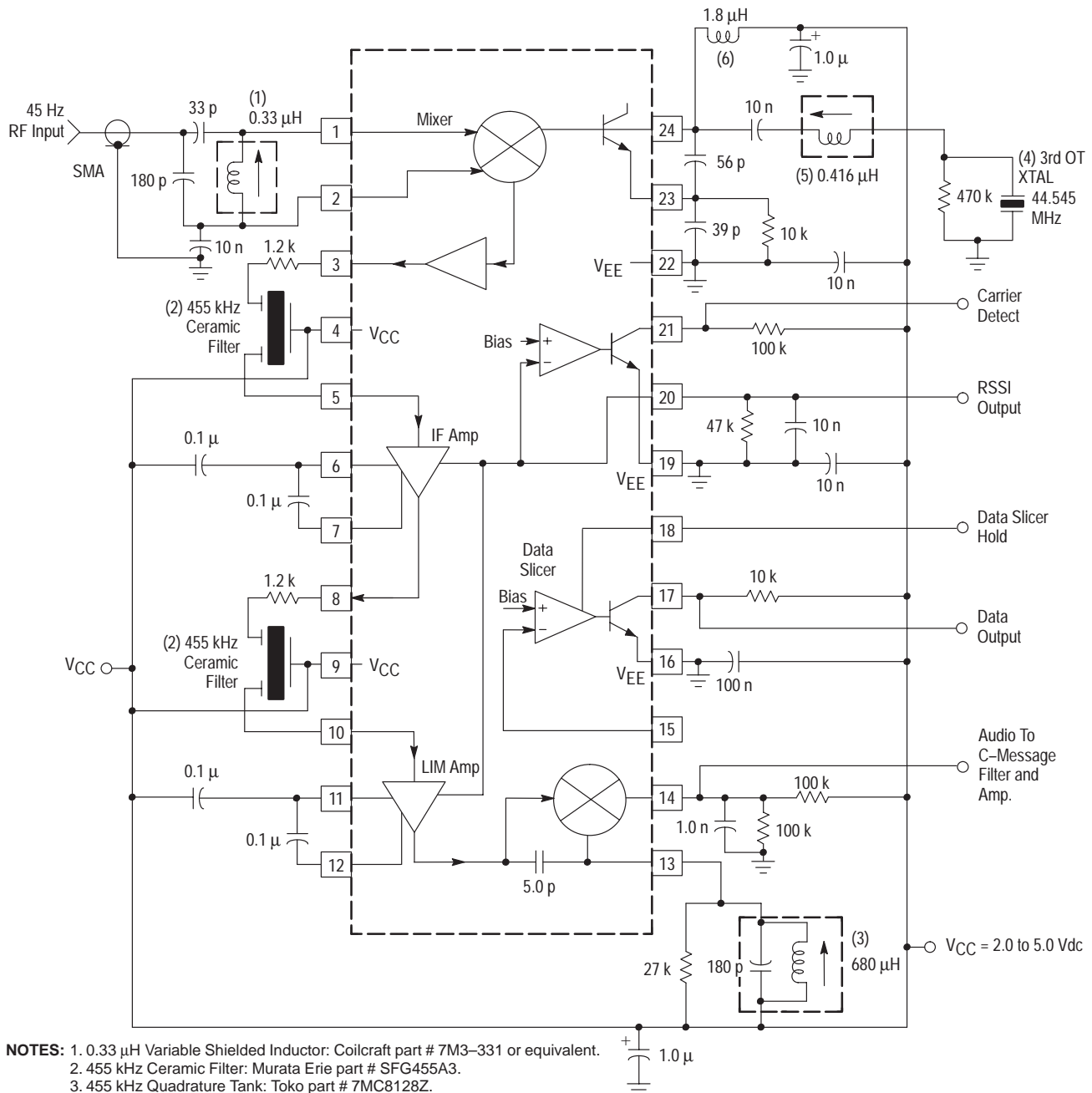
The above application examples utilize a 10.7 MHz IF. In this section a narrowband receiver with a 455 kHz IF will be described. Figure 23 shows a full schematic of a 45 MHz receiver that uses a 3rd overtone crystal with the on-chip oscillator transistor. The oscillator configuration is similar to the one used in Figure 17; it is called an impedance inversion Colpitts. A 44.545 MHz 3rd overtone, series resonant crystal is used to achieve an IF frequency at 455 kHz. The ceramic IF filters selected are Murata Erie part # SFG455A3. 1.2 kΩ chip resistors are used in series with the filters to achieve the terminating resistance of 1.4 kΩ to the filter. The IF decoupling is very important; 0.1 μF chip capacitors are used at Pins 6, 7, 11 and 12. The quadrature detector tank circuit uses a 455 kHz quadrature tank from Toko.

The 12 dB SINAD performance is -109 dBm for a $f_{mod} = 1.0$ kHz and a $f_{dev} = \pm 4.0$ kHz. The RSSI dynamic range is approximately 80 dB of linear range (see Figure 24).

Receiver Design Considerations

The curves of signal levels at various portions of the application receiver with respect to RF input level are shown in Figure 28. This information helps determine the network topology and gain blocks required ahead of the MC13156 to achieve the desired sensitivity and dynamic range of the receiver system. In the application circuit the input third order intercept (IP3) performance of the system is approximately -25 dBm (see Figure 29).

Figure 23. MC13156DW Application Circuit at 45 MHz



- NOTES:** 1. 0.33 μH Variable Shielded Inductor: Coilcraft part # 7M3-331 or equivalent.
 2. 455 kHz Ceramic Filter: Murata Erie part # SFG455A3.
 3. 455 kHz Quadrature Tank: Toko part # 7MC8128Z.
 4. 3rd Overtone, Series Resonant, 25 PPM Crystal at 44.540 MHz.
 5. 0.416 μH Variable Shielded Inductor: Coilcraft part # 143-10J12S.
 6. 1.8 μH Molded Inductor.

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Figure 24. RSSI Output Voltage versus Input Signal Level

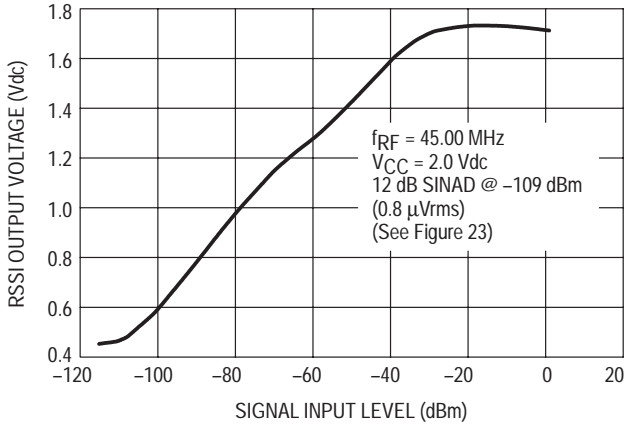


Figure 25. S + N versus RF Input Signal Level

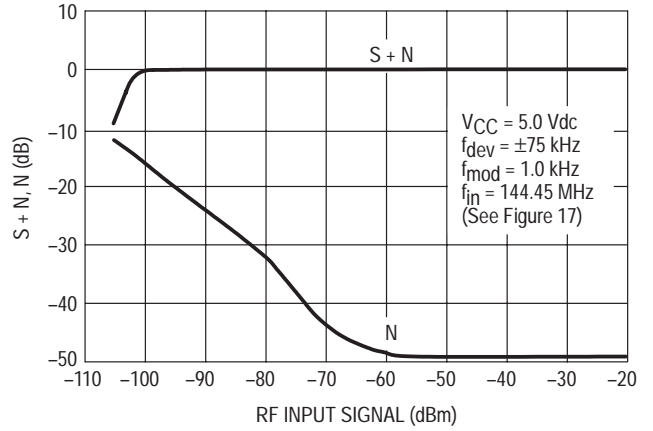


Figure 26. RSSI Output Voltage versus Input Signal Level

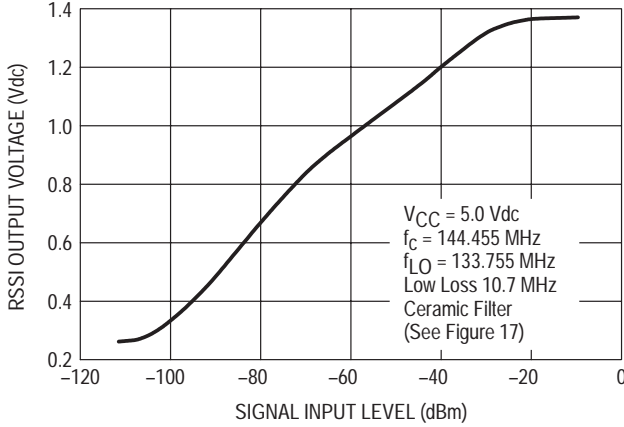


Figure 27. RSSI Output Rise and Fall Times versus RF Input Signal Level

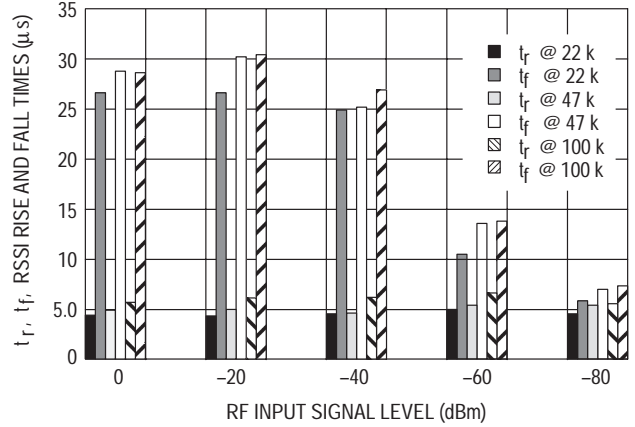


Figure 28. Signal Levels versus RF Input Signal Level

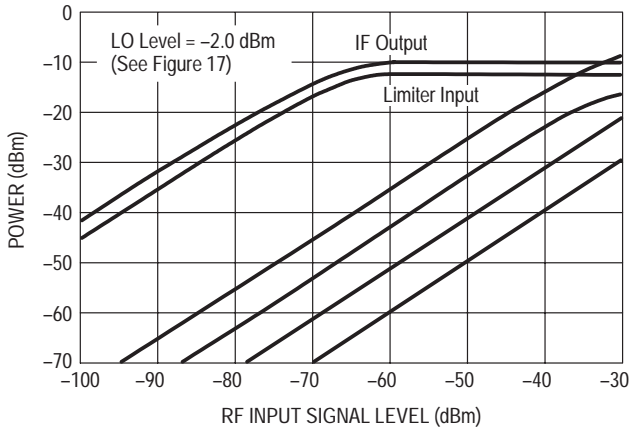
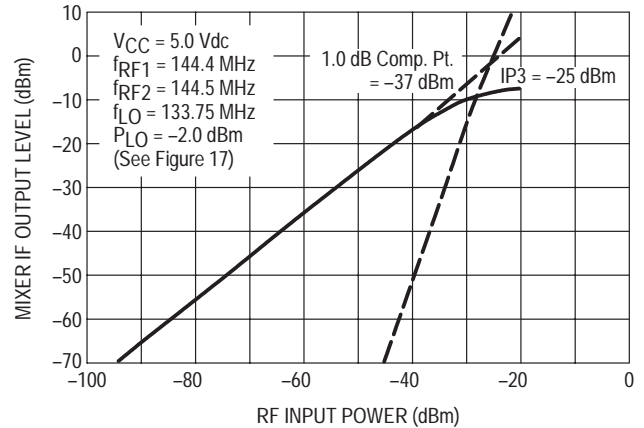


Figure 29. 1.0 dB Compression Pt. and Input Third Order Intercept Pt. versus Input Power



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MC13156

BER TESTING AND PERFORMANCE

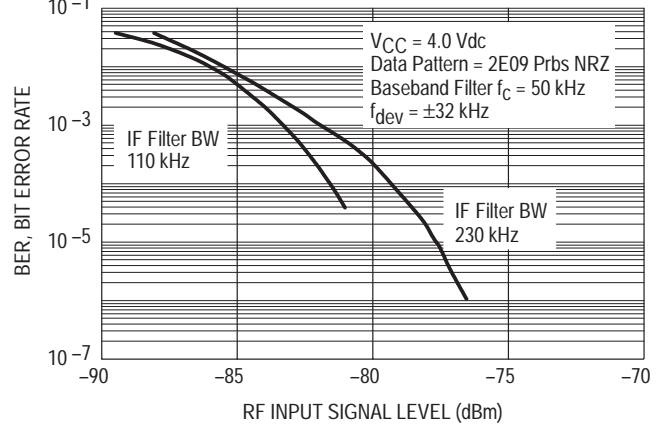
Description

The test setup shown in Figure 31 is configured so that the function generator supplies a 100 kHz clock source to the bit error rate tester. This device generates and receives a repeating data pattern and drives a 5 pole baseband data filter. The filter effectively reduces harmonic content of the baseband data which is used to modulate the RF generator which is running at 144.45 MHz. Following processing of the signal by the receiver (MC13156), the recovered baseband sinewave (data) is AC coupled to the data slicer. The data slicer is essentially an auto-threshold comparator which tracks the zero crossing of the incoming sinewave and provides logic level data at its output. Data errors associated with the recovered data are collected by the bit error rate receiver and displayed.

Bit error rate versus RF signal input level and IF filter bandwidth are shown in Figure 30. The bit error rate data was taken under the following test conditions:

- Data rate = 100 kbps
- Filter cutoff frequency set to 39% of the data rate or 39 kHz.
- Filter type is a 5 pole equal-ripple with 0.5° phase error.
- $V_{CC} = 4.0$ Vdc
- Frequency deviation = ± 32 kHz.

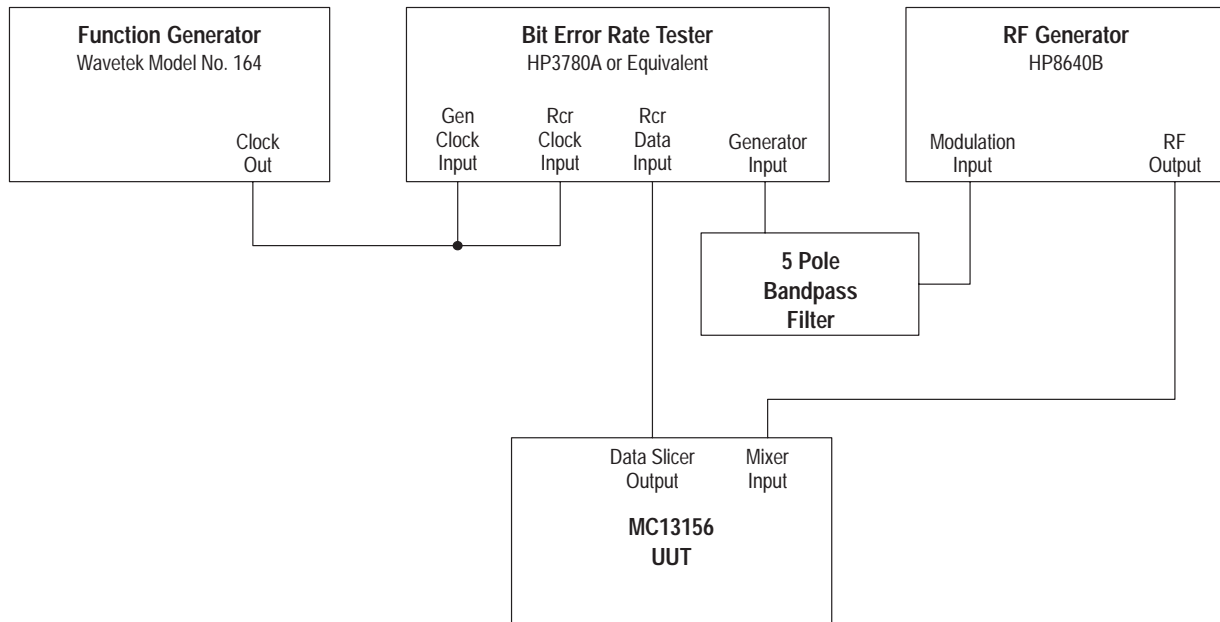
Figure 30. Bit Error Rate versus RF Input Signal Level and IF Bandpass Filter



Evaluation PC Board

The evaluation PCB is very versatile and is intended to be used across the entire useful frequency range of this device. The center section of the board provides an area for attaching all SMT components to the circuit side and radial leaded components to the component ground side (see Figures 32 and 33). Additionally, the peripheral area surrounding the RF core provides pads to add supporting and interface circuitry as a particular application dictates.

Figure 31. Bit Error Rate Test Setup



MC13156

Figure 32. Circuit Side View

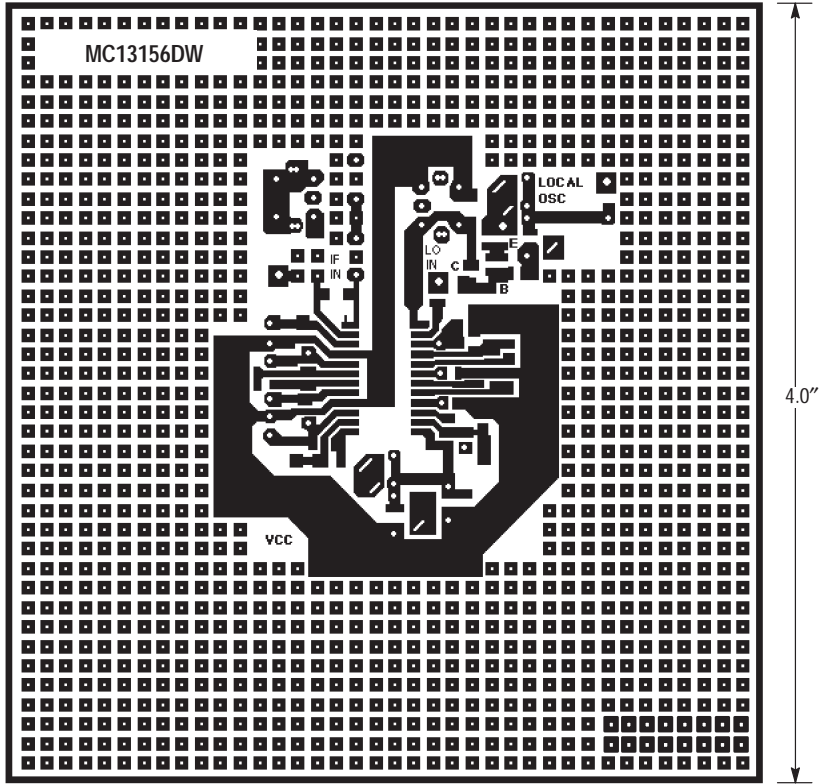
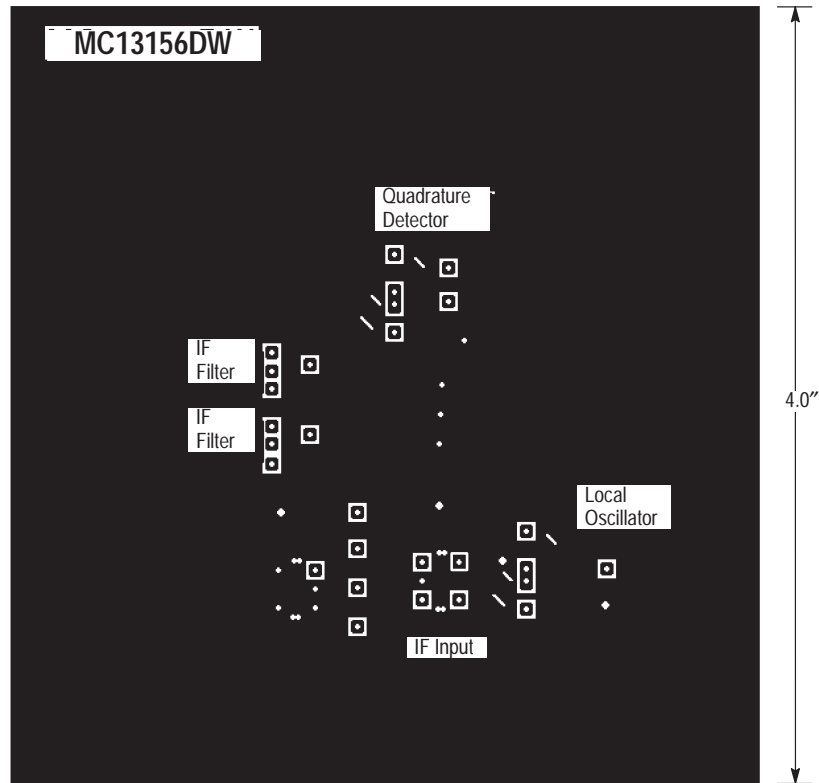


Figure 33. Ground Side View



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Wideband FM IF Subsystem

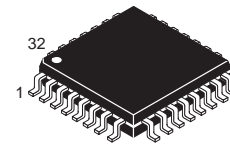
The MC13158 is a wideband IF subsystem that is designed for high performance data and analog applications. Excellent high frequency performance is achieved, with low cost, through the use of Motorola's MOSAIC 1.5™ RF bipolar process. The MC13158 has an on-board grounded collector VCO transistor that may be used with a fundamental or overtone crystal in single channel operation or with a PLL in multi-channel operation. The mixer is useful to 500 MHz and may be used in a balanced differential or single ended configuration. The IF amplifier is split to accommodate two low cost cascaded filters. RSSI output is derived by summing the output of both IF sections. A precision data shaper has an Off function to shut the output off to save current. An enable control is provided to power down the IC for power management in battery operated applications.

Applications include DECT, wideband wireless data links for personal and portable laptop computers and other battery operated radio systems which utilize GFSK, FSK or FM modulation.

- Designed for DECT Applications
- 1.8 to 6.0 Vdc Operating Voltage
- Low Power Consumption in Active and Standby Mode
- Greater than 600 kHz Detector Bandwidth
- Data Slicer with Special Off Function
- Enable Function for Power Down of Battery Operated Systems
- RSSI Dynamic Range of 80 dB Minimum
- Low External Component Count

WIDEBAND FM IF SUBSYSTEM FOR DECT AND DIGITAL APPLICATIONS

SEMICONDUCTOR TECHNICAL DATA

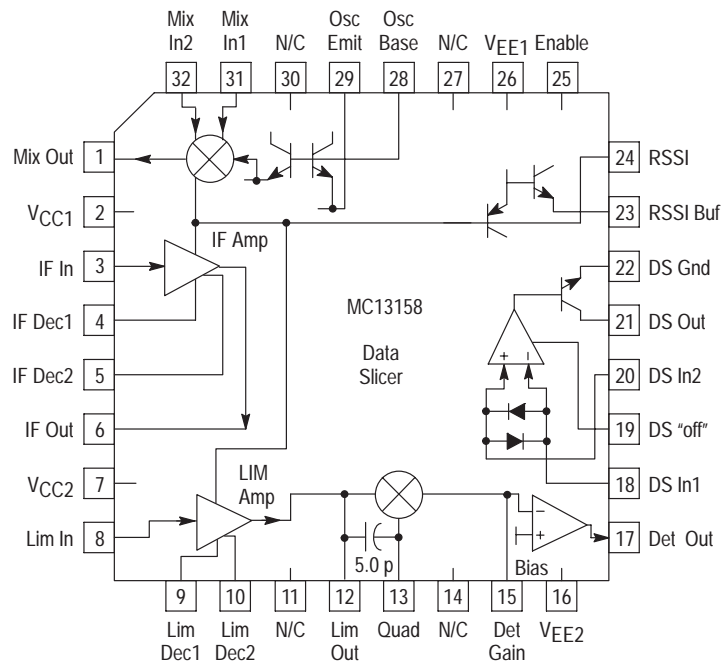


FTB SUFFIX
PLASTIC PACKAGE
CASE 873
(Thin QFP)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13158FTB	T _A = -40 to +85°C	TQFP-32

Representative Block Diagram



This device contains 234 active transistors.

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MAXIMUM RATINGS

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage	16, 26	$V_{S(max)}$	6.5	Vdc
Junction Temperature		T_{JMAX}	+150	°C
Storage Temperature Range		T_{stg}	-65 to +150	°C

NOTE: 1. Devices should not be operated at or outside these values. The "Recommended Operating Conditions" provide for actual device operation.

RECOMMENDED OPERATING CONDITIONS ($V_{CC} = V_2 = V_7$; $V_{EE} = V_{16} = V_{22} = V_{26}$; $V_S = V_{CC} - V_{EE}$)

Rating	Pin	Symbol	Value	Unit
Power Supply Voltage $T_A = 25^\circ\text{C}$ $-40^\circ\text{C} \leq T_A \leq 85^\circ\text{C}$	2, 7 16, 26	V_S	2.0 to 6.0	Vdc
Input Frequency	31, 32	F_{in}	10 to 500	MHz
Ambient Temperature Range		T_A	-40 to +85	°C
Input Signal Level	31, 32	V_{in}	200	mVrms

DC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$; $V_S = 3.0\text{ Vdc}$; No Input Signal; See Figure 1.)

Characteristic	Condition	Pin	Symbol	Min	Typ	Max	Unit
Total Drain Current	$V_S = 2.0\text{ Vdc}$ $V_S = 3.0\text{ Vdc}$ $V_S = 6.0\text{ Vdc}$ See Figure 2	16, 26	I_{TOTAL}	2.5 3.5 3.5	5.5 5.7 6.0	8.5 8.5 9.5	mA

DATA SLICER (Input Voltage Referenced to V_{EE} ; $V_S = 3.0\text{ Vdc}$; No Input Signal)

Output Current; $V_{18}\text{ LO}$; Data Slicer Enabled (DS "on")	$V_{19} = V_{EE}$ $V_{18} < V_{20}$ $V_{20} = V_S/2$ See Figure 3	21	I_{21}	2.0	5.9	–	mA
Output Current; $V_{18}\text{ HI}$; Data Slicer Enabled (DS "on")	$V_{19} = V_{EE}$ $V_{18} > V_{20}$ $V_{20} = V_S/2$ See Figure 4	21	I_{21}	–	0.1	1.0	μA
Output Current; Data Slicer Disabled (DS "off")	$V_{19} = V_{CC}$ $V_{20} = V_S/2$	21	I_{21}	–	0.1	1.0	μA

AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ\text{C}$; $V_S = 3.0\text{ Vdc}$; $f_{RF} = 110.7\text{ MHz}$; $f_{LO} = 100\text{ MHz}$; See Figure 1.)

Characteristic	Condition	Pin	Symbol	Min	Typ	Max	Unit
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MIXER

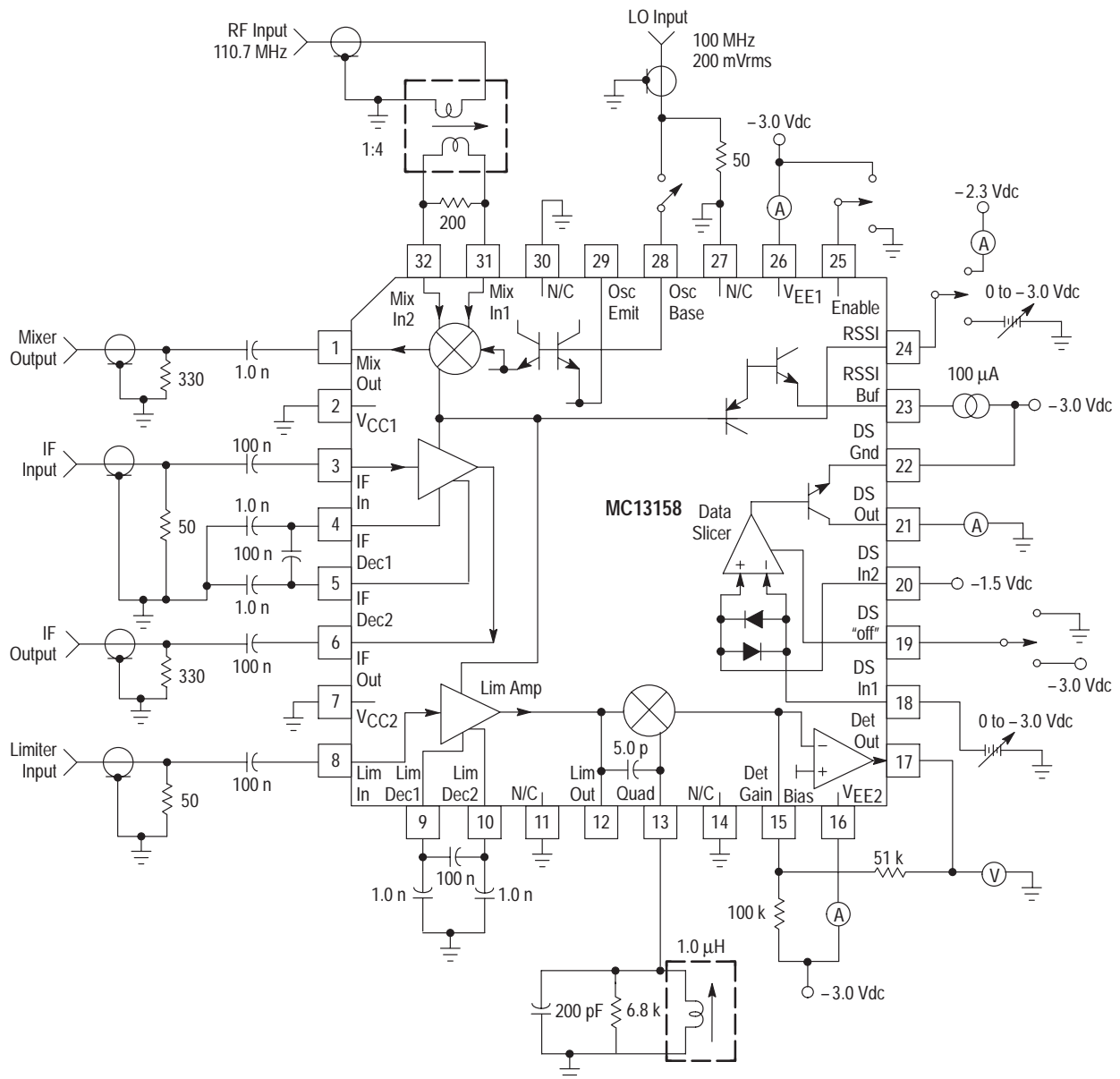
Mixer Conversion Gain	$V_{in} = 1.0\text{ mVrms}$ See Figure 5	31, 32, 1	–	–	22	–	dB
Noise Figure	Input Matched	31, 32, 1	NF	–	14	–	dB
Mixer Input Impedance	Single-Ended See Figure 15	31, 32	R_p C_p	– –	865 1.6	– –	Ω pF
Mixer Output Impedance		1	–	–	330	–	Ω

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AC ELECTRICAL CHARACTERISTICS (continued) ($T_A = 25^\circ\text{C}$; $V_S = 3.0\text{ Vdc}$; $f_{RF} = 110.7\text{ MHz}$; $f_{LO} = 100\text{ MHz}$; See Figure 1.)

Characteristic	Condition	Pin	Symbol	Min	Typ	Max	Unit
IF AMPLIFIER SECTION							
IF RSSI Slope	See Figure 8	23	–	0.15	0.3	0.4	$\mu\text{A/dB}$
IF Gain	$f = 10.7\text{ MHz}$ See Figure 7	3, 6	–	–	36	–	dB
Input Impedance		3	–	–	330	–	Ω
Output Impedance		6	–	–	330	–	Ω
LIMITING AMPLIFIER SECTION							
Limiter RSSI Slope	See Figure 9	23	–	0.15	0.3	0.4	$\mu\text{A/dB}$
Limiter Gain	$f = 10.7\text{ MHz}$	8, 12	–	–	70	–	dB
Input Impedance		8	–	–	330	–	Ω

Figure 1. Test Circuit



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Typical Performance Over Temperature

(per Figure 1)

Figure 2. Total Supply Current versus Ambient Temperature, Supply Voltage

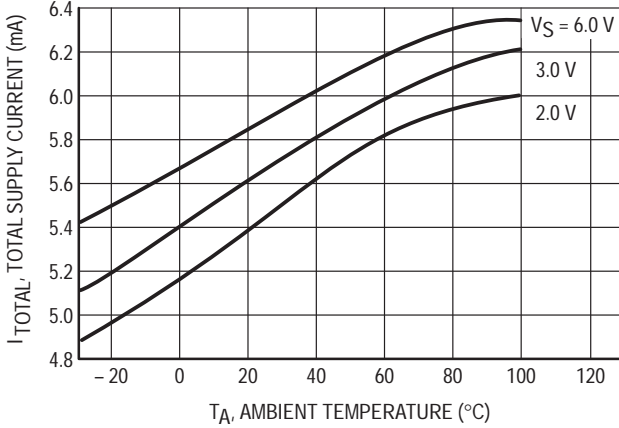


Figure 3. Data Slicer On Output Current versus Ambient Temperature

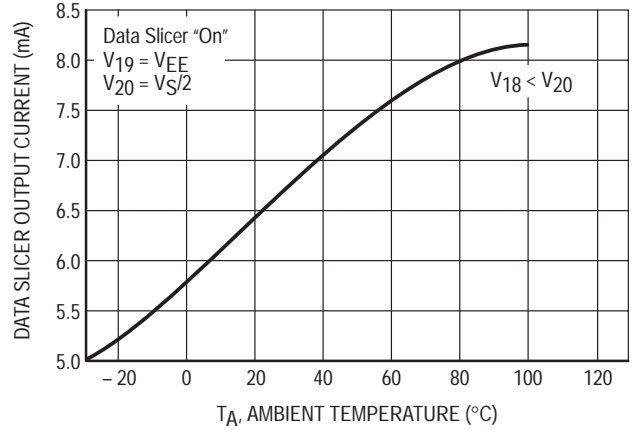


Figure 4. Data Slicer On Output Current versus Ambient Temperature

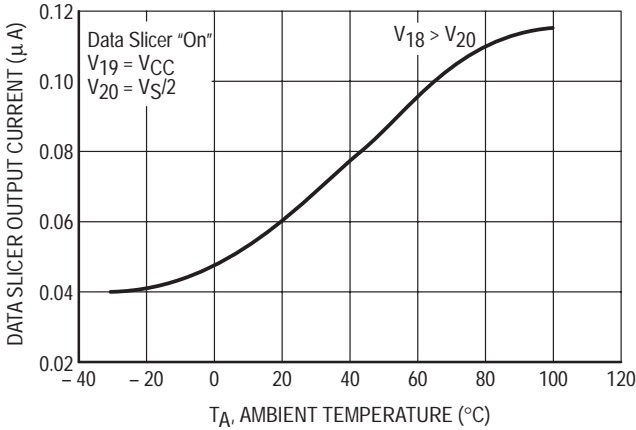


Figure 5. Normalized Mixer Gain versus Ambient Temperature

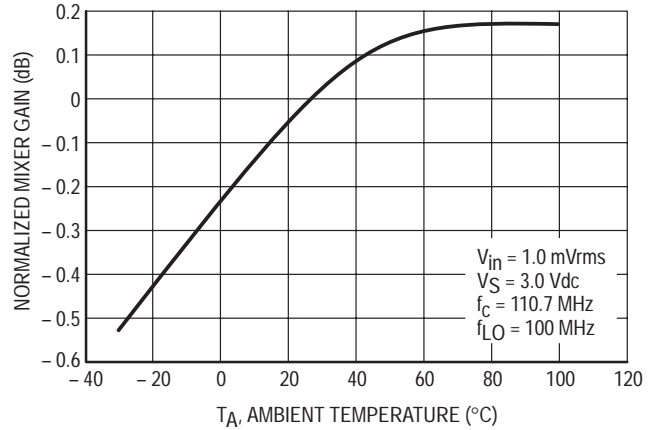


Figure 6. Mixer RSSI Output Current versus Ambient Temperature, Mixer Input Level

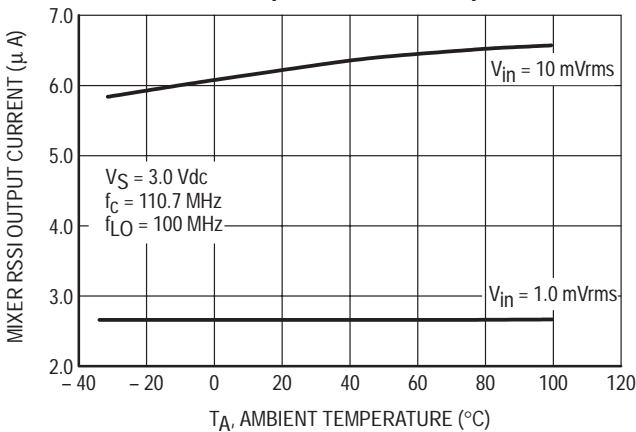
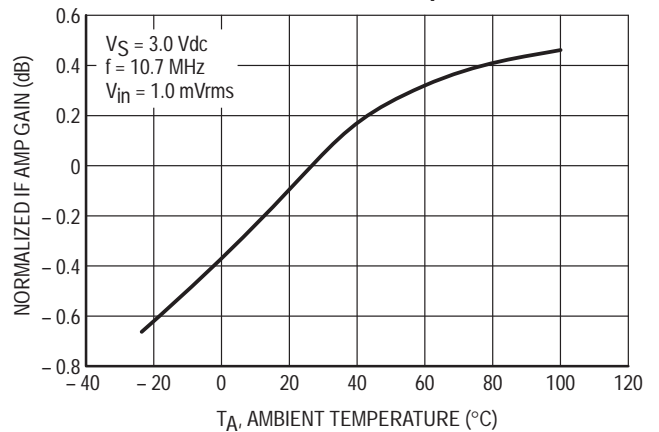


Figure 7. Normalized IF Amp Gain versus Ambient Temperature



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NOT RECOMMENDED FOR NEW DESIGNS

MC13158

tTypical Performance Over Temperature

(per Figure 1)

Figure 8. IF Amp RSSI Output Current versus Ambient Temperature, IF Input Level

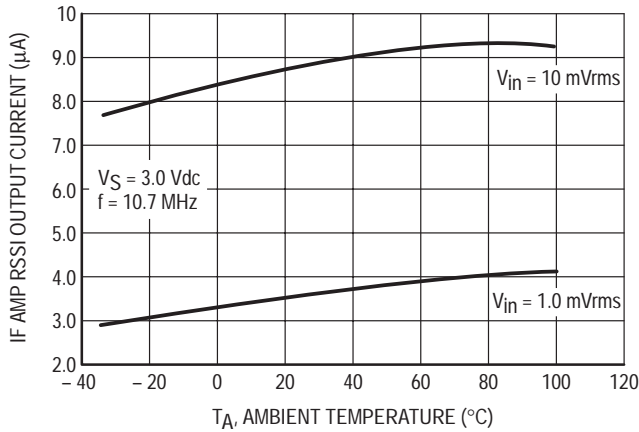


Figure 9. Limiter Amp RSSI Output Current versus Ambient Temperature, Input Signal Level

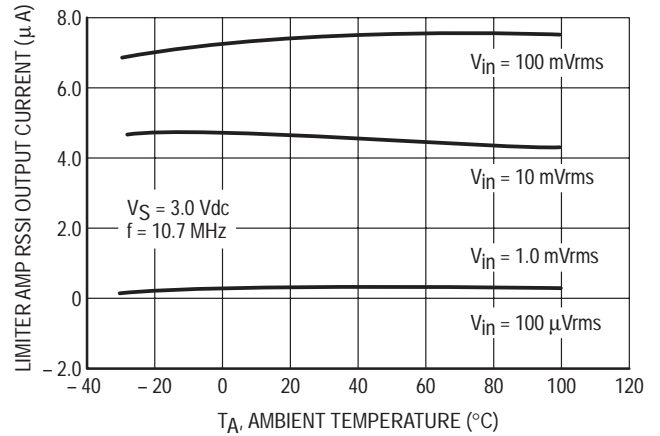


Figure 10. Total RSSI Output Current versus Ambient Temperature (No Signal)

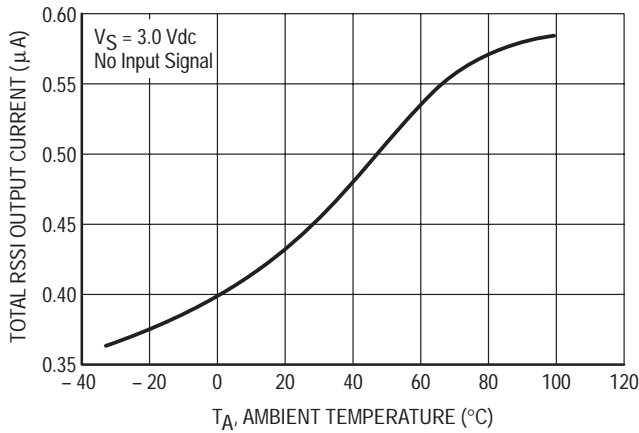
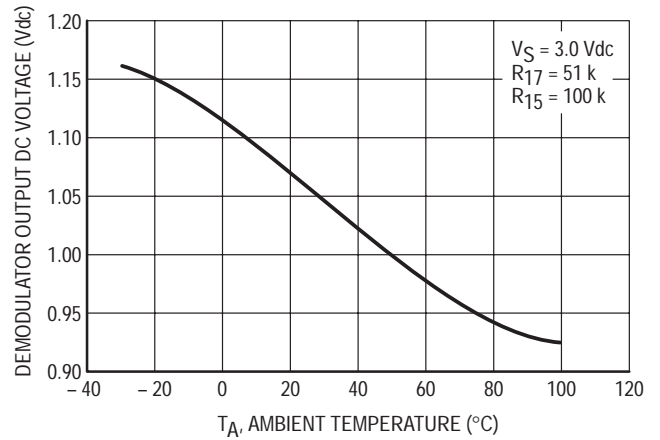


Figure 11. Demodulator DC Voltage versus Ambient Temperature



SYSTEM LEVEL AC ELECTRICAL CHARACTERISTICS ($T_A = 25^\circ C$; $V_S = 3.0$ Vdc; $f_{RF} = 112$ MHz; $f_{LO} = 122.7$ MHz)

Characteristic	Condition	Notes	Symbol	Typ	Unit
12 dB SINAD Sensitivity: Narrowband Application	$f_{RF} = 112$ MHz $f_{mod} = 1.0$ kHz $f_{dev} = \pm 125$ kHz SINAD Curve	1	—		dBm
Without Preamp	Figure 25			-101	
With Preamp	Figure 26			-113	
Third Order Intercept Point	$f_{RF1} = 112$ MHz $f_{RF2} = 112.1$ MHz $V_S = 3.5$ Vdc	2	IIP3	-32	dBm
1.0 dB Comp. Point	Figure 28		1.0 dB C.Pt.	-39	

NOTES: 1. Test Circuit & Test Set per Figure 24.
2. Test Circuit & Test Set per Figure 27.

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MC13158

CIRCUIT DESCRIPTION

General

The MC13158 is a low power single conversion wideband FM receiver incorporating a split IF. This device is designated for use as the backend in digital FM systems such as Digital European Cordless Telephone (DECT) and wideband data links with data rates up to 2.0 Mbps. It contains a mixer, oscillator, Received Signal Strength Indicator (RSSI), IF amplifier, limiting IF, quadrature detector, power down or enable function, and a data slicer with output off function. Further details are covered in the Pin Function Description which shows the equivalent internal circuit and external circuit requirements.

Current Regulation/Enable

Temperature compensating voltage independent current regulators which are controlled by the enable pin (Pin 25) where "low" powers up and "high" powers down the entire circuit.

Mixer

The mixer is a double-balanced four quadrant multiplier and is designed to work up to 500 MHz. It can be used in differential or in single ended mode by connecting the other input to the positive supply rail. The linear gain of the mixer is approximately 22 dB at 100 mVrms LO drive level. The mixer gain and noise figure have been emphasized at the expense of intermodulation performance. RSSI measurements are added in the mixer to extend the range to higher signal levels. The single-ended parallel equivalent input impedance of the mixer is $R_p \sim 1.0 \text{ k}\Omega$ and $C_p \sim 2.0 \text{ pF}$. The buffered output of the mixer is internally loaded resulting in an output impedance of 330 Ω .

Local Oscillator

The on-chip transistor operates with crystal and LC resonant elements up to 220 MHz. Series resonant, overtone crystals are used to achieve excellent local oscillator stability. Third overtone crystals are used through about 65 to 70 MHz. Operation from 70 MHz up to 180 MHz is feasible using the on-chip transistor with a 5th or 7th overtone crystal. To enhance operation using an overtone crystal, the internal transistor bias is increased by adding an external resistor from Pin 29 to V_{EE} ; however, with an external resistor the oscillator stays on during power down. Typically, -10 dBm of local oscillator drive is needed to adequately drive the mixer. With an external oscillator source, the IC can be operated up to 500 MHz.

RSSI

The received signal strength indicator (RSSI) output is a current proportional to the log of the received signal amplitude. The RSSI current output is derived by summing the currents from the mixer, IF and limiting amplifier stages. An increase in RSSI dynamic range, particularly at higher input signal levels is achieved. The RSSI circuit is designed to provide typically 85 dB of dynamic range with temperature compensation.

Linearity of the RSSI is optimized by using external ceramic bandpass filters which have an insertion loss of 4.0 dB and 330 Ω source and load impedance. For higher data rates used in DECT and related applications, LC bandpass filtering is necessary to acquire the desired

bandpass response; however, the RSSI linearity will require the same insertion loss.

RSSI Buffer

The RSSI output current creates a voltage across an external resistor. A unity voltage-gain amplifier is used to buffer this voltage. The output of this buffer has an active pull-up but no pull-down, so it can also be used as a peak detector. The negative slew rate is determined by external capacitance and resistance to the negative supply.

IF Amplifier

The first IF amplifier section is composed of three differential stages with the second and third stages contributing to the RSSI. This section has internal DC feedback and external input decoupling for improved symmetry and stability. The total gain of the IF amplifier block is approximately 40 dB at 10.7 MHz.

The fixed internal input impedance is 330 Ω . When using ceramic filters requiring source and load impedances of 330 Ω , no external matching is necessary. Overall RSSI linearity is dependent on having total midband attenuation of 10 dB (4.0 dB insertion loss plus 6.0 dB impedance matching loss) for the filter. The output of the IF amplifier is buffered and the impedance is 330 Ω .

Limiters

The limiter section is similar to the IF amplifier section except that five differential stages are used. The fixed internal input impedance is 330 Ω . The total gain of the limiting amplifier section is approximately 70 dB. This IF limiting amplifier section internally drives the quadrature detector section and it is also brought out on Pin 12.

Quadrature Detector

The quadrature detector is a doubly balanced four quadrant multiplier with an internal 5.0 pF quadrature capacitor between Pins 12 and 13. An external capacitor may be added between these pins to increase the IF signal to the external parallel RLC resonant circuit that provides the 90 degree phase shift and drives the quadrature detector. A single pin (Pin 13) provides for the external LC parallel resonant network and the internal connection to the quadrature detector.

Internal low pass filter capacitors have been selected to control the bandwidth of the detector. The recovered signal is brought out by the inverting amplifier buffer. An external feedback resistor from the output (Pin 17) to the input of the inverting amplifier (Pin 15) controls the output amplitude; it is combined with another external resistor from the input to the negative supply (Pin 16) to set the output dc level. For a resistor ratio of 1, the DC level at the detector output is $2.0 V_{BE}$ (see Figure 12). A small capacitor C_{17} across the first resistor (from Pin 17 to 15) can be used to reduce the bandwidth.

Data Slicer

The data slicer is a comparator that is designed to square up the data signal. Across the data slicer inputs (Pins 18 and 20) are back to back diodes.

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The recovered data signal from the quadrature detector can be DC coupled to the data slicer DS IN1 (Pin 18). In the application circuit shown in Figure 1 it will be centered at $2.0 V_{BE}$ and allowed to swing $\pm V_{BE}$. A capacitor is placed from DS IN2 (Pin 20) to V_{EE} . The size of this capacitor and the nature of the data signal determine how faithfully the data slicer shapes up the recovered signal. The time constant is short for large peak to peak voltage swings or when there is a change in DC level at the detector output. For small signal or for continuous bits of the same polarity which drift close to the threshold voltage, the time constant is longer.

A unique feature of the data slicer is that the inverting switching stages in the comparator are supplied through the emitter pin of the output transistor (Pin 22 – DS Gnd) to V_{EE} rather than internally to V_{EE} . This is provided in order to reduce switching feedback to the front end. A control pin is provided to shut the data slicer output off (DS “off” – Pin 19). With DS “off” pin at V_{CC} the data slicer output is shut off by shutting down the base drive to the output transistor. When a channel is being monitored to make an RSSI measurement, but not to collect data, the data output may be shut off to save current.

PIN FUNCTION DESCRIPTION

Pin	Symbol	Internal Equivalent Circuit	Description/External Circuit Requirements
1	Mix Out		<p>Mixer Output The mixer output impedance is 330 Ω; it matches to 10.7 MHz ceramic filters with 330 Ω input impedance.</p> <p>Supply Voltage (V_{CC1}) This pin is the V_{CC} pin for the Mixer, Local Oscillator, and IF Amplifier. The operating supply voltage range is from 1.8 Vdc to 5.0 Vdc. In the PCB layout, the V_{CC} trace must be kept as wide as possible to minimize inductive reactances along the trace; it is best to have it completely fill around the surface mount components and traces on the circuit side of the PCB.</p>
2	V_{CC1}		<p>IF Input The input impedance at Pin 3 is 330 Ω. It matches the 330 Ω load impedance of a 10.7 MHz ceramic filter. Thus, no external matching is required.</p> <p>IF DEC1 & DEC2 IF decoupling pins. Decoupling capacitors should be placed directly at the pins to enhance stability. Two capacitors are decoupled to the RF ground V_{CC1}; one is placed between DEC1 & DEC2.</p>
3	IF In		<p>IF Output The output impedance is 330 Ω; it matches the 330 input resistance of a 10.7 MHz ceramic filter.</p>
4	IF Dec1		
5	IF Dec2		
6	IF Out		

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PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol	Internal Equivalent Circuit	Description/External Circuit Requirements
7	V _{CC2}		<p>Supply Voltage (V_{CC2}) This pin is V_{CC} supply for the Limiter, Quadrature Detector, data slicer and RSSI buffer circuits. In the application PC board this pin is tied to a common V_{CC} trace with V_{CC1}.</p> <p>Limiter Input The limiter input impedance is 330 Ω.</p> <p>Limiter Decoupling Decoupling capacitors are placed directly at these pins and to V_{CC} (RF ground). Use the same procedure as in the IF decoupling.</p>
8	Lim In		
9	Lim Dec1		
10	Lim Dec2		
11,14, 27 & 28	N/C		<p>No Connects There is no internal connection to these pins; however it is recommended that these pins be connected externally to V_{CC} (RF ground).</p>
12	Lim Out		<p>Limiter Output The output impedance is low. The limiter drives a quadrature detector circuit with in-phase and quadrature phase signals.</p> <p>Quadrature Detector Circuit The quadrature detector is a doubly balanced four-quadrant multiplier with an internal 5.0 pF capacitor between Pins 12 and 13. An external capacitor may be added to increase the IF signal to Pin 13. The quadrature detector pin is provided to connect the external RLC parallel resonant network which provides the 90 degree phase shift and drives the quadrature detector.</p>
13	Quad		
15	Det Gain		<p>Detector Buffer Amplifier This is an inverting amplifier. An external feedback resistor from Pin 17 to 15, (the inverting input) controls the output amplitude; another resistor from Pin 15 to the negative supply (Pin 16) sets the DC output level. A 1:1 resistor ratio sets the output DC level at two V_{BE} with respect to V_{EE}. A small capacitor from Pin 17 to 15 can be used to set the bandwidth.</p> <p>Supply Ground (VEE2) In the PCB layout, the ground pins (also applies to Pin 26) should be connected directly to chassis ground. Decoupling capacitors to V_{CC} should be placed directly at the ground pins.</p>
17	Det Out		
16	VEE2		

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

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PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol	Internal Equivalent Circuit	Description/External Circuit Requirements
19	DS "off"		<p>Data Slicer Off The data output may be shut off to save current by placing DS "off" (Pin 19) at VCC.</p> <p>Data Slicer Output In the application example a 10 kΩ pull-up resistor is connected to the collector of the output transistor at Pin 21.</p> <p>Data Slicer Ground All the inverting switching stages in the comparator are supplied through the emitter pin of the output transistor (Pin 22) to ground rather than internally to VEE in order to reduce switching feedback to the front end.</p>
21	DS Out		<p>DS Out 21</p> <p>DS Gnd 22</p> <p>DS "off" 19</p>
22	DS Gnd		
18	DS In1		<p>Data Slicer Inputs The data slicer has differential inputs with back to back diodes across them. The recovered signal is DC coupled to DS IN1 (Pin 18) at nominally V_{18} with respect to VEE; thus, it will maintain $V_{18} \pm V_{BE}$ at Pin 18. DS IN2 (Pin 20) is AC coupled to VEE. The choice of coupling capacitor is dependent on the nature of the data signal. For small signal or continuous bits of the same polarity, the response time is relatively large. On the other hand, for large peak to peak voltage swings or when the DC level at the detector output changes, the response time is short. See the discussion in the application section for external circuit design details.</p>
20	DS In2		
23	RSSI Buf		<p>RSSI Buffer A unity gain amplifier is used to buffer the voltage at Pin 24 to 23. The output of the unity gain buffer (Pin 23) has an active pull up but no pull down. An external resistor is placed from Pin 23 to VEE to provide the pull down.</p> <p>RSSI The RSSI output current creates a voltage drop across an external resistor from Pin 24 to VEE. The maximum RSSI current is 26 μA; thus, the maximum RSSI voltage using a 100 kΩ resistor is approximately 2.6 Vdc. Figure 22 shows the RSSI Output Voltage versus Input Signal Level in the application circuit.</p> <p>The negative slew rate is determined by an external capacitor and resistor to VEE (negative supply). The RSSI rise and fall times for various RF input signal levels and R₂₄ values without the capacitor, C₂₄ are displayed in Figure 24. This is the maximum response time of the RSSI.</p>
24	RSSI		

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

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PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol	Internal Equivalent Circuit	Description/External Circuit Requirements
25	Enable		<p>Enable</p> <p>The IC regulators are enabled by placing this pin at V_{EE}.</p>
26	V_{EE1}		
			<p>VCC and VEE ESD Protection</p> <p>ESD protection diodes exist between the V_{CC} and V_{EE} pins. It is important to note that significant differences in potential ($> 0.5 V_{BE}$) between the two V_{CC} pins or between the V_{EE} pins can cause these structures to start to conduct, thus compromising isolation between the supply busses. V_{CC1} & V_{CC2} should be maintained at the same DC potential, as should V_{EE1} & V_{EE2}.</p>
28	Osc Base		<p>Oscillator Base</p> <p>This pin is connected to the base lead of the common collector transistor. Since there is no internal bias resistor to the base, V_{CC} is applied through an external choke or coil.</p>
29	Osc Emitter		<p>Oscillator Emitter</p> <p>This pin is connected to the emitter lead; the emitter is connected internally to a current source of about $200 \mu A$. Additional emitter current may be obtained by connecting an external resistor to V_{EE}; $I_E = V_{29}/R_{29}$.</p> <p>Details of circuits using overtone crystal and LC varactor controlled oscillators are discussed in the application section.</p>
31	Mix In1		<p>Mixer Inputs</p> <p>The parallel equivalent differential input impedance of the mixer is approximately $2.0 k\Omega$ in parallel with $1.0 pF$. This equates to a single ended input impedance of $1.0 k\Omega$ in parallel with $2.0 pF$.</p> <p>The application circuit utilizes a SAW filter having a differential output that requires a $2.0 k\Omega \parallel 2.0 pF$ load. Therefore, little matching is required between the SAW filter and the mixer inputs. This and alternative circuits are discussed in more detail in the application section.</p>
32	Mix In2		

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13158

APPLICATIONS INFORMATION

Evaluation PC Board

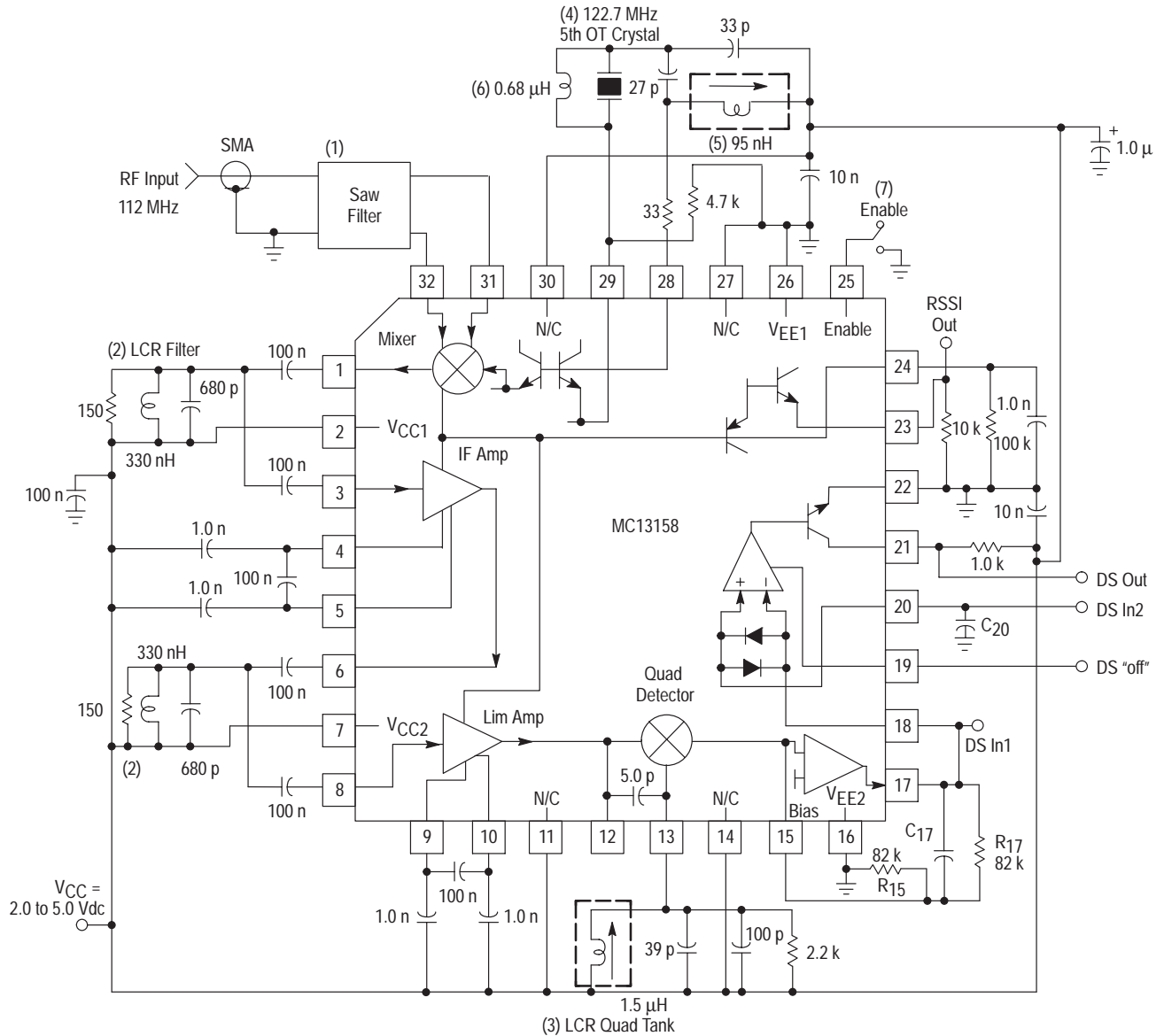
The evaluation PCB is very versatile and is intended to be used across the entire useful frequency range of this device. The center section of the board provides an area for attaching all SMT components to the circuit side and radial leaded components to the component ground side (see Figures 29 and 30). Additionally, the peripheral area surrounding the RF core provides pads to add supporting and interface circuitry as a particular application dictates. This evaluation board will be discussed and referenced in this section.

Component Selection

The evaluation PC board is designed to accommodate specific components, while also being versatile enough to use components from various manufacturers and coil types. Figures 13 and 14 show the placement for the components specified in the application circuit (Figure 12). The application circuit schematic specifies particular components that were used to achieve the results shown in the typical curves and tables but alternate components should give similar results.

MC13158

Figure 12. Application Circuit



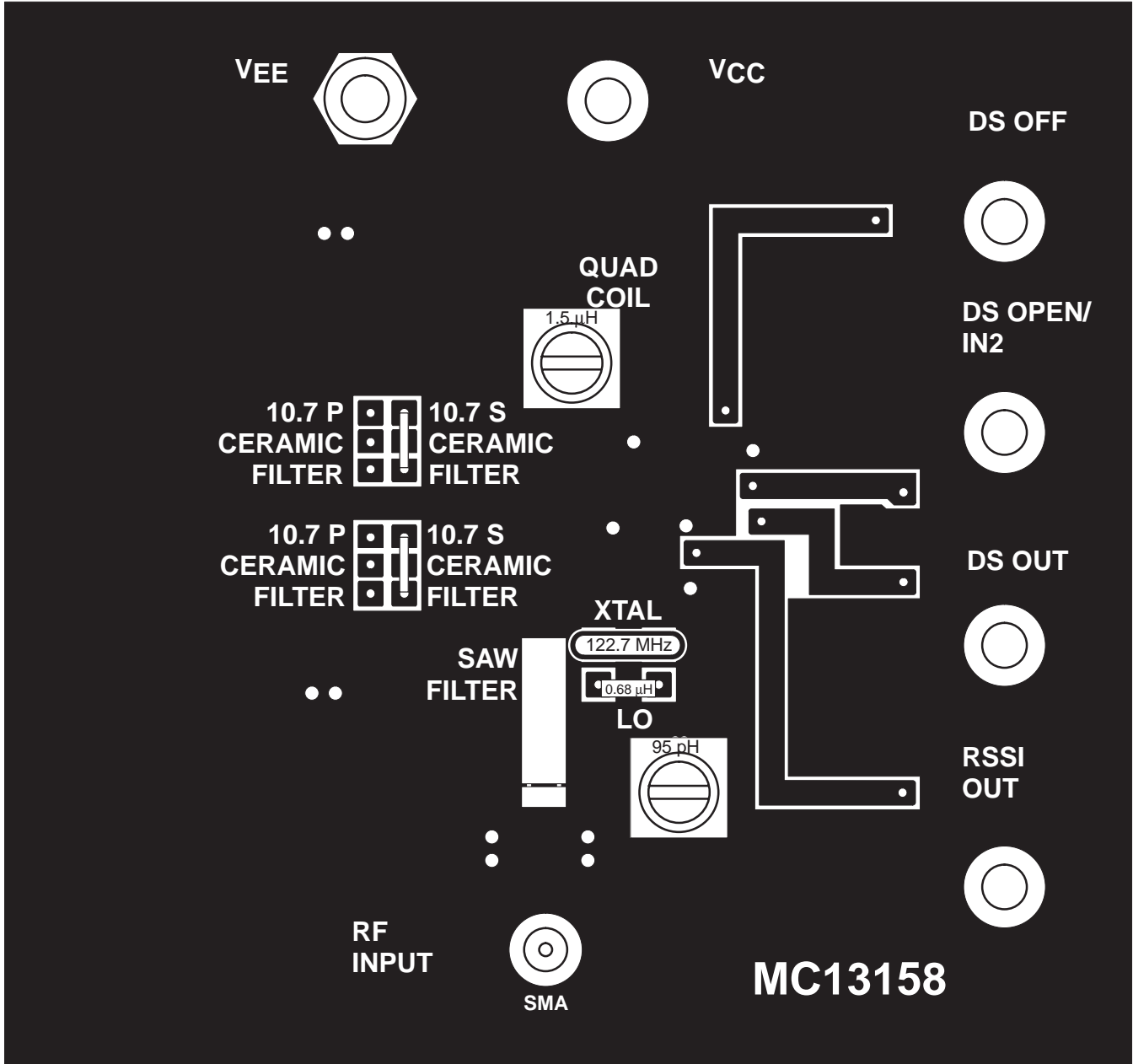
- NOTES:**
1. Saw Filter – Siemens part number Y6970M(5 pin SIP plastic package).
 2. An LCR filter reduces the broadband noise in the IF; ceramic filters may be used for data rates under 500 kHz. 4.0 dB insertion loss filters optimize the linearity of RSSI.
 3. The quadrature tank components are chosen to optimize linearity of the recovered signal while maintaining adequate recovered signal level. 1.5 μH 7.0 mm variable shielded inductor: Toko part # 292SNS-T1373Z. The shunt resistor is approximately equal to $Q(2\pi fL)$, where $Q \sim 18$ (3.0 dB BW = 600 kHz).
 4. The local oscillator circuit utilizes a 122.7 MHz, 5th overtone, series resonant crystal specified with a frequency tolerance of 25 PPM, ESR of 120 Ω max. The oscillator configuration is an emitter coupled butler.
 5. The 95 nH (Nominal) inductor is a 7.0 mm variable shielded inductor: Coilcraft part # 150-04J08S or equivalent.
 6. 0.68 μH axial lead chokes (molded inductor): Coilcraft part # 90-11.
 7. To enable the IC, Pin 25 is taken to VEE. The external pull down resistor at Pin 29 could be linked to the enable function; otherwise if it is taken to VEE as shown, it will keep the oscillator biased at about 500 μA depending on the VCC level.
 8. The other resistors and capacitors are surface mount components.

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13158

Figure 14. Ground Side Component Placement



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Input Matching/Components

It is desirable to use a SAW filter before the mixer to provide additional selectivity and adjacent channel rejection. In a wideband system the primary sensitivity of the receiver backend may be achieved before the last mixer. Bandpass filtering in the limiting IF is costly and difficult to achieve for bandwidths greater than 280 kHz.

The SAW filter should be selected to easily interface with the mixer differential input impedance of approximately 2.0 k Ω in parallel with 1.0 pF. The PC board is dedicated to the Siemens SAW filter (part number Y6970M); the part is designed for DECT at 112 MHz 1st IF frequency. It is designed for a load impedance of 2.0 k Ω in parallel with

2.0 pF; thus, no or little input matching is required between the SAW filter and the mixer.

The Siemens SAW filter has an insertion loss of typically 10 dB and a 3.0 dB bandwidth of 1.0 MHz. The relatively high insertion loss significantly contributes to the system noise and a filter having lower insertion loss would be desirable. In existing low loss SAW filters, the required load impedance is 50 Ω ; thus, interface matching between the filter and the mixer will be required. Figure 15 is a table of the single-ended mixer input impedance. A careful noise analysis is necessary to determine the secondary contribution to system noise.

Figure 15. Mixer Input Impedance
(Single-ended)

f (MHz)	R _s (Ω)	X _s (Ω)	R _p (Ω)	X _p (Ω)	C _p (pF)
50	930	-350	1060	-2820	1.1
100	480	-430	865	-966	1.6
150	270	-400	860	-580	1.8
200	170	-320	770	-410	1.9
250	130	-270	690	-330	1.85
300	110	-250	680	-300	1.8
400	71	-190	580	-220	1.8
500	63	-140	370	-170	1.9
600	49	-110	300	-130	2.0

System Noise Considerations

The system block diagram in Figure 16 shows the cascaded noise stages contributing to the system noise; it represents the application circuit in Figure 12 and a low noise preamp using a MRF941 transistor (see Figure 17). The preamp is designed for a conjugately matched input and output at 2.0 Vdc V_{CE} and 3.0 mAdc I_C. S-parameters at 2.0 V, 3.0 mA and 100 MHz are:

$$\begin{aligned} S_{11} &= 0.86, -20 \\ S_{21} &= 9.0, 164 \\ S_{12} &= 0.02, 79 \\ S_{22} &= 0.96, -12 \end{aligned}$$

The bias network sets V_{CE} at 2.0 V and I_C at 3.0 mA for V_{CC} = 3.0 to 3.5 Vdc. The preamp operates with 18 dB gain and 2.7 dB noise figure.

In the cascaded noise analysis the system noise equation is:

$$F_{\text{system}} = F_1 + [(F_2 - 1)/G_1] + [(F_3 - 1)]/[(G_1)(G_2)]$$

where:

- F1 = the Noise Factor of the Preamp
- G1 = the Gain of the Preamp
- F2 = the Noise factor of the SAW Filter
- G2 = the Gain of the SAW Filter
- F3 = the Noise factor of the Mixer

Note: the proceeding terms are defined as linear relationships and are related to the log form for gain and noise figure by the following:

$$F = \log^{-1}[(\text{NF in dB})/10] \quad \text{and similarly}$$

$$G = \log^{-1}[(\text{Gain in dB})/10]$$

The noise figure and gain measured in dB are shown in the system block diagram. The mixer noise figure is typically 14 dB and the SAW filter adds typically 10 dB insertion loss. Addition of a low noise preamp having a 18 dB gain and 2.7 dB noise figure not only improves the system noise figure but it increases the reverse isolation from the local oscillator to the antenna input at the receiver. Calculating in terms of gain and noise factor yields the following:

$$\begin{aligned} F_1 &= 1.86; \quad G_1 = 63.1 \\ F_2 &= 10; \quad G_2 = 0.1 \\ F_3 &= 25.12 \end{aligned}$$

Thus, substituting in the equation for system noise factor:

$$F_{\text{system}} = 5.82; \quad \text{NF}_{\text{system}} = 7.7 \text{ dB}$$

Figure 16. System Block Diagram for Noise Analysis

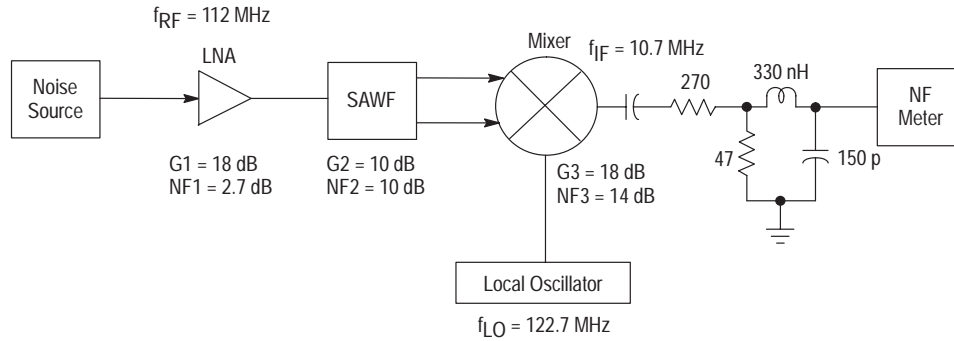
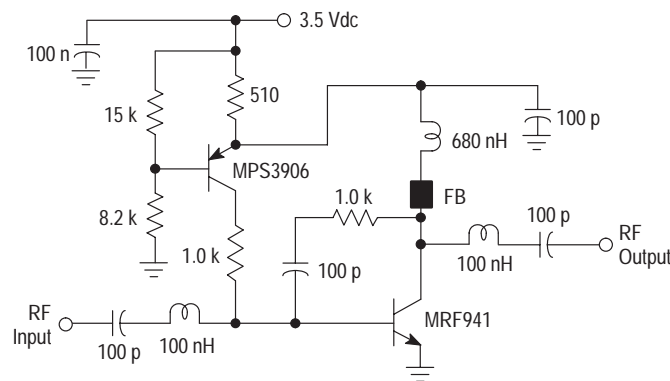


Figure 17. 112 MHz LNA



LOCAL OSCILLATORS

VHF Applications

The on-chip grounded collector transistor may be used for HF and VHF local oscillator with higher order overtone crystals. The local oscillator in the application circuit (Figure 12) shows a 5th overtone oscillator at 122.7 MHz. This circuit uses a Butler overtone oscillator configuration. The amplifier is an emitter follower. The crystal is driven from the emitter and is coupled to the high impedance base through a capacitive tap network. Operation at the desired overtone frequency is ensured by the parallel resonant circuit formed by the variable inductor and the tap capacitors and parasitic capacitances of the on-chip transistor and PC board. The variable inductor specified in the schematic could be replaced with a high tolerance, high Q ceramic or air wound surface mount component if the other components have tight enough tolerances. A variable inductor provides an adjustment for gain and frequency of the resonant tank ensuring lock up and start-up of the crystal oscillator. The overtone crystal is chosen with ESR of typically 80 Ω and 120 Ω maximum; if the resistive loss in the crystal is too high the performance of oscillator may be impacted by lower gain margins.

A series LC network to ground (which is V_{CC}) is comprised of the inductance of the base lead of the on-chip transistor and PC board traces and tap capacitors. Parasitic oscillations often occur in the 200 to 800 MHz range. A small resistor is placed in series with the base (Pin 28) to cancel the

negative resistance associated with this undesired mode of oscillation. Since the base input impedance is so large a small resistor in the range of 27 to 68 Ω has very little effect on the desired Butler mode of oscillation.

The crystal parallel capacitance, C_O , provides a feedback path that is low enough in reactance at frequencies of 5th overtones or higher to cause trouble. C_O has little effect near resonance because of the low impedance of the crystal motional arm ($R_M-L_M-C_M$). As the tunable inductor which forms the resonant tank with the tap capacitors is tuned "off" the crystal resonant frequency it may be difficult to tell if the oscillation is under crystal control. Frequency jumps may occur as the inductor is tuned. In order to eliminate this behavior an inductor, L_O , is placed in parallel with the crystal. L_O is chosen to be resonant with the crystal parallel capacitance, C_O , at the desired operation frequency. The inductor provides a feedback path at frequencies well below resonance; however, the parallel tank network of the tap capacitors and tunable inductor prevent oscillation at these frequencies.

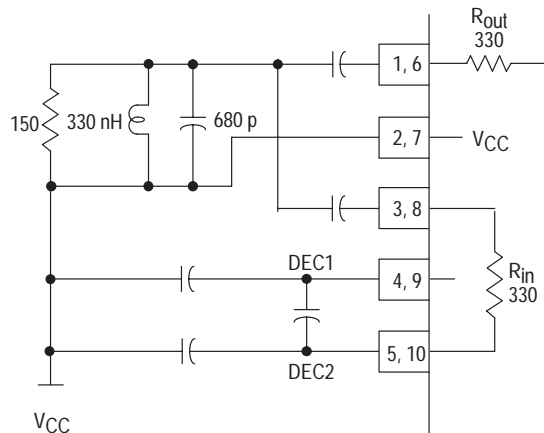
IF Filtering/Matching

In wideband data systems the IF bandpass needed is greater than can be found in low cost ceramic filters operating at 10.7 MHz. It is necessary to bandpass limit with LC networks or series-parallel ceramic filter networks. Murata offers a series-parallel resonator pair (part number

KMFC545) with a 3.0 dB bandwidth of ± 325 kHz and a maximum insertion loss of 5.0 dB. The application PC board is laid out to accommodate this filter pair (a filter pair is used at both locations of the split IF). However, even using a series parallel ceramic filter network yields only a maximum bandpass of 650 kHz. In some applications a wider band IF bandpass is necessary.

A simple LC network yields a bandpass wider than the SAW filter but it does reduce an appreciable amount of wideband IF noise. In the application circuit an LC network is specified using surface mount components. The parallel LC components are placed between the outputs of the mixer and IF amplifier to the V_{CC} trace; internal 330 loads are connected from the mixer and IF amplifier outputs to DEC2 (Pin 5 and 10 respectively). This loads the outputs with the optimal load impedance but creates a low insertion loss filter. An external shunt resistor may be used to widen the bandpass and to acquire the 10 dB composite loss necessary to linearize the RSSI output. The equivalent circuit is shown in Figure 18.

Figure 18. IF LCR Filter



The following equations satisfy the 12 dB loss (1:4 resistive ratio):

$$\frac{(R_{ext})(330)}{(R_{ext} + 330)} = \text{Requivalent}$$

$$\frac{\text{Requivalent}}{(\text{Requivalent} + 330)} = 1/4$$

Solve for Requivalent:

$$4(\text{Requivalent}) = \text{Requivalent} + 330$$

$$3(\text{Requivalent}) = 330$$

$$\text{Requivalent} = 110$$

Substitute for Requivalent and solve for Rext:

$$330(R_{ext}) = 110(R_{ext}) + (330)(110)$$

$$R_{ext} = (330)(110)/220$$

$$R_{ext} = 165 \Omega$$

The IF is 10.7 MHz although any IF between 10 to 20 MHz could be used. The value of the coil is lowered from that used in the quadrature circuit because the unloaded Q must be maintained in a surface mount component. A standard value component having an unloaded Q = 100 at 10.7 MHz is 330 nH; therefore the capacitor is 669 pF. Standard values have been chosen for these components;

$$R_{ext} = 150 \Omega$$

$$C = 680 \text{ pF}$$

$$L = 330 \text{ nH}$$

Computation of the loaded Q of this LCR network is

$$Q = \text{Requivalent}/X_L$$

where: $X_L = 2\pi fL$ and Requivalent is 103 Ω

$$\text{Thus, } Q = 4.65$$

The total system loss is

$$20 \log (103/433) = -12.5 \text{ dB}$$

Quadrature Detector

The quadrature detector is coupled to the IF with an internal 5.0 pF capacitor between Pins 12 and 13. For wideband data applications, the drive to the detector can be increased with an additional external capacitor between these pins; thus, the recovered signal level output is increased for a given bandwidth

The wideband performance of the detector is controlled by the loaded Q of the LC tank circuit. The following equation defines the components which set the detector circuit's bandwidth:

$$Q = R_T/X_L \quad [1]$$

where R_T is the equivalent shunt resistance across the LC Tank

X_L is the reactance of the quadrature inductor at the IF frequency ($X_L = 2\pi fL$).

The inductor and capacitor are chosen to form a resonant LC tank with the PCB and parasitic device capacitance at the desired IF center frequency as predicted by

$$f_c = [2\pi (LC_p)^{1/2}]^{-1} \quad [2]$$

where L is the parallel tank inductor C_p is the equivalent parallel capacitance of the parallel resonant tank circuit.

The following is a design example for a wideband detector at 10.7 MHz and a loaded Q of 18. The loaded Q of the quadrature detector is chosen somewhat less than the Q of the IF bandpass. For an IF frequency of 10.7 MHz and an IF bandpass of 600 kHz, the IF bandpass Q is approximately 6.4.

Example:

Let the external $C_{ext} = 139$ pF. (The minimum value here should be much greater than the internal device and PCB parasitic capacitance, $C_{int} \approx 3.0$ pF). Thus, $C_p = C_{int} + C_{ext} = 142$ pF.

Rewrite equation (2) and solve for L:

$$L = (0.159)^2 / (C_p f_c^2)$$

$$L = 1.56 \mu\text{H}; \text{ Thus, a standard value is}$$

chosen:

$$L = 1.56 \mu\text{H (tunable shielded inductor)}$$

The value of the total damping resistor to obtain the required loaded Q of 18 can be calculated by rearranging equation (1):

$$R_T = Q(2\pi fL)$$

$$R_T = 18(2\pi)(10.7)(1.5) = 1815 \Omega$$

The internal resistance, R_{int} at the quadrature tank Pin 13 is approximately 13 k Ω and is considered in determining the external resistance, R_{ext} which is calculated from

$$R_{ext} = ((R_T)(R_{int})) / (R_{int} - R_T)$$

$$R_{ext} = 2110; \text{ Thus, choose the standard value:}$$

$$R_{ext} = 2.2 \text{ k}\Omega$$

It is important to set the DC level of the detector output at Pin 17 to center the peak to peak swing of the recovered signal. In the equivalent internal circuit shown in the Pin Function Description, the reference voltage at the positive terminal of the inverting op amp buffer amplifier is set at 1.0 V_{BE} . The detector DC level, V_{17} is determined by the following equation:

$$V_{17} = [((R_{15}/R_{17}) + 1) / (R_{15}/R_{17})] V_{BE}$$

Thus, for a 1:1 ratio of R_{15}/R_{17} , $V_{17} = 2.0 V_{BE} = 1.4 \text{ Vdc}$. Similarly for a 2:1, $V_{17} = 1.5 V_{BE} = 1.05 \text{ Vdc}$; and for 3:1, $V_{17} = 1.33 V_{BE} = 0.93 \text{ Vdc}$.

Figure 19 shows the detector "S-Curves", in which the resistor ratio is varied while maintaining a constant gain (R_{17} is held at 62 k). R_{15} is 62 k for a 1:1 ratio; while $R_{15} = 120 \text{ k}$ and 180 k to produce the 2:1 and 3:1 ratios. The IF signal into the detector is swept $\pm 500 \text{ kHz}$ about the 10.7 MHz IF center frequency. The resulting curve show how the resistor ratio and the supply voltage effects the symmetry of the "S-curve" (Figure 21 Test Setup). For the 3:1 and 2:1 ratio, symmetry is maintained with V_S from 2.0 to 5.0 Vdc; however, for the 1:1 ratio, symmetry is lost at 2.0 Vdc.

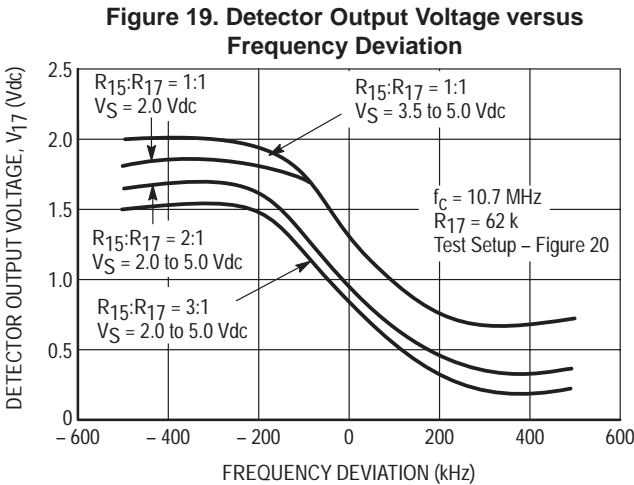
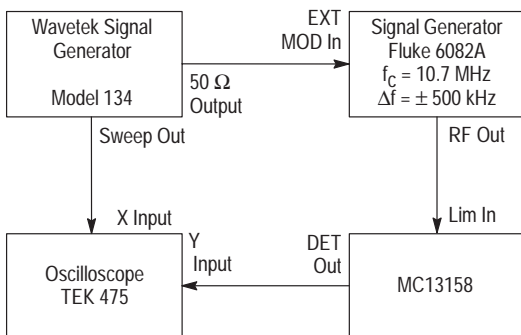


Figure 19. Detector Output Voltage versus Frequency Deviation

Figure 20. Demodulator "S-Curve" Test Setup



Data Slicer Circuit

C_{20} at the input of the data slicer is chosen to maintain a time constant long enough to hold the charge on the capacitor for the longest strings of bits at the same polarity. For a data rate at 576 kHz a bit stream of 15 bits at the same polarity would equate to an apparent data rate of approximately 77 kbps or 38 kHz. The time constant would be approximately 26 μs . The following expression equates the time constant, t , to the external components:

$$t = 2\pi (R_{18})(C_{20})$$

Solve for C_{20} :

$$C_{20} = t / 2\pi (R_{18})$$

where the effective resistance R_{18} is a complex function of the demodulator feedback resistance and the data slicer input circuit. In the data input network the back to back diodes form a charge and discharge path for the capacitor at Pin 20; however, the diodes create a non-linear response. This resistance is loaded by the β , beta of the detector output transistor; beta = 100 is a typical value (see Figure 21). Thus, the apparent value of the resistance at Pin 18 (DS IN1) is approximately equal to:

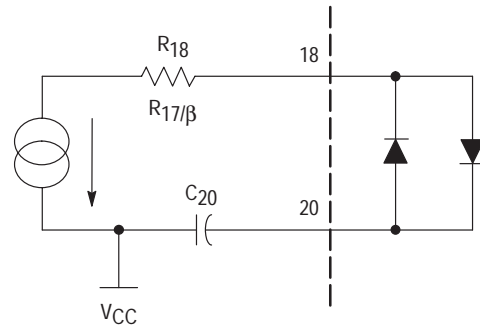
$$R_{18} \sim R_{17} / 100$$

where R_{17} is 82 k Ω , the feedback resistor from Pin 17 to 15. Therefore, substituting for R_{18} and solving for C_{20} :

$$C_{20} = 15.9 (t) / R_{17} = 5.04 \text{ nF}$$

The closest standard value is 4.7 nF.

Figure 21. Data Slicer Equivalent Input Circuit



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13158 SYSTEM PERFORMANCE DATA

RSSI

In Figure 22, the RSSI versus RF Input Level shows the linear response of RSSI over a 65 dB range but it has extended capability over 80 dB from -80 dBm to $+10$ dBm. The RSSI is measured in the application circuit (Figure 12) in which a SAW filter is used before the mixer; thus, the overall sensitivity is compromised for the sake of selectivity. The curves are shown for three filters having different bandwidths:

- 1) LCR Filter with 2.3 MHz 3.0 dB BW (Circuit and Component Placement is shown in Figure 12)
- 2) Series-Parallel Ceramic Filter with 650 kHz 3.0 dB BW (Murata Part # KMFC-545)
- 3) Ceramic Filter with 280 kHz 3.0 dB BW.

Figure 22. RSSI Output Voltage versus Signal Input Level

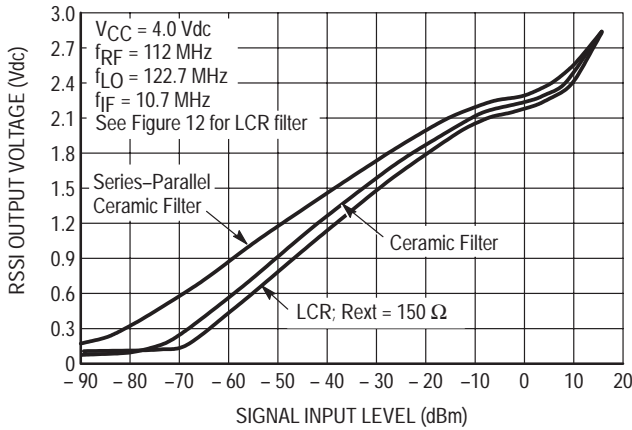
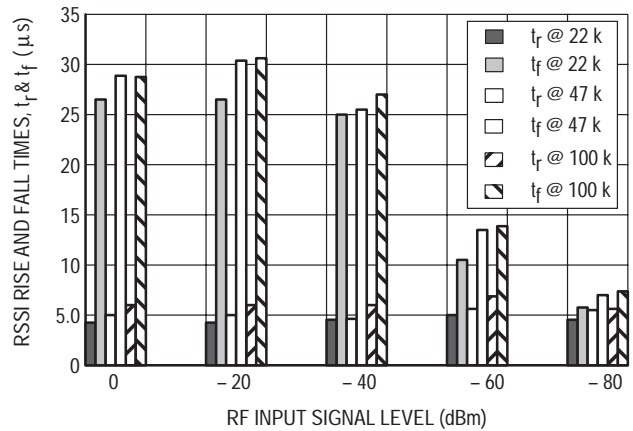


Figure 23. RSSI Output Rise and Fall Times versus RF Input Signal Level



SINAD Performance

Figure 24 shows a test setup for a narrowband demodulator output response in which a C-message filter and an active de-emphasis filter is used following the demodulator. The input is matched using a 1:4 impedance transformer. The SINAD performance is shown in Figure 25 with no preamp and in Figure 26 with a preamp (Preamp – Figure 16). The 12 dB SINAD sensitivity is -101 dBm with no preamp and -113 dBm with the preamp.

Figure 24. Test Setup for Narrowband SINAD

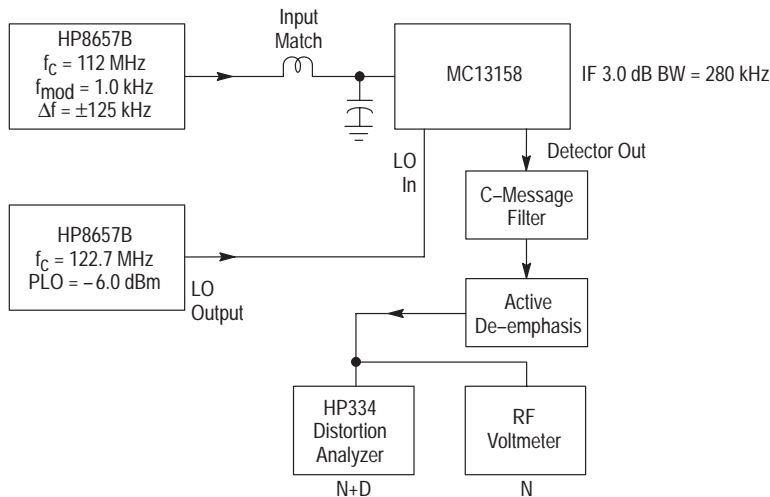


Figure 25. S+N+D, N+D, N versus Input Signal Level (without preamp)

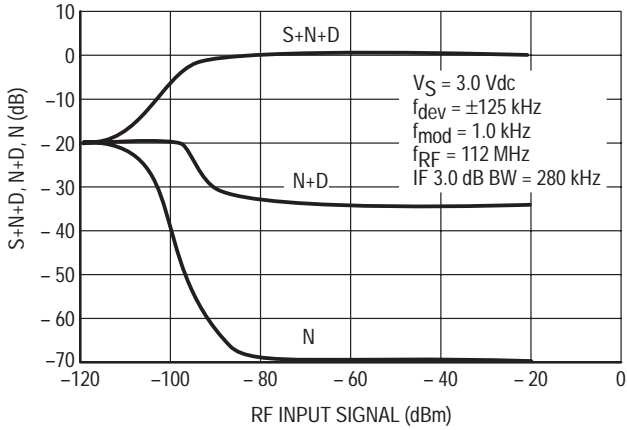


Figure 26. S+N+D, N+D, N versus Input Signal Level (with preamp)

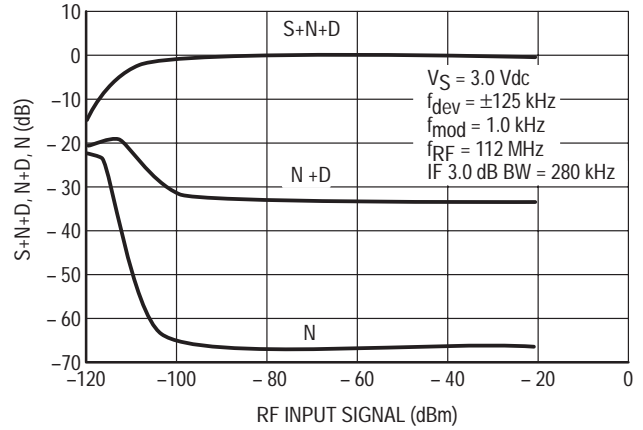


Figure 27. Input IP3, 1.0 dB Compression Pt. Test Setup

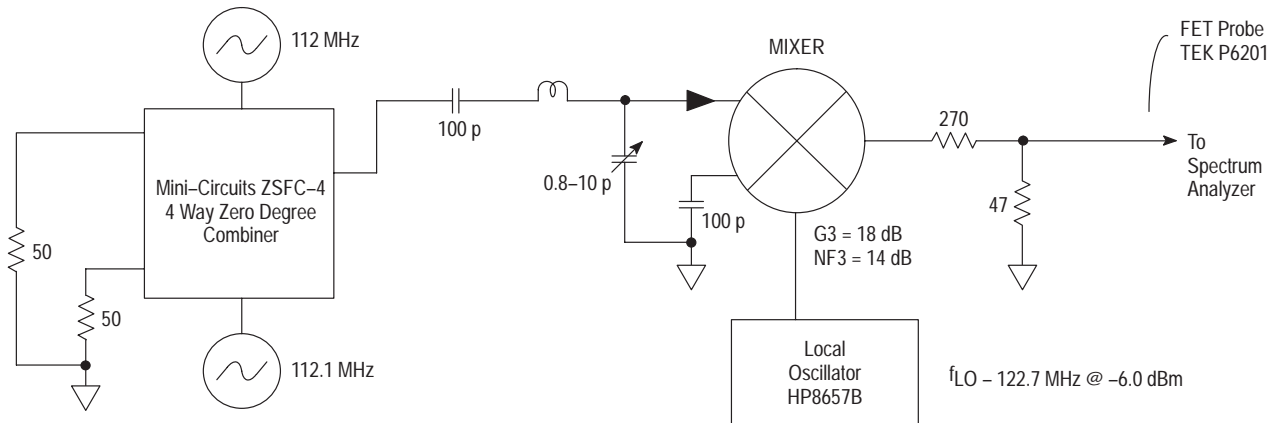
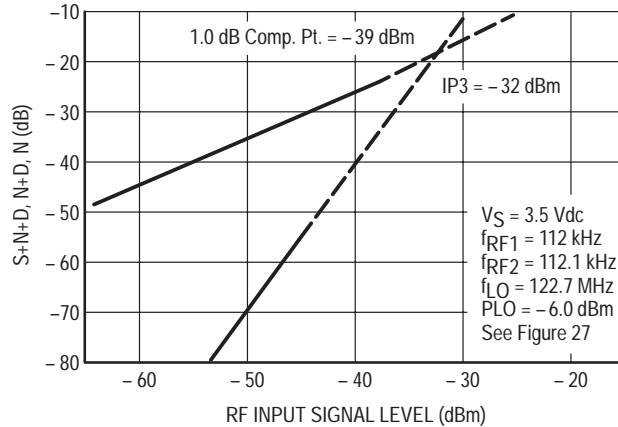


Figure 28. -1.0 dB Compression Pt. and Input Third Order Intercept

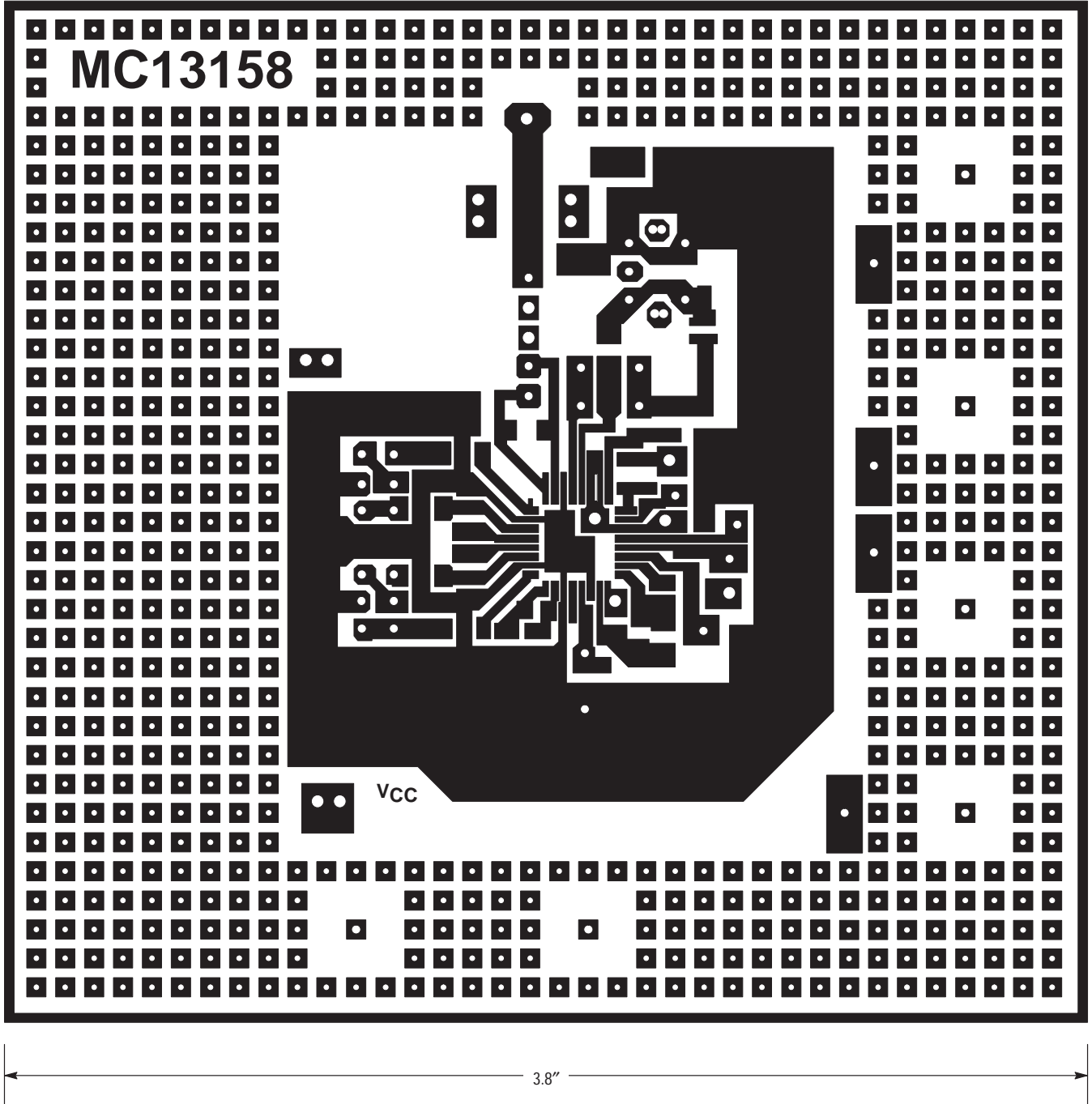


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MC13158

Figure 29. Circuit Side View

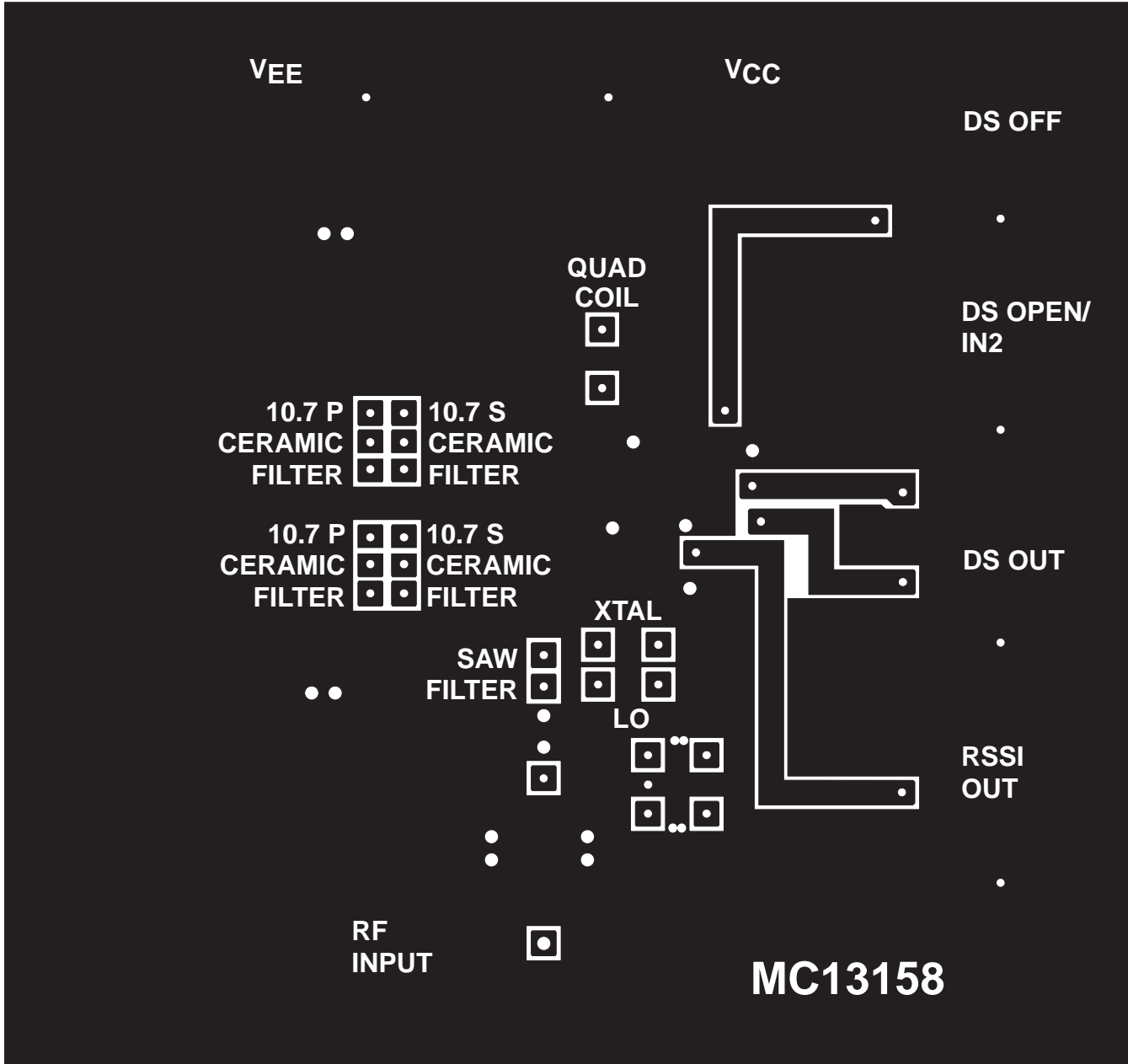


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MC13158

Figure 30. Ground Side View



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UHF FM/AM Transmitter

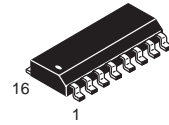
The MC13176 is a one chip FM/AM transmitter subsystem designed for AM/FM communication systems. It include a Colpitts crystal reference oscillator, UHF oscillator, $\times 32$ prescaler and phase detector forming a versatile PLL system. Targeted applications are in the 260 to 470 MHz band and the 902 to 928 MHz band covered by FCC Title 47; Part 15. Other applications include local oscillator sources in UHF and 900 MHz receivers, UHF and 900 MHz video transmitters, RF Local Area Networks (LANs), and high frequency clock drivers. The MC13176 offers the following features:

- UHF Current Controlled Oscillator
- Uses Easily Available 3rd Overtone or Fundamental Crystals for Reference
- Fewer External Parts Required
- Low Operating Supply Voltage (1.8 to 5.0 Vdc)
- Low Supply Drain Currents
- Power Output Adjustable (Up to 10 dBm)
- Differential Output for Loop Antenna or Balun Transformer Networks
- Power Down Feature
- ASK Modulated by Switching Output On and Off
- $f_o = 32 \times f_{ref}$

MC13176

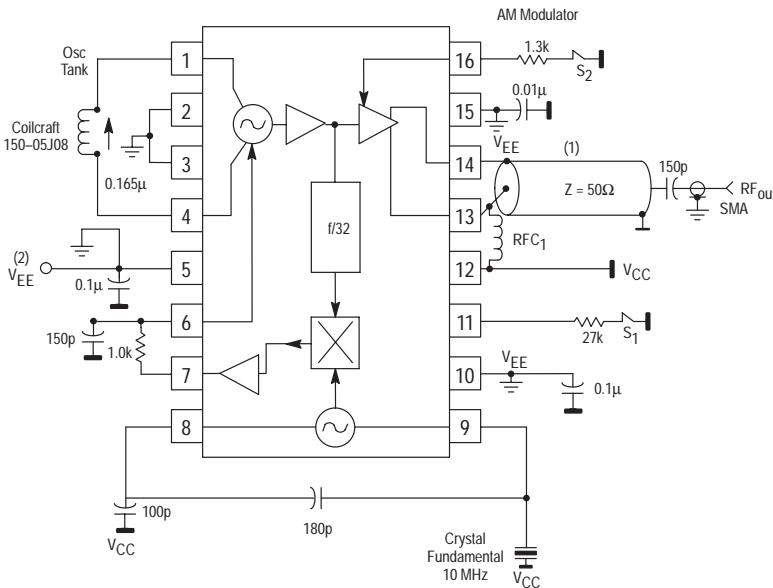
UHF FM/AM TRANSMITTER

SEMICONDUCTOR TECHNICAL DATA



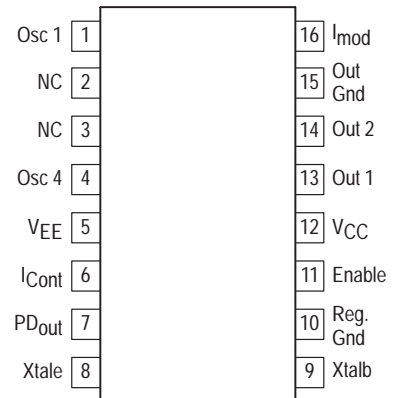
D SUFFIX
PLASTIC PACKAGE
CASE 751B
(SO-16)

Figure 1. Typical Application as 320 MHz AM Transmitter



- NOTES:**
1. 50 Ω coaxial balun, 1/10 wavelength at 320 MHz equals 1.5 inches.
 2. Pins 5, 10 & 15 are ground and connected to V_{EE} which is the component/DC ground plane side of PCB. These pins must be decoupled to V_{CC} ; decoupling capacitors should be placed as close as possible to the pins.

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13176D	$T_A = -40$ to 85°C	SO-16

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13176

PIN FUNCTION DESCRIPTIONS

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Pin	Symbol	Internal Equivalent Circuit	Description/External Circuit Requirements
1 & 4	Osc 1, Osc 4		<p>CCO Inputs</p> <p>The oscillator is a current controlled type. An external oscillator coil is connected to Pins 1 and 4 which forms a parallel resonance LC tank circuit with the internal capacitance of the IC and with parasitic capacitance of the PC board. Three base-emitter capacitances in series configuration form the capacitance for the parallel tank. These are the base-emitters at Pins 1 and 4 and the base-emitter of the differential amplifier. The equivalent series capacitance in the differential amplifier is varied by the modulating current from the frequency control circuit (see Pin 6, internal circuit). A more thorough discussion is found in the Applications Information section.</p>
5	V _{EE}		<p>Supply Ground (V_{EE})</p> <p>In the PCB layout, the ground pins (also applies to Pins 10 and 15) should be connected directly to chassis ground. Decoupling capacitors to V_{CC} should be placed directly at the ground returns.</p>
6	I _{Cont}		<p>Frequency Control</p> <p>For V_{CC} = 3.0 Vdc, the voltage at Pin 6 is approximately 1.55 Vdc. The oscillator is current controlled by the error current from the phase detector. This current is amplified to drive the current source in the oscillator section which controls the frequency of the oscillator. Figures 8 and 9 show the Δf_{osc} versus I_{Cont}. Figure 5 shows the Δf_{osc} versus I_{Cont} at -40°C, +25°C and +85°C for 320 MHz. The CCO may be FM modulated as shown in Figures 17 and 18, MC13176 320 MHz FM Transmitter. A detailed discussion is found in the Applications Information section.</p>
7	PD _{out}		<p>Phase Detector Output</p> <p>The phase detector provides ±30 μA to keep the CCO locked at the desired carrier frequency. The output impedance of the phase detector is approximately 53 kΩ. Under closed loop conditions there is a DC voltage which is dependent upon the free running oscillator and the reference oscillator frequencies. The circuitry between Pins 7 and 6 should be selected for adequate loop filtering necessary to stabilize and filter the loop response. Low pass filtering between Pin 7 and 6 is needed so that the corner frequency is well below the sum of the divider and the reference oscillator frequencies, but high enough to allow for fast response to keep the loop locked. Refer to the Applications Information section regarding loop filtering and FM modulation.</p>

PIN FUNCTION DESCRIPTIONS

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Pin	Symbol	Internal Equivalent Circuit	Description/External Circuit Requirements
8	Xtaleb		<p>Crystal Oscillator Inputs</p> <p>The internal reference oscillator is configured as a common emitter Colpitts. It may be operated with either a fundamental or overtone crystal depending on the carrier frequency and the internal prescaler. Crystal oscillator circuits and specifications of crystals are discussed in detail in the applications section. With $V_{CC} = 3.0$ Vdc, the voltage at Pin 8 is approximately 1.8 Vdc and at Pin 9 is approximately 2.3 Vdc. 500 to 1000 mVp-p should be present at Pin 9. The Colpitts is biased at 200 μA; additional drive may be acquired by increasing the bias to approximately 500 μA. Use 6.2 k from Pin 8 to ground.</p>
9	Xtaleb		
10	Reg. Gnd		<p>Regulator Ground</p> <p>An additional ground pin is provided to enhance the stability of the system. Decoupling to the V_{CC} (RF ground) is essential; it should be done at the ground return for Pin 10.</p>
11	Enable		<p>Device Enable</p> <p>The potential at Pin 11 is approximately 1.25 Vdc. When Pin 11 is open, the transmitter is disabled in a power down mode and draws less than 1.0 μA I_{CC} if the MOD at Pin 16 is also open (i.e., it has no current driving it). To enable the transmitter a current source of 10 μA to 90 μA is provided. Figures 3 and 4 show the relationship between I_{CC}, V_{CC} and $I_{reg. enable}$. Note that I_{CC} is flat at approximately 10 mA for $I_{reg. enable} = 5.0$ to 100 μA ($I_{mod} = 0$).</p>
12	V_{CC}		<p>Supply Voltage (V_{CC})</p> <p>The operating supply voltage range is from 1.8 Vdc to 5.0 Vdc. In the PCB layout, the V_{CC} trace must be kept as wide as possible to minimize inductive reactances along the trace; it is best to have it completely fill around the surface mount components and traces on the circuit side of the PCB.</p>
13 & 14	Out 1 and Out 2		<p>Differential Output</p> <p>The output is configured differentially to easily drive a loop antenna. By using a transformer or balun, as shown in the application schematic, the device may then drive an unbalanced low impedance load. Figure 6 shows how much the Output Power and Free-Running Oscillator Frequency change with temperature at 3.0 Vdc; $I_{mod} = 2.0$ mA.</p>
15	Out_Gnd		<p>Output Ground</p> <p>This additional ground pin provides direct access for the output ground to the circuit board V_{EE}.</p>
16	I_{mod}		<p>AM Modulation/Power Output Level</p> <p>The DC voltage at this pin is 0.8 Vdc with the current source active. An external resistor is chosen to provide a source current of 1.0 to 3.0 mA, depending on the desired output power level at a given V_{CC}. Figure 27 shows the relationship of Power Output to Modulation Current, I_{mod}. At $V_{CC} = 3.0$ Vdc, 3.5 dBm power output can be acquired with about 35 mA I_{CC}. For FM modulation, Pin 16 is used to set the desired output power level as described above. For AM modulation, the modulation signal must ride on a positive DC bias offset which sets a static (modulation off) modulation current. External circuitry for various schemes is further discussed in the Applications Information section.</p>

Figure 3. Supply Current versus Supply Voltage

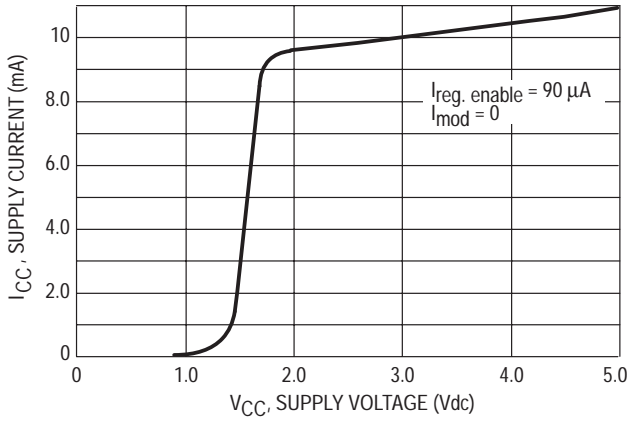


Figure 4. Supply Current versus Regulator Enable Current

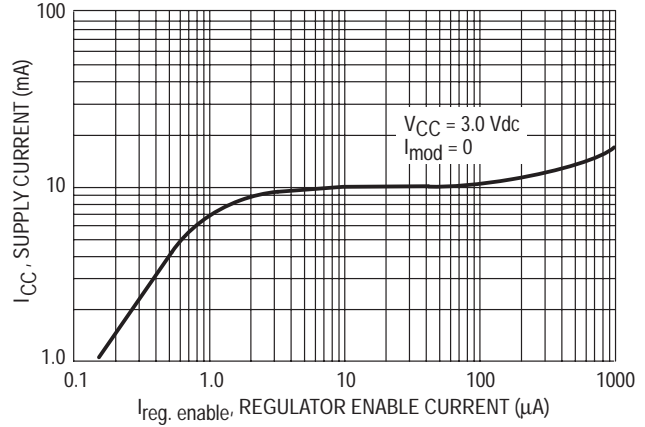


Figure 5. Change Oscillator Frequency versus Oscillator Control Current

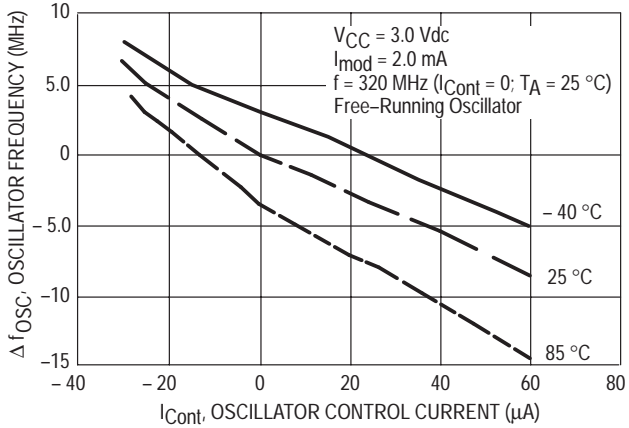


Figure 6. Change in Oscillator Frequency and Output Power versus Ambient Temperature

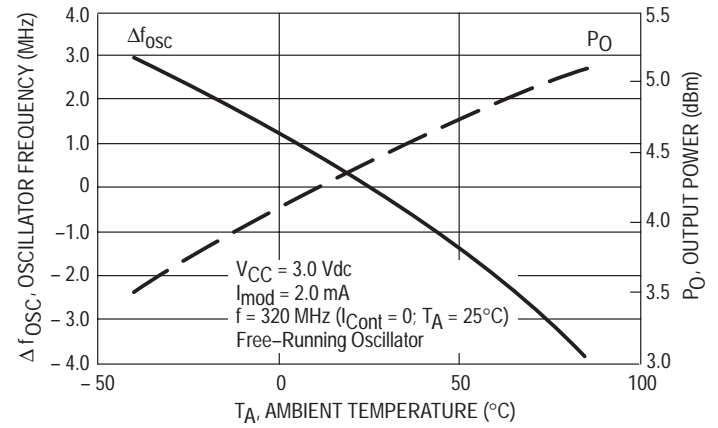
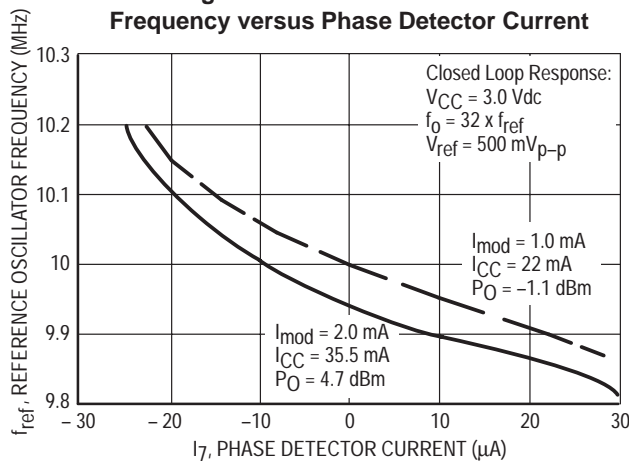


Figure 7. Reference Oscillator Frequency versus Phase Detector Current



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NOT RECOMMENDED FOR NEW DESIGNS

Figure 8. Change in Oscillator Frequency versus Oscillator Control Current

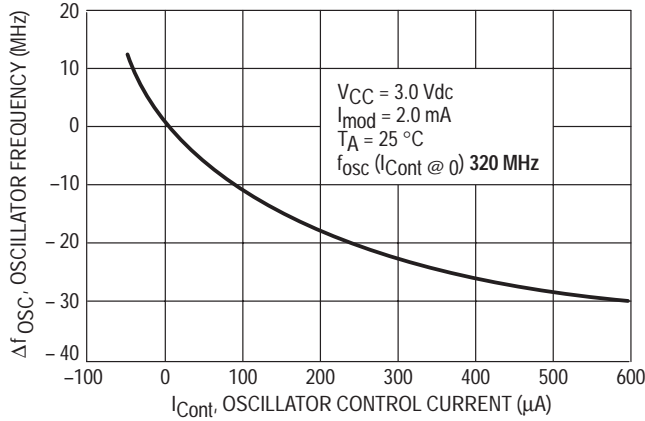
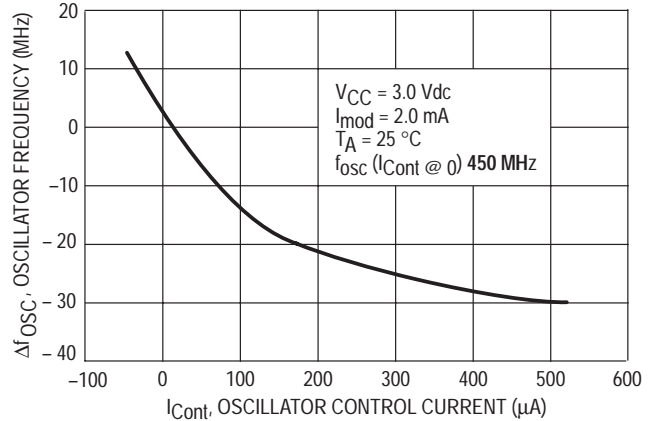


Figure 9. Change in Oscillator Frequency versus Oscillator Control Current



APPLICATIONS INFORMATION

Evaluation PC Board

The evaluation PCB, shown in Figures 32 and 33, is very versatile and is intended to be used across the entire useful frequency range of this device. The center section of the board provides an area for attaching all SMT components to the circuit side and radial leaded components to the component ground side of the PCB (see Figures 34 and 35). Additionally, the peripheral area surrounding the RF core provides pads to add supporting and interface circuitry as a particular application dictates. This evaluation board will be discussed and referenced in this section.

Current Controlled Oscillator (Pins 1 to 4)

It is critical to keep the interconnect leads from the CCO (Pins 1 and 4) to the external inductor symmetrical and equal in length. With a minimum inductor, the maximum free running frequency is greater than 1.0 GHz. Since this inductor will be small, it may be either a microstrip inductor, an air wound inductor or a tuneable RF coil. An air wound inductor may be tuned by spreading the windings, whereas tuneable RF coils are tuned by adjusting the position of an aluminum core in a threaded coilform. As the aluminum core coupling to the windings is increased, the inductance is decreased. The temperature coefficient using an aluminum core is better than a ferrite core. The UniCoil™ inductors made by Coilcraft may be obtained with aluminum cores (Part No. 51-129-169).

Ground (Pins 5, 10 and 15)

Ground Returns: It is best to take the grounds to a backside ground plane via plated through holes or eyelets at the pins. The application PCB layout implements this technique. Note that the grounds are located at or less than 100 mils from the devices pins.

Decoupling: Decoupling each ground pin to V_{CC} isolates each section of the device by reducing interaction between sections and by localizing circulating currents.

Loop Characteristics (Pins 6 and 7)

Figure 10 is the component block diagram of the MC13176D PLL system where the loop characteristics are described by the gain constants. Access to individual components of this PLL system is limited, inasmuch as the loop is only pinned out at the phase detector output and the

frequency control input for the CCO. However, this allows for characterization of the gain constants of these loop components. The gain constants K_p , K_o and K_n are well defined in the MC13176.

Phase Detector (Pin 7)

With the loop in lock, the difference frequency output of the phase detector is DC voltage that is a function of the phase difference. The sinusoidal type detector used in this IC has the following transfer characteristic:

$$I_e = A \sin \theta_e$$

The gain factor of the phase detector, K_p (with the loop in lock) is specified as the ratio of DC output current, I_e to phase error, θ_e :

$$K_p = I_e / \theta_e \text{ (Amps/radians)}$$

$$K_p = A \sin \theta_e / \theta_e$$

$$\sin \theta_e \sim \theta_e \text{ for } \theta_e \leq 0.2 \text{ radians;}$$

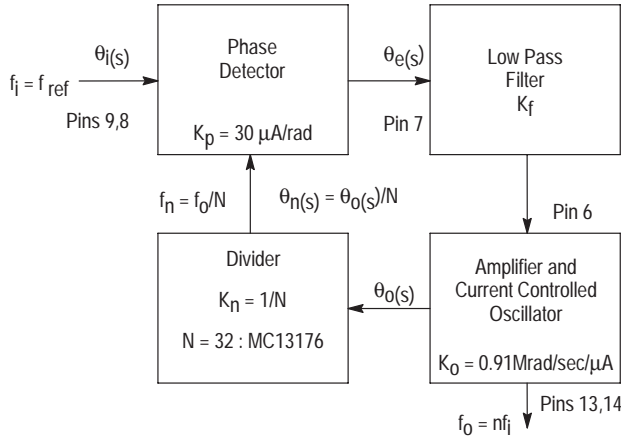
$$\text{thus, } K_p = A \text{ (Amps/radians)}$$

Figure 7 shows that the detector DC current is approximately 30 μA where the loop loses lock at $\theta_e = \pm \pi/2$ radians; therefore, K_p is 30 μA /radians.

Current Controlled Oscillator, CCO (Pin 6)

Figures 8 and 9 show the non-linear change in frequency of the oscillator over an extended range of control current for 320 and 450 MHz applications. K_o ranges from approximately 6.3×10^5 rad/sec/ μA or 100 kHz/ μA (Figure 8) to 8.8×10^5 rad/sec/ μA or 140 kHz/ μA (Figure 9) over a relatively linear response of control current (0 to 100 μA). The oscillator gain factor depends on the operating range of the control current (i.e., the slope is not constant). Included in the CCO gain factor is the internal amplifier which can sink and source at least 30 μA of input current from the phase detector. The internal circuitry at Pin 6 limits the CCO control current to 50 μA of source capability while its sink capability exceeds 200 μA as shown in Figures 8 and 9. Further information to follow shows how to use the full capabilities of the CCO by addition of an external loop amplifier and filter (see Figure 14). This additional circuitry yields at $K_o = 0.145$ MHz/ μA or 9.1×10^5 rad/sec/ μA .

Figure 10. Block Diagram of MC1317XD PLL



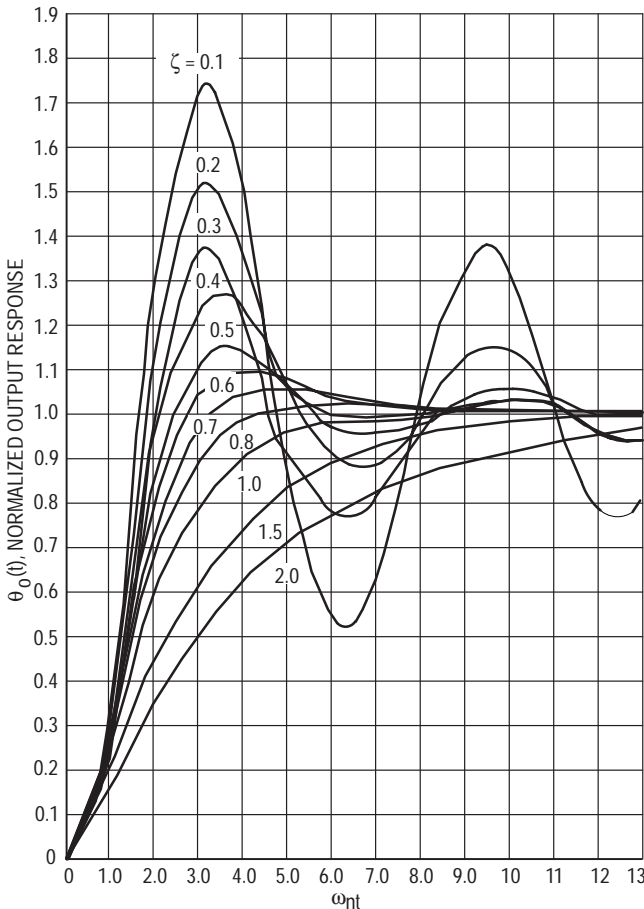
Where: $K_p =$ Phase detector gain constant in $\mu\text{A/rad}$; $K_p = 30 \mu\text{A/rad}$
 $K_f =$ Filter transfer function
 $K_n = 1/N$; $N = 32$
 $K_0 =$ CCO gain constant in $\text{rad/sec}/\mu\text{A}$
 $K_0 = 9.1 \times 10^5 \text{ rad/sec}/\mu\text{A}$

Loop Filtering

The fundamental loop characteristics, such as capture range, loop bandwidth, lock-up time and transient response are controlled externally by loop filtering.

The natural frequency (ω_n) and damping factor (∂) are important in the transient response to a step input of phase or frequency. For a given ∂ and lock time, ω_n can be determined from the plot shown in Figure 11.

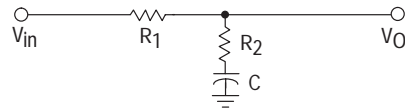
Figure 11. Type 2 Second Order Response



For $\partial = 0.707$ and lock time = 1.0 ms;
 then $\omega_n = 5.0/t = 5.0 \text{ krad/sec}$.

The loop filter may take the form of a simple low pass filter or a lag-lead filter which creates an additional pole at origin in the loop transfer function. This additional pole along with that of the CCO provides two pure integrators ($1/s^2$). In the lag-lead low pass network shown in Figure 12, the values of the low pass filtering parameters R_1 , R_2 and C determine the loop constants ω_n and ∂ . The equations $t_1 = R_1C$ and $t_2 = R_2C$ are related in the loop filter transfer functions $F(s) = 1 + t_2s/1 + (t_1 + t_2)s$.

Figure 12. Lag-Lead Low Pass Filter



The closed loop transfer function takes the form of a 2nd order low pass filter given by,

$$H(s) = K_v F(s)/s + K_v F(s)$$

From control theory, if the loop filter characteristic has $F(0) = 1$, the DC gain of the closed loop, K_v is defined as,

$$K_v = K_p K_0 K_n$$

and the transfer function has a natural frequency,

$$\omega_n = (K_v/t_1 + t_2)^{1/2}$$

and a damping factor,

$$\partial = (\omega_n/2) (t_2 + 1/K_v)$$

Rewriting the above equations and solving for the MC13176 with $\partial = 0.707$ and $\omega_n = 5.0 \text{ k rad/sec}$:

$$K_v = K_p K_0 K_n = (30) (0.91 \times 10^6) (1/32) = 0.853 \times 10^6$$

$$t_1 + t_2 = K_v/\omega_n^2 = 0.853 \times 10^6 / (25 \times 10^6) = 34.1 \text{ ms}$$

$$t_2 = 2\partial/\omega_n = (2) (0.707)/(5 \times 10^3) = 0.283 \text{ ms}$$

$$t_1 = (K_v/\omega_n^2) - t_2 = (34.1 - 0.283) = 33.8 \text{ ms}$$

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For $C = 0.47 \mu$;

then, $R_1 = t_1/C = 33.8 \times 10^{-3}/0.47 \times 10^{-6} = 72 \text{ k}$

thus, $R_2 = t_2/C = 0.283 \times 10^{-3}/0.47 \times 10^{-6} = 0.60 \text{ k}$

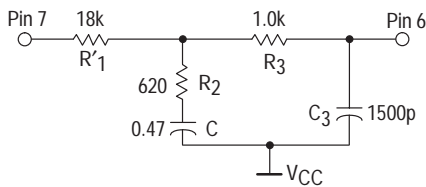
In the above example, the following standard value components are used,

$C = 0.47 \mu$; $R_2 = 620$ and $R'_1 = 72 \text{ k} - 53 \text{ k} \sim 18 \text{ k}$

(R'_1 is defined as $R_1 - 53 \text{ k}$, the output impedance of the phase detector.)

Since the output of the phase detector is high impedance ($\sim 50 \text{ k}$) and serves as a current source, and the input to the frequency control, Pin 6 is low impedance (impedance of the two diode to ground is approximately 500Ω), it is imperative that the second order low pass filter design above be modified. In order to minimize loading of the R_2C shunt network, a higher impedance must be established to Pin 6. A simple solution is achieved by adding a low pass network between the passive second order network and the input to Pin 6. This helps to minimize the loading effects on the second order low pass while further suppressing the sideband spurs of the crystal oscillator. A low pass filter with $R_3 = 1.0 \text{ k}$ and $C_3 = 1500 \text{ p}$ has a corner frequency (f_c) of 106 kHz ; the reference sideband spurs are down greater than -60 dBc .

Figure 13. Modified Low Pass Loop Filter



Hold-In Range

The hold-in range, also called the lock range, tracking range and synchronization range, is the ability of the CCO frequency, f_o to track the input reference signal, $f_{ref} \cdot N$ as it gradually shifted away from the free running frequency, f_f . Assuming that the CCO is capable of sufficient frequency deviation and that the internal loop amplifier and filter are not overdriven, the CCO will track until the phase error, θ_e approaches $\pm\pi/2$ radians. Figures 5 through 7 are a direct

measurement of the hold-in range (i.e. $\Delta f_{ref} \times N = \pm \Delta f_H \times 2\pi$). Since $\sin \theta_e$ cannot exceed ± 1.0 , as θ_e approaches $\pm\pi/2$ the hold-in range is equal to the DC loop gain, $K_V \times N$.

$$\pm \Delta \omega_H = \pm K_V \times N$$

where, $K_V = K_P K_O K_n$.

In the above example,

$$\pm \Delta \omega_H = \pm 27.3 \text{ Mrad/sec}$$

$$\pm \Delta f_H = \pm 4.35 \text{ MHz}$$

Extended Hold-in Range

The hold-in range of about 3.4% could cause problems over temperature in cases where the free-running oscillator drifts more than 2 to 3% because of relatively high temperature coefficients of the ferrite tuned CCO inductor. This problem might worsen for lower frequency applications where the external tuning coil is large compared to internal capacitance at Pins 1 and 4. To improve hold-in range performance, it is apparent that the gain factors involved must be carefully considered.

K_n = is 1/32 in the MC13176.

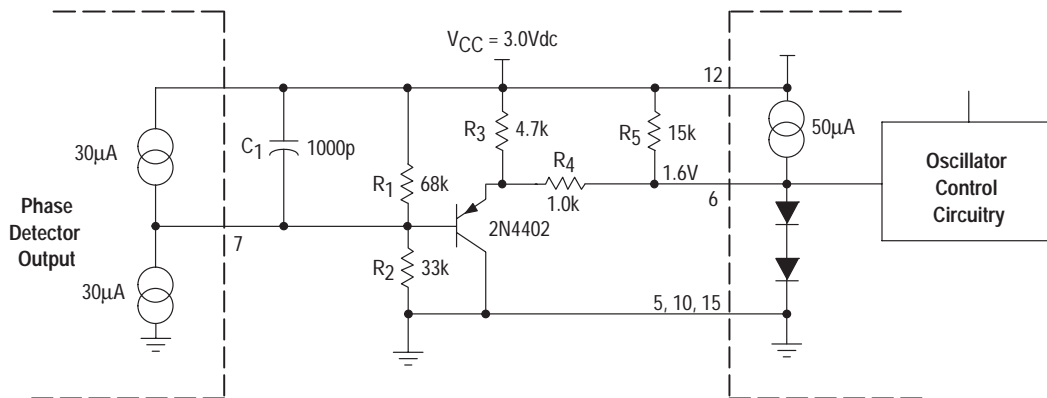
K_p = is fixed internally and cannot be altered.

K_o = Figures 8 and 9 suggest that there is capability of greater control range with more current swing. However, this swing must be symmetrical about the center of the dynamic response. The suggested zero current operating point for $\pm 100 \mu\text{A}$ swing of the CCO is at about $+70 \mu\text{A}$ offset point.

K_a = External loop amplification will be necessary since the phase detector only supplies $\pm 30 \mu\text{A}$.

In the design example in Figure 14, an external resistor (R_5) of 15 k to V_{CC} (3.0 Vdc) provides approximately $100 \mu\text{A}$ of current boost to supplement the existing $50 \mu\text{A}$ internal source current. R_4 (1.0 k) is selected for approximately 0.1 Vdc across it with $100 \mu\text{A}$. R_1 , R_2 and R_3 are selected to set the potential at Pin 7 and the base of 2N4402 at approximately 0.9 Vdc and the emitter at 1.55 Vdc when error current to Pin 6 is approximately zero μA . C_1 is chosen to reduce the level of the crystal sidebands.

Figure 14. External Loop Amplifier

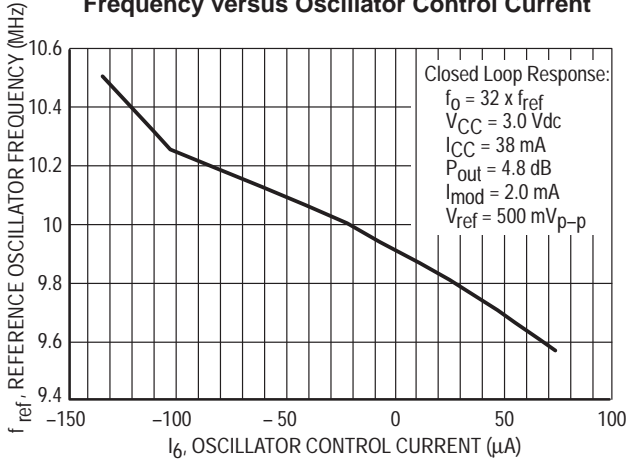


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Figure 15 shows the improved hold-in range of the loop. The Δf_{ref} is moved 950 kHz with over 200 μ A swing of control current for an improved hold-in range of ± 15.2 MHz or ± 95.46 Mrad/sec.

Figure 15. MC13176 Reference Oscillator Frequency versus Oscillator Control Current



Lock-in Range/Capture Range

If a signal is applied to the loop not equal to free running frequency, f_f , then the loop will capture or lock-in the signal by making $f_s = f_o$ (i.e. if the initial frequency difference is not too great). The lock-in range can be expressed as $\Delta\omega_L \sim \pm 2\delta\omega_n$

FM Modulation

Noise external to the loop (phase detector input) is minimized by narrowing the bandwidth. This noise is minimal in a PLL system since the reference frequency is usually derived from a crystal oscillator. FM can be achieved by applying a modulation current superimposed on the control current of the CCO. The loop bandwidth must be narrow enough to prevent the loop from responding to the modulation frequency components, thus, allowing the CCO to deviate in frequency. The loop bandwidth is related to the natural frequency ω_n . In the lag-lead design example where the natural frequency, $\omega_n = 5.0$ krad/sec and a damping factor, $\delta = 0.707$, the loop bandwidth = 1.64 kHz. Characterization data of the closed loop responses at 320 MHz (Figure 7) show satisfactory performance using only a simple low-pass loop filter network. The loop filter response is strongly influenced by the high output impedance of the phase detector.

$$f_c = 0.159/RC;$$

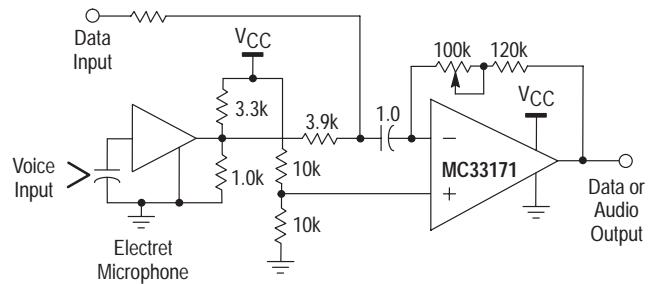
For $R = 1.0 \text{ k} + R_7$ ($R_7 = 53 \text{ k}$) and $C = 390 \text{ pF}$

$$f_c = 7.55 \text{ kHz or } \omega_c = 47 \text{ krad/sec}$$

The application example in Figure 17 of a 320 MHz FM transmitter demonstrates the FM capabilities of the IC. A high value series resistor (100 k) to Pin 6 sets up the current source to drive the modulation section of the chip. Its value is dependent on the peak to peak level of the encoding data and the maximum desired frequency deviation. The data input is AC coupled with a large coupling capacitor which is selected for the modulating frequency. The component placements on the circuit side and ground side of the PC board are shown in Figures 34 and 35, respectively. Figure 19 illustrates the input data of a 10 kHz modulating signal at 1.6 V_{p-p}. Figures 20 and 21 depict the deviation and resulting modulation spectrum showing the carrier null at -40 dBc. Figure 22 shows the unmodulated carrier power output at 3.5 dBm for $V_{CC} = 3.0$ Vdc.

For voice applications using a dynamic or an electret microphone, an op amp is used to amplify the microphone's low level output. The microphone amplifier circuit is shown in Figure 16. Figure 18 shows an application example for NBFM audio or direct FSK in which the reference crystal oscillator is modulated.

Figure 16. Microphone Amplifier



Local Oscillator Application

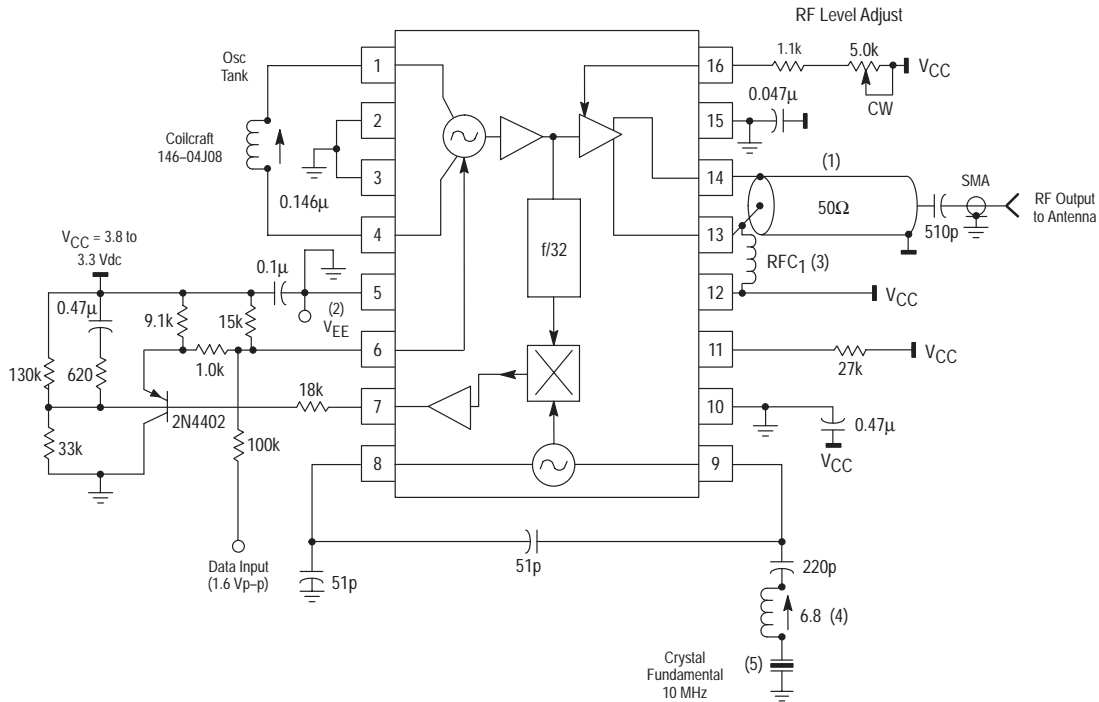
To reduce internal loop noise, a relatively wide loop bandwidth is needed so that the loop tracks out or cancels the noise. This is emphasized to reduce inherent CCO and divider noise or noise produced by mechanical shock and environmental vibrations. In a local oscillator application the CCO and divider noise should be reduced by proper selection of the natural frequency of the loop. Additional low pass filtering of the output will likely be necessary to reduce the crystal sideband spurs to a minimal level.

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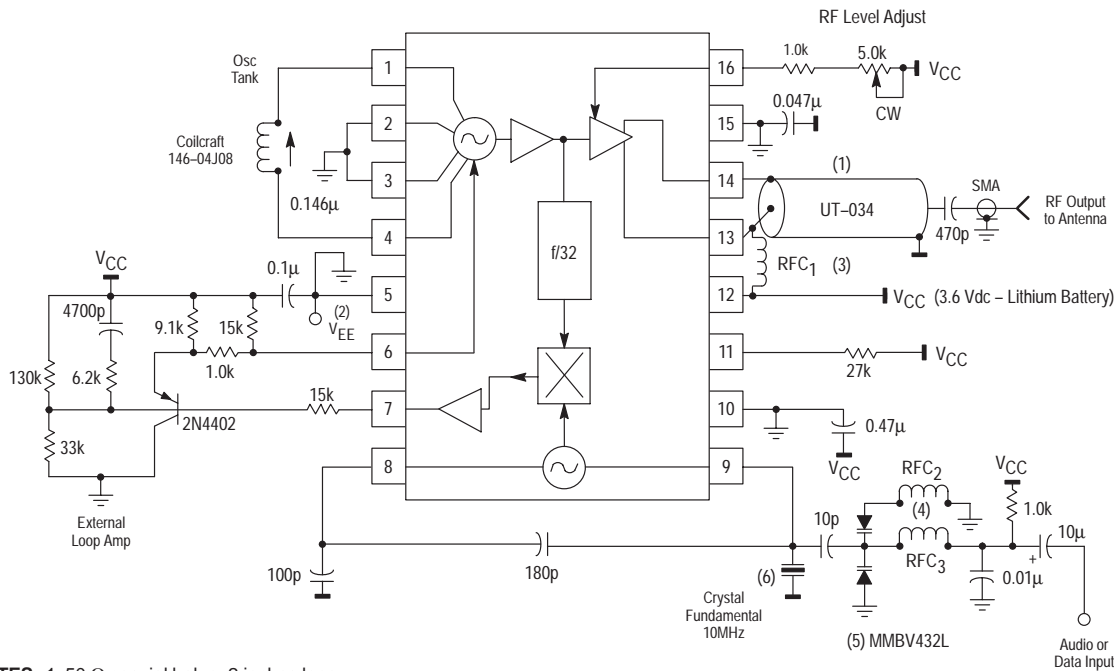
MC13176

Figure 17. 320 MHz MC13176D FM Transmitter



- NOTES:**
1. 50 Ω coaxial balun, 2 inches long.
 - Pins 5, 10 and 15 are grounds and connected to V_{EE} which is the component's side ground plane. These pins must be decoupled to V_{CC} ; decoupling capacitors should be placed as close as possible to the pins.
 - RFC₁ is 180 nH Coilcraft surface mount inductor or 190 nH Coilcraft 146-05J08.
 - Recommended source is a Coilcraft "slot seven" 7.0 mm tuneable inductor, part #7M3-682.
 - The crystal is a parallel resonant, fundamental mode calibrated with 32 pF load capacitance.

Figure 18. 320 MHz NBFM Transmitter



- NOTES:**
1. 50 Ω coaxial balun, 2 inches long.
 - Pins 5, 10 and 15 are grounds and connected to V_{EE} which is the component's side ground plane. These pins must be decoupled to V_{CC} ; decoupling capacitors should be placed as close as possible to the pins.
 - RFC₁ is 180 nH Coilcraft surface mount inductor.
 - RFC₂ and RFC₃ are high impedance crystal frequency of 10 MHz; 8.2 μH molded inductor gives $X_L > 1000 \Omega$.
 - A single varactor like the MV2105 may be used whereby RFC₂ is not needed.
 - The crystal is a parallel resonant, fundamental mode calibrated with 32 pF load capacitance.

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Figure 19. Input Data Waveform

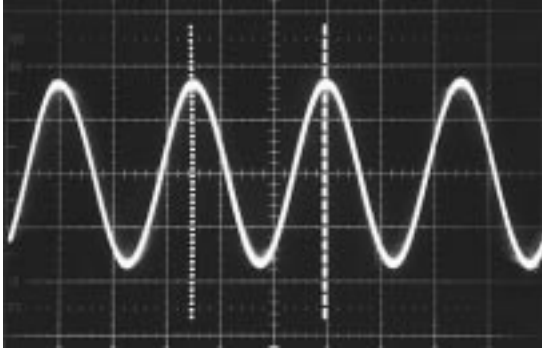


Figure 20. Frequency Deviation



Figure 21. Modulation Spectrum

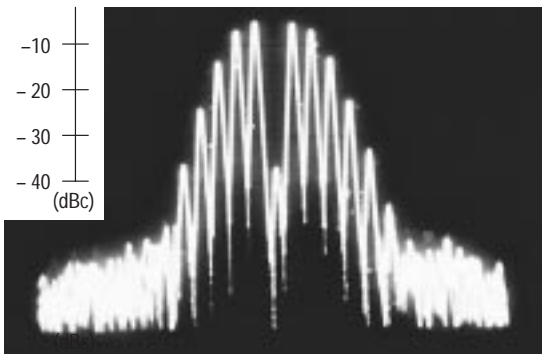


Figure 22. Unmodulated Carrier



Reference Crystal Oscillator (Pins 8 and 9)

Selection of Proper Crystal: A crystal can operate in a number of mechanical modes. The lowest resonant frequency mode is its fundamental while higher order modes are called overtones. At each mechanical resonance, a crystal behaves like a RLC series-tuned circuit having a large inductor and a high Q. The inductor L_S is series resonance with a dynamic capacitor, C_S determined by the elasticity of the crystal lattice and a series resistance R_S , which accounts for the power dissipated in heating the crystal. This series RLC circuit is in parallel with a static capacitance, C_P which is created by the crystal block and by the metal plates and leads that make contact with it.

Figure 23 is the equivalent circuit for a crystal in a single resonant mode. It is assumed that other modes of resonance are so far off frequency that their effects are negligible.

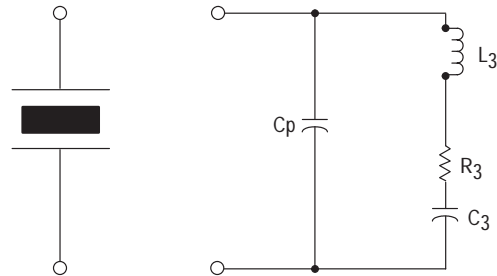
Series resonant frequency, f_S is given by;

$$f_S = 1/2\pi(L_S C_S)^{1/2}$$

and parallel resonant frequency, f_P is given by;

$$f_P = f_S(1 + C_S/C_P)^{1/2}$$

Figure 23. Crystal Equivalent Circuit



the frequency separation at resonance is given by;

$$\Delta f = f_P - f_S = f_S[1 - (1 + C_S/C_P)^{-1/2}]$$

Usually f_P is less than 1% higher than f_S , and a crystal exhibits an extremely wide variation of the reactance with frequency between f_P and f_S . A crystal oscillator circuit is very stable with frequency. This high rate of change of impedance with frequency stabilizes the oscillator, because any significant change in oscillator frequency will cause a large phase shift in the feedback loop keeping the oscillator on frequency.

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Manufacturers specify crystal for either series or parallel resonant operation. The frequency for the parallel mode is calibrated with a specified shunt capacitance called a “load capacitance.” The most common value is 30 to 32 pF. If the load capacitance is placed in series with the crystal, the equivalent circuit will be series resonance at the specified parallel-resonant frequency. Frequencies up to 20 MHz use parallel resonant crystal operating in the fundamental mode, while above 20 MHz to about 60 MHz, a series resonant crystal specified and calibrated for operation in the overtone mode is used.

Application Examples

Two types of crystal oscillator circuits are used in the applications circuits: 1) fundamental mode common emitter Colpitts (Figures 1, 17, 18, and 24), and 2) third overtone impedance inversion Colpitts (also Figures 1 and 24).

The fundamental mode common emitter Colpitts uses a parallel resonant crystal calibrated with a 32 pF load capacitance. The capacitance values are chosen to provide excellent frequency stability and output power of > 500 mVp-p at Pin 9. In Figures 1 and 24, the fundamental mode reference oscillator is fixed tuned relying on the repeatability of the crystal and passive network to maintain the frequency, while in the circuit shown in Figures 17 and 18, the oscillator frequency can be adjusted with the variable inductor for the precise operating frequency.

The reference oscillator can be operated as high as 60 MHz with a third overtone crystal. Therefore, it is possible to use the MC13176 up to 950 MHz (based on the maximum capability of the divider network).

Enable (Pin 11)

The enabling resistor at Pin 11 is calculated by:

$$R_{\text{reg. enable}} = V_{\text{CC}} - 1.0 \text{ Vdc} / I_{\text{reg. enable}}$$

From Figure 4, $I_{\text{reg. enable}}$ is chosen to be 75 μA . So, for a $V_{\text{CC}} = 3.0 \text{ Vdc}$ $R_{\text{reg. enable}} = 26.6 \text{ k}\Omega$, a standard value 27 k Ω resistor is adequate.

Layout Considerations

Supply (Pin 12): In the PCB layout, the V_{CC} trace must be kept as wide as possible to minimize inductive reactance

along the trace; it is best that V_{CC} (RF ground) completely fills around the surface mounted components and interconnect traces on the circuit side of the board. This technique is demonstrated in the evaluation PC board.

Battery/Selection/Lithium Types

The device may be operated from a 3.0 V lithium battery. Selection of a suitable battery is important. Because one of the major problems for long life battery powered equipment is oxidation of the battery terminals, a battery mounted in a clip-in socket is not advised. The battery leads or contact post should be isolated from the air to eliminate oxide build-up. The battery should have PC board mounting tabs which can be soldered to the PCB. Consideration should be given for the peak current capability of the battery. Lithium batteries have current handling capabilities based on the composition of the lithium compound, construction and the battery size. A 1300 mA/hr rating can be achieved in the cylindrical cell battery. The Rayovac CR2/3A lithium-manganese dioxide battery is a crimp sealed, spiral wound 3.0 Vdc, 1300 mA/hr cylindrical cell with PC board mounting tabs. It is an excellent choice based on capacity and size (1.358" long by 0.665" in diameter).

Differential Output (Pins 13, 14)

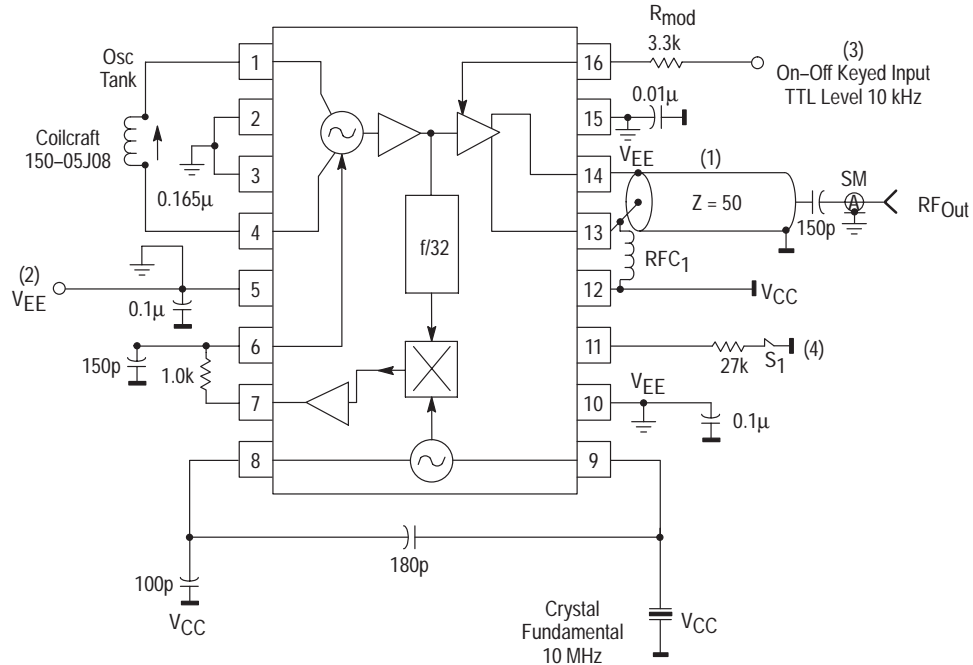
The availability of micro-coaxial cable and small baluns in surface mount and radial-leaded components allows for simple interface to the output ports. A loop antenna may be directly connected with bias via RFC or 50 Ω resistors. Antenna configuration will vary depending on the space available and the frequency of operation.

AM Modulation (Pin 16)

Amplitude Shift Key: The MC13176 is designed to accommodate Amplitude Shift Keying (ASK). ASK modulation is a form of digital modulation corresponding to AM. The amplitude of the carrier is switched between two or more values in response to the PCM code. For the binary case, the usual choice is On-Off Keying (often abbreviated OOK). The resultant amplitude modulated waveform consists of RF pulses called marks, representing binary 1 and spaces representing binary 0.

MC13176

Figure 24. ASK 320 MHz Application Circuit



- NOTES:**
1. 50 Ω coaxial balun, 1/10 wavelength line (1.5") provides the best match to a 50 Ω load.
 2. Pins 5, 10 and 15 are ground and connected to V_{EE} which is the component/DC ground plane side of PCB. These pins must be decoupled to V_{CC}; decoupling capacitors should be placed as close as possible to the pins.

3. The On-Off keyed signal turns the output of the transmitter off and on with TTL level pulses through R_{mod} at Pin 16. The "On" power and I_{CC} is set by the resistor which sets I_{mod} = VTTL - 0.8 / R_{mod}. (see Figure 27).
4. S1 simulates an enable gate pulse from a microprocessor which will enable the transmitter. (see Figure 4 to determine precise value of the enabling resistor based on the potential of the gate pulse and the desired enable.)

Figure 24 shows a typical application in which the output power has been reduced for linearity and current drain. The current draw on the device is 16 mA I_{CC} (average) and -22.5 dBm (average power output) using a 10 kHz modulating rate for the on-off keying. This equates to 20 mA and -2.3 dBm "On", 13 mA and -41 dBm "Off". In Figure 25, the device's modulating waveform and encoded carrier are

displayed. The crystal oscillator enable time is needed to set the acquisition timing. It takes typically 4.0 msec to reach full magnitude of the oscillator waveform (see Figure 26, Oscillator Waveform, at Pin 8). A square waveform of 3.0 V peak with a period that is greater than the oscillator enable time is applied to the Enable (Pin 11).

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

Figure 25. ASK Input Waveform and Modulated Carrier

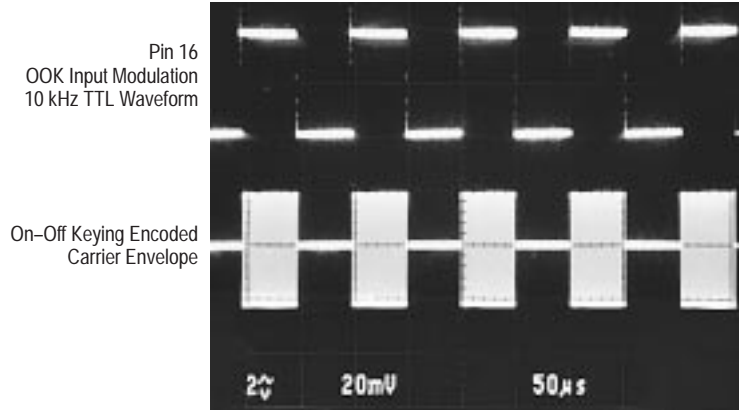


Figure 26. Oscillator Enable Time, Tenable

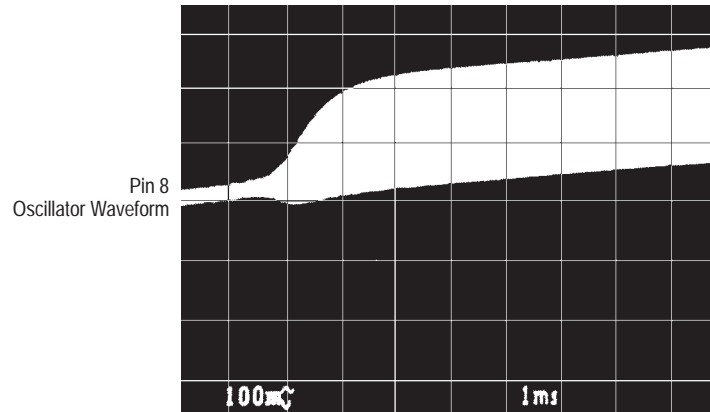
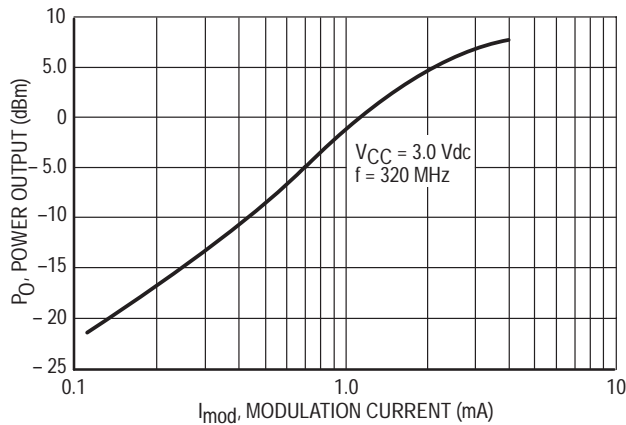


Figure 27. Power Output versus Modulation Current



Analog AM

In analog AM applications, the output amplifier's linearity must be carefully considered. Figure 27 is a plot of Power Output versus Modulation Current at 320 MHz, 3.0 Vdc. In order to achieve a linear encoding of the modulating sinusoidal waveform on the carrier, the modulating signal must amplitude modulate the carrier in the linear portion of its power output response. When using a sinewave modulating signal, the signal rides on a positive DC offset called V_{mod} which sets a static (modulation off) modulation current, I_{mod} . I_{mod} controls the power output of the IC. As the modulating signal moves around this static bias point the modulating current varies causing power output to vary or to be AM modulated. When the IC is operated at modulation current levels greater than 2.0 mA the differential output stage starts to saturate.

NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

In the design example, shown in Figure 28, the operating point is selected as a tradeoff between average power output and quality of the AM.

For $V_{CC} = 3.0\text{Vdc}$; $I_{CC} = 18.5\text{mA}$ and $I_{mod} = 0.5\text{mA}$ and a static DC offset of 1.04Vdc , the circuit shown in Figure 28 completes the design. Figures 29, 30 and 31 show the results of -6.9dBm output power and 100% modulation by the 10kHz and 1.0MHz modulating sinewave signals. The amplitude of the input signals is approximately 800mVp-p .

Where $R_{mod} = (V_{CC} - 1.04\text{Vdc})/0.5\text{mA} = 3.92\text{k}$, use a standard value resistor of 3.9k .

Figure 28. Analog AM Transmitter

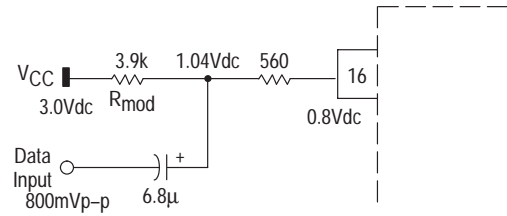


Figure 29. Power Output of Unmodulated Carrier



Figure 30. Input Signal and AM Modulated Carrier for $f_{mod} = 10\text{kHz}$

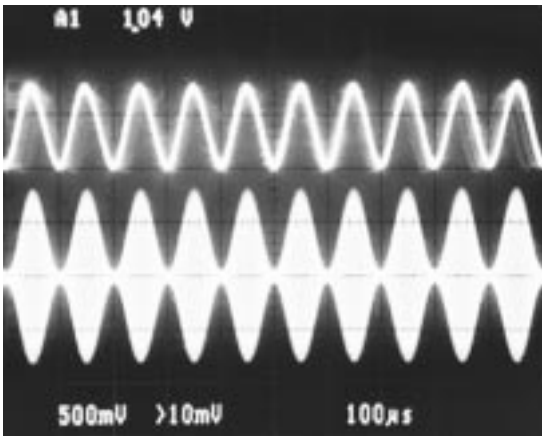
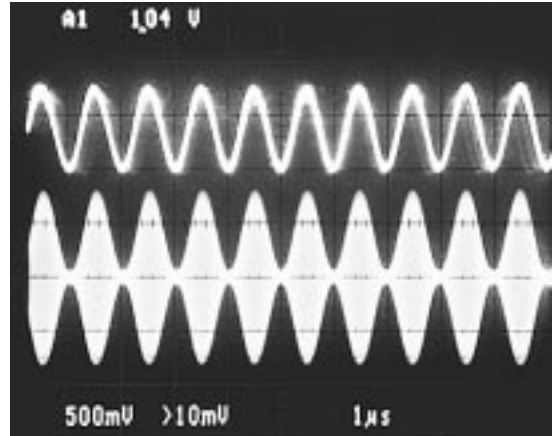


Figure 31. Input Signal and AM Modulated Carrier for $f_{mod} = 1.0\text{MHz}$



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13176

Figure 32. Circuit Side View of MC13176D

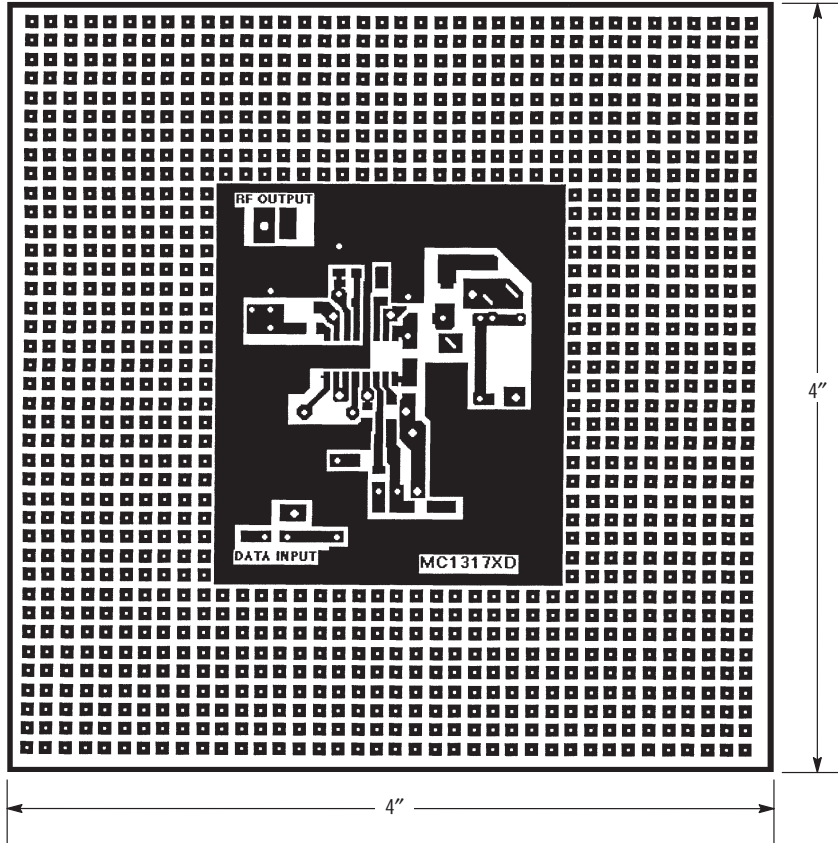
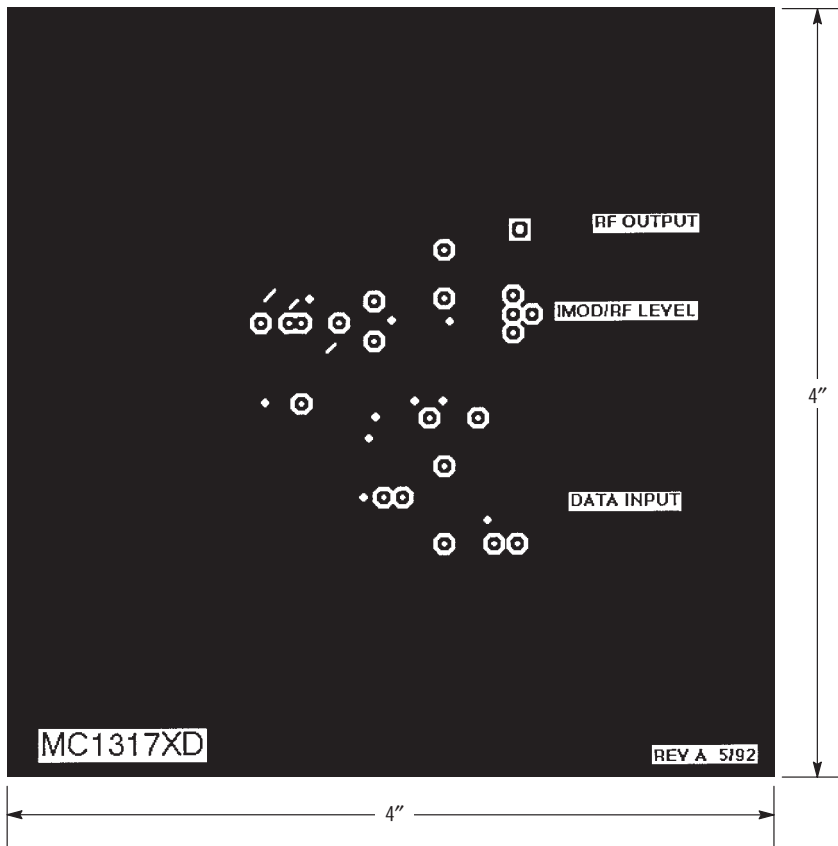


Figure 33. Ground Side View



NOT RECOMMENDED FOR NEW DESIGNS

NOT RECOMMENDED FOR NEW DESIGNS

MC13176

Figure 34. Surface Mounted Components Placement
(on Circuit Side)

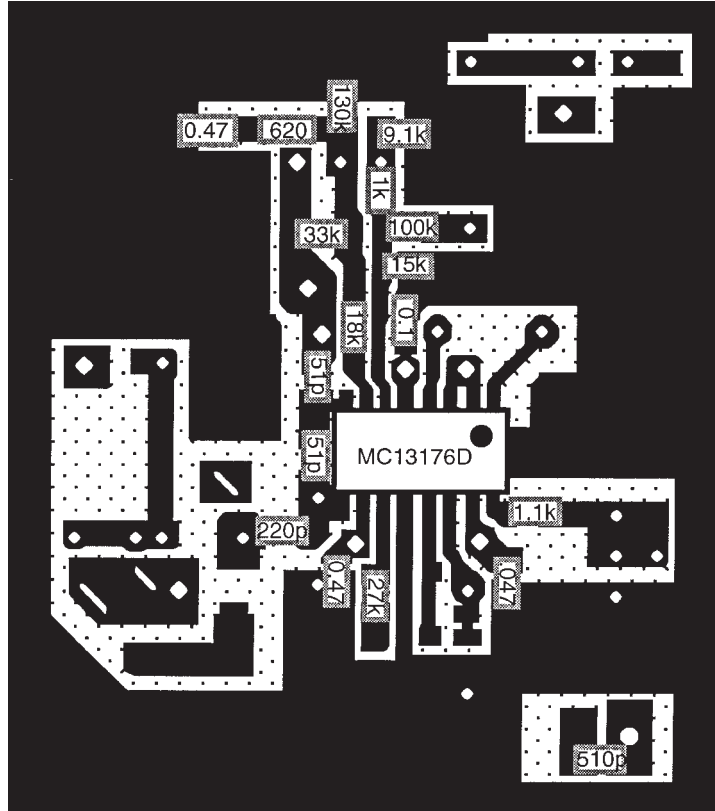
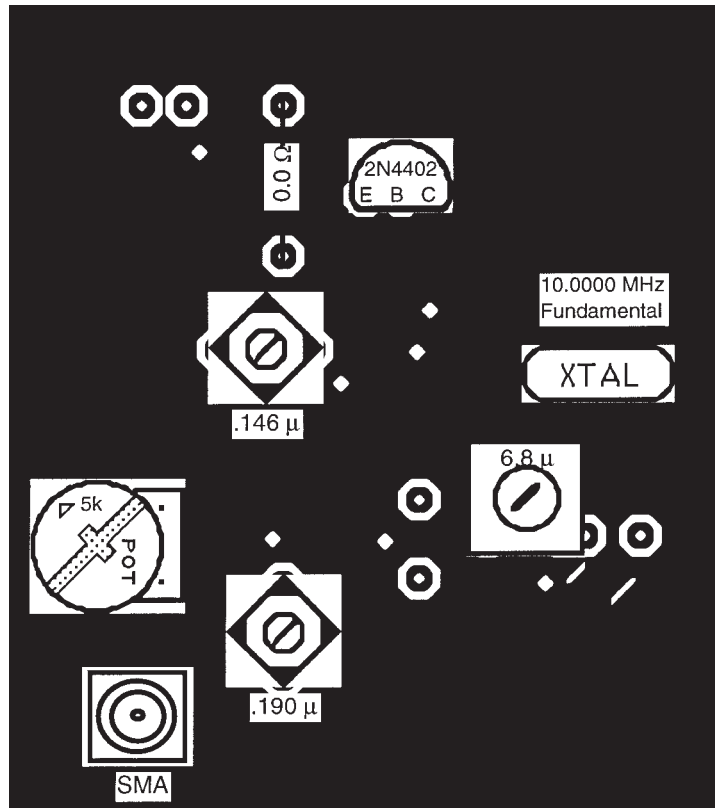


Figure 35. Radial Leaded Components Placement
(on Ground Side)



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NOT RECOMMENDED FOR NEW DESIGNS

Product Preview

GSM/DCS/TDMA/AMPS Multi-Protocol Transceiver

The MC13760 Multi-Protocol, Multi-Band Digital Transceiver IC combines, on a single Advanced BiCMOS chip, the major building blocks required for next generation multi-purpose, multi-band wireless products. The device includes the majority of the circuitry necessary for IF signal processing between the RF front end and the DSP and backend. The MC13760 contains two fractional-N synthesizers, a re-configurable zero IF receiver with programmable bandwidth, receive A/D conversion, multi-rate data interface to the baseband DSP, direct launch digital modulator, full transmit support circuits, and general purpose support circuits such as D/A and A/D converters, battery save and tri-state control switches.

Intended for use in a combined GSM/TDMA/AMPS/iDEN portable wireless phone product in the 800/900/1800/1900 MHz bands. The MC13760 can be used over a wide range of RF and IF frequencies. The main PLL prescaler input is usable to over 2.0 GHz and the IF quadrature downconverter operates up to 400 MHz.

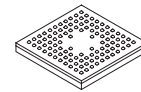
The MC13760 has separate receive IF inputs and a common zero-IF IQ receiver for TDMA and for GSM accommodating the receiver architectural need to use different IF frequencies and filters without the need for additional switches.

- Receiver Functions for all GSM/DCS/TDMA IS-136/AMPS Modes and Frequencies Including GPRS
- Direct Interface to Motorola Baseband Processors, such as the DSP56690 through a Common Programming and Data Interface
- Main Three Accumulator (24-Bit) Fractional-N Synthesizer
 - Resolution Capability of 6.0 Hz
 - Dual-Mode Charge Pump Output for TDMA TX VCO and all RX
 - Independent Charge Pump Output for the GSM/DCS TX VCO
 - GMSK Lookup ROM for Direct Transmission in GSM/DCS Mode
 - Digital 16-Bit Automatic Frequency Control
- Secondary Three Accumulator (24-Bit) Fractional-N Synthesizer for use as an Accurate Frequency-Corrected Clock in GSM, or as an Additional Low Frequency LO
- Coarse Tuning of the VCO(s) via a 6-Bit D/A with Adapt
- Operates at 2.75 V Deep Sleep Mode with Current as low as 50 μ A
- Versatile Frequency Generation including Linear and Constant Envelope Modulation Paths, Ramp and Power Level Control, Direct Gain Control of the RFPA in the TDMA Mode
- D/A Conversion of TDMA TXI and TXQ
- Reference Crystal Oscillator with a Buffered Output, Compensation/Fine Tuning via 9-Bit D/A
- Receiver Gain Adjustment and Bandwidth Down to 6.0 kHz Programmed over the SPI Bus
- A/D Conversion of RXI and RXQ to 8-Bit or 10-Bit Resolution
- Types of Applications
 - GSM/DCS/TDMA/AMPS Global Roaming Multiband Cellular Telephone
 - VHF/UHF 2-Way or Trunked Radio, iDEN, Tetra, or Satellite Communication Radios or Telephones
 - Hand-Held Wireless PDA's
 - Wireless LAN's, Industrial Devices, ISM Band Products
 - Any New Device Containing Some Combination of the Above Functions

MC13760

MULTI-PROTOCOL TRANSCEIVER

SEMICONDUCTOR TECHNICAL DATA



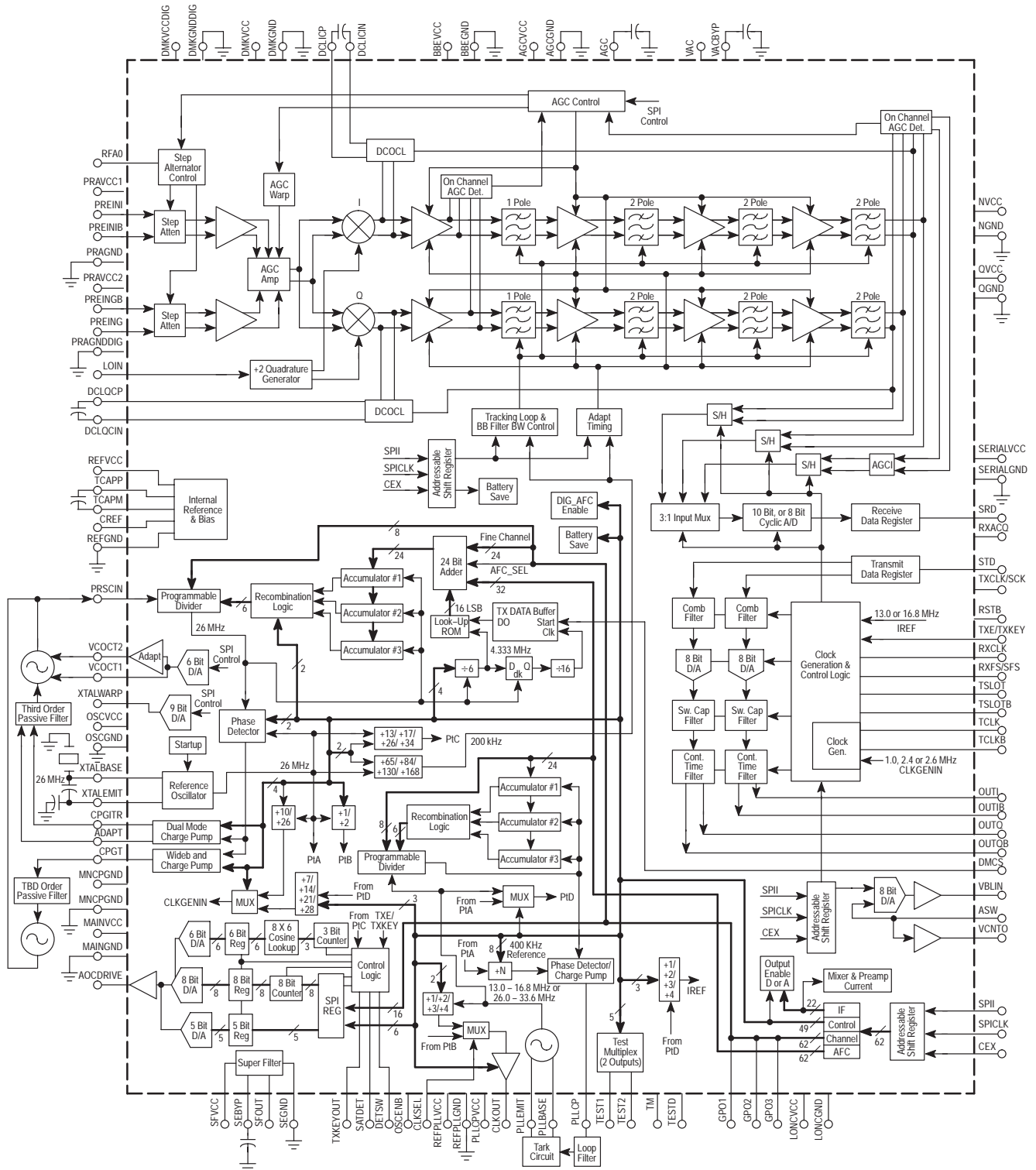
PLASTIC PACKAGE
CASE 1285
(BGA-104)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC13760	T _A = -40 to 85°C	BGA-104

MC13760

Figure 1. MC13760 Detailed Block Diagram



MC13760

Table 1. BGA Contact Identification

BALL #	BALL NAME	DESCRIPTION	SIGNAL TYPE
A1	PRAGNDDIG	Ground for the preamp substrate.	Ground
A2	PRAGND	Ground for the preamp.	Ground
A3	PREINGB	GSM IF preamp input.	RF Input
A4	PREINIB	TDMA IF preamp input.	RF Input
A5	BBFGND	Ground for the baseband filters.	Ground
A6	DCLQCP	DC Offset Correction Loop (input) capacitor – Q channel	Analog Input
A7	CREF	Bypass capacitor for the bandgap regulator.	Analog
A8	OUTQ	TDMA Q channel analog transmit data.	Analog Output
A9	OUTIB	TDMA I channel analog transmit data.	Analog Output
A10	TSLOTB	TDMA low level transmit slot.	Analog Output
A11	TSLOT	TDMA low level transmit slot.	Analog Output
B1	RFA0	RF attenuator 0 control line. (This line is a driver for an external RF attenuator.)	Digital Output
B2	DMXGND	Ground for the mixer.	Ground
B3	PREING	GSM IF preamp input.	RF Input
B4	PREINI	TDMA IF preamp input.	RF Input
B5	PRAVCC2	Supply for the preamp output stage.	Supply 2.775 V
B6	DCLICP	DC Offset Correction Loop (input) capacitor – I channel	Analog Input
B7	GPO3/test_so2	SPI port expansion 3. Or scan data output for MODROM module.	Digital Output
B8	TCAPP	Differential reference capacitor.	Analog
B9	REFGND	Ground for the internal reference.	Ground
B10	REFVCC	Supply for the internal reference.	Supply 2.775 V
B11	TCLK	TDMA low level transmit clock.	Analog Output
C1	DMXVCC	Supply for the mixer.	Supply 2.775 V
C2	DMXGNDDIG	Ground for the mixer substrate and quadrature generator.	Ground
C3	PRAVCC1	Supply for the preamp.	Supply 2.775 V
C4	BBFVCC	Supply for the baseband filters.	Supply 2.775 V
C5	DCLICIN	DC Offset Correction Loop (output) capacitor – TDMA – I channel	Analog Output
C6	DCLQCIN	DC Offset Correction Loop (output) capacitor – TDMA – Q channel	Analog Output
C7	TCAPM	Differential reference capacitor.	Analog
C8	OUTQB	TDMA Q channel analog transmit data.	Analog Output
C9	CLKSEL	Selects the source for the clock output to the digital circuitry of the radio as either the crystal reference/divided crystal reference or the Step Up PLL/divided Step Up PLL. A low on this pin selects the crystal reference/divided crystal reference. A high on this pin selects the Step Up PLL/divided Step Up PLL. Integrated weak pulldown.	Digital Input
C10	TCLKB	TDMA low level transmit clock.	Analog Output
C11	QGND	Quiet analog ground for the PA D/A and the data processing circuits.	Ground
D1	LOIN	Input port for the second LO VCO signal.	RF Input
D2	DMXVCCDIG	Supply for the quadrature generator.	Supply 2.775 V
D3	TEST2/EERQ	Test input/MUX 2 output. (Various signals are buffered and MUX'd to this pin. Output signal is determined by programming of test bits.) Or with EER active, TDMA Q channel transmit data.	Analog Test Point
D4	TEST1/EERI	Test input/MUX 1 output. (Various signals are buffered and MUX'd to this pin. Output signal is determined by programming of test bits.) Or with EER active, TDMA I channel transmit data.	Analog Test Point
D6	PKGGND1	Ground for the package flag (no direct connection to die).	Pkg Ground
D8	OUTI	TDMA I channel analog transmit data.	Analog Output
D9	TESTD/GPO4	Digital test point. (Various digital signals are MUX'd to this pin. Output is determined by programming of test bits.) Or SPI port expansion 4.	Digital Test Point Digital Output

MC13760

Table 1. BGA Contact Identification (continued)

BALL #	BALL NAME	DESCRIPTION	SIGNAL TYPE
D10	QVCC	Quiet analog supply for the PA D/A and the data processing circuits.	Supply 2.775 V
D11	NGND	Noisy analog ground for the VCO D/A, AOC D/A and the data processing circuits.	Ground
E1	VAG	Analog ground.	Analog
E2	AGCGND	Ground for the AGC.	Ground
E3	VAGBYP	Bypass capacitor for the analog ground voltage.	Analog
E9	NVCC	Noisy analog supply for the VCO D/A, AOC D/A and the data processing circuits.	Supply 2.775 V
E10	RSTB	Reset. Low true input. Integrated weak pullup.	Digital Input
E11	TM	Enable for the internal scan test.	Digital Input
F1	AGCVCC	Supply for the AGC.	Supply 2.775 V
F2	TXKEYOUT/test_so4	Conditioned TXKEY out. Or scan data output for reference clock module.	Digital Output
F3	AGC	Capacitor for the TDMA AGC.	Analog
F4	PKGGND2	Ground for the package flag (no direct connection to die).	Pkg Ground
F8	PKGGND3	Ground for the package flag (no direct connection to die).	Pkg Ground
F9	PLLCPVCC	Supply for the Step Up PLL phase detector and charge pump.	Supply 5.0 V
F10	CLKOUT	Clock output to the digital circuitry of the radio. Ranges are 13.0 to 16.8 MHz, or 26.0 to 33.6 MHz. The actual frequency provided will depend upon the configuration of the Step Up PLL and the SPI selected configuration of the MC13760.	Analog Output
F11	PLLCP	Charge pump output for the Step Up PLL.	Analog Output
G1	PRSCIN	Main LO prescaler input.	RF Input
G2	MAINGND	Ground for the main prescaler and divider.	Ground
G3	AOCDRIVE	Output to the PA bias circuitry drive input. (Output drive impedance is 620 Ohms.)	Analog Output
G9	PLLEMIT	Emitter of the oscillator transistor for the Step Up PLL.	RF Output
G10	REFPLLCC	Supply for the Step Up PLL VCO and dividers.	Supply 2.775 V
G11	PLLBASE/vco_clk	Base of the oscillator transistor for the Step Up PLL. Or scan clock input for VCO clock zone.	RF Input
H1	SATDET/test_si4	Input indicating saturation. Or scan data input for reference clock module.	Digital Input
H2	GPO2/test_so8	SPI port expansion 2. Or Main PLL Adapt Timer output. Or scan data output for SSI module.	Digital Output
H3	MAINVCC	Supply for the main prescaler and divider.	Supply 2.775 V
H4	MNCPVCC	Supply for the main phase detector and charge pump.	Supply 5.0 V
H6	PKGGND4	Ground for the package flag (no direct connection to die).	Pkg Ground
H8	TXE/TXKEY/test_si8	Transmit slot enable in TDMA mode; digital input to start/stop the PA Control sequence in GSM mode. Or scan data input for SSI module.	Digital Input
H9	RXACQ/test_si7	Serial bus enable. Or scan data input for 5 bit and 8 bit xtal clock dividers.	Digital Input
H10	REFPLLGND	Ground for the Step Up PLL.	Ground
H11	SERIALVCC	Supply for the SSI and SPI serial communication ports.	Supply 1.8 — 2.775V
J1	GPO1/test_so1	SPI port expansion 1. Or Coarse Tune Adapt Timer output. Or scan data output for main Frac-N.	Digital Output
J2	VCOC2	High current (ADAPT) output of the 6 bit main RX VCO Coarse Tune D/A.	Analog Output
J3	DETSW/test_si1	Output to the PA control circuitry power range input (open drain). Or scan data input for main Frac-N.	Analog Output
J4	SFVCC	Supply for the super filter.	Supply 2.775 V
J5	ASW/sc_inp1	TDMA antenna switch control input. Or scan data input for reference clock Frac-N accumulator module.	Digital Input

MC13760

Table 1. BGA Contact Identification (continued)

BALL #	BALL NAME	DESCRIPTION	SIGNAL TYPE
J6	VCNTO	TDMA RFPA gain control voltage output.	Analog Output
J7	OSCVCC	Supply for the crystal oscillator.	Supply 2.775 V
J8	XTALWARP	Output of the 9 bit WARP D/A to be used for compensation/correction of the reference crystal frequency.	Analog Output
J9	OSCENB	Digital input used to control the crystal oscillator circuit. A logic low selects the internal oscillator. Integrated weak pulldown.	Digital Input
J10	RXCLK/test_so3	SSI RX clock in GSM mode; not used in TDMA mode. Or scan data output for transmit power amp control module.	Digital Output
J11	SRD/test_so6	SSI receive data. Or scan data output for Adapt Generator module.	Digital Output
K1	VCOC1	Low current output of the 6 bit main RX VCO Coarse Tune D/A.	Analog Output
K2	MNCPGND	Ground for the main phase detector and charge pump.	Ground
K3	SFGND	Ground for the super filter.	Ground
K4	SFBYP	Bypass capacitor for the super filter. (1.0 μ f)	Analog
K5	OSCGND	Ground for the crystal oscillator.	Ground
K6	XTALBASE/sc_clk26	Crystal oscillator base. Or scan clock input for xtal clock zone.	RF Input
K7	LOGICVCC	Supply for the main synthesizer logic, adapt control and test MUXs.	Supply 2.775 V
K8	CEX	Digital input that latches in the SPI data. (Low Active)	Digital Input
K9	SPICLK	SPI clock input.	Digital Input
K10	STD/test_si3	SSI transmit data. Or scan data input for transmit.	Digital Input
K11	TXCLK/SCK/test_so5	Bit clock for TX data transfer in GSM mode. Bit clock for RX and TX data transfer in TDMA mode. Or scan data output for reference clock Frac-N accumulator module.	Digital Output
L1	ADAPT	Synthesizer output to adapt the loop filter for the main PLL.	Analog Output
L2	CPGT	Charge pump output for the main TX LO (GSM).	Analog Output
L3	CPGTR	Charge pump output for the main RX LO (GSM, TDMA TX and RX).	Analog Output
L4	SFOUT	Super filter output. (45 mA max) (bypass with 0.01 μ f)	Analog Output
L5	VBLIN	TDMA RFPA bias control voltage output.	Analog Output
L6	XTALEMIT	Crystal oscillator emitter.	RF Output
L7	LOGICGND	Ground for the main synthesizer logic, adapt control and test MUXs.	Ground
L8	SERIALGND	Ground for the SSI and SPI serial communication ports.	Ground
L9	SPII	SPI data input.	Digital Input
L10	DMCS/test_si2	Digital input that starts the GSM TX modulation. Or scan data input for MODROM module.	Digital Input
L11	RXFS/SFS/test_so7	RX SSI frame sync in GSM mode; SSI frame sync in TDMA mode. Or scan data output for 5 bit and 8 bit xtal clock dividers.	Digital Output



MC33411A/B

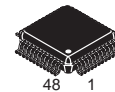
900 MHz Analog Cordless Phone Baseband with Compander

The MC33411 900 MHz Analog Cordless Phone Baseband system is designed to fit the requirements of a 900 MHz analog cordless telephone system. Included are three PLLs (Phase-Locked Loops). Two are intended for use with external VCOs and 64/65 or 128/129 dual modulus prescalers, and can control the transmit and receive (LO1) frequencies for 900 MHz communication. The third PLL is configured as the 2nd local oscillator (LO2), and is functional to 80 MHz. Also included are muting, audio gain adjust (internal and external), low battery/carrier detect, and a wide range for the PLL reference frequency. The power supply range is 2.7 to 5.5 V. "A" version devices have programmable MCU clock out and reference oscillator disable functions, whereas these functions are always enabled for "B" version devices.

- Complete Expander/Compressor for Superior Noise Rejection
- Two PLLs and a LO Suitable for a 900 MHz System
- Minimal External Components
- Transmit Path Includes Adjustable Gain Amplifier, Filters, Mute, Compressor with Bypass and Limiter
- Receive Path Contains Data Slicer, Adjustable Gain Amplifier, Sidetone Attenuator, Filters, Expander with Bypass, Mute, Volume Control and Power Amplifier
- Dual A/Ds are Provided to Monitor RSSI and V_{CC}
- Independent Power Amplifier with Differential Outputs and Mute
- Selectable Frequency for Switched Capacitor Filters, PLLs and the LO
- Reference Frequency Source can be a Crystal or System Clock
- Serial μ P Port to Control Gain, Mute, Frequency Selection, Phase Detector Gain, Power Down Modes, Low Battery Detect and Others
- Power Supply Range: 2.7 to 5.5 V
- Power Down Modes for Power Conservation

900 MHz ANALOG CORDLESS PHONE BASEBAND WITH COMPANDER

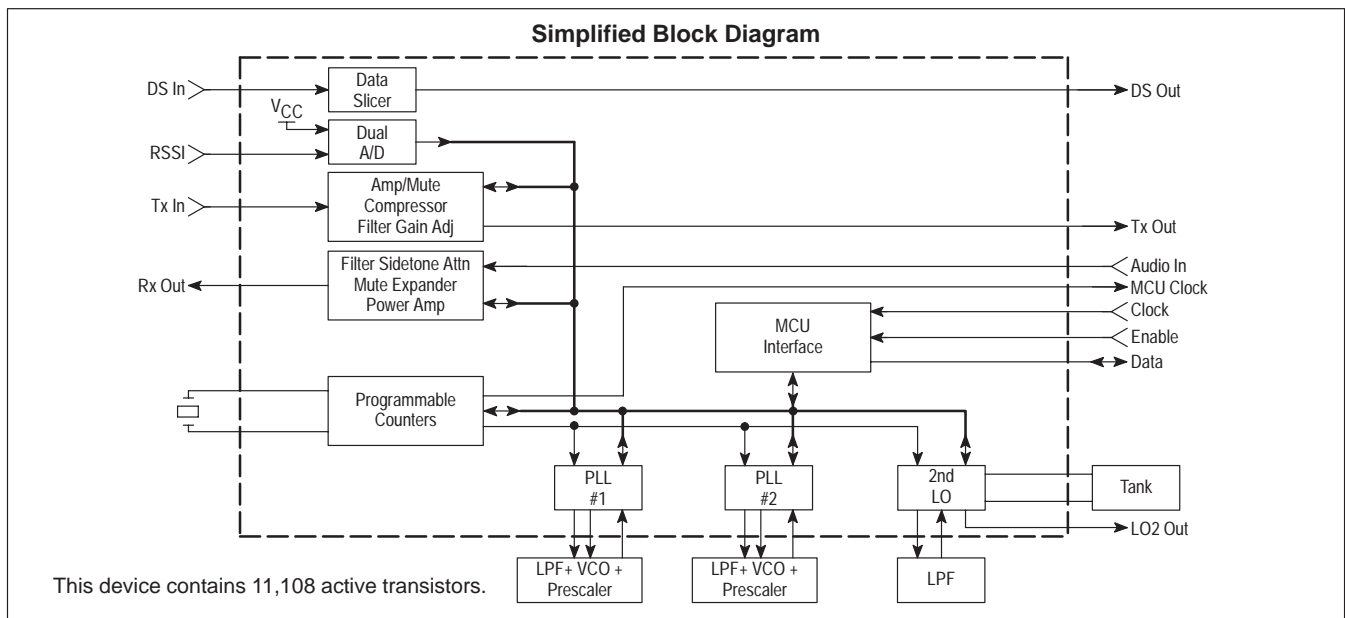
SEMICONDUCTOR TECHNICAL DATA



FTA SUFFIX
PLASTIC PACKAGE
CASE 932
(LQFP-48)

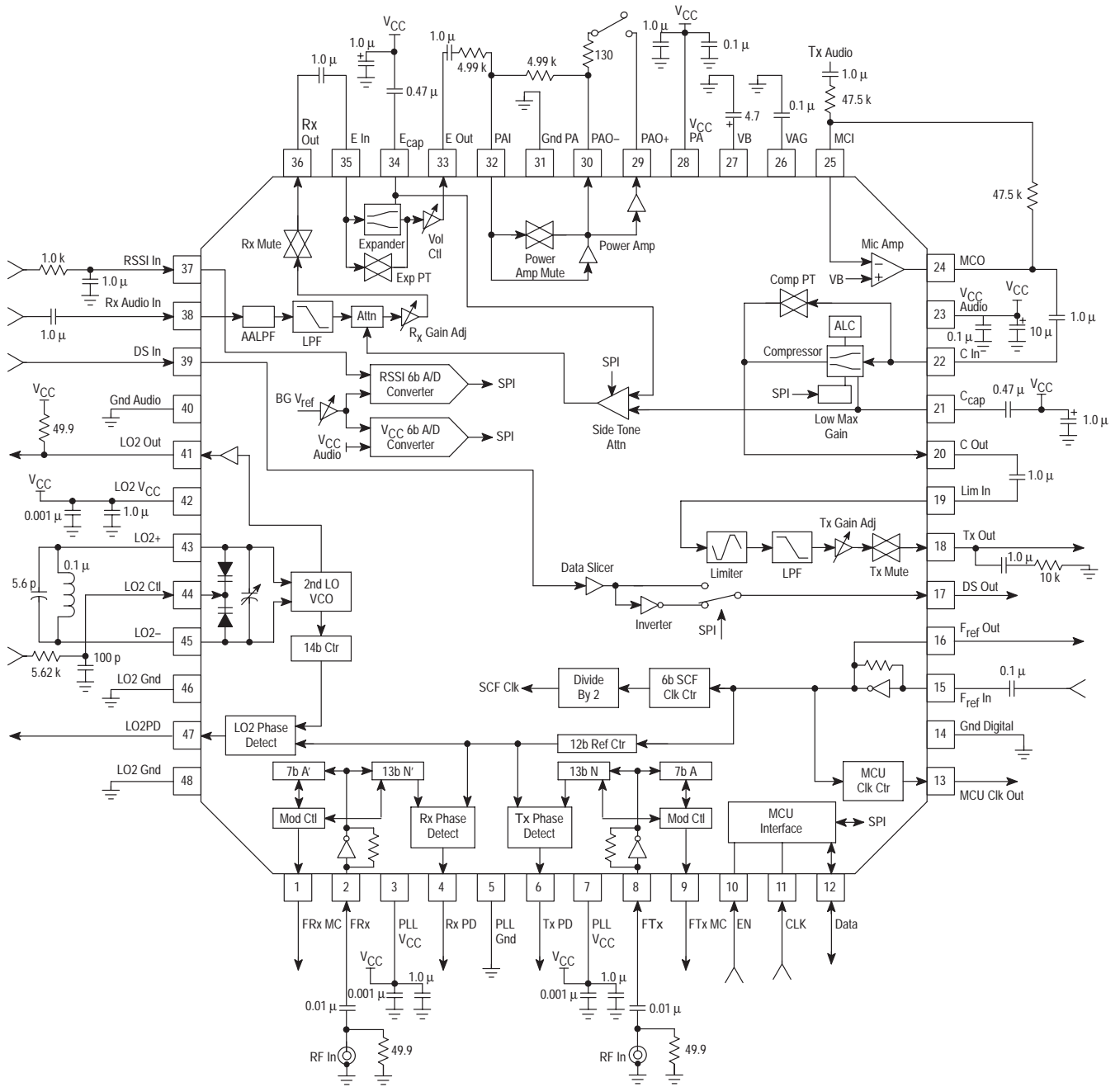
ORDERING INFORMATION

Device	Operating Temperature	Package
MC33411AFTA	T _A = -20 to 70°C	LQFP-48
MC33411BFTA		



MC33411A/B

Figure 1. Test Circuit



MC33411A/B

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Power Supply Voltage	V_{CC}	-0.5 to 6.0	V
Junction Temperature	T_J	-6.5 to 150	°C
Maximum Power Dissipation	P_D	150	mW

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Recommended Operating Conditions, Electrical Characteristics tables or Pin Descriptions section.
2. Meets Human Body Model (HBM) ≤ 2000 V and Machine Model (MM) ≤ 200 V. ESD data available upon request.

RECOMMENDED OPERATING CONDITIONS

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Voltage	V_{CC}	2.7	3.6	5.5	Vdc
Operating Ambient Temperature	T_A	-20	-	70	°C
Input Voltage Low (Data, CLK, EN)	V_{il}	-	-	0.3	V
Input Voltage High (Data, CLK, EN)	V_{ih}	Tx PLL $V_{CC} - 0.3$	-	-	V
Frequency Range (F_{ref} in)	F_{range}	4.0	-	18.25	MHz
Bandgap Reference Voltage	V_B	-	1.5	-	V

DC ELECTRICAL CHARACTERISTICS ($V_{CC} = 3.6$ V, $T_A = 25^\circ\text{C}$, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Static Current					
Active Mode ($R5/8$ to $0 = 0$; $R6/7 = 0$)	ACT I_{CC}	-	15	20	mA
Receive Mode ($R5/8, 7, 3, 2, 0 = 0$; $R6/7 = 0$; $R5/6, 5, 4, 1 = 1$)	Rx I_{CC}	-	10	13	mA
Standby Mode ($R5/0 = 0$; $R6/7 = 0$; $R5/8$ to $1 = 1$)	STD I_{CC}	-	500	1500	μA
Inactive Mode, A only ($R5/8$ to $0 = 1$; $R6/7 = 1$)	INA I_{CC}	-	10	15	μA
Data Slicer Only	DS I_{CC}	-	100	-	μA
RSSI/Batt A/D Only	AD I_{CC}	-	70	-	μA
Tx Audio Only	TxA I_{CC}	-	1.4	-	mA
Rx Audio Only	RxA I_{CC}	-	1.4	-	mA
PA Only	PA I_{CC}	-	1.0	-	mA
2nd LO/ F_{ref} Only	2LO I_{CC}	-	6.0	-	mA
Rx PLL/ F_{ref} Only	RxPLL I_{CC}	-	1.0	-	mA
Tx PLL/ F_{ref} Only	TxPLL I_{CC}	-	1.0	-	mA
Ref Osc Only, "A" version only	ROSC I_{CC}	-	500	-	μA
Reference Voltage, Unadjusted	V_B	1.38	1.5	1.62	V

ELECTRICAL CHARACTERISTICS ($V_{CC} = 3.6$ V, $V_B = 1.5$ V, $T_A = 25^\circ\text{C}$, Active Mode, Rx Gain = 01111, Vol Adj = 0111, $f_{in} = 1.0$ kHz, unless otherwise noted.)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
-----------------	-----------	-------------	--------	-----	-----	-----	------

Rx AUDIO PATH

Absolute Gain ($V_{in} = -20$ dBV)	Rx Audio In	E Out	G	-4.0	0	4.0	dB
Gain Tracking (Referenced to E_{out} for $V_{in} = -20$ dBV)	E In	E Out	G_t				dB
$V_{in} = -30$ dBV				-21	-20	-19	
$V_{in} = -40$ dBV				-42	-40	-38	
Total Harmonic Distortion ($V_{in} = -20$ dBV)	Rx Audio In	PAO-	THD	-	0.7	1.0	%
Maximum Input Voltage ($V_{CC} = 2.7$ V)	Rx Audio In			-	-11.5	-	dBV
Maximum Output Voltage (Increase input voltage until output voltage THD = 5%, then measure output voltage)	E In	E Out	V_{Omax}	-2.0	0	-	dBV

- NOTES:** 1. Values specified are pure numbers to the base 10.
2. Typical performance parameters indicate the potential of the device under ideal operating conditions.

MC33411A/B

ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode, Rx Gain = 01111, Vol Adj = 0111, $f_{in} = 1.0\text{ kHz}$, unless otherwise noted.)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
Rx AUDIO PATH (continued)							
Input Impedance		RxAudio In E In	Z_{in}	– –	600 7.5	– –	$k\Omega$
Attack Time $E_{cap} = 0.5\ \mu\text{F}$, $R_{filt} = 40\text{ k}$	E In	E Out	t_a	–	3.0	–	mS
Release Time $E_{cap} = 0.5\ \mu\text{F}$, $R_{filt} = 40\text{ k}$	E In	E Out	t_r	–	13.5	–	mS
Compressor to Expander Crosstalk ($V_{in} = -10\text{ dBV}$, $V_{E\ In} = \text{AC Gnd}$)	MCI	E Out	C_T	–	-90	-60	dB
Rx Muting ($V_{in} = -20\text{ dBV}$, Rx Gain Adj = 01111)	Rx Audio In	E Out	M_e	–	-84	-60	dB
Rx High Frequency Corner ($V_{in} = -20\text{ dBV}$) SCF Counter = 31 _d	Rx Audio In	Rx Out	Rx f_{ch}	3.6	3.8	4.0	kHz
Low Pass Filter Passband Ripple ($V_{in} = -20\text{ dBV}$)	Rx Audio In	Rx Out	Ripple	–	0.4	0.6	dB
Rx Gain Adjust Range	Rx Audio In	Rx Out	Rx Range	–	-9.0 to 10	–	dB
Rx Gain Adjust Steps	Rx Audio In	Rx Out	Rx n	–	20	–	
Audio Path Noise, C-Message Weighting ($V_{in} = \text{AC Gnd}$)	Rx Audio In	Rx Out E Out PA Out	EN	– – –	-85 <-95 <-95	– – –	dBV
Volume Control Adjust Range	Rx Audio In	E Out	$V_{CtRange}$	–	-14 to 16	–	dB
Volume Control Levels	E In	E Out	V_{cn}	–	16	–	
Side Tone Attenuate Selections	Rx Audio In	Rx Out	STA_n	–	4	–	
Side Tone Attenuate (Referenced to E In) Selection = 00 Selection = 01 Selection = 10 Selection = 11		E Out	STA	– – – –	0.0 1.5 3.0 5.2	– – – –	dB
Side Tone Attenuate Threshold (C Out/E In)			STA_{thr}	–	-3.0	–	dB

POWER AMP/MUTE ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode, $f_{in} = 1.0\text{ kHz}$)

Output Swing, $\pm 5.0\text{ mA}$ load (V_{PAO+} @ -5.0 mA – V_{PAO+} @ 5.0 mA)	PAI	PAO+	V_{Omax}	1.3	2.4	–	V_{pp}
Output Swing, $\pm 5.0\text{ mA}$ load (V_{PAO-} @ -5.0 mA – V_{PAO-} @ 5.0 mA)	PAI	PAO–	V_{Omax}	1.3	2.4	–	V_{pp}
Output Swing, No Load	PAI	PAO+	V_{Omax}	–	2.7	–	V_{pp}
Output Swing, No Load	PAI	PAO–	V_{Omax}	–	2.7	–	V_{pp}
Maximum Output Current		PAO–, PAO+	I_{Omax}	–	± 5.0	–	mA
Power Amp Mute ($V_{in} = -20\text{ dBV}$, $R_L = 130\ \Omega$)	PAI	PAO–	M_{sp}	–	-92	-60	dB

MIC AMP ($V_{CC} = 3.6\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode, $f_{in} = 1.0\text{ kHz}$)

Open Loop Gain	MCI	MCO	AVOL	–	100.000	–	V/V
Gain Bandwidth	MCI	MCO	GBW	–	100	–	kHz
Maximum Output Swing ($R_L = 10\text{ k}\Omega$)	MCI	MCO	V_{Omax}	–	3.2	–	V_{pp}

- NOTES:** 1. Values specified are pure numbers to the base 10.
2. Typical performance parameters indicate the potential of the device under ideal operating conditions.

MC33411A/B

ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode, Rx Gain = 01111, Vol Adj = 0111, $f_{in} = 1.0\text{ kHz}$, unless otherwise noted.)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
Tx AUDIO PATH ($V_{CC} = 3.6\text{ V}$, Limiter, Mutes, ALC disabled, $T_A = 25^\circ\text{C}$, Gain = 1, Active Mode, $f_{in} = 1.0\text{ kHz}$)							
Absolute Gain ($V_{in} = -10\text{ dBV}$)	MCI	Tx Out	G	-4.0	0	4.0	dB
Gain Tracking (Referenced to Tx Out for $V_{in} = -10\text{ dBV}$) $V_{in} = -30\text{ dBV}$ $V_{in} = -40\text{ dBV}$	MCI	Tx Out	G_t	-11 -17	-10 -15	-9.0 -13	dB
Total Harmonic Distortion ($V_{in} = -10\text{ dBV}$)	MCI	Tx Out	THD	-	0.5	1.2	%
Maximum Output Voltage (Increase input voltage until output voltage THD = 5%, then measure output voltage. Tx Gain Adj = 8.0 dB)	MCI	Tx Out	V_{Omax}	-8.0	-5.0	-	dBV
Input Impedance		C In	Z_{in}	-	10	-	$k\Omega$
Attack Time $C_{cap} = 0.5\ \mu\text{F}$, $R_{filt} = 40\text{ k}$	C In	Tx Out	t_a	-	3.0	-	mS
Release Time $C_{cap} = 0.5\ \mu\text{F}$, $R_{filt} = 40\text{ k}$	C In	Tx Out	t_r	-	13.5	-	mS
Expander to Compressor Crosstalk ($V_{in} = -20\text{ dBV}$, PA no load, $V_{Cin} = \text{AC Gnd}$)	E In	Tx Out	C_T	-	-60	-40	dB
Tx Muting ($V_{in} = -10\text{ dBV}$)	MCI	Tx Out	M_C	-	-88	-60	dB
ALC Output Level (When Enabled) $V_{in} = -10\text{ dBV}$ $V_{in} = -2.5\text{ dBV}$	MCI	Tx Out	ALC _{out}	-15 -13	-13 -11	-8.0 -6.0	dBV
ALC Slope (When Enabled) $V_{in} = -10\text{ dBV}$ $V_{in} = -2.5\text{ dBV}$	MCI	Tx Out	Slope	0.1	0.25	0.4	dB/dB
ALC Input Dynamic Range	C In	Tx Out	DR	-	-16 to -2.5	-	dBV
Limiter Output Level (When Enabled, $V_{in} = -2.5\text{ dBV}$)	Lim In	Tx Out	V_{lim}	-10	-7.0	-	dBV
Tx High Frequency Corner ($V_{in} = -10\text{ dBV}$, Unity Gain) SCF Counter = 31 _d	Lim In	Tx Out	Tx f_{ch}	3.45	3.65	3.85	kHz
Low Pass Filter Passband Ripple ($V_{in} = -10\text{ dBV}$)	Lim In	Tx Out	Ripple	-	0.4	1.0	dB
MCU Clock or SCF Spurs ($V_{in} = -10\text{ dBV}$, relative to SCF or MCU Fundamental)	Lim In	Tx Out	-	-	-25	-	dBc
Maximum Compressor Gain ($V_{in} = -70\text{ dBV}$) $R6/8 = 0$ $R6/8 = 1$	MCI	Tx Out	AV_{max}	- -	21 12	- -	dB
Tx Gain Adjust Range	Lim In	Tx Out	Tx Range	-	-9.0 to 10	-	dB
Tx Gain Adjust Steps	Lim In	Tx Out	Tx N	-	20	-	

DATA AMP COMPARATOR ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or Receive Mode)

Hysteresis	DS In	DS Out	Hys	20	42	60	mV
Threshold Voltage	DS In	DS Out	V_T	-	$V_{CC} - 0.7$	-	V
Input Impedance		DS In	Z_{in}	200	250	280	$k\Omega$
Output Impedance		DS Out	Z_{out}	-	100	-	$k\Omega$
Output High Voltage ($V_{in} = V_{CC} - 1.0\text{ V}$, $I_{oh} = 0\text{ mA}$)	DS In	DS Out	V_{oh}	V_{CC} Audio - 0.1	V_{CC} Audio	-	V
Output Low Voltage ($V_{in} = V_{CC} - 0.4\text{ V}$, $I_{ol} = 0\text{ mA}$)	DS In	DS Out	V_{ol}	-	0.1	0.4	V
Maximum Frequency	DS In	DS Out	F_{max}	-	10	-	kHz

- NOTES:** 1. Values specified are pure numbers to the base 10.
2. Typical performance parameters indicate the potential of the device under ideal operating conditions.

MC33411A/B

ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode, Rx Gain = 01111, Vol Adj = 0111, $f_{in} = 1.0\text{ kHz}$, unless otherwise noted.)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
RSSI/LOW BATTERY A/D ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or Receive Mode)							
RSSI Voltage Range Minimum (R5/17–12 = 0) Interim (R5/17–12 = 100000) Maximum (R5/17–12 = 1)	RSSI In	SPI	RSSI Range	– .744 –	0 – 1.6	– .792 –	V
Low Battery Detect Operating Range Minimum Interim (R5/23–18 = 101111) Maximum (R5/23–18 = 1)	V_{CC} Audio	SPI	LOWB Range	– 2.7 –	2.7 – 3.75	– 3.1 –	V
Differential Non-linearity	RSSI In/ V_{CC} Audio	SPI	A/D DNL	–1.0	± 0.5	1.0	LSB
Resolution	RSSI In/ V_{CC} Audio	SPI	Resolution	–	6	–	Bits
Input Current		RSSI In	I_{in}	–80	20	80	nA

REFERENCE FREQUENCY ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode)

Input Current High ($V_{in} = V_{CC}$)		$F_{ref\ in}$	I_{ih}	2.0	5.0	15	μA
Input Current Low ($V_{in} = 0\text{ V}$)		$F_{ref\ in}$	I_{il}	–15	–5.0	–2.0	μA
Minimum Input Voltage $F_{ref\ In}$	$F_{ref\ in}$	$F_{ref\ out}$	V_{in}	300	–	–	mVpp
Input Impedance		$F_{ref\ in}$	Z_{in}	–	2.9 pF 11.6 k Ω	–	
Output Impedance		$F_{ref\ out}$	Z_{out}	–	2.5 pF 4.5 k Ω	–	

MICROPROCESSOR INTERFACE ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or Receive Mode)

Input Low Voltage	Data/EN /CLK		V_{il}	0	–	0.3	V
Input High Voltage	Data/EN /CLK		V_{ih}	Tx PLL $V_{CC} - 0.3$	–	Tx PLL V_{CC}	V
Input Current Low ($V_{in} = 0.3\text{ V}$, Standby Mode) Data, EN, CLK		Data, EN, CLK	I_{il}	–5.0	0.4	–	μA
Input Current High ($V_{in} = 3.3\text{ V}$, Standby Mode) Data, EN, CLK		Data, EN, CLK	I_{ih}	–	1.6	5.0	μA
Hysteresis Voltage Data, EN, CLK		Data, EN, CLK	V_{hys}	–	1.0	–	V
Maximum Clock Frequency	CLK		F_{max}	2.0	–	–	MHz
Input Capacitance Data, EN, CLK		Data, CLK, EN	C_{in}	–	8.0	–	pF
EN to CLK Setup Time		EN, CLK	t_{suEC}	–	200	–	nS
Data to CLK Setup Time		Data, CLK	t_{suDC}	–	100	–	nS
Hold Time		Data, CLK	t_h	–	90	–	nS
Recovery Time		EN, CLK	t_{rec}	–	90	–	nS
Input Pulse Width		EN, CLK	t_w	–	100	–	nS
MCU Interface Power-Up Delay			t_{puMCU}	–	100	–	μS
Output High Voltage ($I_{oh} = 0\text{ mA}$)		MCU Clk Out	V_{oh}	Tx PLL $V_{CC} - 0.3$	3.5	–	V

NOTES: 1. Values specified are pure numbers to the base 10.

2. Typical performance parameters indicate the potential of the device under ideal operating conditions.

MC33411A/B

ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode, Rx Gain = 01111, Vol Adj = 0111, $f_{in} = 1.0\text{ kHz}$, unless otherwise noted.)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
MICROPROCESSOR INTERFACE ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or Receive Mode)							
Output Low Voltage ($I_{ol} = 0\text{ mA}$)		MCU Clk Out	V_{ol}	–	0.1	0.3	V
Output High Voltage ($I_{oh} = 0\text{ mA}$)		Data	V_{oh}	Tx PLL $V_{CC} - 0.3$	3.5	–	V
Output Low Voltage ($I_{ol} = 0\text{ mA}$)		Data	V_{ol}	–	0.1	0.3	V

Rx/Tx PLL CHARACTERISTICS ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active or Receive Mode)

Output Source Current ($V_{PD} = 0.5\text{ V}$ or $V_{CC} - 0.5\text{ V}$) $\pm 100\text{ }\mu\text{A}$ mode $\pm 400\text{ }\mu\text{A}$ mode		Rx PD & Tx PD	I_{oh}	–130 –520	–100 –400	–70 –280	μA
Output Sink Current ($V_{PD} = 0.5\text{ V}$ or $V_{CC} - 0.5\text{ V}$) $\pm 100\text{ }\mu\text{A}$ mode $\pm 400\text{ }\mu\text{A}$ mode		Rx PD & Tx PD	I_{ol}	70 280	100 400	130 520	μA
Current Match, $\pm 100\text{ }\mu\text{A}$ mode or $\pm 400\text{ }\mu\text{A}$ mode, $V_{PD} = V_{CC} / 2$ (i.e., $100 \times (\text{ABS}(I_{oh} / I_{ol}))$)		Rx PD Tx PD	Match	80	100	125	%
Output Off Current ($V_{PD} = V_{CC} / 2$), $\pm 100\text{ }\mu\text{A}$ mode or $\pm 400\text{ }\mu\text{A}$ mode		Rx PD Tx PD	I_{oz}	–80	5.0	80	nA
Input Current Low ($V_{in} = 0\text{ V}$)		FRx FTx	I_{il}	–10	–7.5	–	μA
Input Current High ($V_{in} = V_{CC}$)		FRx FTx	I_{ih}	–	10	14	μA
Input Bias Voltage		FRx FTx	V_{bias}	–	1.5	–	V
Output Voltage High ($I_{oh} = 0\text{ mA}$, Voltage Mode)		FRxMC	V_{oh}	–	Rx PLL $V_{CC} - 0.1$	–	V
Output Voltage High ($I_{oh} = 0\text{ mA}$, Voltage Mode)		FTxMC	V_{oh}	–	Tx PLL $V_{CC} - 0.1$	–	V
Output Voltage Low ($I_{ol} = 0\text{ mA}$, Voltage Mode)		FRxMC FTxMC	V_{ol}	–	0.1	–	V
Output Current High ($V_{oh} = 0.8\text{ V}$, Current Mode)		FRxMC FTxMC	I_{oh}	–130	–100	–70	μA
Output Current Low ($V_{ol} = 0.8\text{ V}$, Current Mode)		FRxMC FTxMC	I_{ol}	70	100	130	μA
Maximum Input Frequency		FRx FTx	F_{max}	20	–	–	MHz
Input Voltage Swing		FRx FTx	V_{in}	200	–	1200	mVpp
Modulus Control Prop Delay	FRx FTx	FRxMC FTxMC	–	–	20	–	nS

LO2 PLL CHARACTERISTICS ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode)

Output Source Current ($V_{PD} = 0.5\text{ V}$ or $V_{CC} - 0.5\text{ V}$) $\pm 100\text{ }\mu\text{A}$ mode $\pm 400\text{ }\mu\text{A}$ mode		LO2PD	I_{oh}	–130 –520	–100 –400	–70 –280	μA
Output Sink Current ($V_{PD} = 0.5\text{ V}$ or $V_{CC} - 0.5\text{ V}$) $\pm 100\text{ }\mu\text{A}$ mode $\pm 400\text{ }\mu\text{A}$ mode		LO2PD	I_{ol}	70 280	100 400	130 520	μA
Current Match, $\pm 100\text{ }\mu\text{A}$ mode or $\pm 400\text{ }\mu\text{A}$ mode, $V_{PD} = V_{CC} / 2$ (i.e., $100 \times (\text{ABS}(I_{oh} / I_{ol}))$)		LO2PD	Match	80	100	125	%

- NOTES:** 1. Values specified are pure numbers to the base 10.
2. Typical performance parameters indicate the potential of the device under ideal operating conditions.

MC33411A/B

ELECTRICAL CHARACTERISTICS (continued) ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode, Rx Gain = 01111, Vol Adj = 0111, $f_{in} = 1.0\text{ kHz}$, unless otherwise noted.)

Characteristics	Input Pin	Measure Pin	Symbol	Min	Typ	Max	Unit
LO2 PLL CHARACTERISTICS ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode)							
Output Off Current ($V_{PD} = V_{CC}/2$)		LO2PD	I_{oz}	-80	5.0	80	nA
Input Current Low ($V_{in} = 0.5\text{ V}$)		LO2Ctl	I_{ij}	-1.0	-0.02	-	μA
Input Current High ($V_{in} = V_{CC} - 0.5\text{ V}$)		LO2Ctl	I_{ih}	-	0.02	1.0	μA
Input Voltage Range		LO2Ctl	V_{range}	0.4	-	V_{CC}	V
Maximum 2nd LO Frequency				65	80	-	MHz
LO2 Out Drive (25 Ω load)			V_{out}	112	180	245	mVpp

COUNTERS ($V_{CC} = 3.6\text{ V}$, $V_B = 1.5\text{ V}$, $T_A = 25^\circ\text{C}$, Active Mode)

12–Bit Reference Counter Range [Note 1]				-	3 to 4095	-	
13–Bit N Counter Range [Note 1]				-	3 to 8191	-	
7–Bit A Counter Range [Note 1] 64/65 Modulus Prescaler 128/129 Modulus Prescaler				-	0 to 63 0 to 127	-	
14–Bit LO2 Counter Range [Note 1]				-	12 to 16383	-	
6–Bit Counters (for SCF) [Note 1]				-	3 to 63	-	

- NOTES:** 1. Values specified are pure numbers to the base 10.
2. Typical performance parameters indicate the potential of the device under ideal operating conditions.

PIN FUNCTION DESCRIPTION

Pin	Symbol/Type	Description	Description
1	FRx MC (Output)		Modulus Control Output for the Rx PLL section. Can be set to output in current mode or voltage mode, selectable with bit 3/16.
2	FRx (Input)		Receives the signal from the external 64/65 or 128/129 prescaler. DC bias is at 1.3 V.

NOTE: 1. All V_{CC} pins must be within $\pm 0.5\text{ V}$ of each other.

MC33411A/B

PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
3	Rx PLL V _{CC} (Input)		Supply pin for the Rx PLL section. Allowable range is 2.7 to 5.5 V and must be within 0.5 V of all other V _{CC} pins. Good bypassing is required and isolation with a 10 Ω resistor is recommended.
4	Rx PD (Output)		Rx Phase Detector Output. The output either sources or sinks current, or neither, depending on the phase difference of the phase detector input signals. During lock, very narrow pulses with a frequency equal to the PLL reference frequency are present. Output current is either ±100 μA or ±400 μA, selectable with bit 2/20.
5	PLL Gnd		Ground pin for the PLL section. A direct connection to a ground plane is strongly recommended.
6	Tx PD (Output)	Same as Pin 4, except powered from Tx PLL V _{CC} .	Tx Phase Detector Output. Description same as for Pin 4, except bit 1/20 controls the current level.
7	Tx PLL V _{CC} (Input)		Supply pin for the Tx PLL section, MCU Serial Interface, MCU Clock Counter, and the Reference Oscillator. Allowable range is 2.7 to 5.5 V and must be within 0.5 V of all other V _{CC} pins. Good bypassing is required and isolation with a 10 Ω resistor is recommended.
8	FTx (Input)	Same as Pin 2.	Receives the signal from the external 64/65 or 128/129 prescaler. DC bias is at 1.5 V.
9	FTx MC (Output)		Modulus Control Output for the Tx PLL section. Can be set to output in a current mode or a voltage mode, selectable with bit 3/16.

NOTE: 1. All V_{CC} pins must be within ±0.5 V of each other.

MC33411A/B

PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
10	EN (Input)		Enable Input for the MCU Interface section. Hysteresis threshold is within 0.5 V of ground and V_{CC} . See text for proper waveform required at this pin.
11	CLK (Input)	Same as Pin 10.	Clock Input for the MCU Interface section. Hysteresis threshold is within 0.5 V of ground and V_{CC} . Data is written or read out on clock's rising edge. Maximum clock rate is 2.0 MHz.
12	Data (I/O)		Data I/O line for the MCU Interface section. Both address and data are provided to/from this pin. Input threshold is within 0.5 V of ground and V_{CC} . Data is written or read out on clock's rising edge.
13	MCU Clk Out (Output)		<p>The microprocessor clock output is derived from the reference oscillator and a programmable divider with divide ratios of 2 to 312.5. It can be used to drive a microprocessor and thereby reduce the number of crystals required in the system design. The driver has an internal resistor in series with the output which can be combined with an external capacitor to form a low-pass filter to reduce radiated noise on the PCB. This output also functions as the output for the counter test modes.</p> <p>1) For the MC33411A the Clk Out can be disabled via the MCU interface.</p> <p>2) For the MC33411B this output is always active (on).</p>
14	Gnd Digital		Ground for the Data, MCU Clk Out, and F_{ref} Out digital Outputs. A direct connection to the ground plane is strongly recommended.

NOTE: 1. All V_{CC} pins must be within ± 0.5 V of each other.

MC33411A/B

PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
15, 16	F _{ref} In, F _{ref} Out		<p>Reference Frequency Input for various portions of the circuit, including the PLLs, SCF clock, etc. A crystal (4 to 18.25 MHz) may be connected as shown, or an external frequency source may be capacitor coupled to Pin 15. See text for crystal requirements.</p> <ol style="list-style-type: none"> 1) For the MC33411A the F_{ref} Out can be disabled via the MCU interface. 2) For the MC33411B this output is always active (on).
17	DS Out (Output)		Data Slicer Output (open collector with internal 100 kΩ pull-up resistor).
18	Tx Out (Output)		Tx Out is the Tx path audio output. Internally this pin has a low-pass filter circuitry with -3.0 dB bandwidth of 4.0 kHz. Tx gain and mute are programmable through the MCU interface. This pin is sensitive to load capacitance.
20	C Out (Output)		C Out is the compressor output.
19	Lim In (Input)		Lim In is the limiter input. This pin is internally biased and has an input impedance of 400 kΩ. Lim In must be ac-coupled.
21	C _{cap}		C _{cap} is the compressor rectifier filter capacitor pin. It is recommended that an external filter capacitor to V _{CC} audio be used. A practical capacitor range is 0.1 to 1.0 μF. The recommended value is 0.47 μF.

NOTE: 1. All V_{CC} pins must be within ±0.5 V of each other.

MC33411A/B

PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
22	C In (Input)		C In is the compressor input. This pin is internally biased and has an input impedance of 12.5 kΩ. C In must be ac-coupled.
23	V _{CC} Audio (Input)		Supply input for the audio section, filters, A/D Converters, and Data Slicer. Allowable range is 2.7 to 5.5 V. Good bypassing is required.
24	MCO (Output)		Output of the Microphone amplifier. Maximum output swing is $\approx 3.0 V_{pp}$ for $V_{CC} \geq 3.0 V$. Maximum output current is $>1.0 mA$ peak.
25	MCI (Input)		Inverting input of the microphone amplifier. Gain and frequency response are set with external resistors and capacitors from this pin to the audio source and to MCO.
26	VAG (Output)		Analog ground for the audio section filters. VAG is equal to V _B and is buffered from V _B . Maximum current which can be sourced from this pin is 500 μA.
27	V _B (Output)		An internal 1.5 V reference for several sections. This voltage is adjustable with bits 3/20–17. Maximum source current is 100 μA. PSRR, noise and crosstalk depends on the external capacitor.
28	V _{CC} PA (Input)		Supply pin for the power amplifier outputs. Allowable range is 2.7 to 5.5 V. Good bypassing is required.

NOTE: 1. All V_{CC} pins must be within $\pm 0.5 V$ of each other.

MC33411A/B

PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
29	PAO+ (Output)		Output of the second power amplifier. This amplifier is set for unity inverting gain and is driven by PAO-. Maximum swing is $2.9 V_{pp}$ and maximum output current is $>5.0 \text{ mA}$ peak. DC level is $\approx 1.5 \text{ V}$.
30	PAO- (Output)	Same as Pin 29.	Output of the first power amplifier. Its gain is set with external resistors and capacitors from this pin to PAI. Output capability is the same as Pin 28.
31	Gnd PA		Ground pin for the power amplifier outputs. A direct connection to a ground plane is strongly recommended.
32	PAI (Input)		Inverting input of the power amplifier. Gain and frequency response are set with external resistors and capacitors from this pin to the audio source and to PAO-.
33	E Out (Output)		Expander output. This output is sensitive to load capacitance. Maximum output signal level is $\approx 2.5 V_{pp}$. Maximum output current is $>1.0 \text{ mA}$.
34	Ecap		E _{cap} is the expander rectifier filter capacitor pin. Connect an external filter capacitor between V _{CC} audio and E _{cap} . The recommended capacitance range is 0.1 to 1.0 μF . The suggested value is 0.47 μF .
35	E In (Input)		The expander input pin is internally biased and has input impedance of 30 k Ω .
36	Rx Out (Output)		Rx Out is the Rx audio output. An internal low-pass filter has a -3.0 dB bandwidth of 4.0 kHz.

NOTE: 1. All V_{CC} pins must be within $\pm 0.5 \text{ V}$ of each other.

MC33411A/B

PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
37	RSSI In (Input)		Voltage input to RSSI A/D converter. Full scale is 0 to 1.6 V.
38	Rx Audio In (Input)		Input to the Rx Audio Path. Input impedance is 600 k Ω . Input signal must be capacitor coupled
39	DS In (Input)		Input for the digital data from the RF Receiver section. Input impedance is 250 k Ω . Hysteresis is internally provided. Input signal level must be between 50 and 700 mVpp.
40	Gnd Audio		Ground pin for the audio section. A direct connection to a ground plan is strongly recommended.
41	LO2 Out (Output)		Buffered output of the 2nd LO. This high frequency output is a current, requiring an external pullup resistor.
42	LO2 V _{CC} (Input)		Supply pin for the LO2 section. Allowable range is 2.7 to 5.5 V and must be within 0.5 V of all other V _{CC} pins. Good bypassing is required and isolation with a 10 Ω resistor is recommended.

NOTE: 1. All V_{CC} pins must be within ± 0.5 V of each other.

MC33411A/B

PIN FUNCTION DESCRIPTION (continued)

Pin	Symbol/Type	Description	Description
43, 45	LO2+, LO2-		The 2nd LO. External tank components are required. The internal capacitance across the pins is adjustable from 0 to 7.6 pF for fine tuning performance with bits 7/20-18.
44	LO2 Ctl (Input)		LO2 Control is the dc control input for this VCO. Typically it is the output of the low-pass filter fed from the phase detector output.
46	LO2 Gnd		Ground pin for the LO2 section. A direct connection to a ground plane is strongly recommended.
47	LO2PD (Output)		LO2 Phase Detector Output. The output either sources or sinks current, or neither, depending on the phase difference of the phase detector input signals. During lock, very narrow pulses with a frequency equal to the PLL reference frequency are present. Output current is either $\pm 100 \mu\text{A}$ or $\pm 400 \mu\text{A}$, selectable with bit 3/14.
48	LO2 Gnd		Ground pin for the LO2 section. A direct connection to a ground plane is strongly recommended.

NOTE: 1. All V_{CC} pins must be within ± 0.5 V of each other.

MC33411A/B

FUNCTIONAL DESCRIPTION

The following text, graphics, tables and schematics are provided to the user as a source of valuable technical information about the MC33411. This information originates from thorough evaluation of the device performance. This data was obtained by using units from typical wafer lots. It is important to note that the forgoing data and information was from a limited number of units. By no means is the user to assume that the data following is a guaranteed parametric. Only the minimum and maximum limits identified in the electrical characteristics tables found earlier in the spec are guaranteed.

Note: In the following descriptions, control bits in the MCU Serial Interface for the various functions will be identified by register number and bit number. For example, bit 3/19 indicates bit 19 of register 3. Bits 5/14–11 indicates register 5, bits 14 through 11. Please refer to Figure 1.

General Circuit Description

The MC33411A/B is a low power baseband IC designed to interface with the MC13145 UHF Wideband Receiver and MC13146 Transmitter for applications up to 2.0 GHz. The devices are primarily designated to be used for 900 MHz ISM band in a CT-900, low power, dual conversion cordless phone, but other applications such as data links with analog processing could be developed. This device contains complete baseband transmit and receive processing sections, a transmit and receive PLL section, a programmable PLL second local oscillator usable to 80 MHz,

RSSI and low battery detect circuitry and serial interface for a microprocessor.

"A" versions of the device have the ability to disable either the reference oscillator or MCU clock outputs. This feature is useful for systems where the MCU has an internal clock, allowing the user to place the MC33411 into Inactive (lowest power consumption) mode. The "A" version is also useful for systems where the MCU has a dedicated clock source, allowing for lower power consumption from the MC33411 by disabling the MCU clock output.

"B" versions of the device are intended for systems where the MCU clock will always be driven from the MC33411. These bits are purposefully "hard-wired" to the enable state to ensure proper operation of the reference oscillator and MCU clock output even during battery discharge/recharge cycles.

All internal registers are completely static – no refreshing is required under normal operation conditions.

DC Current

Figures 2 through 5 are the current consumption for Inactive (MC33411 "A" version only), Standby, Receive, and Active modes versus supply voltages. Figures 6 and 7 show the typical behavior of current consumption in relation to temperature.

Figure 8 illustrates the effect of the MCU clock output frequency to supply current during Active mode.

Figure 2. Supply Current versus Supply Voltage (Inactive Mode)

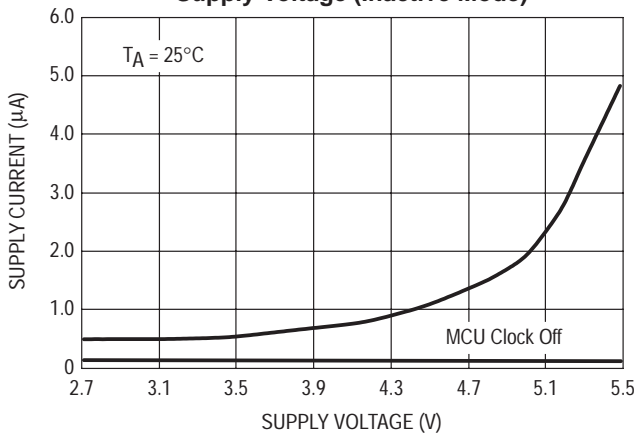


Figure 3. Supply Current versus Supply Voltage (Standby Mode)

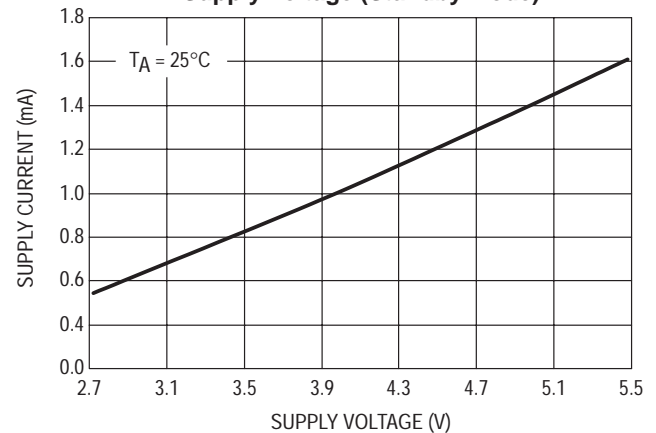


Figure 4. Supply Current versus Supply Voltage (Receive Mode)

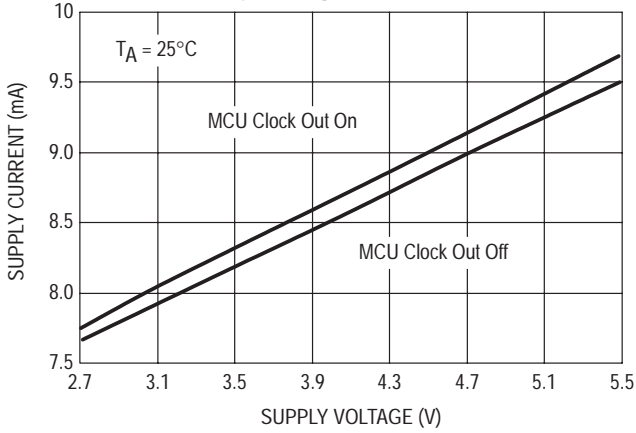


Figure 5. Supply Current versus Supply Voltage (Active Mode)

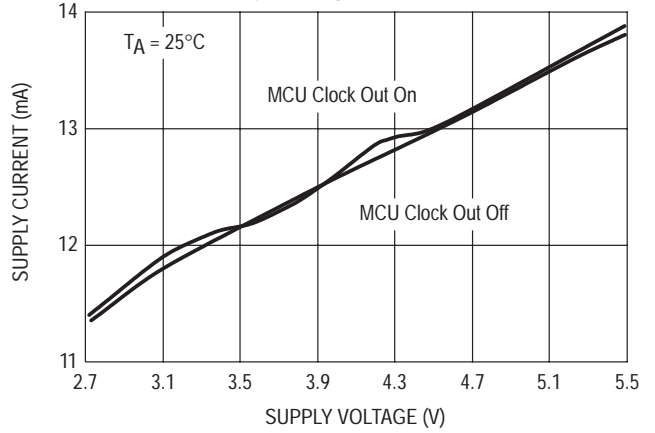


Figure 6. Supply Current versus Temperature Normalized to 25°C (Standby Mode)

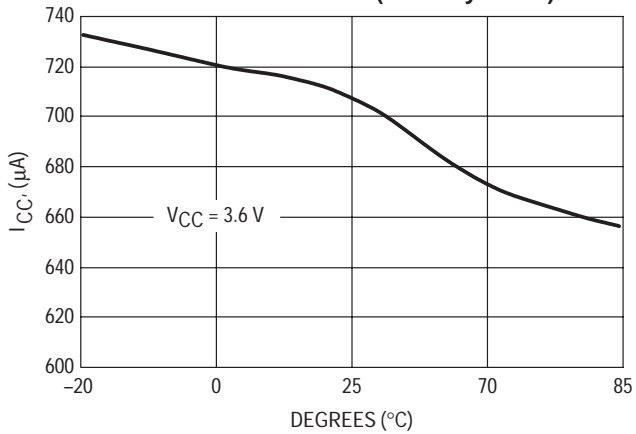


Figure 7. Supply Current versus Temperature Normalized to 25°C (Receive & Active Mode)

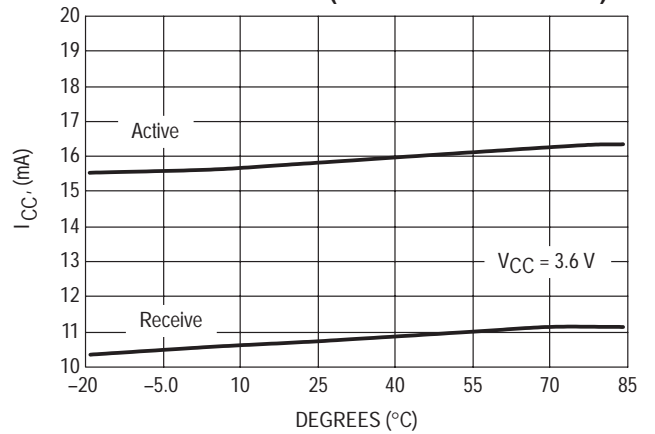


Figure 8. Supply Current versus MCU Clock Output Frequency (Active Mode)

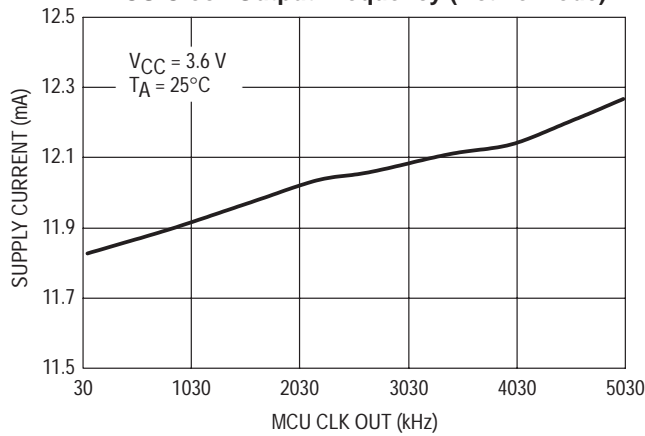


Table 1. Tx Gain Adjust Programming (Register 7)

Gain Control Bit #9	Gain Control Bit #8	Gain Control Bit #7	Gain Control Bit #6	Gain Control Bit #5	Gain Ctl #	Gain/Attenuation Amount
					<6	-9.0 dB
0	0	1	1	0	6	-9.0 dB
0	0	1	1	1	7	-8.0 dB
0	1	0	0	0	8	-7.0 dB
0	1	0	0	1	9	-6.0 dB
0	1	0	1	0	10	-5.0 dB
0	1	0	1	1	11	-4.0 dB
0	1	1	0	0	12	-3.0 dB
0	1	1	0	1	13	-2.0 dB
0	1	1	1	0	14	-1.0 dB
0	1	1	1	1	15	0 dB
1	0	0	0	0	16	1.0 dB
1	0	0	0	1	17	2.0 dB
1	0	0	1	0	18	3.0 dB
1	0	0	1	1	19	4.0 dB
1	0	1	0	0	20	5.0 dB
1	0	1	0	1	21	6.0 dB
1	0	1	1	0	22	7.0 dB
1	0	1	1	1	23	8.0 dB
1	1	0	0	0	24	9.0 dB
1	1	0	0	1	25	10 dB
-	-	-	-	-	>25	10 dB

Transmit Speech Processing System

This portion of the audio path goes from "Tx Audio" to "Tx Out". The gain of the microphone amplifier is set with external resistors to receive the audio from the microphone hybrid or any other audio source. The MCO output has rail-to-rail capability. The "Tx Audio" pin will be ac-coupled. The audio transmit signal path includes automatic level control (ALC) (also referred to as the Compressor), Tx mute, limiter, filters, and Tx gain adjust. The ALC provides "soft" limiting to the output signal swing as the input voltage slowly increases. With this technique the gain is slightly lowered to help reduce distortion of the audio signal. The limiter section provides hard limiting due to rapidly changing signal levels, or transients. The ALC, TX mute, and limiter functions can be enabled or disabled via the MCU serial interface. The Tx gain adjust can also be remotely controlled to set different desired signal levels.

The adjustable gain stage provides 20 levels of gain in 1.0 dB increments. It is controlled with bits 7/9–5 as shown in Table 1. The effect of the gain setting under various ALC/Limiter On/Off settings is shown in Figure 9.

The Low-Pass Filter before the gain stage is a switched capacitor filter with a corner frequency at 3.7 kHz. This

frequency is dependent upon the SCF clock, nominally set to 165 kHz and is directly proportional to the SCF clock. The filter response for inband, ripple, wideband, as well as phase and group delay, are shown in Figures 10 through 14.

The mute switch at Pin 18 will mute a minimum of 60 dB. Bit 6/2 controls the mute. The limiter can be disabled by programming a logic 1 into 6/5.

The compressor with ALC transfer characteristic is shown in Figure 15. The ALC gain is controlled by bits 6/11–12. If both bits are programmed to a logic 0, the ALC gain is set to 5.0 dB. If bit 6/11 is set to a logic 1, the ALC gain will be set to 10 dB, whereas if bit 6/12 is set to a logic 1 the ALC gain will be 25 dB. The ALC function may be disabled by programming a logic 1 into bit 6/6.

The compressor low maximum gain can be set with bit 6/8. Programming this bit to a logic 0 sets the maximum gain to 23 dB. A lower maximum gain, nominally 13.5 dB, is achieved by programming the bit to a logic 1. The entire compressor can be bypassed (i.e., 0 dB) by programming bit 6/4 to a logic 1.

Figures 16 through 22 describe the characteristics of the compressor, ALC, and limiter.

Figure 9. Tx Audio Output Voltage versus Gain Control Setting

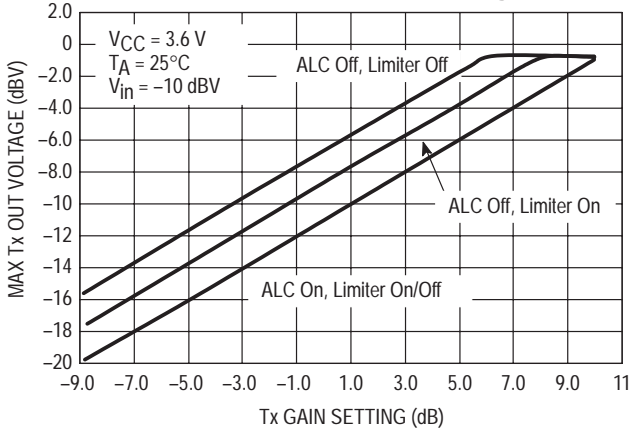


Figure 10. Lim In to Tx Out Gain versus Frequency (Inband)

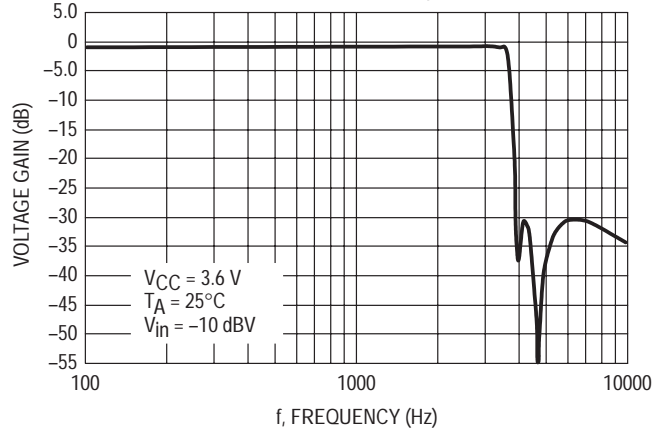


Figure 11. Lim In to Tx Out Gain versus Frequency (Ripple)

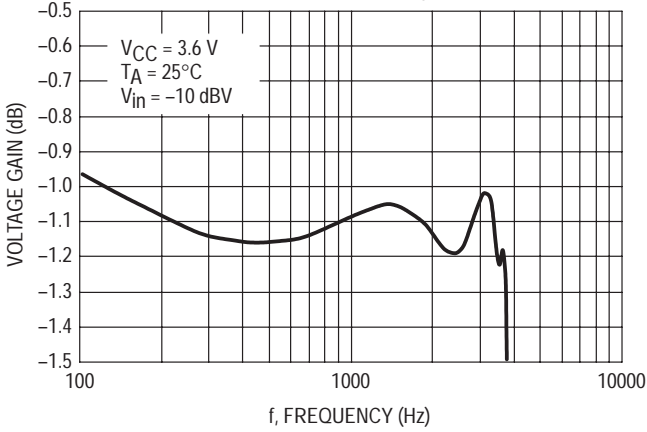


Figure 12. Lim In to Tx Out Gain versus Frequency (Wideband)

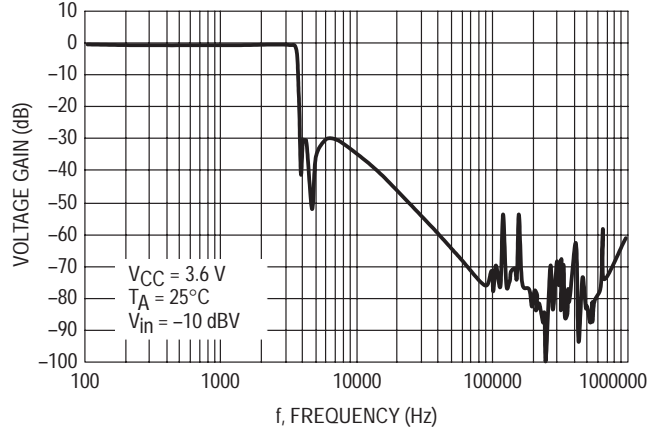


Figure 13. Lim In to Tx Out Phase versus Frequency

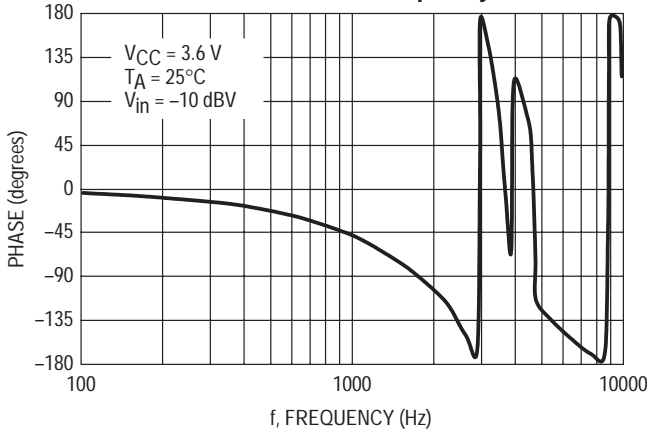


Figure 14. Lim In to Tx Out Group Delay versus Frequency

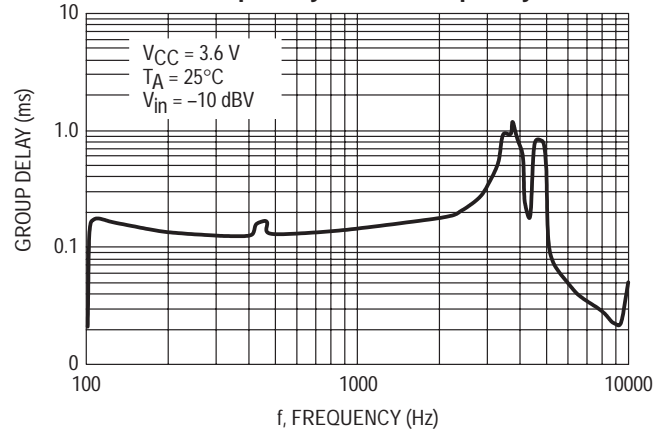


Figure 15. Compressor Characteristic with Programmable Compressor Maximum Gain

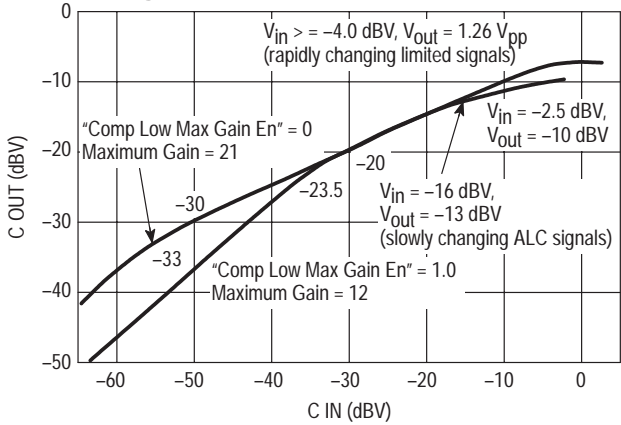


Figure 16. Tx Audio Compressor Response (Distortion & Amplitude, ALC off, Lim off)

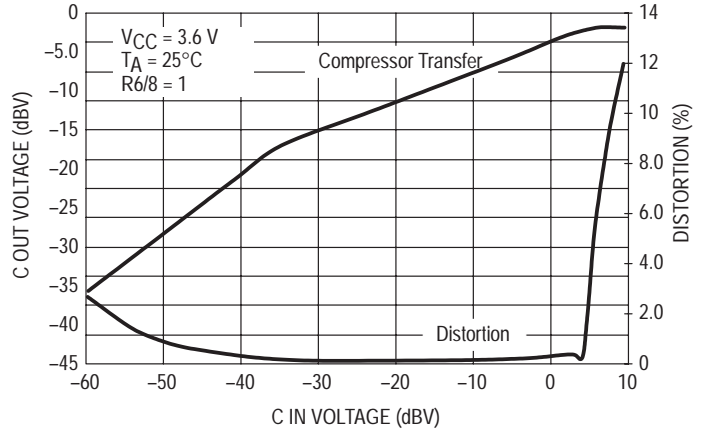


Figure 17. Tx Audio Compressor Response (Distortion & Amplitude, ALC off, Lim off)

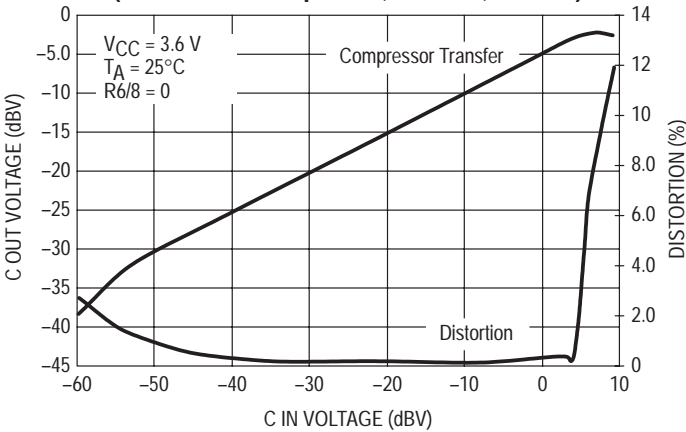


Figure 18. Tx Output Audio Response (Lim & ALC off)

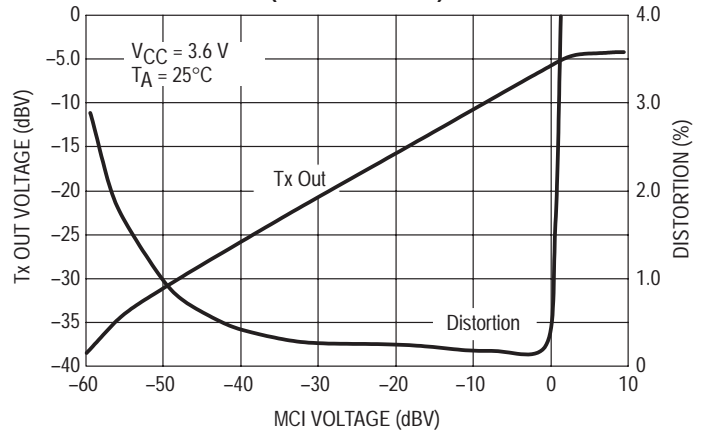


Figure 19. Tx Output Audio Response (Lim on, ALC off)

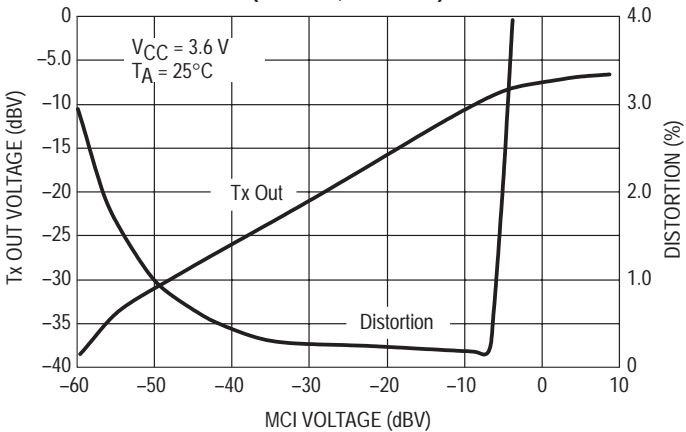


Figure 20. Tx Output Audio Response (Lim off, ALC on)

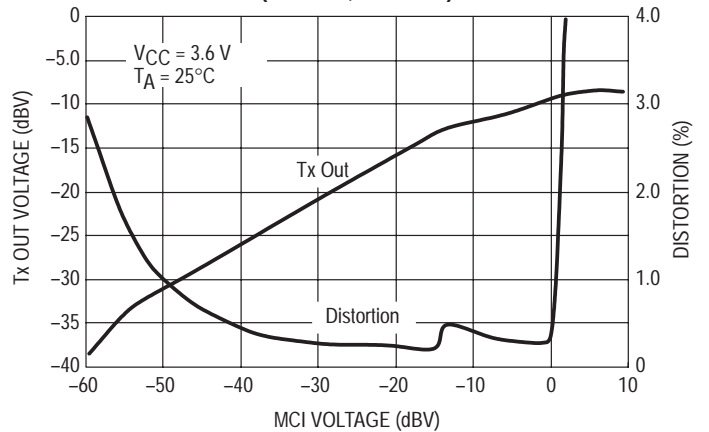


Figure 21. Tx Output Audio Response (Lim off, R6/11 = 1)

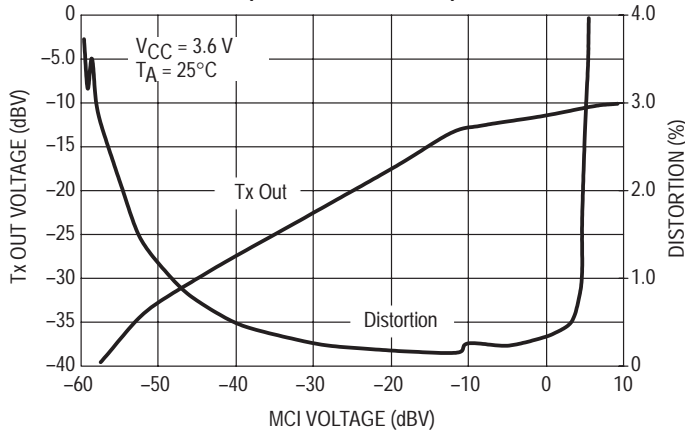
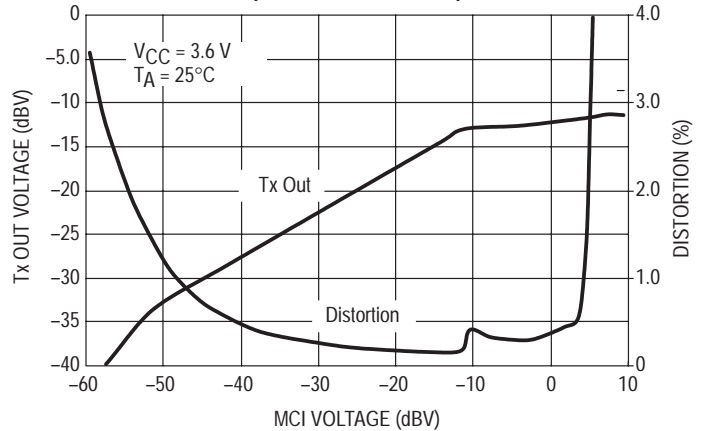


Figure 22. Tx Output Audio Response (Lim off, R6/12 = 1)



Data Slicer

The data slicer will receive the low level digital signal from the RF receiver section at Pin 39. The input signal to the data slicer must be >200 mVpp. Hysteresis of 40 mV is internally provided. The output of the data slicer will be same waveform, but with an amplitude of 0 to V_{CC}, and can be observed at Pin 17 if bits 5/9–8 are set to 00. The output can be inverted by setting bit 5/9 = 1. The data slicer can be disabled by setting bit 5/8 = 1.

Receive Audio Path

The Receive Audio Path (Pins 38, 36–33) consists of an anti-aliasing filter, a low-pass filter, side tone attenuator, gain adjust stage, a mute switch, expander and volume control.

The switched capacitor low-pass filter is an 8 pole filter, with a corner frequency at 3.8 kHz. This is designed to provide bandwidth limiting in the audio range.

The gain stage provides 20 dB of gain adjustment in 1.0 dB steps, measured from Pin 38 to 36. Bits 7/4–0 are used to set the gain according to Table 3. The mute switch, controlled by bit 6/1, will mute a minimum of 60 dB.

When the compressor output is within 3.0 dB of the expander input level, the Rx output (Pin 36) can be attenuated (referenced to the expander output) by bits 6/10–9. For 6/10–9 = 00, the attenuation is 0 dB. For the other combinations, 6/10–9 = 01, attenuation = 3.0 dB; 6/10–9 = 10, attenuation = 6.0 dB; and 6/10–9 = 11, attenuation = 10.4 dB (See Table 2).

The expander can be bypassed by setting bit 6/3 = 1.

Table 3 shows the various gain control settings which can be accessed in Register 7. Table 4 is the volume control settings, also located in Register 7.

Figures 23 through 31 illustrate the various characteristics of the receive audio path.

Table 2. Side Tone Attenuate Programming

Side Tone Attenuate Bit #1	Side Tone Attenuate Bit #0	Select #	Side Tone Attenuate Amount at Expander Input	Side Tone Attenuate Amount at Expander Output
0	0	0	0 dB	0 dB
0	1	1	1.5 dB	3.0 dB
1	0	2	3.0 dB	6.0 dB
1	1	3	5.2 dB	10.4 dB

Table 3. Rx Gain Adjust Programming (Register 7)

Gain Control Bit #4	Gain Control Bit #3	Gain Control Bit #2	Gain Control Bit #1	Gain Control Bit #0	Gain Ctl #	Gain/Attenuation Amount
–	–	–	–	–	<6	–9.0 dB
0	0	1	1	0	6	–9.0 dB
0	0	1	1	1	7	–8.0 dB
0	1	0	0	0	8	–7.0 dB
0	1	0	0	1	9	–6.0 dB
0	1	0	1	0	10	–5.0 dB
0	1	0	1	1	11	–4.0 dB
0	1	1	0	0	12	–3.0 dB
0	1	1	0	1	13	–2.0 dB

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Table 3. Rx Gain Adjust Programming (Register 7) (continued)

Gain Control Bit #4	Gain Control Bit #3	Gain Control Bit #2	Gain Control Bit #1	Gain Control Bit #0	Gain Ctl #	Gain/Attenuation Amount
0	1	1	1	0	14	-1.0 dB
0	1	1	1	1	15	0 dB
1	0	0	0	0	16	1.0 dB
1	0	0	0	1	17	2.0 dB
1	0	0	1	0	18	3.0 dB
1	0	0	1	1	19	4.0 dB
1	0	1	0	0	20	5.0 dB
1	0	1	0	1	21	6.0 dB
1	0	1	1	0	22	7.0 dB
1	0	1	1	1	23	8.0 dB
1	1	0	0	0	24	9.0 dB
1	1	0	0	1	25	10 dB
-	-	-	-	-	>25	10 dB

Table 4. Volume Control Programming

Volume Control Bit #13	Volume Control Bit #12	Volume Control Bit #11	Volume Control Bit #10	Volume Ctl #	Gain/Attenuation Amount
0	0	0	0	0	-14 dB
0	0	0	1	1	-12 dB
0	0	1	0	2	-10 dB
0	0	1	1	3	-8.0 dB
0	1	0	0	4	-6.0 dB
0	1	0	1	5	-4.0 dB
0	1	1	0	6	-2.0 dB
0	1	1	1	7	0 dB
1	0	0	0	8	2.0 dB
1	0	0	1	9	4.0 dB
1	0	1	0	10	6.0 dB
1	0	1	1	11	8.0 dB
1	1	0	0	12	10 dB
1	1	0	1	13	12 dB
1	1	1	0	14	14 dB
1	1	1	1	15	16 dB

Figure 23. Rx Out Maximum Output Voltage versus Gain Control Setting

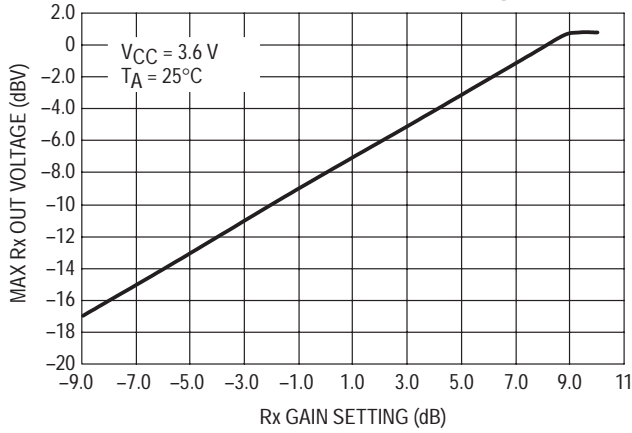


Figure 24. E Out Maximum Output Voltage versus Volume Control Setting

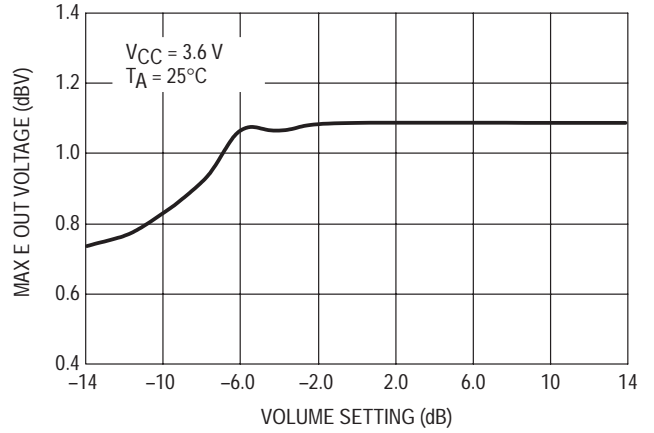


Figure 25. Rx Audio In to Rx Out Gain versus Frequency (Inband)

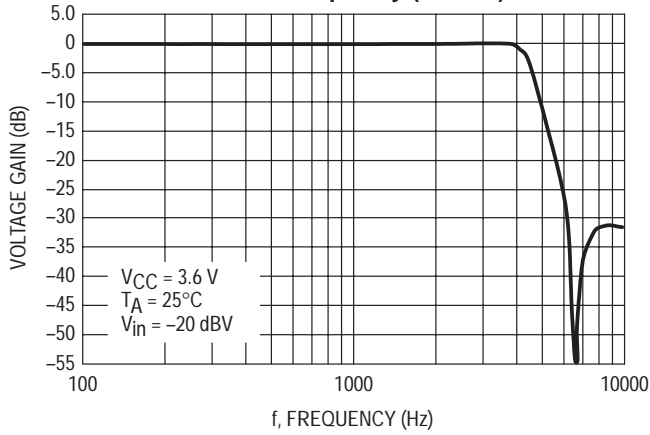


Figure 26. Rx Audio In to Rx Out Gain versus Frequency (Ripple)

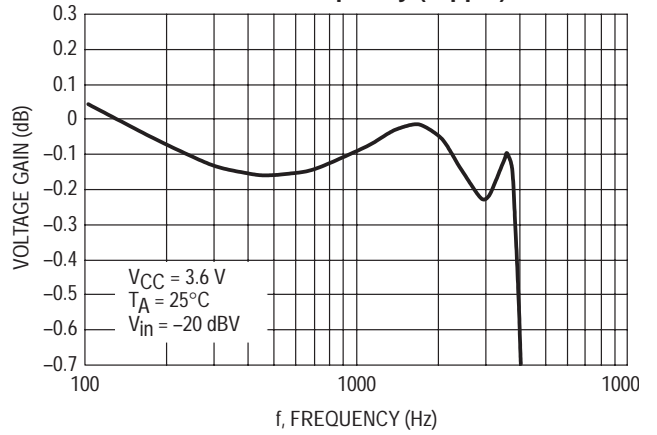


Figure 27. Rx Audio In to Rx Out Gain versus Frequency (Wideband)

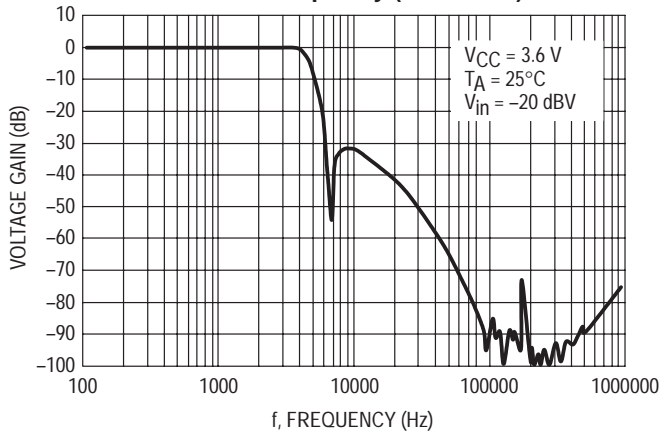


Figure 28. Rx Audio In to Rx Out Phase versus Frequency

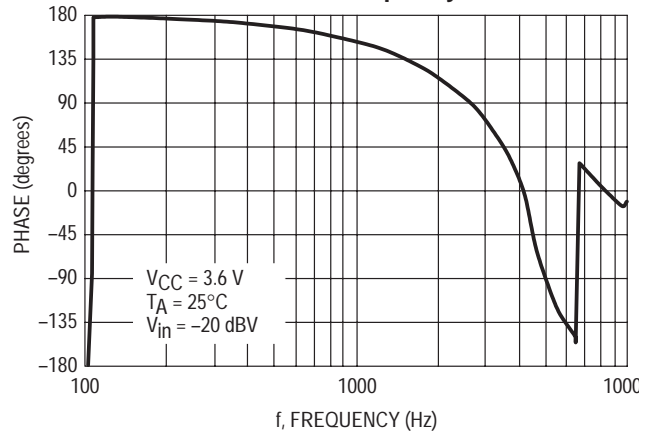


Figure 29. Rx Audio In to Rx Out Group Delay versus Frequency

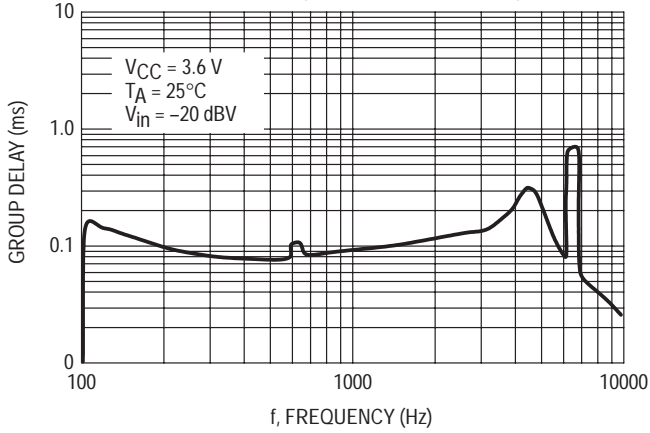


Figure 30. AALPF Response Gain versus Frequency

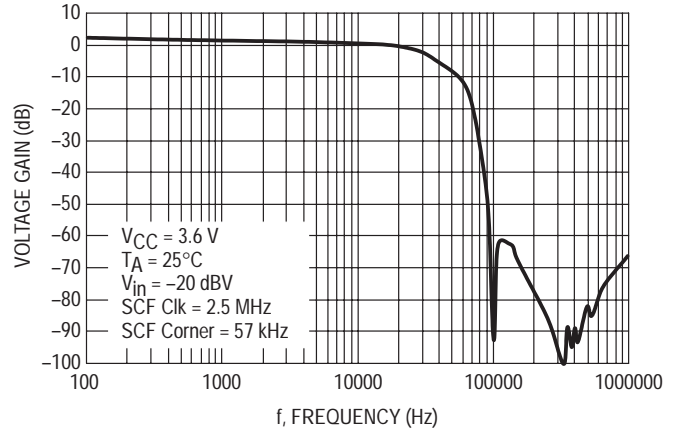
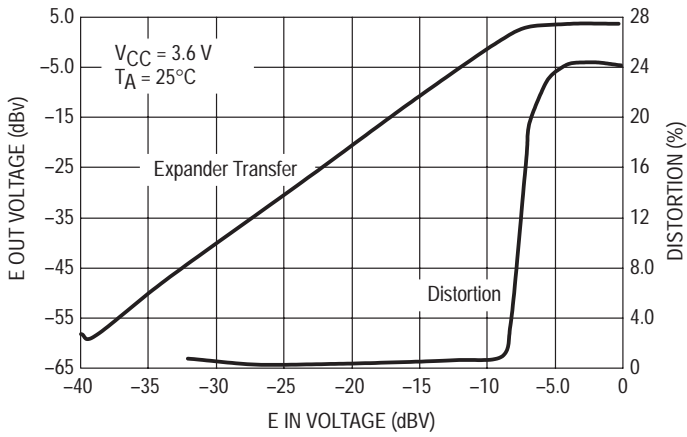


Figure 31. E In to E Out Transfer Curve



Power Amplifiers

The power amplifiers (Pins 29, 30, 32) are designed to drive the earpiece in a handset, or the telephone line via a hybrid circuit in the base unit. Each output (PAO+ and PAO-) can source and sink 5.0 mA, and can swing $1.3 V_{pp}$ each. For high impedance loads, each output can swing $2.7 V_{pp}$ ($5.4 V_{pp}$ differential). The gain of the amplifiers is set with a feedback resistor from Pin 30 to 32, and an input resistor at Pin 32. The differential gain is 2x the resistor ratio. Capacitors

can be used for frequency shaping. The pins' dc level is V_B ($\approx 1.5 V$).

The Mute switch, controlled with bit 6/0, will provide 60 dB of muting with a 50 k Ω feedback resistor. The amount of muting will depend on the value of the feedback resistor.

Figures 32 and 33 show the power amplifier swing/distortion for $V_{CC} = 3.6 V$, and Figure 34 illustrates the maximum swing capability for various value of V_{CC} .

Figure 32. Power Amplifier Maximum Output Swing

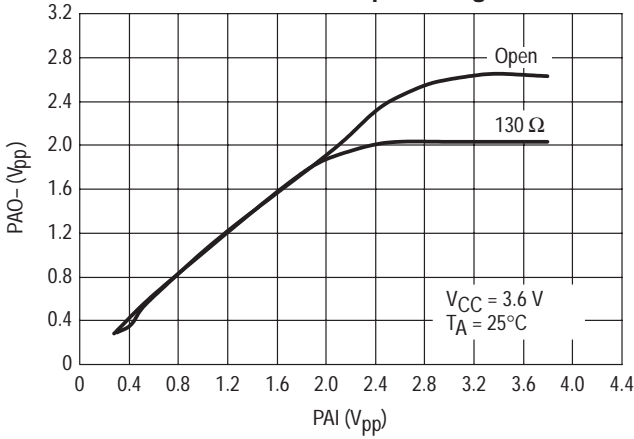


Figure 33. Power Amplifier Distortion

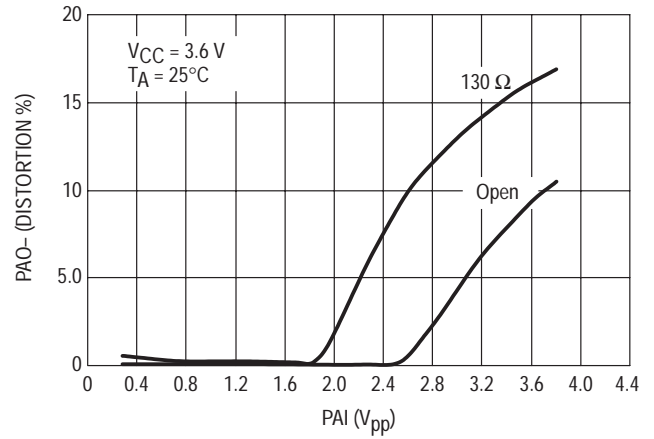
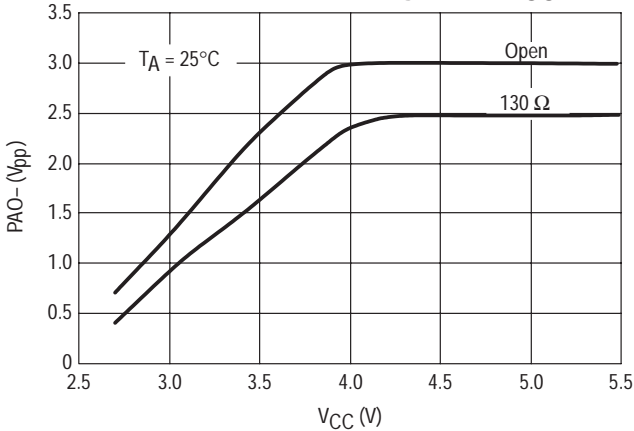


Figure 34. Power Amplifier Maximum Output Swing versus VCC



Reference Oscillator/MCU Clk Out

The reference oscillator provides the frequency basis for the three PLLs, the switched capacitor filters, and the MCU clock output. The source for the reference clock can be a crystal in the range of 4.0 to 18.25 MHz connected to Pins 15 & 16, or it can be an external source connected to F_{ref In} (Pin 15). The reference frequency is directed to:

- a. A programmable 12-bit counter (register bits 4/11-0) to provide the reference frequency for the three PLLs. The 12-bit counter is to be set such that, in conjunction with the programmable counters within each PLL, the proper frequencies can be produced by each VCO.
- b. A programmable 6-bit counter (register bits 4/17-12), followed by a +2 stage, to set the frequency for the switched capacitor filters to 165 kHz, or as close to that as possible.
- c. A programmable 3-bit counter (register bits 7/16-14) which provides the MCU clock output (see Tables 5 and 6).

A representation of the reference oscillator is given by Figures 39 and 36.

Figure 35. Reference Oscillator Schematic

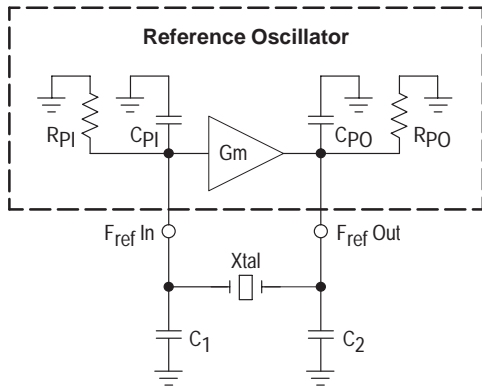


Figure 36. Reference Oscillator Input and Output Impedance

Input Impedance ($R_{PI} // C_{PI}$)	11.6 k Ω // 2.9 pF
Output Impedance ($R_{PO} // C_{PO}$)	4.5 k Ω // 2.5 pF

Figures 37 and 38 show a typical gain/phase response of the oscillator. Load capacitance (C_L), equivalent series resistance (ESR), and even supply voltage will have an effect on the oscillator response as shown in Figures 39 and 40. It should be noted that optimum performance is achieved when $C1$ equals $C2$ ($C1/C2 = 1$).

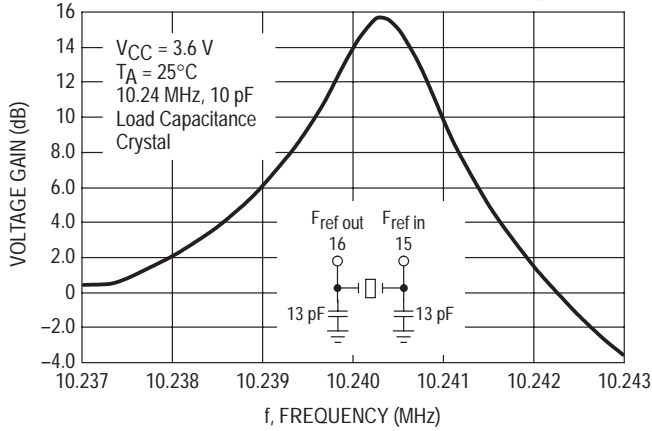
Figure 41 represents the ESR versus crystal load capacitance for the reference oscillator. This relationship was defined by using a 6.0 dB minimum loop gain margin at 3.6 V. This is considered the minimum gain margin to guarantee oscillator start-up.

Oscillator start-up is also significantly affected by the crystal load capacitance selection. In Figure 39, the relationship between crystal load capacitance and ESR can be seen. The lower the load capacitance the better the performance.

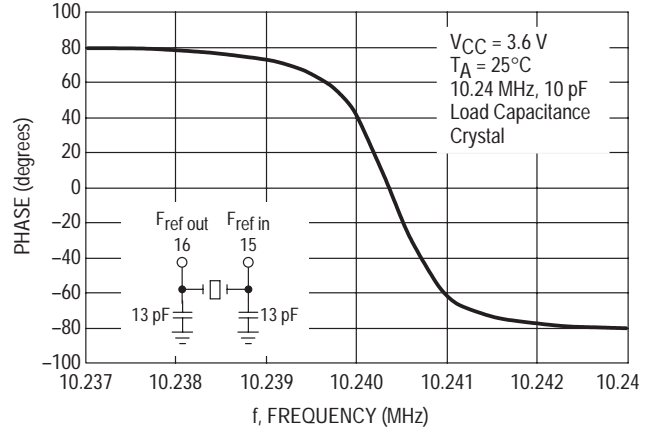
Given the desired crystal load capacitance, $C1$ and $C2$ can be determined from Figure 42. It should also be pointed out that current consumption increases when $C1 \neq C2$.

Be careful not to overdrive the crystal. This could cause a noise problem. An external series resistor on the crystal output can be added to reduce the drive level, if necessary.

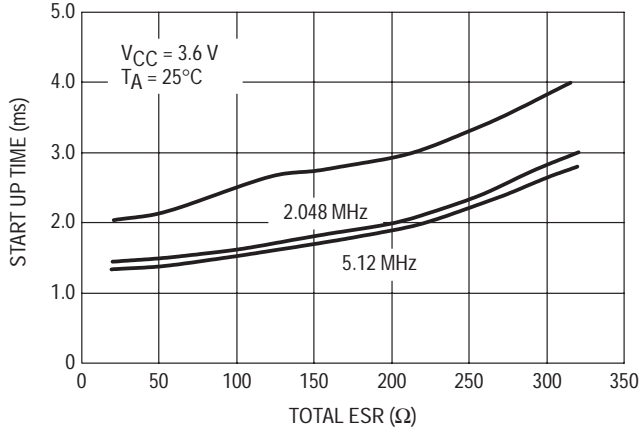
**Figure 37. Reference Oscillator
Open Loop Gain versus Frequency**



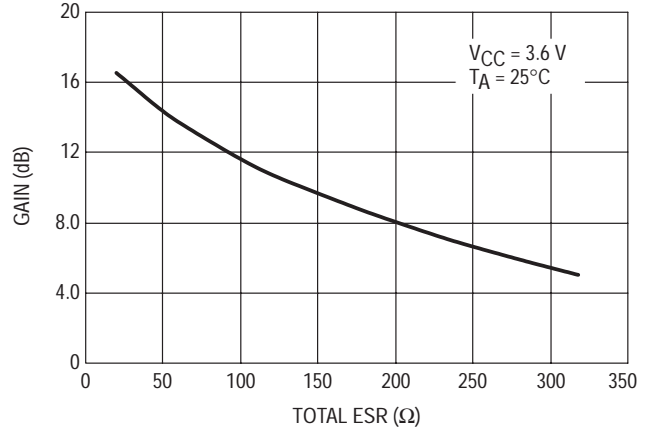
**Figure 38. Reference Oscillator
Open Loop Phase versus Frequency**



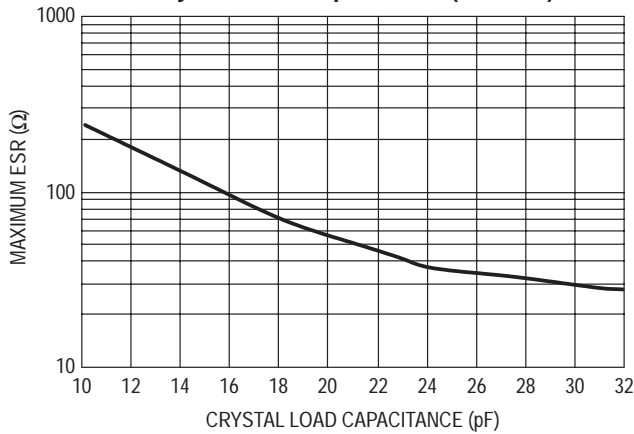
**Figure 39. Reference Oscillator Startup Time
versus Total ESR – Inactive to Rx Mode**



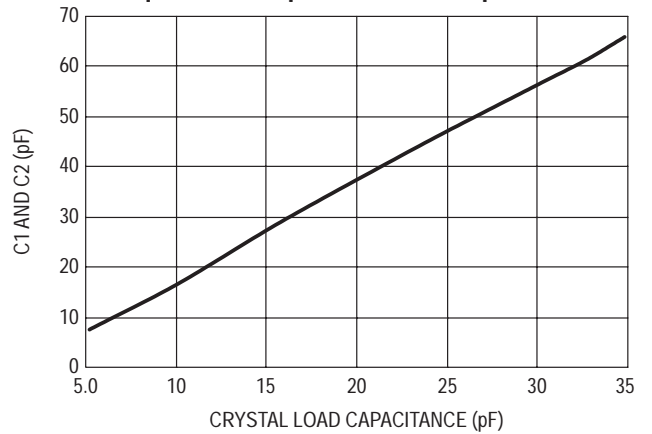
**Figure 40. Reference Oscillator
Open Loop Gain versus ESR**



**Figure 41. Maximum ESR versus
Crystal Load Capacitance (C1 = C2)**



**Figure 42. Optimum Values for C1, C2 versus
Equivalent Required Parallel Capacitance**



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Table 5. MCU Clock Divider Programming

MCU Clk Bit #16	MCU Clk Bit #15	MCU Clk Bit #14	Clk Out Divider Value
0	0	0	2.0
0	0	1	3.0
0	1	0	4.0
0	1	1	5.0
1	0	0	2.5
1	0	1	20
1	1	0	80
1	1	1	312.5

Table 6. MCU Clock Divider Frequencies

Crystal Frequency	Clock Output Divider							
	2.0	2.5	3.0	4.0	5.0	20	80	312.5
10.24 MHz	5.12 MHz	4.096 MHz	3.413 MHz	2.56 MHz	2.048 MHz	512 kHz	128 kHz	32.768 kHz
11.15 MHz	5.575 MHz	4.46 MHz	3.717 MHz	2.788 MHz	2.23 MHz	557 kHz	139 kHz	35.68 kHz
12 MHz	6.0 MHz	4.8 MHz	4.0 MHz	3.0 MHz	2.4 MHz	600 kHz	150 kHz	38.4 kHz

Transmit and Receive (LO1) PLL Sections

The transmit and receive PLLs (Pins 6–9 and 1–4, respectively) are designed to be part of a 900 MHz system. In a typical application the Transmit PLL section will be set up to generate the transmit frequency, and the Receive PLL section will be set up to generate the LO1 frequency. The two sections are identical, and function independently. External requirements for each include a low-pass filter, a 900 MHz VCO, and a 64/65 or 128/129 dual modulus prescaler.

The frequency output of the VCO is to be reduced by the dual modulus prescaler, and then input to the MC33411 (at Pin 8 or 2). That frequency is then further reduced by the programmable 13-bit counter (bits 1/19–7 or 2/19–7), and provided to one side of the Phase Detector, where it is compared with the PLL reference frequency. The output of the phase detector (at Pin 6 or 4) is a Three-State charge pump which drives the VCO through the low-pass filter. Bits 1/20 and 2/20 set the gain of each of the two charge pumps to either $100/2\pi \mu\text{A/radian}$ or $400/2\pi \mu\text{A/radian}$. The polarity of the two phase detector outputs is set with bits 1/21 and 2/21. If the bit = 0, the appropriate PLL is configured to operate with a non-inverting low-pass filter/VCO combination. If the low-pass filter/VCO combination is inverting, the polarity bit should be set to 1.

The 7-bit A and A' counters (bits 1/6–0 and 2/6–0) are to be set to drive the Modulus Control input of the 64/65 or 128/129 dual modulus prescalers. The Modulus Control outputs (Pins 9 and 1) can be set to either a voltage mode (logic 1) or a current mode (logic 0) with bit 3/16.

To calculate the settings of the N and A registers, the following procedure is used:

$$\frac{f_{VCO}}{f_{PLL}} = Nt \text{ (Nt must be an integer)} \quad (1)$$

$$\frac{Nt}{P} = N \quad (2)$$

$$A = \text{Remainder of Equation 2} \text{ (decimal part of } N \times P) \quad (3)$$

where: f_{VCO} = the VCO frequency
 f_{PLL} = the PLL Reference Frequency set within the MC33411
 P = the smaller divisor of the dual modulus prescaler (64 for a 64/65 prescaler)
 N = the whole number portion is the setting for the N (or N') counter within the MC33411
 A = the setting for the A (or A') counter within the MC33411

For example, if the VCO is to provide 910 MHz, and the internal PLL reference frequency is 50 kHz, then the equations yield:

$$Nt = \frac{910 \times 10^6}{50 \times 10^3} = 18,200$$

$$N = \frac{18,200}{64} = 284.375$$

$$A = 0.375 \times 64 = 24$$

The N register setting is 284 (0 0001 0001 1100), and the A register setting is 24 (001 1000).

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2nd LO (LO2)

This PLL is designed to be the 2nd Local Oscillator in a typical 900 MHz system, and is designed for frequencies up to 80 MHz. The VCO and varactor diodes are included, and are to be used with an external tank circuit (Pins 43–45).

Bits 4/20–18 are used to select an internal capacitor, with a value in the range of 0 to 7.6 pF, to parallel the varactor diodes and the tank's external capacitor. This permits a certain amount of fine tuning of the oscillator's performance. See Table 7.

A buffered output is provided to drive, e.g., a mixer. The frequency is set with the programmable 14-bit counter (bits 3/13–0) in conjunction with the PLL reference frequency. For example, if the reference frequency is 50 kHz,

and the 2nd LO frequency is to be 63.3 MHz, the 14-bit counter needs to be set to 1266_d (00 0100 1111 0010). The output level is dependent on the value of the impedance at Pin 41, partly determined by the external pull-up resistor.

The output of the phase detector is a Three-State charge pump which drives the varactor diodes through an external low-pass filter. Bit 3/14 sets the gain of the charge pump to either $100/2\pi$ $\mu\text{A}/\text{radian}$ (logic 0) or $400/2\pi$ $\mu\text{A}/\text{radian}$ (logic 1). Bit 3/15 sets its polarity – if 0, the PLL is configured to operate with a non-inverting low-pass filter/VCO combination. If the low-pass filter/VCO combination is inverting, the polarity bit should be set to 1. Please note that the 2nd LO VCO on the MC33411 is of the non-inverting type. Figures 43 through 45 describe the response of the 2nd LO.

Table 7. LO2 Capacitor Select Programming

LO2 Capacitor Select Bit #20	LO2 Capacitor Select Bit #19	LO2 Capacitor Select Bit #18	Select #	LO2 Capacitor Select Value
0	0	0	0	0 pF
0	0	1	1	1.1 pF
0	1	0	2	2.2 pF
0	1	1	3	3.3 pF
1	0	0	4	4.3 pF
1	0	1	5	5.4 pF
1	1	0	6	6.5 pF
1	1	1	7	7.6 pF

Figure 43. Varicap Capacitance versus Control Voltage

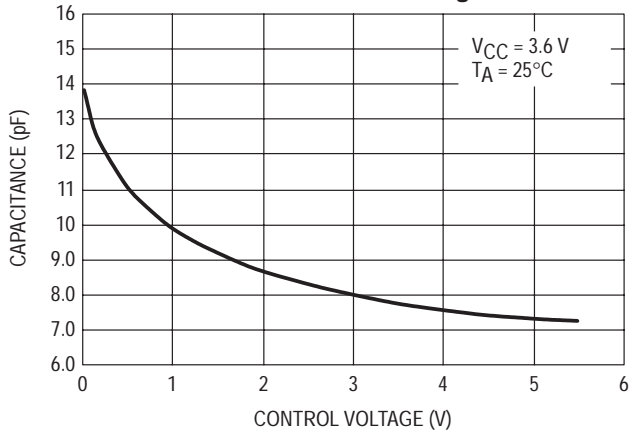


Figure 44. Minimum Overall Q versus Coil Inductance for LO2

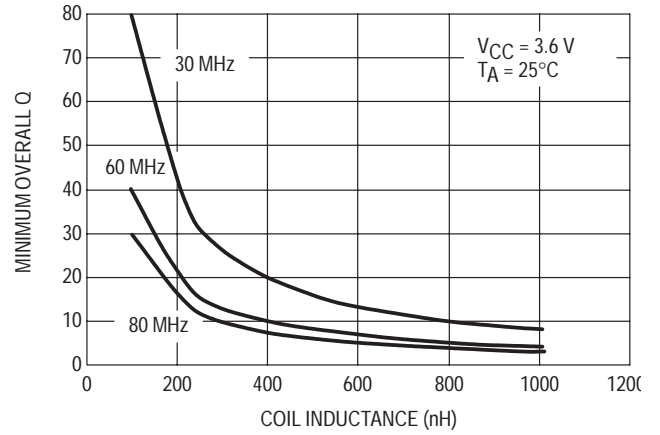
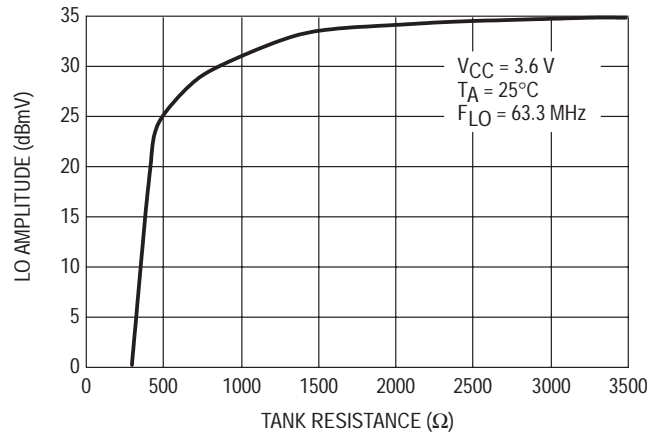


Figure 45. LO2 Amplitude versus Overall Tank Parallel Resistance

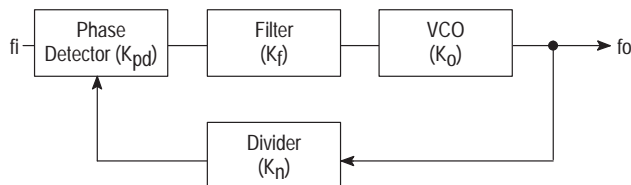


Loop Filter Characteristics

Let's consider the following discussion on loop filters. The fundamental loop characteristics, such as capture range, loop bandwidth, lock-up time, and transient response are controlled externally by loop filtering.

Figure 96 is the general model for a Phase Lock Loop (PLL).

Figure 46. PLL Model



Where:

- K_{pd} = Phase Detector Gain Constant
- K_f = Loop Filter Transfer Function
- K_0 = VCO Gain Constant
- K_n = Divide Ratio (N)
- f_i = Input frequency
- f_o = Output frequency
- f_o/N = Feedback frequency divided by N

From control theory the loop transfer function can be represented as follows:

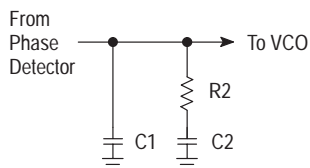
$$A = \frac{K_{pd} K_f K_0}{K_n} \text{ Open loop gain}$$

K_{pd} can be either expressed as being $200 \mu A/4\pi$ or $800 \mu A/4\pi$. More details about performance of different type PLL loops, refer to Motorola application note AN535.

The loop filter can take the form of a simple low pass filter. A current output, type 2 filter will be used in this discussion since it has the advantage of improved step response, velocity, and acceleration.

The type 2 low pass filter discussed here is represented as follows:

Figure 47. Loop Filter with Additional Integrating Element

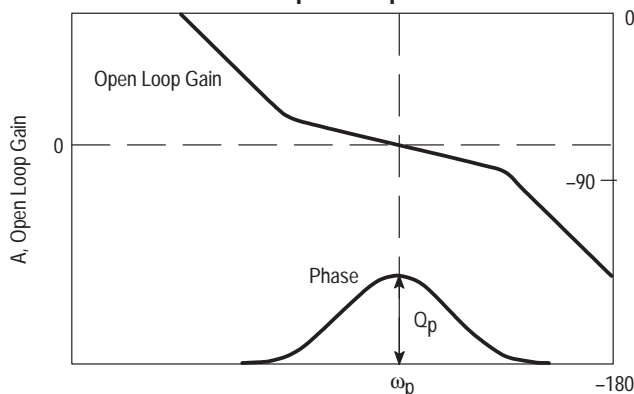


From Figure 97, capacitor C1 forms an additional integrator, providing the type 2 response, and filters the discrete current steps from the phase detector output. The function of the additional components R2 and C2 is to create a pole and a zero (together with C1) around the 0 dB point of the open loop gain. This will create sufficient phase margin for stable loop operation.

In Figure 98, the open loop gain and the phase is displayed in the form of a Bode plot. Since there are two integrating functions in the loop, originating from the loopfilter and the VCO gain, the open loop gain response follows a second order slope (-40 dB/dec) creating a phase of -180 degrees at the lower and higher frequencies. The filter characteristic needs to be determined such that it is adding a

pole and a zero around the 0 dB point to guarantee sufficient phase margin in this design (Q_p in Figure 98).

Figure 48. Bode Plot of Gain and Phase in Open Loop Condition



The open loop gain including the filter response can be expressed as:

$$A_{openloop} = \frac{K_{pd} K_0 (1 + j\omega(R_2 C_2))}{j\omega K_n \left(j\omega \left(1 + j\omega \left(\frac{R_2 C_1 C_2}{C_1 + C_2} \right) \right) \right)} \quad (4)$$

The two time constants creating the pole and the zero in the Bode plot can now be defined as:

$$T_1 = \frac{R_2 C_1 C_2}{C_1 + C_2} \quad T_2 = R_2 C_2 \quad (5)$$

By substituting equation (5) into (4), it follows:

$$A_{openloop} = \left(\frac{K_{pd} K_0 T_1}{\omega^2 C_1 K_n T_2} \right) \left(\frac{1 + j\omega T_2}{1 + j\omega T_1} \right) \quad (6)$$

The phase margin (phase + 180) is thus determined by:

$$Q_p = \arctan(\omega T_2) - \arctan(\omega T_1) \quad (7)$$

At $\omega = \omega_p$, the derivative of the phase margin may be set to zero in order to assure maximum phase margin occurs at ω_p (see also Figure 98). This provides an expression for ω_p :

$$\frac{dQ_p}{d\omega} = 0 = \frac{T_2}{1 + (\omega T_2)^2} - \frac{T_1}{1 + (\omega T_1)^2} \quad (8)$$

$$\omega = \omega_p = \frac{1}{\sqrt{T_2 T_1}} \quad (9)$$

Or rewritten:

$$T_1 = \frac{1}{\omega_p^2 T_2} \quad (10)$$

By substituting into equation (7), solve for T2:

$$T_2 = \frac{\tan\left(\frac{Q_p}{2} + \frac{\pi}{4}\right)}{\omega_p} \quad (11)$$

By choosing a value for ω_p and Q_p , T_1 and T_2 can be calculated. The choice of Q_p determines the stability of the loop. In general, choosing a phase margin of 45 degrees is a good choice to start calculations. Choosing lower phase margins will provide somewhat faster lock-times, but also generate higher overshoots on the control line to the VCO. This will present a less stable system. Larger values of phase margin provide a more stable system, but also increase lock-times. The practical range for phase margin is 30 degrees up to 70 degrees.

The selection of ω_p is strongly related to the desired lock-time. Since it is quite complicated to accurately calculate lock time, a good first order approach is:

$$T_{lock} \approx \frac{3}{\omega_p} \quad (12)$$

Equation (12) only provides an order of magnitude for lock time. It does not clearly define what the exact frequency difference is from the desired frequency and it does not show the effect of phase margin. It assumes, however, that the phase detector steps up to the desired control voltage without hesitation. In practice, such step response approach is not really valid. If the two input frequencies are not locked, their phase maybe momentarily zero and force the phase detector into a high impedance mode. Hence, the lock times may be found to be somewhat higher.

In general, ω_p should be chosen far below the reference frequency in order for the filter to provide sufficient attenuation at that frequency. In some applications, the reference frequency might represent the spacing between channels. Any feedthrough to the VCO that shows up as a spur might affect adjacent channel rejection. In theory, with the loop in lock, there is no signal coming from the phase detector. But in practice small current pulses and leakage currents will be supplied to both the VCO and the phase detector. The external capacitors may show some leakage, too. Hence, the lower ω_p , the better the reference frequency is filtered, but the longer it takes for the loop to lock.

As shown in Figure 98, the open loop gain at ω_p is 1 (or 0 dB), and thus the absolute value of the complex open loop gain as shown in equation (6) solves C_1 :

$$C_1 = \left(\frac{K_{pd}K_oT_1}{\omega^2K_nT_2} \right) \sqrt{\frac{(1 + \omega_pT_2)^2}{(1 + \omega_pT_1)^2}} \quad (13)$$

With C_1 known, and equation (5) solve C_2 and R_2 :

$$C_2 = C_1 \left(\frac{T_2}{T_1} - 1 \right) \quad (14)$$

$$R_2 = \frac{T_2}{C_2} \quad (15)$$

The VCO gain is dependent on the selection of the external inductor and the frequency required. The free running frequency of the VCO is determined by:

$$f = \frac{1}{2\pi\sqrt{LC_T}} \quad (16)$$

In which L represents the external inductor value and C_T represents the total capacitance (including internal capacitance) in parallel with the inductor. The VCO gain can be easily calculated via the internal varicap transfer curve shown in Figure 43.

As can be derived from Figure 43, the varicap capacitance changes 2.0 pF over the voltage range from 1.0 V to 3.0 V:

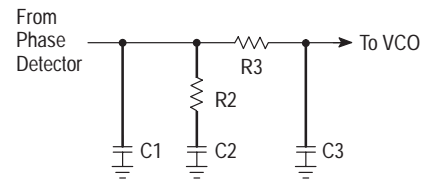
$$\Delta C_{var} = \frac{2.0 \text{ pF}}{2.0 \text{ V}} \quad (17)$$

Combining (16) with (17) the VCO gain can be determined by:

$$K_o = \frac{1}{j2.0V} \left\{ \frac{1}{2\pi\sqrt{LC_T}} - \frac{1}{2\pi\sqrt{L\left(C_T + \frac{\Delta C_{var}}{2}\right)}} \right\} \quad (18)$$

Although the basic loopfilter previously described provides adequate performance for most applications, an extra pole may be added for additional reference frequency filtering. Given that the channel spacing is based on the reference frequency, and any feedthrough to the first LO may effect parameters like adjacent channel rejection and intermodulation. Figure 100 shows a loopfilter architecture incorporating an additional pole.

Figure 49. Loop Filter with Additional Integrating Element



For the additional pole formed by R_3 and C_3 to be efficient, the cut-off frequency must be much lower than the reference frequency. However, it must also be higher than ω_p in order not to compromise phase margin too much. The following equations were derived in a similar manner as for the basic filter previously described.

Similarly, it can be shown:

$$A_{\text{openloop}} = -\frac{K_{pd}K_o}{K_n\omega^2((C1 + C2 + C3) - \omega^2C1C2C3R2R3)} + \frac{1 + j\omega T2}{1 + j\omega T1} \quad (19)$$

In which:

$$T1 = \frac{(C1 + C2)T2 + (C1C2)T3}{C1 + C2 + C3 - \omega^2C1T2T3} \quad (20)$$

$$T2 = R2C2 \quad (21) \quad T3 = R3C3 \quad (22)$$

From T1 it can be derived that:

$$C2 = \frac{(T1 + T2)C3 - C1(T2 + T3 - T1 + \omega^2T1T2T3)}{T3 - T1} \quad (23)$$

In analogy with (13), by forcing the loopgain to 1 (0 dB) at ω_p , we obtain:

$$C1(T1 + T2) + C2T3 + C3T2 = \left(\frac{K_{pd}K_o}{K_n\omega_p^2}\right) \sqrt{\frac{1 + (\omega_p T2)^2}{1 + (\omega_p T1)^2}} \quad (24)$$

Solving for C1:

$$C1 = \frac{(T2 - T1)T3C3 - (T3 - T1)T2C3 + (T3 - T1)\left(\frac{K_{pd}K_o T1}{\omega_p^2 K_n}\right) \sqrt{\frac{1 + (\omega_p T2)^2}{1 + (\omega_p T1)^2}}}{(T3 - T1)T2 + (T3 - T1)T3 - (T2 + T3 - T1 + \omega_p^2 T1 T2 T3)T3} \quad (25)$$

By selecting ω_p via (12), the additional time constant expressed as T3, can be set to:

$$T3 = \frac{1}{K\omega_p} \quad (26)$$

The K-factor shown determines how far the additional pole frequency will be separated from ω_p . Selecting too small of a K-factor, the equations may provide negative capacitance or resistor values. Too large of a K-factor may not provide the maximum attenuation.

By selecting R3 to be 100 k Ω , C3 becomes known and C1 and C2 can be solved from the equations. By using equations (11) and (10), time constants T2 and T1 can be derived by selecting a phase margin. Finally, R2 follows from T2 and C2.

A test circuit with the following components and conditions was constructed with these results:

Loop Filter (See Figure 100):

- C1 = 470 pF
- R2 = 68 k Ω
- C2 = 3.9 nF
- R3 = 270 k Ω
- C3 = 82 pF

LO2 Tank:

- Ctotal = 39.3 pF
- Lext = 150 nH, Q = 50 @ 250 MHz
- Reference Frequency = 10.24 MHz (unadjusted)
- R Counter = 205
- LO2 Counter = 1266
- AC Load = 25 Ω
- Frequency of LO2 = 63.258 MHz
- Phase Noise @ 50 kHz offset = -107 dBc
- Sidebands @ 50 kHz & 100 kHz offsets = -69 dBc

Low Battery/ RSSI Voltage Measurement

Both the Low Battery (bits 5/23–18) and RSSI (bits 5/17–12) measurement circuits have a 6-bit A/D converter whose value may be read back via the SPI. The A/D's sample their voltages at a frequency equal to the internal SCF clock frequency divided by 128. The Low Battery Measurement A/D senses and divides by 2.5 the supply voltage (at Pin 23). Please note that the minimum Low Battery Detect (LBD) voltage is 2.7 V, since there is no guarantee that the device will operate below this value. The RSSI Measurement senses the voltage at Pin 37.

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These values are compared to the internal reference VB (≈ 1.5 V) which is available at Pin 37. The value read back from the LBD A/D will therefore be approximately:

$$N(\text{for LBD}) \approx \frac{63 (V_{CC})}{2.5(V_B)(1.07)} \quad (27)$$

and for the RSSI

$$N(\text{for RSSI}) \approx \frac{63 (\text{RSSI Voltage})}{(V_B)(1.07)} \quad (28)$$

VB Voltage Adjust and Characteristics

VB has a production tolerance of $\pm 8\%$, and can be adjusted over a $\pm 9\%$ range using bits 3/20–17. The adjustment steps will be $\approx 1.2\%$ each (See Table 8). If desired, VB can be used to bias external circuitry, as long as the load current on this pin does not exceed $10 \mu\text{A}$. VB varies by less than $\pm 0.5\%$ over supply voltage, referenced to $V_{CC} = 3.6$ V.

The value of the de-coupling capacitor connected from VB to ground affects both the noise and crosstalk from the receive and transmit audio paths, so the value should be chosen with caution. Figures 50 and 51 show this relationship.

Table 8. VB Voltage Reference Programming

V _{ref} Adjust Bit #20	V _{ref} Adjust Bit #19	V _{ref} Adjust Bit #18	V _{ref} Adjust Bit #17	V _{ref} Adjust #	Voltage Reference Adjustment Amount
0	0	0	0	0	-9.0%
0	0	0	1	1	-7.8%
0	0	1	0	2	-6.6%
0	0	1	1	3	-5.4%
0	1	0	0	4	-4.2%
0	1	0	1	5	-3.0%
0	1	1	0	6	-1.8%
0	1	1	1	7	-0.6%
1	0	0	0	8	0.6%
1	0	0	1	9	1.8%
1	0	1	0	10	3.0%
1	0	1	1	11	4.2%
1	1	0	0	12	5.4%
1	1	0	1	13	6.6%
1	1	1	0	14	7.8%
1	1	1	1	15	9.0%

Figure 50. Crosstalk/Noise from C In to E Out versus VB Capacitor

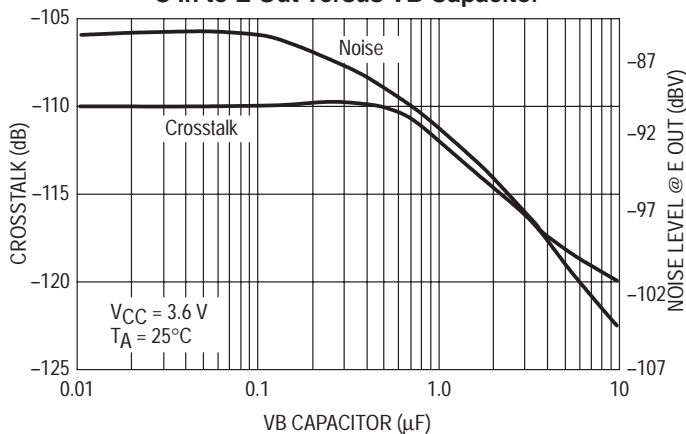
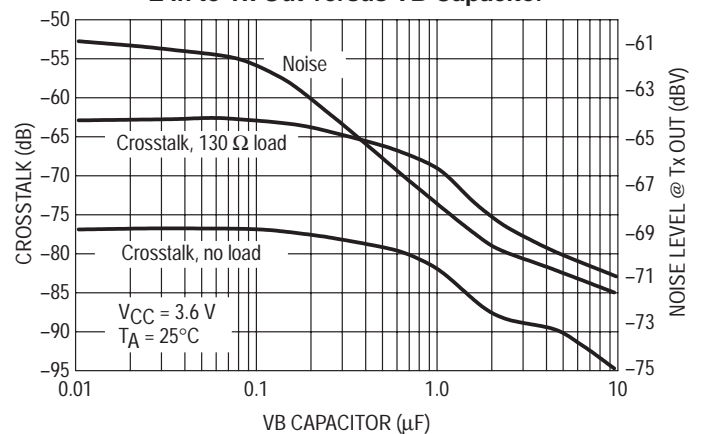


Figure 51. Crosstalk/Noise from E In to Tx Out versus VB Capacitor



MCU Serial Interface

The MCU Serial Interface is a 3-wire interface, consisting of a Clock line, an Enable line, and a bi-directional Data line. The interface is always active, i.e., it cannot be powered down as all other sections of the MC33411 are disabled and enabled through this interface.

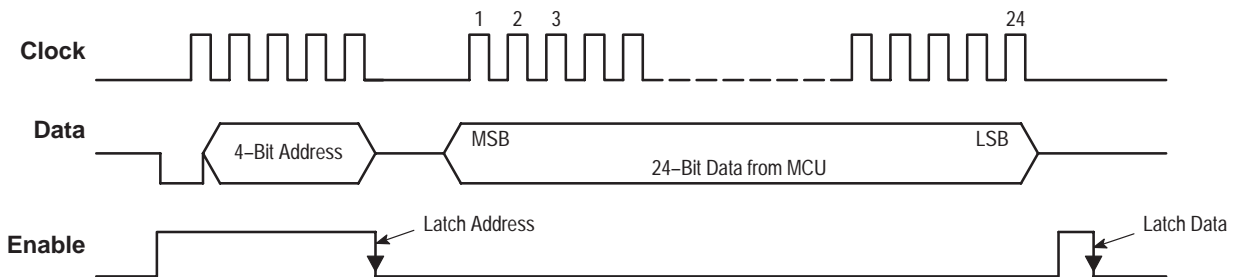
After the device power-up (or whenever a reset condition is required), the MCU should perform the following steps:

14. Initialize the Data line to a high impedance state.
15. Initialize the Clock line to a logic low.
16. Initialize the Enable line to a logic low.
17. Pulse the Clock line a minimum of once (RZ format) while leaving the Enable line continuously low. This places the SPI port into a known condition.
18. Load all registers with their desired initial values.

The clock (Return-to-Zero format) must be supplied to the MC33411 at Pin 11 to write or read data, and can be any frequency up to 2.0 MHz. The clock need not be present when data is not being transferred. The Enable line must be low when data is not being transferred.

Internally there are 7 data registers, 24-bits each, addressed with 4-bits ranging from \$h1 to \$h7 (see Tables 9 and 10). Register 5, bits 23–12 are read-only bits, while all other register bits are Read/Write. All unused/unimplemented bits are reserved for Motorola use only. The contents of the 7 registers can be read out at any time. All bits are written in, or read out, on the clock's positive transition. The write and read operations are as follows:

Figure 52. Writing Data to the MC33411

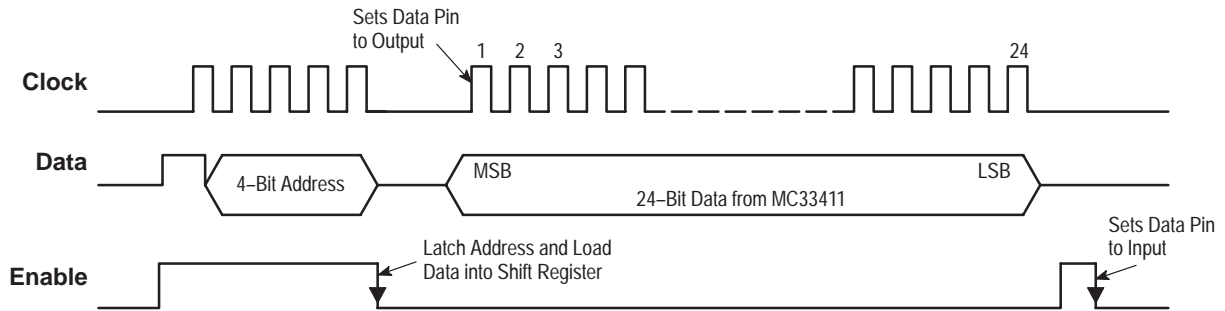


a. Write Operation:

- To write data to the MC33411, the following sequence is required (see Figure 52):
19. The Enable line is taken high.
 20. Five bits are entered:
 - The first bit must be a 0 to indicate a Write operation.
 - The next four bits identify the register address (0001–0111). The MSB is entered first.
 21. The Enable line is taken low. At this transition, the address is latched in and decoded.
 22. The Enable line is maintained low while the data bits are clocked in. The MSB is entered first, and the LSB last. If 24-bits are written to a register which has less than 24 active bits (e.g., register 6), the unassigned bits are to be 0.
 23. After the last bit is entered, the Enable line is to be taken high and then low. The falling edge of this pulse latches in the just entered data. The clock line must be at a logic low and must not transition in either direction during this Enable pulse.
 24. The Enable line must then be kept low until the next communication.

Note: If less than 24 bits are to be written to a data register, it is not necessary to enter the full 24 bits, as long as they are all lower order bits. For example, if bits 0–6 of a register are to be updated, they can be entered as 7 bits with 7 clock cycles in step 4 above. However, if this procedure is used, a minimum of 4 bits, with 4 clock pulses, must be entered.

Figure 53. Reading Data from the MC33411



b. Read Operation:

- To read the output bits (bits 5/23–12), or the contents of any register, the following sequence is required (see Figure 53):

1. The Enable line is taken high.
2. Five bits are entered:
 - The first bit must be a 1 to indicate a Read operation.
 - The next four bits identify the register address (0001–0111). The MSB is entered first.
3. The Enable line is taken low. At this transition, the address is latched in and decoded, and the contents of the selected register is loaded into the 24-bit output shift register. At this point, the Data line (Pin 12) is still an input.
4. While maintaining the Enable line low, the data is read out. The first clock rising edge will change the Data line to an output, and the MSB will be present on this line.
5. The full contents of the register are then read out (MSB first, LSB last) with a total of 24 clock rising edges, including the one in step 4 above. It is recommended that the MCU read the bits after the clock's falling edge.
6. After the last clock pulse, the Enable line is to be taken high and then low. The falling edge of this pulse returns the Data Pin to be an input. The clock line must be at a logic low and must not transition in either direction during this Enable pulse.
7. The Enable line must then be kept low until the next communication.

Power Supply/Power Saving Modes

The power supply voltage, applied to all V_{CC} pins, can range from 2.7 to 5.5 V. All V_{CC} pins must be within ± 0.5 V of each other, and each must be bypassed. It is recommended a ground plane be used, and all leads to the MC33411 be as short and direct as possible. To reduce the possibility of device latch-up, it is highly recommended that the Audio, Synthesizer and RF V_{CC} portions of the chip be isolated from the main supply through 10 to 25 Ω resistors (see the Evaluation PCB Schematic, Figure 54). This also provides RF-to-Audio noise isolation. The supply and ground pins are distributed as follows:

1. Pin 23 provides power to the audio section. Pin 40 is the ground pin.
2. Pin 28 provides power to the speaker amplifier section. Pin 31 is the ground pin.

3. Pin 3 provides power to the Rx PLL section. Pin 5 is the ground pin.
4. Pin 7 provides power to the Tx PLL section, and the MCU interface. Pin 5 is the ground pin.
5. Pin 42 provides power to the 2nd LO section. Pins 46 and 48 are the ground pins.
6. Pin 14 is the ground pin for the digital circuitry. Power for the digital circuitry is derived from Pin 23.

To conserve power, various sections can be individually disabled by using bits 5/7–0 and 6/7 (setting a bit to 1 disables the section).

1. Reference Oscillator Disable (bit 5/0) – The reference oscillator at Pins 15 and 16 is disabled, thereby denying a clock to the three PLLs and the switched capacitor filters. This function is not available on the “B” version.
2. Tx PLL Disable (bit 5/1) – The 13-bit and 7-bit counters, input buffer, phase detector, and modulus control blocks are disabled. The charge pump output at Pin 6 will be in a Hi-Z state.
3. Rx PLL Disable (bit 5/2) – The 13-bit and 7-bit counters, input buffer, phase detector, and modulus control blocks are disabled. The charge pump output at Pin 4 will be in a Hi-Z state.
4. LO2 PLL Disable (bit 5/3) – The VCO, 14-bit counter, output buffer, and phase detector are disabled. The charge pump output at Pin 47 will be in a Hi-Z state.
5. Power Amplifier Disable (bit 5/4) – The two speaker amplifiers are disabled. Their outputs will go to a high impedance state.
6. Rx Audio Path Disable (bit 5/5) – The anti-aliasing filter, low-pass filter, and variable gain stage are disabled.
7. Tx Audio Path Disable (bit 5/6) – Disables the microphone amplifier and low-pass filter.
8. Low Battery/RSSI Measurement Disable (bit 5/7) – Both 6-bit A/Ds are disabled.
9. Data Slicer Disable (bit 5/8) – The data slicer is disabled and DS Out goes to high impedance.
10. MCU Clock Disable (bit 6/7) – The MCU clock counter is disabled and the MCU Clock Output will be in a Hi-Z state. This function is not available on the “B” version.

Note: The 12-bit reference counter is disabled if the three PLLs are disabled (bits 5/1–3 = 1).

Table 9. Register Map

Reg Add	Reg Num	MSB Bit 23	Bit 22	Bit 21	Bit 20	Bit 19	Bit 18	Bit 17	Bit 16	Bit 15	Bit 14	Bit 13	Bit 12	Bit 11	Bit 10	Bit 9	Bit 8	Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	LSB Bit 0			
0001	1			Tx Polarity Select	Tx PD Cur Sel	MSB														MSB						LSB		
0010	2			Rx Polarity Select	Rx PD Cur Sel	MSB														MSB						LSB		
0011	3						VB Voltage Reference Adjust		FTxMC/FRxMC Mode	LO2 Polarity Select	2nd LO PD Cur Sel	MSB														LSB		
0100	4		Test Modes		LO2 Capacitor Select		6-Bit Switched Capacitor Filter Counter Divide Value					MSB														LSB		
0101	5		6-Bit Battery Voltage A/D Output									6-Bit RSSI/A/D Output														LSB		
0110	6												ALC Gain = 25	ALC Gain = 10	Side Tone Attenuate Select	Data Slicer Invert	Data Slicer Disable	Comp. Low Max. Gain En.	MCU Clk Disable	Tx Audio ALC Disable	Rx Audio Limiter Disable	Rx Audio Disable	Tx Audio Disable	Power Amp Disable	2nd LO PLL Expander Pass-through	Rx PLL Disable	Tx PLL Disable	Ref Osc Disable
0111	7														Volume Control													

* These bits not included in "B" version.

Table 10. Register Map: Power-Up Defaults

Reg Add	Reg Num	MSB Bit 23	Bit 22	Bit 21	Bit 20	Bit 19	Bit 18	Bit 17	Bit 16	Bit 15	Bit 14	Bit 13	Bit 12	Bit 11	Bit 10	Bit 9	Bit 8	Bit 7	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	LSB Bit 0			
0001	1			Tx Polarity Select	Tx PD Cur Sel	MSB																				LSB		
0010	2			Rx Polarity Select	Rx PD Cur Sel	MSB																				LSB		
0011	3						VB Voltage Reference Adjust		FTxMC/FRxMC Mode	LO2 Polarity Select	2nd LO PD Cur Sel	MSB														LSB		
0100	4		Test Modes		LO2 Capacitor Select		6-Bit Switched Capacitor Filter Counter Divide Value					MSB														LSB		
0101	5		6-Bit Battery Voltage A/D Output									6-Bit RSSI/A/D Output														LSB		
0110	6												ALC Gain = 25	ALC Gain = 10	Side Tone Attenuate Select	Data Slicer Invert	Data Slicer Disable	Comp. Low Max. Gain En.	MCU Clk Disable	Tx Audio ALC Disable	Rx Audio Limiter Disable	Rx Audio Disable	Tx Audio Disable	Power Amp Disable	2nd LO PLL Expander Pass-through	Rx PLL Disable	Tx PLL Disable	Ref Osc Disable
0111	7													Volume Control														

* These bits not included in "B" version.

MC33411A/B

Evaluation PCB

The evaluation PCB is a versatile board which allows the MC33411 to be configured to analyze individual operating parameters or the complete audio transmit and receive paths.

The general purpose schematic and associated parts list for the PCB are given in Figure 54. With the jumpers

positioned as shown in the parts list (either shunt or open), the PCB is configured to analyze complete transmit and receive audio paths.

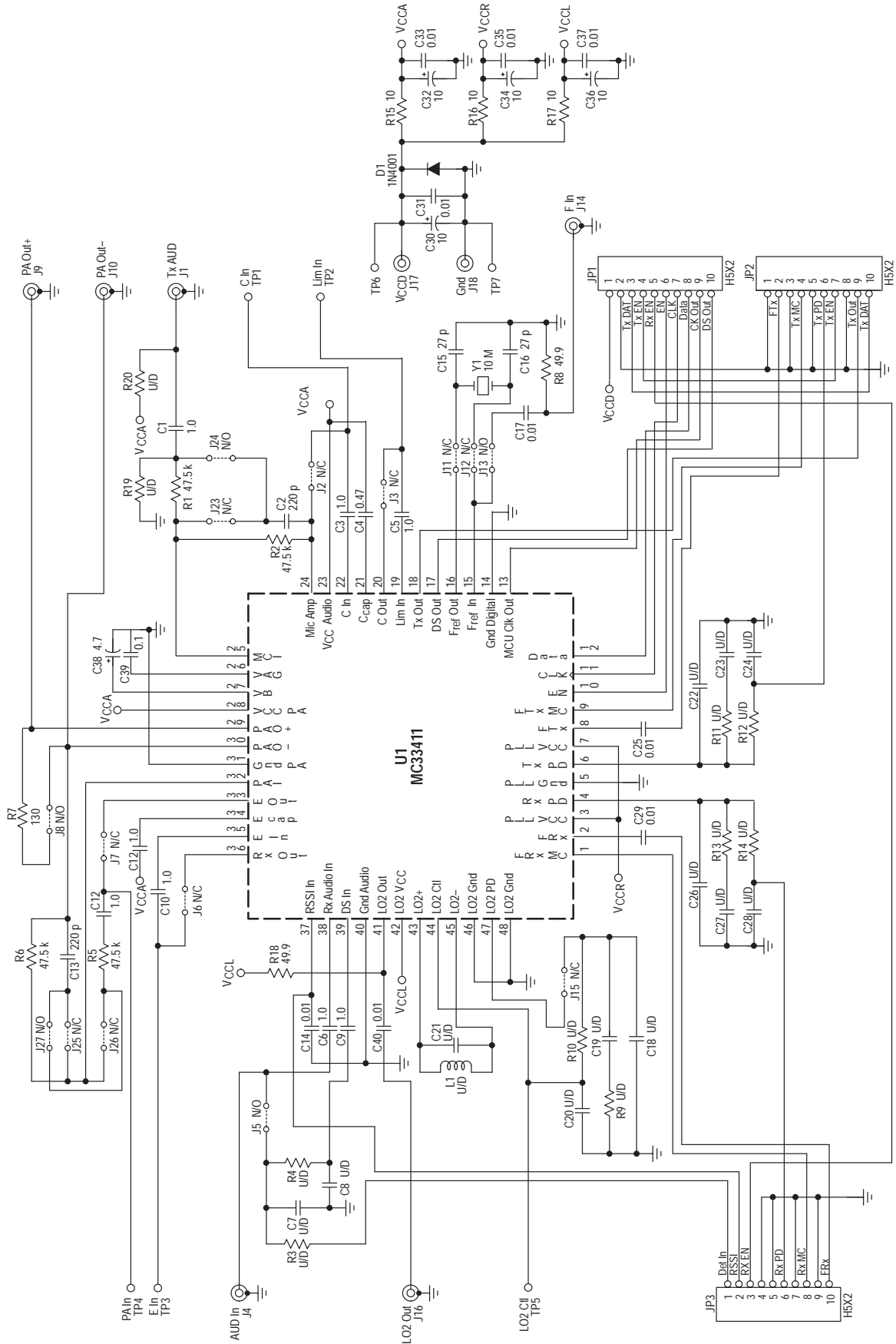
Parts lists as "user defined" can be installed to analyze other functions of the device. Table 2 lists these devices along with their respective functions.

Table 11.

Component(s)	Function	Notes
R20	Microphone Bias	
R19,J24,J27	Pre-emphasis/De-emphasis	
R3,C7,J5	Detector Low-Pass Filter (LPF)	
R4,C8	Data Slicer LPF	
L1,C21	2nd LO Tank	See Equations 16 and 17
C18,R9,C19,R10,C20	2nd LO LPF	See Eq. 10, 11, 12, 21, 23, 25, and 26
C26,R13,C27,R14,C28	Rx 1st LO LPF	See Eq. 10, 11, 12, 21, 23, 25, and 26
C22,R11,C23,R12,C24	Tx 1st LO LPF	See Eq. 10, 11, 12, 21, 23, 25, and 26

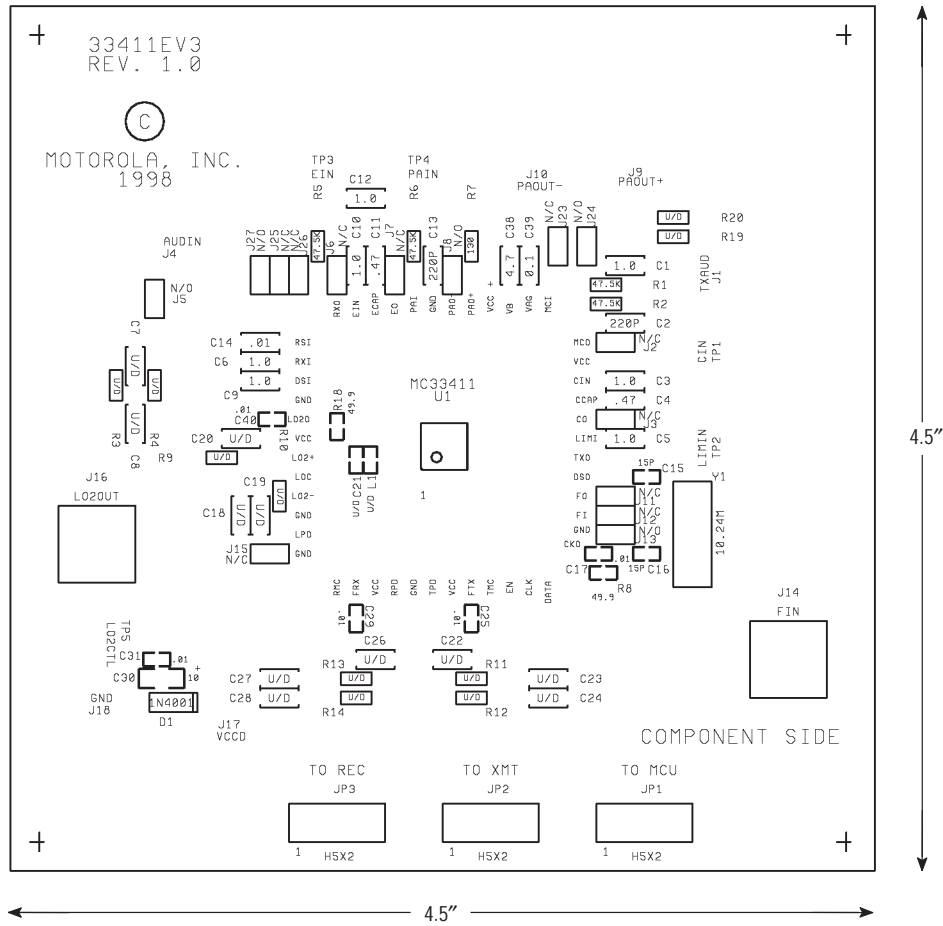
MC33411A/B

Figure 54. MC33411A/B Evaluation PCB Schematic



MC33411A/B

Figure 55. MC33411A/B Evaluation PCB Component Side

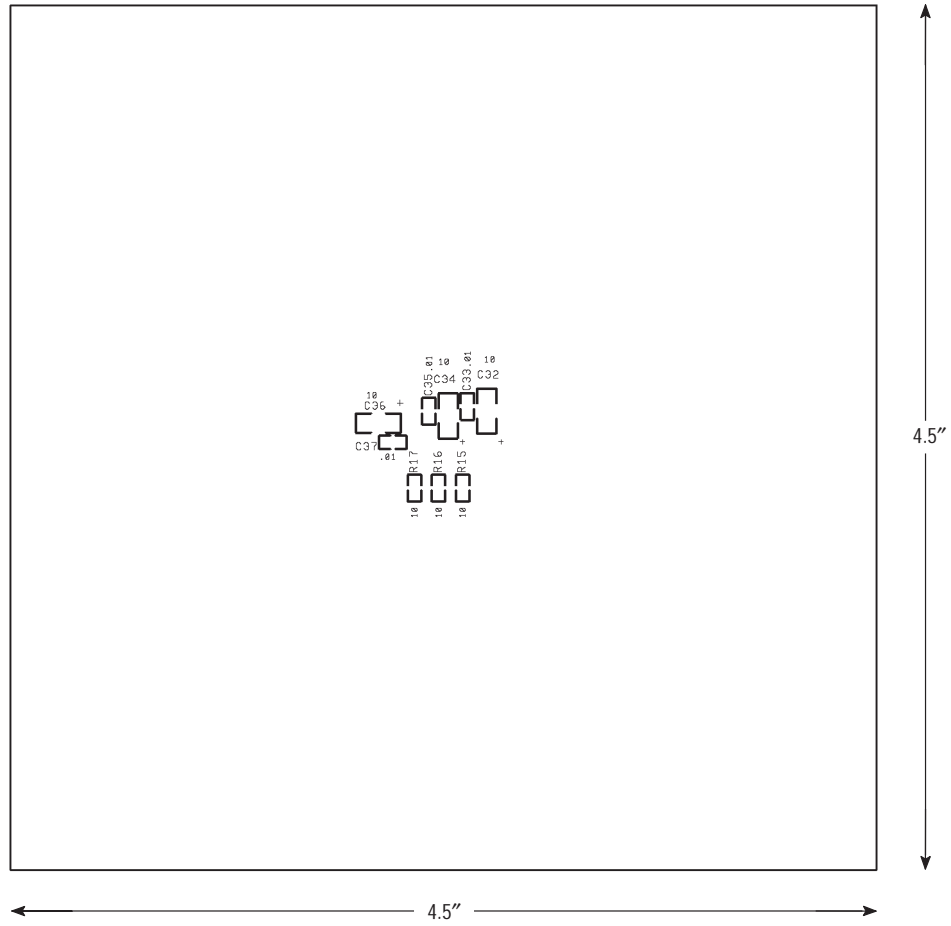


C1,C3,C5,C6,C9,C10,C12	1.0	JP1,JP2,JP3	Header, 5x2
C13,C2	220 p	J1,J4,J9,J10	AudioJack
C4,C11	0.47		Switchcraft 3501FP
L1,R3,R4,C7,C8,R9,R10, R11,R12,R13,R14,C18,R19, C19,R20,C20,C21,C22,C23, C24,C26,C27,C28	User defined	J2,J3,J6,J7,J11,J12,J15, J23,J25,J26	Shunt
C14,C17,C25,C29,C31,C33, C35,C37,C40	0.01	J5,J8,J13,J24,J27	Open
C15,C16	27 p	J14,J16	SMA EF Johnson 142-0701-201
C30,C32,C34,C36	10	J17,J18	Bananna Johnson Components 108-0902-001
C38	4.7	R1,R2,R5,R6	47.5 k
C39	0.1	R7	130
D1	1N4001	R8,R18	49.9
		R15,R16,R17	10
		U1	MC33411AFTA or MC33411BFTA
		Y1	10 M Raltron A-10.000-18

Default Units: Microfarads, Microhenries, and Ohms

MC33411A/B

Figure 56. MC33411A/B Evaluation PCB Solder Side



Digital-to-Analog Converters with Serial Interface

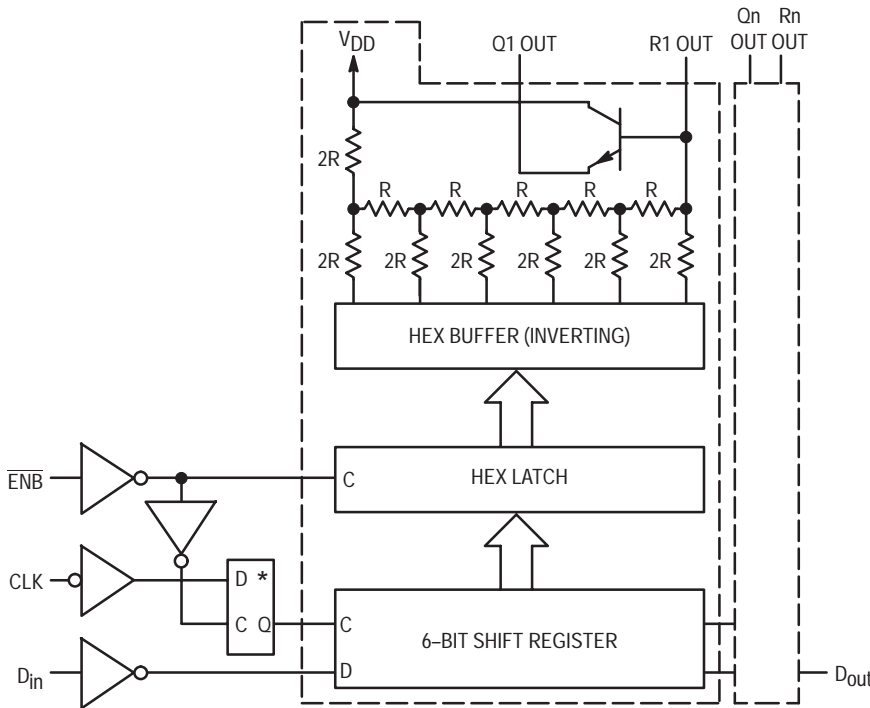
CMOS LSI

The MC144110 and MC144111 are low-cost 6-bit D/A converters with serial interface ports to provide communication with CMOS microprocessors and microcomputers. The MC144110 contains six static D/A converters; the MC144111 contains four converters.

Due to a unique feature of these DACs, the user is permitted easy scaling of the analog outputs of a system. Over a 5 to 15 V supply range, these DACs may be directly interfaced to CMOS MPUs operating at 5 V.

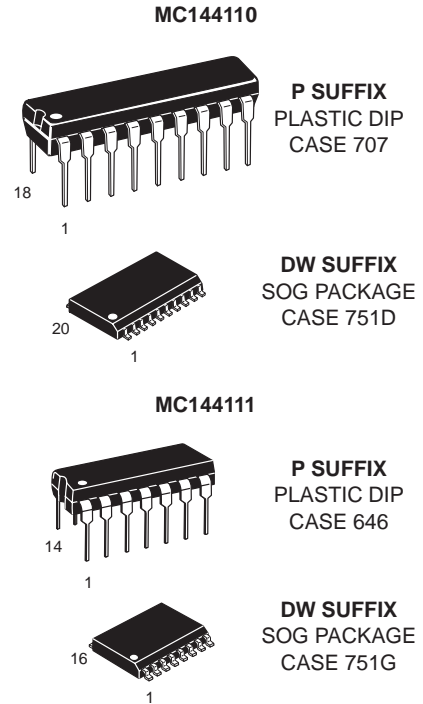
- Direct R-2R Network Outputs
- Buffered Emitter-Follower Outputs
- Serial Data Input
- Digital Data Output Facilitates Cascading
- Direct Interface to CMOS μ P
- Wide Operating Voltage Range: 4.5 to 15 V
- Wide Operating Temperature Range: 0 to 85°C
- Software Information is Contained in Document M68HC11RM/AD

BLOCK DIAGRAM



* Transparent Latch

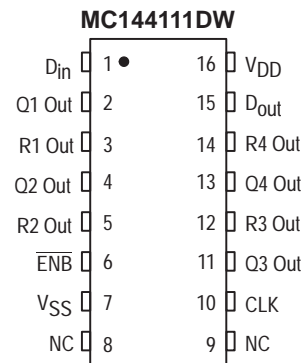
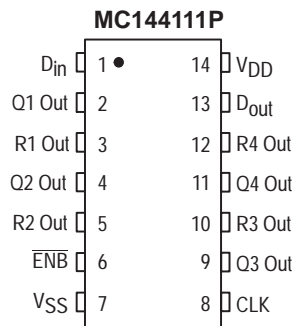
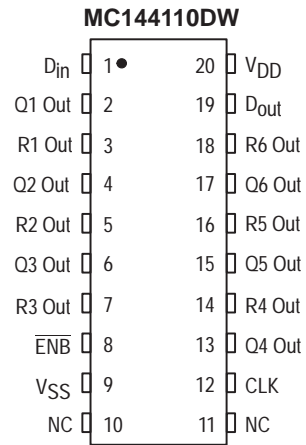
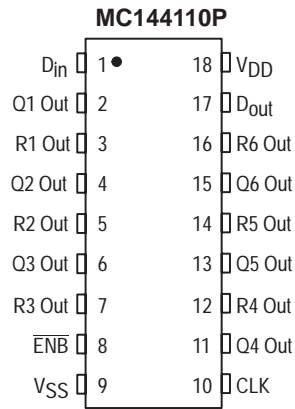
MC144110 MC144111



ORDERING INFORMATION

MC144110P	Plastic DIP
MC144110DW	SOG Package
MC144111P	Plastic DIP
MC144111DW	SOG Package

PIN ASSIGNMENTS



NC = NO CONNECTION

MAXIMUM RATINGS* (Voltages referenced to V_{SS})

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{DD}	- 0.5 to + 18	V
Input Voltage, All Inputs	V_{in}	- 0.5 to $V_{DD} + 0.5$	V
DC Input Current, per Pin	I	± 10	mA
Power Dissipation (Per Output) $T_A = 70^\circ\text{C}$, MC144110 MC144111 $T_A = 85^\circ\text{C}$, MC144110 MC144111	P_{OH}	30 50 10 20	mW
Power Dissipation (Per Package) $T_A = 70^\circ\text{C}$, MC144110 MC144111 $T_A = 85^\circ\text{C}$, MC144110 MC144111	P_D	100 150 25 50	mW
Storage Temperature Range	T_{stg}	- 65 to + 150	$^\circ\text{C}$

* Maximum Ratings are those values beyond which damage to the device may occur.

This device contains protection circuitry to guard against damage due to high static voltages or electric fields; however, it is advised that precautions be taken to avoid application of voltage higher than maximum rated voltages to this high-impedance circuit. For proper operation it is recommended that V_{in} and V_{out} be constrained to the range $V_{SS} \leq (V_{in} \text{ or } V_{out}) \leq V_{DD}$.

Unused inputs must always be tied to an appropriate logic voltage level (e.g., either V_{SS} or V_{DD}).

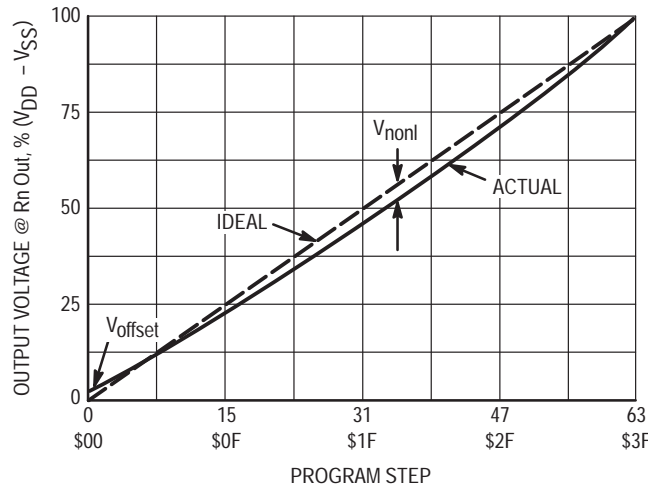
ELECTRICAL CHARACTERISTICS (Voltages referenced to V_{SS} , $T_A = 0$ to 85°C unless otherwise indicated)

Symbol	Parameter	Test Conditions	V_{DD}	Min	Max	Unit
V_{IH}	High-Level Input Voltage (D_{in} , \overline{ENB} , CLK)		5 10 15	3.0 3.5 4	— — —	V
V_{IL}	Low-Level Input Voltage (D_{in} , \overline{ENB} , CLK)		5 10 15	— — —	0.8 0.8 0.8	V
I_{OH}	High-Level Output Current (D_{out})	$V_{out} = V_{DD} - 0.5 \text{ V}$	5	- 200	—	μA
I_{OL}	Low-Level Output Current (D_{out})	$V_{out} = 0.5 \text{ V}$	5	200	—	μA
I_{DD}	Quiescent Supply Current MC144110 MC144111	$I_{out} = 0 \mu\text{A}$	15 15	— —	12 8	mA
I_{in}	Input Leakage Current (D_{in} , \overline{ENB} , CLK)	$V_{in} = V_{DD}$ or 0 V	15	—	± 1	μA
V_{nonl}	Nonlinearity Voltage (R_n Out)	See Figure 1	5 10 15	— — —	100 200 300	mV
V_{step}	Step Size (R_n Out)	See Figure 2	5 10 15	19 39 58	137 274 411	mV
V_{offset}	Offset Voltage from V_{SS}	$D_{in} = \$00$, See Figure 1	—	—	1	LSB
I_E	Emitter Leakage Current	$V_{Rn \text{ Out}} = 0 \text{ V}$	15	—	10	μA
h_{FE}	DC Current Gain	$I_E = 0.1$ to 10.0 mA $T_A = 25^\circ\text{C}$	—	40	—	—
V_{BE}	Base-to-Emitter Voltage Drop	$I_E = 1.0 \text{ mA}$	—	0.4	0.7	V

SWITCHING CHARACTERISTICS

(Voltages referenced to V_{SS} , $T_A = 0$ to 85°C , $C_L = 50$ pF, Input $t_r = t_f = 20$ ns unless otherwise indicated)

Symbol	Parameter	V_{DD}	Min	Max	Unit
t_{wH}	Positive Pulse Width, CLK (Figures 3 and 4)	5	2	—	μs
		10	1.5	—	
		15	1	—	
t_{wL}	Negative Pulse Width, CLK (Figure 3 and 4)	5	5	—	μs
		10	3.5	—	
		15	2	—	
t_{su}	Setup Time, $\overline{\text{ENB}}$ to CLK (Figures 3 and 4)	5	5	—	μs
		10	3.5	—	
		15	2	—	
t_{su}	Setup Time, D_{in} to CLK (Figures 3 and 4)	5	1000	—	ns
		10	750	—	
		15	500	—	
t_h	Hold Time, CLK to $\overline{\text{ENB}}$ (Figures 3 and 4)	5	5	—	μs
		10	3.5	—	
		15	2	—	
t_h	Hold Time, CLK to D_{in} (Figures 3 and 4)	5	5	—	μs
		10	3.5	—	
		15	2	—	
t_r, t_f	Input Rise and Fall Times	5 – 15	—	2	μs
C_{in}	Input Capacitance	5 – 15	—	7.5	pF



LINEARITY ERROR (integral linearity). A measure of how straight a device's transfer function is, it indicates the worst-case deviation of linearity of the actual transfer function from the best-fit straight line. It is normally specified in parts of an LSB.

Figure 1. D/A Transfer Function

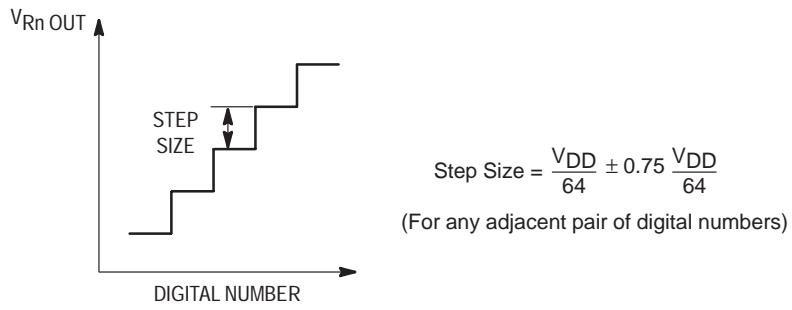


Figure 2. Definition of Step Size

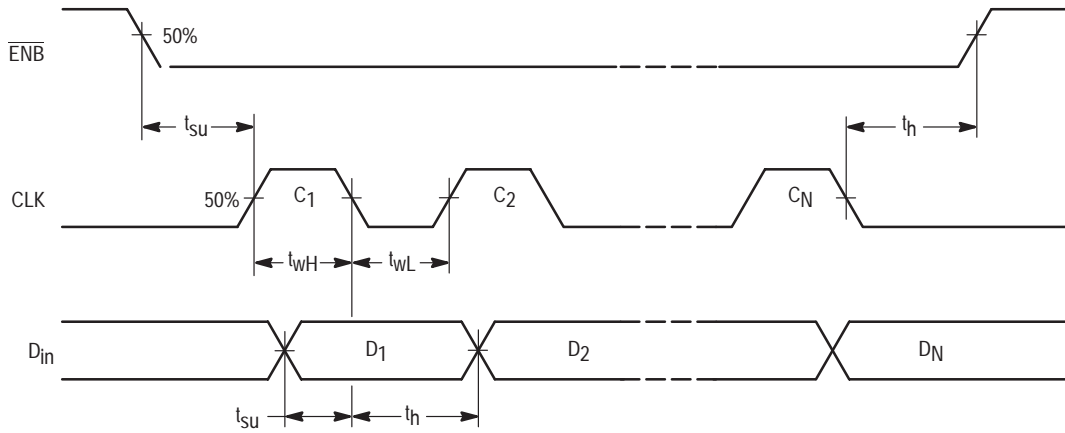


Figure 3. Serial Input, Positive Clock

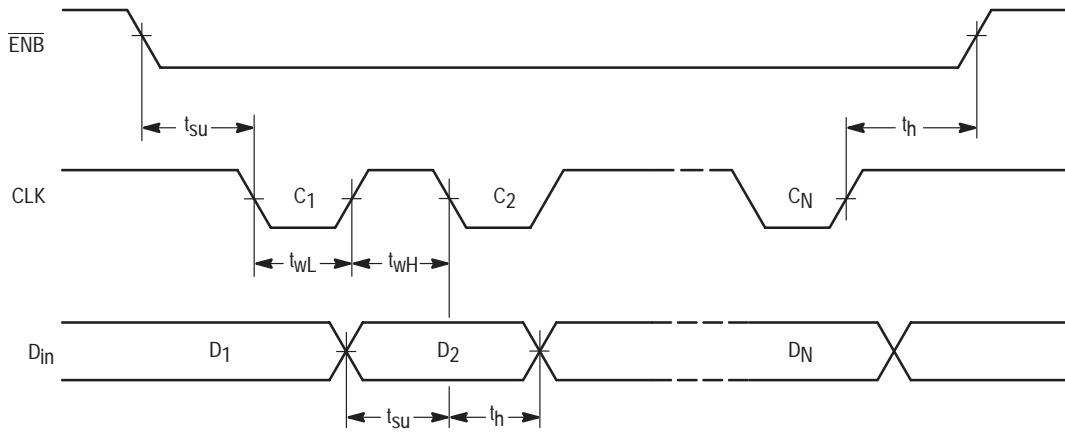


Figure 4. Serial Input, Negative Clock

PIN DESCRIPTIONS

INPUTS

D_{in} Data Input

Six-bit words are entered serially, MSB first, into digital data input, D_{in} . Six words are loaded into the MC144110 during each D/A cycle; four words are loaded into the MC144111.

The last 6-bit word shifted in determines the output level of pins Q1 Out and R1 Out. The next-to-last 6-bit word affects pins Q2 Out and R2 Out, etc.

\overline{ENB} Negative Logic Enable

The \overline{ENB} pin must be low (active) during the serial load. On the low-to-high transition of \overline{ENB} , data contained in the shift register is loaded into the latch.

CLK Shift Register Clock

Data is shifted into the register on the high-to-low transition of CLK. CLK is fed into the D-input of a transparent latch, which is used for inhibiting the clocking of the shift register when \overline{ENB} is high.

The number of clock cycles required for the MC144110 is usually 36. The MC144111 usually uses 24 cycles. See Table 1 for additional information.

OUTPUTS

D_{out} Data Output

The digital data output is primarily used for cascading the DACs and may be fed into D_{in} of the next stage.

R1 Out through Rn Out Resistor Network Outputs

These are the R-2R resistor network outputs. These outputs may be fed to high-impedance input FET op amps to bypass the on-chip bipolar transistors. The R value of the resistor network ranges from 7 to 15 k Ω .

Q1 Out through Qn Out NPN Transistor Outputs

Buffered DAC outputs utilize an emitter-follower configuration for current-gain, thereby allowing interface to low-impedance circuits.

SUPPLY PINS

V_{SS} Negative Supply Voltage

This pin is usually ground.

V_{DD} Positive Supply Voltage

The voltage applied to this pin is used to scale the analog output swing from 4.5 to 15 V p-p.

Table 1. Number of Channels vs Clocks Required

Number of Channels Required	Number of Clock Cycles	Outputs Used on MC144110	Outputs Used on MC144111
1	6	Q1/R1	Q1/R1
2	12	Q1/R1, Q2/R2	Q1/R1, Q2/R2
3	18	Q1/R1, Q2/R2, Q3/R3	Q1/R1, Q2/R2, Q3/R3
4	24	Q1/R1, Q2/R2, Q3/R3, Q4/R4	Q1/R1, Q2/R2, Q3/R3, Q4/R4
5	30	Q1/R1, Q2/R2, Q3/R3, Q4/R4, Q5/R5	Not Applicable
6	36	Q1/R1, Q2/R2, Q3/R3, Q4/R4, Q5/R5, Q6/R6	Not Applicable

Encoder and Decoder Pairs CMOS

These devices are designed to be used as encoder/decoder pairs in remote control applications.

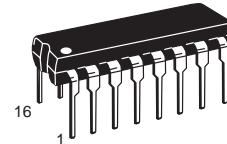
The MC145026 encodes nine lines of information and serially sends this information upon receipt of a transmit enable (\overline{TE}) signal. The nine lines may be encoded with trinary data (low, high, or open) or binary data (low or high). The words are transmitted twice per encoding sequence to increase security.

The MC145027 decoder receives the serial stream and interprets five of the trinary digits as an address code. Thus, 243 addresses are possible. If binary data is used at the encoder, 32 addresses are possible. The remaining serial information is interpreted as four bits of binary data. The valid transmission (VT) output goes high on the MC145027 when two conditions are met. First, two addresses must be consecutively received (in one encoding sequence) which both match the local address. Second, the 4 bits of data must match the last valid data received. The active VT indicates that the information at the Data output pins has been updated.

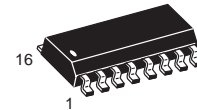
The MC145028 decoder treats all nine trinary digits as an address which allows 19,683 codes. If binary data is encoded, 512 codes are possible. The VT output goes high on the MC145028 when two addresses are consecutively received (in one encoding sequence) which both match the local address.

- Operating Temperature Range: -40 to $+85^{\circ}\text{C}$
- Very-Low Standby Current for the Encoder: 300 nA Maximum @ 25°C
- Interfaces with RF, Ultrasonic, or Infrared Modulators and Demodulators
- RC Oscillator, No Crystal Required
- High External Component Tolerance; Can Use $\pm 5\%$ Components
- Internal Power-On Reset Forces All Decoder Outputs Low
- Operating Voltage Range: MC145026 = 2.5 to 18 V*
MC145027, MC145028 = 4.5 to 18 V
- For Infrared Applications, See Application Note AN1016/D

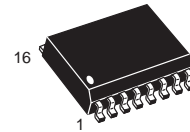
MC145026
MC145027
MC145028



P SUFFIX
PLASTIC DIP
CASE 648



D SUFFIX
SOG PACKAGE
CASE 751B

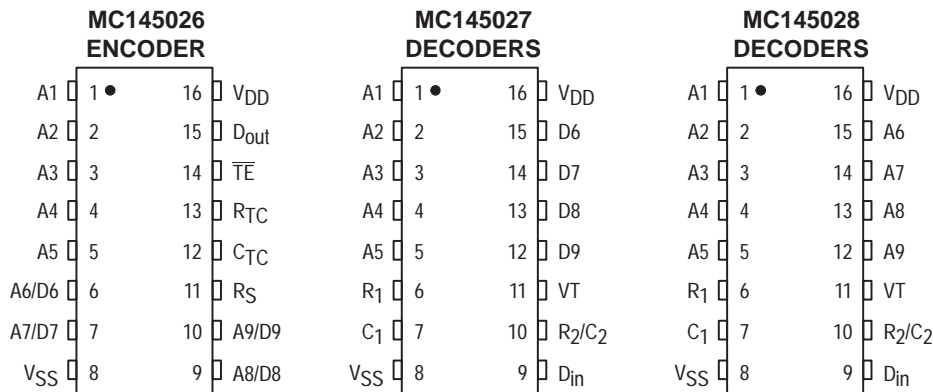


DW SUFFIX
SOG PACKAGE
CASE 751G

ORDERING INFORMATION

MC145026P	Plastic DIP
MC145026D	SOG Package
MC145027P	Plastic DIP
MC145027DW	SOG Package
MC145028P	Plastic DIP
MC145028DW	SOG Package

PIN ASSIGNMENTS



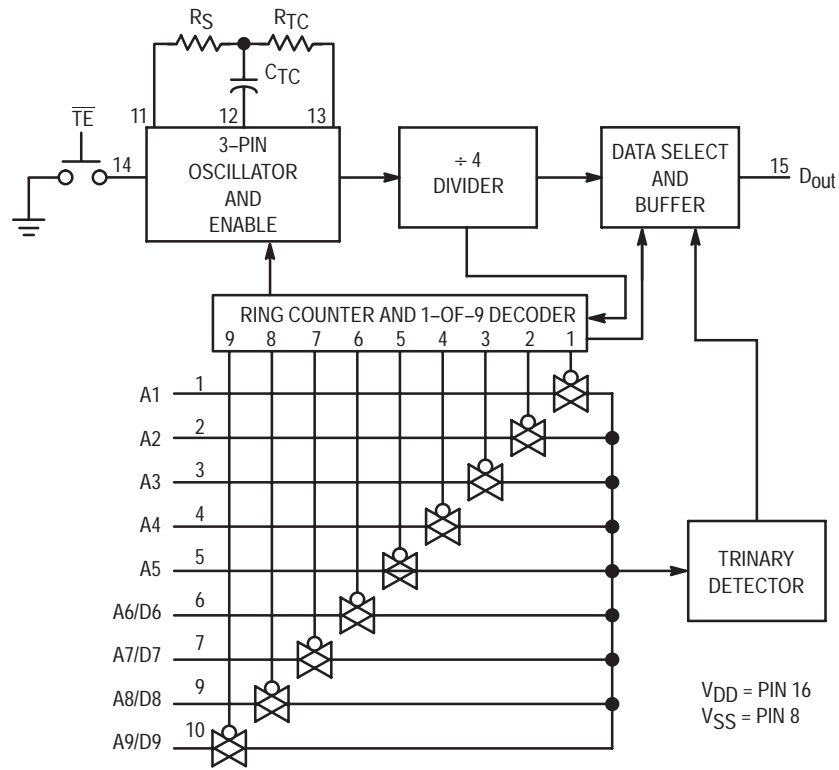


Figure 1. MC145026 Encoder Block Diagram

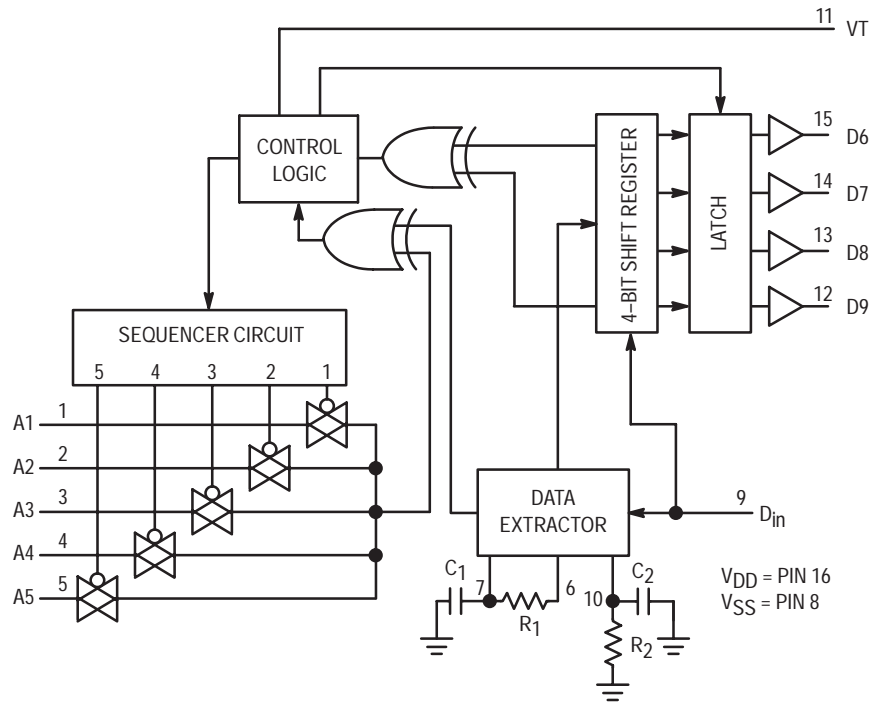


Figure 2. MC145027 Decoder Block Diagram

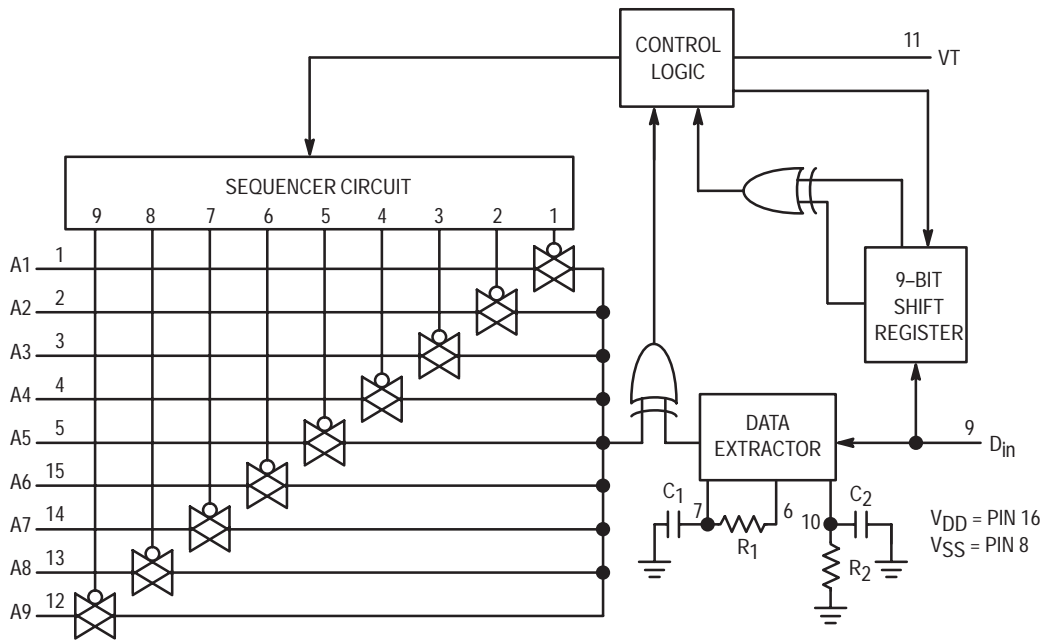


Figure 3. MC145028 Decoder Block Diagram

MAXIMUM RATINGS* (Voltages Referenced to V_{SS})

Rating	Symbol	Value	Unit
V_{DD}	DC Supply Voltage (except SC41343, SC41344)	- 0.5 to + 18	V
V_{DD}	DC Supply Voltage (SC41343, SC41344 only)	- 0.5 to + 10	V
V_{in}	DC Input Voltage	- 0.5 to $V_{DD} + 0.5$	V
V_{out}	DC Output Voltage	- 0.5 to $V_{DD} + 0.5$	V
I_{in}	DC Input Current, per Pin	± 10	mA
I_{out}	DC Output Current, per Pin	± 10	mA
P_D	Power Dissipation, per Package	500	mW
T_{stg}	Storage Temperature	- 65 to + 150	$^{\circ}C$
T_L	Lead Temperature, 1 mm from Case for 10 Seconds	260	$^{\circ}C$

* Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section.

This device contains protection circuitry to guard against damage due to high static voltages or electric fields. However, precautions must be taken to avoid applications of any voltage higher than maximum rated voltages to this high-impedance circuit. For proper operation, V_{in} and V_{out} should be constrained to the range $V_{SS} \leq (V_{in} \text{ or } V_{out}) \leq V_{DD}$.

ELECTRICAL CHARACTERISTICS — MC145026*, MC145027, and MC145028 (Voltage Referenced to V_{SS})

Symbol	Characteristic	V_{DD} V	Guaranteed Limit						Unit
			- 40°C		25°C		85°C		
			Min	Max	Min	Max	Min	Max	
V _{OL}	Low-Level Output Voltage ($V_{in} = V_{DD}$ or 0)	5.0	—	0.05	—	0.05	—	0.05	V
		10	—	0.05	—	0.05	—	0.05	
		15	—	0.05	—	0.05	—	0.05	
V _{OH}	High-Level Output Voltage ($V_{in} = 0$ or V_{DD})	5.0	4.95	—	4.95	—	4.95	—	V
		10	9.95	—	9.95	—	9.95	—	
		15	14.95	—	14.95	—	14.95	—	
V _{IL}	Low-Level Input Voltage ($V_{out} = 4.5$ or 0.5 V) ($V_{out} = 9.0$ or 1.0 V) ($V_{out} = 13.5$ or 1.5 V)	5.0	—	1.5	—	1.5	—	1.5	V
		10	—	3.0	—	3.0	—	3.0	
		15	—	4.0	—	4.0	—	4.0	
V _{IH}	High-Level Input Voltage ($V_{out} = 0.5$ or 4.5 V) ($V_{out} = 1.0$ or 9.0 V) ($V_{out} = 1.5$ or 13.5 V)	5.0	3.5	—	3.5	—	3.5	—	V
		10	7.0	—	7.0	—	7.0	—	
		15	11	—	11	—	11	—	
I _{OH}	High-Level Output Current ($V_{out} = 2.5$ V) ($V_{out} = 4.6$ V) ($V_{out} = 9.5$ V) ($V_{out} = 13.5$ V)	5.0	-2.5	—	-2.1	—	-1.7	—	mA
		5.0	-0.52	—	-0.44	—	-0.36	—	
		10	-1.3	—	-1.1	—	-0.9	—	
		15	-3.6	—	-3.0	—	-2.4	—	
I _{OL}	Low-Level Output Current ($V_{out} = 0.4$ V) ($V_{out} = 0.5$ V) ($V_{out} = 1.5$ V)	5.0	0.52	—	0.44	—	0.36	—	mA
		10	1.3	—	1.1	—	0.9	—	
		15	3.6	—	3.0	—	2.4	—	
I _{in}	Input Current — $\bar{T}E$ (MC145026, Pull-Up Device)	5.0	—	—	3.0	11	—	—	μA
		10	—	—	16	60	—	—	
		15	—	—	35	120	—	—	
I _{in}	Input Current R_S (MC145026), D_{in} (MC145027, MC145028)	15	—	± 0.3	—	± 0.3	—	± 1.0	μA
		5.0	—	—	—	± 110	—	—	
		10	—	—	—	± 500	—	—	
I _{in}	Input Current A1 – A5, A6/D6 – A9/D9 (MC145026), A1 – A5 (MC145027), A1 – A9 (MC145028)	5.0	—	—	—	± 110	—	—	μA
		10	—	—	—	± 500	—	—	
		15	—	—	—	± 1000	—	—	
C _{in}	Input Capacitance ($V_{in} = 0$)	—	—	—	—	7.5	—	—	pF
I _{DD}	Quiescent Current — MC145026	5.0	—	—	—	0.1	—	—	μA
		10	—	—	—	0.2	—	—	
		15	—	—	—	0.3	—	—	
I _{DD}	Quiescent Current — MC145027, MC145028	5.0	—	—	—	50	—	—	μA
		10	—	—	—	100	—	—	
		15	—	—	—	150	—	—	
I _{dd}	Dynamic Supply Current — MC145026 ($f_C = 20$ kHz)	5.0	—	—	—	200	—	—	μA
		10	—	—	—	400	—	—	
		15	—	—	—	600	—	—	
I _{dd}	Dynamic Supply Current — MC145027, MC145028 ($f_C = 20$ kHz)	5.0	—	—	—	400	—	—	μA
		10	—	—	—	800	—	—	
		15	—	—	—	1200	—	—	

* Also see next Electrical Characteristics table for 2.5 V specifications.

ELECTRICAL CHARACTERISTICS — MC145026 (Voltage Referenced to V_{SS})

Symbol	Characteristic	V _{DD} V	Guaranteed Limit						Unit
			- 40°C		25°C		85°C		
			Min	Max	Min	Max	Min	Max	
V _{OL}	Low-Level Output Voltage (V _{in} = 0 V or V _{DD})	2.5	—	0.05	—	0.05	—	0.05	V
V _{OH}	High-Level Output Voltage (V _{in} = 0 V or V _{DD})	2.5	2.45	—	2.45	—	2.45	—	V
V _{IL}	Low-Level Input Voltage (V _{out} = 0.5 V or 2.0 V)	2.5	—	0.3	—	0.3	—	0.3	V
V _{IH}	High-Level Input Voltage (V _{out} = 0.5 V or 2.0 V)	2.5	2.2	—	2.2	—	2.2	—	V
I _{OH}	High-Level Output Current (V _{out} = 1.25 V)	2.5	0.28	—	0.25	—	0.2	—	mA
I _{OL}	Low-Level Output Current (V _{out} = 0.4 V)	2.5	0.22	—	0.2	—	0.16	—	mA
I _{in}	Input Current (\overline{TE} — Pull-Up Device)	2.5	—	—	0.09	1.8	—	—	μA
I _{in}	Input Current (A1–A5, A6/D6–A9/D9)	2.5	—	—	—	± 25	—	—	μA
I _{DD}	Quiescent Current	2.5	—	—	—	0.05	—	—	μA
I _{dd}	Dynamic Supply Current (f _c = 20 kHz)	2.5	—	—	—	40	—	—	μA

SWITCHING CHARACTERISTICS — MC145026*, MC145027, and MC145028 (C_L = 50 pF, T_A = 25°C)

Symbol	Characteristic	Figure No.	V _{DD}	Guaranteed Limit		Unit
				Min	Max	
t _{TLH} , t _{THL}	Output Transition Time	4, 8	5.0 10 15	— — —	200 100 80	ns
t _r	D _{in} Rise Time — Decoders	5	5.0 10 15	— — —	15 15 15	μs
t _f	D _{in} Fall Time — Decoders	5	5.0 10 15	— — —	15 5.0 4.0	μs
f _{osc}	Encoder Clock Frequency	6	5.0 10 15	0.001 0.001 0.001	2.0 5.0 10	MHz
f	Decoder Frequency — Referenced to Encoder Clock	12	5.0 10 15	1.0 1.0 1.0	240 410 450	kHz
t _w	\overline{TE} Pulse Width — Encoders	7	5.0 10 15	65 30 20	— — —	ns

* Also see next Switching Characteristics table for 2.5 V specifications.

SWITCHING CHARACTERISTICS — MC145026 (C_L = 50 pF, T_A = 25°C)

Symbol	Characteristic	Figure No.	V _{DD}	Guaranteed Limit		Unit
				Min	Max	
t _{TLH} , t _{THL}	Output Transition Time	4, 8	2.5	—	450	ns
f _{osc}	Encoder Clock Frequency	6	2.5	1.0	250	kHz
t _w	\overline{TE} Pulse Width	7	2.5	1.5	—	μs

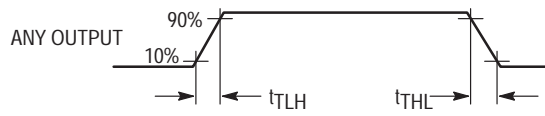


Figure 4.

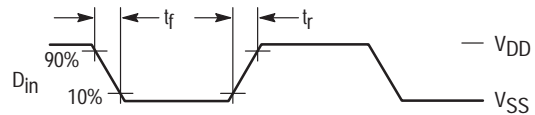


Figure 5.

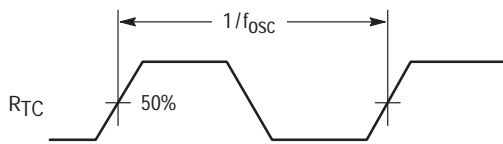


Figure 6.

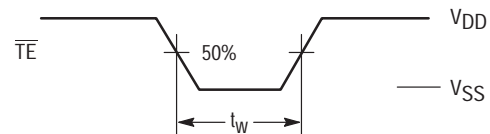
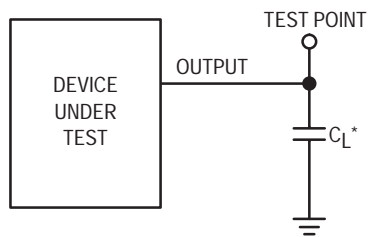


Figure 7.



* Includes all probe and fixture capacitance.

Figure 8. Test Circuit

OPERATING CHARACTERISTICS

MC145026

The encoder serially transmits trinary data as defined by the state of the A1 – A5 and A6/D6 – A9/D9 input pins. These pins may be in either of three states (low, high, or open) allowing 19,683 possible codes. The transmit sequence is initiated by a low level on the \overline{TE} input pin. Upon power-up, the MC145026 can continuously transmit as long as \overline{TE} remains low (also, the device can transmit two-word sequences by pulsing \overline{TE} low). However, no MC145026 application should be designed to rely upon the first data word transmitted immediately after power-up because this word may be invalid. Between the two data words, no signal is sent for three data periods (see Figure 10).

Each transmitted trinary digit is encoded into pulses (see Figure 11). A logic 0 (low) is encoded as two consecutive short pulses, a logic 1 (high) as two consecutive long pulses, and an open (high impedance) as a long pulse followed by a short pulse. The input state is determined by using a weak “output” device to try to force each input high then low. If only a high state results from the two tests, the input is assumed to be hardwired to V_{DD} . If only a low state is obtained, the input is assumed to be hardwired to V_{SS} . If both a high and a low can be forced at an input, an open is assumed and is encoded as such. The “high” and “low” levels are 70% and 30% of the supply voltage as shown in the Electrical Characteristics table. The weak “output” device sinks/sources up to 110 μ A at a 5 V supply level, 500 μ A at 10 V, and 1 mA at 15 V.

The \overline{TE} input has an internal pull-up device so that a simple switch may be used to force the input low. While \overline{TE} is high and the second-word transmission has timed out, the encoder is completely disabled, the oscillator is inhibited, and the current drain is reduced to quiescent current. When \overline{TE} is brought low, the oscillator is started and the transmit sequence begins. The inputs are then sequentially selected, and determinations are made as to the input logic states. This information is serially transmitted via the D_{Out} pin.

MC145027

This decoder receives the serial data from the encoder and outputs the data, if it is valid. The transmitted data, consisting of two identical words, is examined bit by bit during reception. The first five trinary digits are assumed to be the address. If the received address matches the local address, the next four (data) bits are internally stored, but are not transferred to the output data latch. As the second encoded word is received, the address must again match. If a match occurs, the new data bits are checked against the previously stored data bits. If the two nibbles of data (four bits each) match, the data is transferred to the output data latch by VT and remains until new data replaces it. At the same time, the VT output pin is brought high and remains high until an error is received or until no input signal is received for four data periods (see Figure 10).

Although the address information may be encoded in trinary, the data information must be either a 1 or 0. A trinary (open) data line is decoded as a logic 1.

MC145028

This decoder operates in the same manner as the MC145027 except that nine address lines are used and no data output is available. The VT output is used to indicate that a valid address has been received. For transmission security, two identical transmitted words must be consecutively received before a VT output signal is issued.

The MC145028 allows 19,683 addresses when trinary levels are used. 512 addresses are possible when binary levels are used.

PIN DESCRIPTIONS

MC145026 ENCODER

A1 – A5, A6/D6 – A9/D9

Address, Address/Data Inputs (Pins 1 – 7, 9, and 10)

These address/data inputs are encoded and the data is sent serially from the encoder via the D_{Out} pin.

RS, CTC, RTC

(Pins 11, 12, and 13)

These pins are part of the oscillator section of the encoder (see Figure 9).

If an external signal source is used instead of the internal oscillator, it should be connected to the R_S input and the R_{TC} and C_{TC} pins should be left open.

\overline{TE}

Transmit Enable (Pin 14)

This active-low transmit enable input initiates transmission when forced low. An internal pull-up device keeps this input normally high. The pull-up current is specified in the Electrical Characteristics table.

D_{Out}

Data Out (Pin 15)

This is the output of the encoder that serially presents the encoded data word.

V_{SS}

Negative Power Supply (Pin 8)

The most-negative supply potential. This pin is usually ground.

V_{DD}

Positive Power Supply (Pin 16)

The most-positive power supply pin.

MC145027 AND MC145028 DECODERS

A1 – A5, A1 – A9

Address Inputs (Pins 1 – 5) — MC145027,

Address Inputs (Pins 1 – 5, 15, 14, 13, 12) — MC145028

These are the local address inputs. The states of these pins must match the appropriate encoder inputs for the VT pin to go high. The local address may be encoded with trinary or binary data.

D6 – D9

Data Outputs (Pins 15, 14, 13, 12) — MC145027 Only

These outputs present the binary information that is on encoder inputs A6/D6 through A9/D9. Only binary data is

acknowledged; a trinary open at the MC145026 encoder is decoded as a high level (logic 1).

D_{in}
Data In (Pin 9)

This pin is the serial data input to the decoder. The input voltage must be at CMOS logic levels. The signal source driving this pin must be dc coupled.

R₁, C₁
Resistor 1, Capacitor 1 (Pins 6, 7)

As shown in Figures 2 and 3, these pins accept a resistor and capacitor that are used to determine whether a narrow pulse or wide pulse has been received. The time constant $R_1 \times C_1$ should be set to 1.72 encoder clock periods:

$$R_1 C_1 = 3.95 R_{TC} C_{TC}$$

R₂/C₂
Resistor 2/Capacitor 2 (Pin 10)

As shown in Figures 2 and 3, this pin accepts a resistor and capacitor that are used to detect both the end of a received word and the end of a transmission. The time constant $R_2 \times C_2$ should be 33.5 encoder clock periods (four data periods per Figure 11): $R_2 C_2 = 77 R_{TC} C_{TC}$. This time

constant is used to determine whether the D_{in} pin has remained low for four data periods (end of transmission). A separate on-chip comparator looks at the voltage-equivalent two data periods ($0.4 R_2 C_2$) to detect the dead time between received words within a transmission.

VT
Valid Transmission Output (Pin 11)

This valid transmission output goes high after the second word of an encoding sequence when the following conditions are satisfied:

1. the received addresses of both words match the local decoder address, and
2. the received data bits of both words match.

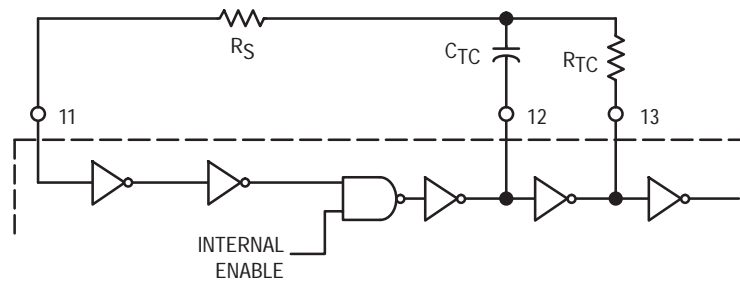
VT remains high until either a mismatch is received or no input signal is received for four data periods.

V_{SS}
Negative Power Supply (Pin 8)

The most-negative supply potential. This pin is usually ground.

V_{DD}
Positive Power Supply (Pin 16)

The most-positive power supply pin.



This oscillator operates at a frequency determined by the external RC network; i.e.,

$$f \approx \frac{1}{2.3 R_{TC} C_{TC'}} \text{ (Hz)}$$

for $1 \text{ kHz} \leq f \leq 400 \text{ kHz}$

where: $C_{TC'} = C_{TC} + C_{\text{layout}} + 12 \text{ pF}$

$R_S \approx 2 R_{TC}$

$R_S \geq 20 \text{ k}$

$R_{TC} \geq 10 \text{ k}$

$400 \text{ pF} < C_{TC} < 15 \text{ }\mu\text{F}$

The value for R_S should be chosen to be ≥ 2 times R_{TC} . This range ensures that current through R_S is insignificant compared to current through R_{TC} . The upper limit for R_S must ensure that $R_S \times 5 \text{ pF}$ (input capacitance) is small compared to $R_{TC} \times C_{TC}$.

For frequencies outside the indicated range, the formula is less accurate. The minimum recommended oscillation frequency of this circuit is 1 kHz. Susceptibility to externally induced noise signals may occur for frequencies below 1 kHz and/or when resistors utilized are greater than 1 M Ω .

Figure 9. Encoder Oscillator Information

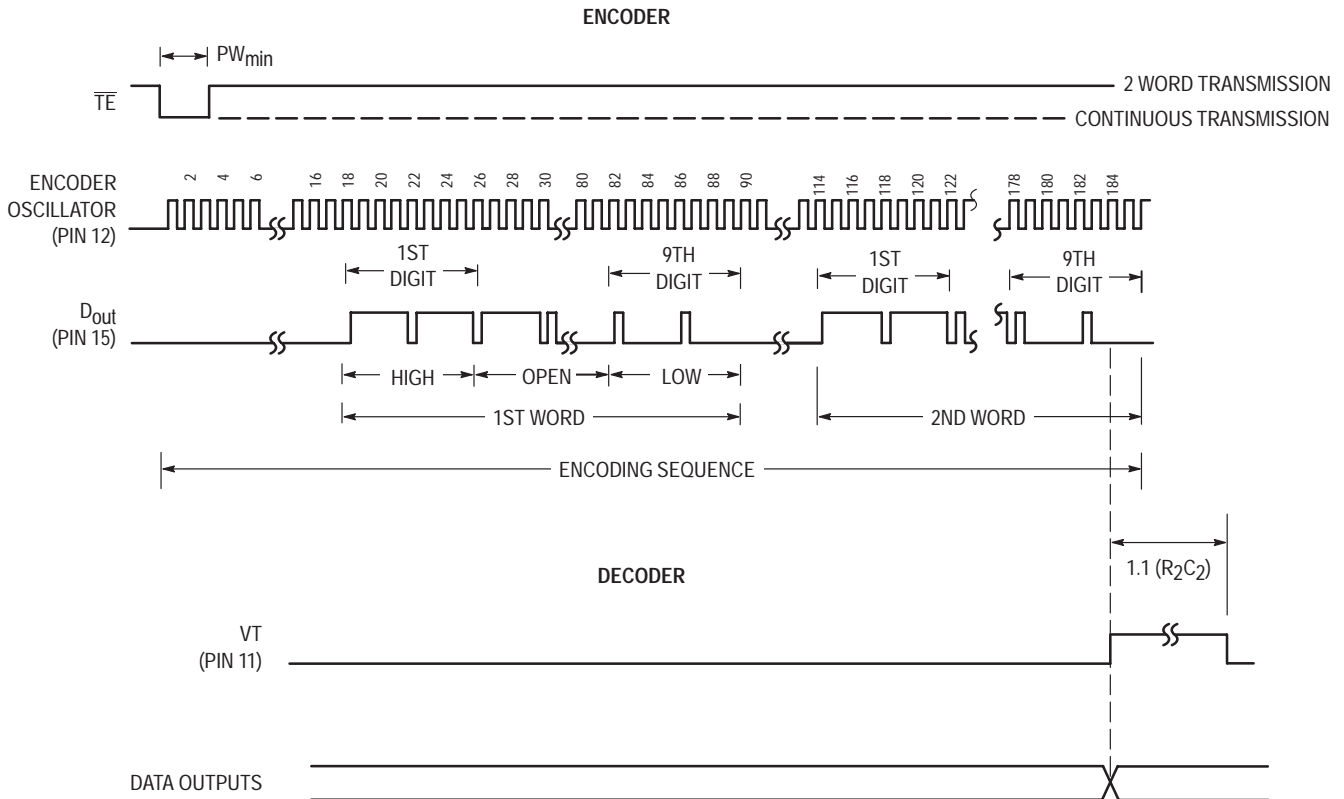


Figure 10. Timing Diagram

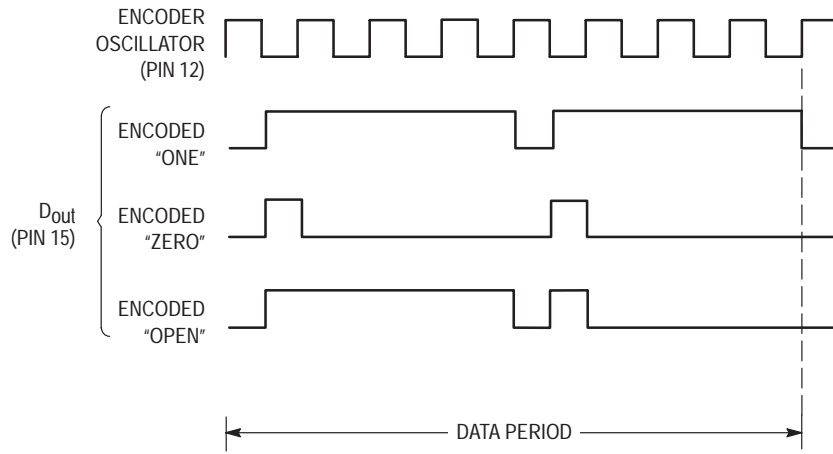


Figure 11. Encoder Data Waveforms

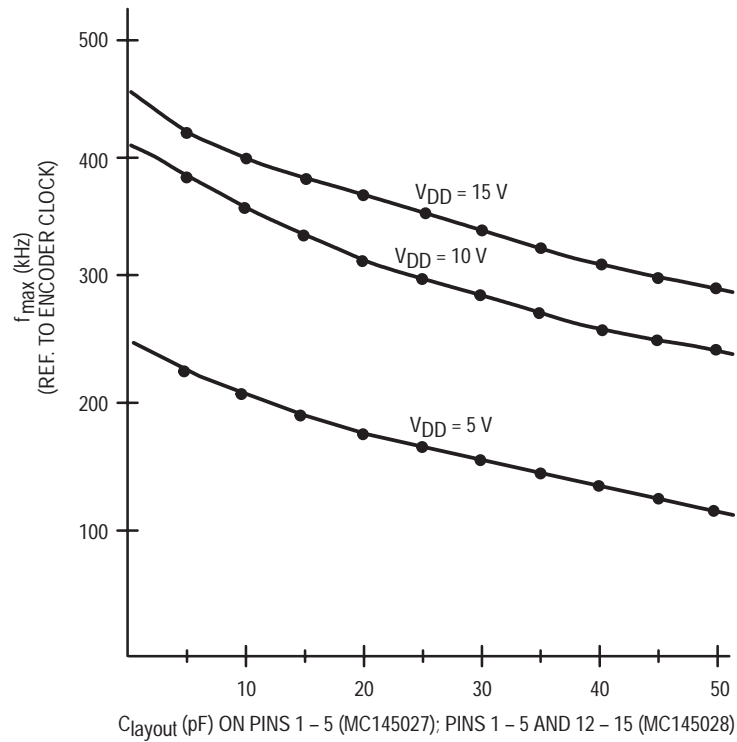


Figure 12. f_{max} vs C_{layout} — Decoders Only

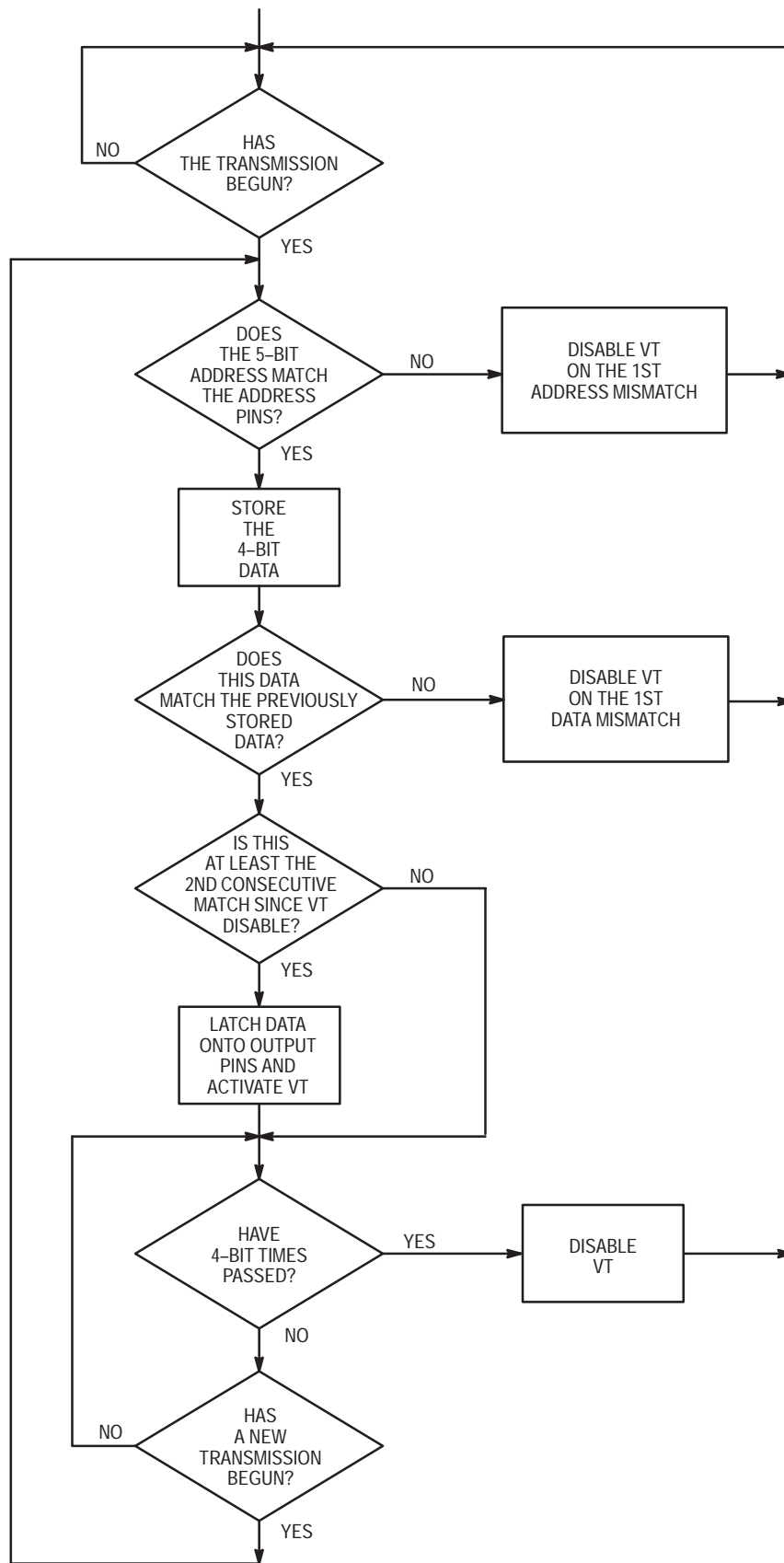


Figure 13. MC145027 Flowchart

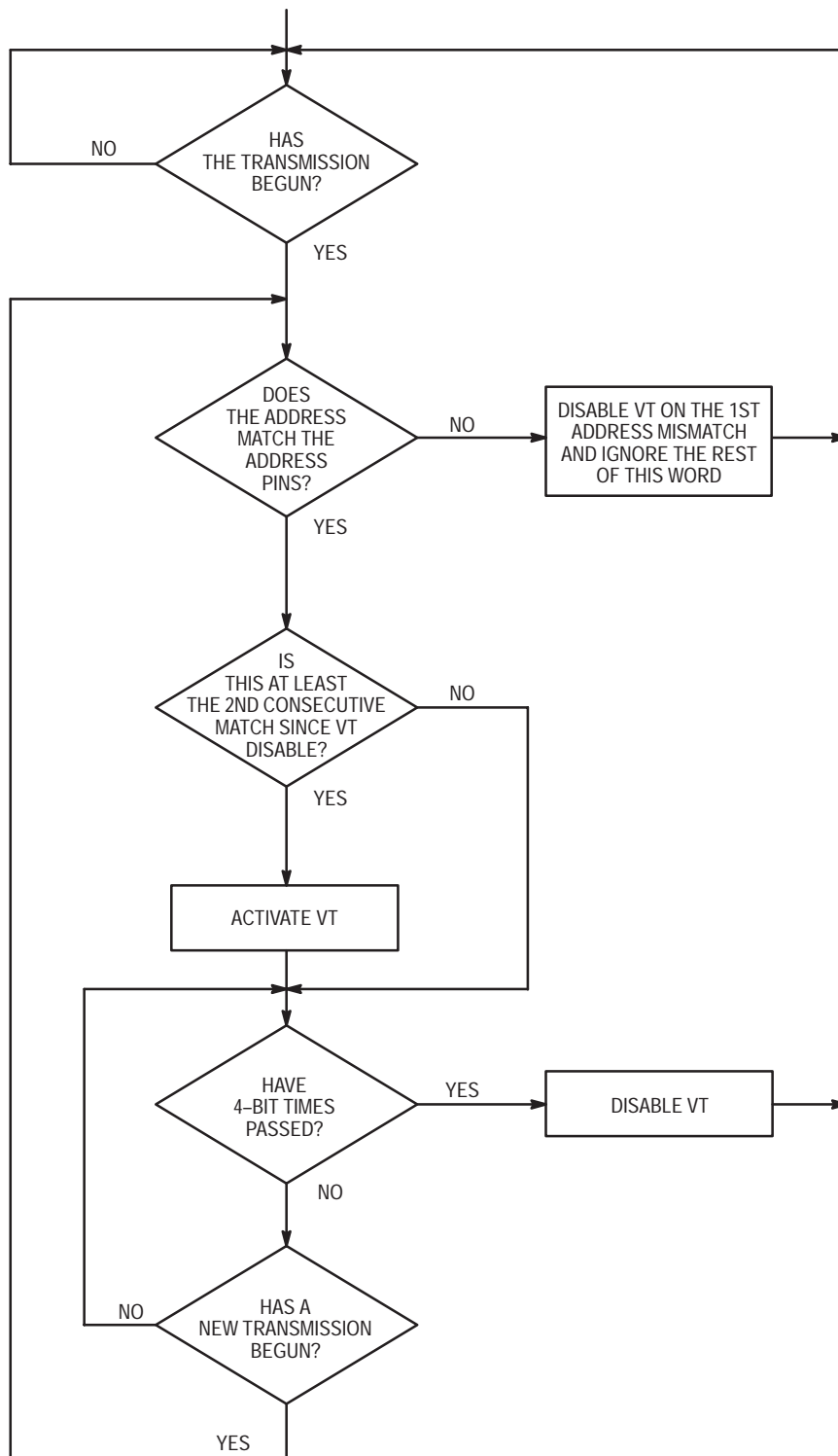


Figure 14. MC145028 Flowchart

MC145027 AND MC145028 TIMING

To verify the MC145027 or MC145028 timing, check the waveforms on C1 (Pin 7) and R2/C2 (Pin 10) as compared to the incoming data waveform on D_{in} (Pin 9).

The R–C decay seen on C1 discharges down to $1/3 V_{DD}$ before being reset to V_{DD} . This point of reset (labelled “DOS” in Figure 15) is the point in time where the decision is made whether the data seen on D_{in} is a 1 or 0. DOS should not be too close to the D_{in} data edges or intermittent operation may occur.

The other timing to be checked on the MC145027 and MC145028 is on R2/C2 (see Figure 16). The R–C decay is continually reset to V_{DD} as data is being transmitted. Only between words and after the end-of-transmission (EOT) does R2/C2 decay significantly from V_{DD} . R2/C2 can be used to identify the internal end-of-word (EOW) timing edge which is generated when R2/C2 decays to $2/3 V_{DD}$. The internal EOT timing edge occurs when R2/C2 decays to $1/3 V_{DD}$. When the waveform is being observed, the R–C decay should go down between the $2/3$ and $1/3 V_{DD}$ levels, but not too close to either level before data transmission on D_{in} resumes.

Verification of the timing described above should ensure a good match between the MC145026 transmitter and the MC145027 and MC145028 receivers.

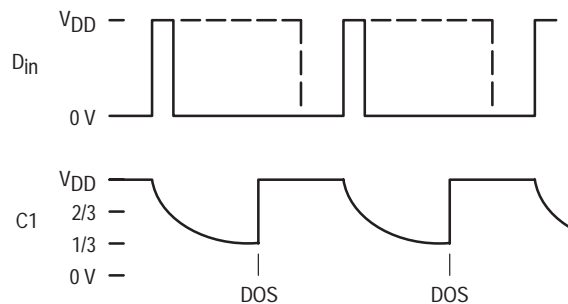


Figure 15. R–C Decay on Pin 7 (C1)

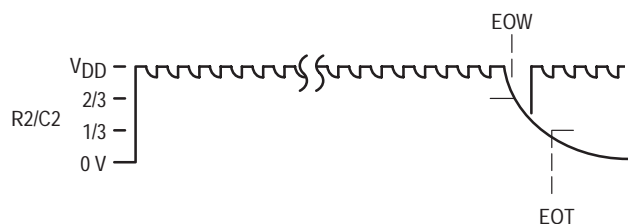
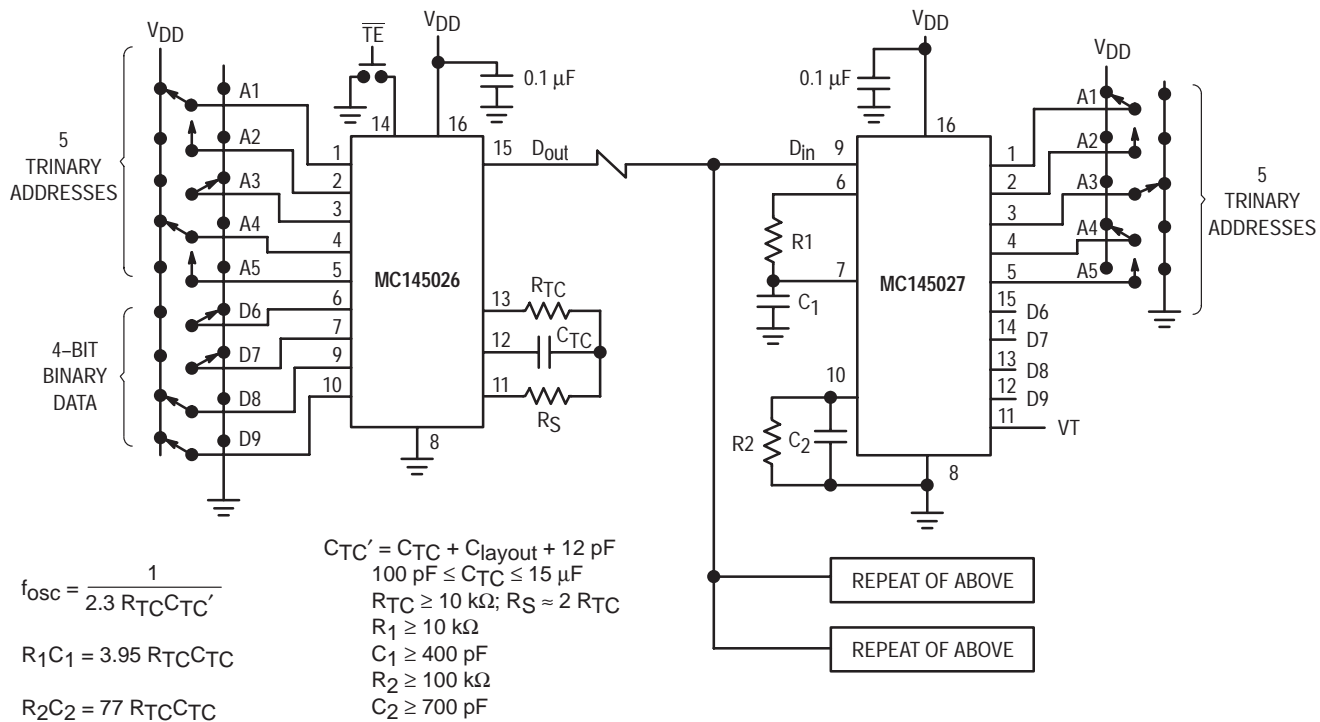


Figure 16. R–C Decay on Pin 10 (R2/C2)



Example R/C Values (All Resistors and Capacitors are ± 5%)

($C_{TC}' = C_{TC} + 20 \text{ pF}$)

f _{osc} (kHz)	R _{TC}	C _{TC} '	R _S	R ₁	C ₁	R ₂	C ₂
362	10 k	120 pF	20 k	10 k	470 pF	100 k	910 pF
181	10 k	240 pF	20 k	10 k	910 pF	100 k	1800 pF
88.7	10 k	490 pF	20 k	10 k	2000 pF	100 k	3900 pF
42.6	10 k	1020 pF	20 k	10 k	3900 pF	100 k	7500 pF
21.5	10 k	2020 pF	20 k	10 k	8200 pF	100 k	0.015 μF
8.53	10 k	5100 pF	20 k	10 k	0.02 μF	200 k	0.02 μF
1.71	50 k	5100 pF	100 k	50 k	0.02 μF	200 k	0.1 μF

Figure 17. Typical Application

APPLICATIONS INFORMATION

INFRARED TRANSMITTER

In Figure 18, the MC145026 encoder is set to run at an oscillator frequency of about 4 to 9 kHz. Thus, the time required for a complete two-word encoding sequence is about 20 to 40 ms. The data output from the encoder gates an RC oscillator running at 50 kHz; the oscillator shown starts rapidly enough to be used in this application. When the "send" button is not depressed, both the MC145026 and oscillator are in a low-power standby state. The RC oscillator has to be trimmed for 50 kHz and has some drawbacks for frequency stability. A superior system uses a ceramic resonator oscillator running at 400 kHz. This oscillator feeds a divider as shown in Figure 19. The unused inputs of the MC14011UB must be grounded.

The MLED81 IRED is driven with the 50 kHz square wave at about 200 to 300 mA to generate the carrier. If desired, two IREDs wired in series can be used (see Application Note AN1016 for more information). The bipolar IRED switch, shown in Figure 18, offers two advantages over a FET. First, a logic FET has too much gate capacitance for the MC14011UB to drive without waveform distortion. Second, the bipolar drive permits lower supply voltages, which are an advantage in portable battery-powered applications.

The configuration shown in Figure 18 operates over a supply range of 4.5 to 18 V. A low-voltage system which operates down to 2.5 V could be realized if the oscillator section of a MC74HC4060 is used in place of the MC14011UB. The data output of the MC145026 is inverted and fed to the RESET pin of the MC74HC4060. Alternately, the MC74HCU04 could be used for the oscillator.

Information on the MC14011UB is in book number DL131/D. The MC74HCU04 and MC74HC4060 are found in book number DL129/D.

INFRARED RECEIVER

The receiver in Figure 20 couples an IR-sensitive diode to input preamp A1, followed by band-pass amplifier A2 with a gain of about 10. Limiting stage A3 follows, with an output of about 800 mV p-p. The limited 50 kHz burst is detected by comparator A4 that passes only positive pulses, and peak-

detected and filtered by a diode/RC network to extract the data envelope from the burst. Comparator A5 boosts the signal to logic levels compatible with the MC145027/28 data input. The D_{in} pin of these decoders is a standard CMOS high-impedance input which must **not** be allowed to float. Therefore, direct coupling from A5 to the decoder input is utilized.

Shielding should be used on at least A1 and A2, with good ground and high-sensitivity circuit layout techniques applied.

For operation with supplies higher than +5 V, limiter A4's positive output swing needs to be limited to 3 to 5 V. This is accomplished via adding a zener diode in the negative feedback path, thus avoiding excessive system noise. The biasing resistor stack should be adjusted such that V3 is 1.25 to 1.5 V.

This system works up to a range of about 10 meters. The gains of the system may be adjusted to suit the individual design needs. The 100 Ω resistor in the emitter of the first 2N5088 and the 1 k Ω resistor feeding A2 may be altered if different gain is required. In general, more gain does not necessarily result in increased range. This is due to noise floor limitations. The designer should increase transmitter power and/or increase receiver aperture with Fresnel lensing to greatly improve range. See Application Note AN1016 for additional information.

Information on the MC34074 is in data book DL128/D.

TRINARY SWITCH MANUFACTURERS

Midland Ross—Electronic Connector Div.
Greyhill
Augat/Alcoswitch
Aries Electronics

The above companies may not have the switches in a DIP. For more information, call them or consult *eem Electronic Engineers Master Catalog* or the *Gold Book*. **Ask for SPDT with center OFF.**

Alternative: An SPST can be placed in series between a SPDT and the Encoder or Decoder to achieve trinary action.

Motorola cannot recommend one supplier over another and in no way suggests that this is a complete listing of trinary switch manufacturers.

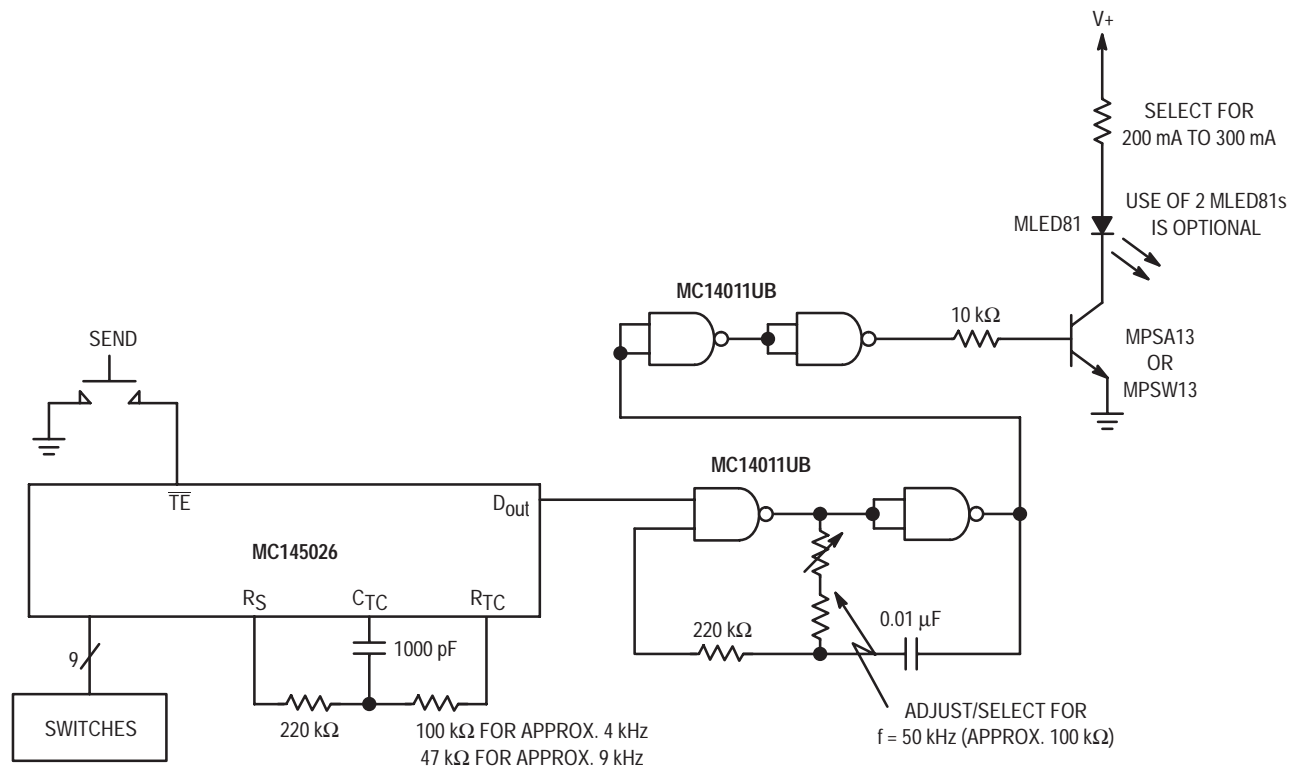


Figure 18. IRED Transmitter Using RC Oscillator to Generate Carrier Frequency

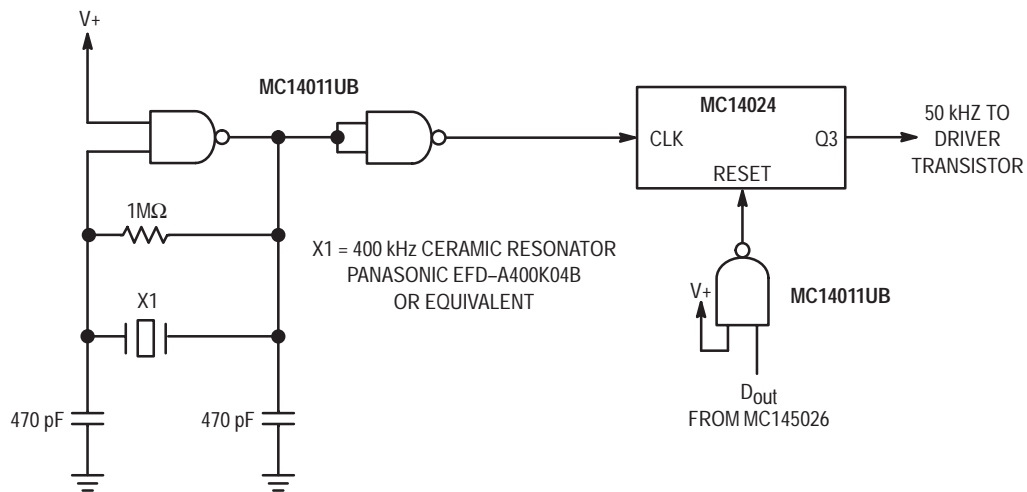


Figure 19. Using a Ceramic Resonator to Generate Carrier Frequency

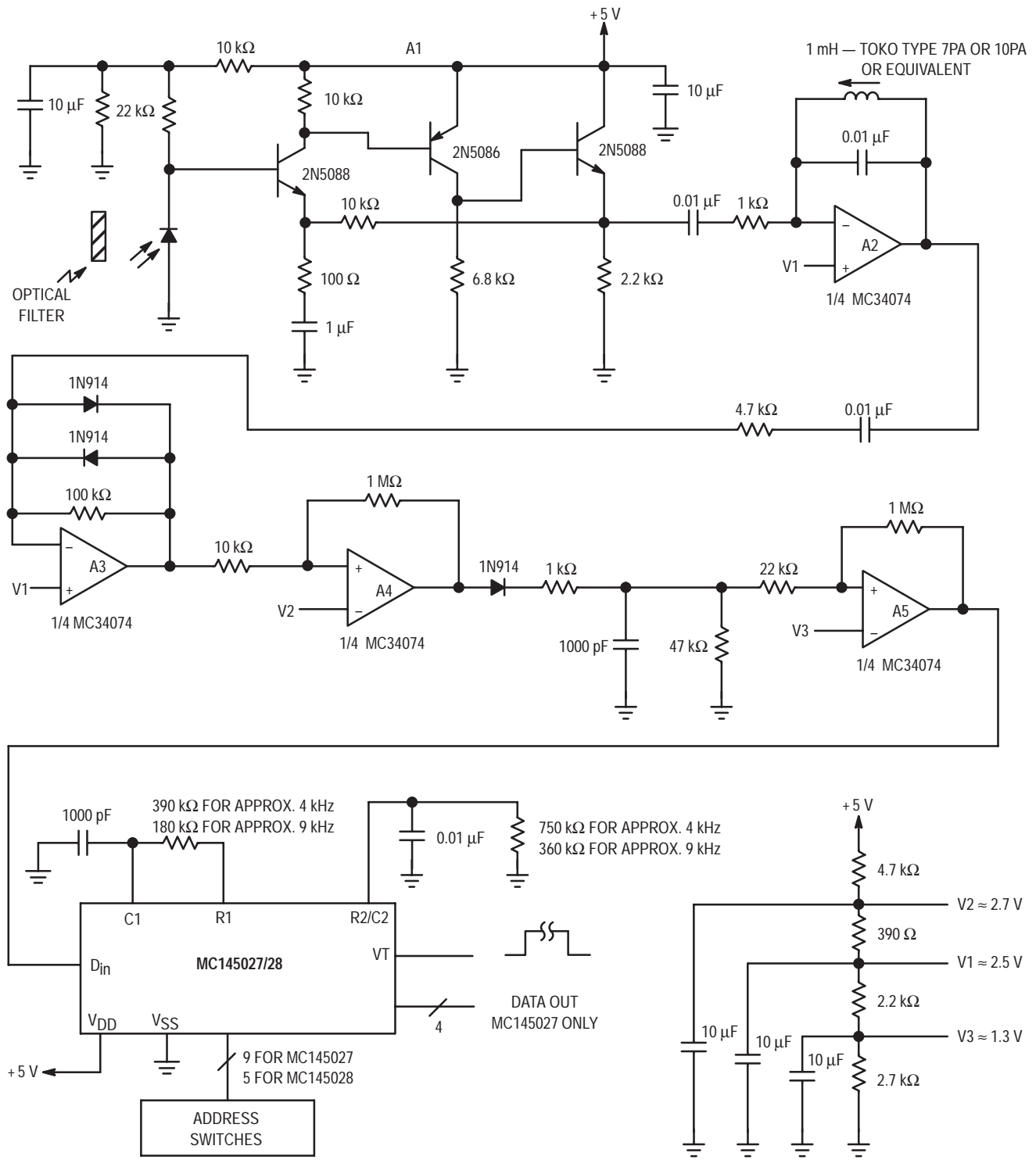


Figure 20. Infrared Receiver

Chapter Four

Frequency Synthesis

Section One	4.1–0
Frequency Synthesis – Selector Guide	
Section Two	4.2–0
Frequency Synthesis – Data Sheets	

Section One Selector Guide

Frequency Synthesis

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Frequency Synthesis

Single PLL Synthesizers

Maximum Frequency (MHz)	Supply Voltage (V)	Nominal Supply Current (mA)	Features	Device	Suffix/Case
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Parallel Interface	MC145151-2	DW/751F
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Parallel Interface, Uses External Dual-Modulus Prescaler	MC145152-2	DW/751F
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Serial Interface	MC145157-2	DW/751G
20 @ 5.0 V	3.0 to 9.0	7.5 @ 5 V	Serial Interface, Uses External Dual-Modulus Prescaler	MC145158-2	DW/751G
100 @ 3.0 V 185 @ 4.5 V	2.7 to 5.5	2 @ 3 V 6 @ 5 V	Serial Interface, Auxiliary Reference Divider, Evaluation Kit – MC145170EVK	MC145170-2	P/648, D/751B, DT/948C
1100	2.7 to 5.5	7 @ 5 V	Serial Interface, Standby, Auxiliary Reference Divider, Evaluation Kit – MC145193EVK	MC145193	F/751J, DT/948D
2000	2.7 to 5.5	4 @ 3 V	Serial Interface, Standby, Auxiliary Reference Device, Evaluation Kit – MC145202-1EVK	MC145202-1	F/751J, DT/948D
2500	2.7 to 5.5	9.5	Serial Interface	MC12210	D/751B, DT/948E
2800	4.5 to 5.5	3.5	Fixed Divider	MC12179	D/751

Dual PLL Synthesizers

Maximum Frequency (MHz)	Supply Voltage (V)	Nominal Supply Current (mA)	Phase Detector	Device	Suffix/Case
1100 both loops	2.7 to 5.5	12	Serial Interface, Standby, Evaluation Kit – MC145220EVK	MC145220	F/803C, DT/948D

PLL Building Blocks

Prescalers

Frequency (MHz)	Divide Ratios	Single or Dual Modulus	Supply Voltage (V)	Supply Current (mA)	Features	Device	Suffix/Case
1100	64/65, 128/129	Dual	2.7 to 5.5	2.0 max	Low Power	MC12052A	D/751
1100	10,20,40,80	Single	4.5 to 5.5	5.0 max		MC12080	D/751
1100	2, 4, 8	Single	2.7 to 5.5	4.5 max	Standby	MC12093	D/751
2000	64/65, 128/129	Dual	2.7 to 5.5	2.6 max	Low Power	MC12054A	D/751
2500	2, 4	Single	2.7 to 5.5	14 max	Standby	MC12095	D/751
2800	64, 128, 256	Single	4.5 to 5.5	11.5 max		MC12079	D/751

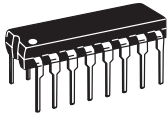
Voltage Control Oscillators

Frequency (MHz)	Supply Voltage (V)	Features	Device	Suffix/Case
1300	2.7 to 5.5	Two high drive open collector outputs (Q, QB), Adjustable output amplitude, Low drive output for prescaler	MC12149	D/751

Phase–Frequency Detectors

Frequency (MHz)	Supply Voltage (V)	Features	Device	Suffix/Case
800 (Typ)	4.75 to 5.5	MECL10H compatible	MCH12140	D/751
800 (Typ)	4.2 to 5.5	100K ECL compatible	MCK12140	D/751

Frequency Synthesis Packages



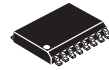
CASE 648
P SUFFIX
(DIP-16)



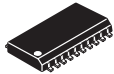
CASE 751
D SUFFIX
(SO-8)



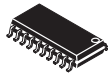
CASE 751B
D SUFFIX
(SO-16)



CASE 751G
DW SUFFIX
(SO-16W)



CASE 751J
F SUFFIX
(SO-20)



CASE 803C
F SUFFIX
(SO-20)



CASE 948C
DT SUFFIX
(TSSOP-16)



CASE 948D
DT SUFFIX
(TSSOP-20)



CASE 948E
DT SUFFIX
(TSSOP-20HS)

Section Two

Frequency Synthesis – Data Sheets

Device Number	Page Number	Device Number	Page Number
PLL Synthesizers		PLL Building Blocks	
Single		Prescalers	
MC12179	4.2-54	MC12026A	4.2-3
MC12210	4.2-64	MC12038A	4.2-8
MC145151-2	4.2-78	MC12052A	4.2-12
MC145152-2	4.2-81	MC12054A	4.2-15
MC145157-2	4.2-85	MC12079	4.2-17
MC145158-2	4.2-88	MC12080	4.2-20
MC145170-2	4.2-100	MC12093	4.2-23
MC145193	4.2-124	MC12095	4.2-25
MC145202-1	4.2-146	VCOs	
Dual		MC12147	4.2-29
MC145220	4.2-168	MC12148	4.2-40
Evaluation Kit Technical Summaries		MC12149	4.2-43
MC145220EVK	4.2-193	Phase Frequency Detectors	
		MCH12140	4.2-74
		MCK12140	4.2-74



1.1 GHz Dual Modulus Prescaler

The MC12026 is a high frequency, low voltage dual modulus prescaler used in phase-locked loop (PLL) applications.

The MC12026A can be used with CMOS synthesizers requiring positive edges to trigger internal counters such as Motorola's MC145xxx series in a PLL to provide tuning signals up to 1.1 GHz in programmable frequency steps.

The MC12026B can be used with CMOS synthesizers requiring negative edges to trigger internal counters.

A Divide Ratio Control (SW) permits selection of an 8/9 or 16/17 divide ratio as desired.

The Modulus Control (MC) selects the proper divide number after SW has been biased to select the desired divide ratio.

NOTE: The "B" Version Is Not Recommended for New Designs

- 1.1 GHz Toggle Frequency
- Supply Voltage 4.5 to 5.5 V
- Low Power 4.0 mA Typical
- Operating Temperature Range of -40 to 85°C
- The MC12026 is Pin Compatible With the MC12022
- Short Setup Time (t_{set}) 6ns Typical @ 1.1 GHz
- Modulus Control Input Level is Compatible With Standard CMOS and TTL

MC12026A IS NOT RECOMMENDED FOR NEW DESIGN
DEVICE TO BE PHASED OUT.
No replacement available.
MC12026B is on Life Time Buy

FUNCTIONAL TABLE

SW	MC	Divide Ratio
H	H	8
H	L	9
L	H	16
L	L	17

NOTES: 1. SW: H = V_{CC} , L = Open. A logic L can also be applied by grounding this pin, but this is not recommended due to increased power consumption.
2. MC: H = 2.0 V to V_{CC} , L = GND to 0.8 V.

MAXIMUM RATINGS

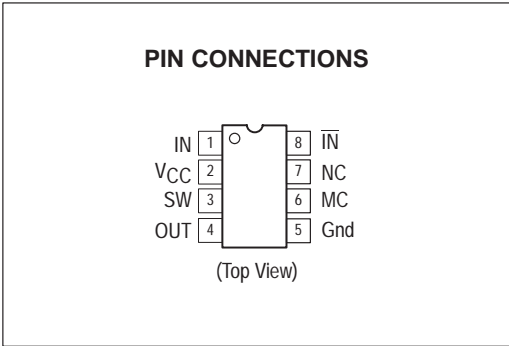
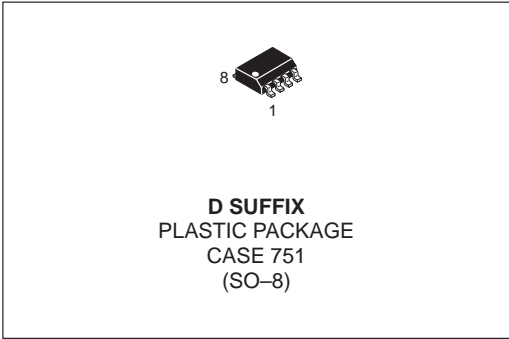
Characteristics	Symbol	Range	Unit
Power Supply Voltage, Pin 2	V_{CC}	-0.5 to 7.0	Vdc
Operating Temperature Range	T_A	-40 to 85	°C
Storage Temperature Range	T_{stg}	-65 to 150	°C
Modulus Control Input, Pin 6	MC	-0.5 to 6.5	Vdc
Maximum Output Current, Pin 4	I_O	10.0	mA

NOTE: ESD data available upon request.

MC12026A MC12026B

MECL PLL COMPONENTS ÷8/9, ÷16/17 DUAL MODULUS PRESCALER

**SEMICONDUCTOR
TECHNICAL DATA**



ORDERING INFORMATION

Device	Operating Temp Range	Package
MC12026AD	$T_A = -40$ to 85°C	SO-8
MC12026BD		

MC12026A MC12026B

ELECTRICAL CHARACTERISTICS ($V_{CC} = 4.5$ to 5.5 ; $T_A = -40$ to 85°C , unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sin Wave)	f_t	0.1	1.4	1.1	GHz
Supply Current Output Unloaded (Pin 2)	I_{CC}	–	4.0	5.3	mA
Modulus Control Input High (MC)	V_{IH1}	2.0	–	V_{CC}	V
Modulus Control Input Low (MC)	V_{IL1}	GND	–	0.8	V
Divide Ratio Control Input High (SW)	V_{IH2}	$V_{CC} - 0.5\text{ V}$	V_{CC}	$V_{CC} + 0.5\text{ V}$	V
Divide Ratio Control Input Low (SW)	V_{IL2}	OPEN	OPEN	OPEN	–
Output Voltage Swing ($R_L = 560\ \Omega$; $I_O = 5.5\text{ mA}$) ¹ ($R_L = 1.1\text{ k}\Omega$; $I_O = 2.9\text{ mA}$) ²	V_{out}	1.0	1.6	–	V_{pp}
Modulus Setup Time MC to Out ³	t_{SET}	–	6	9	ns
Input Voltage Sensitivity 100–250 MHz 250–1100 MHz	V_{in}	400 100	– –	1000 1000	mVpp

notes: 1. Divide Ratio of +8/9 at 1.1 GHz, $C_L = 8.0\text{ pF}$
 2. Divide Ratio of +16/17 at 1.1 GHz, $C_L = 8.0\text{ pF}$
 3. Assuming $R_L = 560\ \Omega$ at 1.1 GHz

Figure 1. Logic Diagram (MC12026A)

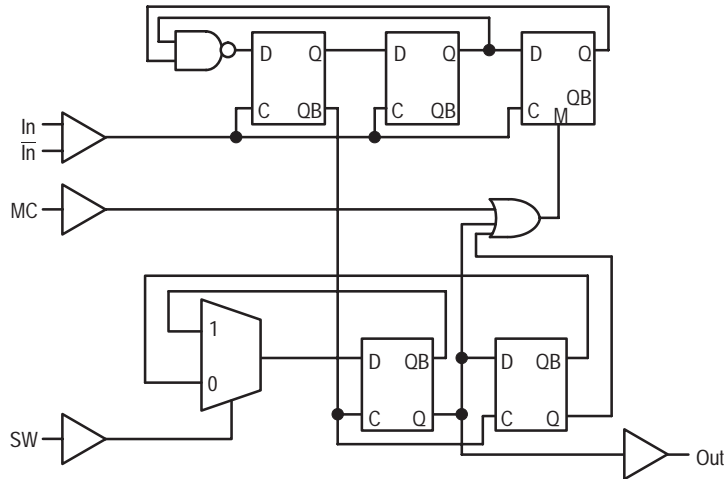
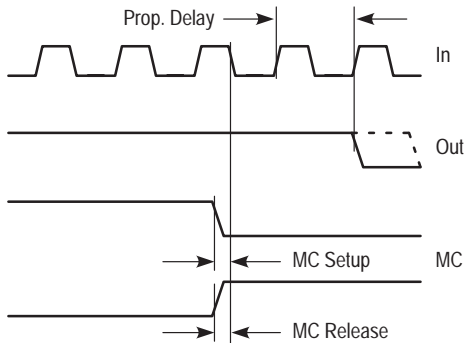


Figure 2. Modulus Setup Time



Modulus setup time MC to out is the MC setup or MC release plus the prop delay.

MC12026A MC12026B

Figure 3. AC Test Circuit

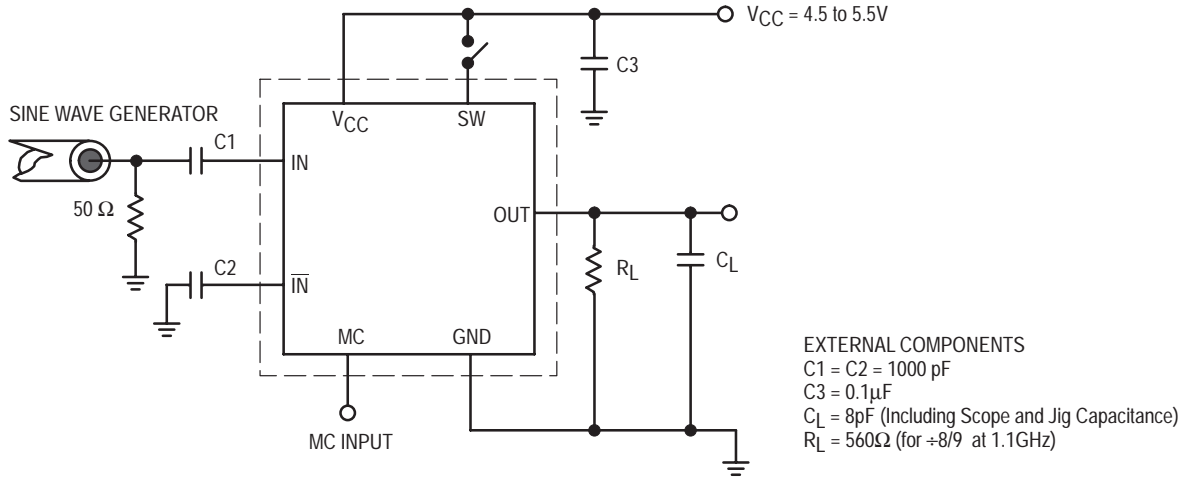


Figure 4. Input Signal Amplitude versus Input Frequency

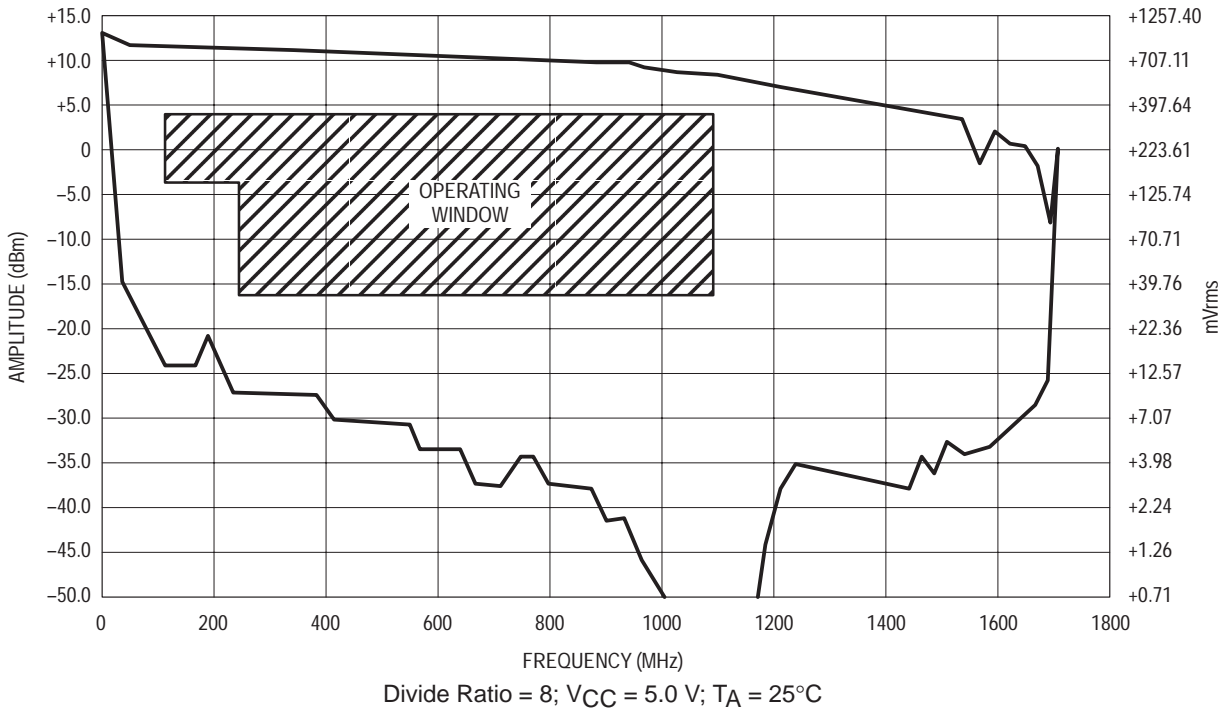
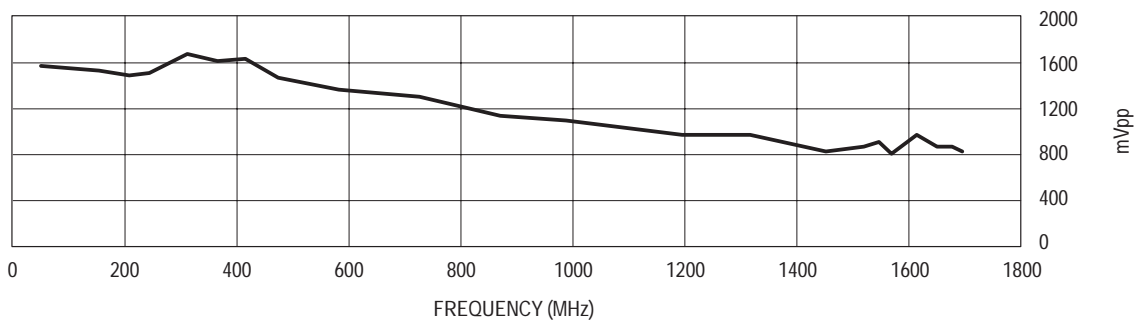
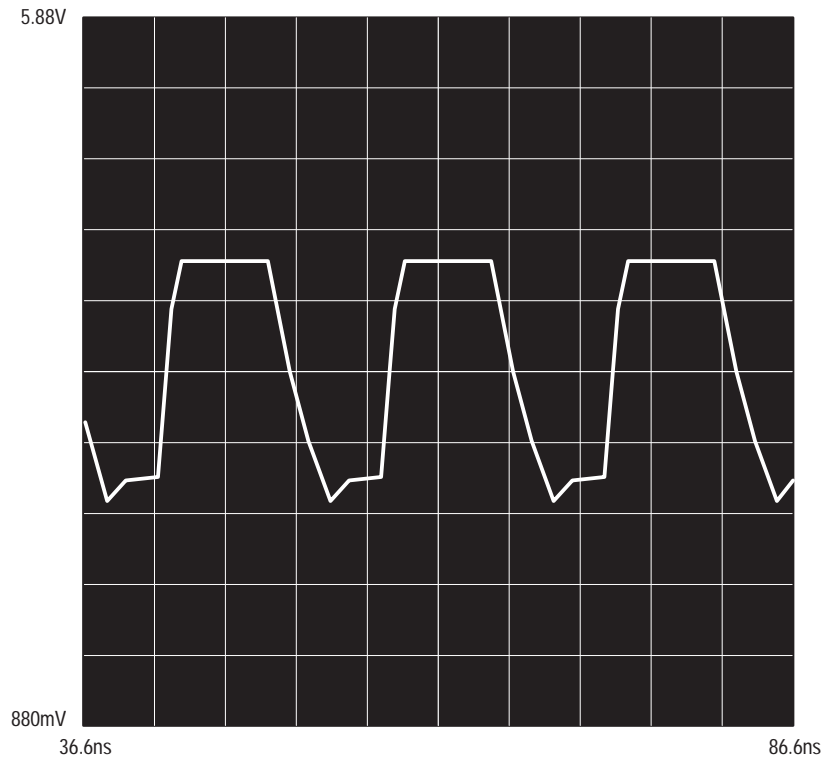


Figure 5. Output Amplitude versus Input Frequency



MC12026A MC12026B

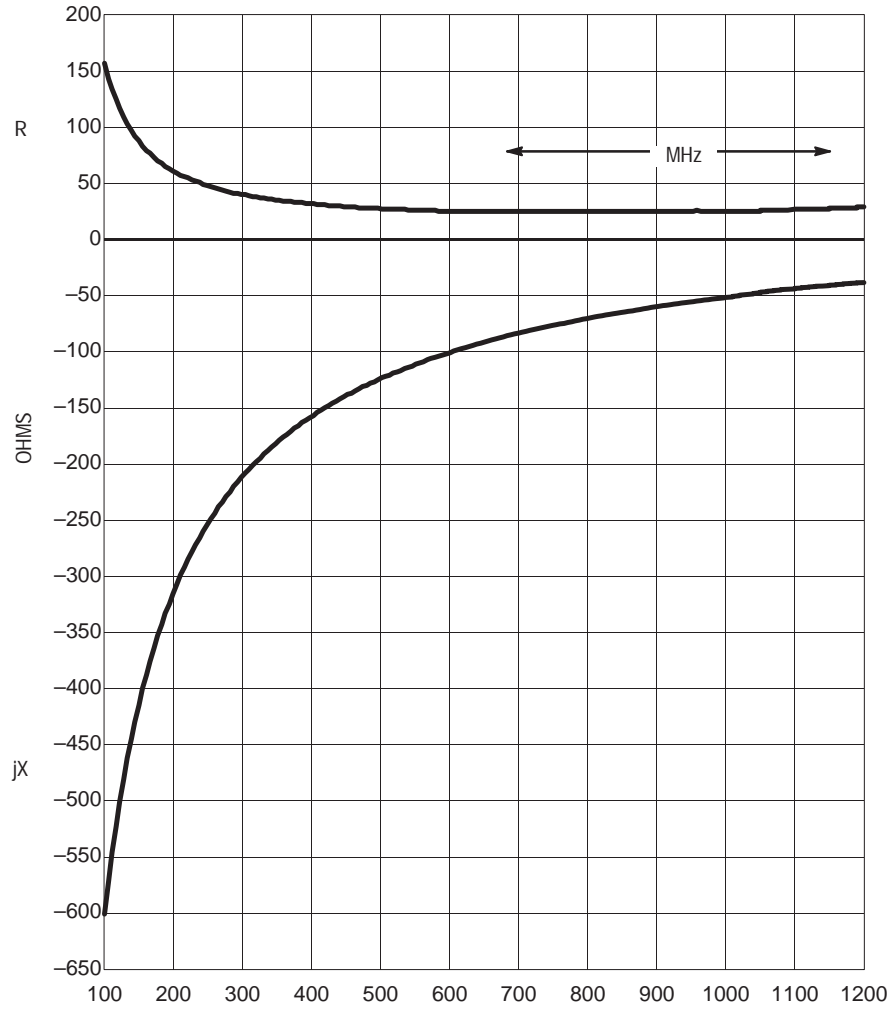
Figure 6. Typical Output Waveform



(±8, 1.1 GHz Input Frequency, $V_{CC} = 5.0$, $T_A = 25^\circ\text{C}$, Output Loaded With 8.0pF)

MC12026A MC12026B

Figure 7. Typical Input Impedance versus Input Frequency





1.1 GHz Low Power Dual Modulus Prescaler

The MC12038A can be used with CMOS synthesizers requiring positive edges to trigger internal counters such as Motorola's MC145XXX series in a PLL to provide tuning signals up to 1.1 GHz in programmable frequency steps.

A Divide Ratio Control (SW) permits selection of a 127/128 or 255/256 divide ratio as desired.

The Modulus Control (MC) selects the proper divide number after SW has been biased to select the desired divide ratio.

- 1.1 GHz Toggle Frequency
- Supply Voltage of 4.5 to 5.5 V
- Low-Power 4.8 mA Typical
- Operating Temperature Range of -40 to 85°C
- Short Setup Time (t_{set}) 16ns Maximum @ 1.1 GHz
- Modulus Control Input Level Is Compatible With Standard CMOS and TTL
- On-Chip Output Termination

**NOT RECOMMENDED FOR NEW DESIGN
DEVICE TO BE PHASED OUT.
No replacement available.**

FUNCTIONAL TABLE

SW	MC	Divide Ratio
H	H	127
H	L	128
L	H	255
L	L	256

NOTES: 1. SW: H = V_{CC} , L = Open. A logic L can also be applied by grounding this pin, but this is not recommended due to increased power consumption.
2. MC: H = 2.0 V to V_{CC} , L = GND to 0.8 V.

DESIGN GUIDE

Criteria	Value	Unit
Internal Gate Count*	67	ea
Internal Gate Propagation Delay	200	ps
Internal Gate Power Dissipation	0.75	mW
Speed Power Product	0.15	pJ

NOTE: * Equivalent to a two-input NAND gate

MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Power Supply Voltage, Pin 2	V_{CC}	-0.5 to 7.0	Vdc
Operating Temperature Range	T_A	-40 to 85	°C
Storage Temperature Range	T_{stg}	-65 to 150	°C
Modulus Control Input, Pin 6	MC	-0.5 to 6.5	Vdc

NOTE: ESD data available upon request.

MC12038A

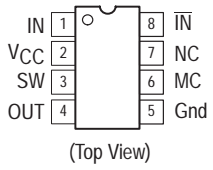
MECL PLL COMPONENTS ÷127/128, ÷255/256 DUAL MODULUS PRESCALER

SEMICONDUCTOR TECHNICAL DATA



**D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)**

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12038AD	$T_A = -40$ to 85°C	SO-8

MC12038A

ELECTRICAL CHARACTERISTICS ($V_{CC} = 4.5$ to $5.5V$; $T_A = -40$ to $85^\circ C$, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave Input)	f_t	0.1	1.4	1.1	GHz
Supply Current Output Unloaded (Pin 2) at 5.0 Vdc	I_{CC}	–	4.8	6.5	mA
Modulus Control Input High (MC)	V_{IH1}	2.0	–	V_{CC}	V
Modulus Control Input Low (MC)	V_{IL1}	–	–	0.8	V
Divide Ratio Control Input High (SW)	V_{IH2}	V_{CC}	V_{CC}	V_{CC}	Vdc
Divide Ratio Control Input Low (SW)	V_{IL2}	Open	Open	Open	–
Output Voltage Swing ($C_L = 8.0$ pF)	V_{out}	1.0	1.6	–	V_{pp}
Modulus Setup Time MC to Out	t_{set}	–	11	16	ns
Input Voltage Sensitivity 250–1100 MHz 100–250 MHz	$V_{in(min)}$	100 400	– –	1500 1500	mVpp

Figure 1. Logic Diagram (MC12038A)

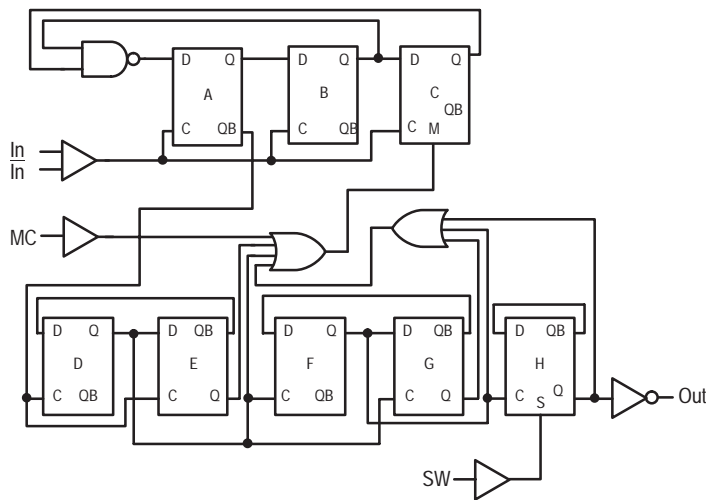
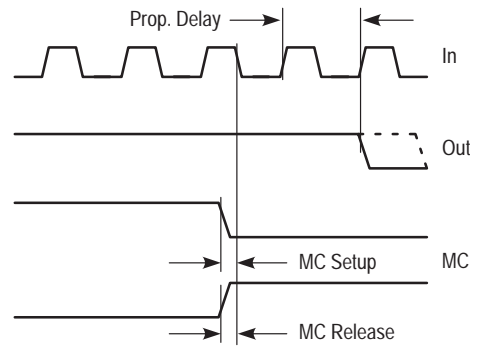
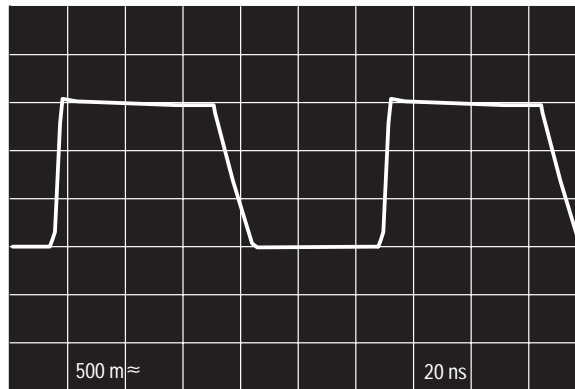


Figure 2. Modulus Setup Time



Modulus setup time MC to out is the MC setup or MC release plus the prop delay.

Figure 3. Typical Output Waveforms



(± 128 , 1.1 GHz Input Frequency, $V_{CC} = 5.0$ V, $T_A = 25^\circ C$, Output Loaded)

MC12038A

Figure 4. AC Test Circuit

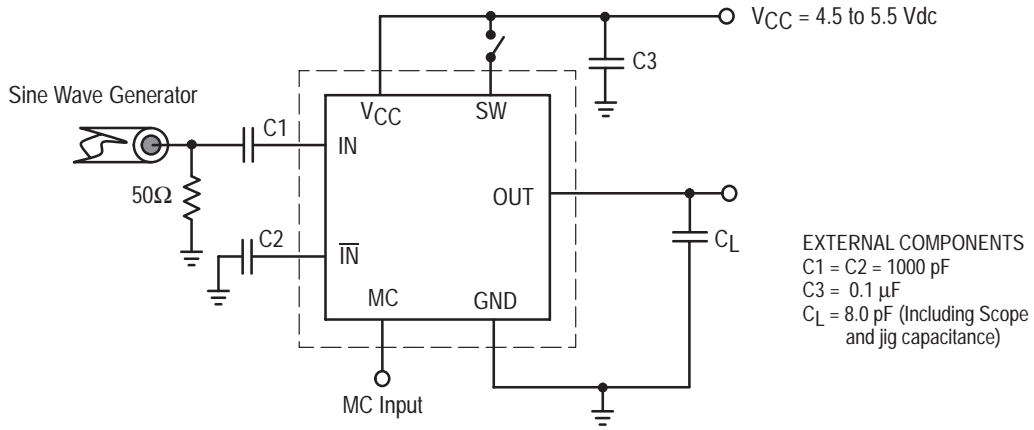
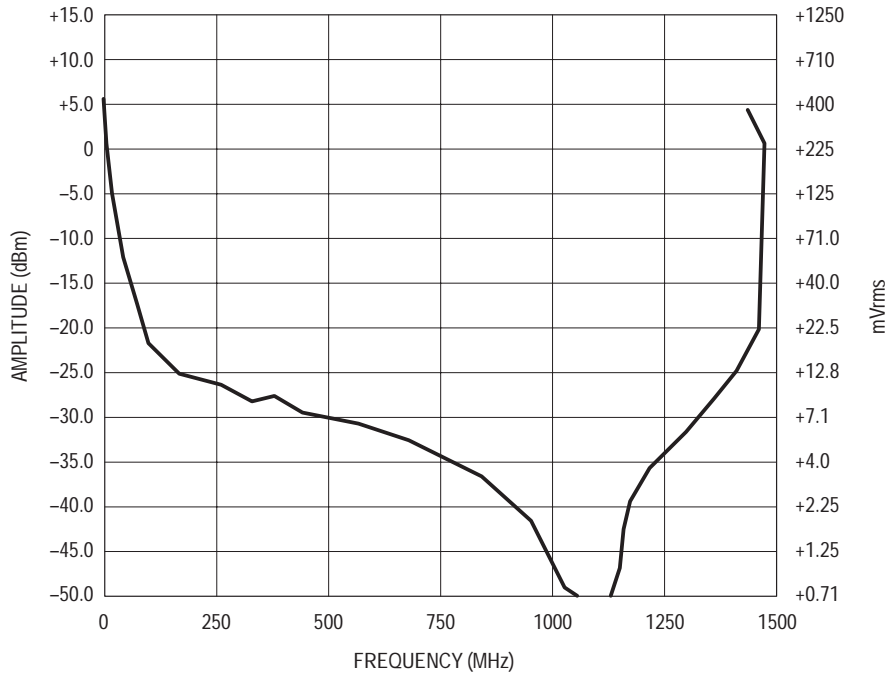
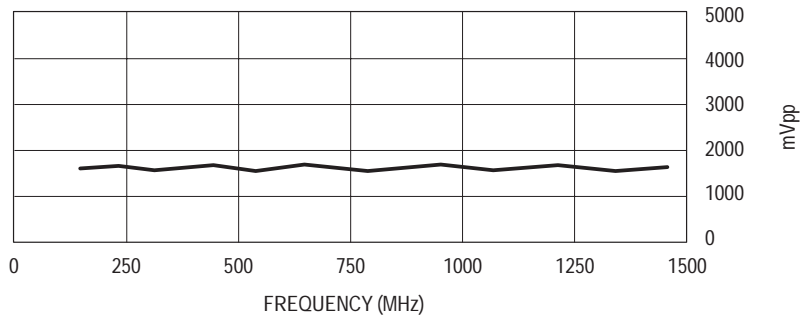


Figure 5. Input Signal Amplitude versus Input Frequency



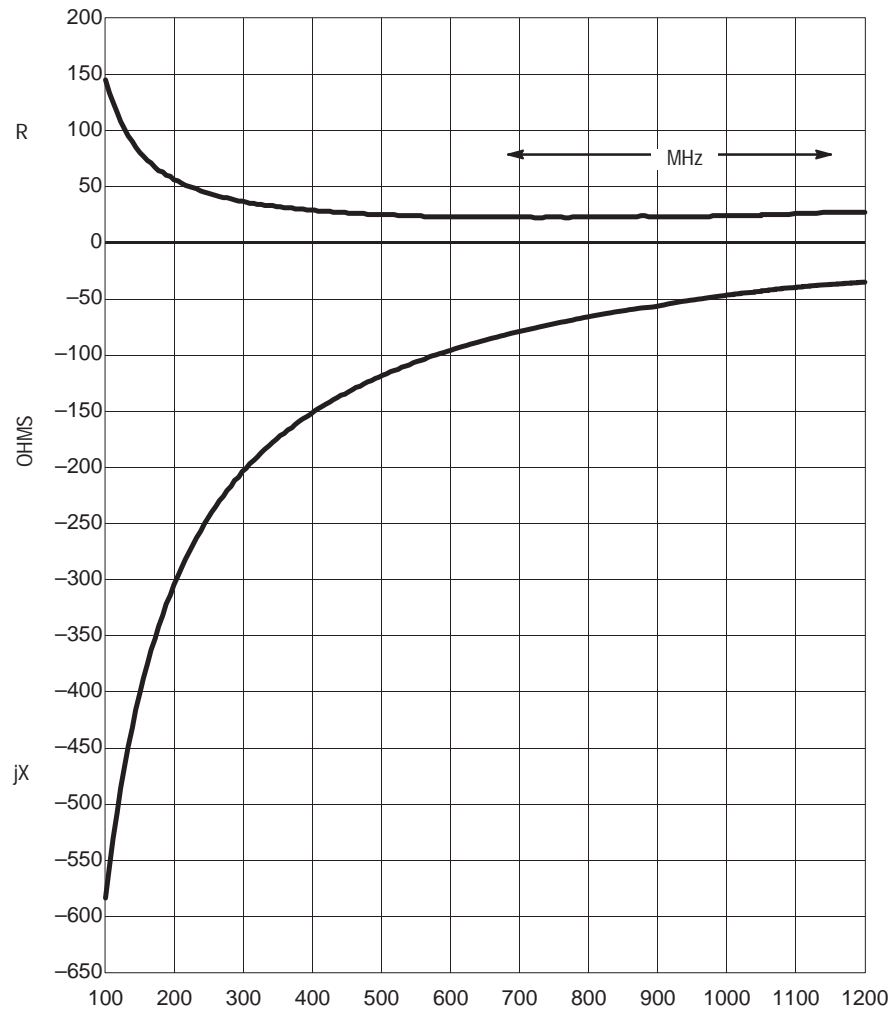
Divide Ratio = 128; $V_{CC} = 5.0 \text{ V}$; $T_A = 25^\circ\text{C}$

Figure 6. Output Amplitude versus Input Frequency



MC12038A

Figure 7. Typical Input Impedance versus Input Frequency





1.1 GHz Super Low Power Dual Modulus Prescaler

The MC12052A is a super low power dual modulus prescaler used in phase-locked loop applications. Motorola's advanced Bipolar MOSAIC™ V technology is utilized to achieve low power dissipation of 2.7 mW at a minimum supply voltage of 2.7 V.

The MC12052A can be used with CMOS synthesizers requiring positive edges to trigger internal counters such as Motorola's MC145XXX series in a PLL to provide tuning signals up to 1.1 GHz in programmable frequency steps.

A Divide Ratio Control (SW) permits selection of a 64/65 or 128/129 divide ratio as desired.

The Modulus Control (MC) selects the proper divide number after SW has been biased to select the desired divide ratio.

- 1.1 GHz Toggle Frequency
- The MC12052 is Pin and Functionally Compatible with the MC12022
- Low Power 1.0 mA Typical
- 2.0 mA Maximum, -40 to 85°C, V_{CC} = 2.7 to 5.5 Vdc
- Short Setup Time (t_{set}) 16 ns Maximum @ 1.1 GHz
- Modulus Control Input Level is Compatible with Standard CMOS and TTL
- Maximum Input Voltage Should Be Limited to 6.5 Vdc

MOSAIC V is a trademark of Motorola

FUNCTIONAL TABLE

SW	MC	Divide Ratio
H	H	64
H	L	65
L	H	128
L	L	129

NOTES: 1. SW: H = V_{CC}, L = Open. A logic L can also be applied by grounding this pin, but this is not recommended due to increased power consumption.
 2. MC: H = 2.0 V to V_{CC}, L = GND to 0.8 V.

MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Power Supply Voltage, Pin 2	V _{CC}	-0.5 to 7.0	Vdc
Operating Temperature Range	T _A	-40 to 85	°C
Storage Temperature Range	T _{stg}	-65 to 150	°C
Modulus Control Input, Pin 6	MC	-0.5 to 6.5	Vdc

MC12052A

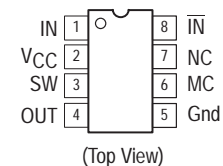
MECL PLL COMPONENTS ÷64/65, ÷128/129 LOW POWER DUAL MODULUS PRESCALER

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temp Range	Package
MC12052AD	T _A = -40 to 85°C	SO-8

MC12052A

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ to 5.5 VDC, $T_A = -40$ to 85°C , unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave Input)	f_t	0.1	1.4	1.1	GHz
Supply Current (Pin 2)	I_{CC}	–	1.0	2.0	mA
Modulus Control Input High (MC)	V_{IH1}	2.0	–	$V_{CC} + 0.5$ V	V
Modulus Control Input Low (MC)	V_{IL1}	Gnd	–	0.8	V
Divide Ratio Control Input High (SW)	V_{IH2}	$V_{CC} - 0.5$ V	V_{CC}	$V_{CC} + 0.5$ V	VDC
Divide Ratio Control Input Low (SW)	V_{IL2}	Open	Open	Open	–
Output Voltage Swing (Note 2) ($C_L = 8.0$ pF, $R_L = 3.3$ k Ω)	V_{out}	0.8	1.1	–	V _{PP}
Modulus Setup Time MC to Out @ 1100 MHz	t_{set}	–	11	16	ns
Input Voltage Sensitivity 250–1100 MHz 100–250 MHz	V_{in}	100 400	– –	1000 1000	mV _{PP}
Output Current (Note 1) $V_{CC} = 2.7$ V, $C_L = 8.0$ pF, $R_L = 3.3$ k Ω $V_{CC} = 5.0$ V, $C_L = 8.0$ pF, $R_L = 7.2$ k Ω	I_O	– –	0.5 0.5	3.0 3.0	mA

NOTES: 1. Divide ratio of +64/65 @ 1.1 GHz
2. Valid over voltage range 2.7 to 5.5 V; $R_L = 3.3$ k Ω @ $V_{CC} = 2.7$ V; $R_L = 7.2$ k Ω @ $V_{CC} = 5.0$ V

Figure 1. Logic Diagram (MC12052A)

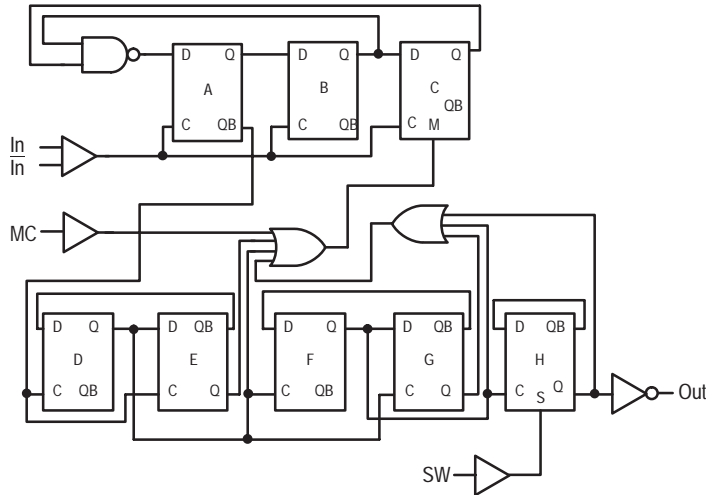


Figure 2. Modulus Setup Time

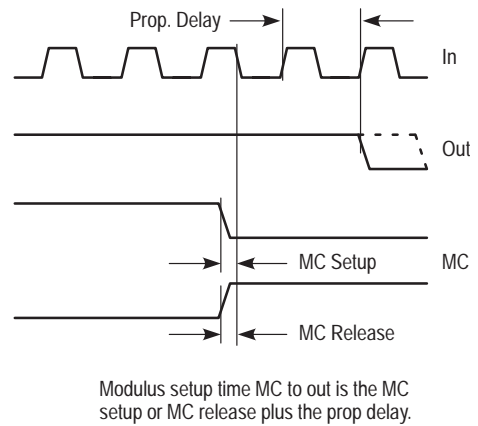
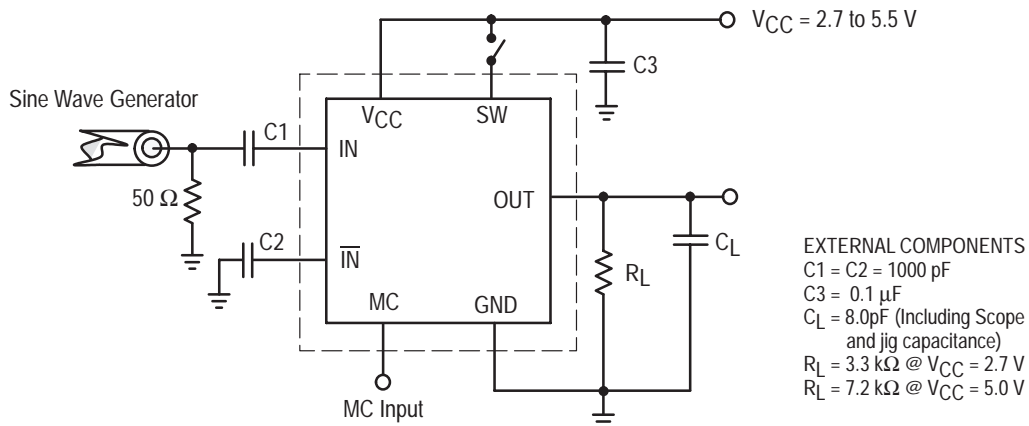
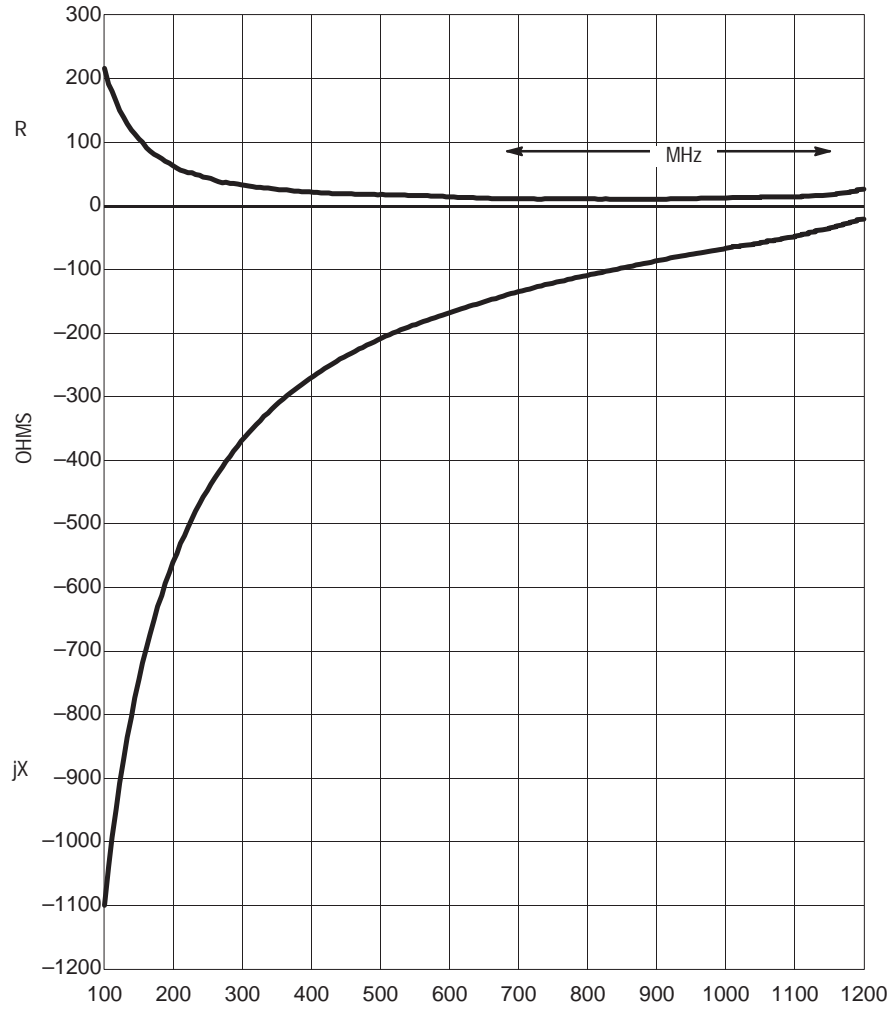


Figure 3. AC Test Circuit



MC12052A

Figure 4. Typical Input Impedance versus Input Frequency





MOTOROLA

2.0 GHz Super Low Power Dual Modulus Prescaler

The MC12054A is a super low power dual modulus prescaler used in phase-locked loop applications. Motorola's advanced Bipolar MOSAIC™ V technology is utilized to achieve low power dissipation of 5.4 mW at a minimum supply voltage of 2.7 V.

The MC12054A can be used with CMOS synthesizers requiring positive edges to trigger internal counters such as Motorola's MC145XXX series in a PLL to provide tuning signals up to 2.0 GHz in programmable frequency steps.

A Divide Ratio Control (SW) permits selection of a 64/65 or 128/129 divide ratio as desired.

The Modulus Control (MC) selects the proper divide number after SW has been biased to select the desired divide ratio.

- 2.0 GHz Toggle Frequency
- The MC12054 is Pin and Functionally Compatible with the MC12031
- Low Power 2.0 mA Typical
- 2.6mA Maximum, -40 to 85°C, V_{CC} = 2.7 to 5.5 Vdc
- Short Setup Time (t_{set}) 10ns Maximum @ 2.0 GHz
- Modulus Control Input Level is Compatible with Standard CMOS and TTL
- Maximum Input Voltage Should Be Limited to 6.5 Vdc

MOSAIC V is a trademark of Motorola

FUNCTIONAL TABLE

SW	MC	Divide Ratio
H	H	64
H	L	65
L	H	128
L	L	129

NOTES: 1. SW: H = V_{CC}, L = Open. A logic L can also be applied by grounding this pin, but this is not recommended due to increased power consumption.
 2. MC: H = 2.0 V to V_{CC}, L = GND to 0.8 V.

MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Power Supply Voltage, Pin 2	V _{CC}	-0.5 to 7.0	Vdc
Operating Temperature Range	T _A	-40 to 85	°C
Storage Temperature Range	T _{stg}	-65 to 150	°C
Modulus Control Input, Pin 6	MC	-0.5 to 6.5	Vdc

NOTE: ESD data available upon request.

MC12054A

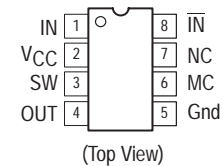
MECL PLL COMPONENTS ÷64/65, ÷128/129 LOW POWER DUAL MODULUS PRESCALER

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
 PLASTIC PACKAGE
 CASE 751
 (SO-8)

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temp Range	Package
MC12054AD	T _A = -40 to 85°C	SO-8

MC12054A

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ to 5.5 Vdc, $T_A = -40$ to 85°C , unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave Input)	f_t	0.1	2.5	2.0	GHz
Supply Current (Pin 2)	I_{CC}	–	2.0	2.6	mA
Modulus Control Input High (MC)	V_{IH1}	2.0	–	$V_{CC} + 0.5$ V	V
Modulus Control Input Low (MC)	V_{IL1}	Gnd	–	0.8	V
Divide Ratio Control Input High (SW)	V_{IH2}	$V_{CC} - 0.5$ V	V_{CC}	$V_{CC} + 0.5$ V	VDC
Divide Ratio Control Input Low (SW)	V_{IL2}	Open	Open	Open	–
Output Voltage Swing (Note 2) ($C_L = 8.0$ pF, $R_L = 1.65$ k Ω)	V_{out}	0.8	1.1	–	V_{pp}
Modulus Setup Time MC to Out @ 2000 MHz	t_{set}	–	8.0	10	ns
Input Voltage Sensitivity 250–2000 MHz 100–250 MHz	V_{in}	100 400	– –	1000 1000	mVpp
Output Current (Note 1) $V_{CC} = 2.7$ V, $C_L = 8.0$ pF, $R_L = 1.65$ k Ω $V_{CC} = 5.0$ V, $C_L = 8.0$ pF, $R_L = 3.6$ k Ω	I_O	– –	1.0 1.0	4.0 4.0	mA

NOTES: 1. Divide ratio of +64/65 @ 2.0 GHz
2. Valid over voltage range 2.7 to 5.5 V; $R_L = 1.65$ k Ω @ $V_{CC} = 2.7$ V; $R_L = 3.6$ k Ω @ $V_{CC} = 5.0$ V

Figure 1. Logic Diagram (MC12054A)

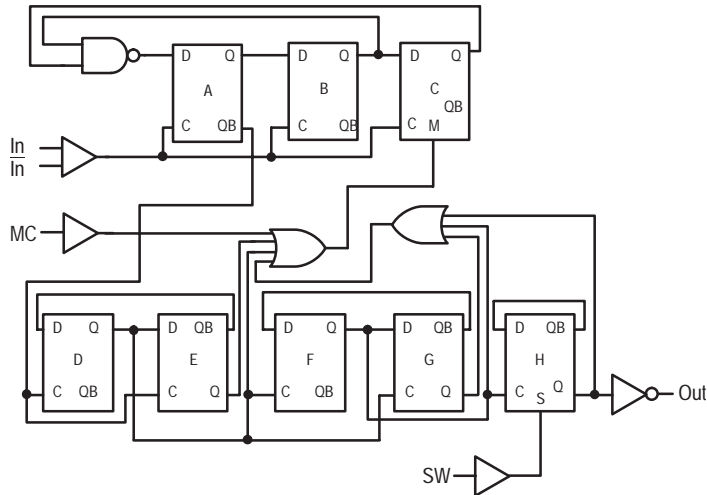
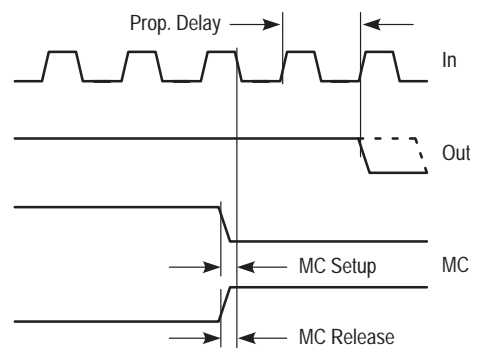
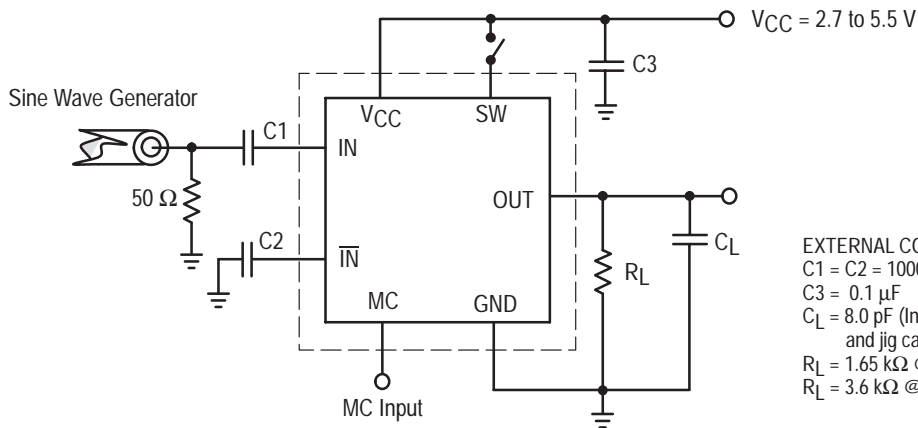


Figure 2. Modulus Setup Time



Modulus setup time MC to out is the MC setup or MC release plus the prop delay.

Figure 3. AC Test Circuit



EXTERNAL COMPONENTS
 $C_1 = C_2 = 1000$ pF
 $C_3 = 0.1$ μ F
 $C_L = 8.0$ pF (Including Scope and jig capacitance)
 $R_L = 1.65$ k Ω @ $V_{CC} = 2.7$ V
 $R_L = 3.6$ k Ω @ $V_{CC} = 5.0$ V



2.8 GHz Prescaler

The MC12079 is a single modulus divide by 64, 128, 256 prescaler for low power frequency division of a 2.8 GHz (typical) high frequency input signal. Divide ratio control inputs SW1 and SW2 select the required divide ratio of ÷64, ÷128, or ÷256.

An external load resistor is required to terminate the output. A 1.2 kΩ resistor is recommended to achieve a 1.6 V_{pp} output swing, when dividing a 1.1 GHz input signal by the minimum divide ratio of 64, assuming a 12 pF load. Output current can be minimized dependent on conditions such as output frequency, capacitive load being driven, and output voltage swing required. Typical values for load resistors are included in the V_{out} specification for various divide ratios at 2.8 GHz input frequency.

- 2.8 GHz Toggle Frequency
- Supply Voltage 4.5 to 5.5 V
- Low Power 9mA Typical at V_{CC} = 5.0 V
- Operating Temperature Range of -40 to 85°C

FUNCTIONAL TABLE

SW1	SW2	Divide Ratio
H	H	64
H	L	128
L	H	128
L	L	256

NOTE: SW1 & SW2: H = V_{CC}, L = Open.

MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Power Supply Voltage, Pin 2	V _{CC}	-0.5 to 7.0	Vdc
Operating Temperature Range	T _A	-40 to 85	°C
Storage Temperature Range	T _{stg}	-65 to 150	°C
Maximum Output Current, Pin 4	I _O	4.0	mA

NOTE: ESD data available upon request.

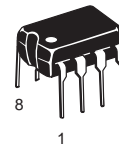
MC12079

MECL PLL COMPONENTS ÷64/128/256 PRESCALER

SEMICONDUCTOR TECHNICAL DATA

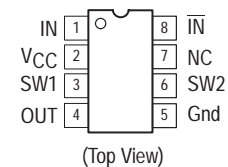


D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)



P SUFFIX
PLASTIC PACKAGE
CASE 626

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12079D	T _A = -40° to +85°C	SO-8
MC12079P		Plastic

MC12079

ELECTRICAL CHARACTERISTICS ($V_{CC} = 4.5$ to 5.5 V; $T_A = -40$ to 85°C , unless otherwise noted.)

Parameter	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave)	ft	0.25	3.4	2.8	GHz
Supply Current Output (Pin 2)	I_{CC}	–	9.0	11.5	mA
Input Voltage Sensitivity	V_{in}	400 100	– –	1000 1000	mVpp
Divide Ratio Control Input High (SW)	V_{IH}	V_{CC}	V_{CC}	V_{CC}	V
Divide Ratio Control Input Low (SW)	V_{IL}	Open	Open	Open	–
Output Voltage Swing	V_{out}	1.0	1.6	–	Vpp
$(C_L = 12$ pF; $R_L = 1.2$ k Ω ; $I_O = 2.7$ mA) ¹ $(C_L = 12$ pF; $R_L = 2.2$ k Ω ; $I_O = 1.5$ mA) ² $(C_L = 12$ pF; $R_L = 3.9$ k Ω ; $I_O = 0.85$ mA) ³					

NOTES: 1. Divide ratio of +64 at 2.8 GHz.
 2. Divide ratio of +128 at 2.8 GHz.
 3. Divide ratio of +256 at 2.8 GHz.

Figure 1. Logic Diagram (MC12079)

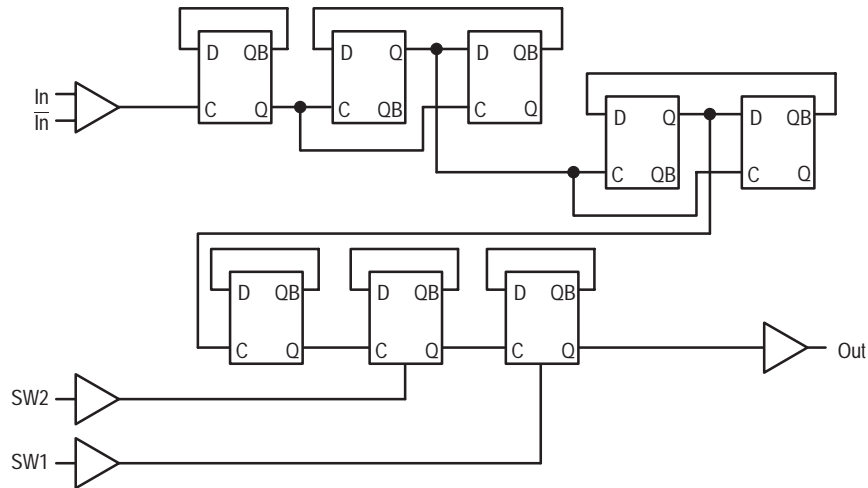
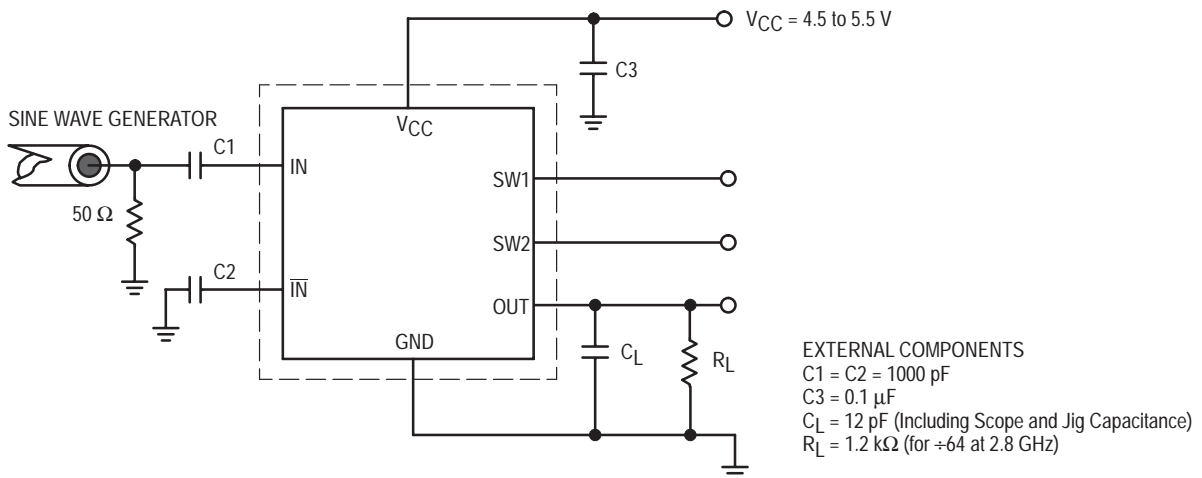
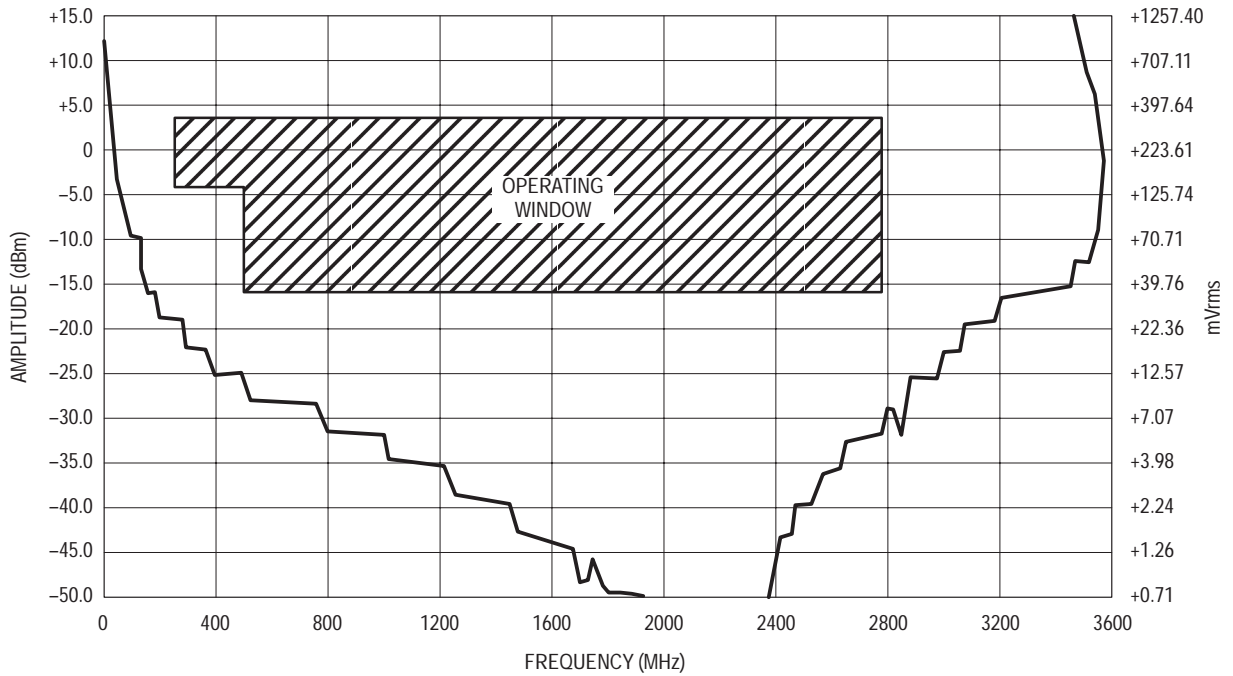


Figure 2. AC Test Circuit



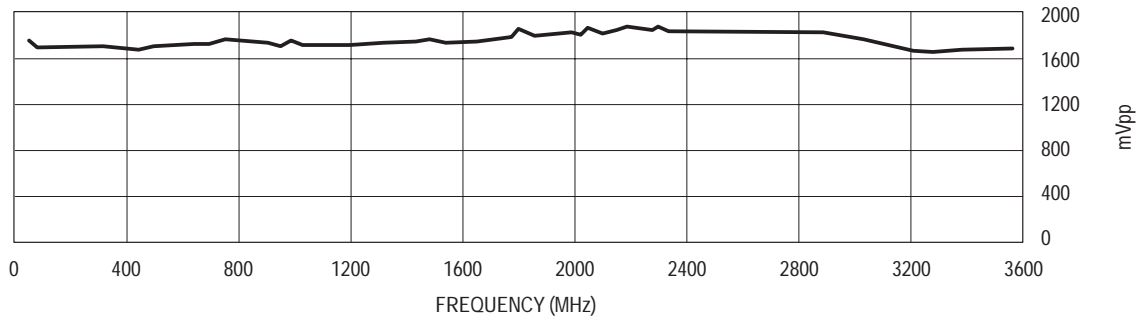
MC12079

Figure 3. Input Signal Amplitude versus Input Frequency



Divide Ratio = 64; $V_{CC} = 5.0$ V; $T_A = 25^\circ\text{C}$

Figure 4. Output Amplitude versus Input Frequency



1.1 GHz Prescaler

The MC12080 is a single modulus divide by 10, 20, 40, 80 prescaler for low power frequency division of a 1.1 GHz high frequency input signal. Divide ratio control inputs SW1, SW2 and SW3 select the required divide ratio of ÷10, ÷20, ÷40, or ÷80.

An external load resistor is required to terminate the output. A 820 Ω resistor is recommended to achieve a 1.2 V_{pp} output swing, when dividing a 1.1 GHz input signal by the minimum divide by ratio of 10, assuming a 8.0 pF load. Output current can be minimized dependent on conditions such as output frequency, capacitive load being driven, and output voltage swing required. Typical values for load resistors are included in the V_{out} specification for various divide ratios at 1.1 GHz input frequency.

- 1.1 GHz Toggle Frequency
- Supply Voltage 4.5 to 5.5 V
- Low Power 3.7mA Typical at V_{CC} = 5.0 V
- Operating Temperature Range of -40 to 85°C

FUNCTIONAL TABLE

SW1	SW2	SW3	Divide Ratio
L	L	L	80
L	L	H	40
L	H	L	40
L	H	H	20
H	L	L	40
H	L	H	20
H	H	L	20
H	H	H	10

NOTE: SW1, SW2 and SW3: H = V_{CC}, L = Open.

MAXIMUM RATINGS

Characteristic	Symbol	Range	Unit
Power Supply Voltage, Pin 2	V _{CC}	-0.5 to 7.0	Vdc
Operating Temperature Range	T _A	-40 to 85	°C
Storage Temperature Range	T _{stg}	-65 to 150	°C
Maximum Output Current, Pin 4	I _O	10	mA

NOTE: ESD data available upon request.

MC12080

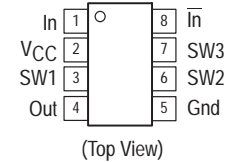
MECL PLL COMPONENTS ÷10/20/40/80 PRESCALER

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8, Tape and Reel Only)

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12080DR2	T _A = -40 to 85°C	SO-8

MC12080

ELECTRICAL CHARACTERISTICS ($V_{CC} = 4.5$ to 5.5 V; $T_A = -40$ to 85°C , unless otherwise noted.)

Parameter	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave)	ft	0.1	1.4	1.1	GHz
Supply Current Output (Pin 2)	I_{CC}	–	3.7	5.0	mA
Input Voltage Sensitivity 100 to 250 MHz 250 to 1100 MHz	V_{in}	400 100	– –	1000 1000	mVpp
Divide Ratio Control Input High (SW1, SW2, SW3)	V_{IH}	$V_{CC} - 0.5$ V	V_{CC}	$V_{CC} + 0.5$ V	V
Divide Ratio Control Input Low (SW1, SW2, SW3)	V_{IL}	Open	Open	Open	–
Output Voltage Swing [Note] $R_L = 820 \Omega$, $I_O = 4.0$ mA for $\div 10$ $R_L = 1.6$ k Ω , $I_O = 2.1$ mA for $\div 20$ $R_L = 3.3$ k Ω , $I_O = 1.1$ mA for $\div 40$ $R_L = 6.2$ k Ω , $I_O = 0.57$ mA for $\div 80$	V_{out}	0.8	1.2	–	V_{pp}

NOTE: Assumes 8.0 pF load and 1.1 GHz input frequency (typical), I_O at $V_{CC} = 5.0$ V and $T_A = 25^\circ\text{C}$

Figure 1. Logic Diagram

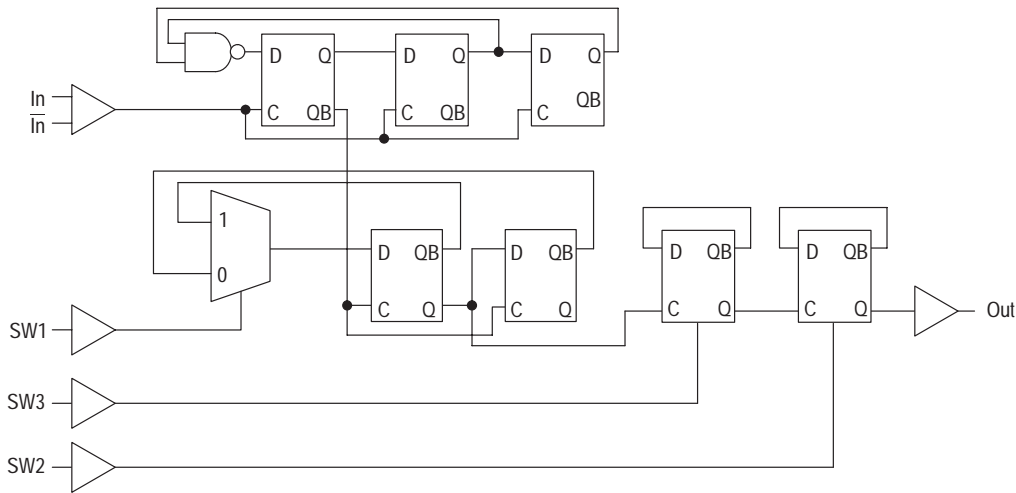
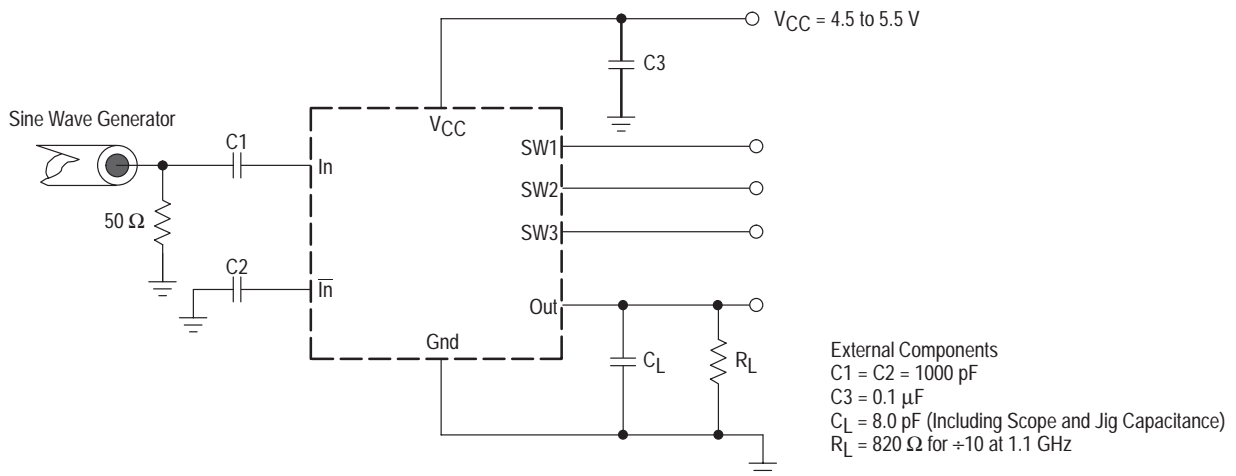


Figure 2. AC Test Circuit



MC12080

Figure 3. Input Signal Amplitude versus Input Frequency

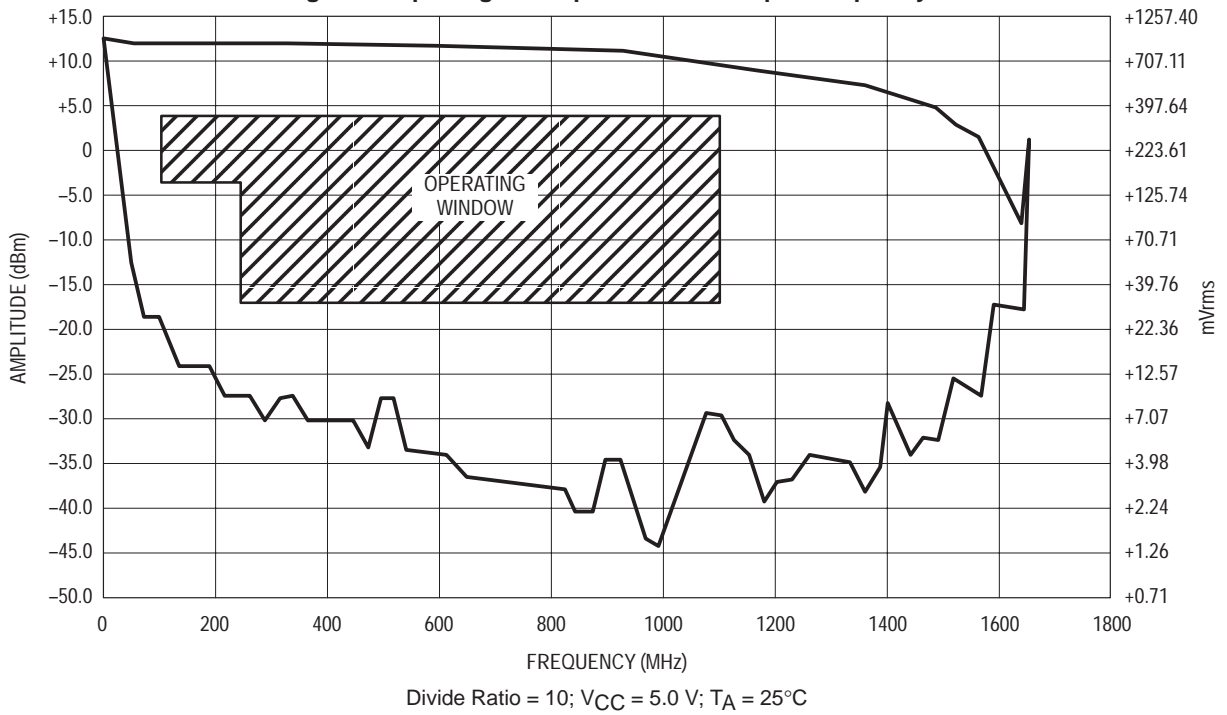
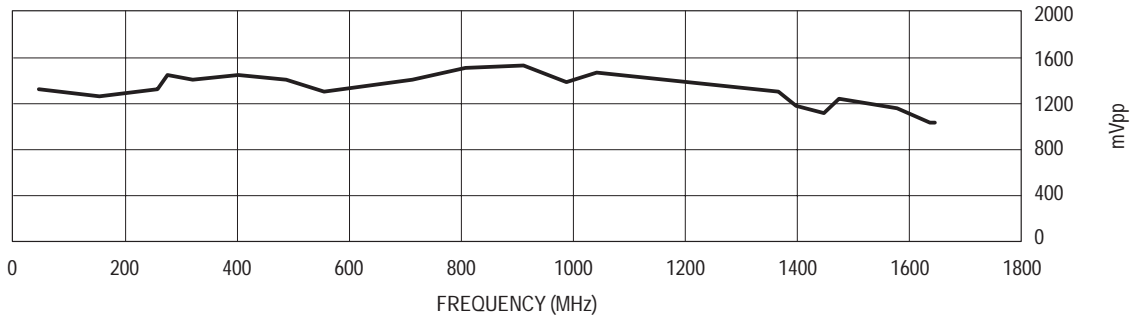


Figure 4. Output Amplitude versus Input Frequency





MOTOROLA

÷2, ÷4, ÷8 1.1GHz Low Power Prescaler with Stand-By Mode

The MC12093 is a single modulus prescaler for low power frequency division of a 1.1 GHz high frequency input signal. Motorola's advanced MOSAIC™ V technology is utilized to achieve low power dissipation of 6.75 mW at a minimum supply voltage of 2.7 V.

On-chip output termination provides output current to drive a 2.0 pF (typical) high impedance load. If additional drive is required for the prescaler output, an external resistor can be added parallel from the OUT pin to GND to increase the output power. Care must be taken not to exceed the maximum allowable current through the output.

Divide ratio control inputs SW1 and SW2 select the required divide ratio of ÷2, ÷4, or ÷8.

Stand-By mode is featured to reduce current drain to 50 µA typical when the standby pin SB is switched LOW disabling the prescaler.

- 1.1 GHz Toggle Frequency
- Supply Voltage 2.7 V to 5.5 Vdc
- Low Power 3.0 mA Typical
- Operating Temperature -40 to 85°C
- Divide by 2, 4 or 8 Selected by SW1 and SW2 Pins
- On-Chip Termination

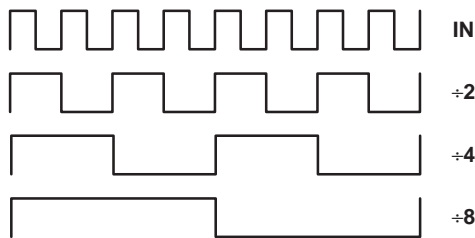
MOSAIC V is a trademark of Motorola

FUNCTIONAL TABLE

SW	SW2	Divide Ratio
L	L	8
H	L	4
L	H	4
H	H	2

NOTES: 1. SW1 & SW2: H = (V_{CC} - 0.5 V) to V_{CC}; L = Open.
 2. SB: H = 2.0 V to V_{CC}, L = GND to 0.8 V.

Function Chart



MC12093

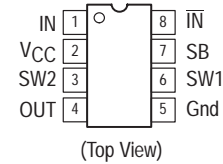
MECL PLL COMPONENTS ÷2, ÷4, ÷8 LOW POWER PRESCALER WITH STAND-BY MODE

**SEMICONDUCTOR
 TECHNICAL DATA**



D SUFFIX
 PLASTIC PACKAGE
 CASE 751
 (SO-8)

PIN CONNECTIONS



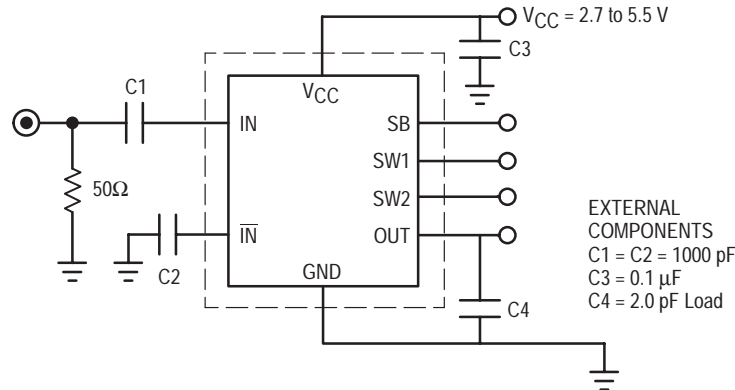
A LOW on the Stand-By Pin 7 disables the device.

ORDERING INFORMATION

Device	Operating Temp Range	Package
MC12093D	T _A = -40 to 85°C	SO-8

MC12093

Figure 1. AC Test Circuit



MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
Power Supply Voltage, Pin 2	V_{CC}	-0.5 to 6.0	Vdc
Operating Temperature Range	T_A	-40 to 85	°C
Storage Temperature Range	T_{stg}	-65 to 150	°C
Maximum Output Current, Pin 4	I_O	4.0	mA

NOTE: ESD data available upon request.

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ to 5.5 V; $T_A = -40$ to 85°C)

Parameter	Symbol	Min	Typ	Max	Unit
Toggle Frequency (Sine Wave)	ft	0.1	1.4	1.1	GHz
Supply Current	I_{CC}	-	3.0	4.5	mA
Stand-By Current	ISB	-	120	200	μA
Stand-By Input HIGH (SB)	V_{IH1}	2.0	-	V_{CC}	V
Stand-By Input LOW (SB)	V_{IL1}	Gnd	-	0.8	V
Divide Ratio Control Input HIGH (SW1 & SW2)	V_{IH2}	$V_{CC} - 0.5$	V_{CC}	$V_{CC} + 0.5$	V
Divide Ratio Control Input LOW (SW1 & SW2)	V_{IL2}	OPEN	OPEN	OPEN	
Output Voltage Swing (2.0 pF Load)	V_{OUT}				V_{pp}
Output Frequency 12.5–350 MHz (Note 1)		0.6	0.80	-	
Output Frequency 350–400 MHz (Note 2)		0.5	0.70	-	
Output Frequency 400–450 MHz (Note 3)		0.4	0.55	-	
Output Frequency 450–550 MHz (Note 4)		0.3	0.45	-	
Input Voltage Sensitivity					mVpp
250–1100 MHz	V_{IN}	100	-	1000	
100–250 MHz		400	-	1000	

NOTES: 1. Input frequency 1.1 GHz, +8, minimum output frequency of 12.5 MHz.

2. Input frequency 700–800 MHz, +2.

3. Input frequency 800–900 MHz, +2.

4. Input frequency 900–1100 MHz, +2.



2.5 GHz Low Power Prescaler With Stand-By Mode

The MC12095 is a single modulus prescaler for low power frequency division of a 2.5 GHz high frequency input signal. Motorola's advanced MOSAIC™ V technology is utilized to achieve low power dissipation of 24 mW at a minimum supply voltage of 2.7 V.

On-chip output termination provides output current to drive a 2.0 pF (typical) high impedance load. If additional drive is required for the prescaler output, an external resistor can be added in parallel from the OUT pin to GND to increase the output power. Care must be taken not to exceed the maximum allowable current through the output.

Divide ratio control input (SW) selects the required divide ratio of ÷2 or ÷4. Stand-By mode is available to reduce current drain to 100µA typical when the standby pin SB is switched LOW disabling the prescaler.

- 2.5 GHz Toggle Frequency
- Supply Voltage 2.7 V to 5.5 Vdc
- Low Power 8.7 mA Typical
- Operating Temperature -40 to 85°C
- Divide by 2 or 4 Selected by the SW Pin

NOTE: For applications up to 1.1 GHz, please consult the MC12093 datasheet.

MOSAIC V is a trademark of Motorola

FUNCTIONAL TABLE

SW	Divide Ratio
H	2
L	4

NOTES: 1. SW: H = (V_{CC} - 0.4 V) to V_{CC}; L = OPEN
 2. SB: H = 2.0 V to V_{CC}; L = GND to 0.8 V

MC12095

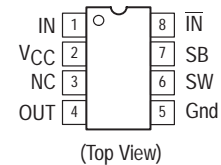
MECL PLL COMPONENTS ÷2, ÷4 LOW POWER PRESCALER WITH STAND-BY MODE

SEMICONDUCTOR TECHNICAL DATA

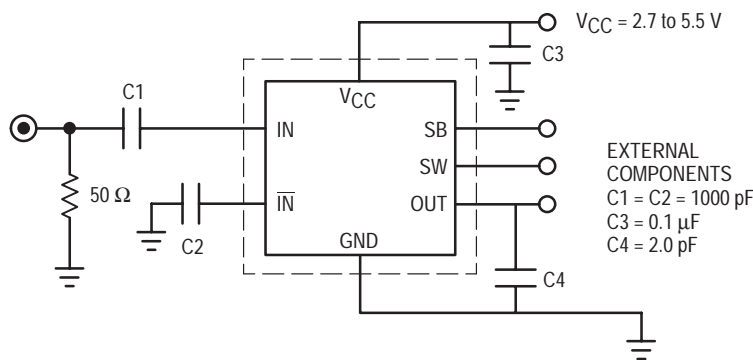


D SUFFIX
 PLASTIC PACKAGE
 CASE 751
 (SO-8)

PIN CONNECTIONS



AC Test Circuit



ORDERING INFORMATION

Device	Operating Temp Range	Package
MC12095D	T _A = -40 to 85°C	SO-8

MC12095

MAXIMUM RATINGS

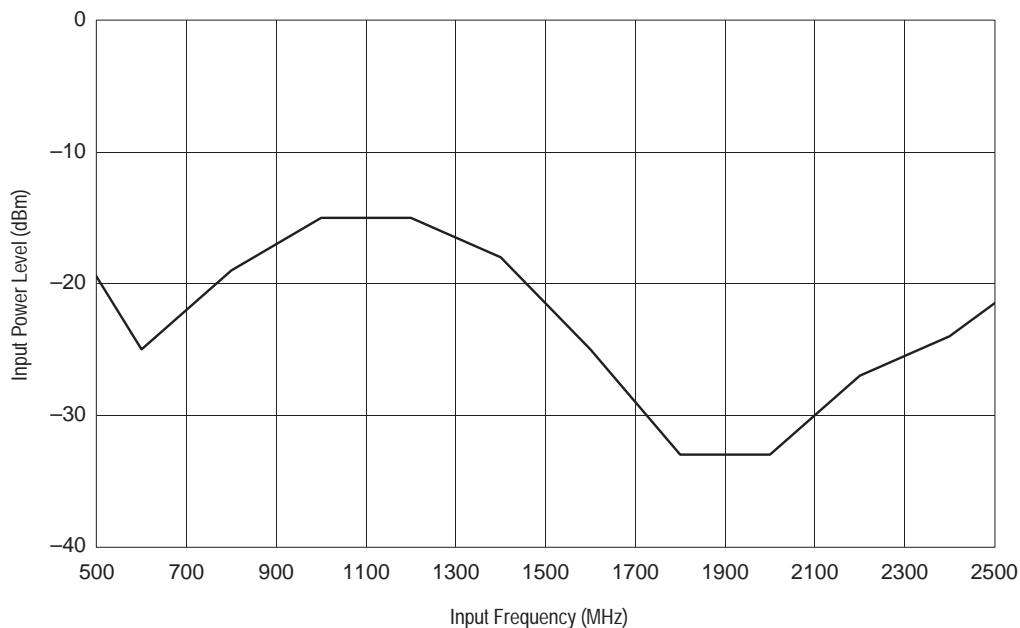
Parameter	Symbol	Value	Unit
Power Supply Voltage, Pin 2	V_{CC}	-0.5 to 6.0	Vdc
Operating Temperature Range	T_A	-40 to 85	°C
Storage Temperature Range	T_{stg}	-65 to 150	°C
Maximum Output Current, Pin 4	I_O	8.0	mA

NOTE: ESD data available upon request.

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ to 5.5 V; $T_A = -40$ to 85°C , unless otherwise noted.)

Parameter	Symbol	Min	Typ	Max	Unit	
Toggle Frequency (Sine Wave)	f_t	500	3.0	2.5	GHz	
Supply Current	I_{CC}	-	8.7	14	mA	
Stand-By Current	ISB	-	100	200	μA	
Stand-By Input HIGH (SB)	V_{IH1}	2.0	-	$V_{CC} + 0.5$ V	V	
Stand-By Input LOW (SB)	V_{IL1}	GND	-	0.8	V	
Divide Ratio Control Input HIGH (SW)	V_{IH2}	$V_{CC} - 0.4$	V_{CC}	$V_{CC} + 0.5$ V	V	
Divide Ratio Control Input LOW (SW)	V_{IL2}	OPEN	OPEN	OPEN		
Output Voltage Swing (2pF Load)	V_{OUT}	500–1000 MHz Input	800	-	-	mVpp
		1000–1500 MHz Input	400	450	-	
		1500–2500 MHz Input	200	250	-	
Input Voltage Sensitivity	V_{IN}	200	-	1000	mVpp	

Figure 1. Typical Minimum Input Sensitivity versus Input Frequency



(Divide By 2 Mode, $T = 25^\circ\text{C}$, $V_{CC} = 2.7$ V)

MC12095

Figure 2. Typical Output Amplitude versus Frequency over Temperature

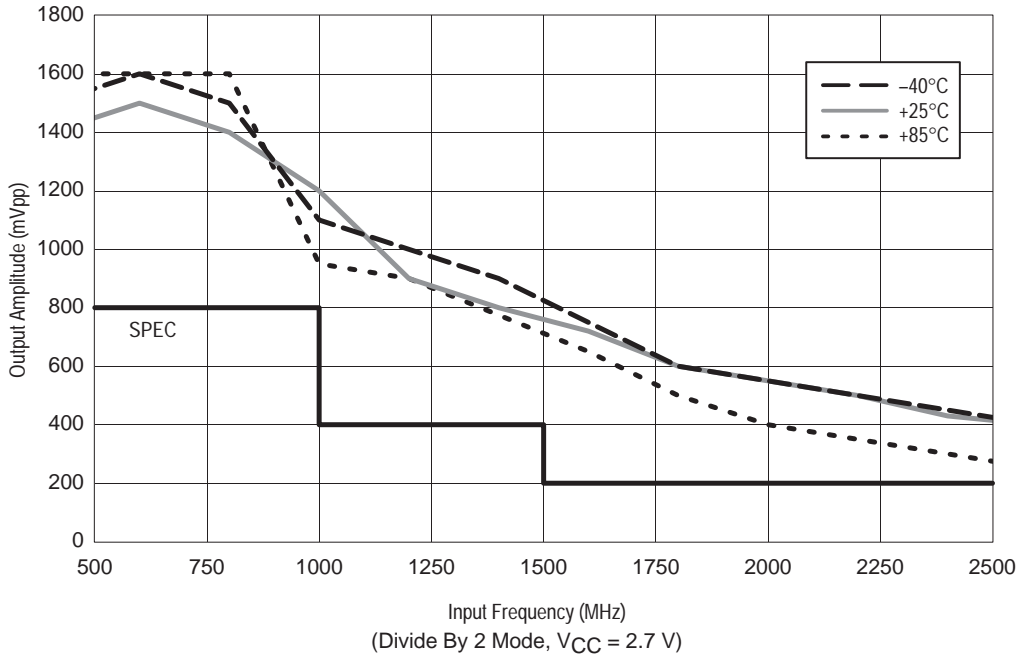
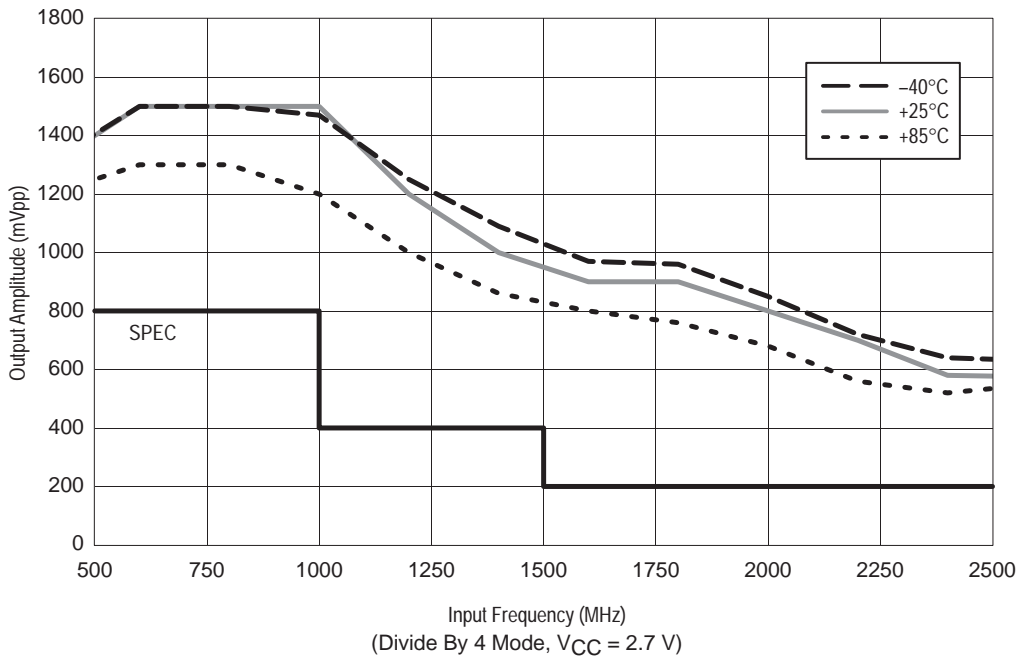


Figure 3. Typical Output Amplitude versus Frequency over Temperature



MC12095

Figure 4. Input Impedance versus Frequency

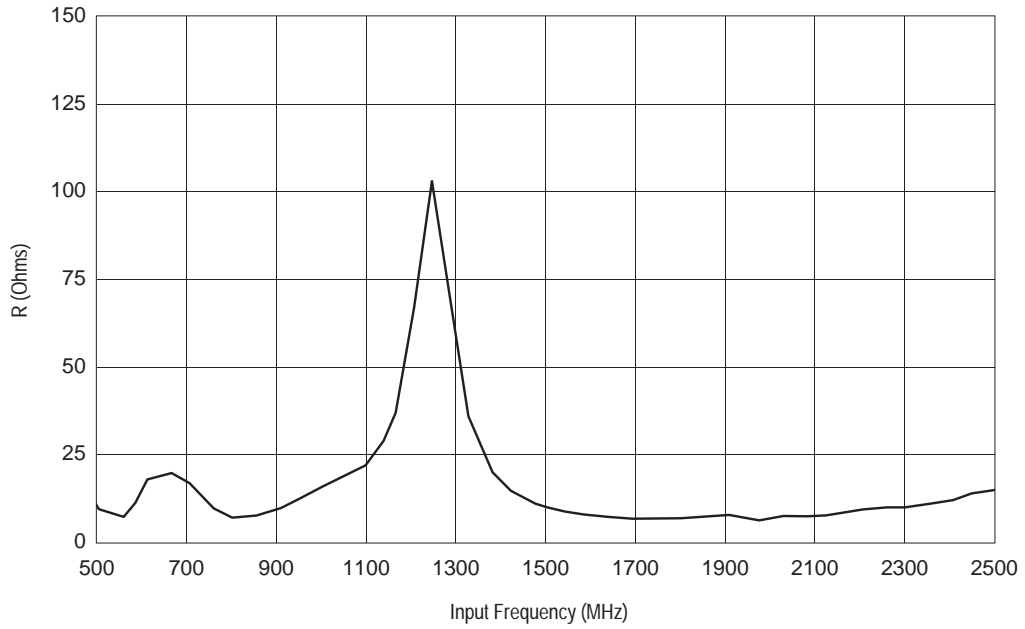
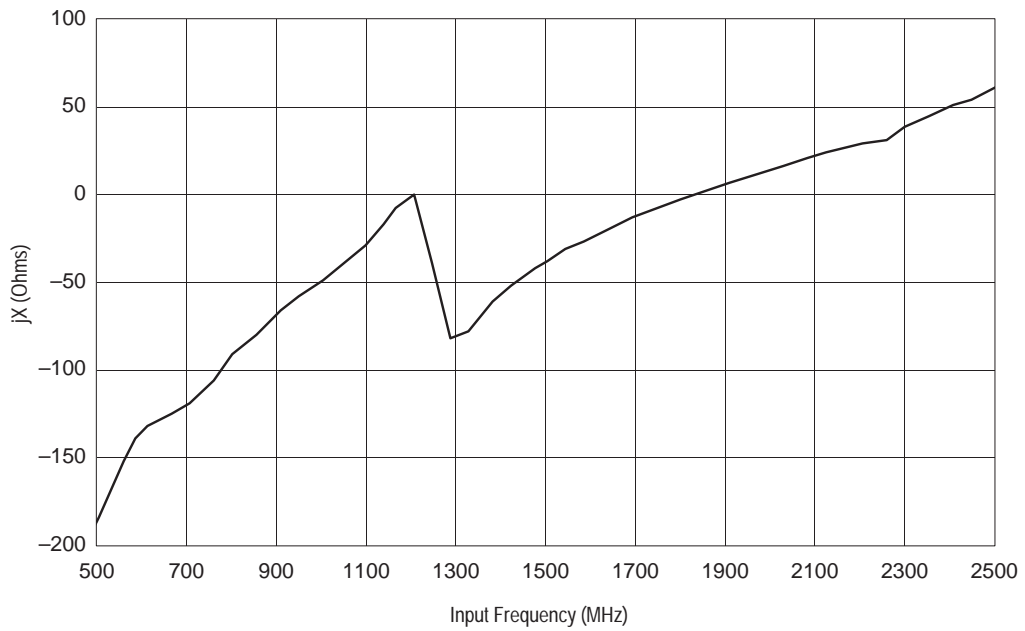


Figure 5. Input Impedance versus Frequency





Low Power Voltage Controlled Oscillator Buffer

The MC12147 is intended for applications requiring high frequency signal generation up to 1300 MHz. An external tank circuit is used to determine the desired frequency of operation. The VCO is realized using an emitter-coupled pair topology. The MC12147 can be used with an integrated PLL IC such as the MC12202 1.1 GHz Frequency Synthesizer to realize a complete PLL sub-system. The device is specified to operate over a voltage supply range of 2.7 to 5.5 V. It has a typical current consumption of 13 mA at 3.0 V which makes it attractive for battery operated handheld systems.

**NOT RECOMMENDED FOR NEW DESIGN
DEVICE TO BE PHASED OUT.
Consider MC12149 for New Designs.**

NOTE: The MC12147 is NOT suitable as a crystal oscillator.

- Operates Up to 1.3 GHz
- Space-Efficient 8-Pin SOIC or SSOP Package
- Low Power 13 mA Typical @ 3.0 V Operation
- Supply Voltage of 2.7 to 5.5 V
- Typical 900MHz Performance
 - Phase Noise -105 dBc/Hz @ 100 kHz Offset
 - Tuning Voltage Sensitivity of 20 MHz/V
- Output Amplitude Adjustment Capability
- Two High Drive Outputs With a Typical Range from -8.0 to -2.0 dBm

The device has two high frequency outputs which make it attractive for transceiver applications which require both a transmit and receive local oscillator (LO) signal. The outputs Q and QB are available for servicing the receiver IF and transmitter up-converter single-ended. In receiver applications, the outputs can be used together if it is necessary to generate a differential signal for the receiver IF. Because the Q and QB outputs are open collector, terminations to the V_{CC} supply are required for proper operation. Since the outputs are complementary, BOTH outputs must be terminated even if only one is needed. The Q and QB outputs have a nominal drive level of -8dBm to conserve power. If addition signal amplitude is needed, a level adjustment pin (CNTL) is available, which when tied to ground, boosts the nominal output levels to -2.0 dBm.

External components required for the MC12147 are: (1) tank circuit (LC network); (2) Inductor/capacitor to provide the termination for the open collector outputs; and (3) adequate supply voltage bypassing. The tank circuit consists of a high-Q inductor and varactor components. The preferred tank configuration allows the user to tune the VCO across the full supply range. VCO performance such as center frequency, tuning voltage sensitivity, and noise characteristics are dependent on the particular components and configuration of the VCO tank circuit.

PIN NAMES

Pin	Function
V _{CC}	Power Supply
CNTL	Amplitude Control for Q, QB Output Pair
TANK	Tank Circuit Input
V _{REF}	Bias Voltage Output
QB	Open Collector Output
GND	Ground
Q	Open Collector Output

MC12147

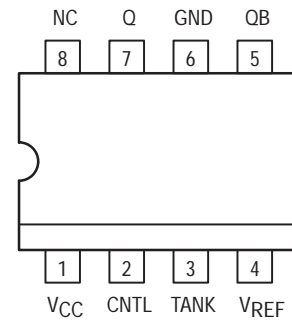
LOW POWER VOLTAGE CONTROLLED OSCILLATOR BUFFER

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)

PIN CONNECTIONS



(Top View)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12147D	T _A = -40 to 85°C	SO-8

MC12147

MAXIMUM RATINGS (Note 1)

Parameter	Symbol	Value	Unit
Power Supply Voltage, Pin 1	V_{CC}	-0.5 to +7.0	V
Operating Temperature Range	T_A	-40 to +85	°C
Storage Temperature Range	T_{STG}	-65 to +150	°C
Maximum Output Current, Pin 5,7	I_O	12	mA

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the Recommended Operating Conditions.
2. ESD data available upon request.

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ to 5.5 VDC, $T_A = -40$ to 85°C , unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current (CNTL=GND) $V_{CC} = 3.3$ V $V_{CC} = 5.5$ V	I_{CC}	–	14.0 23.5	18 28	mA
Supply Current (CNTL=OPEN) $V_{CC} = 3.3$ V $V_{CC} = 5.5$ V	I_{CC}	–	8 13	13.0 22.5	mA
Output Amplitude (Pin 5 & 7) [Note 1] 50Ω to V_{CC} $V_{CC} = 2.7$ V $V_{CC} = 2.7$ V	V_{OH} , V_{OL}	2.6 2.1	2.7 2.3	– 2.4	V
Output Amplitude (Pin 5 & 7) [Note 1] 50Ω to V_{CC} $V_{CC} = 5.5$ V $V_{CC} = 5.5$ V	V_{OH} , V_{OL}	5.4 4.8	5.5 5.0	– 5.1	V
Tuning Voltage Sensitivity [Notes 2 and 3]	T_{stg}	–	20	–	MHz/V
Frequency of Operation	F_C	100	–	1300	MHz
CSR at 10 kHz Offset, 1.0 Hz BW [Notes 2 and 3]	$\mathcal{L}(f)$	–	–85	–	dBc/Hz
CSR at 100 kHz Offset, 1.0 Hz BW [Notes 2 and 3]	$\mathcal{L}(f)$	–	–105	–	dBc/Hz
Frequency Stability [Notes 2 and 3] Supply Drift Thermal Drift	F_{sts} f_{stt}	– –	0.8 50	– –	MHz/V kHz/°C

- NOTES:** 1. CNTL pin tied to ground.
2. Actual performance depends on tank components selected.
3. See Figure 12, 750 MHz tank.
4. $T = 25^\circ\text{C}$, $V_{CC} = 5.0$ V $\pm 10\%$

MC12147

OPERATIONAL CHARACTERISTICS

A simplified schematic of the MC12147 is found in Figure 1. The oscillator incorporates positive feedback by coupling the base of transistor Q2 to the collector of transistor Q1. In order to minimize interaction between the VCO outputs and the oscillator tank transistor pair, a buffer is incorporated into the circuit. This differential buffer is realized by the Q3 and Q4 transistor pair. The differential buffer drives the gate which contains the primary open collector outputs, Q and QB. The output is actually a current which has been set by an internal bias driver to a nominal current of 4mA. Additional circuitry is incorporated into the tail of the current source which allows the current source to be increased to approximately 10mA. This is accommodated by the addition of a resistor which is brought out to the CNTL pin. When this pin is tied to ground, the additional current is sourced through the current source thus increasing the output amplitude of the Q/QB output pair. If less than 10 mA of current is needed, a resistor can be added to ground which reduces the amount of current.

APPLICATION INFORMATION

Figure 2 illustrates the external components necessary for the proper operation of the VCO buffer. The tank circuit configuration in this figure allows the VCO to be tuned across the full operating voltage of the power supply. This is very important in 3V applications where it is desirable to utilize as much of the operating supply range as possible so as to minimize the VCO sensitivity (MHz/V). In most situations, it is desirable to keep the sensitivity low so the circuit will be less susceptible to external noise influences. An additional benefit to this configuration is that additional regulation/ filtering can

be incorporated into the V_{CC} line without compromising the tuning range of the VCO. With the AC-coupled tank configuration, the V_{tune} voltage can be greater than the V_{CC} voltage supplied to the device.

There are four main areas that the user directly influences the performance of the VCO. These include Tank Design, Output Termination Selection, Power Supply Decoupling, and Circuit Board Layout/Grounding.

The design of the tank circuit is critical to the proper operation of the VCO. This tank circuit directly impacts the main VCO operating characteristics:

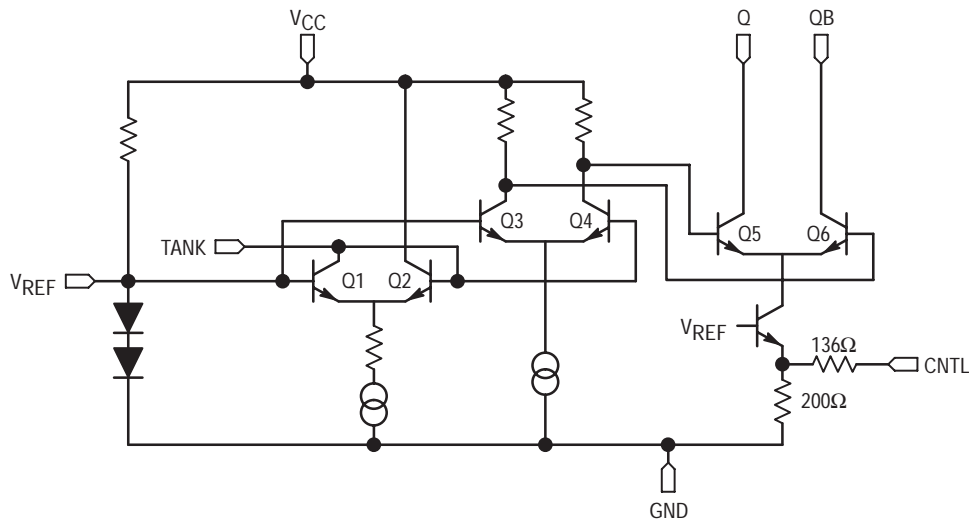
- 1) Frequency of Operation
- 2) Tuning Sensitivity
- 3) Voltage Supply Pushing
- 4) Phase Noise Performance

The tank circuit, in its simplest form, is realized as an LC circuit which determines the VCO operating frequency. This is described in Equation 1.

$$f_0 = \frac{1}{2\pi \sqrt{LC}} \quad \text{Equation 1}$$

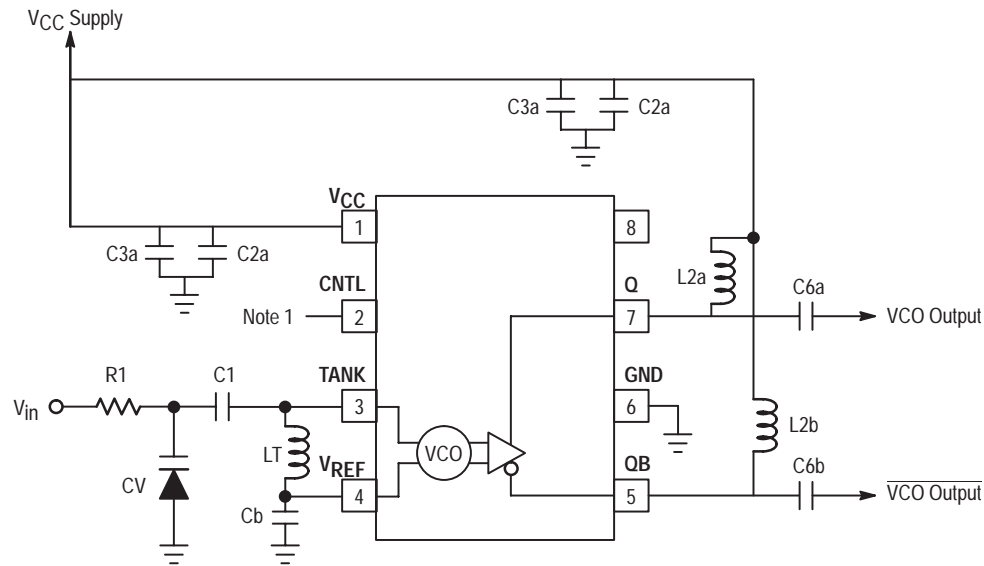
In the practical case, the capacitor is replaced with a varactor diode whose capacitance changes with the voltage applied, thus changing the resonant frequency at which the VCO tank operates. The capacitive component in Equation 1 also needs to include the input capacitance of the device and other circuit and parasitic elements. Typically, the inductor is realized as a surface mount chip or a wound-coil. In addition, the lead inductance and board inductance and capacitance also have an impact on the final operating point.

Figure 1. Simplified Schematic



MC12147

Figure 2. MC12147 Typical External Component Connections



1. This input can be left open, tied to ground, or tied with a resistor to ground, depending on the desired output amplitude needed at the Q and QB output pair.
2. Typical values for R1 range from 5.0 kΩ to 10 kΩ.

A simplified linear approximation of the device, package, and typical board parasitics has been developed to aid the designer in selecting the proper tank circuit values. All the parasitic contributions have been lumped into a parasitic capacitive component and a parasitic inductive component. While this is not entirely accurate, it gives the designer a solid starting point for selecting the tank components.

Below are the parameters used in the model.

- Cp Parasitic Capacitance
- Lp Parasitic Inductance
- LT Inductance of Coil
- C1 Coupling Capacitor Value
- Cb Capacitor for decoupling the Bias Pin
- CV Varactor Diode Capacitance (Variable)

The values for these components are substituted into the following equations:

$$C_i = \frac{C_1 \times CV}{C_1 + CV} + C_p \quad \text{Equation 2}$$

$$C = \frac{C_i \times C_b}{C_i + C_b} \quad \text{Equation 3}$$

$$L = L_p + LT \quad \text{Equation 4}$$

From Figure 2, it can be seen that the varactor capacitance (CV) is in series with the coupling capacitor (C1). This is calculated in Equation 2. For analysis purposes, the parasitic capacitances (CP) are treated as a lumped element and placed in parallel with the series combination of C1 and CV. This compound capacitance (Ci) is in series with the bias capacitor (Cb) which is calculated in Equation 3. The influences of the various capacitances; C1, CP, and Cb, impact the design by reducing the variable capacitance effects of the varactor which controls the tank resonant frequency and tuning range.

Now the results calculated from Equation 2, Equation 3 and Equation 4 can be substituted into Equation 1 to calculate the actual frequency of the tank.

To aid in analysis, it is recommended that the designer use a simple spreadsheet based on Equation 1 through Equation 4 to calculate the frequency of operation for various varactor/inductor selections before determining the initial starting condition for the tank.

The two main components at the heart of the tank are the inductor (LT) and the varactor diode (CV). The capacitance of a varactor diode junction changes with the amount of reverse bias voltage applied across the two terminals. This is the element which actually “tunes” the VCO. One characteristic of the varactor is the tuning ratio which is the ratio of the capacitance at specified minimum and maximum voltage points. For characterizing the MC12147, a Matsushita (Panasonic) varactor – MA393 was selected. This device has a typical capacitance of 11 pF at 1V and 3.7 pF at 4V and the C–V characteristic is fairly linear over that range. Similar performance was also achieved with Loral varactors. A multi-layer chip inductor was used to realize the LT component. These inductors had typical Q values in the 35–50 range for frequencies between 500 and 1000MHz.

Note: There are many suppliers of high performance varactors and inductors an Motorola can not recommend one vendor over another.

The Q (quality factor) of the components in the tank circuit has a direct impact on the resulting phase noise of the oscillator. In general, the higher the Q, the lower the phase noise of the resulting oscillator. In addition to the LT and CV components, only high quality surface-mount RF chip capacitors should be used in the tank circuit. These capacitors should have very low dielectric loss (high-Q). At a minimum, the capacitors selected should be operating 100 MHz below their series resonance point. As the desired frequency of operation increases, the values of the C1 and Cb capacitors will decrease since the series resonance point

MC12147

is a function of the capacitance value. To simplify the selection of C1 and Cb, a table has been constructed based on the intended operating frequency to provide recommended starting points. These may need to be altered depending on the value of the varactor selected.

Frequency	C1	Cb
200 – 500 MHz	47 pF	47 pF
500 – 900 MHz	5.1 pF	15 pF
900 – 1200 MHz	2.7 pF	15 pF

The value of the Cb capacitor influences the VCO supply pushing. To minimize pushing, the Cb capacitor should be kept small. Since C1 is in series with the varactor, there is a strong relationship between these two components which influences the VCO sensitivity. Increasing the value of C1 tends to increase the sensitivity of the VCO.

The parasitic contributions Lp and Cp are related to the MC12147 as well as parasitics associated with the layout, tank components, and board material selected. The input capacitance of the device, bond pad, the wire bond, package/lead capacitance, wire bond inductance, lead inductance, printed circuit board layout, board dielectric, and proximity to the ground plane all have an impact on these parasitics. For example, if the ground plane is located directly below the tank components, a parasitic capacitor will be formed consisting of the solder pad, metal traces, board dielectric material, and the ground plane. The test fixture used for characterizing the device consisted of a two sided copper clad board with ground plane on the back. Nominal values were determined by selecting a varactor and characterizing the device with a number of different tank/frequency combinations and then performing a curve fit with the data to determine values for Lp and Cp. The nominal values for the parasitic effects are seen below:

Parasitic Capacitance	Cp	4.2 pF
Parasitic Inductance	Lp	2.2 nH

These values will vary based on the users unique circuit board configuration.

Basic Guidelines:

1. Select a varactor with high Q and a reasonable capacitance versus voltage slope for the desired frequency range.
2. Select the value of Cb and C1 from the table above .
3. Calculate a value of inductance (L) which will result in achieving the desired center frequency. Note that L includes both LT and Lp.
4. Adjust the value of C1 to achieve the proper VCO sensitivity.
5. Re-adjust value of L to center VCO.
6. Prototype VCO design using selected components. It is important to use similar construction techniques and materials, board thickness, layout, ground plane spacing as intended for the final product.
7. Characterize tuning curve over the voltage operation conditions.
8. Adjust, as necessary, component values – L,C1, and Cb to compensate for parasitic board effects.
9. Evaluate over temperature and voltage limits.

10. Perform worst case analysis of tank component variation to insure proper VCO operation over full temperature and voltage range and make any adjustments as needed.

Outputs Q and QB are open collector outputs and need a inductor to VCC to provide the voltage bias to the output transistor. In most applications, dc-blocking capacitors are placed in series with the output to remove the dc component before interfacing to other circuitry. These outputs are complementary and should have identical inductor values for each output. This will minimize switching noise on the VCC supply caused by the outputs switching. It is important that both outputs be terminated, even if only one of the outputs is used in the application.

Referring to Figure 2, the recommended value for L2a and L2b should be 47 nH and the inductor components resonance should be at least 300 MHz greater than the maximum operating frequency. For operation above 1100 MHz, it may be necessary to reduce that inductor value to 33 nH. The recommended value for the coupling capacitors C6a, C6b, and C7 is 47 pF. Figure 2 also includes decoupling capacitors for the supply line as well as decoupling for the output inductors. Good RF decoupling practices should be used with a series of capacitors starting with high quality 100 pF chip capacitors close to the device. A typical layout is shown below in Figure 3.

The output amplitude of the Q and QB can be adjusted using the CNTL pin. Referring to Figure 1, if the CNTL pin is connected to ground, additional current will flow through the current source. When the pin is left open, the nominal current flowing through the outputs is 4 mA. When the pin is grounded, the current increases to a nominal value of 10 mA. So if a 50 ohm resistor was connected between the outputs and VCC, the output amplitude would change from 200 mV pp to 500 mV pp with an additional current drain for the device of 6 mA. To select a value between 4 and 10 mA, an external resistor can be added to ground. The equation below is used to calculate the current.

$$I_{out(nom)} = \frac{(200 + 136 + R_{ext}) \times 0.8V}{200 \times (136 + R_{ext})}$$

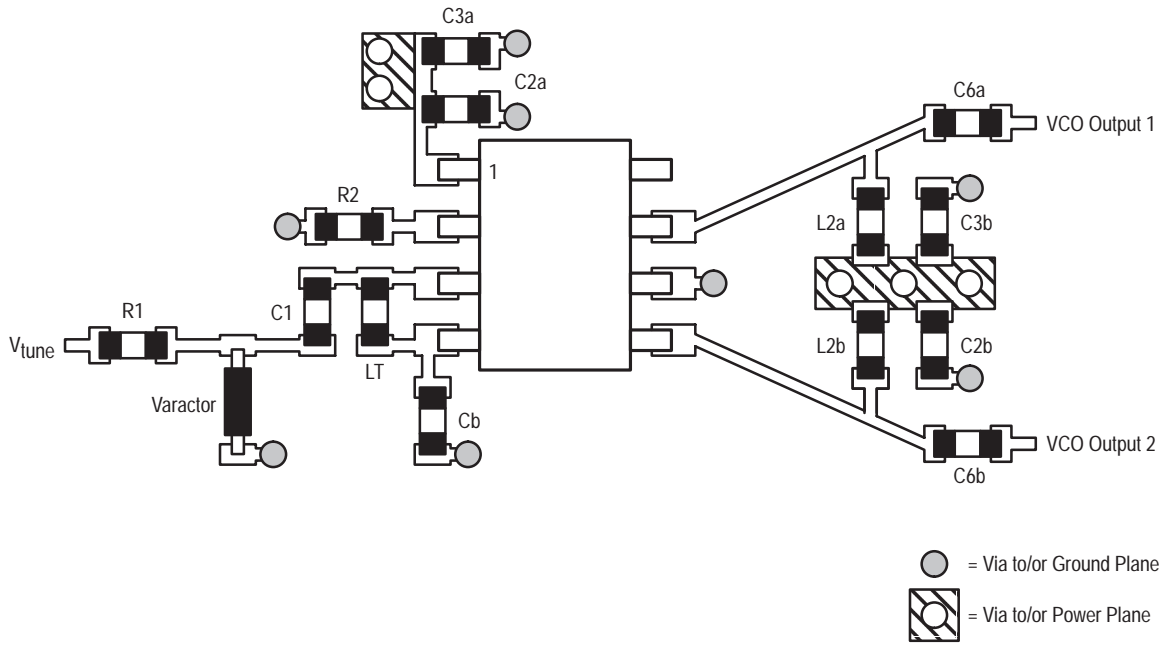
Figure 4 through Figure 13 illustrate typical performance achieved with the MC12147. The curves illustrate the tuning curve, supply pushing characteristics, output power, current drain, output spectrum, and phase noise performance. In most cases, data is present for both a 750 MHz and 1200 MHz tank design. The table below illustrates the component values used in the designs.

Component	750MHz Tank	1200MHz Tank	Units
R1	5000	5000	Ω
C1	5.1	2.7	pF
LT	4.7	1.8	nH
CV	3.7 @ 1.0 V 11 @ 4.0 V	3.7 @ 1.0 V 11 @ 4.0 V	pF
Cb	100*	15	pF
C6, C7	47	33	pF
L2	47	47	nH

* The value of Cb should be reduced to minimize pushing.

MC12147

Figure 3. MC12147 Typical Layout
(Not to Scale)



MC12147

Figure 4. Typical VCO Tuning Curve, 750 MHz Tank

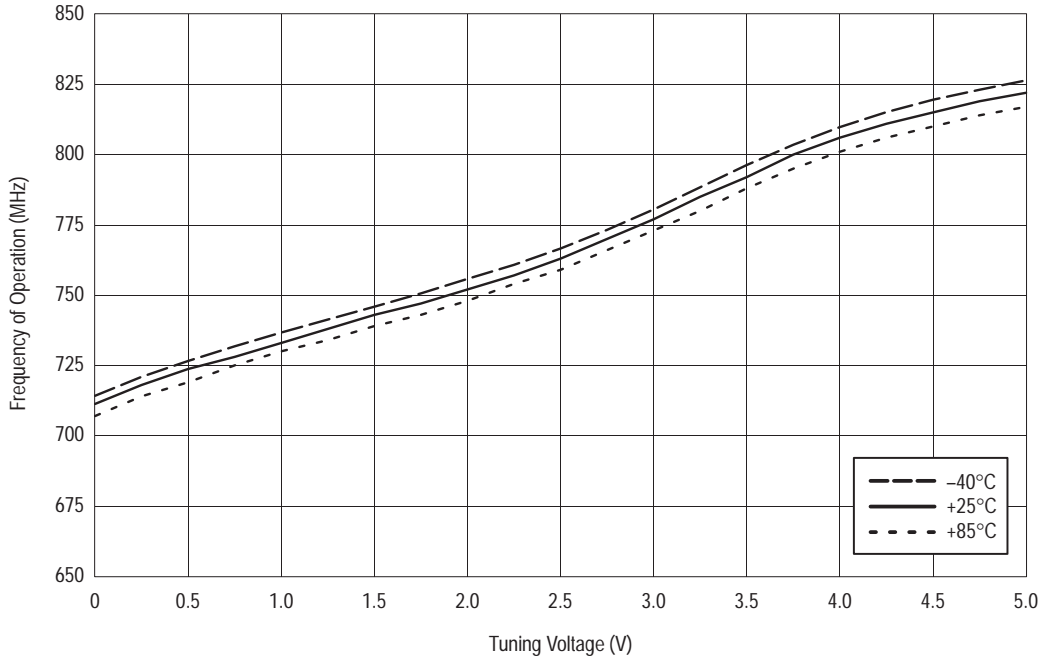
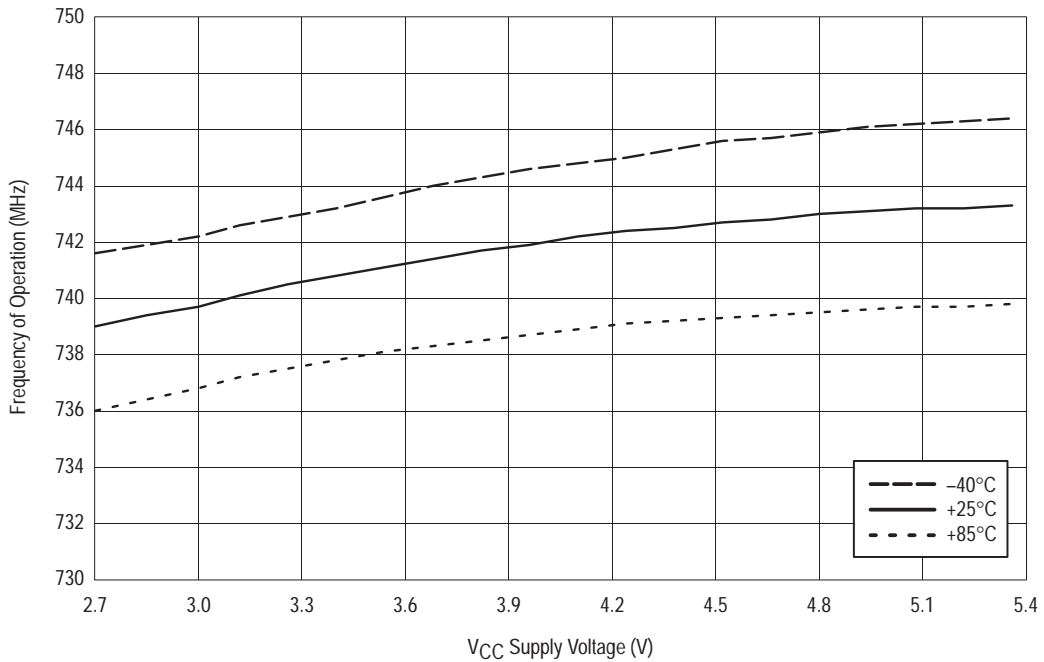


Figure 5. Typical Supply Pushing, 750MHz Tank



MC12147

Figure 6. Typical Q/QB Output Power versus Supply, 750 MHz Tank

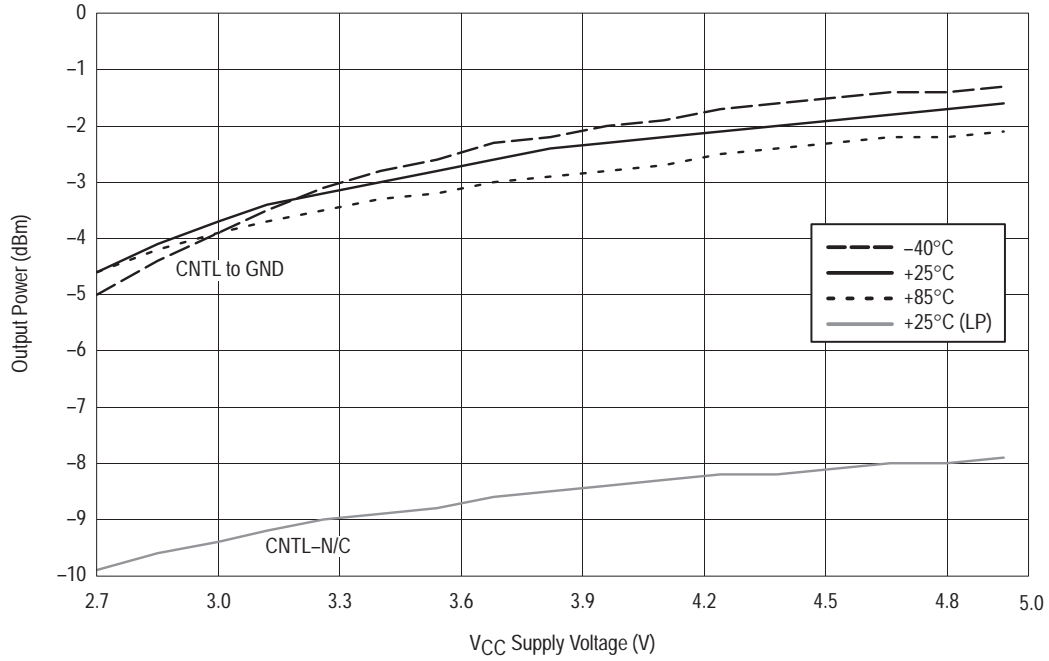
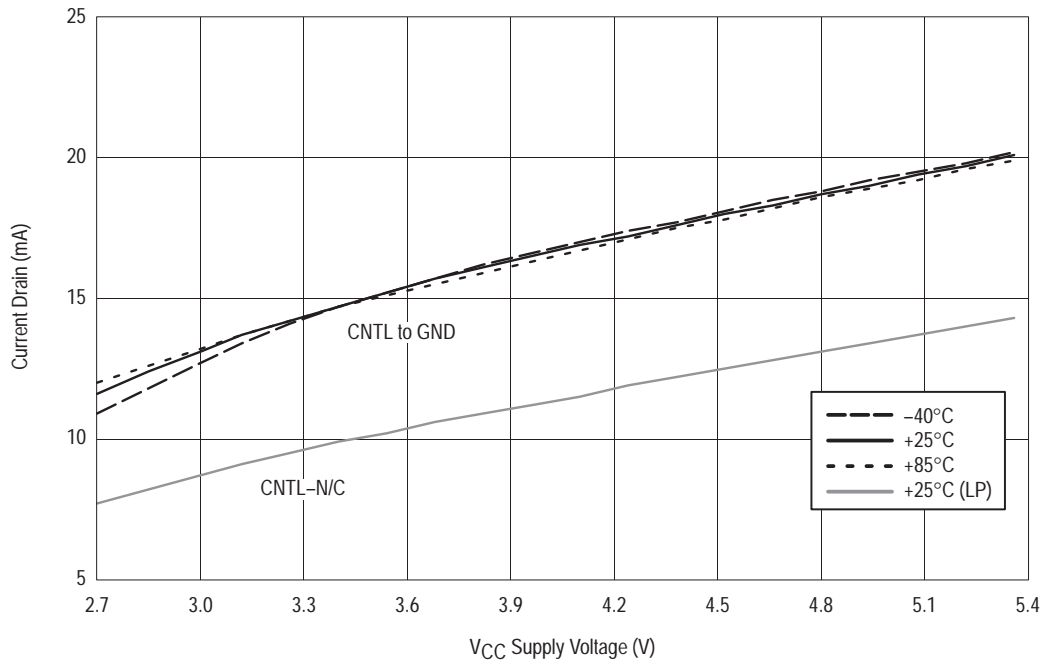


Figure 7. Typical Current Drain versus Supply, 750 MHz Tank



MC12147

Figure 8. Typical VCO Tuning Curve, 1200 MHz Tank
($V_{CC} = 5.0\text{ V}$)

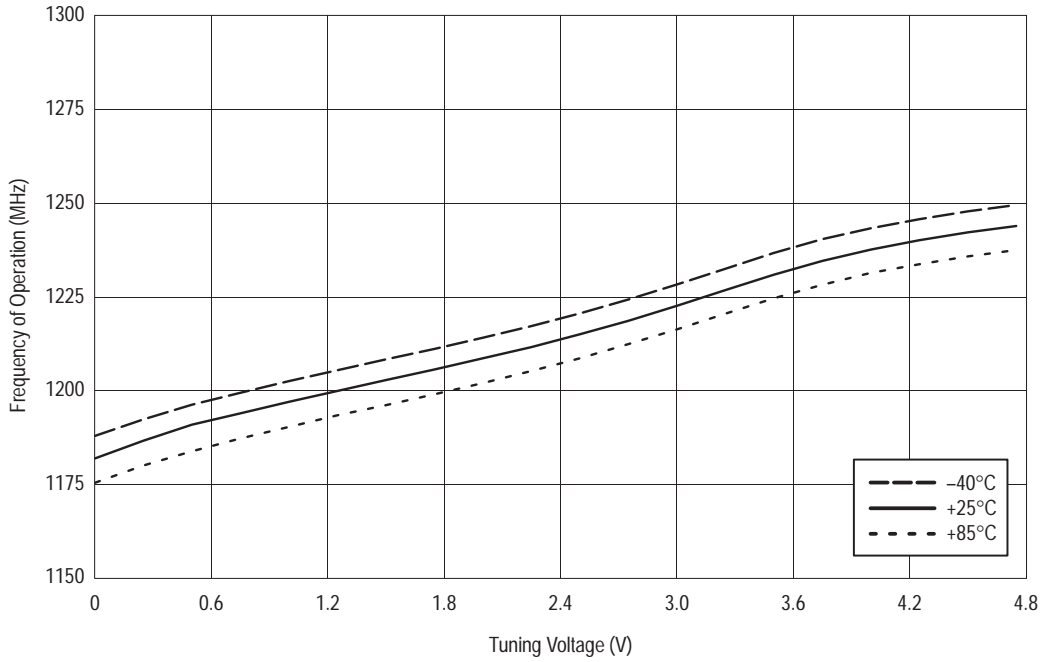
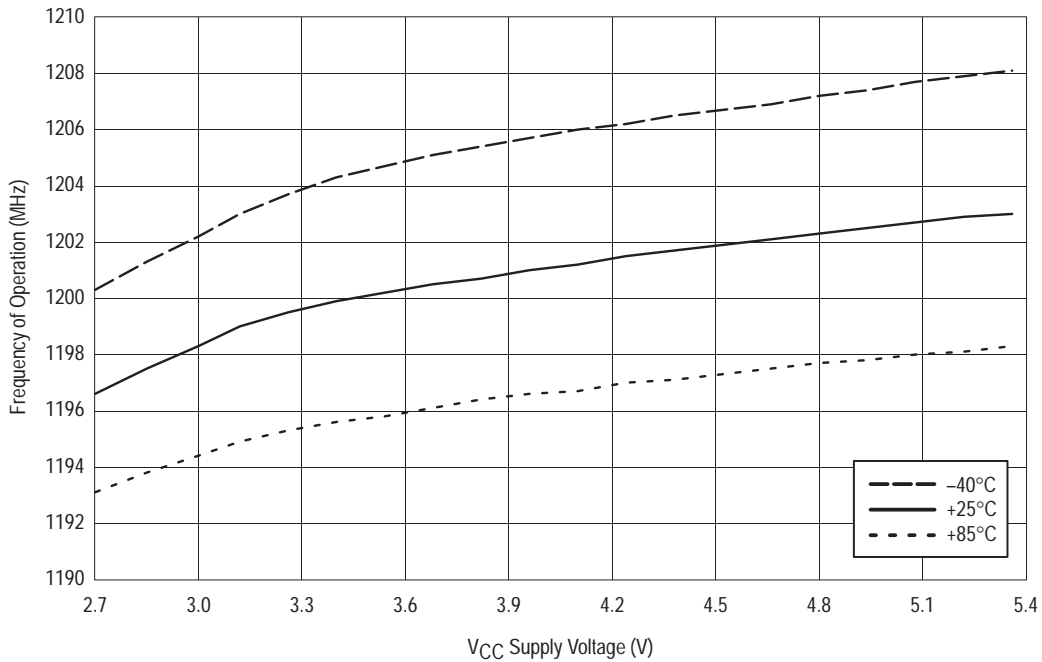


Figure 9. Typical Supply Pushing, 1200 MHz Tank



MC12147

Figure 10. Q/QB Output Power versus Supply, 1200 MHz Tank

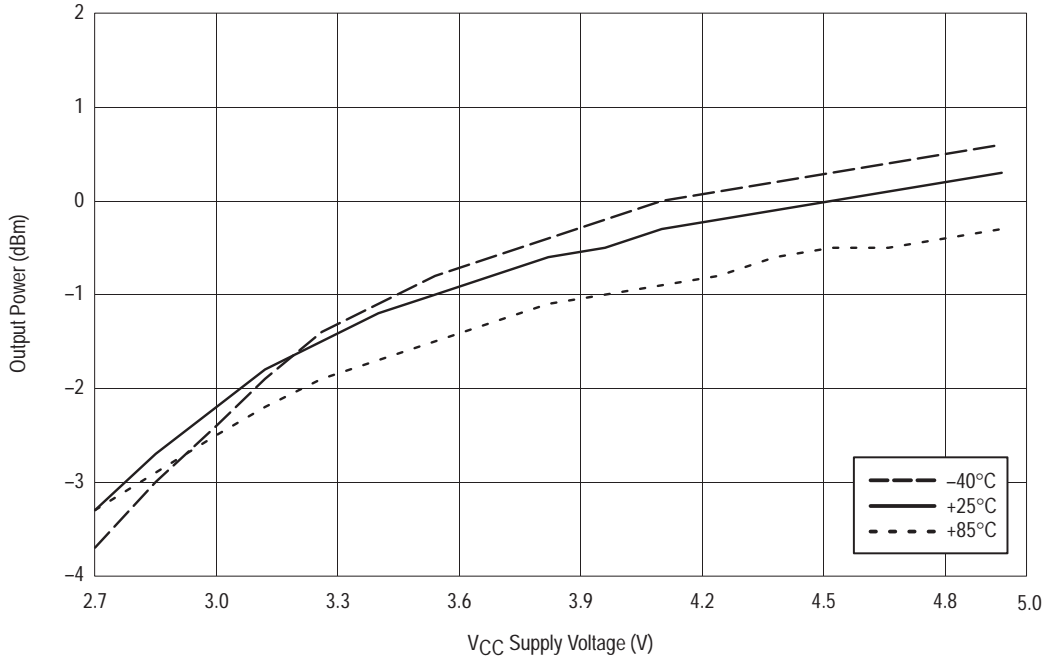


Figure 11. Typical VCO Output Spectrum

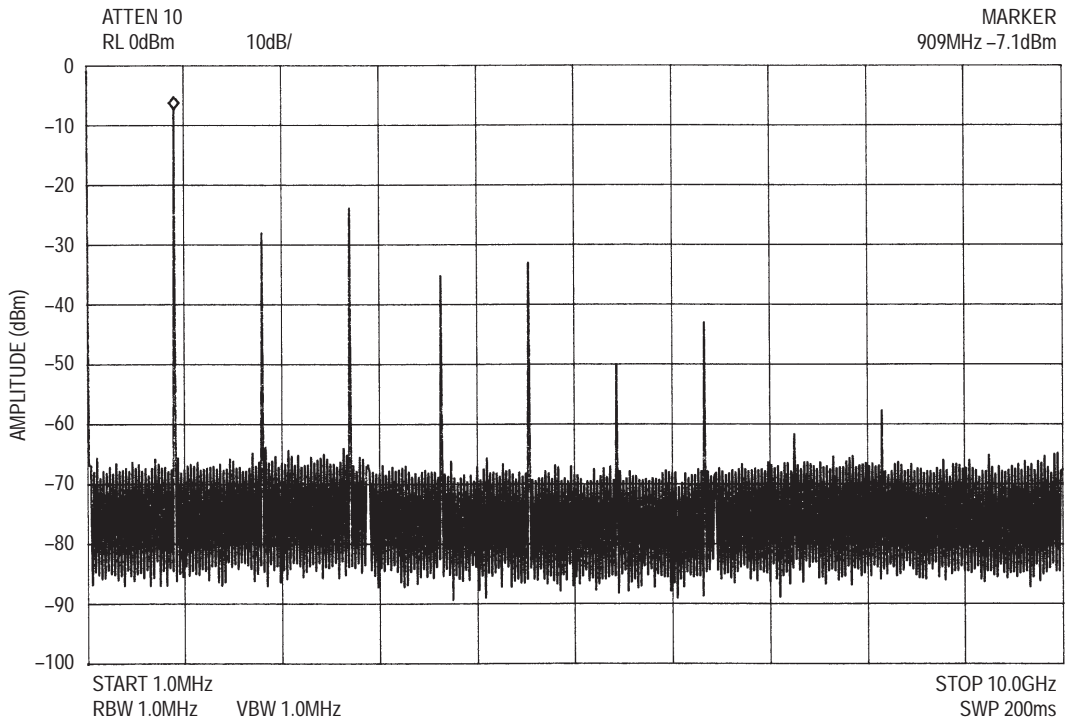


Figure 12. Typical Phase Noise Plot, 750 MHz Tank

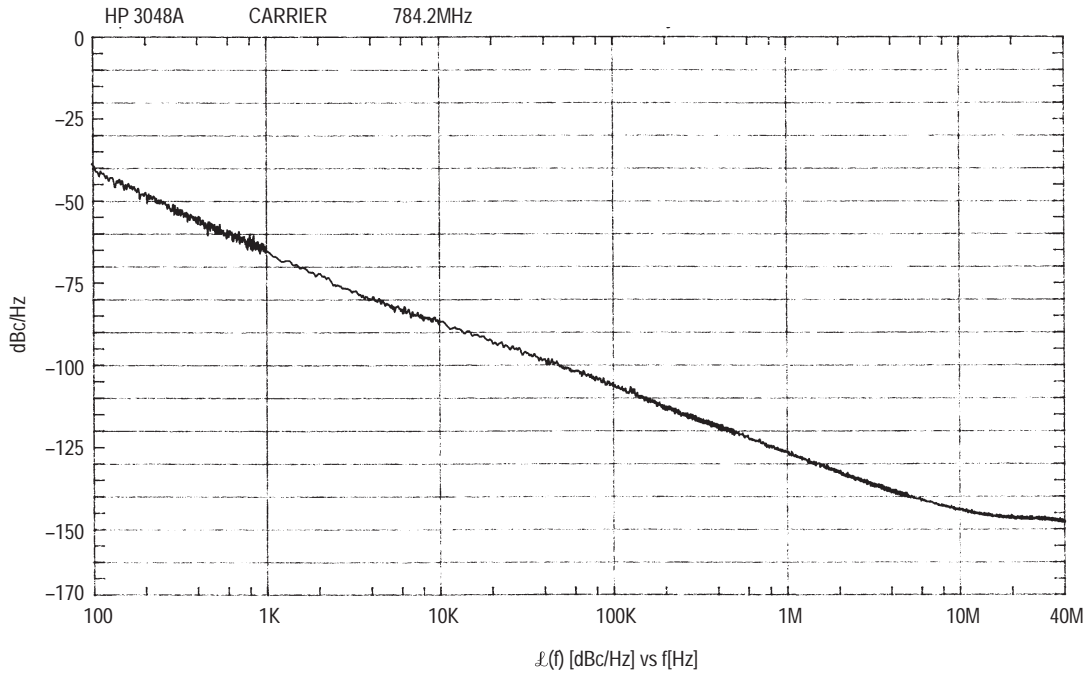
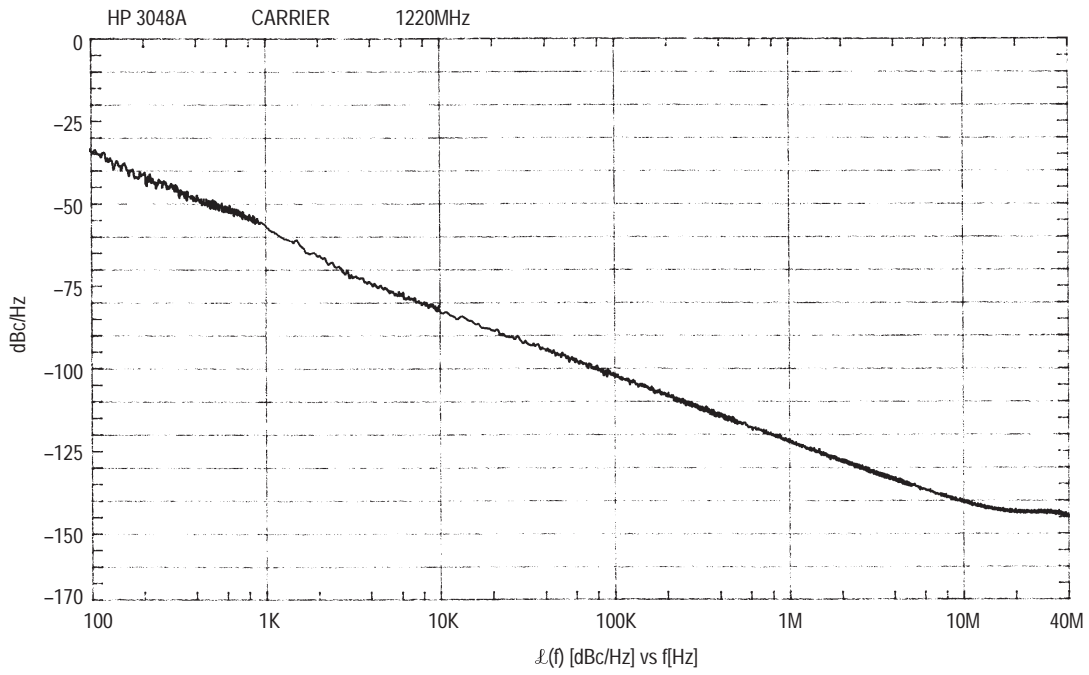


Figure 13. Typical Phase Noise Plot, 1200 MHz Tank



Low Power Voltage Controlled Oscillator

The MC12148 requires an external parallel tank circuit consisting of the inductor (L) and capacitor (C). A varactor diode may be incorporated into the tank circuit to provide a voltage variable input for the oscillator (VCO). This device may also be used in many other applications requiring a fixed frequency clock.

The MC12148 is ideal in applications requiring a local oscillator. Systems include electronic test equipment and digital high-speed telecommunications.

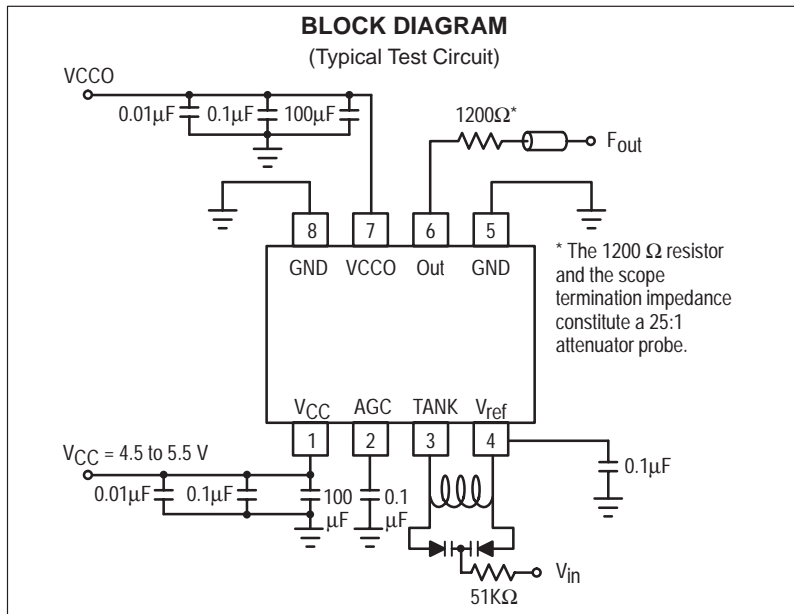
The MC12148 is based on the VCO circuit topology of the MC1648. The MC12148 has been realized utilizing Motorola's MOSAIC III advanced bipolar process technology which results in a design which can operate at a much higher frequency than the MC1648 while utilizing half the current. Please consult with the MC1648 data sheet for additional background information.

The ECL output circuitry of the MC12148 is not a traditional open emitter output structure and instead has an on-chip termination resistor with a nominal value of 500 ohms. This facilitates direct ac-coupling of the output signal into a transmission line. Because of this output configuration, an external pull-down resistor is not required to provide the output with a dc current path. This output is intended to drive one ECL load. If the user needs to fanout the signal, an ECL buffer such as the MC10EL16 Line Receiver/Driver should be used.

NOTE: The MC12148 is NOT useable as a crystal oscillator.

- Typical Operating Frequency Up to 1100 MHz
- Low-Power 20 mA at 5.0 Vdc Power Supply
- 8-Pin SOIC Package
- Phase Noise -90 dBc/Hz at 25 kHz Typical

NOT RECOMMENDED FOR NEW DESIGN
DEVICE TO BE PHASED OUT.
Consider MC12149 for New Designs.



MC12148

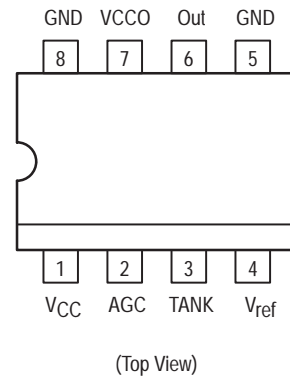
LOW POWER VOLTAGE CONTROLLED OSCILLATOR

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)

PIN CONNECTIONS



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12148D	T _A = -40 to 85°C	SO-8

MC12148

MAXIMUM RATINGS

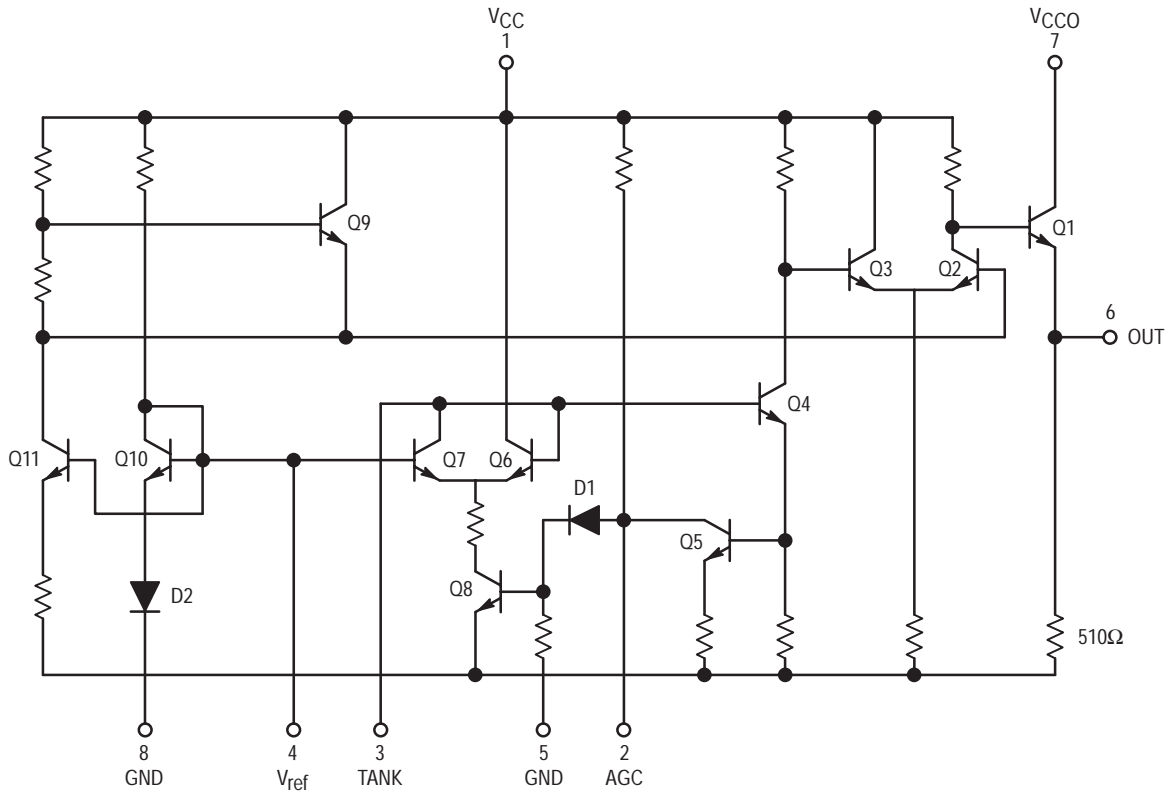
Parameter	Symbol	Value	Unit
Power Supply Voltage, Pins 1, 7	V_{CC}	-0.5 to 7.0	Vdc
Operating Temperature Range	T_A	-40 to 85	°C
Storage Temperature Range	T_{stg}	-65 to 150	°C

NOTE: ESD data available upon request.

ELECTRICAL CHARACTERISTICS ($V_{CC} = 5.0\text{ V}$; $T_A = -40\text{ to }85^\circ\text{C}$, unless otherwise noted.)

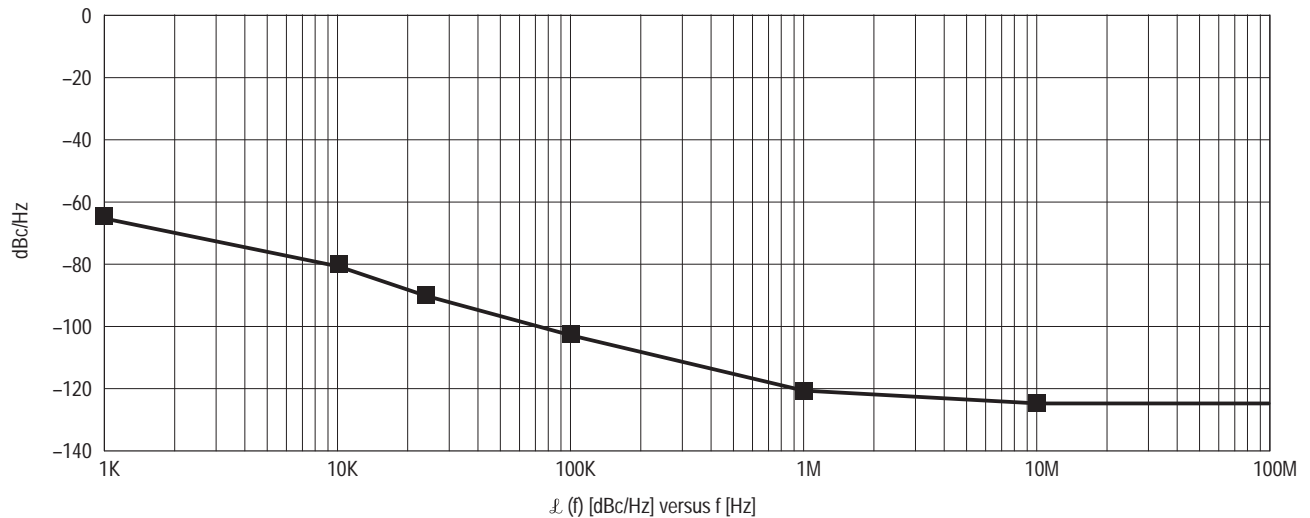
Characteristic	Symbol	Min	Typ	Max	Unit	
Supply Current	I_{CC}	-	19	25	mA	
Output Level HIGH (1.0 M Ω Impedance)	V_{OH}	3.95	4.17	4.61	V	
Output Level LOW (1.0 M Ω Impedance)	V_{OL}	3.04	3.41	3.60	V	
CSR @ 25 kHz Offset, 1.0 Hz BW	$\mathcal{L}(f)$	-	-90	-	dBc/Hz	
CSR @ 1.0 MHz Offset, 1.0 Hz BW	$\mathcal{L}(f)$	-	-120	-	dBc/Hz	
SNR (Signal to Noise Ratio from Carrier)	SNR	-	40	-	dB	
Frequency Stability	Supply Drift	Fsts	-	3.6	-	KHz/mV
	Thermal Drift	Fstt	-	0.1	-	KHz/°C
Second Harmonic (from Carrier)	H2	-	-25	-	dBc	

Figure 1. Circuit Schematic



MC12148

Figure 2. Typical Evaluation Results
(CSR MC12148 5.0 Vdc; V_{CC} @ 25°C; 930 MHz CW)



Tank Component Suppliers

Below are suppliers who manufacture tuning varactors and inductors which can be used to build an external tank circuit. Motorola has used these varactors and inductors for evaluation purposes, however, there are other vendors who manufacture similar products.

Coilcraft Inductors A01T thru A05T

Coilcraft—Coilcraft, Inc.
1102 Silver Lake Rd.
Gary, Illinois 60013
708-639-6400

Alpha Tuning Diodes DVH6730 Series

Alpha Semiconductor Devices Division
20 Sylvan Road
Woburn, MA 01801
617-935-5150

Loral Tuning Varactors GC1500 Series

Loral
16 Maple Road
Chelmsford, Massachusetts 01824
508-256-8101 or 508-256-4113

* At 1.1 GHz, use a Coilcraft A01T Springair coil at 2.5 nH and a Loral Varactor 3.0 to 8.0 pF at V_{IN} = 1.0 to 5.0 V.



MOTOROLA

Low Power Voltage Controlled Oscillator Buffer

The MC12149 is intended for applications requiring high frequency signal generation up to 1300 MHz. An external tank circuit is used to determine the desired frequency of operation. The VCO is realized using an emitter-coupled pair topology. The MC12149 can be used with an integrated PLL IC such as the MC12202 1.1 GHz Frequency Synthesizer to realize a complete PLL sub-system. The device is specified to operate over a voltage supply range of 2.7 to 5.5 V. It has a typical current consumption of 15 mA at 3.0 V which makes it attractive for battery operated handheld systems.

NOTE: The MC12149 is NOT suitable as a crystal oscillator.

- Operates Up to 1.3 GHz
- Space-Efficient 8-Pin SOIC or SSOP Package
- Low Power 15 mA Typical @ 3.0 V Operation
- Supply Voltage of 2.7 to 5.5 V
- Typical 900 MHz Performance
 - Phase Noise -105 dBc/Hz @ 100 kHz Offset
 - Tuning Voltage Sensitivity of 20 MHz/V
- Output Amplitude Adjustment Capability
- Two High Drive Outputs With a Typical Range from -8.0 to -2.0 dBm
- One Low-Drive Output for Interfacing to a Prescaler

The device has three high frequency outputs which make it attractive for transceiver applications which require both a transmit and receive local oscillator (LO) signal as well as a lower amplitude signal to drive the prescaler input of the frequency synthesizer. The outputs Q and QB are available for servicing the receiver IF and transmitter up-converter single-ended. In receiver applications, the outputs can be used together if it is necessary to generate a differential signal for the receiver IF. Because the Q and QB outputs are open collector, terminations to the V_{CC} supply are required for proper operation. Since the outputs are complementary, BOTH outputs must be terminated even if only one is needed. The Q and QB outputs have a nominal drive level of -8dBm to conserve power. If addition signal amplitude is needed, a level adjustment pin (CNTL) is available, which when tied to ground, boosts the nominal output levels to -2.0 dBm. A low power VCO output (Q2) is also provided to drive the prescaler input of the PLL. The amplitude of this signal is nominally 500 mV which is suitable for most prescalers.

External components required for the MC12149 are: (1) tank circuit (LC network); (2) Inductor/capacitor to provide the termination for the open collector outputs; and (3) adequate supply voltage bypassing. The tank circuit consists of a high-Q inductor and varactor components. The preferred tank configuration allows the user to tune the VCO across the full supply range. VCO performance such as center frequency, tuning voltage sensitivity, and noise characteristics are dependent on the particular components and configuration of the VCO tank circuit.

MC12149

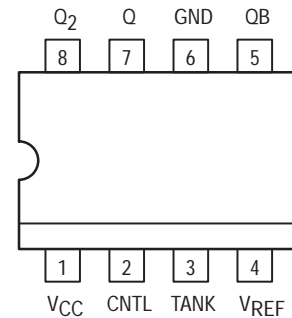
LOW POWER VOLTAGE CONTROLLED OSCILLATOR BUFFER

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)

PIN CONNECTIONS



(Top View)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12149D	T _A = -40 to 85°C	SO-8

MC12149

PIN NAMES

Pin	Function
V _{CC}	Power Supply
CNTL	Amplitude Control for Q, QB Output Pair
TANK	Tank Circuit Input
V _{REF}	Bias Voltage Output
QB	Open Collector Output
GND	Ground
Q	Open Collector Output
Q ₂	Low Power Output

MAXIMUM RATINGS (Note 1)

Parameter	Symbol	Value	Unit
Power Supply Voltage, Pin 1	V _{CC}	-0.5 to 7.0	V
Operating Temperature Range	T _A	-40 to 85	°C
Storage Temperature Range	T _{STG}	-65 to 150	°C
Maximum Output Current, Pin 8	I _O	7.5	mA
Maximum Output Current, Pin 5,7	I _O	12	mA

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the Recommended Operating Conditions.
2. ESD data available upon request.

ELECTRICAL CHARACTERISTICS (V_{CC} = 2.7 to 5.5 VDC, T_A = -40 to 85°C, unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current (CNTL=GND) V _{CC} = 3.3 V V _{CC} = 5.5 V	I _{CC}	–	16 23.5	20 30	mA
Supply Current (CNTL=OPEN) V _{CC} = 3.3 V V _{CC} = 5.5 V	I _{CC}	–	10 15	15.0 24.5	mA
Output Amplitude (Pin 8) V _{CC} = 2.7 V High Impedance Load V _{CC} = 2.7 V	V _{OH} , V _{OL}	1.75 1.20	1.85 1.35	1.95 1.50	V
Output Amplitude (Pin 8) V _{CC} = 5.5 V High Impedance Load V _{CC} = 5.5 V	V _{OH} , V _{OL}	4.50 3.85	4.6 4.0	4.70 4.15	V
Output Amplitude (Pin 5 & 7) [Note 1] V _{CC} = 2.7 V 50 Ω to V _{CC} V _{CC} = 2.7 V	V _{OH} , V _{OL}	2.6 2.1	2.7 2.3	– 2.4	V
Output Amplitude (Pin 5 & 7) [Note 1] V _{CC} = 5.5 V 50 Ω to V _{CC} V _{CC} = 5.5 V	V _{OH} , V _{OL}	5.4 4.8	5.5 5.0	– 5.1	V
Tuning Voltage Sensitivity [Notes 2 and 3]	T _{stg}	–	20	–	MHz/V
Frequency of Operation	F _C	100	–	1300	MHz
CSR at 10 kHz Offset, 1Hz BW [Notes 2 and 3]	L(f)	–	–85	–	dBc/Hz
CSR at 100 kHz Offset, 1Hz BW [Notes 2 and 3]	L(f)	–	–105	–	dBc/Hz
Frequency Stability [Notes 3 and 4] Supply Drift Thermal Drift	F _{sts} f _{stt}	– –	0.8 50	– –	MHz/V KHz/°C

- NOTES:** 1. CNTL pin tied to ground.
2. Actual performance depends on tank components selected.
3. See Figure 12, 750 MHz tank.
4. T = 25°C, V_{CC} = 5.0 V ±10%

MC12149

OPERATIONAL CHARACTERISTICS

A simplified schematic of the MC12149 is found in Figure 1. The oscillator incorporates positive feedback by coupling the base of transistor Q2 to the collector of transistor Q1. In order to minimize interaction between the VCO outputs and the oscillator tank transistor pair, a buffer is incorporated into the circuit. This differential buffer is realized by the Q3 and Q4 transistor pair. The differential buffer drives the gate which contains the primary open collector outputs, Q and QB. The output is actually a current which has been set by an internal bias driver to a nominal current of 4mA. Additional circuitry is incorporated into the tail of the current source which allows the current source to be increased to approximately 10 mA. This is accommodated by the addition of a resistor which is brought out to the CNTL pin. When this pin is tied to ground, the additional current is sourced through the current source thus increasing the output amplitude of the Q/QB output pair. If less than 10mA of current is needed, a resistor can be added to ground which reduces the amount of current.

The Q/QB outputs drive an additional differential buffer which generate the Q2 output signal. To minimize current, the circuit is realized as an emitter-follower buffer with an on chip pull down resistor. This output is intended to drive the prescaler input of the PLL synthesizer block.

APPLICATION INFORMATION

Figure 2 illustrates the external components necessary for the proper operation of the VCO buffer. The tank circuit configuration in this figure allows the VCO to be tuned across the full operating voltage of the power supply. This is very important in 3.0 V applications where it is desirable to utilize as much of the operating supply range as possible so as to minimize the VCO sensitivity (MHz/V). In most situations, it is desirable to keep the sensitivity low so the circuit will be less

susceptible to external noise influences. An additional benefit to this configuration is that additional regulation/ filtering can be incorporated into the V_{CC} line without compromising the tuning range of the VCO. With the ac-coupled tank configuration, the V_{tune} voltage can be greater than the V_{CC} voltage supplied to the device.

There are four main areas that the user directly influences the performance of the VCO. These include Tank Design, Output Termination Selection, Power Supply Decoupling, and Circuit Board Layout/Grounding.

The design of the tank circuit is critical to the proper operation of the VCO. This tank circuit directly impacts the main VCO operating characteristics:

- 1) Frequency of Operation
- 2) Tuning Sensitivity
- 3) Voltage Supply Pushing
- 4) Phase Noise Performance

The tank circuit, in its simplest form, is realized as an LC circuit which determines the VCO operating frequency. This is described in Equation 1.

$$f_o = \frac{1}{2\pi \sqrt{LC}} \quad \text{Equation 1}$$

In the practical case, the capacitor is replaced with a varactor diode whose capacitance changes with the voltage applied, thus changing the resonant frequency at which the VCO tank operates. The capacitive component in Equation 1 also needs to include the input capacitance of the device and other circuit and parasitic elements. Typically, the inductor is realized as a surface mount chip or a wound-coil. In addition, the lead inductance and board inductance and capacitance also have an impact on the final operating point.

Figure 1. Simplified Schematic

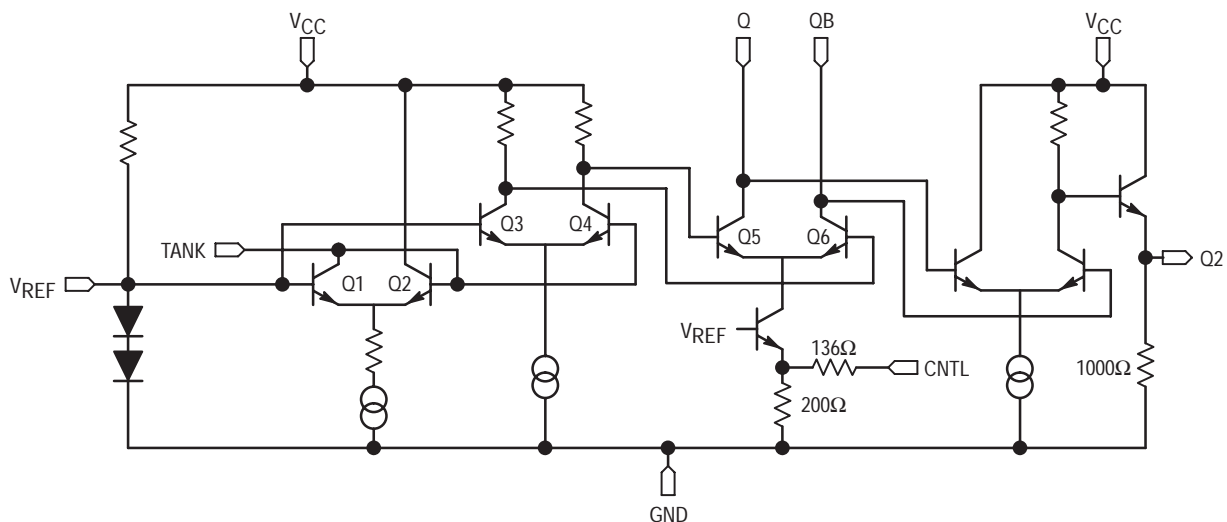
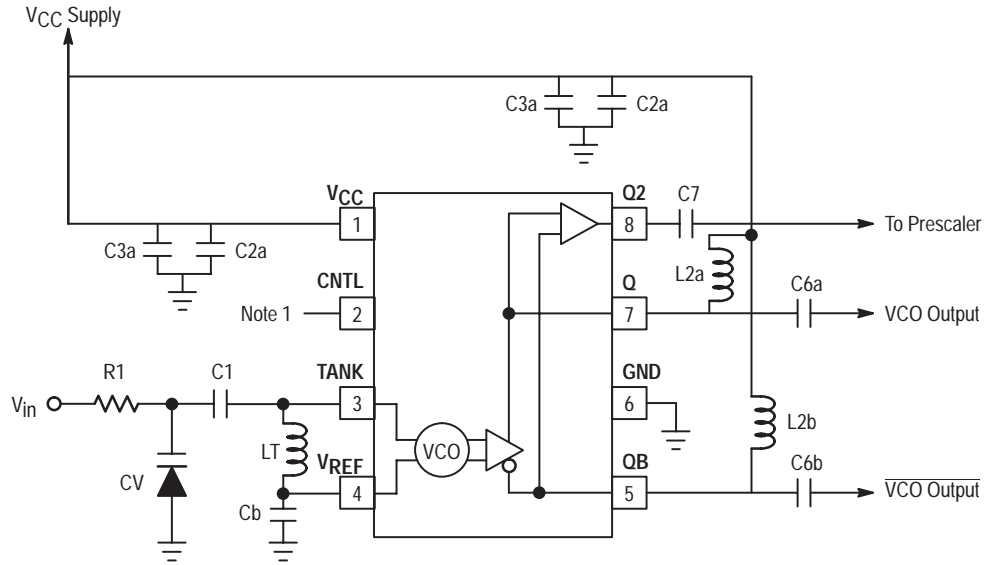


Figure 2. MC12149 Typical External Component Connections



1. This input can be left open, tied to ground, or tied with a resistor to ground, depending on the desired output amplitude needed at the Q and QB output pair.
2. Typical values for R1 range from 5.0 kΩ to 10 kΩ.

A simplified linear approximation of the device, package, and typical board parasitics has been developed to aid the designer in selecting the proper tank circuit values. All the parasitic contributions have been lumped into a parasitic capacitive component and a parasitic inductive component. While this is not entirely accurate, it gives the designer a solid starting point for selecting the tank components.

Below are the parameters used in the model.

- Cp Parasitic Capacitance
- Lp Parasitic Inductance
- LT Inductance of Coil
- C1 Coupling Capacitor Value
- Cb Capacitor for decoupling the Bias Pin
- CV Varactor Diode Capacitance (Variable)

The values for these components are substituted into the following equations:

$$C_i = \frac{C_1 \times C_V}{C_1 + C_V} + C_p \quad \text{Equation 2}$$

$$C = \frac{C_i \times C_b}{C_i + C_b} \quad \text{Equation 3}$$

$$L = L_p + L_T \quad \text{Equation 4}$$

From Figure 2, it can be seen that the varactor capacitance (CV) is in series with the coupling capacitor (C1). This is calculated in Equation 2. For analysis purposes, the parasitic capacitances (CP) are treated as a lumped element and placed in parallel with the series combination of C1 and CV. This compound capacitance (Ci) is in series with the bias capacitor (Cb) which is calculated in Equation 3. The influences of the various capacitances; C1, CP, and Cb, impact the design by reducing the variable capacitance effects of the varactor which controls the tank resonant frequency and tuning range.

Now the results calculated from Equation 2, Equation 3 and Equation 4 can be substituted into Equation 1 to calculate the actual frequency of the tank.

To aid in analysis, it is recommended that the designer use a simple spreadsheet based on Equation 1 through Equation 4 to calculate the frequency of operation for various varactor/inductor selections before determining the initial starting condition for the tank.

The two main components at the heart of the tank are the inductor (LT) and the varactor diode (CV). The capacitance of a varactor diode junction changes with the amount of reverse bias voltage applied across the two terminals. This is the element which actually “tunes” the VCO. One characteristic of the varactor is the tuning ratio which is the ratio of the capacitance at specified minimum and maximum voltage points. For characterizing the MC12149, a Matsushita (Panasonic) varactor – MA393 was selected. This device has a typical capacitance of 11 pF at 1.0 V and 3.7 pF at 4.0 V and the C–V characteristic is fairly linear over that range. Similar performance was also achieved with Loral varactors. A multi-layer chip inductor was used to realize the LT component. These inductors had typical Q values in the 35 to 50 range for frequencies between 500 and 1000 MHz.

Note: There are many suppliers of high performance varactors and inductors and Motorola can not recommend one vendor over another.

The Q (quality factor) of the components in the tank circuit has a direct impact on the resulting phase noise of the oscillator. In general, the higher the Q, the lower the phase noise of the resulting oscillator. In addition to the LT and CV components, only high quality surface-mount RF chip capacitors should be used in the tank circuit. These capacitors should have very low dielectric loss (high-Q). At a minimum, the capacitors selected should be operating 100 MHz below their series resonance point. As the desired frequency of operation increases, the values of the C1 and Cb capacitors will decrease since the series resonance point

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is a function of the capacitance value. To simplify the selection of C1 and Cb, a table has been constructed based on the intended operating frequency to provide recommended starting points. These may need to be altered depending on the value of the varactor selected.

Frequency	C1	Cb
200 – 500 MHz	47 pF	47 pF
500 – 900 MHz	5.1 pF	15 pF
900 – 1200 MHz	2.7 pF	15 pF

The value of the Cb capacitor influences the VCO supply pushing. To minimize pushing, the Cb capacitor should be kept small. Since C1 is in series with the varactor, there is a strong relationship between these two components which influences the VCO sensitivity. Increasing the value of C1 tends to increase the sensitivity of the VCO.

The parasitic contributions Lp and Cp are related to the MC12149 as well as parasitics associated with the layout, tank components, and board material selected. The input capacitance of the device, bond pad, the wire bond, package/lead capacitance, wire bond inductance, lead inductance, printed circuit board layout, board dielectric, and proximity to the ground plane all have an impact on these parasitics. For example, if the ground plane is located directly below the tank components, a parasitic capacitor will be formed consisting of the solder pad, metal traces, board dielectric material, and the ground plane. The test fixture used for characterizing the device consisted of a two sided copper clad board with ground plane on the back. Nominal values were determined by selecting a varactor and characterizing the device with a number of different tank/frequency combinations and then performing a curve fit with the data to determine values for Lp and Cp. The nominal values for the parasitic effects are seen below:

Parasitic Capacitance	Cp	4.2 pF
Parasitic Inductance	Lp	2.2 nH

These values will vary based on the users unique circuit board configuration.

Basic Guidelines:

1. Select a varactor with high Q and a reasonable capacitance versus voltage slope for the desired frequency range.
2. Select the value of Cb and C1 from the table above .
3. Calculate a value of inductance (L) which will result in achieving the desired center frequency. Note that L includes both LT and Lp.
4. Adjust the value of C1 to achieve the proper VCO sensitivity.
5. Re-adjust value of L to center VCO.
6. Prototype VCO design using selected components. It is important to use similar construction techniques and materials, board thickness, layout, ground plane spacing as intended for the final product.
7. Characterize tuning curve over the voltage operation conditions.
8. Adjust, as necessary, component values – L, C1, and Cb to compensate for parasitic board effects.
9. Evaluate over temperature and voltage limits.

10. Perform worst case analysis of tank component variation to insure proper VCO operation over full temperature and voltage range and make any adjustments as needed.

Outputs Q and QB are open collector outputs and need a inductor to VCC to provide the voltage bias to the output transistor. In most applications, DC-blocking capacitors are placed in series with the output to remove the DC component before interfacing to other circuitry. These outputs are complementary and should have identical inductor values for each output. This will minimize switching noise on the VCC supply caused by the outputs switching. It is important that both outputs be terminated, even if only one of the outputs is used in the application.

Referring to Figure 2, the recommended value for L2a and L2b should be 47 nH and the inductor components resonance should be at least 300 MHz greater than the maximum operating frequency. For operation above 1100 MHz, it may be necessary to reduce that inductor value to 33 nH. The recommended value for the coupling capacitors C6a, C6b, and C7 is 47 pF. Figure 2 also includes decoupling capacitors for the supply line as well as decoupling for the output inductors. Good RF decoupling practices should be used with a series of capacitors starting with high quality 100 pF chip capacitors close to the device. A typical layout is shown below in Figure 3.

The output amplitude of the Q and QB can be adjusted using the CNTL pin. Referring to Figure 1, if the CNTL pin is connected to ground, additional current will flow through the current source. When the pin is left open, the nominal current flowing through the outputs is 4 mA. When the pin is grounded, the current increases to a nominal value of 10 mA. So if a 50 ohm resistor was connected between the outputs and VCC, the output amplitude would change from 200 mV pp to 500 mV pp with an additional current drain for the device of 6 mA. To select a value between 4 and 10 mA, an external resistor can be added to ground. The equation below is used to calculate the current.

$$I_{out(nom)} = \frac{(200 + 136 + R_{ext}) \times 0.8V}{200 \times (136 + R_{ext})}$$

Figure 4 through Figure 13 illustrate typical performance achieved with the MC12149. The curves illustrate the tuning curve, supply pushing characteristics, output power, current drain, output spectrum, and phase noise performance. In most cases, data is present for both a 750 MHz and 1200 MHz tank design. The table below illustrates the component values used in the designs.

Component	750MHz Tank	1200MHz Tank	Units
R1	5000	5000	Ω
C1	5.1	2.7	pF
LT	4.7	1.8	nH
CV	3.7 @ 1.0 V 11 @ 4.0 V	3.7 @ 1.0 V 11 @ 4.0 V	pF
Cb	100*	15	pF
C6, C7	47	33	pF
L2	47	47	nH

NOTE: * The value of Cb should be reduced to minimize pushing.

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Figure 3. MC12149 Typical Layout
(Not to Scale)

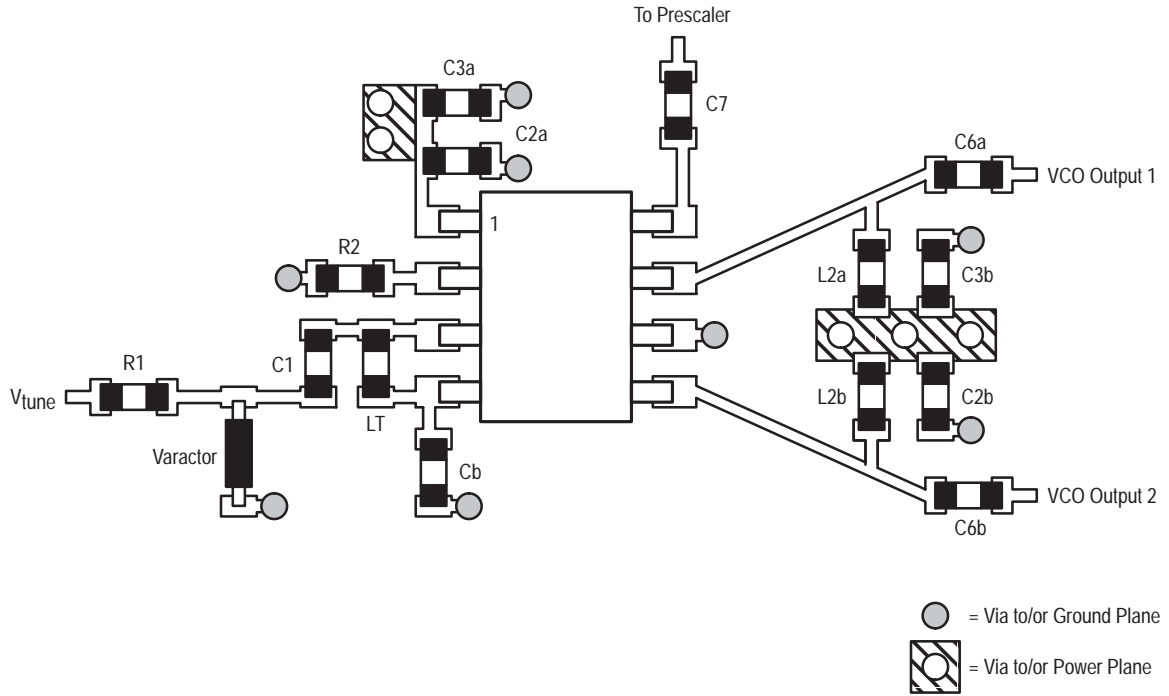


Figure 4. Typical VCO Tuning Curve, 750 MHz Tank

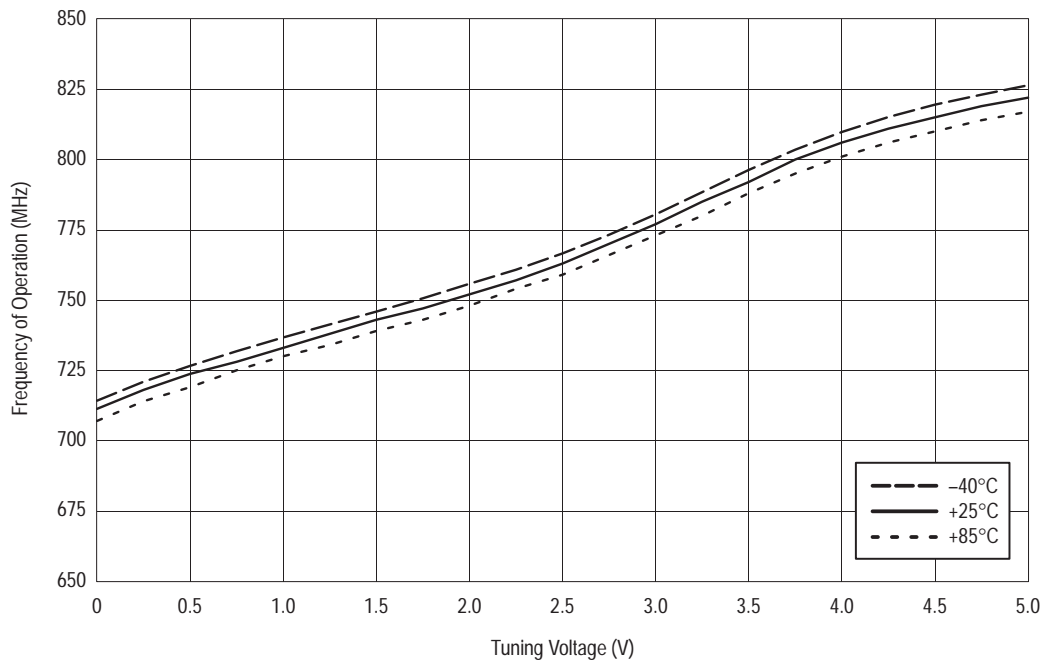
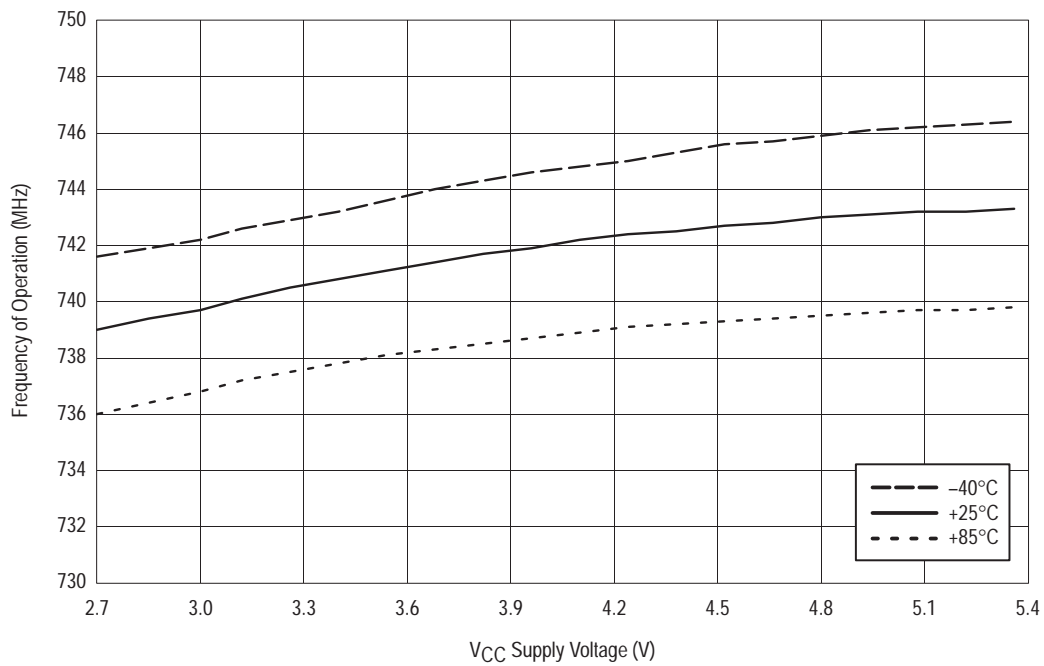


Figure 5. Typical Supply Pushing, 750 MHz Tank



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Figure 6. Typical Q/QB Output Power versus Supply, 750 MHz Tank

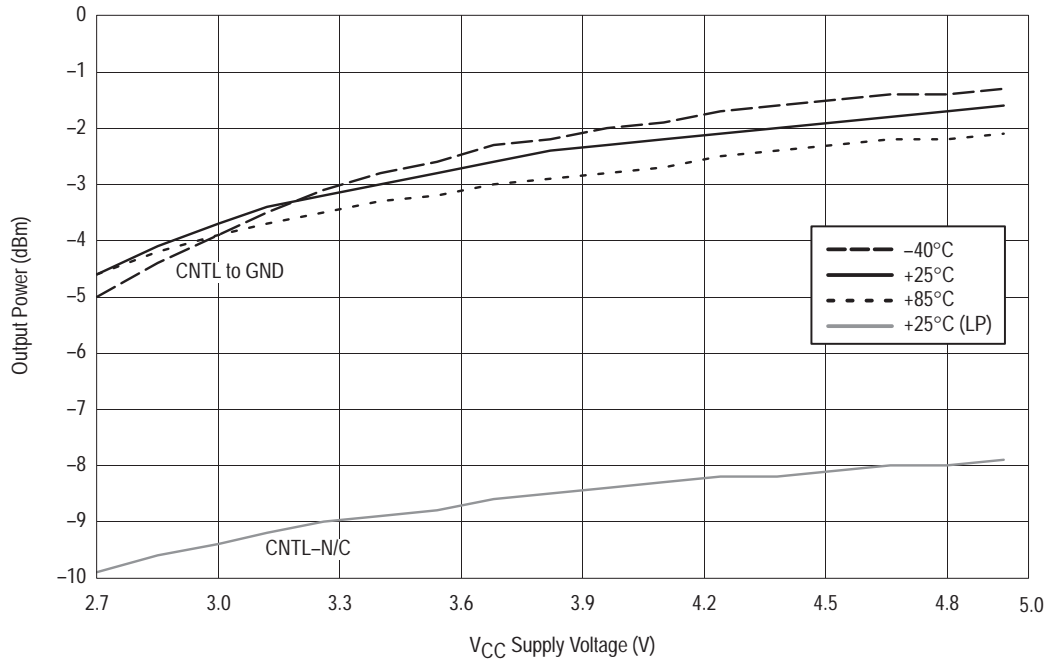
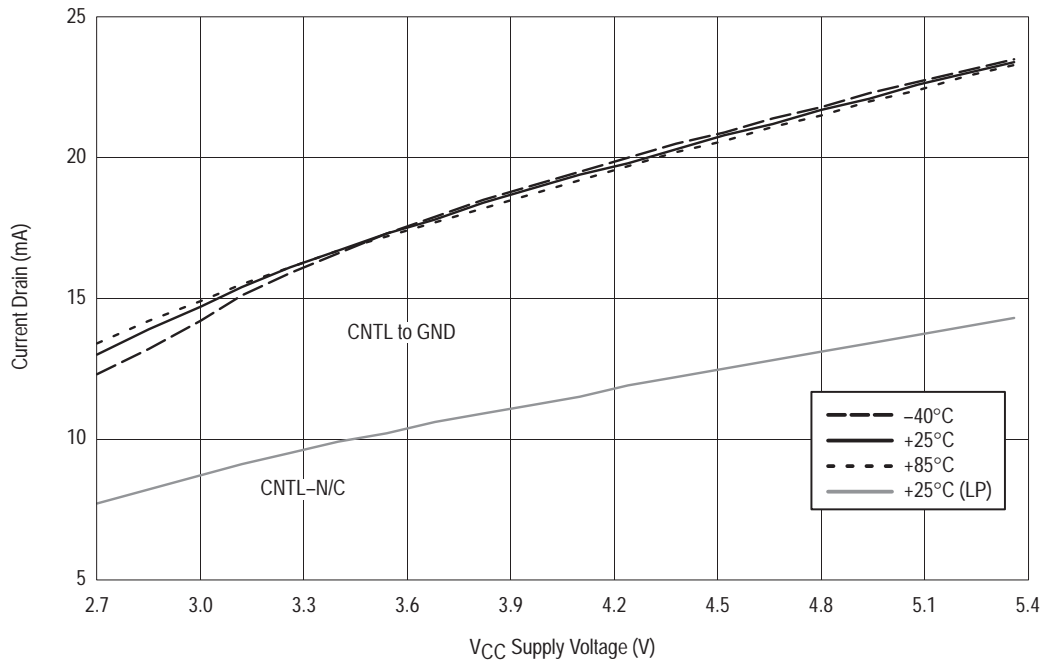


Figure 7. Typical Current Drain versus Supply, 750 MHz Tank



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Figure 8. Typical VCO Tuning Curve, 1200 MHz Tank
($V_{CC} = 5.0$ V)

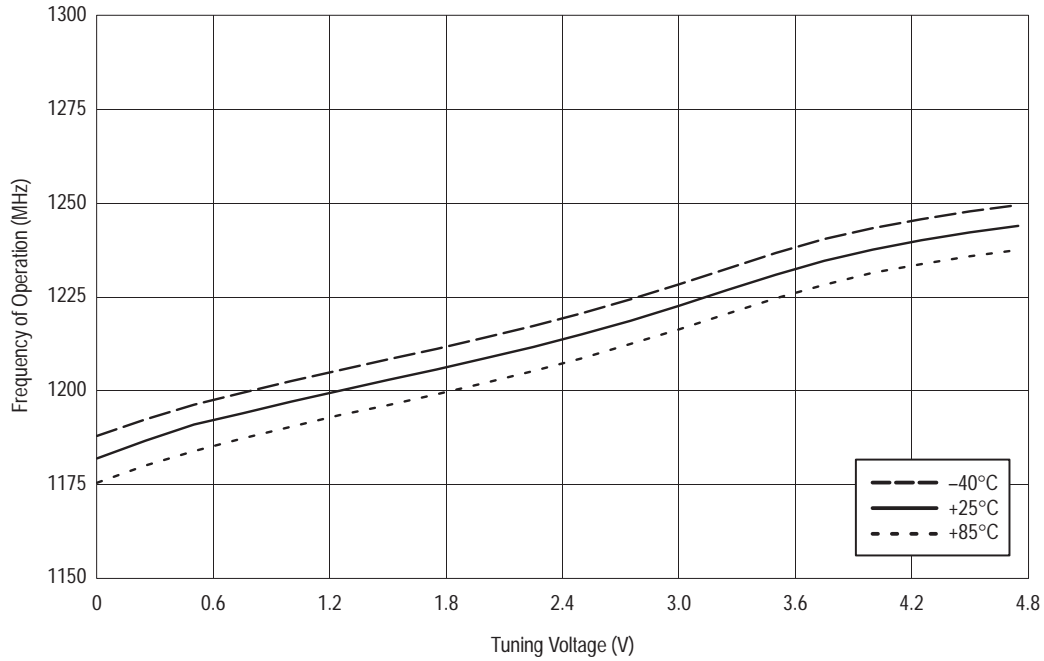
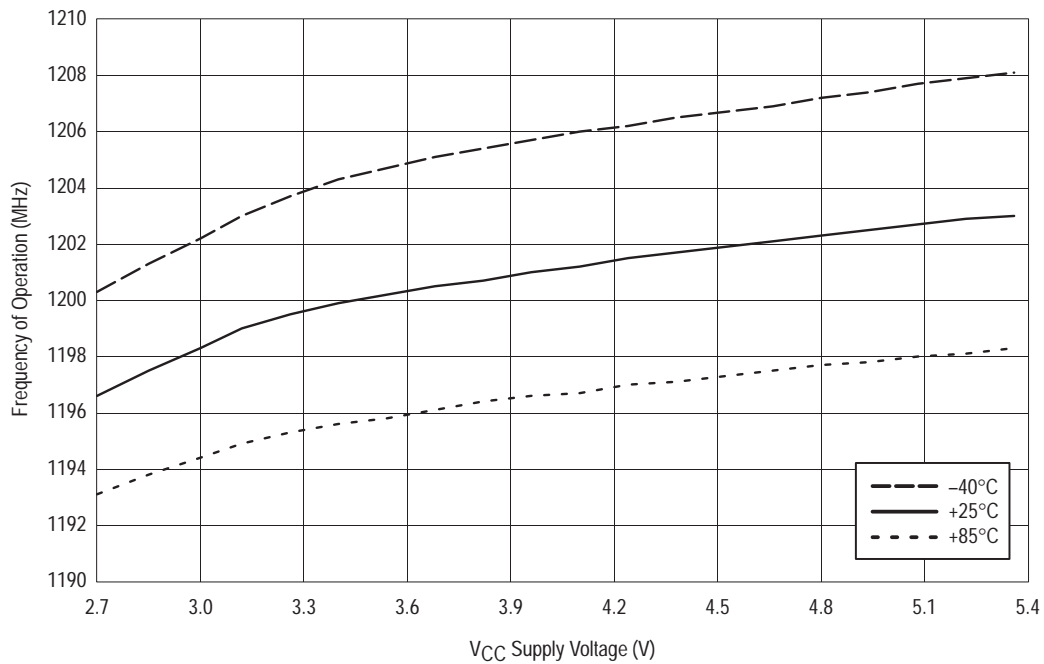


Figure 9. Typical Supply Pushing, 1200 MHz Tank



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Figure 10. Q/QB Output Power versus Supply, 1200 MHz Tank

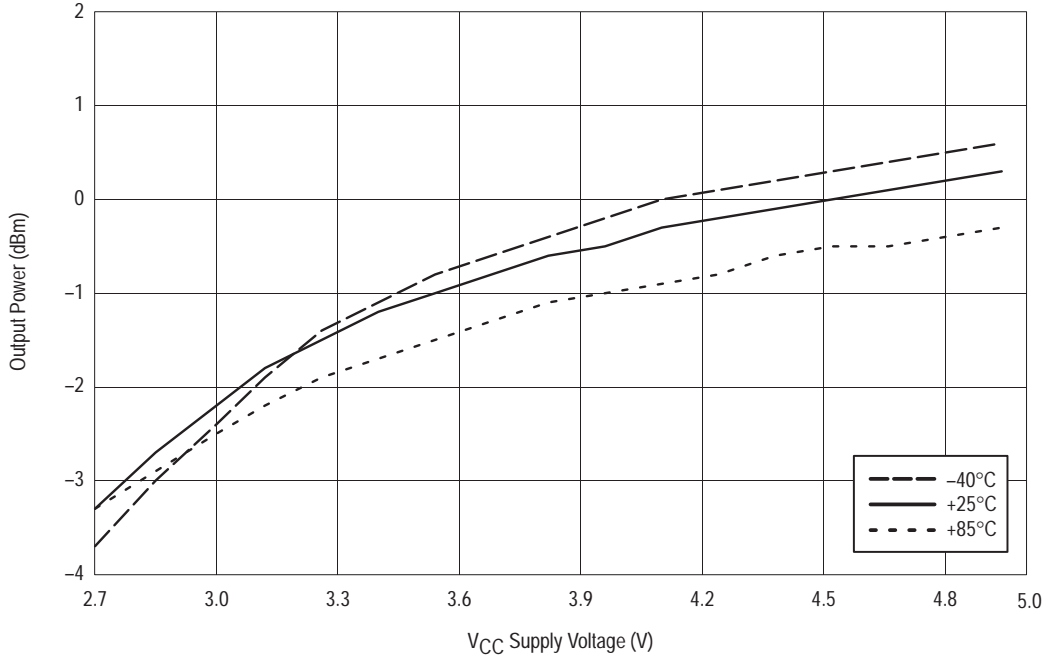


Figure 11. Typical VCO Output Spectrum

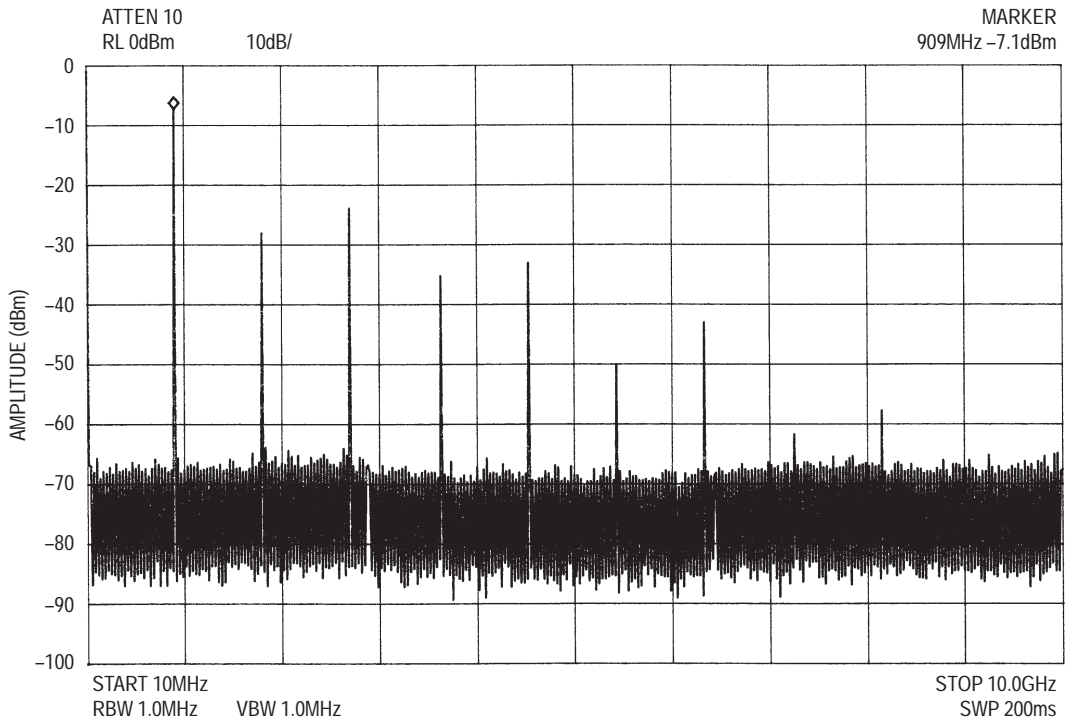


Figure 12. Typical Phase Noise Plot, 750 MHz Tank

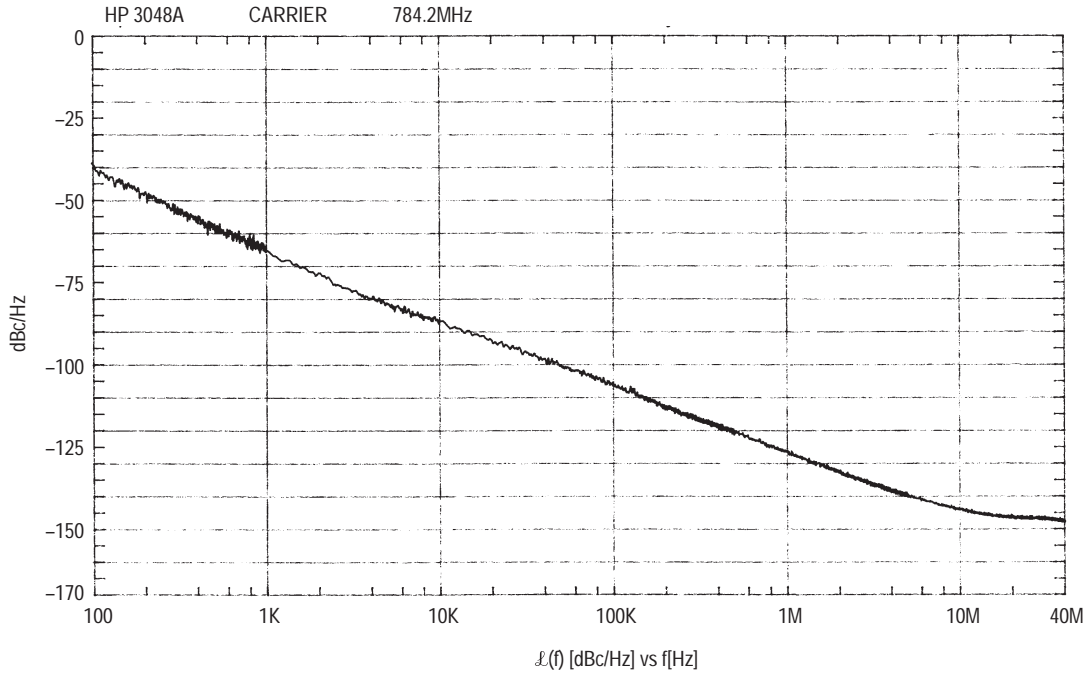
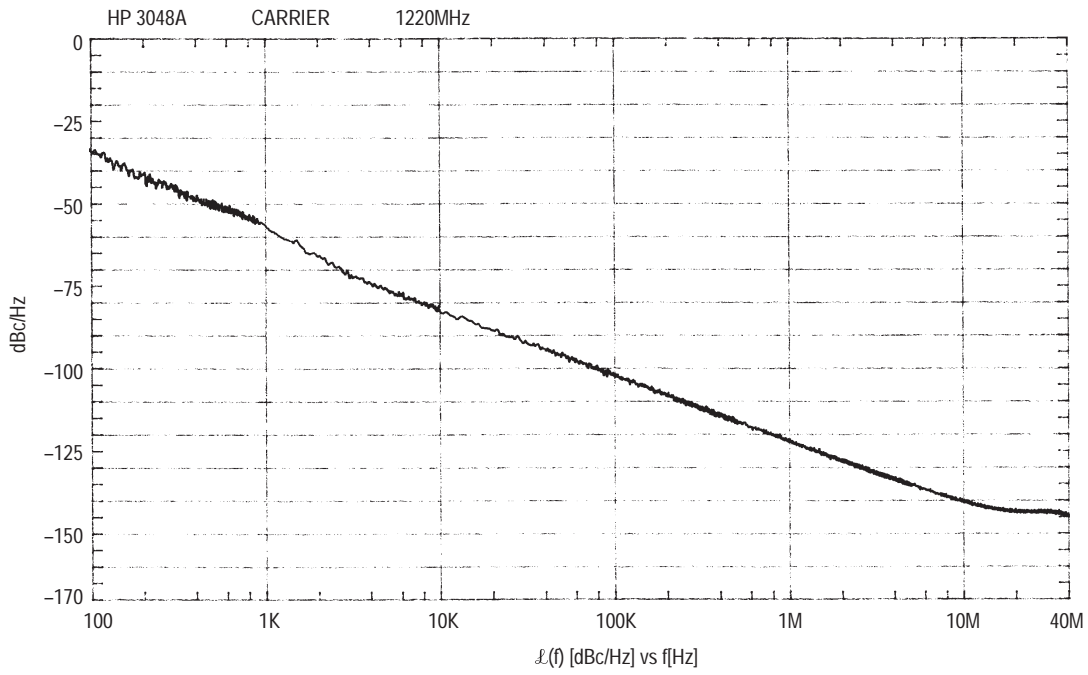


Figure 13. Typical Phase Noise Plot, 1200 MHz Tank





500-2800 MHz Single Channel Frequency Synthesizer

The MC12179 is a monolithic Bipolar synthesizer integrating the high frequency prescaler, phase/frequency detector, charge pump, and reference oscillator/buffer functions. When combined with an external loop filter and VCO, the MC12179 serves as a complete PLL subsystem. Motorola's advanced MOSAIC™ V technology is utilized for low power operation at a 5.0 V supply voltage. The device is designed for operation up to 2.8 GHz for high frequency applications such as CATV down converters and satellite receiver tuners.

- 2.8 GHz Maximum Operating Frequency
- Low Power Supply Current of 3.5 mA Typical, Including I_{CC} and I_p Currents
- Supply Voltage of 5.0 V Typical
- Integrated Divide by 256 Prescaler
- On-Chip Reference Oscillator/Buffer
 - 2.0 to 11 MHz Operation When Driven From Reference Source
 - 5.0 to 11 MHz Operation When Used With a Crystal
- Digital Phase/Frequency Detector with Linear Transfer Function
- Balanced Charge Pump Output
- Space Efficient 8-Lead SOIC
- Operating Temperature Range of -40 to 85°C

For additional information on calculating the loop filter components, an *InterActiveApNote*™ document containing software (based on a Microsoft Excel spreadsheet) and an Application Note is available. Please order DK306/D from the Motorola Literature Distribution Center.

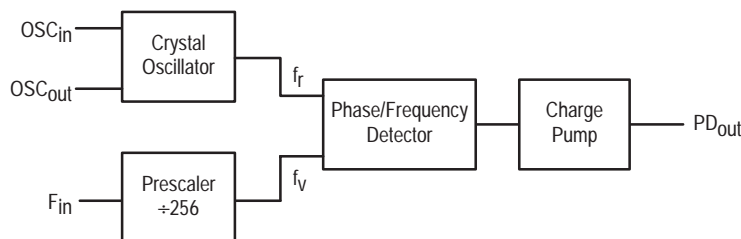
MOSAIC V, M_{fax} and *InterActiveApNote* are trademarks of Motorola, Inc.

MAXIMUM RATINGS (Note 1)

Parameter	Symbol	Value	Unit
Power Supply Voltage, Pin 2	V _{CC}	-0.5 to 6.0	Vdc
Power Supply Voltage, Pin 7	V _P	V _{CC} to 6.0	Vdc
Storage Temperature Range	T _{stg}	-65 to 150	°C

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the Recommended Operating Conditions as identified in the Electrical Characteristics table.
2. ESD data available upon request.

Block Diagram



MC12179

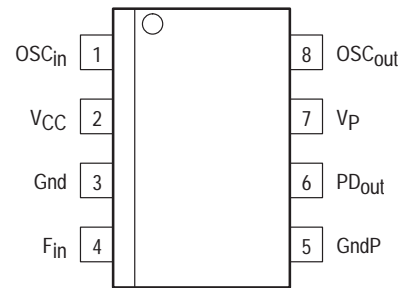
500 – 2800 MHz SINGLE CHANNEL FREQUENCY SYNTHESIZER

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)

PIN CONNECTIONS



(Top View)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12179D	T _A = -40° to +85°C	SO-8

MC12179

ELECTRICAL CHARACTERISTICS ($V_{CC} = 4.5$ to 5.5 V; $V_P = V_{CC}$ to 5.5 V; $T_A = -40$ to 85°C , unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit	Condition	
Supply Current for V_{CC}	I_{CC}	–	3.1	5.6	mA	Note 1	
Supply Current for V_P	I_P	–	0.4	1.3	mA	Note 1	
Operating Frequency	f_{INmax} f_{INmin}	2800 –	– –	– 500	MHz	Note 2	
Operating Frequency	Crystal Mode External Oscillator OSC_{in}	5 2	– –	11 11	MHz	Note 3 Note 4	
Input Sensitivity	F_{in}	V_{IN}	200	–	1000	mV $_{P-P}$	Note 2
Input Sensitivity	External Oscillator OSC_{in}	V_{OSC}	500	–	2200	mV $_{P-P}$	Note 4
Output Source Current ⁵	(PD_{out})	I_{OH}	–2.8	–2.2	–1.6	mA	$V_P = 4.5$ V, $V_{PDout} = V_P/2$
Output Sink Current ⁵	(PD_{out})	I_{OL}	1.6	2.2	2.8	mA	$V_P = 4.5$ V, $V_{PDout} = V_P/2$
Output Leakage Current	(PD_{out})	I_{OZ}	–	0.5	15	nA	$V_P = 5.0$ V, $V_{PDout} = V_P/2$

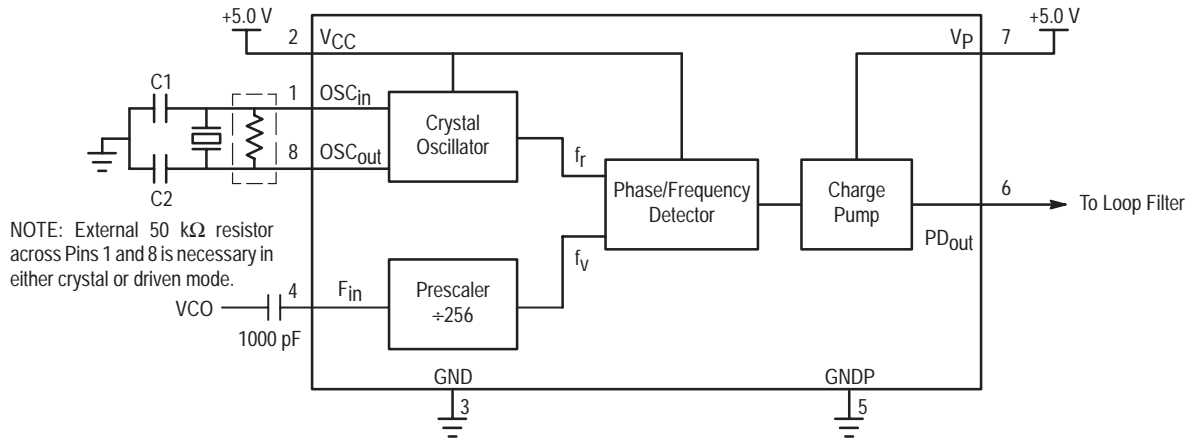
- NOTES:** 1. V_{CC} and $V_P = 5.5$ V; $F_{IN} = 2.56$ GHz; $F_{OSC} = 10$ MHz crystal; PD_{out} open.
 2. AC coupling, F_{IN} measured with a 1000 pF capacitor.
 3. Assumes C_1 and C_2 (Figure 1) limited to ≤ 30 pF each including stray and parasitic capacitances.
 4. AC coupling to OSC_{in} .
 5. Refer to Figure 15 and Figure 16 for typical performance curves over temperature and power supply voltage.

PIN FUNCTION DESCRIPTION

Pin	Symbol	I/O	Function
1	OSC_{in}	I	Oscillator Input — An external parallel-resonant, fundamental crystal is connected between OSC_{in} and OSC_{out} to form an internal reference oscillator (crystal mode). External capacitors C_1 and C_2 , as shown in Figure 1, are required to set the proper crystal load capacitance and oscillator frequency. For an external reference oscillator, an external signal is AC-coupled to the OSC_{in} pin with a 1000 pF coupling capacitor, with no connection to OSC_{out} . In either mode, a resistor with a nominal value of 50 k Ω MUST be placed across the OSC_{in} and OSC_{out} pins for proper operation.
2	V_{CC}	—	Positive Power Supply. Bypass capacitors should be placed as close as possible to the pin and be connected directly to the ground plane.
3	Gnd	—	Ground.
4	F_{in}	I	Prescaler Input — The VCO signal is AC coupled into the F_{in} pin.
5	GndP	—	Ground — For charge pump circuitry.
6	PD_{out}	O	Single ended phase/frequency detector output (charge pump output). Three-state current sink/source output for use as a loop error signal when combined with an external low pass filter. The phase/frequency detector is characterized by a linear transfer function.
7	V_P	—	Positive power supply for charge pump. V_P MUST be equal or greater than V_{CC} . Bypass capacitors should be placed as close as possible to the pin and be connected directly to the ground plane.
8	OSC_{out}	O	Oscillator output, for use with an external crystal as shown in Figure 1.

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Figure 1. MC12179 Expanded Block Diagram



PHASE CHARACTERISTICS

The phase comparator in the MC12179 is a high speed digital phase/frequency detector circuit. The circuit determines the “lead” or “lag” phase relationship and time difference between the leading edges of the VCO (f_v) signal and the reference (f_r) input. The detector can cover a range of $\pm 2\pi$ radian of f_v/f_r phase difference. The operation of the charge pump output is shown in Figure 2.

f_r lags f_v in phase OR $f_v > f_r$ in frequency

When the phase of f_r lags that of f_v or the frequency of f_v is greater than f_r , the Do output will sink current. The pulse width will be determined by the time difference between the two rising edges.

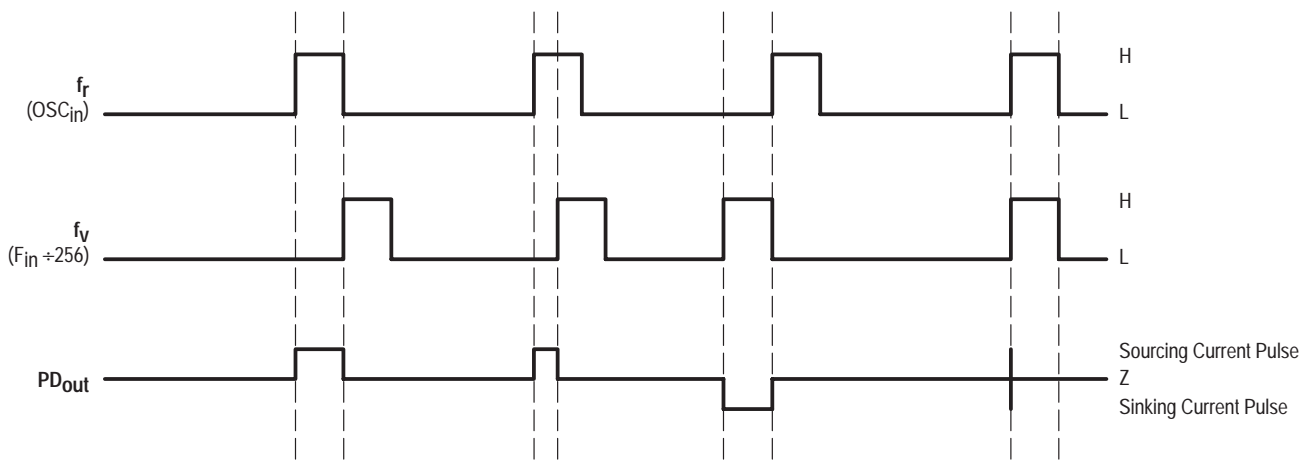
f_r leads f_v in phase OR $f_v < f_r$ in frequency

When the phase of f_r leads that of f_v or the frequency of f_v is less than f_r , the Do output will source current. The pulse width will be determined by the time difference between the two rising edges.

$f_r = f_v$ in phase and frequency

When the phase and frequency of f_r and f_v are equal, the charge pump will be in a quiet state, except for current spikes when signals are in phase. This situation indicates that the loop is in lock and the phase comparator will maintain the loop in its locked state.

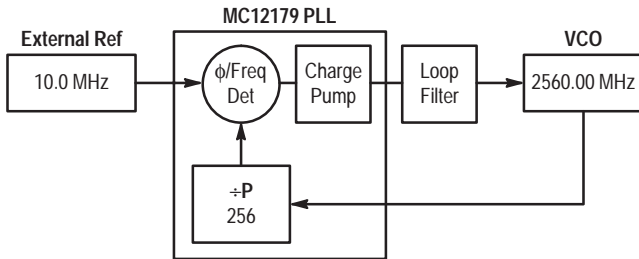
Figure 2. Phase/Frequency Detector and Charge Pump Waveforms



$$K_p\text{-Charge Pump Gain} \approx \frac{|I_{\text{source}}| + |I_{\text{sink}}|}{4\pi} = \frac{|2.2| + |-2.2|}{4\pi} = \frac{1.1 \text{ mA}}{\pi \text{ radian}}$$

The MC12179 is intended for applications where a fixed local oscillator is required to be synthesized. The prescaler on the MC12179 operates up to 2.8GHz which makes the part ideal for many satellite receiver applications as well as applications in the 2nd ISM (Industrial, Scientific, and Medical) band which covers the frequency range of 2400MHz to 2483MHz. The part is also intended for MMDS (Multi-channel Multi-point Distribution System) block downconverter applications. Below is a typical block diagram of the complete PLL.

Figure 3. Typical Block Diagram of Complete PLL



As can be seen from the block diagram, with the addition of a VCO, a loop filter, and either an external oscillator or crystal, a complete PLL sub-system can be realized. Since most of the PLL function is integrated into the MC12179, the user's primary focus is on the loop filter design and the crystal reference circuit. Figure 13 and Figure 14 illustrate typical VCO spectrum and phase noise characteristics. Figure 17 and Figure 18 illustrate the typical input impedance versus frequency for the prescaler input.

Crystal Oscillator Design

The MC12179 is used as a multiply-by-256 PLL circuit which transfers the high stability characteristic of a low frequency reference source to the high frequency VCO in the PLL loop. To facilitate this, the device contains an input circuit which can be configured as a crystal oscillator or a buffer for accepting an external signal source.

In the external reference mode, the reference source is AC-coupled into the OSC_{IN} input pin. The input level signal should be between 500–2200 mVpp. When configured with an external reference, the device can operate with input frequencies down to 2MHz, thus allowing the circuit to control the VCO down to 512 MHz. To optimize the phase noise of the PLL when used in this mode, the input signal amplitude should be closer to the upper specification limit. This maximizes the slew rate of the input signal as it switches against the internal voltage reference.

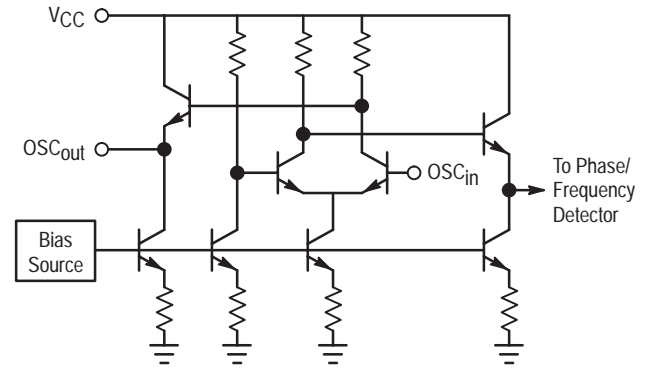
In the crystal mode, an external parallel-resonant fundamental mode crystal is connected between the OSC_{IN} and OSC_{OUT} pins. This crystal must be between 5.0 MHz and 11 MHz. External capacitors, C1 and C2 as shown in Figure 1, are required to set the proper crystal load capacitance and oscillator frequency. The values of the capacitors are dependent on the crystal chosen and the input capacitance of the device and any stray board capacitance.

In either mode, a 50kΩ resistor must be connected between the OSC_{IN} and the OSC_{OUT} pins for proper device operation. The value of this resistor is not critical so a 47kΩ or 51kΩ ±10% resistor is acceptable.

Since the MC12179 is realized with an all-bipolar ECL style design, the internal oscillator circuitry is different from more traditional CMOS oscillator designs which realize the crystal oscillator with a modified inverter topology. These CMOS designs typically excite the crystal with a rail-to-rail signal which may overdrive the crystal resulting in damage or unstable operation. The MC12179 design does not exhibit these phenomena because the swing out of the OSC_{OUT} pin is less than 600mV. This has the added advantage of minimizing EMI and switching noise which can be generated by rail-to-rail CMOS outputs. The OSC_{OUT} output should not be used to drive other circuitry.

The oscillator buffer in the MC12179 is a single stage, high speed, differential input/output amplifier; it may be considered to be a form of the Pierce oscillator. A simplified circuit diagram is seen in Figure 4.

Figure 4. Simplified Crystal Oscillator/Buffer Circuit



OSC_{IN} drives the base of one input of an NPN transistor differential pair. The non-inverting input of the differential pair is internally biased. OSC_{OUT} is the inverted input signal and is buffered by an emitter follower with a 70 μA pull-down current and has a voltage swing of about 600 mVpp. Open loop output impedance is about 425Ω. The opposite side of the differential amplifier output is used internally to drive another buffer stage which drives the phase/frequency detector. With the 50 kΩ feedback resistor in place, OSC_{IN} and OSC_{OUT} are biased to approximately 1.1V below VCC. The amplifier has a voltage gain of about 15 dB and a bandwidth in excess of 150 MHz. Adherence to good RF design and layout techniques, including power supply pin decoupling, is strongly recommended.

A typical crystal oscillator application is shown in Figure 1. The crystal and the feedback resistor are connected directly between OSC_{IN} and OSC_{OUT}, while the loading capacitors, C1 and C2, are connected between OSC_{IN} and ground, and OSC_{OUT} and ground respectively. It is important to understand that as far as the crystal is concerned, the two loading capacitors are in series (albeit through ground). So when the crystal specification defines a specific loading capacitance, this refers to the total external (to the crystal) capacitance seen across its two pins.

This capacitance consists of the capacitance contributed by the amplifier (IC and packaging), layout capacitance, and the series combination of the two loading capacitors. This is illustrated in the equation below:

$$C_I = C_{AMP} + C_{STRAY} + \frac{C_1 \times C_2}{C_1 + C_2}$$

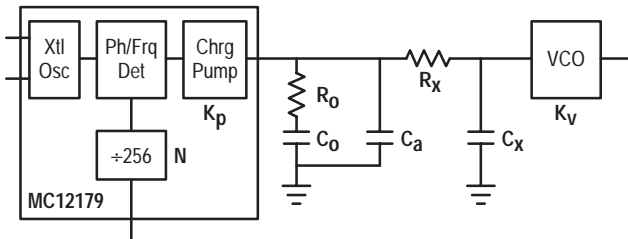
Provided the crystal and associated components are located immediately next to the IC, thus minimizing the stray capacitance, the combined value of C_{AMP} and C_{STRAY} is approximately 5pF. Note that the location of the OSC_{IN} and OSC_{OUT} pins at the end of the package, facilitates placing the crystal, resistor and the C1 and C2 capacitors very close to the device. Usually, one of the capacitors is in parallel with an adjustable capacitor used to trim the frequency of oscillation. It is important that the total external (to the IC) capacitance seen by either OSC_{IN} or OSC_{OUT} , be no greater than 30pF.

In operation, the crystal oscillator will start up with the application of power. If the crystal is in a can that is not grounded it is often possible to monitor the frequency of oscillation by connecting an oscilloscope probe to the can; this technique minimizes any disturbance to the circuit. If a malfunction is indicated, a high impedance, low capacitance, FET probe may be connected to either OSC_{IN} or OSC_{OUT} . Signals typically seen at those points will be very nearly sinusoidal with amplitudes of roughly 300 to 600 mVpp. Some distortion is inevitable and has little bearing on the accuracy of the signal going to the phase detector.

Loop Filter Design

Because the device is designed for a non-frequency agile synthesizer (i.e., how fast it tunes is not critical) the loop filter design is very straight forward. The current output of the charge pump allows the loop filter to be realized without the need of any active components. The preferred topology for the filter is illustrated below in Figure 5.

Figure 5. Loop Filter



The R_0/C_0 components realize the primary loop filter. C_a is added to the loop filter to provide for reference sideband suppression. If additional suppression is needed, the R_x/C_x realizes an additional filter. In most applications, this will not be necessary. If all components are used, this results in a 4th order PLL, which makes analysis difficult. To simplify this, the loop design will be treated as a 2nd order loop (R_0/C_0) and additional guidelines are provided to minimize the influence of the other components. If more rigorous analysis is needed, mathematical/system simulation tools can be used.

Component	Guideline
C_a	$<0.1 \times C_0$
R_x	$>10 \times R_0$
C_x	$<0.1 \times C_0$

The focus of the design effort is to determine what the loop's natural frequency, ω_0 , should be. This is determined by R_0 , C_0 , K_p , K_v , and N . Because K_p , K_v , and N are given, it is only necessary to calculate values for R_0 and C_0 . There are 3 considerations in selecting the loop bandwidth:

- 1) Maximum loop bandwidth for minimum tuning speed
- 2) Optimum loop bandwidth for best phase noise performance
- 3) Minimum loop bandwidth for greatest reference sideband suppression

Usually a compromise is struck between these 3 cases, however, for the fixed frequency application, minimizing the tuning speed is not a critical parameter.

To specify the loop bandwidth for optimal phase noise performance, an understanding of the sources of phase noise in the system and the effect of the loop filter on them is required. There are 3 major sources of phase noise in the phase-locked loop – the crystal reference, the VCO, and the loop contribution. The loop filter acts as a low-pass filter to the crystal reference and the loop contribution equal to the total divide-by-N ratio. This is mathematically described in Figure 10. The loop filter acts as a high-pass filter to the VCO with an in-band gain equal to unity. This is described in Figure 11. The loop contribution includes the PLL IC, as well as noise in the system; supply noise, switching noise, etc. For this example, a loop contribution of 15 dB has been selected, which corresponds to data in Figure 14.

The crystal reference and the VCO are characterized as high-order 1/f noise sources. Graphical analysis is used to determine the optimum loop bandwidth. It is necessary to have noise plots from the manufacturer. This method provides a straightforward approximation suitable for quickly estimating the optimal bandwidth. The loop contribution is characterized as white-noise or low-order 1/f noise given in the form of a noise factor which combines all the noise effects into a single value. The phase noise of the Crystal Reference is increased by the noise factor of the PLL IC and related circuitry. It is further increased by the total divide-by-N ratio of the loop. This is illustrated in Figure 6.

The point at which the VCO phase noise crosses the amplified phase noise of the Crystal Reference is the point of the optimum loop bandwidth. In the example of Figure 6, the optimum bandwidth is approximately 15 KHz.

Figure 6. Graphical Analysis of Optimum Bandwidth

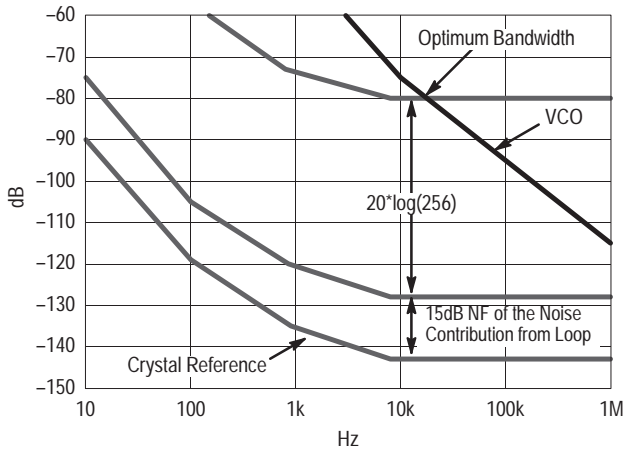
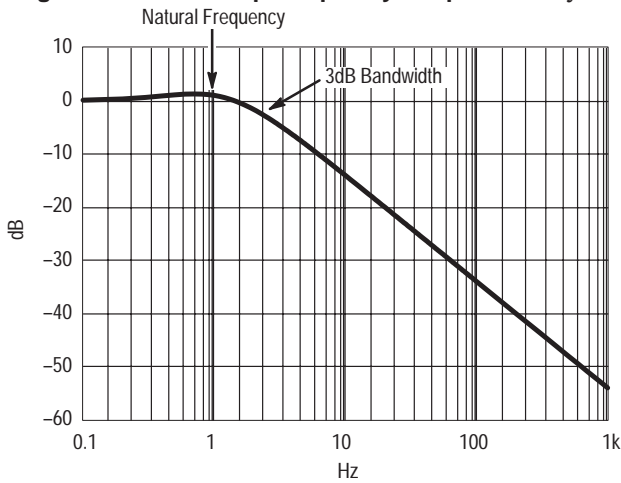


Figure 7. Closed Loop Frequency Response for $\zeta = 1$



To simplify analysis further a damping factor of 1 will be selected. The normalized closed loop response is illustrated in Figure 7 where the loop bandwidth is 2.5 times the loop natural frequency (the loop natural frequency is the frequency at which the loop would oscillate if it were unstable). Therefore the optimum loop bandwidth is

15kHz/2.5 or 6kHz (37.7krads) with a damping coefficient, $\zeta \approx 1$. $T(s)$ is the transfer function of the loop filter.

Figure 8. Design Equations for the 2nd Order System

$$T(s) = \frac{R_0 C_0 s + 1}{\left(\frac{N C_0}{K_p K_v}\right) s^2 + R_0 C_0 s + 1} = \frac{\left(\frac{2\zeta}{\omega_0}\right) s + 1}{\left(\frac{1}{\omega_0^2}\right) s^2 + \left(\frac{2\zeta}{\omega_0}\right) s + 1}$$

$$\left(\frac{N C_0}{K_p K_v}\right) = \left(\frac{1}{\omega_0^2}\right) \rightarrow \omega_0 = \sqrt{\frac{K_p K_v}{N C_0}} \rightarrow C_0 \approx \left(\frac{K_p K_v}{N \omega_0^2}\right)$$

$$R_0 C_0 = \left(\frac{2\zeta}{\omega_0}\right) \rightarrow \zeta = \left(\frac{\omega_0 R_0 C_0}{2}\right) \rightarrow R_0 = \left(\frac{2\zeta}{\omega_0 C_0}\right)$$

In summary, follow the steps given below:

- Step 1: Plot the phase noise of crystal reference and the VCO on the same graph.
- Step 2: Increase the phase noise of the crystal reference by the noise contribution of the loop.
- Step 3: Convert the divide-by-N to dB ($20\log 256 - 48$ dB) and increase the phase noise of the crystal reference by that amount.
- Step 4: The point at which the VCO phase noise crosses the amplified phase noise of the Crystal Reference is the point of the optimum loop bandwidth. This is approximately 15 kHz in Figure 6.
- Step 5: Correlate this loop bandwidth to the loop natural frequency and select components per Figure 8. In this case the 3.0 dB bandwidth for a damping coefficient of 1 is 2.5 times the loop's natural frequency. The relationship between the 3.0 dB loop bandwidth and the loop's "natural" frequency will vary for different values of ζ . Making use of the equations defined above in a math tool or spreadsheet is useful. To aid in the use of such a tool the equations are summarized in Figures 9 through 11.

Figure 9. Loop Parameter Relations

Let: $\frac{N C_0}{K_p K_v} = \frac{1}{\omega_0^2}$, $R_0 C_0 = \frac{2\zeta}{\omega_0}$

Let: $C_a = a C_0$, $C_x = b C_0$, $A = 1 + a$, and $B = 1 + a + b$

Let: $R_0 C_0 = \frac{1}{\omega_3}$, $R_x C_x = \frac{1}{\omega_4}$, $R_0(C_a + C_x) = \frac{1}{\omega_5}$

Let: $K_3 \omega_3 = \omega_0$, $K_4 \omega_4 = \omega_0$, $K_5 \omega_5 = \omega_0$

Figure 10. Transfer Function for the Crystal Noise in the Frequency Plane

$$T(j\omega) = N \cdot \frac{1 + j \left(2\zeta \frac{\omega}{\omega_0} \right)}{\left(1 + K_3K_4 \frac{\omega^4}{\omega_0^4} - B \frac{\omega^2}{\omega_0^2} \right) + j \left(2\zeta \frac{\omega}{\omega_0} - (AK_4 + K_5) \frac{\omega^3}{\omega_0^3} \right)}$$

Figure 11. Transfer Function for the VCO Noise in the Frequency Plane

$$T(j\omega) = \frac{\left(K_3K_4 \frac{\omega^4}{\omega_0^4} - B \frac{\omega^2}{\omega_0^2} \right) - j \left((AK_4 + K_5) \frac{\omega^3}{\omega_0^3} \right)}{\left(1 + K_3K_4 \frac{\omega^4}{\omega_0^4} - B \frac{\omega^2}{\omega_0^2} \right) + j \left(2\zeta \frac{\omega}{\omega_0} - (AK_4 + K_5) \frac{\omega^3}{\omega_0^3} \right)}$$

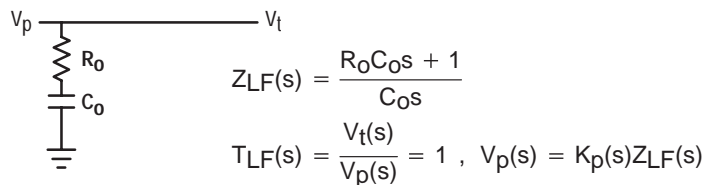
Appendix: Derivation of Loop Filter Transfer Function

The purpose of the loop filter is to convert the current from the phase detector to a tuning voltage for the VCO. The total transfer function is derived in two steps. Step 1 is to find the voltage generated by the impedance of the loop filter. Step 2 is to find the transfer function from the input of the loop filter to its output. The “voltage” times the “transfer function” is the

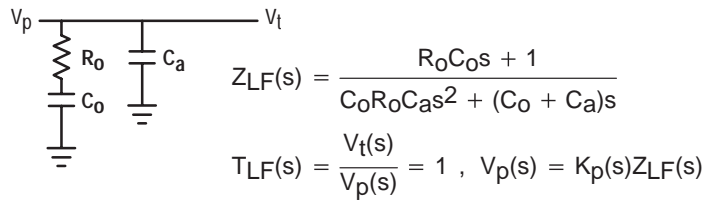
overall transfer function of the loop filter. To use these equations in determining the overall transfer function of a PLL multiply the filter’s impedance by the gain constant of the phase detector then multiply that by the filter’s transfer function (which is unity in the 2nd and 3rd order cases below).

Figure 12. Overall Transfer Function of the PLL

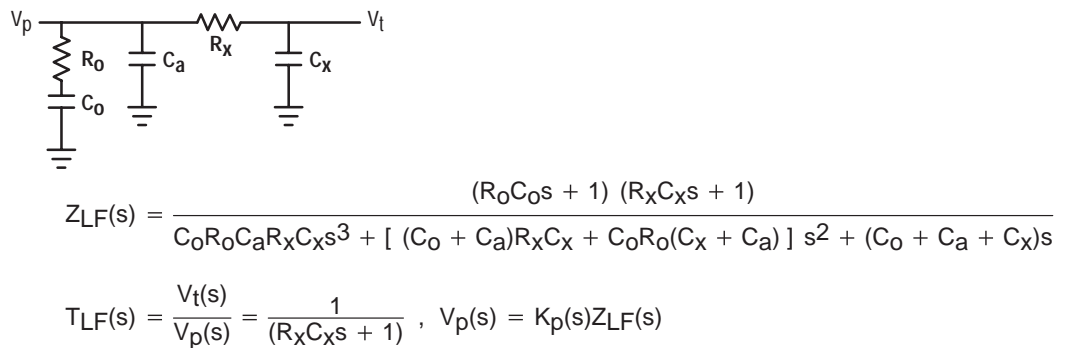
For the 2nd Order PLL:



For the 3rd Order PLL:



For the 4th Order PLL:



MC12179

Figure 15. Typical Charge Pump Current versus Temperature
($V_{CC} = V_{pp} = 5.0\text{ V}$)

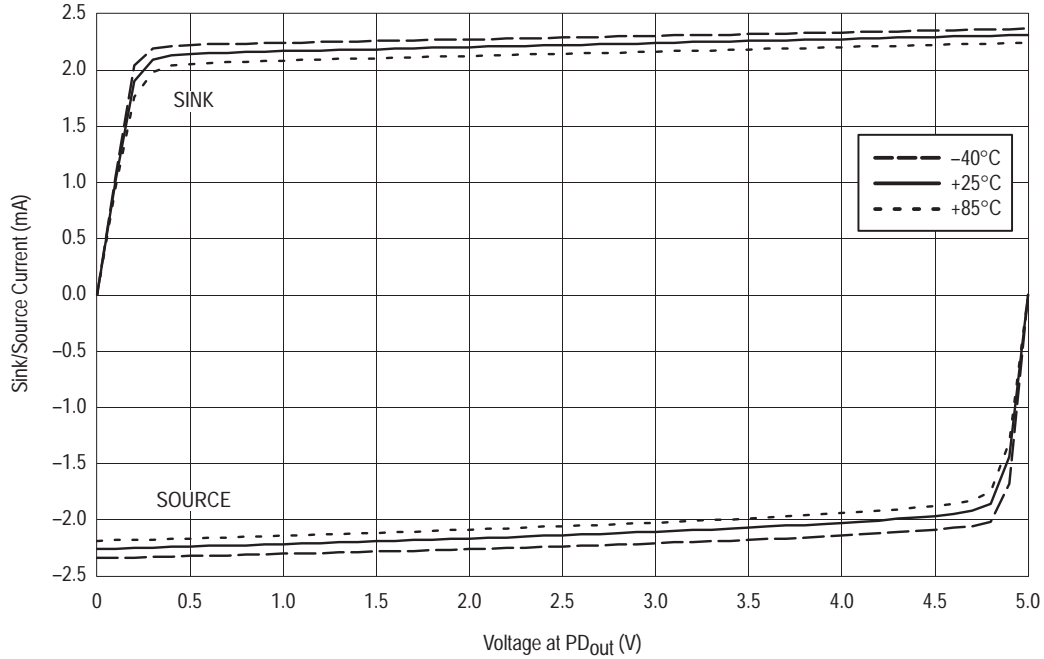
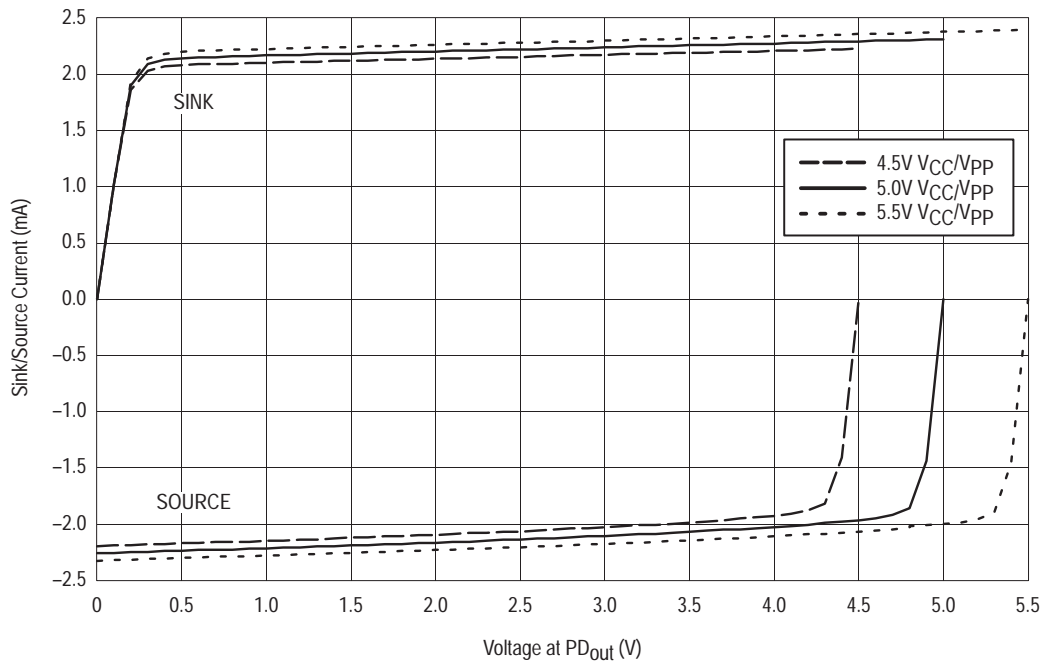


Figure 16. Typical Charge Pump Current versus Voltage
($T = 25^\circ\text{C}$)



MC12179

Figure 17. Typical Real Input Impedance versus Input Frequency
(For the F_{in} Input)

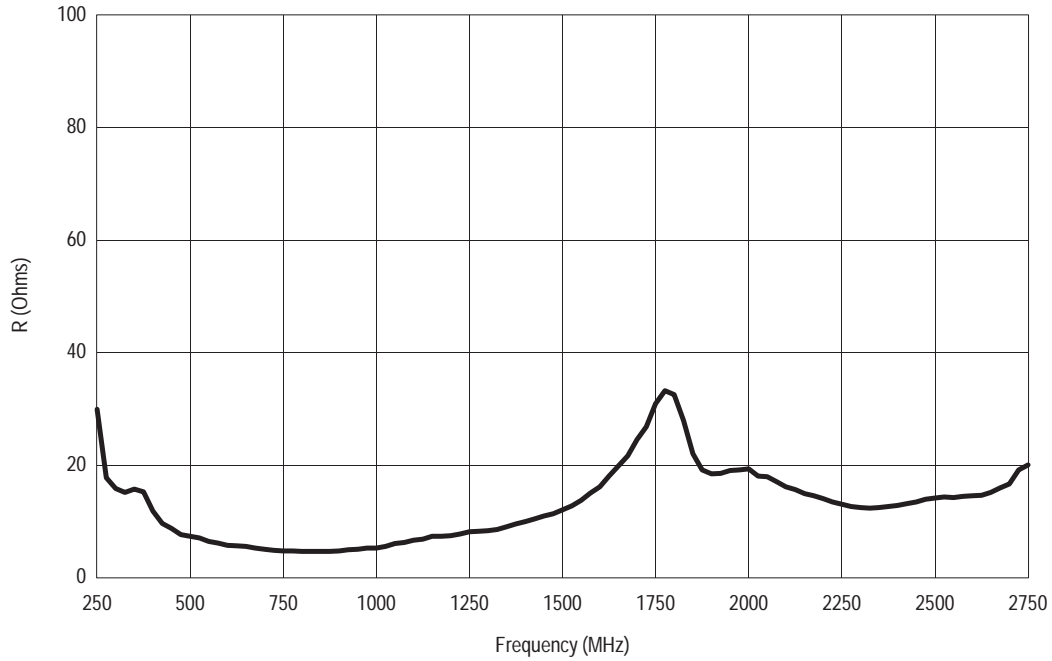
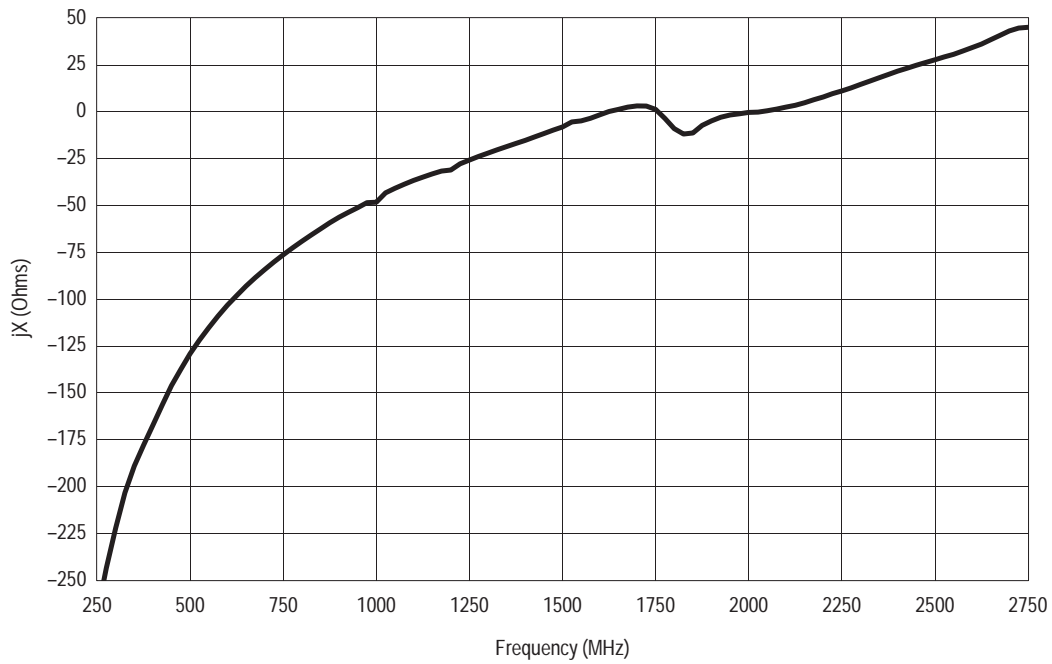


Figure 18. Typical Imaginary Input Impedance versus Input Frequency
(For the F_{in} Input)





Serial Input PLL Frequency Synthesizer

The MC12210 is a 2.5 GHz Bipolar monolithic serial input phase locked loop (PLL) synthesizer with pulse–swallow function. It is designed to provide the high frequency local oscillator signal of an RF transceiver in handheld communication applications.

Motorola’s advanced Bipolar MOSAIC™ V technology is utilized for low power operation at a minimum supply voltage of 2.7 V. The device is designed for operation over 2.7 to 5.5 V supply range for input frequencies up to 2.5 GHz with a typical current drain of 9.5 mA. The low power consumption makes the MC12210 ideal for handheld battery operated applications such as cellular or cordless telephones, wireless LAN or personal communication services. A dual modulus prescaler is integrated to provide either a 32/33 or 64/65 divide ratio.

For additional applications information, two *InterActiveApNote*™ documents containing software (based on a Microsoft Excel spreadsheet) and an Application Note are available. Please order DK305/D and DK306/D from the Motorola Literature Distribution Center.

- Low Power Supply Current of 8.8 mA Typical for I_{CC} and 0.7 mA Typical for I_p
- Supply Voltage of 2.7 to 5.5 V
- Dual Modulus Prescaler With Selectable Divide Ratios of 32/33 or 64/65
- On–Chip Reference Oscillator/Buffer
- Programmable Reference Divider Consisting of a Binary 14–Bit Programmable Reference Counter
- Programmable Divider Consisting of a Binary 7–Bit Swallow Counter and an 11–Bit Programmable Counter
- Phase/Frequency Detector With Phase Conversion Function
- Balanced Charge Pump Outputs
- Dual Internal Charge Pumps for Bypassing the First Stage of the Loop Filter to Decrease Lock Time
- Outputs for External Charge Pump
- Operating Temperature Range of –40 to 85°C
- Space Efficient Plastic Surface Mount SOIC or TSSOP Packages

MOSAIC V, Mfax and *InterActiveApNote* are trademarks of Motorola, Inc.

MAXIMUM RATINGS (Note 1)

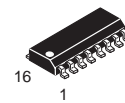
Parameter	Symbol	Value	Unit
Power Supply Voltage, Pin 4 (Pin 5 in 20–lead package)	V _{CC}	–0.5 to 6.0	Vdc
Power Supply Voltage, Pin 3 (Pin 4 in 20–lead package)	V _p	V _{CC} to 6.0	Vdc
Storage Temperature Range	T _{stg}	–65 to 150	°C

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the Recommended Operating Conditions.
2. ESD data available upon request.

MC12210

MECL PLL COMPONENTS SERIAL PLL FREQUENCY SYNTHESIZER

SEMICONDUCTOR TECHNICAL DATA



D SUFFIX
PLASTIC PACKAGE
CASE 751B
(SO–16)

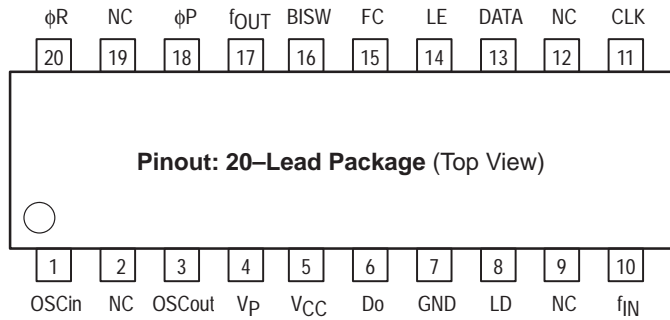
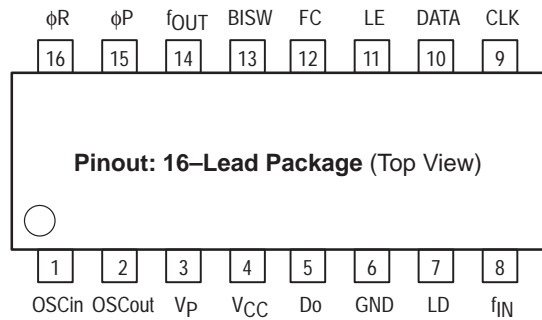


DT SUFFIX
PLASTIC PACKAGE
CASE 948E
(TSSOP–20)

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC12210D	T _A = – 40° to +85°C	SO–16
MC12210DT		TSSOP–20

MC12210

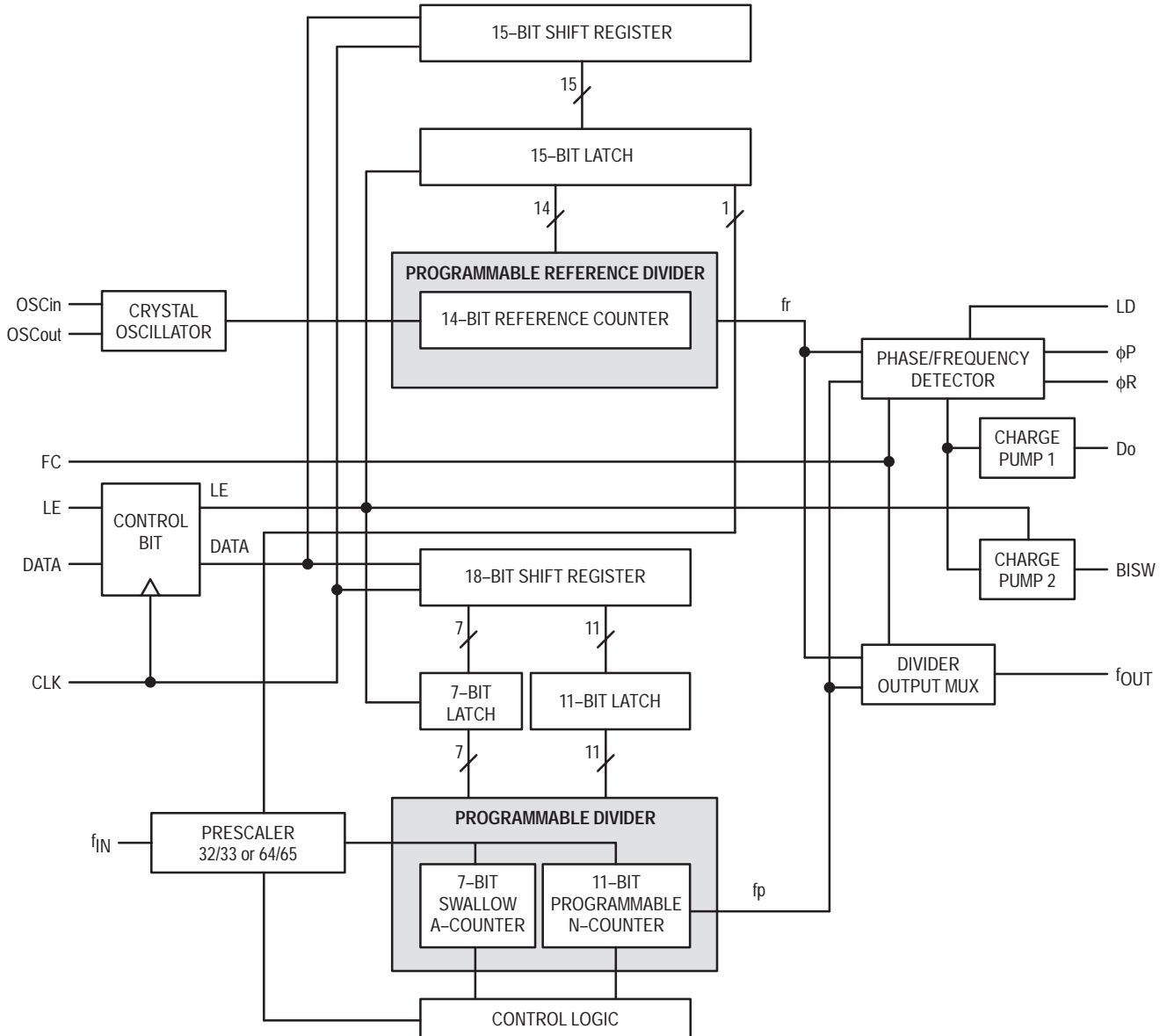


PIN NAMES

Pin	I/O	Function	16-Lead Pkg Pin No.	20-Lead Pkg Pin No.
OSCin	I	Oscillator input. A crystal may be connected between OSCin and OSCout. It is highly recommended that an external source be ac coupled into this pin (see text).	1	1
OSCout	O	Oscillator output. Pin should be left open if external source is used	2	3
Vp	—	Power supply for charge pumps (Vp should be greater than or equal to VCC) Vp provides power to the Do, BISW and φP outputs	3	4
VCC	—	Power supply voltage input. Bypass capacitors should be placed as close as possible to this pin and be connected directly to the ground plane.	4	5
Do	O	Internal charge pump output. Do remains on at all times	5	6
GND	—	Ground	6	7
LD	O	Lock detect, phase comparator output	7	8
fIN	I	Prescaler input. The VCO signal is AC-coupled into this pin	8	10
CLK	I	Clock input. Rising edge of the clock shifts data into the shift registers	9	11
DATA	I	Binary serial data input	10	13
LE	I	Load enable input (with internal pull up resistor). When LE is HIGH or OPEN, data stored in the shift register is transferred into the appropriate latch (depending on the level of control bit). Also, when LE is HIGH or OPEN, the output of the second internal charge pump is connected to the BISW pin	11	14
FC	I	Phase control select (with internal pull up resistor). When FC is LOW, the characteristics of the phase comparator and charge pump are reversed. FC also selects fp or fr on the fOUT pin	12	15
BISW	O	Analog switch output. When LE is HIGH or OPEN ("analog switch is ON") the output of the second charge pump is connected to the BISW pin. When LE is LOW, BISW is high impedance	13	16
fOUT	O	Phase comparator input signal. When FC is HIGH, fOUT=fr, programmable reference divider output; when FC is LOW, fOUT=fp, programmable divider output	14	17
φP	O	Output for external charge pump. Standard CMOS output level	15	18
φR	O	Output for external charge pump. Standard CMOS output level	16	20
NC	—	No connect	—	2, 9, 12, 19

MC12210

Figure 1. MC12210 Block Diagram

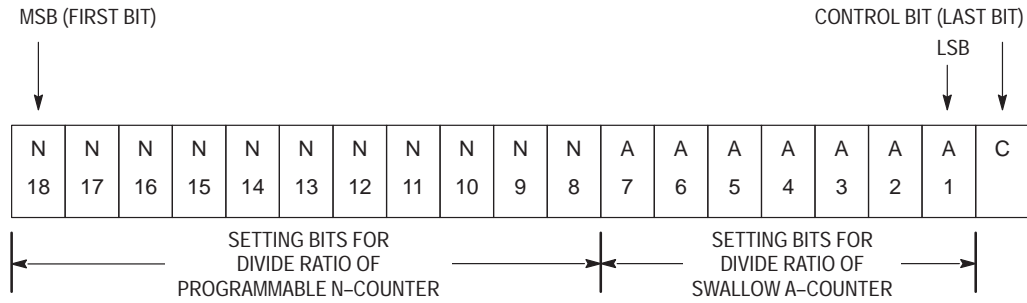


MC12210

PROGRAMMABLE DIVIDER

19-bit serial data format for the programmable divider is shown below. If the control bit is LOW, data is transferred from the 18-bit shift register into the 18-bit latch which specifies the swallow A-counter divide ratio (0 to 127) and the programmable N-counter divide ratio (16 to 2047). An N-counter divide ratio less than 16 is prohibited.

For Control bit (C) = LOW:



DIVIDE RATIO OF PROGRAMMABLE N-COUNTER

DIVIDE RATIO OF SWALLOW A-COUNTER

Divide Ratio N	N 18	N 17	N 16	N 15	N 14	N 13	N 12	N 11	N 10	N 9	N 8	Divide Ratio A	A 7	A 6	A 5	A 4	A 3	A 2	A 1
16	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	1	0	0	0	1	1	0	0	0	0	0	0	1
•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
2047	1	1	1	1	1	1	1	1	1	1	1	127	1	1	1	1	1	1	1

DIVIDE RATIO SETTING

$$fvco = [(P \cdot N) + A] \cdot fosc \div R \text{ with } A < N$$

fvco: Output frequency of external voltage controlled oscillator (VCO)

N: Preset divide ratio of binary 11-bit programmable counter (16 to 2047)

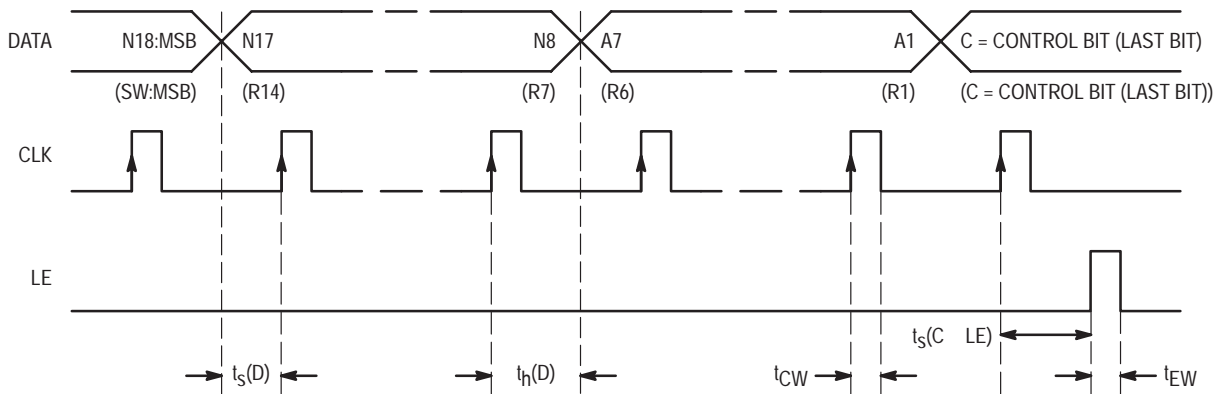
A: Preset divide ratio of binary 7-bit swallow counter (0 to 127, A < N)

fosc: Output frequency of the external frequency oscillator

R: Preset divide ratio of binary 14-bit programmable reference counter (8 to 16383)

P: Preset mode of dual modulus prescaler (32 or 64)

Figure 2. Serial Data Input Timing



NOTES: Programmable reference divider data shown in parenthesis. Data shifted into register on rising edge of CLK.

$t_s(D)$ = Setup Time DATA to CLK	$t_s(D) \geq 10$ ns
$t_h(D)$ = Hold Time DATA to CLK	$t_h(D) \geq 20$ ns
t_{CW} = CLK Pulse Width	$t_{CW} \geq 30$ ns
t_{EW} = LE Pulse Width	$t_{EW} \geq 20$ ns
$t_s(C \text{ LE})$ = Setup Time CLK to LE	$t_s(C \text{ LE}) \geq 30$ ns

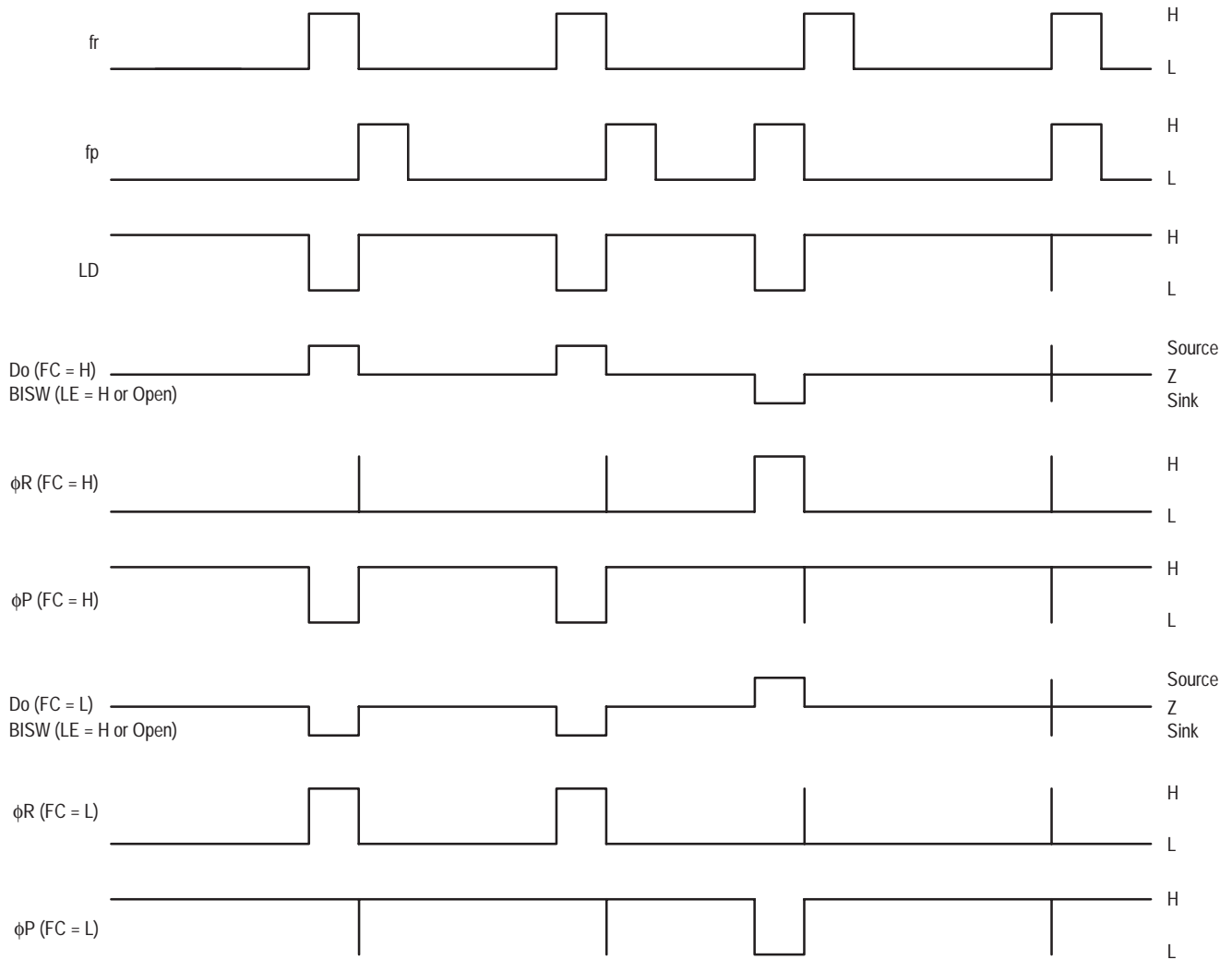
MC12210

PHASE CHARACTERISTICS/VCO CHARACTERISTICS

The phase comparator in the MC12210 is a high speed digital phase frequency detector circuit. The circuit determines the “lead” or “lag” phase relationship and time difference between the leading edges of the VCO (fp) signal and the reference (fr) input. Since these edges occur only once per cycle, the detector has a range of $\pm 2\pi$ radians. The phase comparator outputs are standard CMOS rail-to-rail levels (V_P to GND for ϕ_P and V_{CC} to GND for ϕ_R), designed for up to 20MHz operation into a 15pF load. These phase comparator outputs can be used along with an external charge pump to enhance the PLL characteristics.

The operation of the phase comparator is shown in Figures 3 and 5. The phase characteristics of the phase comparator are controlled by the FC pin. The polarity of the phase comparator outputs, ϕ_R and ϕ_P , as well as the charge pump output Do can be reversed by switching the FC pin.

Figure 3. Phase/Frequency Detector, Internal Charge Pump and Lock Detect Waveforms



NOTES: Do and BISW are current outputs.
 Phase difference detection range: -2π to $+2\pi$
 Spike difference depends on charge pump characteristics. Also, the spike is output in order to diminish dead band.
 When $f_r > f_p$ or $f_r < f_p$, spike might not appear depending upon charge pump characteristics.

$$\text{Internal Charge Pump Gain} \approx \left| \frac{I_{\text{source}} + I_{\text{sink}}}{4\pi} \right| = \frac{4\text{mA}}{4\pi}$$

For FC = HIGH:

fr lags fp in phase OR fp > fr in frequency

When the phase of fr lags that of fp or the frequency of fp is greater than fr, the φP output will remain in a HIGH state while the φR output will pulse from LOW to HIGH. The output pulse will reach a minimum 50% duty cycle under a 180° out of phase condition. The signal on φR indicates to the VCO to decrease in frequency to bring the loop into lock.

fr leads fp in phase OR fp < fr in frequency

When the phase of fr leads that of fp or the frequency of fp is less than fr, the φR output will remain in a LOW state while the φP output pulses from HIGH to LOW. The output pulse will reach a minimum 50% duty cycle under a 180° out of phase condition. The signal on φP indicates to the VCO to increase in frequency to bring the loop to lock.

fr = fp in phase and frequency

When the phase and frequency of fr and fp are equal, the output φP will remain in a HIGH state and φR will remain in a LOW state except for voltage spikes when signals are in phase. This situation indicates that the loop is in lock and the phase comparator will maintain the loop in its locked state.

When FC = LOW, the operation of the phase comparator is reversed from the above explanation.

For FC = LOW:

fr lags fp in phase OR fp > fr in frequency

When the phase of fr lags that of fp or the frequency of fp is greater than fr, the φR output will remain in a LOW state while the φP output will pulse from HIGH to LOW. The output pulse will reach a minimum 50% duty cycle under a 180° out of phase condition. The signal on φP indicates to the VCO to increase in frequency to bring the loop into lock.

fr leads fp in phase OR fp < fr in frequency

When the phase of fr leads that of fp or the frequency of fp is less than fr, the φP output will remain in a HIGH state while the φR output pulses from LOW to HIGH. The output pulse will reach a minimum 50% duty cycle under a 180° out of phase condition. The signal on φR indicates to the VCO to decrease in frequency to bring the loop to lock.

fr = fp in phase and frequency

When the phase and frequency of fr and fp are equal, the output φP will remain in a HIGH state and φR will remain in a LOW state except for voltage spikes when signals are in phase. This situation indicates that the loop is in lock and the phase comparator will maintain the loop in its locked state.

The FC pin controls not only the phase characteristics, but also controls the f_{OUT} test pin. The FC pin permits the user to monitor either of the phase comparator input signals, fr or fp, at the f_{OUT} output providing a test mode where the programming of the dividers and the output of the counters can be checked. When FC is HIGH, f_{OUT} = fr, the programmable reference divider output. When FC is LOW, f_{OUT} = fp, the programmable divider output.

Hence,

If VCO characteristics are like (1), FC should be set HIGH or OPEN. $f_{OUT} = fr$

If VCO characteristics are like (2), FC should be set LOW. $f_{OUT} = fp$

Figure 4. VCO Characteristics

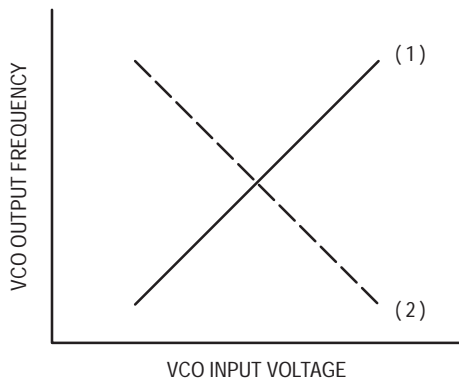


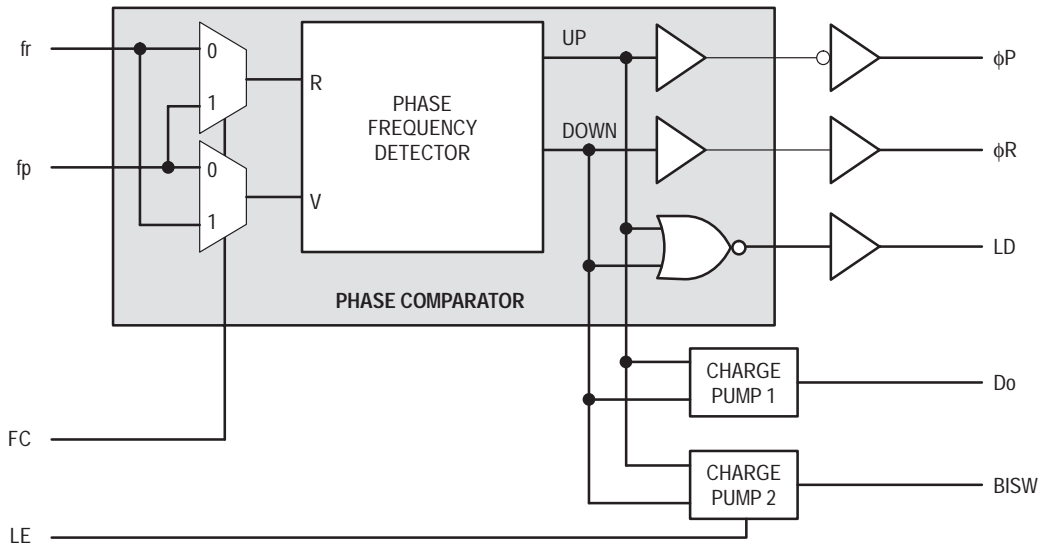
Figure 5. Phase Comparator, Internal Charge Pump, and f_{OUT} Characteristics

	FC = HIGH or OPEN				FC = LOW			
	Do	φR	φP	f _{OUT}	Do	φR	φP	f _{OUT}
fp < fr	H	L	L	fr	L	H	H	fp
fp > fr	L	H	H	fr	H	L	L	fp
fp = fr	Z	L	H	fr	Z	L	H	fp

NOTES: Z = High impedance
When LE is HIGH or Open, BISW has the same characteristics as Do.

MC12210

Figure 6. Detailed Phase Comparator Block Diagram



LOCK DETECT

The Lock Detect (LD) output pin provides a LOW pulse when fr and fp are not equal in phase or frequency. The output is normally HIGH. LD is designed to be the logical NORing of the phase frequency detector’s outputs UP and DOWN. See Figure 6. In typical applications the output signal drives external circuitry which provides a steady LOW signal when the loop is locked. See Figure 9.

OSCILLATOR INPUT

For best operation, an external reference oscillator is recommended. The signal should be AC-coupled to the OSCin pin through a coupling capacitor. In this case, no connection to OSCout is required. The magnitude of the AC-coupled signal must be between 500 and 2200 mV peak-to-peak. To optimize the phase noise of the PLL when used in this mode, the input signal amplitude should be closer to the upper specification limit. This maximizes the slew rate of the signal as it switches against the internal voltage reference.

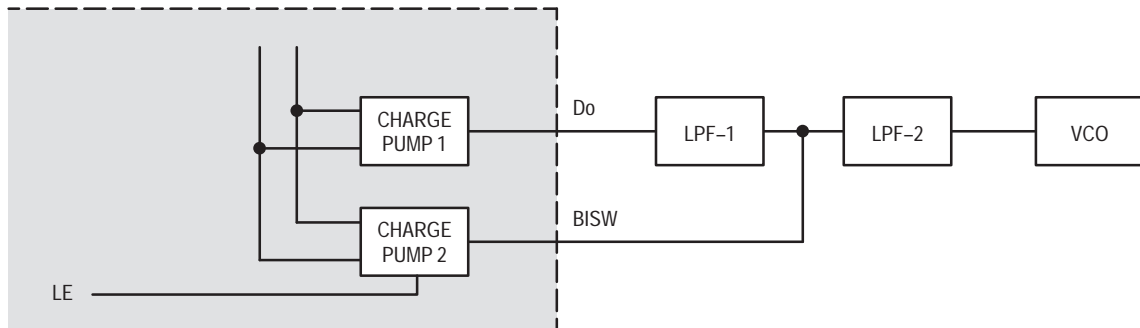
The device incorporates an on-chip reference oscillator/buffer so that an external parallel-resonant fundamental crystal can be connected between OSCin and OSCout. External capacitor C1 and C2 as shown in Figure 10 are required to set the proper crystal load capacitance and oscillator frequency. The values of the capacitors are dependent on the crystal chosen (up to a maximum of 30 pF each including parasitic and stray capacitance). However, using the on-chip reference oscillator greatly increases the synthesized phase noise.

DUAL INTERNAL CHARGE PUMPS (“ANALOG SWITCH”)

Due to the pure Bipolar nature of the MC12210 design, the “analog switch” function is implemented with dual internal charge pumps. The loop filter time constant can be decreased by bypassing the first stage of the loop filter with the charge pump output BISW as shown in Figure 7 below. This enables the VCO to lock in a shorter amount of time.

When LE is HIGH or OPEN (“analog switch is ON”), the output of the second internal charge pump is connected to the BISW pin, and the Do output is ON. The charge pump 2 output on BISW is essentially equal to the charge pump 1 output on Do. When LE is LOW, BISW is in a high impedance state and Do output is active.

Figure 7. “Analog Switch” Block Diagram



MC12210

ELECTRICAL CHARACTERISTICS ($V_{CC} = 2.7$ to 5.5 V; $T_A = -40$ to $+85^\circ\text{C}$, unless otherwise noted.)

Parameter	Symbol	Min	Typ	Max	Unit	Condition	
Supply Current for V_{CC}	I_{CC}	–	8.8	13.0	mA	Note 1	
		–	10.2	16.0		Note 2	
Supply Current for V_P	I_P	–	0.7	1.1	mA	Note 3	
		–	0.8	1.3		Note 4	
Operating Frequency	f_{INmax} f_{INmin}	2500	–	–	MHz	Note 5	
		–	–	500			
Operating Frequency (OSCin)	F_{OSC}	–	12	20	MHz	Crystal Mode	
		–	–	40	MHz	External Reference Mode	
Input Sensitivity	f_{IN}	V_{IN}	200	–	1000	mVpp	
	OSCin	V_{OSC}	500	–	2200	mVpp	
Input HIGH Voltage	CLK, DATA, LE, FC	V_{IH}	$0.7 V_{CC}$	–	–	V	
Input LOW Voltage	CLK, DATA, LE, FC	V_{IL}	–	–	$0.3 V_{CC}$	V	
Input HIGH Current (DATA and CLK)		I_{IH}	–	1.0	2.0	μA	$V_{CC} = 5.5$ V
Input LOW Current (DATA and CLK)		I_{IL}	–10	–5.0	–	μA	$V_{CC} = 5.5$ V
Input Current (OSCin)		I_{OSC}	–	130	–	μA	OSCin = V_{CC} OSCin = $V_{CC} - 2.2$ V
Input HIGH Current (LE and FC)		I_{IH}	–	1.0	2.0	μA	
Input LOW Current (LE and FC)		I_{IL}	–75	–60	–	μA	
Charge Pump Output Current Do and BISW	I_{Source}^6	–2.6	–2.0	–1.4	mA	$V_{DO} = V_P/2$; $V_P = 2.7$ V $V_{BISW} = V_P/2$; $V_P = 2.7$ V	
	I_{Sink}^6	+1.4	+2.0	+2.6			
	I_{Hi-Z}	–15	–	+15	nA	$0.5 < V_{DO} < V_P - 0.5$ $0.5 < V_{BISW} < V_P - 0.5$	
Output HIGH Voltage (LD, ϕ_R , ϕ_P , f_{OUT})	V_{OH}	4.4	–	–	V	$V_{CC} = 5.0$ V	
		2.4	–	–	V	$V_{CC} = 3.0$ V	
Output LOW Voltage (LD, ϕ_R , ϕ_P , f_{OUT})	V_{OL}	–	–	0.4	V	$V_{CC} = 5.0$ V	
		–	–	0.4	V	$V_{CC} = 3.0$ V	
Output HIGH Current (LD, ϕ_R , ϕ_P , f_{OUT})		I_{OH}	–1.0	–	–	mA	
Output LOW Current (LD, ϕ_R , ϕ_P , f_{OUT})		I_{OL}	1.0	–	–	mA	

- $V_{CC} = 3.3$ V, all outputs open.
- $V_{CC} = 5.5$ V, all outputs open.
- $V_P = 3.3$ V, all outputs open.

- $V_P = 6.0$ V, all outputs open.
- AC coupling, F_{IN} measured with a 1000 pF capacitor.
- Source current flows out of the pin and sink current flows into the pin.

Figure 8. Typical External Charge Pump Circuit

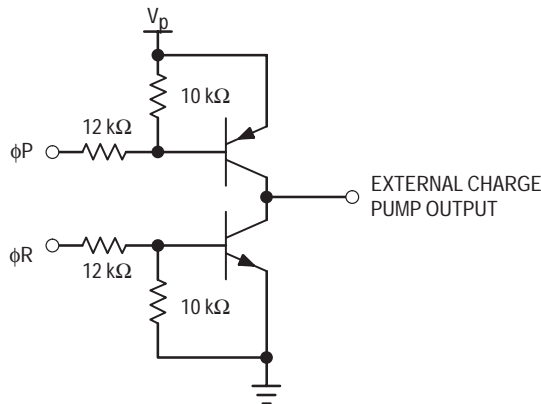
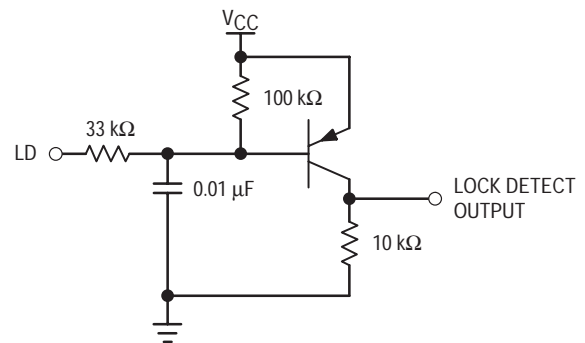
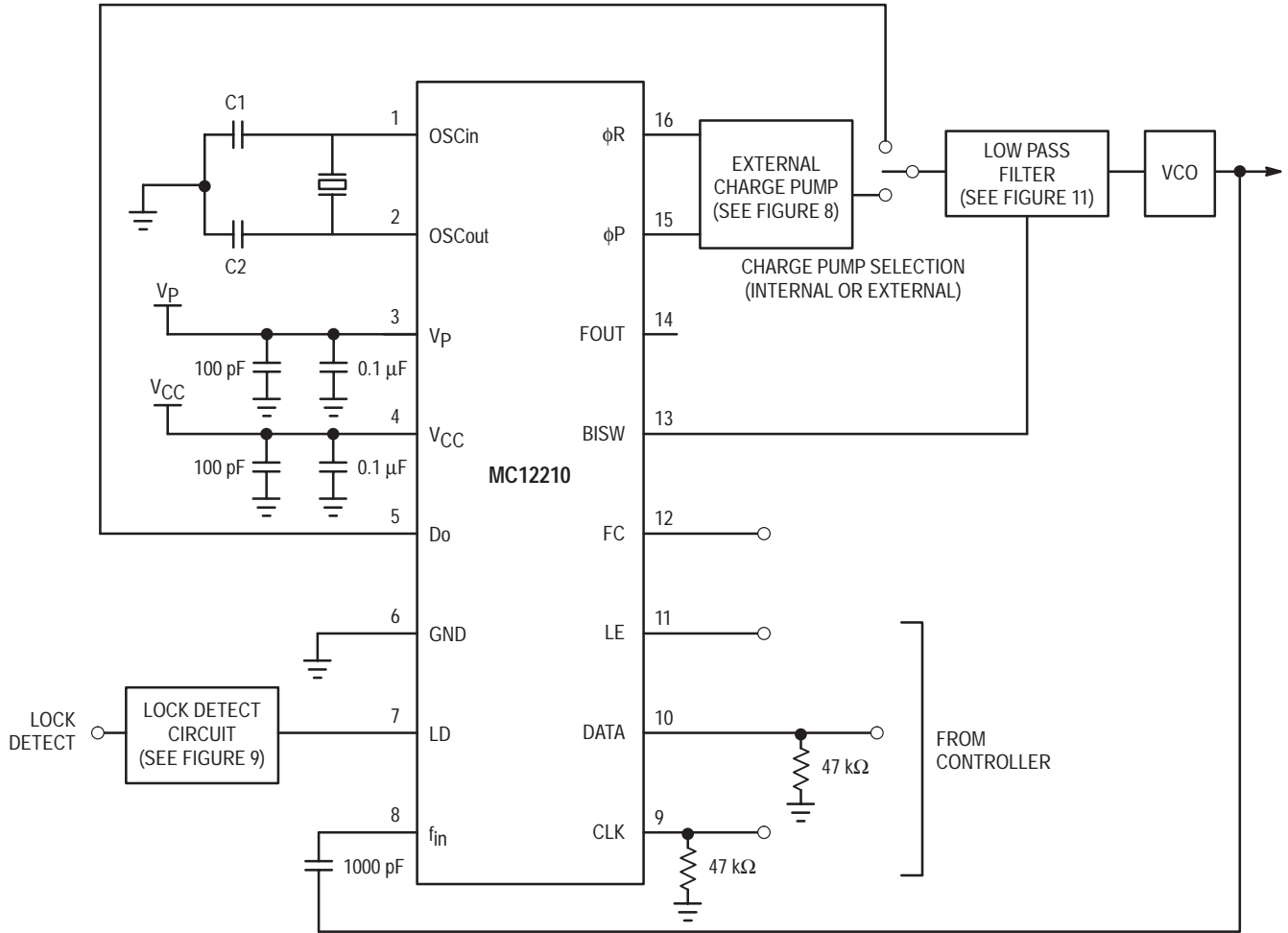


Figure 9. Typical Lock Detect Circuit



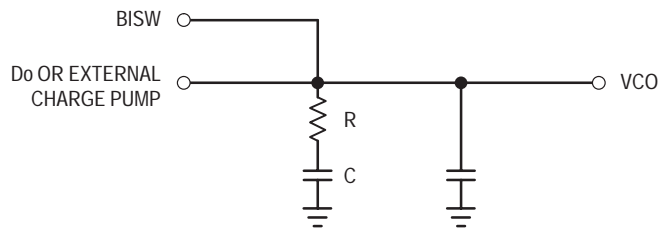
MC12210

Figure 10. Typical Applications Example (16-Pin Package)



C1, C2: Dependent on Crystal Oscillator

Figure 11. Typical Loop Filter





Phase-Frequency Detector

The MCH/K12140 is a phase frequency-detector intended for phase-locked loop applications which require a minimum amount of phase and frequency difference at lock. When used in conjunction with the MC12147, MC12148 or MC12149 VCO, a high bandwidth PLL can be realized. The device is functionally compatible with the MC12040 phase-frequency detector, however the MOSAIC™ III process is used to push the maximum frequency to 800 MHz and significantly reduce the dead zone of the detector. When the Reference (R) and VCO (V) inputs are unequal in frequency and/or phase, the differential UP (U) and DOWN (D) outputs will provide pulse streams which when subtracted and integrated provide an error voltage for control of a VCO.

The device is packaged in a small outline, surface mount 8-lead SOIC package. There are two versions of the device to provide I/O compatibility to the two existing ECL standards. The MCH12140 is compatible with MECL10H™ logic levels while the MCK12140 is compatible to 100K ECL logic levels. This device can also be used in +5.0 V systems. Please refer to Motorola Application Note AN1406/D, "Designing with PECL (ECL at +5.0 V)" for more information.

- 800 MHz Typical Bandwidth
- Small Outline 8-Lead SOIC Package
- 75 kΩ Internal Input Pulldown Resistors
- >1000 V ESD Protection

For proper operation, the input edge rate of the R and V inputs should be less than 5ns.

MOSAIC III and MECL 10H are trademarks of Motorola

MCH12140 MCK12140

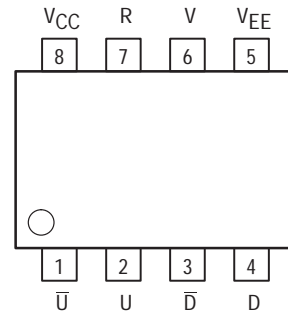
PHASE-FREQUENCY DETECTOR

SEMICONDUCTOR TECHNICAL DATA



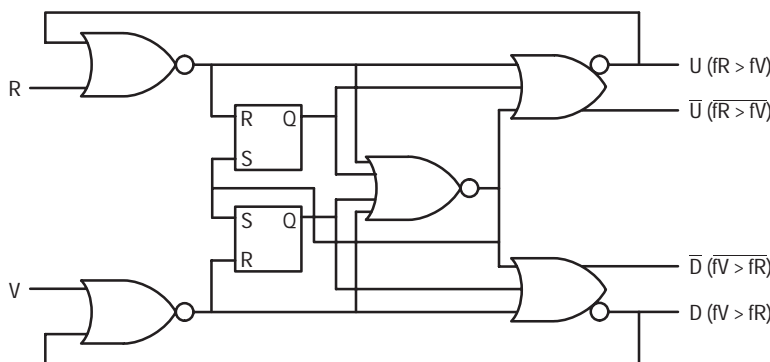
D SUFFIX
PLASTIC PACKAGE
CASE 751
(SO-8)

PIN CONNECTIONS



(Top View)

LOGIC DIAGRAM



ORDERING INFORMATION

Device	Operating Temperature Range	Package
MCH12140D	$T_A = -40^\circ \text{ to } +70^\circ \text{C}$	SO-8
MCK12140D		

MCH12140 MCK12140

TRUTH TABLE*

Input		Output				Input		Output			
R	V	U	D	\bar{U}	\bar{D}	R	V	U	D	\bar{U}	\bar{D}
0	0	X	X	X	X	1	1	0	0	1	1
0	1	X	X	X	X	1	0	0	0	1	1
1	1	X	X	X	X	1	1	0	1	1	0
0	1	X	X	X	X	1	0	0	1	1	0
1	1	1	0	0	1	1	1	0	1	1	0
0	1	1	0	0	1	0	1	0	1	1	0
1	1	1	0	0	1	1	1	0	1	1	0
1	0	1	0	0	1	1	1	0	0	1	1

NOTE: * This is not strictly a functional table; i.e., it does not cover all possible modes of operation. However, it gives a sufficient number of tests to ensure that the device will function properly.

H-SERIES DC CHARACTERISTICS ($V_{EE} = V_{EE}(\min) - V_{EE}(\max)$; $V_{CC} = GND^1$, unless otherwise noted.)

Characteristic	Symbol	-40°C		0°C		25°C		70°C		Unit
		Min	Max	Min	Max	Min	Max	Min	Max	
Output HIGH Voltage	V_{OH}	-1080	-890	-1020	-840	-980	-810	-910	-720	mV
Output LOW Voltage	V_{OL}	-1950	-1650	-1950	-1630	-1950	-1630	-1950	-1595	mV
Input HIGH Voltage	V_{IH}	-1230	-890	-1170	-840	-1130	-810	-1060	-720	mV
Input LOW Voltage	V_{IL}	-1950	-1500	-1950	-1480	-1950	-1480	-1950	-1445	mV
Input LOW Current	I_{IL}	0.5	—	0.5	—	0.5	—	0.3	—	μA

NOTE: 1. 10H circuits are designed to meet the DC specifications shown in the table after thermal equilibrium has been established. The circuit is in a test socket or mounted on a printed circuit board and transverse airflow greater than 500lpm is maintained. Outputs are terminated through a 50 Ω resistor to -2.0V except where otherwise specified on the individual data sheets.

K-SERIES DC CHARACTERISTICS ($V_{EE} = V_{EE}(\min) - V_{EE}(\max)$; $V_{CC} = GND^1$, unless otherwise noted.)

Characteristic	Symbol	-40°C			0°C to 70°C			Unit	Condition
		Min	Typ	Max	Min	Typ	Max		
Output HIGH Voltage	V_{OH}	-1085	-1005	-880	-1025	-955	-880	mV	$V_{IN} = V_{IH}(\max)$ or $V_{IL}(\min)$
Output LOW Voltage	V_{OL}	-1830	-1695	-1555	-1810	-1705	-1620	mV	
Output HIGH Voltage	V_{OHA}	-1095	—	—	-1035	—	—	mV	$V_{IN} = V_{IH}(\min)$ or $V_{IL}(\max)$
Output LOW Voltage	V_{OLA}	—	—	-1555	—	—	-1610	mV	
Input HIGH Voltage	V_{IH}	-1165	—	-880	-1165	—	-880	mV	
Input LOW Voltage	V_{IL}	-1810	—	-1475	-1810	—	-1475	mV	
Input LOW Current	I_{IL}	0.5	—	—	0.5	—	—	μA	$V_{IN} = V_{IL}(\max)$

NOTE: 1. This table replaces the three tables traditionally seen in ECL 100K data books. The same DC parameter values at $V_{EE} = -4.5V$ now apply across the full V_{EE} range of -4.2V to -5.5V. Outputs are terminated through a 50 Ω resistor to -2.0V except where otherwise specified on the individual data sheets.

ABSOLUTE MAXIMUM RATINGS (Note 1)

Characteristic	Symbol	Rating	Unit
Power Supply ($V_{CC} = 0V$)	V_{EE}	-8.0 to 0	VDC
Input Voltage ($V_{CC} = 0V$)	V_I	0 to -6.0	VDC
Output Current	I_{out}	50 100	mA
Operating Temperature Range	T_A	-40 to +70	°C
Operating Range ^{1,2}	V_{EE}	-5.7 to -4.2	V

NOTES: 1. Absolute maximum rating, beyond which, device life may be impaired, unless otherwise specified on an individual data sheet.

2. Parametric values specified at: H-Series: -4.20 V to -5.50 V

K-Series: -4.94 V to -5.50 V

3. ESD data available upon request.

MCH12140 MCK12140

DC CHARACTERISTICS ($V_{EE} = V_{EE(\min)} - V_{EE(\max)}$; $V_{CC} = \text{GND}$, unless otherwise noted.)

Characteristic	Symbol	-40°C			0°C			25°C			70°C			Unit
		Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
Power Supply Current	I_{EE}		45		38	45	52	38	45	52	38	45	52	mA
Power Supply Voltage	V_{EE}	-4.75	-5.2	-5.5	-4.75	-5.2	-5.5	-4.75	-5.2	-5.5	-4.75	-5.2	-5.5	V
Input HIGH Current	I_{IH}			150			150			150			150	μA

AC CHARACTERISTICS ($V_{EE} = V_{EE(\min)} - V_{EE(\max)}$; $V_{CC} = \text{GND}$, unless otherwise noted.)

Characteristic	Symbol	-40°C			0°C			25°C			70°C			Unit
		Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
Maximum Toggle Frequency	F_{MAX}		800		650	800		650	800		650	800		
Propagation Delay to Output	t_{PLH} t_{PHL}		440		320	440	580	320	440	580	360	480	620	ps
Output Rise/Fall Times	t_r t_f		225		100	225	350	100	225	350	100	225	350	ps

APPLICATIONS INFORMATION

The 12140 is a high speed digital circuit used as a phase comparator in an analog phase-locked loop. The device determines the "lead" or "lag" phase relationship and time difference between the leading edges of a VCO (V) signal and a Reference (R) input. Since these edges occur only once per cycle, the detector has a range of $\pm 2\pi$ radians.

The operation of the 12140 can best be described using the plots of Figure 1. Figure 1 plots the average value of \bar{U} , \bar{D} and the difference between \bar{U} and \bar{D} versus the phase difference between the V and R inputs.

There are four potential relationships between V and R: R lags or leads V and the frequency of R is less than or greater than the frequency of V. Under these four conditions the 12140 will function as follows:

R lags V in phase

When the R and V inputs are equal in frequency and the phase of R lags that of V the \bar{D} output will stay HIGH while the \bar{U} output will pulse from HIGH to LOW. The magnitude of the pulse will be proportional to the phase difference between the V and R inputs reaching a minimum 50% duty cycle under a 180° out of phase condition. The signal on \bar{D} indicates to the VCO to decrease in frequency to bring the loop into lock.

V frequency > R frequency

When the frequency of V is greater than that of R the 12140 behaves in a similar fashion as above. Again the signal on \bar{D} indicates that the VCO frequency must be decreased to bring the loop into lock.

R leads V in phase

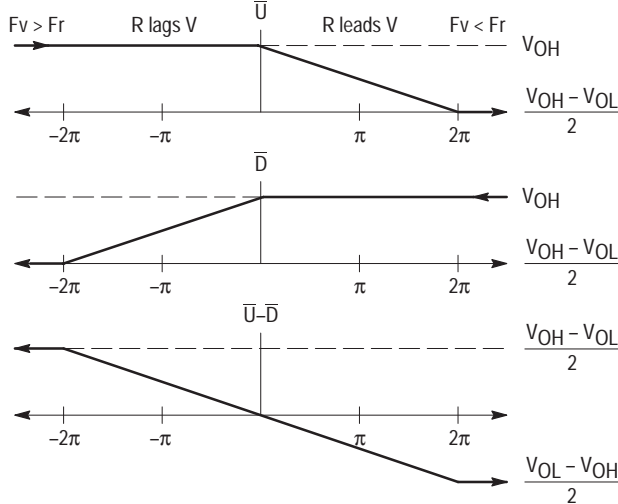
When the R and V inputs are equal in frequency and the phase of R leads that of V the \bar{U} output will pulse from HIGH to LOW. The magnitude of the pulse will be proportional to the phase difference between the V and R inputs reaching a minimum 50% duty cycle under a 180° out of phase condition. The signal on \bar{U} indicates to the VCO to increase in frequency to bring the loop into lock.

V frequency < R frequency

When the frequency of V is less than that of R the 12140 behaves in a similar fashion as above. Again the signal on \bar{U} indicates that the VCO frequency must be decreased to bring the loop into lock.

From Figure 1 when V and R are at the same frequency and in phase the value of $\bar{U} - \bar{D}$ is zero thus providing a zero error voltage to the VCO. This situation indicates the loop is in lock and the 12140 action will maintain the loop in its locked state.

Figure 1. Average Output Voltage versus Phase Difference



PLL Frequency Synthesizer Family

CMOS

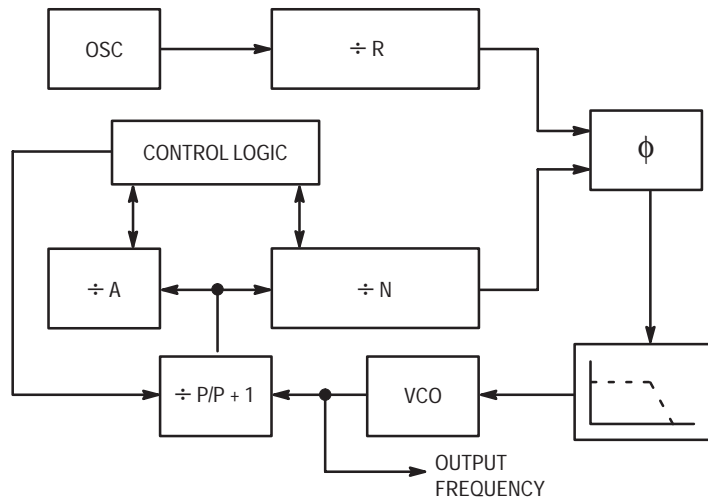
MC145151-2
MC145152-2
MC145157-2
MC145158-2

The devices described in this document are typically used as low-power, phase-locked loop frequency synthesizers. When combined with an external low-pass filter and voltage-controlled oscillator, these devices can provide all the remaining functions for a PLL frequency synthesizer operating up to the device's frequency limit. For higher VCO frequency operation, a down mixer or a prescaler can be used between the VCO and the synthesizer IC.

These frequency synthesizer chips can be found in the following and other applications:

CATV
AM/FM Radios
Two-Way Radios

TV Tuning
Scanning Receivers
Amateur Radio



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MC145151-2

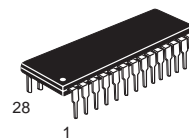
Parallel-Input PLL Frequency Synthesizer

Interfaces with Single-Modulus Prescalers

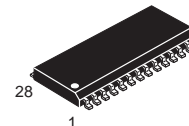
The MC145151-2 is programmed by 14 parallel-input data lines for the N counter and three input lines for the R counter. The device features consist of a reference oscillator, selectable-reference divider, digital-phase detector, and 14-bit programmable divide-by-N counter.

The MC145151-2 is an improved-performance drop-in replacement for the MC145151-1. The power consumption has decreased and ESD and latch-up performance have improved.

- Operating Temperature Range: - 40 to 85°C
- Low Power Consumption Through Use of CMOS Technology
- 3.0 to 9.0 V Supply Range
- On- or Off-Chip Reference Oscillator Operation
- Lock Detect Signal
- ÷ N Counter Output Available
- Single Modulus/Parallel Programming
- 8 User-Selectable ÷ R Values: 8, 128, 256, 512, 1024, 2048, 2410, 8192
- ÷ N Range = 3 to 16383
- "Linearized" Digital Phase Detector Enhances Transfer Function Linearity
- Two Error Signal Options: Single-Ended (Three-State) or Double-Ended
- Chip Complexity: 8000 FETs or 2000 Equivalent Gates



P SUFFIX
PLASTIC DIP
CASE 710



DW SUFFIX
SOG PACKAGE
CASE 751F

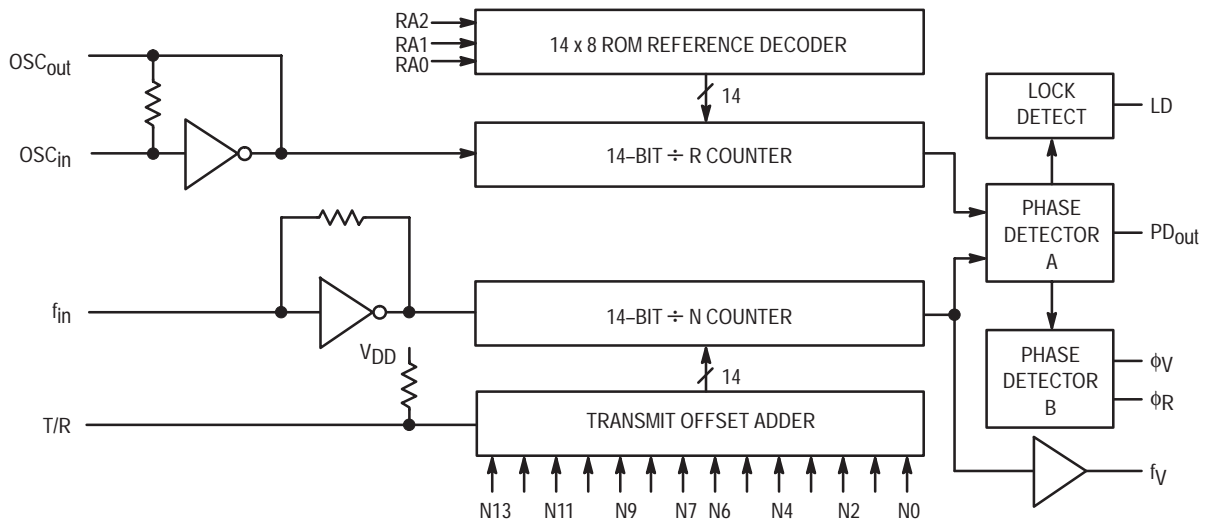
ORDERING INFORMATION

MC145151P2 Plastic DIP
MC145151DW2 SOG Package

PIN ASSIGNMENT

f_{in}	1	28	LD
V_{SS}	2	27	OSC _{in}
V_{DD}	3	26	OSC _{out}
PD _{out}	4	25	N11
RA0	5	24	N10
RA1	6	23	N13
RA2	7	22	N12
ϕ_R	8	21	T/R
ϕ_V	9	20	N9
f_V	10	19	N8
N0	11	18	N7
N1	12	17	N6
N2	13	16	N5
N3	14	15	N4

MC145151-2 BLOCK DIAGRAM



NOTE: N0 – N13 inputs and inputs RA0, RA1, and RA2 have pull-up resistors that are not shown.

PIN DESCRIPTIONS

INPUT PINS

f_{in} Frequency Input (Pin 1)

Input to the $\div N$ portion of the synthesizer. f_{in} is typically derived from loop VCO and is ac coupled into the device. For larger amplitude signals (standard CMOS logic levels) dc coupling may be used.

RA0 – RA2 Reference Address Inputs (Pins 5, 6, 7)

These three inputs establish a code defining one of eight possible divide values for the total reference divider, as defined by the table below.

Pull-up resistors ensure that inputs left open remain at a logic 1 and require only a SPST switch to alter data to the zero state.

Reference Address Code			Total Divide Value
RA2	RA1	RA0	
0	0	0	8
0	0	1	128
0	1	0	256
0	1	1	512
1	0	0	1024
1	0	1	2048
1	1	0	2410
1	1	1	8192

N0 – N11 N Counter Programming Inputs (Pins 11 – 20, 22 – 25)

These inputs provide the data that is preset into the $\div N$ counter when it reaches the count of zero. N0 is the least significant and N13 is the most significant. Pull-up resistors en-

sure that inputs left open remain at a logic 1 and require only an SPST switch to alter data to the zero state.

T/R Transmit/Receive Offset Adder Input (Pin 21)

This input controls the offset added to the data provided at the N inputs. This is normally used for offsetting the VCO frequency by an amount equal to the IF frequency of the transceiver. This offset is fixed at 856 when T/R is low and gives no offset when T/R is high. A pull-up resistor ensures that no connection will appear as a logic 1 causing no offset addition.

OSCin, OSCout Reference Oscillator Input/Output (Pins 27, 26)

These pins form an on-chip reference oscillator when connected to terminals of an external parallel resonant crystal. Frequency setting capacitors of appropriate value must be connected from OSCin to ground and OSCout to ground. OSCin may also serve as the input for an externally-generated reference signal. This signal is typically ac coupled to OSCin, but for larger amplitude signals (standard CMOS logic levels) dc coupling may also be used. In the external reference mode, no connection is required to OSCout.

OUTPUT PINS

PDout Phase Detector A Output (Pin 4)

Three-state output of phase detector for use as loop-error signal. Double-ended outputs are also available for this purpose (see ϕ_V and ϕ_R).

Frequency $f_V > f_R$ or f_V Leading: Negative Pulses

Frequency $f_V < f_R$ or f_V Lagging: Positive Pulses

Frequency $f_V = f_R$ and Phase Coincidence: High-Impedance State

ϕ_R , ϕ_V

Phase Detector B Outputs (Pins 8, 9)

These phase detector outputs can be combined externally for a loop-error signal. A single-ended output is also available for this purpose (see **PD_{out}**).

If frequency f_V is greater than f_R or if the phase of f_V is leading, then error information is provided by ϕ_V pulsing low. ϕ_R remains essentially high.

If the frequency f_V is less than f_R or if the phase of f_V is lagging, then error information is provided by ϕ_R pulsing low. ϕ_V remains essentially high.

If the frequency of $f_V = f_R$ and both are in phase, then both ϕ_V and ϕ_R remain high except for a small minimum time period when both pulse low in phase.

f_V

N Counter Output (Pin 10)

This is the buffered output of the $\div N$ counter that is inter-

nally connected to the phase detector input. With this output available, the $\div N$ counter can be used independently.

LD

Lock Detector Output (Pin 28)

Essentially a high level when loop is locked (f_R , f_V of same phase and frequency). Pulses low when loop is out of lock.

POWER SUPPLY

V_{DD}

Positive Power Supply (Pin 3)

The positive power supply potential. This pin may range from +3 to +9 V with respect to V_{SS} .

V_{SS}

Negative Power Supply (Pin 2)

The most negative supply potential. This pin is usually ground.

TYPICAL APPLICATIONS

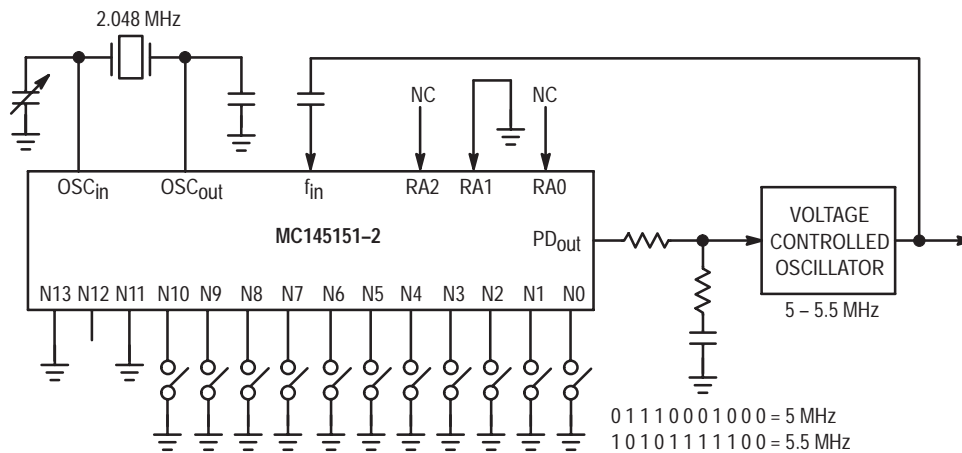
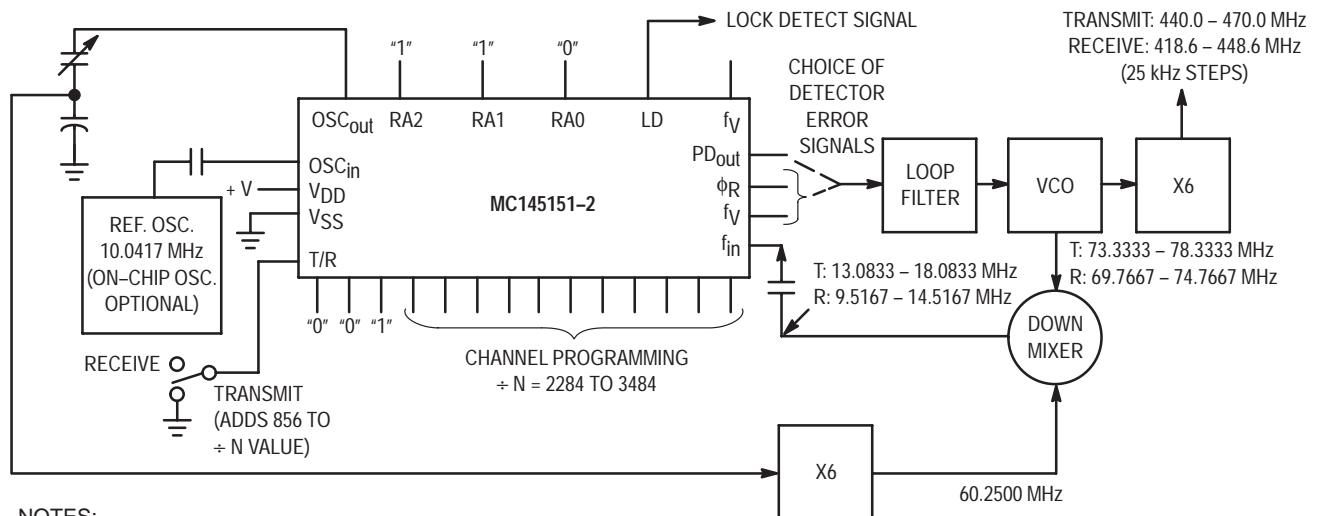


Figure 1. 5 MHz to 5.5 MHz Local Oscillator Channel Spacing = 1 kHz



NOTES:

1. $f_R = 4.1667$ kHz; $\div R = 2410$; 21.4 MHz low side injection during receive.
2. Frequency values shown are for the 440 - 470 MHz band. Similar implementation applies to the 406 - 440 MHz band. For 470 - 512 MHz, consider reference oscillator frequency X9 for mixer injection signal (90.3750 MHz).

Figure 2. Synthesizer for Land Mobile Radio UHF Bands

MC145151-2 Data Sheet Continued on Page 4.2-91

MC145152-2

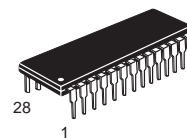
Parallel-Input PLL Frequency Synthesizer

Interfaces with Dual-Modulus Prescalers

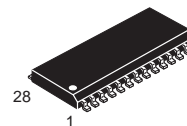
The MC145152-2 is programmed by sixteen parallel inputs for the N and A counters and three input lines for the R counter. The device features consist of a reference oscillator, selectable-reference divider, two-output phase detector, 10-bit programmable divide-by-N counter, and 6-bit programmable ÷ A counter.

The MC145152-2 is an improved-performance drop-in replacement for the MC145152-1. Power consumption has decreased and ESD and latch-up performance have improved.

- Operating Temperature Range: - 40 to 85°C
- Low Power Consumption Through Use of CMOS Technology
- 3.0 to 9.0 V Supply Range
- On- or Off-Chip Reference Oscillator Operation
- Lock Detect Signal
- Dual Modulus/Parallel Programming
- 8 User-Selectable ÷ R Values: 8, 64, 128, 256, 512, 1024, 1160, 2048
- ÷ N Range = 3 to 1023, ÷ A Range = 0 to 63
- Chip Complexity: 8000 FETs or 2000 Equivalent Gates
- See Application Note AN980



P SUFFIX
PLASTIC DIP
CASE 710



DW SUFFIX
SOG PACKAGE
CASE 751F

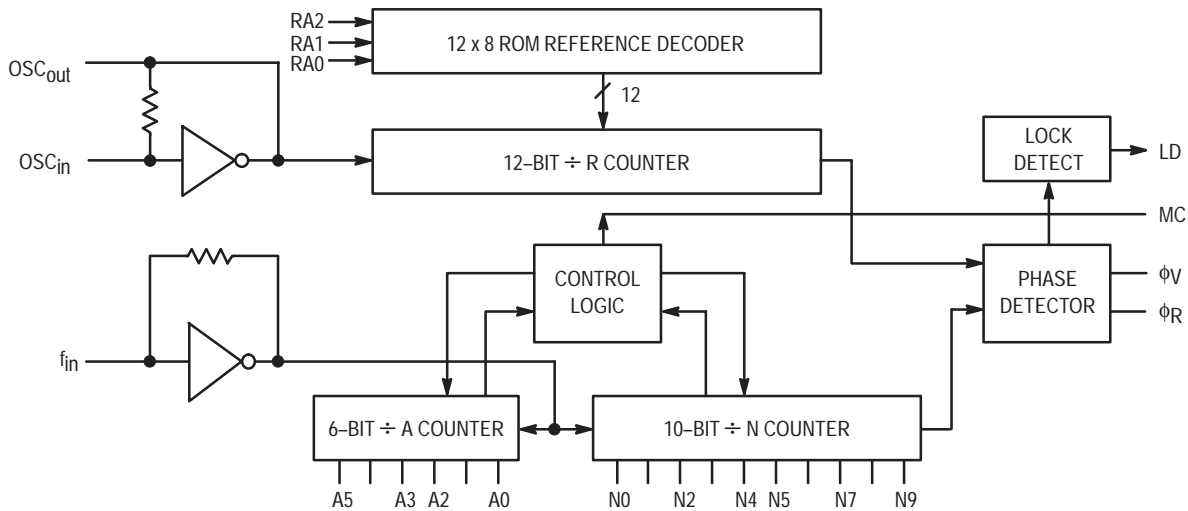
ORDERING INFORMATION

MC145152P2 Plastic DIP
MC145152DW2 SOG Package

PIN ASSIGNMENT

f_{in}	1	28	LD
VSS	2	27	OSC _{in}
V _{DD}	3	26	OSC _{out}
RA0	4	25	A4
RA1	5	24	A3
RA2	6	23	A0
ϕ_R	7	22	A2
ϕ_V	8	21	A1
MC	9	20	N9
A5	10	19	N8
N0	11	18	N7
N1	12	17	N6
N2	13	16	N5
N3	14	15	N4

MC145152-2 BLOCK DIAGRAM



NOTE: N0 – N9, A0 – A5, and RA0 – RA2 have pull-up resistors that are not shown.

PIN DESCRIPTIONS

INPUT PINS

f_{in} Frequency Input (Pin 1)

Input to the positive edge triggered $\div N$ and $\div A$ counters. f_{in} is typically derived from a dual-modulus prescaler and is ac coupled into the device. For larger amplitude signals (standard CMOS logic levels) dc coupling may be used.

RA0, RA1, RA2 Reference Address Inputs (Pins 4, 5, 6)

These three inputs establish a code defining one of eight possible divide values for the total reference divider. The total reference divide values are as follows:

Reference Address Code			Total Divide Value
RA2	RA1	RA0	
0	0	0	8
0	0	1	64
0	1	0	128
0	1	1	256
1	0	0	512
1	0	1	1024
1	1	0	1160
1	1	1	2048

N0 – N9 N Counter Programming Inputs (Pins 11 – 20)

The N inputs provide the data that is preset into the $\div N$ counter when it reaches the count of 0. N0 is the least significant digit and N9 is the most significant. Pull-up resistors ensure that inputs left open remain at a logic 1 and require only a SPST switch to alter data to the zero state.

A0 – A5 A Counter Programming Inputs (Pins 23, 21, 22, 24, 25, 10)

The A inputs define the number of clock cycles of f_{in} that require a logic 0 on the MC output (see **Dual-Modulus**

Prescaling section). The A inputs all have internal pull-up resistors that ensure that inputs left open will remain at a logic 1.

OSC_in, OSC_out Reference Oscillator Input/Output (Pins 27, 26)

These pins form an on-chip reference oscillator when connected to terminals of an external parallel resonant crystal. Frequency setting capacitors of appropriate value must be connected from OSC_{IN} to ground and OSC_{OUT} to ground. OSC_{IN} may also serve as the input for an externally-generated reference signal. This signal is typically ac coupled to OSC_{IN}, but for larger amplitude signals (standard CMOS logic levels) dc coupling may also be used. In the external reference mode, no connection is required to OSC_{OUT}.

OUTPUT PINS

ϕ_R , ϕ_V Phase Detector B Outputs (Pins 7, 8)

These phase detector outputs can be combined externally for a loop-error signal.

If the frequency f_V is greater than f_R or if the phase of f_V is leading, then error information is provided by ϕ_V pulsing low. ϕ_R remains essentially high.

If the frequency f_V is less than f_R or if the phase of f_V is lagging, then error information is provided by ϕ_R pulsing low. ϕ_V remains essentially high.

If the frequency of $f_V = f_R$ and both are in phase, then both ϕ_V and ϕ_R remain high except for a small minimum time period when both pulse low in phase.

MC Dual-Modulus Prescale Control Output (Pin 9)

Signal generated by the on-chip control logic circuitry for controlling an external dual-modulus prescaler. The MC level will be low at the beginning of a count cycle and will remain low until the $\div A$ counter has counted down from its programmed value. At this time, MC goes high and remains high until the $\div N$ counter has counted the rest of the way down from its programmed value ($N - A$ additional counts since both $\div N$ and $\div A$ are counting down during the first

portion of the cycle). MC is then set back low, the counters preset to their respective programmed values, and the above sequence repeated. This provides for a total programmable divide value (N_T) = $N \cdot P + A$ where P and P + 1 represent the dual-modulus prescaler divide values respectively for high and low MC levels, N the number programmed into the ÷ N counter, and A the number programmed into the ÷ A counter.

LD
Lock Detector Output (Pin 28)

Essentially a high level when loop is locked (f_R , f_V of same phase and frequency). Pulses low when loop is out of lock.

POWER SUPPLY

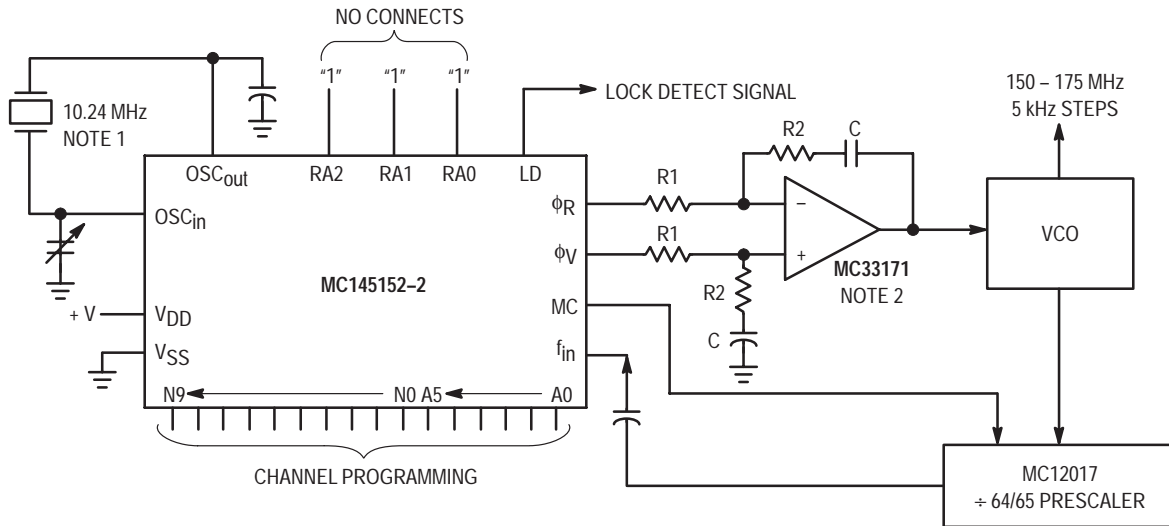
V_{DD}
Positive Power Supply (Pin 3)

The positive power supply potential. This pin may range from + 3 to + 9 V with respect to V_{SS}.

V_{SS}
Negative Power Supply (Pin 2)

The most negative supply potential. This pin is usually ground.

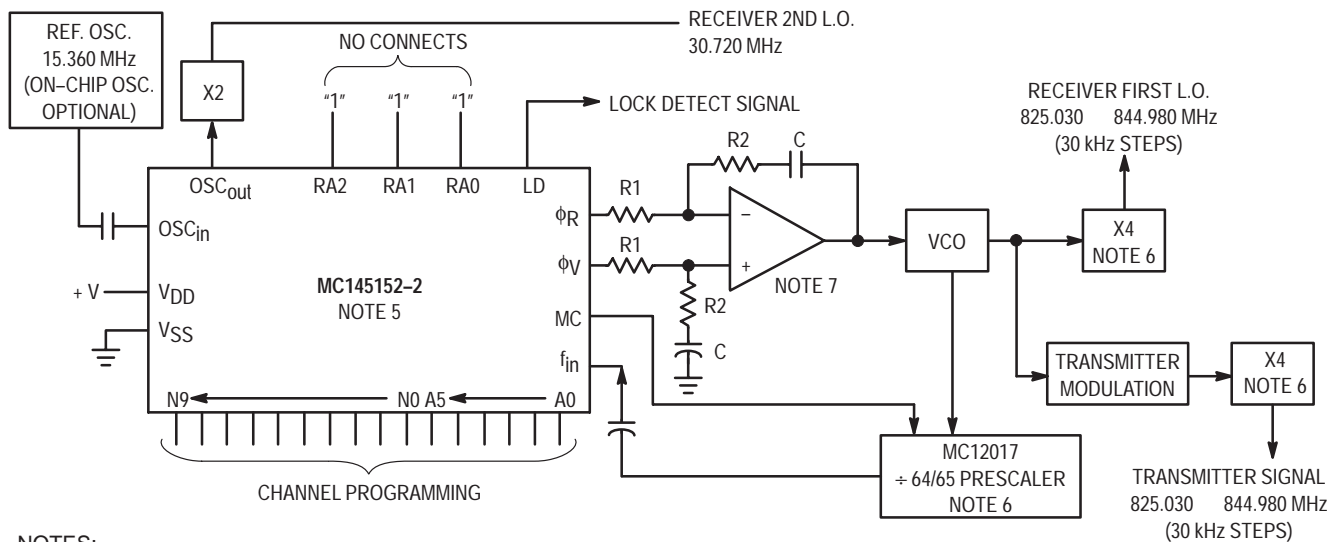
TYPICAL APPLICATIONS



NOTES:

1. Off-chip oscillator optional.
2. The ϕ_R and ϕ_V outputs are fed to an external combiner/loop filter. See the Phase-Locked Loop — Low-Pass Filter Design page for additional information. The ϕ_R and ϕ_V outputs swing rail-to-rail. Therefore, the user should be careful not to exceed the common mode input range of the op amp used in the combiner/loop filter.

Figure 1. Synthesizer for Land Mobile Radio VHF Bands



NOTES:

1. Receiver 1st I.F. = 45 MHz, low side injection; Receiver 2nd I.F. = 11.7 MHz, low side injection.
2. Duplex operation with 45 MHz receiver/transmit separation.
3. $f_R = 7.5 \text{ kHz}$; $\div R = 2048$.
4. $N_{\text{total}} = N \cdot 64 + A = 27501 \text{ to } 28166$; $N = 429 \text{ to } 440$; $A = 0 \text{ to } 63$.
5. MC145158-2 may be used where serial data entry is desired.
6. High frequency prescalers (e.g., MC12018 [520 MHz] and MC12022 [1 GHz]) may be used for higher frequency VCO and f_{ref} implementations.
7. The ϕ_R and ϕ_V outputs are fed to an external combiner/loop filter. See the Phase-Locked Loop — Low-Pass Filter Design page for additional information. The ϕ_R and ϕ_V outputs swing rail-to-rail. Therefore, the user should be careful not to exceed the common mode input range of the op amp used in the combiner/loop filter.

Figure 2. 666-Channel, Computer-Controlled, Mobile Radiotelephone Synthesizer for 800 MHz Cellular Radio Systems

MC145157-2

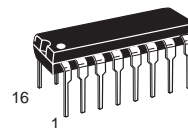
Serial-Input PLL Frequency Synthesizer

Interfaces with Single-Modulus Prescalers

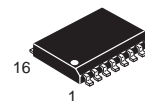
The MC145157-2 has a fully programmable 14-bit reference counter, as well as a fully programmable $\div N$ counter. The counters are programmed serially through a common data input and latched into the appropriate counter latch, according to the last data bit (control bit) entered.

The MC145157-2 is an improved-performance drop-in replacement for the MC145157-1. Power consumption has decreased and ESD and latch-up performance have improved.

- Operating Temperature Range: - 40 to 85°C
- Low Power Consumption Through Use of CMOS Technology
- 3.0 to 9.0 V Supply Range
- Fully Programmable Reference and $\div N$ Counters
- $\div R$ Range = 3 to 16383
- $\div N$ Range = 3 to 16383
- f_V and f_R Outputs
- Lock Detect Signal
- Compatible with the Serial Peripheral Interface (SPI) on CMOS MCUs
- "Linearized" Digital Phase Detector
- Single-Ended (Three-State) or Double-Ended Phase Detector Outputs
- Chip Complexity: 6504 FETs or 1626 Equivalent Gates



P SUFFIX
PLASTIC DIP
CASE 648



DW SUFFIX
SOG PACKAGE
CASE 751G

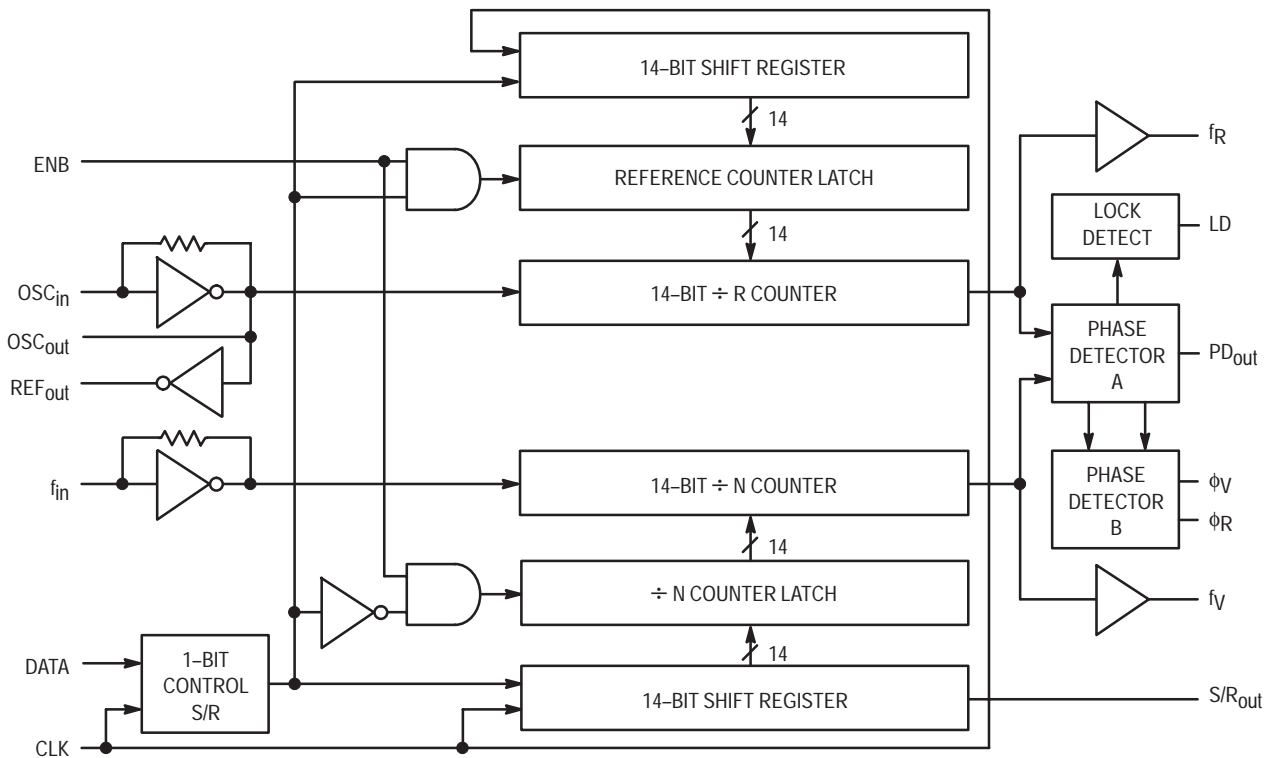
ORDERING INFORMATION

MC145157P2 Plastic DIP
MC145157DW2 SOG Package

PIN ASSIGNMENT

OSC _{in}	1	16	ϕ_R
OSC _{out}	2	15	ϕ_V
f_V	3	14	REF _{out}
V _{DD}	4	13	f_R
PD _{out}	5	12	S/R _{out}
V _{SS}	6	11	ENB
LD	7	10	DATA
f_{in}	8	9	CLK

MC145157-2 BLOCK DIAGRAM



PIN DESCRIPTIONS

INPUT PINS

f_{in} Frequency Input (Pin 8)

Input frequency from VCO output. A rising edge signal on this input decrements the $\div N$ counter. This input has an inverter biased in the linear region to allow use with ac coupled signals as low as 500 mV p-p. For larger amplitude signals (standard CMOS logic levels), dc coupling may be used.

CLK, DATA Shift Clock, Serial Data Inputs (Pins 9, 10)

Each low-to-high transition of the clock shifts one bit of data into the on-chip shift registers. The last data bit entered determines which counter storage latch is activated; a logic 1 selects the reference counter latch and a logic 0 selects the $\div N$ counter latch. The entry format is as follows:



ENB Latch Enable Input (Pin 11)

A logic high on this pin latches the data from the shift register into the reference divider or $\div N$ latches depending on the control bit. The reference divider latches are activated if the control bit is at a logic high and the $\div N$ latches are activated

if the control bit is at a logic low. A logic low on this pin allows the user to change the data in the shift registers without affecting the counters. ENB is normally low and is pulsed high to transfer data to the latches.

OSCin, OSCout Reference Oscillator Input/Output (Pins 1, 2)

These pins form an on-chip reference oscillator when connected to terminals of an external parallel resonant crystal. Frequency setting capacitors of appropriate value must be connected from OSCin to ground and OSCout to ground. OSCin may also serve as the input for an externally-generated reference signal. This signal is typically ac coupled to OSCin, but for larger amplitude signals (standard CMOS logic levels) dc coupling may also be used. In the external reference mode, no connection is required to OSCout.

OUTPUT PINS

PDout Single-Ended Phase Detector A Output (Pin 5)

This single-ended (three-state) phase detector output produces a loop-error signal that is used with a loop filter to control a VCO.

- Frequency $f_V > f_R$ or f_V Leading: Negative Pulses
- Frequency $f_V < f_R$ or f_V Lagging: Positive Pulses
- Frequency $f_V = f_R$ and Phase Coincidence: High-Impedance State

ϕ_R, ϕ_V Double-Ended Phase Detector B Outputs (Pins 16, 15)

These outputs can be combined externally for a loop-error signal. A single-ended output is also available for this purpose (see PDout).

If frequency f_V is greater than f_R or if the phase of f_V is leading, then error information is provided by ϕ_V pulsing low. ϕ_R remains essentially high.

If the frequency f_V is less than f_R or if the phase of f_V is lagging, then error information is provided by ϕ_R pulsing low. ϕ_V remains essentially high.

If the frequency of $f_V = f_R$ and both are in phase, then both ϕ_V and ϕ_R remain high except for a small minimum time period when both pulse low in phase.

f_R, f_V

R Counter Output, N Counter Output (Pins 13, 3)

Buffered, divided reference and f_{in} frequency outputs. The f_R and f_V outputs are connected internally to the $\div R$ and $\div N$ counter outputs respectively, allowing the counters to be used independently, as well as monitoring the phase detector inputs.

LD

Lock Detector Output (Pin 7)

This output is essentially at a high level when the loop is locked (f_R, f_V of same phase and frequency), and pulses low when loop is out of lock.

REF_{out}

Buffered Reference Oscillator Output (Pin 14)

This output can be used as a second local oscillator, reference oscillator to another frequency synthesizer, or as the system clock to a microprocessor controller.

S/R_{out}

Shift Register Output (Pin 12)

This output can be connected to an external shift register to provide band switching, control information, and counter programming code checking.

POWER SUPPLY

V_{DD}

Positive Power Supply (Pin 4)

The positive power supply potential. This pin may range from +3 to +9 V with respect to V_{SS} .

V_{SS}

Negative Power Supply (Pin 6)

The most negative supply potential. This pin is usually ground.

MC145158-2

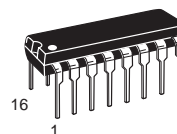
Serial-Input PLL Frequency Synthesizer

Interfaces with Dual-Modulus Prescalers

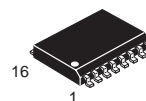
The MC145158-2 has a fully programmable 14-bit reference counter, as well as fully programmable $\div N$ and $\div A$ counters. The counters are programmed serially through a common data input and latched into the appropriate counter latch, according to the last data bit (control bit) entered.

The MC145158-2 is an improved-performance drop-in replacement for the MC145158-1. Power consumption has decreased and ESD and latch-up performance have improved.

- Operating Temperature Range: -40 to 85°C
- Low Power Consumption Through Use of CMOS Technology
- 3.0 to 9.0 V Supply Range
- Fully Programmable Reference and $\div N$ Counters
- $\div R$ Range = 3 to 16383
- $\div N$ Range = 3 to 1023
- Dual Modulus Capability; $\div A$ Range = 0 to 127
- f_V and f_R Outputs
- Lock Detect Signal
- Compatible with the Serial Peripheral Interface (SPI) on CMOS MCUs
- "Linearized" Digital Phase Detector
- Single-Ended (Three-State) or Double-Ended Phase Detector Outputs
- Chip Complexity: 6504 FETs or 1626 Equivalent Gates



P SUFFIX
PLASTIC DIP
CASE 648



DW SUFFIX
SOG PACKAGE
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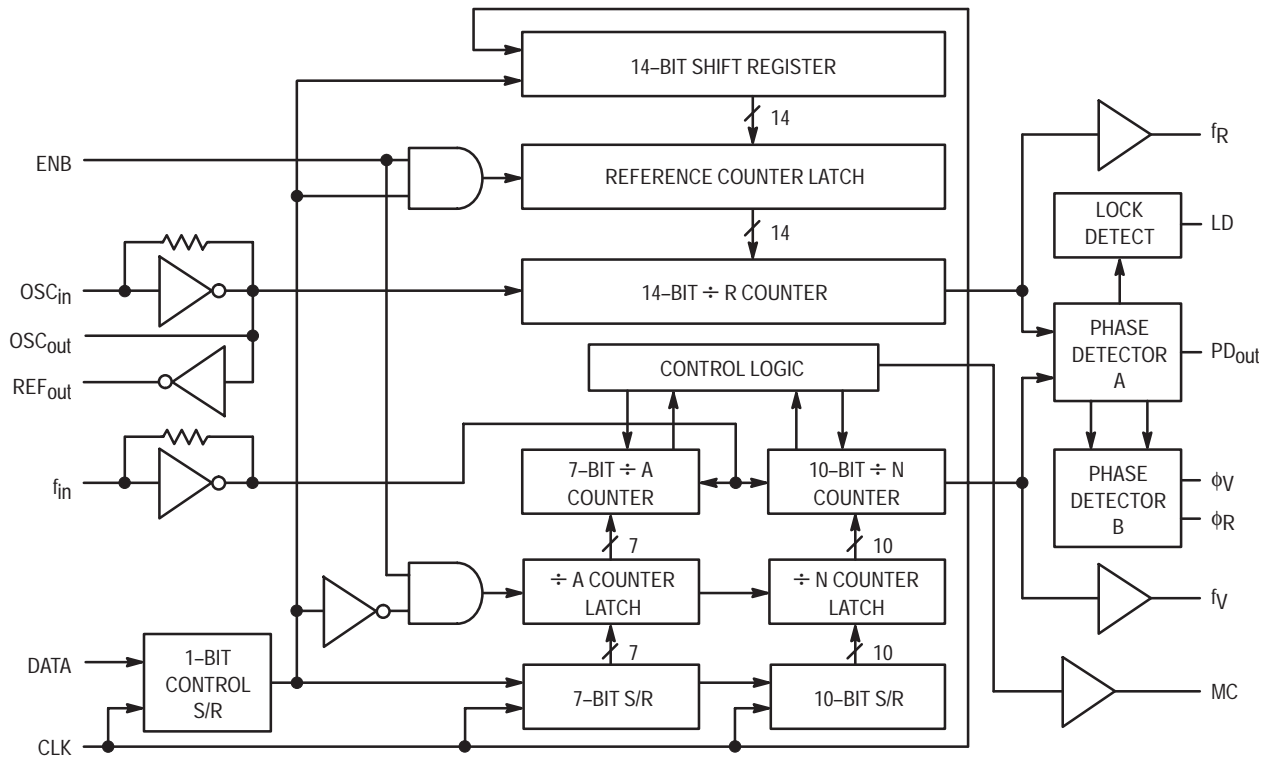
ORDERING INFORMATION

MC145158P2	Plastic DIP
MC145158DW2	SOG Package

PIN ASSIGNMENT

OSC _{in}	1	16	ϕ_R
OSC _{out}	2	15	ϕ_V
f_V	3	14	REF _{out}
V _{DD}	4	13	f_R
PD _{out}	5	12	MC
V _{SS}	6	11	ENB
LD	7	10	DATA
f_{in}	8	9	CLK

MC145158-2 BLOCK DIAGRAM



PIN DESCRIPTIONS

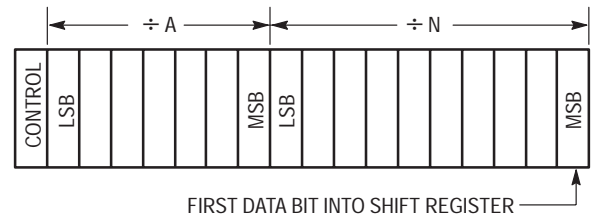
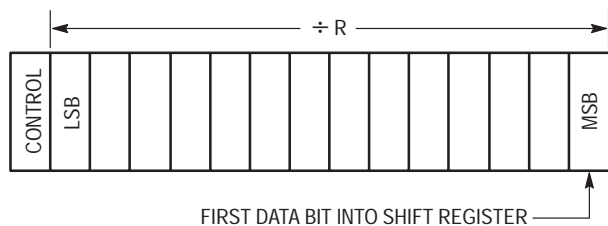
INPUT PINS

f_{in} Frequency Input (Pin 8)

Input frequency from VCO output. A rising edge signal on this input decrements the $\div A$ and $\div N$ counters. This input has an inverter biased in the linear region to allow use with ac coupled signals as low as 500 mV p-p. For larger amplitude signals (standard CMOS logic levels), dc coupling may be used.

CLK, DATA Shift Clock, Serial Data Inputs (Pins 9, 10)

Each low-to-high transition of the CLK shifts one bit of data into the on-chip shift registers. The last data bit entered determines which counter storage latch is activated; a logic 1 selects the reference counter latch and a logic 0 selects the $\div A$, $\div N$ counter latch. The data entry format is as follows:



ENB Latch Enable Input (Pin 11)

A logic high on this pin latches the data from the shift register into the reference divider or $\div N$, $\div A$ latches depending on the control bit. The reference divider latches are activated if the control bit is at a logic high and the $\div N$, $\div A$ latches are activated if the control bit is at a logic low. A logic low on this pin allows the user to change the data in the shift registers without affecting the counters. ENB is normally low and is pulsed high to transfer data to the latches.

OSCin, OSCout Reference Oscillator Input/Output (Pins 1, 2)

These pins form an on-chip reference oscillator when connected to terminals of an external parallel resonant crystal. Frequency setting capacitors of appropriate value must be connected from OSCin to ground and OSCout to ground. OSCin may also serve as the input for an externally-generated reference signal. This signal is typically ac coupled to OSCin, but for larger amplitude signals (standard CMOS logic levels) dc coupling may also be used. In the external reference mode, no connection is required to OSCout.

OUTPUT PINS

PD_{out}

Phase Detector A Output (Pin 5)

This single-ended (three-state) phase detector output produces a loop-error signal that is used with a loop filter to control a VCO.

Frequency $f_V > f_R$ or f_V Leading: Negative Pulses

Frequency $f_V < f_R$ or f_V Lagging: Positive Pulses

Frequency $f_V = f_R$ and Phase Coincidence: High-Impedance State

ϕ_R, ϕ_V

Phase Detector B Outputs (Pins 16, 15)

Double-ended phase detector outputs. These outputs can be combined externally for a loop-error signal. A single-ended output is also available for this purpose (see PD_{out}).

If frequency f_V is greater than f_R or if the phase of f_V is leading, then error information is provided by ϕ_V pulsing low. ϕ_R remains essentially high.

If the frequency f_V is less than f_R or if the phase of f_V is lagging, then error information is provided by ϕ_R pulsing low. ϕ_V remains essentially high.

If the frequency of $f_V = f_R$ and both are in phase, then both ϕ_V and ϕ_R remain high except for a small minimum time period when both pulse low in phase.

MC

Dual-Modulus Prescale Control Output (Pin 12)

This output generates a signal by the on-chip control logic circuitry for controlling an external dual-modulus prescaler. The MC level is low at the beginning of a count cycle and remains low until the $\div A$ counter has counted down from its programmed value. At this time, MC goes high and remains high until the $\div N$ counter has counted the rest of the way down from its programmed value ($N - A$ additional counts since both $\div N$ and $\div A$ are counting down during the first portion of the cycle). MC is then set back low, the counters preset to their respective programmed values, and the above sequence repeated. This provides for a total programmable divide value (N_T) = $N \cdot P + A$ where P and $P + 1$ represent the

dual-modulus prescaler divide values respectively for high and low modulus control levels, N the number programmed into the $\div N$ counter, and A the number programmed into the $\div A$ counter. Note that when a prescaler is needed, the dual-modulus version offers a distinct advantage. The dual-modulus prescaler allows a higher reference frequency at the phase detector input, increasing system performance capability, and simplifying the loop filter design.

f_R, f_V

R Counter Output, N Counter Output (Pins 13, 3)

Buffered, divided reference and f_{in} frequency outputs. The f_R and f_V outputs are connected internally to the $\div R$ and $\div N$ counter outputs respectively, allowing the counters to be used independently, as well as monitoring the phase detector inputs.

LD

Lock Detector Output (Pin 7)

This output is essentially at a high level when the loop is locked (f_R, f_V of same phase and frequency), and pulses low when loop is out of lock.

REF_{out}

Buffered Reference Oscillator Output (Pin 14)

This output can be used as a second local oscillator, reference oscillator to another frequency synthesizer, or as the system clock to a microprocessor controller.

POWER SUPPLY

V_{DD}

Positive Power Supply (Pin 4)

The positive power supply potential. This pin may range from +3 to +9 V with respect to V_{SS}.

V_{SS}

Negative Power Supply (Pin 6)

The most negative supply potential. This pin is usually ground.

MC14515X–2 FAMILY CHARACTERISTICS AND DESCRIPTIONS

MAXIMUM RATINGS* (Voltages Referenced to V_{SS})

Symbol	Parameter	Value	Unit
V _{DD}	DC Supply Voltage	– 0.5 to + 10.0	V
V _{in} , V _{out}	Input or Output Voltage (DC or Transient) except SW1, SW2	– 0.5 to V _{DD} + 0.5	V
V _{out}	Output Voltage (DC or Transient), SW1, SW2 (R _{pull-up} = 4.7 kΩ)	– 0.5 to + 15	V
I _{in} , I _{out}	Input or Output Current (DC or Transient), per Pin	± 10	mA
I _{DD} , I _{SS}	Supply Current, V _{DD} or V _{SS} Pins	± 30	mA
P _D	Power Dissipation, per Package†	500	mW
T _{stg}	Storage Temperature	– 65 to + 150	°C
T _L	Lead Temperature, 1 mm from Case for 10 seconds	260	°C

* Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section.

† Power Dissipation Temperature Derating:

Plastic DIP: – 12 mW/°C from 65 to 85°C

SOG Package: – 7 mW/°C from 65 to 85°C

These devices contain protection circuitry to protect against damage due to high static voltages or electric fields. However, precautions must be taken to avoid applications of any voltage higher than maximum rated voltages to these high-impedance circuits. For proper operation, V_{in} and V_{out} should be constrained to the range V_{SS} ≤ (V_{in} or V_{out}) ≤ V_{DD} except for SW1 and SW2.

SW1 and SW2 can be tied through external resistors to voltages as high as 15 V, independent of the supply voltage.

Unused inputs must always be tied to an appropriate logic voltage level (e.g., either V_{SS} or V_{DD}), except for inputs with pull-up devices. Unused outputs must be left open.

ELECTRICAL CHARACTERISTICS (Voltages Referenced to V_{SS})

Symbol	Parameter	Test Condition	V _{DD} V	– 40°C		25°C		85°C		Unit
				Min	Max	Min	Max	Min	Max	
V _{DD}	Power Supply Voltage Range		—	3	9	3	9	3	9	V
I _{SS}	Dynamic Supply Current	f _{in} = OSC _{in} = 10 MHz, 1 V p-p ac coupled sine wave R = 128, A = 32, N = 128	3 5 9	— — —	3.5 10 30	— — —	3 7.5 24	— — —	3 7.5 24	mA
I _{SS}	Quiescent Supply Current (not including pull-up current component)	V _{in} = V _{DD} or V _{SS} I _{out} = 0 μA	3 5 9	— — —	800 1200 1600	— — —	800 1200 1600	— — —	1600 2400 3200	μA
V _{in}	Input Voltage — f _{in} , OSC _{in}	Input ac coupled sine wave	—	500	—	500	—	500	—	mV p-p
V _{IL}	Low-Level Input Voltage — f _{in} , OSC _{in}	V _{out} ≥ 2.1 V Input dc V _{out} ≥ 3.5 V coupled V _{out} ≥ 6.3 V square wave	3 5 9	— — —	0 0 0	— — —	0 0 0	— — —	0 0 0	V
V _{IH}	High-Level Input Voltage — f _{in} , OSC _{in}	V _{out} ≤ 0.9 V Input dc V _{out} ≤ 1.5 V coupled V _{out} ≤ 2.7 V square wave	3 5 9	3.0 5.0 9.0	— — —	3.0 5.0 9.0	— — —	3.0 5.0 9.0	— — —	V
V _{IL}	Low-Level Input Voltage — except f _{in} , OSC _{in}		3 5 9	— — —	0.9 1.5 2.7	— — —	0.9 1.5 2.7	— — —	0.9 1.5 2.7	V
V _{IH}	High-Level Input Voltage — except f _{in} , OSC _{in}		3 5 9	2.1 3.5 6.3	— — —	2.1 3.5 6.3	— — —	2.1 3.5 6.3	— — —	V
I _{in}	Input Current (f _{in} , OSC _{in})	V _{in} = V _{DD} or V _{SS}	9	± 2	± 50	± 2	± 25	± 2	± 22	μA
I _{IL}	Input Leakage Current (Data, CLK, ENB — without pull-ups)	V _{in} = V _{SS}	9	—	– 0.3	—	– 0.1	—	– 1.0	μA
I _{IH}	Input Leakage Current (all inputs except f _{in} , OSC _{in})	V _{in} = V _{DD}	9	—	0.3	—	0.1	—	1.0	μA

(continued)

DC ELECTRICAL CHARACTERISTICS (continued)

Symbol	Parameter	Test Condition	V _{DD} V	- 40°C		25°C		85°C		Unit
				Min	Max	Min	Max	Min	Max	
I _{IL}	Pull-up Current (all inputs with pull-ups)	V _{in} = V _{SS}	9	- 20	- 400	- 20	- 200	- 20	- 170	μA
C _{in}	Input Capacitance		—	—	10	—	10	—	10	pF
V _{OL}	Low-Level Output Voltage — OSC _{out}	I _{out} ≈ 0 μA V _{in} = V _{DD}	3	—	0.9	—	0.9	—	0.9	V
			5	—	1.5	—	1.5	—	1.5	
			9	—	2.7	—	2.7	—	2.7	
V _{OH}	High-Level Output Voltage — OSC _{out}	I _{out} ≈ 0 μA V _{in} = V _{SS}	3	2.1	—	2.1	—	2.1	—	V
			5	3.5	—	3.5	—	3.5	—	
			9	6.3	—	6.3	—	6.3	—	
V _{OL}	Low-Level Output Voltage — Other Outputs	I _{out} ≈ 0 μA	3	—	0.05	—	0.05	—	0.05	V
			5	—	0.05	—	0.05	—	0.05	
			9	—	0.05	—	0.05	—	0.05	
V _{OH}	High-Level Output Voltage — Other Outputs	I _{out} ≈ 0 μA	3	2.95	—	2.95	—	2.95	—	V
			5	4.95	—	4.95	—	4.95	—	
			9	8.95	—	8.95	—	8.95	—	
V(BR)DSS	Drain-to-Source Breakdown Voltage — SW1, SW2	R _{pull-up} = 4.7 kΩ	—	15	—	15	—	15	—	V
I _{OL}	Low-Level Sinking Current — MC	V _{out} = 0.3 V V _{out} = 0.4 V V _{out} = 0.5 V	3	1.30	—	1.10	—	0.66	—	mA
			5	1.90	—	1.70	—	1.08	—	
			9	3.80	—	3.30	—	2.10	—	
I _{OH}	High-Level Sourcing Current — MC	V _{out} = 2.7 V V _{out} = 4.6 V V _{out} = 8.5 V	3	- 0.60	—	- 0.50	—	- 0.30	—	mA
			5	- 0.90	—	- 0.75	—	- 0.50	—	
			9	- 1.50	—	- 1.25	—	- 0.80	—	
I _{OL}	Low-Level Sinking Current — LD	V _{out} = 0.3 V V _{out} = 0.4 V V _{out} = 0.5 V	3	0.25	—	0.20	—	0.15	—	mA
			5	0.64	—	0.51	—	0.36	—	
			9	1.30	—	1.00	—	0.70	—	
I _{OH}	High-Level Sourcing Current — LD	V _{out} = 2.7 V V _{out} = 4.6 V V _{out} = 8.5 V	3	- 0.25	—	- 0.20	—	- 0.15	—	mA
			5	- 0.64	—	- 0.51	—	- 0.36	—	
			9	- 1.30	—	- 1.00	—	- 0.70	—	
I _{OL}	Low-Level Sinking Current — SW1, SW2	V _{out} = 0.3 V V _{out} = 0.4 V V _{out} = 0.5 V	3	0.80	—	0.48	—	0.24	—	mA
			5	1.50	—	0.90	—	0.45	—	
			9	3.50	—	2.10	—	1.05	—	
I _{OL}	Low-Level Sinking Current — Other Outputs	V _{out} = 0.3 V V _{out} = 0.4 V V _{out} = 0.5 V	3	0.44	—	0.35	—	0.22	—	mA
			5	0.64	—	0.51	—	0.36	—	
			9	1.30	—	1.00	—	0.70	—	
I _{OH}	High-Level Sourcing Current — Other Outputs	V _{out} = 2.7 V V _{out} = 4.6 V V _{out} = 8.5 V	3	- 0.44	—	- 0.35	—	- 0.22	—	mA
			5	- 0.64	—	- 0.51	—	- 0.36	—	
			9	- 1.30	—	- 1.00	—	- 0.70	—	
I _{OZ}	Output Leakage Current — PD _{out}	V _{out} = V _{DD} or V _{SS} Output in Off State	9	—	± 0.3	—	± 0.1	—	± 1.0	μA
I _{OZ}	Output Leakage Current — SW1, SW2	V _{out} = V _{DD} or V _{SS} Output in Off State	9	—	± 0.3	—	± 0.1	—	± 3.0	μA
C _{out}	Output Capacitance — PD _{out}	PD _{out} — Three-State	—	—	10	—	10	—	10	pF

AC ELECTRICAL CHARACTERISTICS ($C_L = 50$ pF, Input $t_r = t_f = 10$ ns)

Symbol	Parameter	V _{DD} V	Guaranteed Limit 25°C	Guaranteed Limit - 40 to 85°C	Unit
t _{PLH} , t _{PHL}	Maximum Propagation Delay, f _{IN} to MC (Figures 1 and 4)	3 5 9	110 60 35	120 70 40	ns
t _{PHL}	Maximum Propagation Delay, ENB to SW1, SW2 (Figures 1 and 5)	3 5 9	160 80 50	180 95 60	ns
t _w	Output Pulse Width, φ _R , φ _V , and LD with f _R in Phase with f _V (Figures 2 and 4)	3 5 9	25 to 200 20 to 100 10 to 70	25 to 260 20 to 125 10 to 80	ns
t _{TLH}	Maximum Output Transition Time, MC (Figures 3 and 4)	3 5 9	115 60 40	115 75 60	ns
t _{THL}	Maximum Output Transition Time, MC (Figures 3 and 4)	3 5 9	60 34 30	70 45 38	ns
t _{TLH} , t _{THL}	Maximum Output Transition Time, LD (Figures 3 and 4)	3 5 9	180 90 70	200 120 90	ns
t _{TLH} , t _{THL}	Maximum Output Transition Time, Other Outputs (Figures 3 and 4)	3 5 9	160 80 60	175 100 65	ns

SWITCHING WAVEFORMS

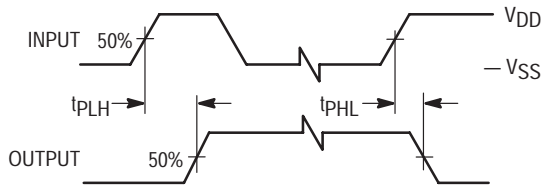


Figure 1.

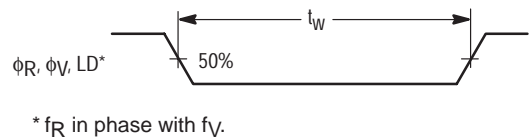


Figure 2.

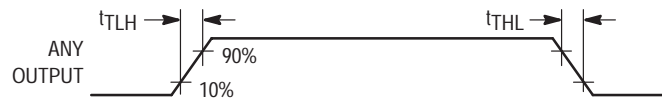
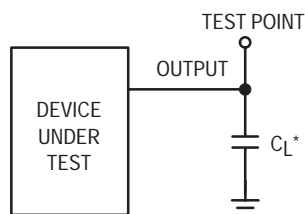
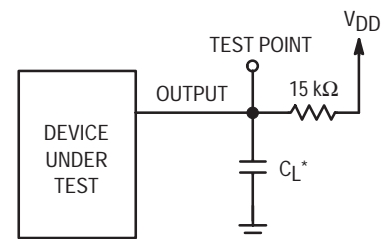


Figure 3.



* Includes all probe and fixture capacitance.

Figure 4. Test Circuit



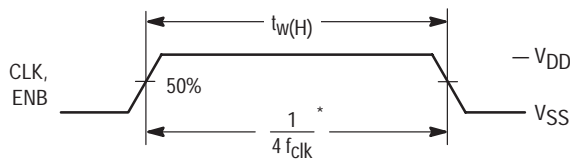
* Includes all probe and fixture capacitance.

Figure 5. Test Circuit

TIMING REQUIREMENTS (Input $t_r = t_f = 10$ ns unless otherwise indicated)

Symbol	Parameter	V _{DD} V	Guaranteed Limit 25°C	Guaranteed Limit – 40 to 85°C	Unit
f _{clk}	Serial Data Clock Frequency, Assuming 25% Duty Cycle NOTE: Refer to CLK $t_{w(H)}$ below (Figure 6)	3 5 9	dc to 5.0 dc to 7.1 dc to 10	dc to 3.5 dc to 7.1 dc to 10	MHz
t _{su}	Minimum Setup Time, Data to CLK (Figure 7)	3 5 9	30 20 18	30 20 18	ns
t _h	Minimum Hold Time, CLK to Data (Figure 7)	3 5 9	40 20 15	40 20 15	ns
t _{su}	Minimum Setup Time, CLK to ENB (Figure 7)	3 5 9	70 32 25	70 32 25	ns
t _{rec}	Minimum Recovery Time, ENB to CLK (Figure 7)	3 5 9	5 10 20	5 10 20	ns
t _{w(H)}	Minimum Pulse Width, CLK and ENB (Figure 6)	3 5 9	50 35 25	70 35 25	ns
t _r , t _f	Maximum Input Rise and Fall Times — Any Input (Figure 8)	3 5 9	5 4 2	5 4 2	μs

SWITCHING WAVEFORMS



*Assumes 25% Duty Cycle.

Figure 6.

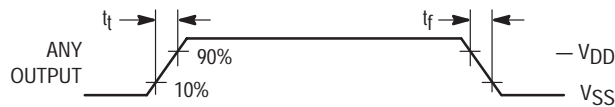


Figure 8.

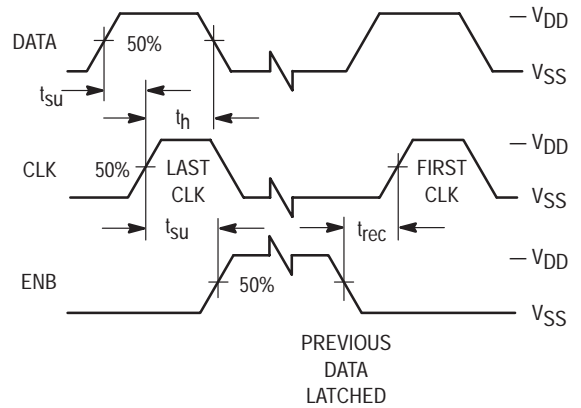
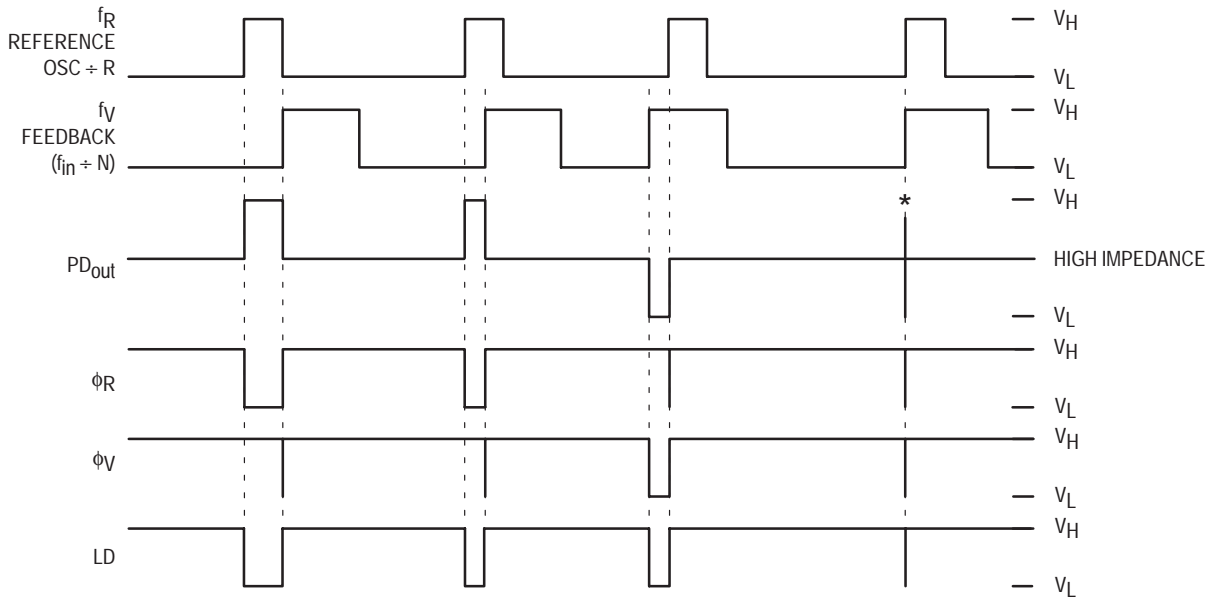


Figure 7.

FREQUENCY CHARACTERISTICS (Voltages Referenced to V_{SS} , $C_L = 50$ pF, Input $t_r = t_f = 10$ ns unless otherwise indicated)

Symbol	Parameter	Test Condition	V_{DD} V	- 40°C		25°C		85°C		Unit
				Min	Max	Min	Max	Min	Max	
f_i	Input Frequency (f_{in} , OSC_{in})	$R \geq 8$, $A \geq 0$, $N \geq 8$ $V_{in} = 500$ mV p-p ac coupled sine wave	3	—	6	—	6	—	6	MHz
			5	—	15	—	15	—	15	
			9	—	15	—	15	—	15	
		$R \geq 8$, $A \geq 0$, $N \geq 8$ $V_{in} = 1$ V p-p ac coupled sine wave	3	—	12	—	12	—	7	MHz
			5	—	22	—	20	—	20	
			9	—	25	—	22	—	22	
		$R \geq 8$, $A \geq 0$, $N \geq 8$ $V_{in} = V_{DD}$ to V_{SS} dc coupled square wave	3	—	13	—	12	—	8	MHz
			5	—	25	—	22	—	22	
			9	—	25	—	25	—	25	

NOTE: Usually, the PLL's propagation delay from f_{in} to MC plus the setup time of the prescaler determines the upper frequency limit of the system. The upper frequency limit is found with the following formula: $f = P / (t_p + t_{set})$ where f is the upper frequency in Hz, P is the lower of the dual modulus prescaler ratios, t_p is the f_{in} to MC propagation delay in seconds, and t_{set} is the prescaler setup time in seconds. For example, with a 5 V supply, the f_{in} to MC delay is 70 ns. If the MC12028A prescaler is used, the setup time is 16 ns. Thus, if the 64/65 ratio is utilized, the upper frequency limit is $f = P / (t_p + t_{set}) = 64 / (70 + 16) = 744$ MHz.



V_H = High Voltage Level.

V_L = Low Voltage Level.

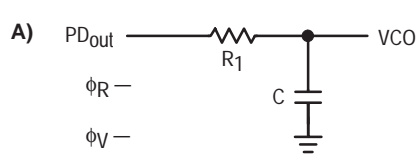
* At this point, when both f_R and f_V are in phase, the output is forced to near mid-supply.

NOTE: The PD_{out} generates error pulses during out-of-lock conditions. When locked in phase and frequency the output is high and the voltage at this pin is determined by the low-pass filter capacitor.

Figure 9. Phase Detector/Lock Detector Output Waveforms

DESIGN CONSIDERATIONS

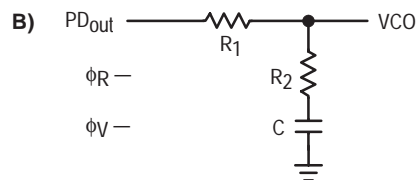
PHASE-LOCKED LOOP — LOW-PASS FILTER DESIGN



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NR_1 C}}$$

$$\zeta = \frac{N\omega_n}{2K_\phi K_{VCO}}$$

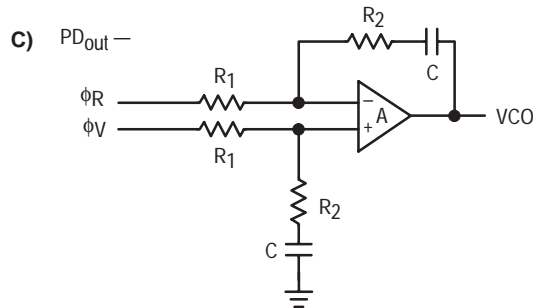
$$F(s) = \frac{1}{R_1 s C + 1}$$



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NC(R_1 + R_2)}}$$

$$\zeta = 0.5 \omega_n \left(R_2 C + \frac{N}{K_\phi K_{VCO}} \right)$$

$$F(s) = \frac{R_2 s C + 1}{(R_1 + R_2) s C + 1}$$



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NCR_1}}$$

$$\zeta = \frac{\omega_n R_2 C}{2}$$

ASSUMING GAIN A IS VERY LARGE, THEN:

$$F(s) = \frac{R_2 s C + 1}{R_1 s C}$$

NOTE: Sometimes R_1 is split into two series resistors, each $R_1 \div 2$. A capacitor C_C is then placed from the midpoint to ground to further filter ϕ_V and ϕ_R . The value of C_C should be such that the corner frequency of this network does not significantly affect ω_n . The ϕ_R and ϕ_V outputs swing rail-to-rail. Therefore, the user should be careful not to exceed the common mode input range of the op amp used in the combiner/loop filter.

DEFINITIONS:

N = Total Division Ratio in feedback loop

K_ϕ (Phase Detector Gain) = $V_{DD}/4\pi$ for PD_{out}

K_ϕ (Phase Detector Gain) = $V_{DD}/2\pi$ for ϕ_V and ϕ_R

K_{VCO} (VCO Gain) = $\frac{2\pi\Delta f_{VCO}}{\Delta V_{VCO}}$

for a typical design ω_n (Natural Frequency) $\approx \frac{2\pi f_r}{10}$ (at phase detector input).

Damping Factor: $\zeta \cong 1$

RECOMMENDED READING:

Gardner, Floyd M., *Phaselock Techniques (second edition)*. New York, Wiley-Interscience, 1979.

Manassewitsch, Vadim, *Frequency Synthesizers: Theory and Design (second edition)*. New York, Wiley-Interscience, 1980.

Blanchard, Alain, *Phase-Locked Loops: Application to Coherent Receiver Design*. New York, Wiley-Interscience, 1976.

Egan, William F., *Frequency Synthesis by Phase Lock*. New York, Wiley-Interscience, 1981.

Rohde, Ulrich L., *Digital PLL Frequency Synthesizers Theory and Design*. Englewood Cliffs, NJ, Prentice-Hall, 1983.

Berlin, Howard M., *Design of Phase-Locked Loop Circuits, with Experiments*. Indianapolis, Howard W. Sams and Co., 1978.

Kinley, Harold, *The PLL Synthesizer Cookbook*. Blue Ridge Summit, PA, Tab Books, 1980.

AN535, Phase-Locked Loop Design Fundamentals, Motorola Semiconductor Products, Inc., 1970.

AR254, Phase-Locked Loop Design Articles, Motorola Semiconductor Products, Inc., Reprinted with permission from *Electronic Design*, 1987.

CRYSTAL OSCILLATOR CONSIDERATIONS

The following options may be considered to provide a reference frequency to Motorola's CMOS frequency synthesizers.

Use of a Hybrid Crystal Oscillator

Commercially available temperature-compensated crystal oscillators (TCXOs) or crystal-controlled data clock oscillators provide very stable reference frequencies. An oscillator capable of sinking and sourcing 50 μ A at CMOS logic levels may be direct or dc coupled to OSC_{in}. In general, the highest frequency capability is obtained utilizing a direct-coupled square wave having a rail-to-rail (V_{DD} to V_{SS}) voltage swing. If the oscillator does not have CMOS logic levels on the outputs, capacitive or ac coupling to OSC_{in} may be used. OSC_{out}, an unbuffered output, should be left floating.

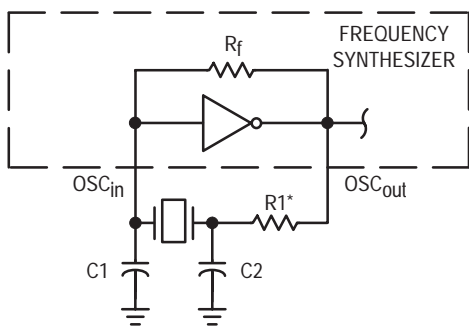
For additional information about TCXOs and data clock oscillators, please consult the latest version of the *eem Electronic Engineers Master Catalog*, the *Gold Book*, or similar publications.

Design an Off-Chip Reference

The user may design an off-chip crystal oscillator using ICs specifically developed for crystal oscillator applications, such as the MC12061 MECL device. The reference signal from the MECL device is ac coupled to OSC_{in}. For large amplitude signals (standard CMOS logic levels), dc coupling is used. OSC_{out}, an unbuffered output, should be left floating. In general, the highest frequency capability is obtained with a direct-coupled square wave having rail-to-rail voltage swing.

Use of the On-Chip Oscillator Circuitry

The on-chip amplifier (a digital inverter) along with an appropriate crystal may be used to provide a reference source frequency. A fundamental mode crystal, parallel resonant at the desired operating frequency, should be connected as shown in Figure 10.



* May be deleted in certain cases. See text.

Figure 10. Pierce Crystal Oscillator Circuit

For V_{DD} = 5.0 V, the crystal should be specified for a loading capacitance, C_L, which does not exceed 32 pF for frequencies to approximately 8.0 MHz, 20 pF for frequencies in the area of 8.0 to 15 MHz, and 10 pF for higher frequencies. These are guidelines that provide a reasonable compromise between IC capacitance, drive capability, swamping variations in stray and IC input/output capacitance, and realistic

C_L values. The shunt load capacitance, C_L, presented across the crystal can be estimated to be:

$$C_L = \frac{C_{in}C_{out}}{C_{in} + C_{out}} + C_a + C_o + \frac{C_1 \cdot C_2}{C_1 + C_2}$$

where

C_{in} = 5 pF (see Figure 11)

C_{out} = 6 pF (see Figure 11)

C_a = 1 pF (see Figure 11)

C_o = the crystal's holder capacitance

(see Figure 12)

C1 and C2 = external capacitors (see Figure 10)

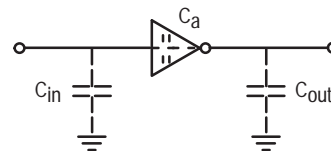
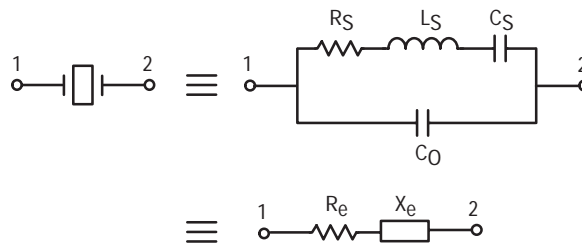


Figure 11. Parasitic Capacitances of the Amplifier



NOTE: Values are supplied by crystal manufacturer (parallel resonant crystal).

Figure 12. Equivalent Crystal Networks

The oscillator can be "trimmed" on-frequency by making a portion or all of C1 variable. The crystal and associated components must be located as close as possible to the OSC_{in} and OSC_{out} pins to minimize distortion, stray capacitance, stray inductance, and startup stabilization time. In some cases, stray capacitance should be added to the value for C_{in} and C_{out}.

Power is dissipated in the effective series resistance of the crystal, R_e, in Figure 12. The drive level specified by the crystal manufacturer is the maximum stress that a crystal can withstand without damage or excessive shift in frequency. R1 in Figure 10 limits the drive level. The use of R1 may not be necessary in some cases (i.e., R1 = 0 Ω).

To verify that the maximum dc supply voltage does not overdrive the crystal, monitor the output frequency as a function of voltage at OSC_{out}. (Care should be taken to minimize loading.) The frequency should increase very slightly as the dc supply voltage is increased. An overdriven crystal will decrease in frequency or become unstable with an increase in supply voltage. The operating supply voltage must be reduced or R1 must be increased in value if the overdriven condition exists. The user should note that the oscillator start-up time is proportional to the value of R1.

Through the process of supplying crystals for use with CMOS inverters, many crystal manufacturers have developed expertise in CMOS oscillator design with crystals. Discussions with such manufacturers can prove very helpful (see Table 1).

Table 1. Partial List of Crystal Manufacturers

Motorola — Internet Address <i>http://motorola.com</i> (Search for resonators)
United States Crystal Corp.
Crystek Crystal
Statek Corp.
Fox Electronics

NOTE: Motorola cannot recommend one supplier over another and in no way suggests that this is a complete listing of crystal manufacturers.

RECOMMENDED READING

- Technical Note TN–24, Statek Corp.
- Technical Note TN–7, Statek Corp.
- E. Hafner, “The Piezoelectric Crystal Unit – Definitions and Method of Measurement”, *Proc. IEEE*, Vol. 57, No. 2 Feb., 1969.
- D. Kemper, L. Rosine, “Quartz Crystals for Frequency Control”, *Electro–Technology*, June, 1969.
- P. J. Ottowitz, “A Guide to Crystal Selection”, *Electronic Design*, May, 1966.

DUAL–MODULUS PRESCALING

OVERVIEW

The technique of dual–modulus prescaling is well established as a method of achieving high performance frequency synthesizer operation at high frequencies. Basically, the approach allows relatively low–frequency programmable counters to be used as high–frequency programmable counters with speed capability of several hundred MHz. This is possible without the sacrifice in system resolution and performance that results if a fixed (single–modulus) divider is used for the prescaler.

In dual–modulus prescaling, the lower speed counters must be uniquely configured. Special control logic is necessary to select the divide value P or P + 1 in the prescaler for the required amount of time (see modulus control definition). Motorola’s dual–modulus frequency synthesizers contain this feature and can be used with a variety of dual–modulus prescalers to allow speed, complexity and cost to be tailored to the system requirements. Prescalers having P, P + 1 divide values in the range of ÷ 3/÷ 4 to ÷ 128/÷ 129 can be controlled by most Motorola frequency synthesizers.

Several dual–modulus prescaler approaches suitable for use with the MC145152–2, MC145156–2, or MC145158–2 are:

MC12009	÷ 5/÷ 6	440 MHz
MC12011	÷ 8/÷ 9	500 MHz
MC12013	÷ 10/÷ 11	500 MHz
MC12015	÷ 32/÷ 33	225 MHz
MC12016	÷ 40/÷ 41	225 MHz
MC12017	÷ 64/÷ 65	225 MHz
MC12018	÷ 128/÷ 129	520 MHz
MC12028A	÷ 32/33 or ÷ 64/65	1.1 GHz
MC12052A	÷ 64/65 or ÷ 128/129	1.1 GHz
MC12054A	÷ 64/65 or ÷ 128/129	2.0 GHz

DESIGN GUIDELINES

The system total divide value, N_{total} (N_T) will be dictated by the application:

$$N_T = \frac{\text{frequency into the prescaler}}{\text{frequency into the phase detector}} = N \cdot P + A$$

N is the number programmed into the ÷ N counter, A is the number programmed into the ÷ A counter, P and P + 1 are the two selectable divide ratios available in the dual–modulus prescalers. To have a range of N_T values in sequence, the ÷ A counter is programmed from zero through P – 1 for a particular value N in the ÷ N counter. N is then incremented to N + 1 and the ÷ A is sequenced from 0 through P – 1 again.

There are minimum and maximum values that can be achieved for N_T. These values are a function of P and the size of the ÷ N and ÷ A counters.

The constraint N ≥ A always applies. If A_{max} = P – 1, then N_{min} ≥ P – 1. Then N_{Tmin} = (P – 1) P + A or (P – 1) P since A is free to assume the value of 0.

$$N_{Tmax} = N_{max} \cdot P + A_{max}$$

To maximize system frequency capability, the dual–modulus prescaler output must go from low to high after each group of P or P + 1 input cycles. The prescaler should divide by P when its modulus control line is high and by P + 1 when its MC is low.

For the maximum frequency into the prescaler (f_{VCOmax}), the value used for P must be large enough such that:

- f_{VCOmax} divided by P may not exceed the frequency capability of f_{in} (input to the ÷ N and ÷ A counters).
- The period of f_{VCO} divided by P must be greater than the sum of the times:
 - Propagation delay through the dual–modulus prescaler.
 - Prescaler setup or release time relative to its MC signal.
 - Propagation time from f_{in} to the MC output for the frequency synthesizer device.

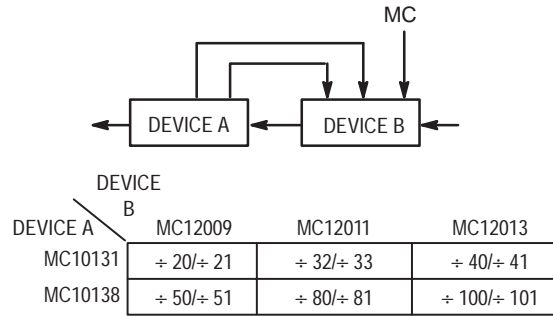
A sometimes useful simplification in the programming code can be achieved by choosing the values for P of 8, 16, 32, or 64. For these cases, the desired value of N_T results when N_T in binary is used as the program code to the ÷ N and ÷ A counters treated in the following manner:

- Assume the ÷ A counter contains “a” bits where 2^a ≥ P.
- Always program all higher order ÷ A counter bits above “a” to 0.

3. Assume the ÷ N counter and the ÷ A counter (with all the higher order bits above “a” ignored) combined into a single binary counter of n + a bits in length (n = number of divider stages in the ÷ N counter). The MSB of this “hypothetical” counter is to correspond to the MSB of ÷ N and

the LSB is to correspond to the LSB of ÷ A. The system divide value, N_T , now results when the value of N_T in binary is used to program the “new” n + a bit counter.

By using the two devices, several dual-modulus values are achievable (shown in Figure 13).



NOTE: MC12009, MC12011, and MC12013 are pin equivalent.
MC12015, MC12016, and MC12017 are pin equivalent.

Figure 13. Dual-Modulus Values

PLL Frequency Synthesizer with Serial Interface

The new MC145170-2 is pin-for-pin compatible with the MC145170-1. A comparison of the two parts is shown in the table below. The MC145170-2 is recommended for new designs and has a more robust power-on reset (POR) circuit that is more responsive to momentary power supply interruptions. The two devices are actually the same chip with mask options for the POR circuit. The more robust POR circuit draws approximately 20 μ A additional supply current. Note that the maximum specification of 100 μ A quiescent supply current has not changed.

The MC145170-2 is a single-chip synthesizer capable of direct usage in the MF, HF, and VHF bands. A special architecture makes this PLL easy to program. Either a bit- or byte-oriented format may be used. Due to the patented BitGrabber™ registers, no address/steering bits are required for *random access* of the three registers. Thus, tuning can be accomplished via a 2-byte serial transfer to the 16-bit N register.

The device features fully programmable R and N counters, an amplifier at the f_{in} pin, on-chip support of an external crystal, a programmable reference output, and both single- and double-ended phase detectors with linear transfer functions (no dead zones). A configuration (C) register allows the part to be configured to meet various applications. A patented feature allows the C register to shut off unused outputs, thereby minimizing noise and interference.

In order to reduce lock times and prevent erroneous data from being loaded into the counters, a patented jam-load feature is included. Whenever a new divide ratio is loaded into the N register, both the N and R counters are jam-loaded with their respective values and begin counting down together. The phase detectors are also initialized during the jam load.

- Operating Voltage Range: 2.7 to 5.5 V
- Maximum Operating Frequency:
 - 185 MHz @ $V_{in} = 500$ mVpp, 4.5 V Minimum Supply
 - 100 MHz @ $V_{in} = 500$ mVpp, 3.0 V Minimum Supply
- Operating Supply Current:
 - 0.6 mA @ 3.0 V, 30 MHz
 - 1.5 mA @ 3.0 V, 100 MHz
 - 3.0 mA @ 5.0 V, 50 MHz
 - 5.8 mA @ 5.0 V, 185 MHz
- Operating Temperature Range: -40 to 85°C
- R Counter Division Range: 1 and 5 to 32,767
- N Counter Division Range: 40 to 65,535
- Direct Interface to Motorola SPI Serial Data Port
- See Application Notes AN1207/D and AN1671/D
- See web site *mot-sps.com* for MC145170 control software. Select in order, Products, Wireless Semiconductor, Download, then PLL Demo Software. Choose PLLGEN.EXE.

BitGrabber is a trademark of Motorola Inc.

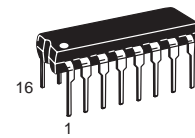
COMPARISON OF THE PLL FREQUENCY SYNTHESIZERS

Parameter	MC145170-2	MC145170-1
Minimum Supply Voltage	2.7 V	2.5 V
Maximum Input Current, f_{in}	150 μ A	120 μ A
Dynamic Characteristics, f_{in} (Figure 23)	Unchanged	-
Power-On Reset Circuit	Improved	-

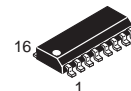
MC145170-2

CMOS PLL FREQUENCY SYNTHESIZER WITH SERIAL INTERFACE

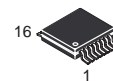
SEMICONDUCTOR TECHNICAL DATA



P SUFFIX
PLASTIC PACKAGE
CASE 648

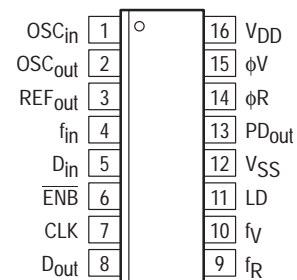


D SUFFIX
PLASTIC PACKAGE
CASE 751B
(SOG-16)



DT SUFFIX
PLASTIC PACKAGE
CASE 948C
(TSSOP-16)

PIN CONNECTIONS

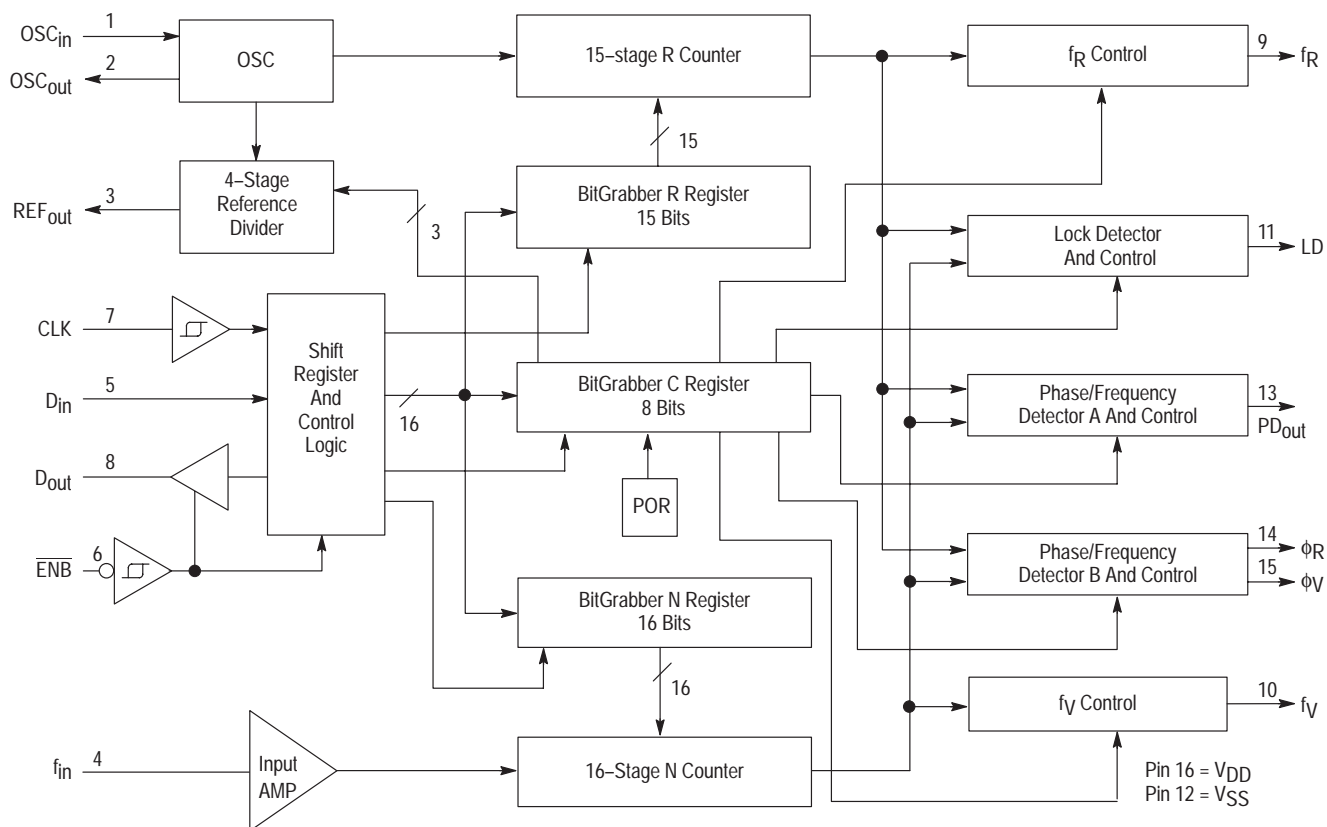


(Top View)

ORDERING INFORMATION

Device	Operating Temp Range	Package
MC145170P2	$T_A = -40$ to 85°C	Plastic DIP
MC145170D2		SOG-16
MC145170DT2		TSSOP-16

MC145170-2 BLOCK DIAGRAM



This device contains 4,800 active transistors.

MAXIMUM RATINGS (Voltages Referenced to V_{SS})

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{DD}	-0.5 to 5.5	V
DC Input Voltage	V_{in}	-0.5 to $V_{DD} + 0.5$	V
DC Output Voltage	V_{out}	-0.5 to $V_{DD} + 0.5$	V
DC Input Current, per Pin	I_{in}	± 10	mA
DC Output Current, per Pin	I_{out}	± 20	mA
DC Supply Current, V_{DD} and V_{SS} Pins	I_{DD}	± 30	mA
Power Dissipation, per Package	P_D	300	mW
Storage Temperature	T_{stg}	-65 to 150	$^{\circ}\text{C}$
Lead Temperature, 1 mm from Case for 10 seconds	T_L	260	$^{\circ}\text{C}$

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section.
2. ESD data available upon request.

This device contains protection circuitry to guard against damage due to high static voltages or electric fields. However, precautions must be taken to avoid applications of any voltage higher than maximum rated voltages to this high-impedance circuit. For proper operation, V_{in} and V_{out} should be constrained to the range $V_{SS} \leq (V_{in} \text{ or } V_{out}) \leq V_{DD}$.

Unused inputs must always be tied to an appropriate logic voltage level (e.g., either V_{SS} or V_{DD}). Unused outputs must be left open.

MC145170-2

ELECTRICAL CHARACTERISTICS (Voltages Referenced to V_{SS} , $T_A = -40$ to 85°C)

Parameter	Test Condition	Symbol	V_{DD} V	Guaranteed Limit	Unit
Power Supply Voltage Range		V_{DD}	–	2.7 to 5.5	V
Maximum Low-Level Input Voltage [Note 1] (D_{in} , CLK, \overline{ENB} , f_{in})	dc Coupling to f_{in}	V_{IL}	2.7 4.5 5.5	0.54 1.35 1.65	V
Minimum High-Level Input Voltage [Note 1] (D_{in} , CLK, \overline{ENB} , f_{in})	dc Coupling to f_{in}	V_{IH}	2.7 4.5 5.5	2.16 3.15 3.85	V
Minimum Hysteresis Voltage (CLK, \overline{ENB})		V_{Hys}	2.7 5.5	0.15 0.20	V
Maximum Low-Level Output Voltage (Any Output)	$I_{out} = 20 \mu\text{A}$	V_{OL}	2.7 5.5	0.1 0.1	V
Minimum High-Level Output Voltage (Any Output)	$I_{out} = -20 \mu\text{A}$	V_{OH}	2.7 5.5	2.6 5.4	V
Minimum Low-Level Output Current (PD_{out} , REF_{out} , f_R , f_V , LD, ϕ_R , ϕ_V)	$V_{out} = 0.3 \text{ V}$ $V_{out} = 0.4 \text{ V}$ $V_{out} = 0.5 \text{ V}$	I_{OL}	2.7 4.5 5.5	0.12 0.36 0.36	mA
Minimum High-Level Output Current (PD_{out} , REF_{out} , f_R , f_V , LD, ϕ_R , ϕ_V)	$V_{out} = 2.4 \text{ V}$ $V_{out} = 4.1 \text{ V}$ $V_{out} = 5.0 \text{ V}$	I_{OH}	2.7 4.5 5.5	-0.12 -0.36 -0.36	mA
Minimum Low-Level Output Current (D_{out})	$V_{out} = 0.4 \text{ V}$	I_{OL}	4.5	1.6	mA
Minimum High-Level Output Current (D_{out})	$V_{out} = 4.1 \text{ V}$	I_{OH}	4.5	-1.6	mA
Maximum Input Leakage Current (D_{in} , CLK, \overline{ENB} , OSC_{in})	$V_{in} = V_{DD}$ or V_{SS}	I_{in}	5.5	± 1.0	μA
Maximum Input Current (f_{in})	$V_{in} = V_{DD}$ or V_{SS}	I_{in}	5.5	± 150	μA
Maximum Output Leakage Current (PD_{out}) (D_{out})	$V_{in} = V_{DD}$ or V_{SS} , Output in High-Impedance State	I_{OZ}	5.5 5.5	± 100 ± 5.0	nA μA
Maximum Quiescent Supply Current	$V_{in} = V_{DD}$ or V_{SS} ; Outputs Open; Excluding f_{in} Amp Input Current Component	I_{DD}	5.5	100	μA
Maximum Operating Supply Current	$f_{in} = 500 \text{ mVpp}$; $OSC_{in} = 1.0 \text{ MHz @ } 1.0 \text{ Vpp}$; LD, f_R , f_V , $REF_{out} = \text{Inactive and No Connect}$; OSC_{out} , ϕ_V , ϕ_R , $PD_{out} = \text{No Connect}$; D_{in} , \overline{ENB} , CLK = V_{DD} or V_{SS}	I_{dd}	–	[Note 2]	mA

NOTES: 1. When dc coupling to the OSC_{in} pin is used, the pin must be driven rail-to-rail. In this case, OSC_{out} should be floated.

2. The nominal values at 3.0 V are 0.6 mA @ 30 MHz, and 1.5 mA @ 100 MHz. The nominal values at 5.0 V are 3.0 mA @ 50 MHz, and 5.8 mA @ 185 MHz. These are not guaranteed limits.

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AC INTERFACE CHARACTERISTICS ($T_A = -40$ to 85°C , $C_L = 50$ pF, Input $t_r = t_f = 10$ ns, unless otherwise noted.)

Parameter	Symbol	Figure No.	V _{DD} V	Guaranteed Limit	Unit
Serial Data Clock Frequency (Note: Refer to Clock t_w Below)	f_{clk}	1	2.7 4.5 5.5	dc to 3.0 dc to 4.0 dc to 4.0	MHz
Maximum Propagation Delay, CLK to D _{Out}	t_{PLH} , t_{PHL}	1, 5	2.7 4.5 5.5	150 85 85	ns
Maximum Disable Time, D _{Out} Active to High Impedance	t_{PLZ} , t_{PHZ}	2, 6	2.7 4.5 5.5	300 200 200	ns
Access Time, D _{Out} High Impedance to Active	t_{PZL} , t_{PZH}	2, 6	2.7 4.5 5.5	0 to 200 0 to 100 0 to 100	ns
Maximum Output Transition Time, D _{Out} CL = 50 pF CL = 200 pF	t_{TLH} , t_{THL}	1, 5	2.7 4.5 5.5	150 50 50	ns
		1, 5	2.7 4.5 5.5	900 150 150	ns
Maximum Input Capacitance – D _{in} , $\overline{\text{ENB}}$, CLK	C_{in}		–	10	pF
Maximum Output Capacitance – D _{Out}	C_{out}		–	10	pF

TIMING REQUIREMENTS ($T_A = -40$ to 85°C , Input $t_r = t_f = 10$ ns, unless otherwise noted.)

Parameter	Symbol	Figure No.	V _{DD} V	Guaranteed Limit	Unit
Minimum Setup and Hold Times, D _{in} vs CLK	t_{su} , t_{h}	3	2.7 4.5 5.5	55 40 40	ns
Minimum Setup, Hold, and Recovery Times, $\overline{\text{ENB}}$ vs CLK	t_{su} , t_{h} , t_{rec}	4	2.7 4.5 5.5	135 100 100	ns
Minimum Inactive-High Pulse Width, $\overline{\text{ENB}}$	$t_{\text{w(H)}}$	4	2.7 4.5 5.5	400 300 300	ns
Minimum Pulse Width, CLK	t_{w}	1	2.7 4.5 5.5	166 125 125	ns
Maximum Input Rise and Fall Times, CLK	t_r , t_f	1	2.7 4.5 5.5	100 100 100	μs

MC145170-2 SWITCHING WAVEFORMS

Figure 1.

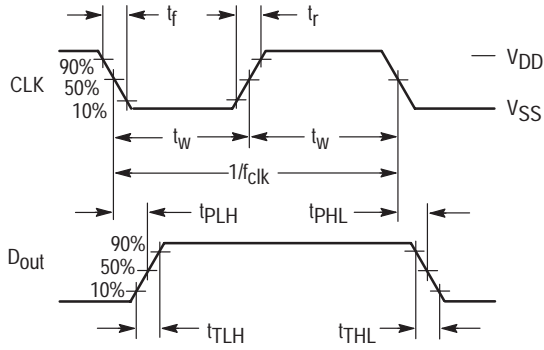


Figure 2.

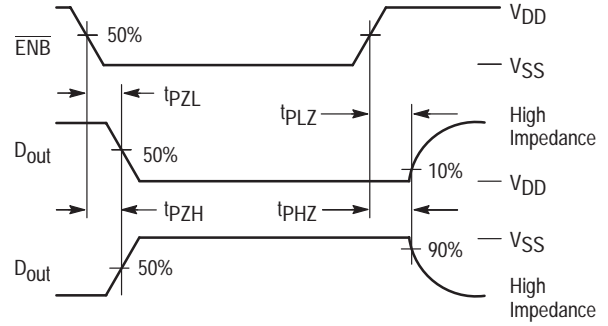


Figure 3.

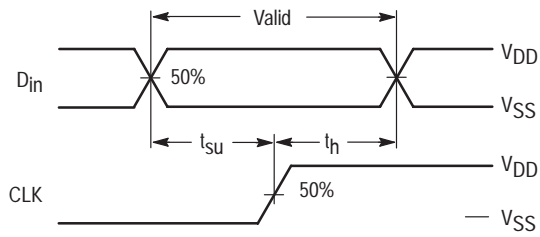


Figure 4.

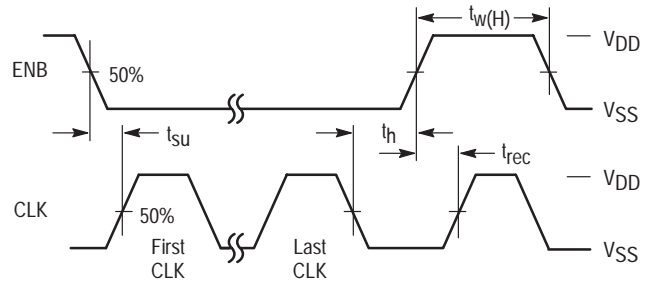
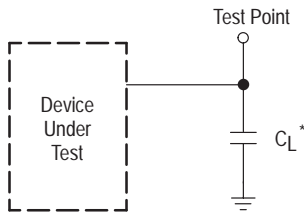
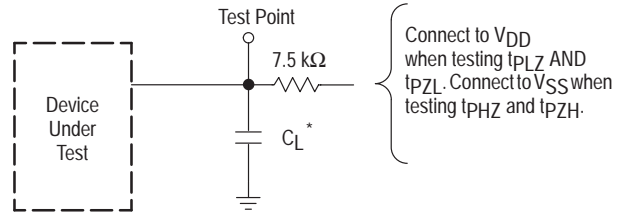


Figure 5. Test Circuit



* Includes all probe and fixture capacitance.

Figure 6. Test Circuit



* Includes all probe and fixture capacitance.

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LOOP SPECIFICATIONS ($T_A = -40$ to 85°C)

Parameter	Test Condition	Symbol	Figure No.	V _{DD} V	Guaranteed Range		Unit
					Min	Max	
Input Frequency, f_{in} [Note]	$V_{in} \geq 500$ mVpp Sine Wave, N Counter Set to Divide Ratio Such that $f_V \leq 2.0$ MHz	f	7	2.7 3.0 4.5 5.5	5.0 5.0 25 45	80 100 185 185	MHz
Input Frequency, OSC _{in} Externally Driven with ac-coupled Signal	$V_{in} \geq 1.0$ V _{pp} Sine Wave, OSC _{out} = No Connect, R Counter Set to Divide Ratio Such that $f_R \leq 2$ MHz	f	8a	2.7 3.0 4.5 5.5	1.0* 1.0* 1.0* 1.0*	22 25 30 35	MHz
Crystal Frequency, OSC _{in} and OSC _{out}	$C_1 \leq 30$ pF $C_2 \leq 30$ pF Includes Stray Capacitance	f _{X TAL}	9	2.7 3.0 4.5 5.5	2.0 2.0 2.0 2.0	12 12 15 15	MHz
Output Frequency, REF _{out}	$C_L = 30$ pF	f _{out}	10, 12	2.7 4.5 5.5	dc dc dc	– 10 10	MHz
Operating Frequency of the Phase Detectors		f		2.7 4.5 5.5	dc dc dc	– 2.0 2.0	MHz
Output Pulse Width, ϕ_R , ϕ_V , and LD	f_R in Phase with f_V $C_L = 50$ pF	t _w	11, 12	2.7 4.5 5.5	– 20 16	– 100 90	ns
Output Transition Times, ϕ_R , ϕ_V , LD, f_R , and f_V	$C_L = 50$ pF	t _{TLH} , t _{THL}	11, 12	2.7 4.5 5.5	– – –	– 65 60	ns
Input Capacitance		C _{in}					
	f_{in}			–	–	7.0	pF
	OSC _{in}			–	–	7.0	pF

* IF lower frequency is desired, use wave shaping or higher amplitude sinusoidal signal in ac-coupled case. Also, see Figure 22 for dc coupling.

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Figure 7. Test Circuit, f_{in}

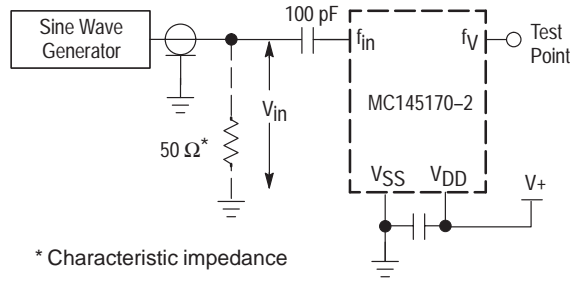


Figure 8.

Figure 8a. Test Circuit, OSC Circuit Externally Driven [Note] Figure 8b. Circuit to Eliminate Self-Oscillation, OSC Circuit Externally Driven [Note]

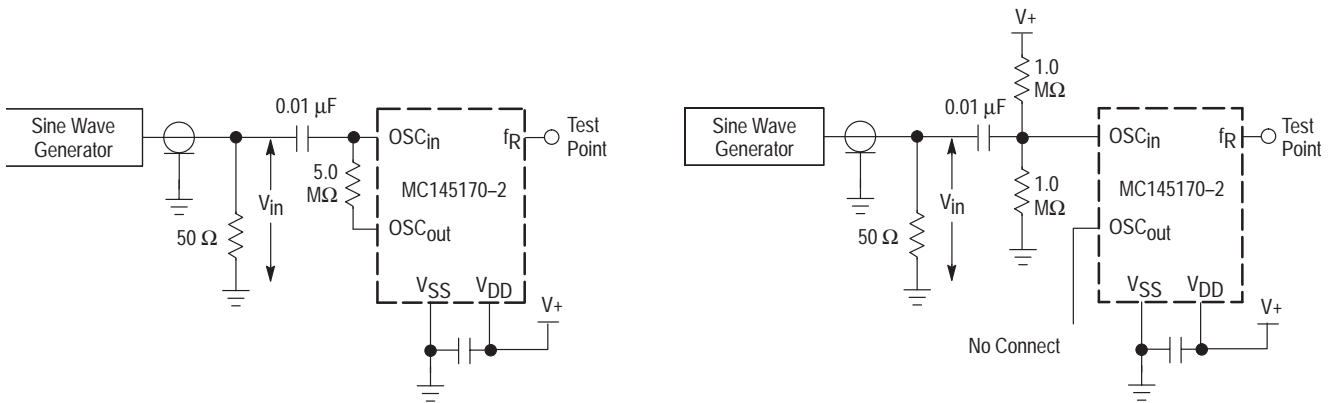


Figure 9. Test Circuit, OSC Circuit with Crystal

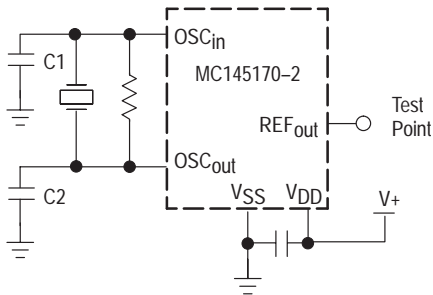


Figure 10. Switching Waveform

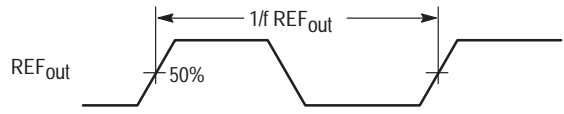


Figure 11. Switching Waveform

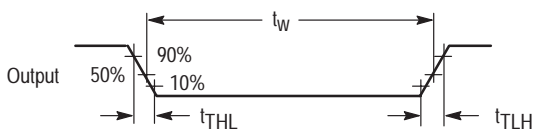
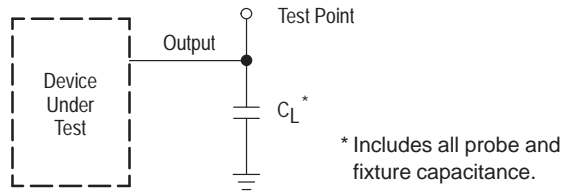


Figure 12. Test Load Circuit



NOTE: Use the circuit of Figure 8b to eliminate self-oscillation of the OSC_{in} pin when the MC145170-2 has power applied with no external signal applied at V_{in}. (Self-oscillation is not harmful to the MC145170-2 and does not damage the IC.)

MC145170–2

PIN DESCRIPTIONS

DIGITAL INTERFACE PINS

D_{in}

Serial Data Input (Pin 5)

The bit stream begins with the most significant bit (MSB) and is shifted in on the low-to-high transition of CLK. The bit pattern is 1 byte (8 bits) long to access the C or configuration register, 2 bytes (16 bits) to access the N register, or 3 bytes (24 bits) to access the R register. Additionally, the R register can be accessed with a 15-bit transfer (see Table 1). An optional pattern which resets the device is shown in Figure 13. The values in the C, N, and R registers do not change during shifting because the transfer of data to the registers is controlled by $\overline{\text{ENB}}$.

The bit stream needs neither address nor steering bits due to the innovative BitGrabber registers. Therefore, all bits in the stream are available to be data for the three registers. Random access of any register is provided (i.e., the registers may be accessed in any sequence). Data is retained in the registers over a supply range of 2.7 to 5.5 V. The formats are shown in Figures 13, 14, 15, and 16.

D_{in} typically switches near 50% of V_{DD} to maximize noise immunity. This input can be directly interfaced to CMOS devices with outputs guaranteed to switch near rail-to-rail. When interfacing to NMOS or TTL devices, either a level shifter (MC74HC14A, MC14504B) or pull-up resistor of 1 to 10 k Ω must be used. Parameters to consider when sizing the resistor are worst-case I_{OL} of the driving device, maximum tolerable power consumption, and maximum data rate.

Table 1. Register Access
(MSBs are shifted in first, C0, N0, and R0 are the LSBs)

Number of Clocks	Accessed Register	Bit Nomenclature
9 to 13	See Figure 13	(Reset)
8	C Register	C7, C6, C5, . . . , C0
16	N Register	N15, N14, N13, . . . , N0
15 or 24	R Register	R14, R13, R12, . . . , R0
Other Values \leq 32	None	
Values > 32	See Figures 24 — 31	

CLK

Serial Data Clock Input (Pin 7)

Low-to-high transitions on Clock shift bits available at D_{in}, while high-to-low transitions shift bits from D_{out}. The chip's 16–1/2–stage shift register is static, allowing clock rates down to dc in a continuous or intermittent mode.

Four to eight clock cycles followed by five clock cycles are needed to reset the device; this is optional. Eight clock cycles are required to access the C register. Sixteen clock cycles are needed for the N register. Either 15 or 24 cycles can be used to access the R register (see Table 1 and Figures 13, 14, 15, and 16). For cascaded devices, see Figures 24 to 31.

CLK typically switches near 50% of V_{DD} and has a Schmitt-triggered input buffer. Slow CLK rise and fall times are allowed. See the last paragraph of D_{in} for more information.

NOTE

To guarantee proper operation of the power-on reset (POR) circuit, the CLK pin must be held at the potential of either the V_{SS} or V_{DD} pin during power up. That is, the CLK input should not be floated or toggled while the V_{DD} pin is ramping from 0 to at least 2.7 V. If control of the CLK pin is not practical during power up, the initialization sequence shown in Figure 13 must be used.

$\overline{\text{ENB}}$

Active-Low Enable Input (Pin 6)

This pin is used to activate the serial interface to allow the transfer of data to/from the device. When $\overline{\text{ENB}}$ is in an inactive high state, shifting is inhibited, D_{out} is forced to the high-impedance state, and the port is held in the initialized state. To transfer data to the device, $\overline{\text{ENB}}$ (which must start inactive high) is taken low, a serial transfer is made via D_{in} and CLK, and $\overline{\text{ENB}}$ is taken back high. The low-to-high transition on $\overline{\text{ENB}}$ transfers data to the C, N, or R register depending on the data stream length per Table 1.

NOTE

Transitions on $\overline{\text{ENB}}$ must not be attempted while CLK is high. This puts the device out of synchronization with the microcontroller. Resynchronization occurs when $\overline{\text{ENB}}$ is high and CLK is low.

This input is also Schmitt-triggered and switches near 50% of V_{DD}, thereby minimizing the chance of loading erroneous data into the registers. See the last paragraph of D_{in} for more information.

D_{out}

Three-State Serial Data Output (Pin 8)

Data is transferred out of the 16–1/2–stage shift register through D_{out} on the high-to-low transition of CLK. This output is a No Connect, unless used in one of the manners discussed below.

D_{out} could be fed back to an MCU/MPU to perform a wrap-around test of serial data. This could be part of a system check conducted at power up to test the integrity of the system's processor, PC board traces, solder joints, etc.

The pin could be monitored at an in-line QA test during board manufacturing.

Finally, D_{out} facilitates troubleshooting a system and permits cascading devices.

REFERENCE PINS

OSC_{in}/OSC_{out}

Reference Oscillator Input/Output (Pins 1, 2)

These pins form a reference oscillator when connected to terminals of an external parallel-resonant crystal. Frequency-setting capacitors of appropriate values as recommended by the crystal supplier are connected from each pin to ground (up to a maximum of 30 pF each, including stray capacitance). An external feedback resistor of 1.0 to 5.0 M Ω is connected directly across the pins to ensure linear operation of the amplifier. The required connections for the components are shown in Figure 9.

If desired, an external clock source can be ac coupled to OSC_{in}. A 0.01 μ F coupling capacitor is used for measurement purposes and is the minimum size

recommended for applications. An external feedback resistor of approximately 5 M Ω is required across the OSC_{in} and OSC_{out} pins in the ac-coupled case (see Figure 8a or alternate circuit 8b). OSC_{out} is an internal node on the device and should not be used to drive any loads (i.e., OSC_{out} is unbuffered). However, the buffered REF_{out} is available to drive external loads.

The external signal level must be at least 1 V_{p-p}; the maximum frequencies are given in the **Loop Specifications** table. These maximum frequencies apply for R Counter divide ratios as indicated in the table. For very small ratios, the maximum frequency is limited to the divide ratio times 2 MHz. (Reason: the phase/frequency detectors are limited to a maximum input frequency of 2 MHz.)

If an external source is available which swings virtually rail-to-rail (V_{DD} to V_{SS}), then dc coupling can be used. In the dc-coupled case, no external feedback resistor is needed. OSC_{out} must be a No Connect to avoid loading an internal node on the device, as noted above. *For frequencies below 1 MHz, dc coupling must be used.* The R counter is a static counter and may be operated down to dc. However, wave shaping by a CMOS buffer may be required to ensure fast rise and fall times into the OSC_{in} pin. See Figure 22.

Each rising edge on the OSC_{in} pin causes the R counter to decrement by one.

REF_{out}

Reference Frequency Output (Pin 3)

This output is the buffered output of the crystal-generated reference frequency or externally provided reference source. This output may be enabled, disabled, or scaled via bits in the C register (see Figure 14).

REF_{out} can be used to drive a microprocessor clock input, thereby saving a crystal. Upon power up, the on-chip power-on-initialize circuit forces REF_{out} to the OSC_{in} divided-by-8 mode.

REF_{out} is capable of operation to 10 MHz; see the **Loop Specifications** table. Therefore, divide values for the reference divider are restricted to two or higher for OSC_{in} frequencies above 10 MHz.

If unused, the pin should be floated and should be disabled via the C register to minimize dynamic power consumption and electromagnetic interference (EMI).

COUNTER OUTPUT PINS

f_R

R Counter Output (Pin 9)

This signal is the buffered output of the 15-stage R counter. f_R can be enabled or disabled via the C register (patented). The output is disabled (static low logic level) upon power up. If unused, the output should be left disabled and unconnected to minimize interference with external circuitry.

The f_R signal can be used to verify the R counter's divide ratio. This ratio extends from 5 to 32,767 and is determined by the binary value loaded into the R register. Also, direct access to the phase detector via the OSC_{in} pin is allowed by choosing a divide value of 1 (see Figure 15). The maximum frequency which the phase detectors operate is 2 MHz. Therefore, the frequency of f_R must not exceed 2 MHz.

When activated, the f_R signal appears as normally low and pulses high. The pulse width is 4.5 cycles of the OSC_{in} pin signal, except when a divide ratio of 1 is selected. When 1 is

selected, the OSC_{in} signal is buffered and appears at the f_R pin.

f_V

N Counter Output (Pin 10)

This signal is the buffered output of the 16-stage N counter. f_V can be enabled or disabled via the C register (patented). The output is disabled (static low logic level) upon power up. If unused, the output should be left disabled and unconnected to minimize interference with external circuitry.

The f_V signal can be used to verify the N counter's divide ratio. This ratio extends from 40 to 65,535 and is determined by the binary value loaded into the N register. The maximum frequency which the phase detectors operate is 2 MHz. Therefore, the frequency of f_V must not exceed 2 MHz.

When activated, the f_V signal appears as normally low and pulses high.

LOOP PINS

f_{in}

Frequency Input (Pin 4)

This pin is a frequency input from the VCO. This pin feeds the on-chip amplifier which drives the N counter. This signal is normally sourced from an external voltage-controlled oscillator (VCO), and is ac-coupled into f_{in}. A 100 pF coupling capacitor is used for measurement purposes and is the minimum size recommended for applications (see Figure 7). The frequency capability of this input is dependent on the supply voltage as listed in the **Loop Specifications** table. For small divide ratios, the maximum frequency is limited to the divide ratio times 2 MHz. (Reason: the phase/frequency detectors are limited to a maximum frequency of 2 MHz.)

For signals which swing from at least the V_{IL} to V_{IH} levels listed in the **Electrical Characteristics** table, dc coupling may be used. Also, for low frequency signals (less than the minimum frequencies shown in the **Loop Specifications** table), dc coupling is a requirement. The N counter is a static counter and may be operated down to dc. However, wave shaping by a CMOS buffer may be required to ensure fast rise and fall times into the f_{in} pin. See Figure 22.

Each rising edge on the f_{in} pin causes the N counter to decrement by 1.

PD_{out}

Single-Ended Phase/Frequency Detector Output (Pin 13)

This is a three-state output for use as a loop error signal when combined with an external low-pass filter. Through use of a Motorola patented technique, the detector's dead zone has been eliminated. Therefore, the phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detector is described below and is shown in Figure 17.

POL bit (C7) in the C register = low (see Figure 14)

Frequency of f_V > f_R or Phase of f_V Leading f_R: negative pulses from high impedance

Frequency of f_V < f_R or Phase of f_V Lagging f_R: positive pulses from high impedance

Frequency and Phase of f_V = f_R: essentially high-impedance state; voltage at pin determined by loop filter

POL bit (C7) = high

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Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : positive pulses from high impedance

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : negative pulses from high impedance

Frequency and Phase of $f_V = f_R$: essentially high-impedance state; voltage at pin determined by loop filter

This output can be enabled, disabled, and inverted via the C register. If desired, PD_{out} can be forced to the high-impedance state by utilization of the disable feature in the C register (patented).

ϕ_R and ϕ_V

Double-Ended Phase/Frequency Detector Outputs (Pins 14, 15)

These outputs can be combined externally to generate a loop error signal. Through use of a Motorola patented technique, the detector's dead zone has been eliminated. Therefore, the phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detector is described below and is shown in Figure 17.

POL bit (C7) in the C register = low (see Figure 14)

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : $\phi_V =$ negative pulses, $\phi_R =$ essentially high

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : $\phi_V =$ essentially high, $\phi_R =$ negative pulses

Frequency and Phase of $f_V = f_R$: ϕ_V and ϕ_R remain essentially high, except for a small minimum time period when both pulse low in phase

POL bit (C7) = high

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : $\phi_R =$ negative pulses, $\phi_V =$ essentially high

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : $\phi_R =$ essentially high, $\phi_V =$ negative pulses

Frequency and Phase of $f_V = f_R$: ϕ_V and ϕ_R remain essentially high, except for a small minimum time period when both pulse low in phase

These outputs can be enabled, disabled, and interchanged via the C register (patented).

LD

Lock Detector Output (Pin 11)

This output is essentially at a high level with narrow low-going pulses when the loop is locked (f_R and f_V of the same phase and frequency). The output pulses low when f_V and f_R are out of phase or different frequencies (see Figure 17).

This output can be enabled and disabled via the C register (patented). Upon power up, on-chip initialization circuitry disables LD to a static low logic level to prevent a false "lock" signal. If unused, LD should be disabled and left open.

POWER SUPPLY

VDD

Most Positive Supply Potential (Pin 16)

This pin may range from 2.7 to 5.5 V with respect to V_{SS} .

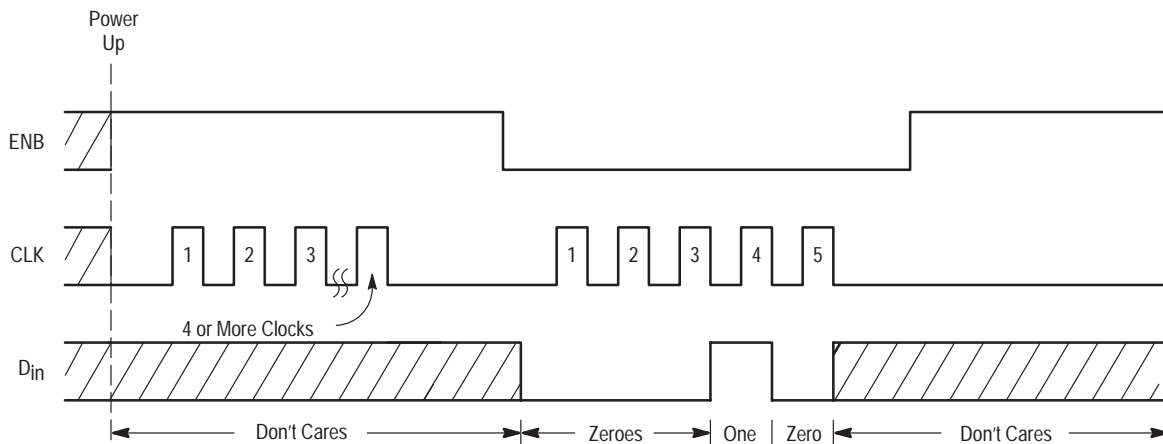
For optimum performance, V_{DD} should be bypassed to V_{SS} using low-inductance capacitor(s) mounted very close to the device. Lead lengths on the capacitor(s) should be minimized. (The very fast switching speed of the device causes current spikes on the power leads.)

VSS

Most Negative Supply Potential (Pin 12)

This pin is usually ground. For measurement purposes, the V_{SS} pin is tied to a ground plane.

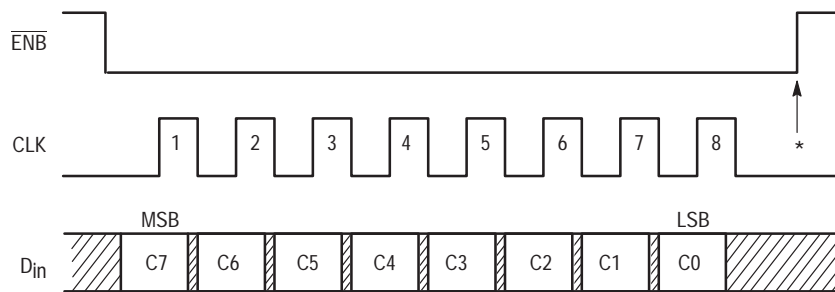
Figure 13. Reset Sequence



NOTE: This initialization sequence is usually not necessary because the on-chip power-on reset circuit performs the initialization function. However, this initialization sequence must be used immediately after power up if control of the CLK pin is not possible. That is, if CLK (Pin 7) toggles or floats upon power up, use the above sequence to reset the device. Also, use this sequence if power is momentarily interrupted such that the supply voltage to the device is reduced to below 2.7 V, but not down to at least 1 V (for example, the supply drops down to 2 V). This is necessary because the on-chip power-on reset is only activated when the supply ramps up from a voltage below approximately 1.0 V.

MC145170-2

Figure 14. C Register Access and Format (8 Clock Cycles are Used)



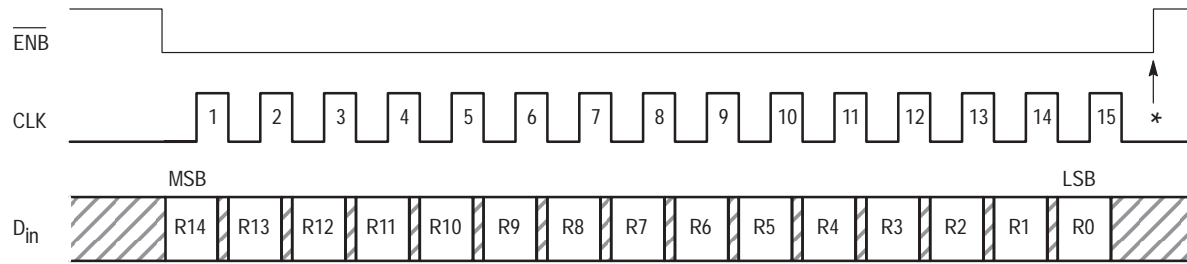
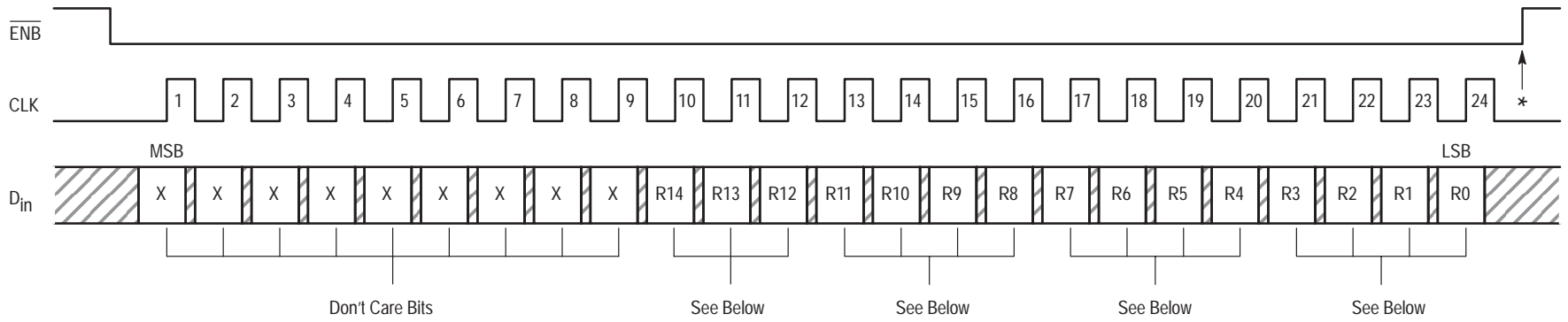
* At this point, the new byte is transferred to the C register and stored. No other registers are affected.

- C7 — POL:** Selects the output polarity of the phase/frequency detectors. When set high, this bit inverts PD_{out} and interchanges the ϕ_{R} function with ϕ_{V} as depicted in Figure 17. Also see the phase detector output pin descriptions for more information. This bit is cleared low at power up.
- C6 — PDA/B:** Selects which phase/frequency detector is to be used. When set high, enables the output of phase/frequency detector A (PD_{out}) and disables phase/frequency detector B by forcing ϕ_{R} and ϕ_{V} to the static high state. When cleared low, phase/frequency detector B is enabled (ϕ_{R} and ϕ_{V}) and phase/frequency detector A is disabled with PD_{out} forced to the high-impedance state. This bit is cleared low at power up.
- C5 — LDE:** Enables the lock detector output when set high. When the bit is cleared low, the LD output is forced to a static low level. This bit is cleared low at power up.
- C4 — C2, OSC2 — OSC0:** Reference output controls which determine the REF_{out} characteristics as shown below. Upon power up, the bits are initialized such that $\text{OSC}_{\text{in}}/8$ is selected.

C4	C3	C2	REF_{out} Frequency
0	0	0	dc (Static Low)
0	0	1	OSC_{in}
0	1	0	$\text{OSC}_{\text{in}}/2$
0	1	1	$\text{OSC}_{\text{in}}/4$
1	0	0	$\text{OSC}_{\text{in}}/8$ (POR Default)
1	0	1	$\text{OSC}_{\text{in}}/16$
1	1	0	$\text{OSC}_{\text{in}}/8$
1	1	1	$\text{OSC}_{\text{in}}/16$

- C1 — f_{VE} :** Enables the f_{V} output when set high. When cleared low, the f_{V} output is forced to a static low level. The bit is cleared low upon power up.
- C0 — f_{RE} :** Enables the f_{R} output when set high. When cleared low, the f_{R} output is forced to a static low level. The bit is cleared low upon power up.

Figure 15. R Register Access and Formats (Either 24 or 15 Clock Cycles Can Be Used)



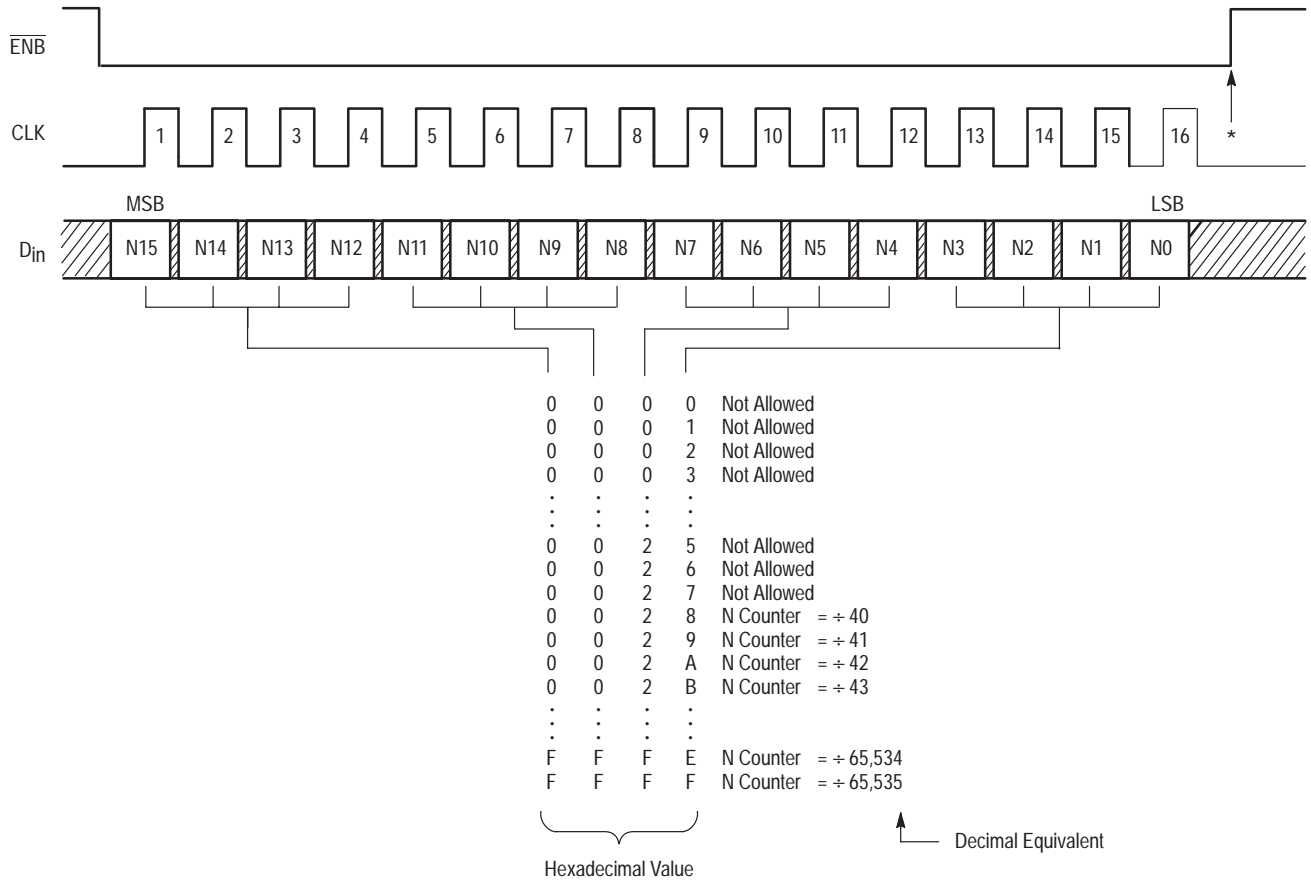
0	0	0	0	Not Allowed
0	0	0	1	R Counter = ∓ 1 (Direct Access to Reference Side of Phase/Frequency Detector)
0	0	0	2	Not Allowed
0	0	0	3	Not Allowed
0	0	0	4	Not Allowed
0	0	0	5	R Counter = ∓ 5
0	0	0	6	R Counter = ∓ 6
0	0	0	7	R Counter = ∓ 7
⋮	⋮	⋮	⋮	⋮
7	F	F	E	R Counter = $\mp 32,766$
7	F	F	F	R Counter = $\mp 32,767$

Octal Value Hexadecimal Value Decimal Equivalent

* At this point, the new data is transferred to the R register and stored. No other registers are affected.

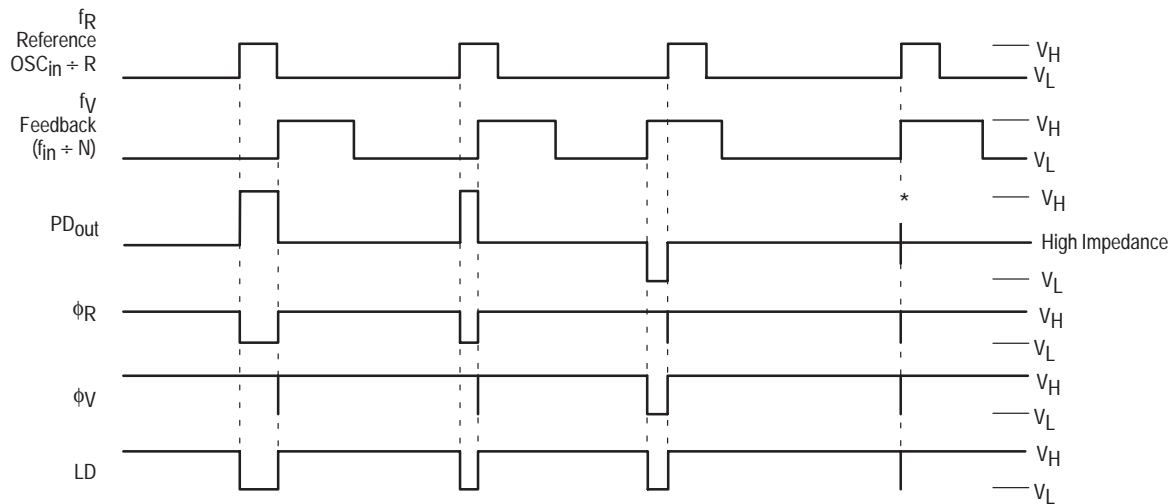
MC145170-2

Figure 16. N Register Access and Format (16 Clock Cycles Are Used)



* At this point, the two new bytes are transferred to the N register and stored. No other registers are affected. In addition, the N and R counters are jam-loaded and begin counting down together.

Figure 17. Phase/Frequency Detectors and Lock Detector Output Waveforms



V_H = High voltage level

V_L = Low voltage level

*At this point, when both f_R and f_V are in phase, both the sinking and sourcing output FETs are turned on for a very short interval.

NOTE: The PD_{out} generates error pulses during out-of-lock conditions. When locked in phase and frequency, the output is high impedance and the voltage at that pin is determined by the low-pass filter capacitor. PD_{out}, φ_R, and φ_V are shown with the polarity bit (POL) = low; see Figure 14 for POL.

MC145170-2

DESIGN CONSIDERATIONS

CRYSTAL OSCILLATOR CONSIDERATIONS

The following options may be considered to provide a reference frequency to Motorola's CMOS frequency synthesizers.

Use of a Hybrid Crystal Oscillator

Commercially available temperature-compensated crystal oscillators (TCXOs) or crystal-controlled data clock oscillators provide very stable reference frequencies. An oscillator capable of CMOS logic levels at the output may be direct or dc coupled to OSC_{in}. If the oscillator does not have CMOS logic levels on the outputs, capacitive or ac coupling to OSC_{in} may be used (see Figures 8a and 8b).

For additional information about TCXOs, visit motorola.com on the world wide web.

Use of the On-Chip Oscillator Circuitry

The on-chip amplifier (a digital inverter) along with an appropriate crystal may be used to provide a reference source frequency. A fundamental mode crystal, parallel resonant at the desired operating frequency, should be connected as shown in Figure 18.

The crystal should be specified for a loading capacitance (C_L) which does not exceed 20 pF when used at the highest operating frequencies listed in the **Loop Specifications** table. Larger C_L values are possible for lower frequencies. Assuming R1 = 0 Ω, the shunt load capacitance (C_L) presented across the crystal can be estimated to be:

$$C_L = \frac{C_{in}C_{out}}{C_{in} + C_{out}} + C_a + C_{stray} + \frac{C1 \times C2}{C1 + C2}$$

where

C_{in} = 5.0 pF (see Figure 19)

C_{out} = 6.0 pF (see Figure 19)

C_a = 1.0 pF (see Figure 19)

C1 and C2 = external capacitors (see Figure 18)

C_{stray} = the total equivalent external circuit stray capacitance appearing across the crystal terminals

The oscillator can be "trimmed" on-frequency by making a portion or all of C1 variable. The crystal and associated components must be located as close as possible to the OSC_{in} and OSC_{out} pins to minimize distortion, stray capacitance, stray inductance, and startup stabilization time. Circuit stray capacitance can also be handled by adding the appropriate stray value to the values for C_{in} and C_{out}. For this approach, the term C_{stray} becomes 0 in the above expression for C_L.

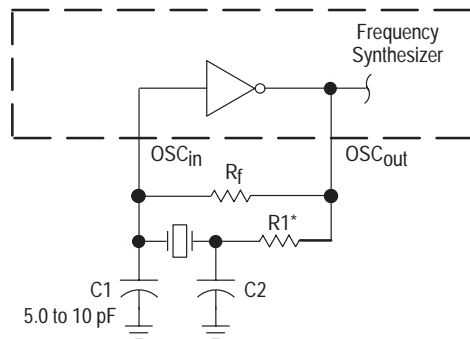
A good design practice is to pick a small value for C1, such as 5 to 10 pF. Next, C2 is calculated. C1 < C2 results in a more robust circuit for start-up and is more tolerant of crystal parameter variations.

Power is dissipated in the effective series resistance of the crystal, R_e, in Figure 20. The maximum drive level specified by the crystal manufacturer represents the maximum stress that the crystal can withstand without damage or excessive shift in operating frequency. R1 in Figure 18 limits the drive level. The use of R1 is not necessary in most cases.

To verify that the maximum dc supply voltage does not cause the crystal to be overdriven, monitor the output frequency at the REF_{out} pin (OSC_{out} is not used because loading impacts the oscillator). The frequency should increase very slightly as the dc supply voltage is increased. An overdriven crystal decreases in frequency or becomes unstable with an increase in supply voltage. The operating supply voltage must be reduced or R1 must be increased in value if the overdriven condition exists. The user should note that the oscillator start-up time is proportional to the value of R1.

Through the process of supplying crystals for use with CMOS inverters, many crystal manufacturers have developed expertise in CMOS oscillator design with crystals. Discussions with such manufacturers can prove very helpful (see Table 2).

Figure 18. Pierce Crystal Oscillator Circuit



* May be needed in certain cases. See text.

Figure 19. Parasitic Capacitances of the Amplifier and C_{stray}

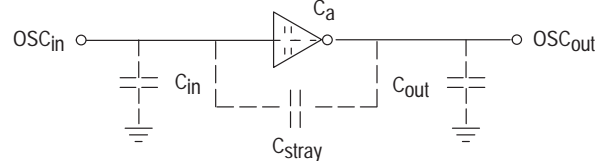
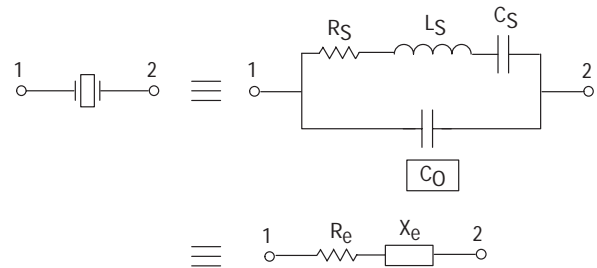


Figure 20. Equivalent Crystal Networks



NOTE: Values are supplied by crystal manufacturer (parallel resonant crystal).

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RECOMMENDED READING

Technical Note TN-24, Statek Corp.

Technical Note TN-7, Statek Corp.

E. Hafner, "The Piezoelectric Crystal Unit-Definitions and Method of Measurement", *Proc. IEEE*, Vol. 57, No. 2, Feb. 1969.

D. Kemper, L. Rosine, "Quartz Crystals for Frequency Control", *Electro-Technology*, June 1969.

P. J. Ottowitz, "A Guide to Crystal Selection", *Electronic Design*, May 1966.

D. Babin, "Designing Crystal Oscillators", *Machine Design*, March 7, 1985.

D. Babin, "Guidelines for Crystal Oscillator Design", *Machine Design*, April 25, 1985.

See web site mot-sps.com for MC145170-2 control software. Select in order, Products, Wireless Semiconductor, Download, then PLL Demo Software. Choose PLLGEN.EXE.

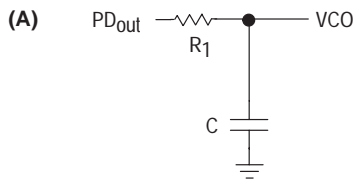
Table 2. Partial List of Crystal Manufacturers

CTS Corp.
United States Crystal Corp.
Crystek Crystal
Statek Corp.
Fox Electronics

NOTE: Motorola cannot recommend one supplier over another and in no way suggests that this is a complete listing of crystal manufacturers.

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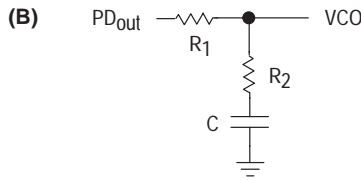
PHASE-LOCKED LOOP — LOW PASS FILTER DESIGN



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NR_1C}}$$

$$\zeta = \frac{N\omega_n}{2K_\phi K_{VCO}}$$

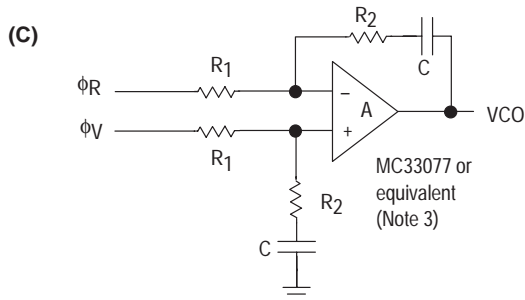
$$F(s) = \frac{1}{R_1sC + 1}$$



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NC(R_1 + R_2)}}$$

$$\zeta = 0.5 \omega_n \left(R_2C + \frac{N}{K_\phi K_{VCO}} \right)$$

$$F(s) = \frac{R_2sC + 1}{(R_1 + R_2)sC + 1}$$



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NCR_1}}$$

$$\zeta = \frac{\omega_n R_2 C}{2}$$

Assuming Gain A Is Very Large, Then:

$$F(s) = \frac{R_2sC + 1}{R_1sC}$$

NOTES:

- 8 For (C), R_1 is frequently split into two series resistors; each resistor is equal to R_1 divided by 2. A capacitor C_C is then placed from the midpoint to ground to further filter the error pulses. The value of C_C should be such that the corner frequency of this network does not significantly affect ω_n .
- 9 The ϕ_R and ϕ_V outputs swing rail-to-rail. Therefore, the user should be careful not to exceed the common mode input range of the op amp.
- 10 For the latest information on MC33077 or equivalent, see the Motorola Analog IC web site at <http://www.mot-sps.com/analog>.

DEFINITIONS:

N = Total Division Ratio in Feedback Loop

K_ϕ (Phase Detector Gain) = $V_{DD} / 4\pi$ volts per radian for PD_{out}

K_ϕ (Phase Detector Gain) = $V_{DD} / 2\pi$ volts per radian for ϕ_V and ϕ_R

$$K_{VCO} \text{ (VCO Gain)} = \frac{2\pi\Delta f_{VCO}}{\Delta V_{VCO}}$$

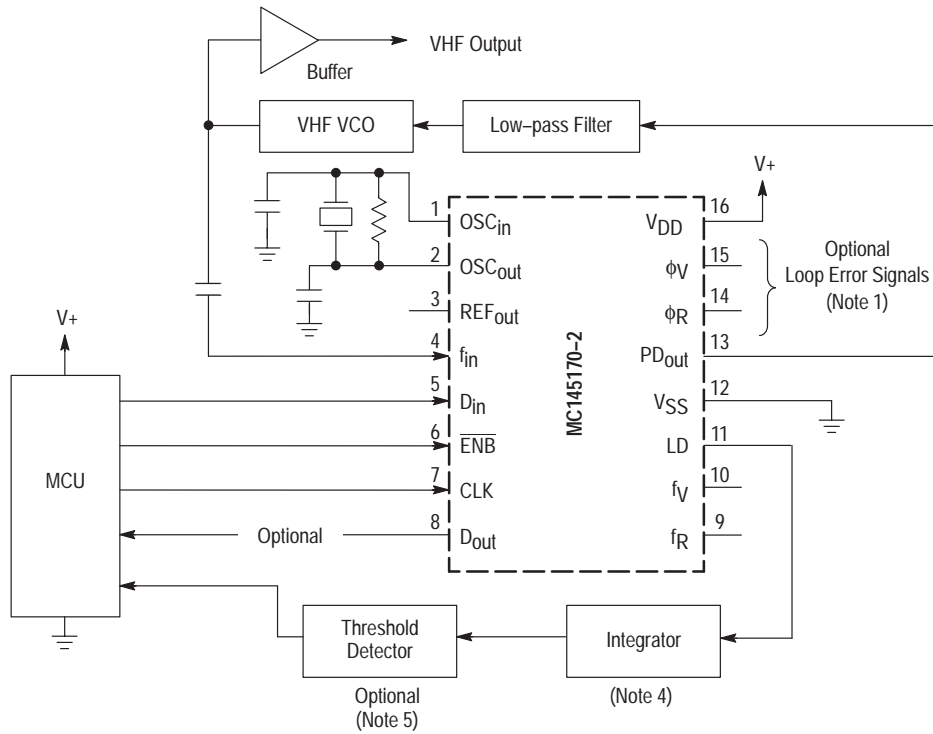
For a nominal design starting point, the user might consider a damping factor $\zeta \approx 0.7$ and a natural loop frequency $\omega_n \approx (2\pi f_R / 50)$ where f_R is the frequency at the phase detector input. Larger ω_n values result in faster loop lock times and, for similar sideband filtering, higher f_R -related VCO sidebands.

RECOMMENDED READING:

- Gardner, Floyd M., *Phaselock Techniques (second edition)*. New York, Wiley-Interscience, 1979.
- Manassewitsch, Vadim, *Frequency Synthesizers: Theory and Design (second edition)*. New York, Wiley-Interscience, 1980.
- Blanchard, Alain, *Phase-Locked Loops: Application to Coherent Receiver Design*. New York, Wiley-Interscience, 1976.
- Egan, William F., *Frequency Synthesis by Phase Lock*. New York, Wiley-Interscience, 1981.
- Rohde, Ulrich L., *Digital PLL Frequency Synthesizers Theory and Design*. Englewood Cliffs, NJ, Prentice-Hall, 1983.
- Berlin, Howard M., *Design of Phase-Locked Loop Circuits, with Experiments*. Indianapolis, Howard W. Sams and Co., 1978.
- Kinley, Harold, *The PLL Synthesizer Cookbook*. Blue Ridge Summit, PA, Tab Books, 1980.
- Seidman, Arthur H., *Integrated Circuits Applications Handbook*, Chapter 17, pp. 538-586. New York, John Wiley & Sons.
- Fadrhons, Jan, "Design and Analyze PLLs on a Programmable Calculator," *EDN*. March 5, 1980.
- AN535, Phase-Locked Loop Design Fundamentals, Motorola Semiconductor Products, Inc., 1970.
- AR254, Phase-Locked Loop Design Articles, Motorola Semiconductor Products, Inc., Reprinted with permission from *Electronic Design*, 1987.
- AN1207, The MC145170 in Basic HF and VHF Oscillators, Motorola Semiconductor Products, Inc., 1992.
- AN1671, MC145170 PSpice Modeling Kit, Motorola Semiconductor Products, Inc., 1998.

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Figure 21. Example Application

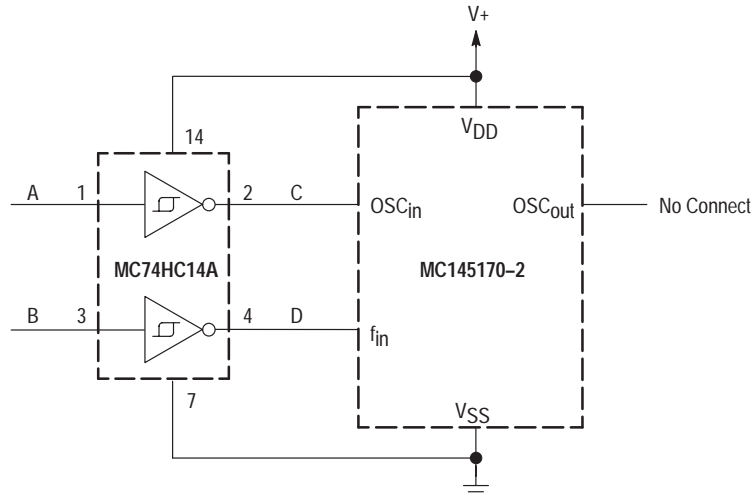


NOTES:

- 1 The ϕ_R and ϕ_V outputs are fed to an external combiner/loop filter. See the Phase-Locked Loop — Low-Pass Filter Design page for additional information. The ϕ_R and ϕ_V outputs swing rail-to-rail. Therefore, the user should be careful not to exceed the common mode input range of the op amp used in the combiner/loop filter.
- 2 For optimum performance, bypass the V_{DD} pin to V_{SS} (GND) with one or more low-inductance capacitors.
- 3 The R counter is programmed for a divide value = OSC_{in}/f_R . Typically, f_R is the tuning resolution required for the VCO. Also, the VCO frequency divided by $f_R = N$, where N is the divide value of the N counter.
- 4 May be an R-C low-pass filter.
- 5 May be a bipolar transistor.

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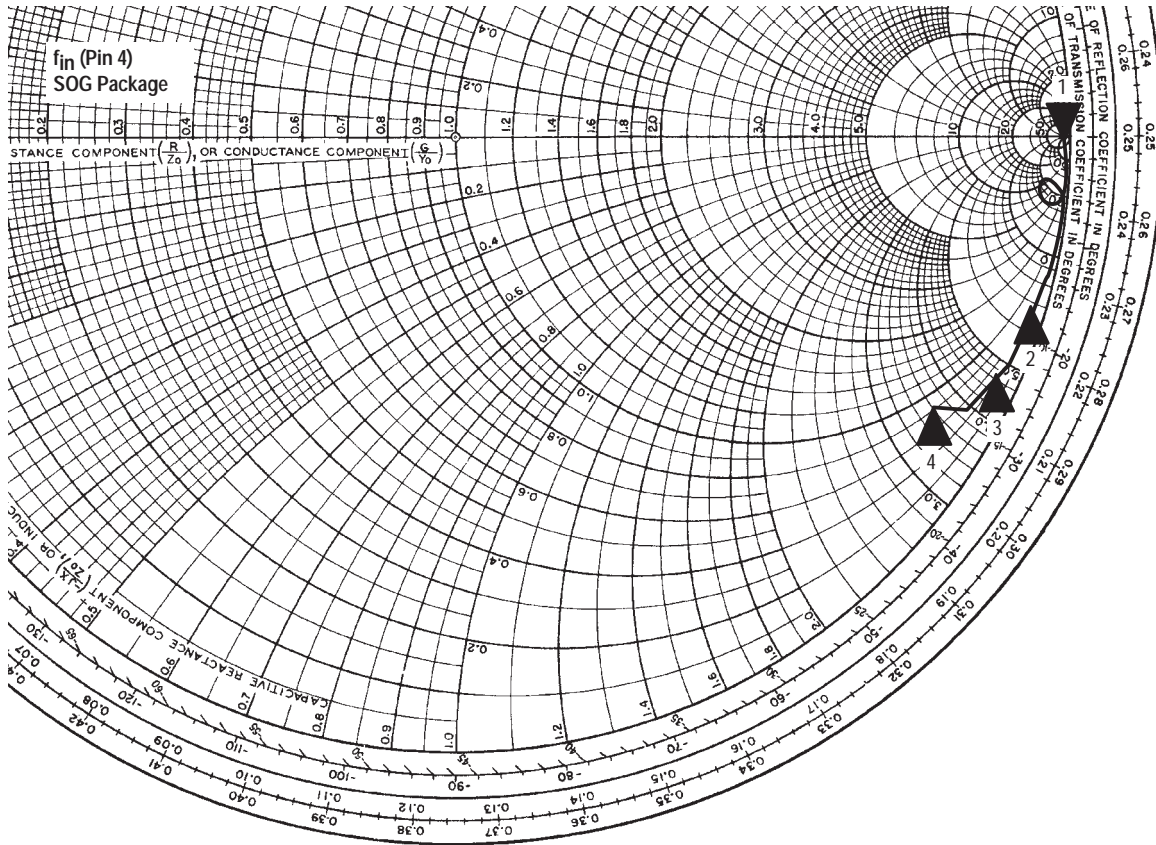
Figure 22. Low Frequency Operation Using dc Coupling



NOTE: The signals at Points A and B may be low-frequency sinusoidal or square waves with slow edge rates or noisy signal edges. At Points C and D, the signals are cleaned up, have sharp edge rates, and rail-to-rail signal swings. With signals as described at Points C and D, the MC145170-2 is guaranteed to operate down to a frequency as low as dc. Refer to the MC74HC14A data sheet for input switching levels and hysteresis voltage range.

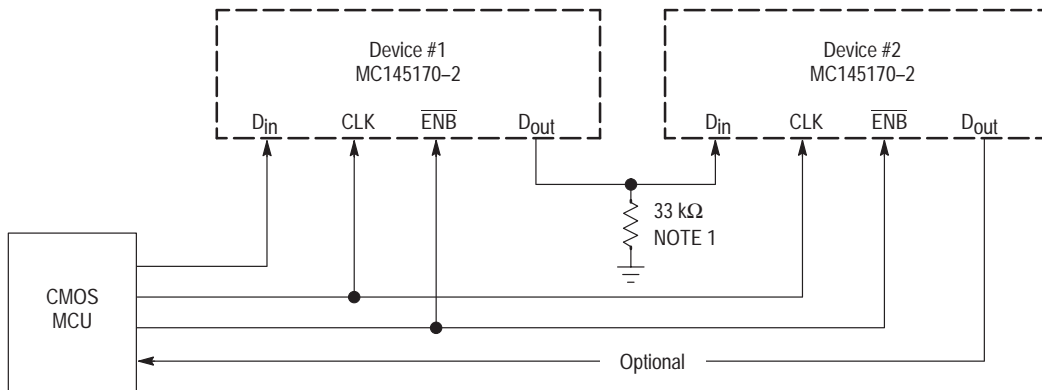
MC145170-2

Figure 23. Input Impedance at f_{in} — Series Format ($R + jX$)
(5.0 MHz to 185 MHz)



Marker	Frequency (MHz)	Resistance (Ω)	Reactance (Ω)	Capacitance (pF)
1	5	2390	-5900	5.39
2	100	39.2	-347	4.58
3	150	25.8	-237	4.48
4	185	42.6	-180	4.79

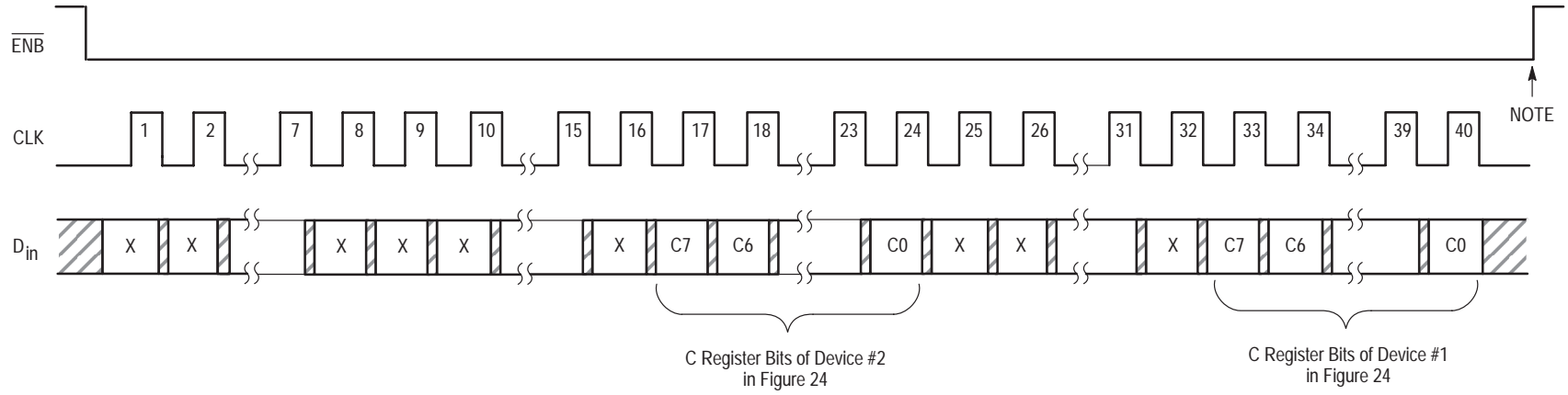
Figure 24. Cascading Two MC145170-2 Devices



NOTES:

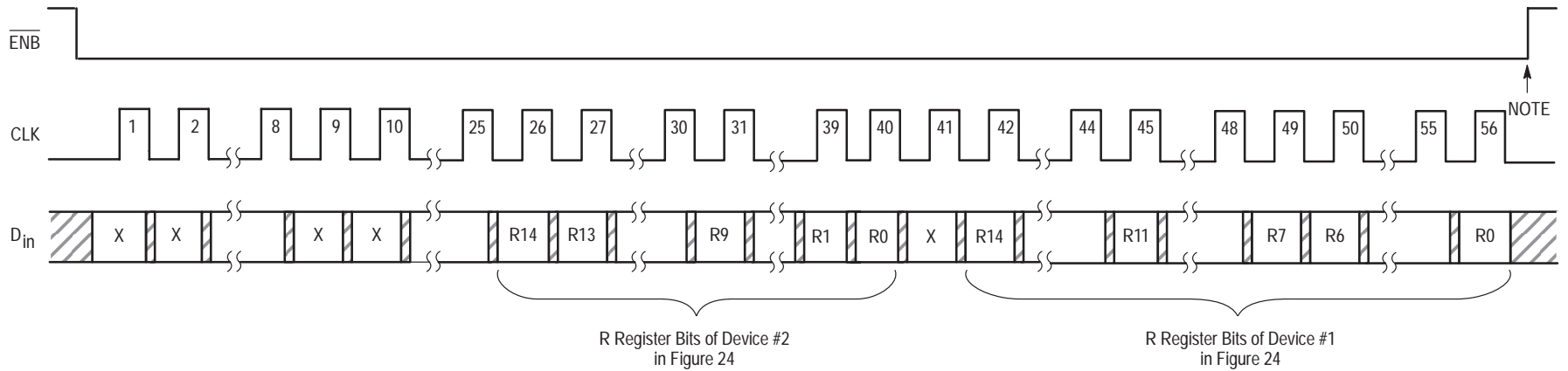
- 1 The 33 k Ω resistor is needed to prevent the D_{in} pin from floating. (The D_{out} pin is a three-state output.)
- 2 See related Figures 25, 26, and 27.

Figure 25. Accessing the C Registers of Two Cascaded MC145170-2 Devices



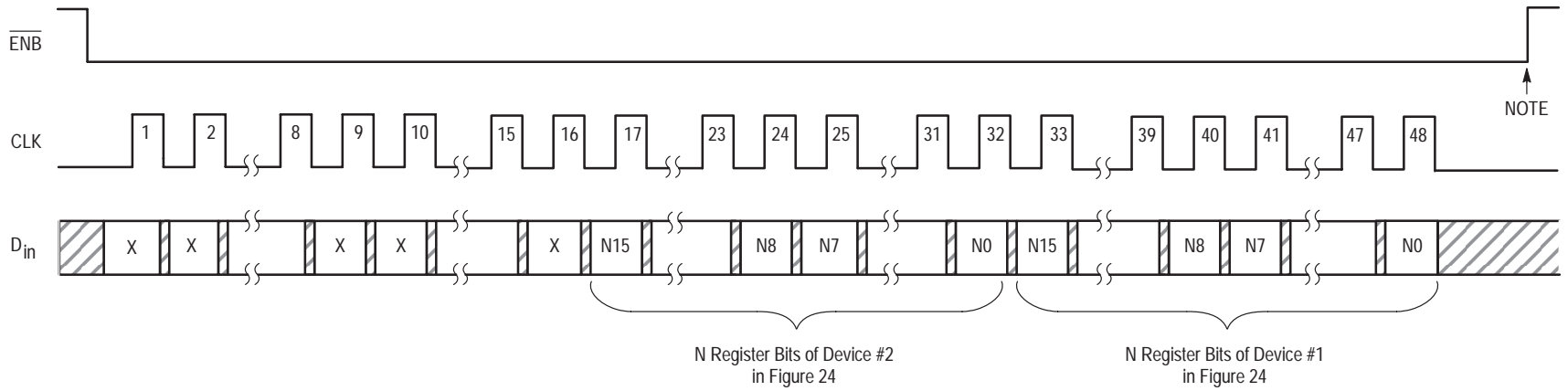
NOTE: At this point, the new data is transferred to the C registers of both devices and stored. No other registers are affected.

Figure 26. Accessing the R Registers of Two Cascaded MC145170-2 Devices



NOTE: At this point, the new data is transferred to the R registers of both devices and stored. No other registers are affected.

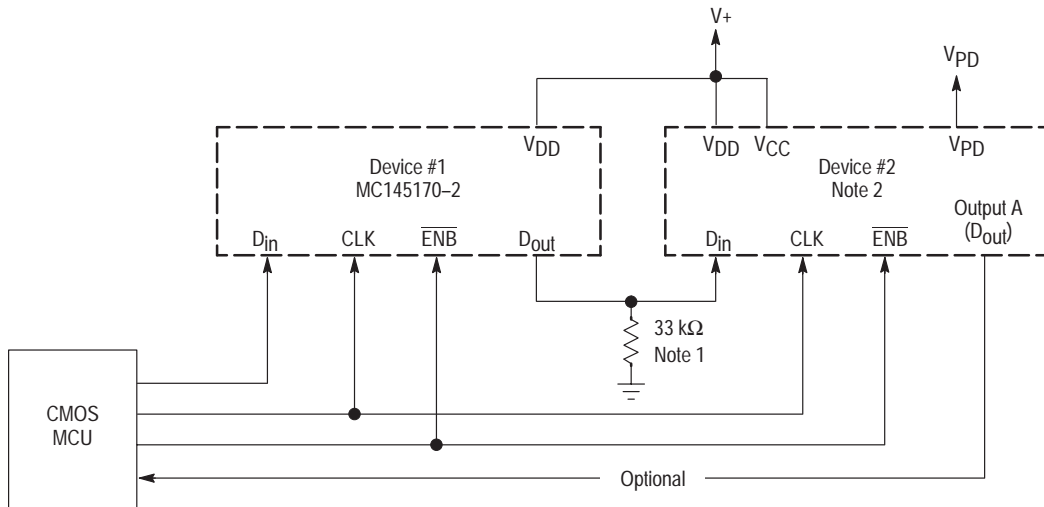
Figure 27. Accessing the N Registers of Two Cascaded MC145170-2 Devices



NOTE: At this point, the new data is transferred to the N registers of both devices and stored. No other registers are affected.

MC145170-2

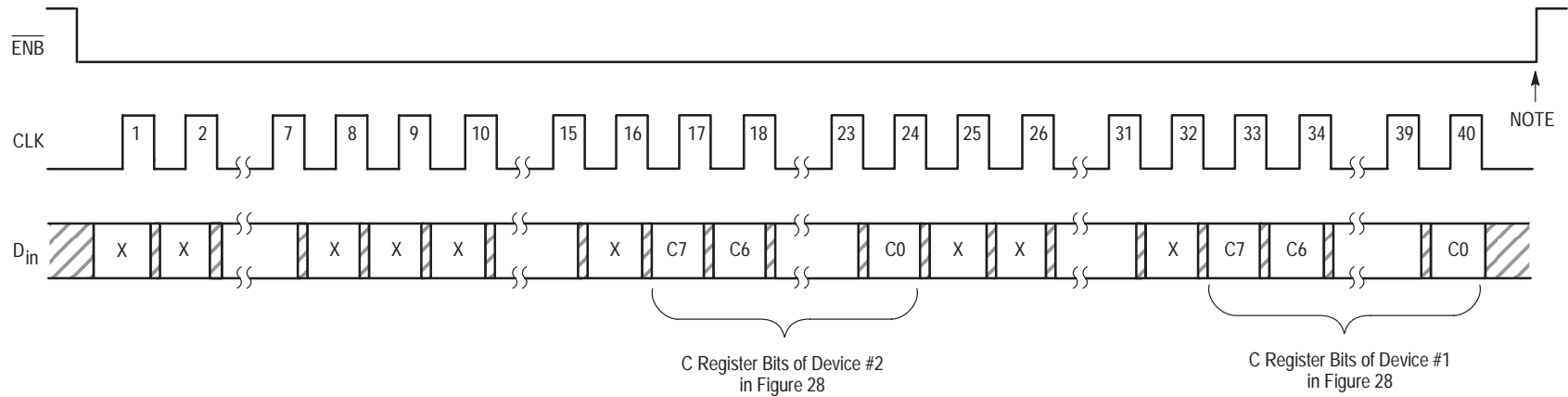
Figure 28. Cascading Two Different Device Types



NOTES:

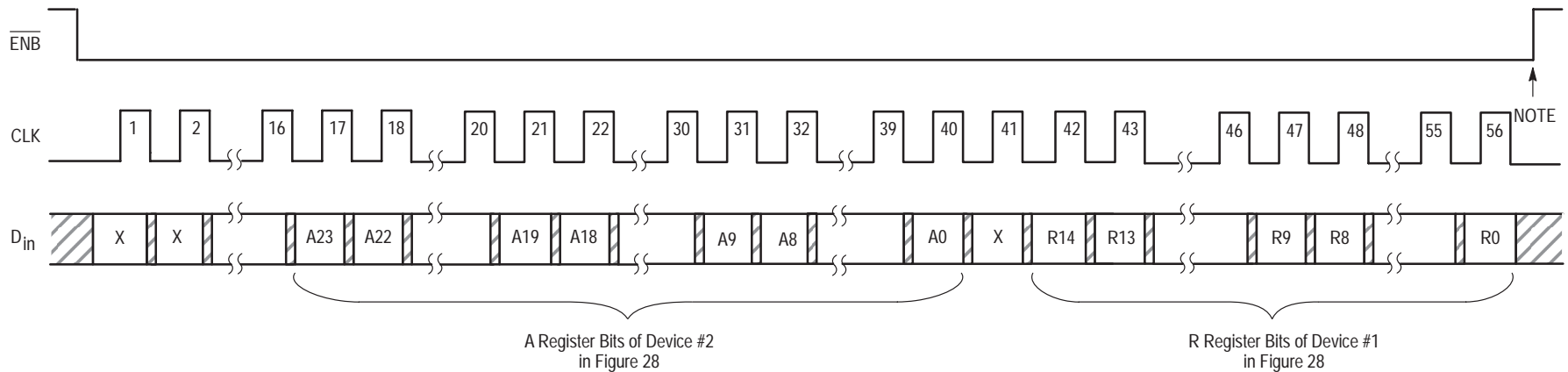
- 1 The 33 kΩ resistor is needed to prevent the D_{in} pin from floating. (The D_{out} pin is a three-state output.)
- 2 This PLL Frequency Synthesizer may be a MC145190, MC145191, MC145192, MC145200, or MC145201.
- 3 See related Figures 29, 30, and 31.

Figure 29. Accessing the C Registers of Two Different Device Types



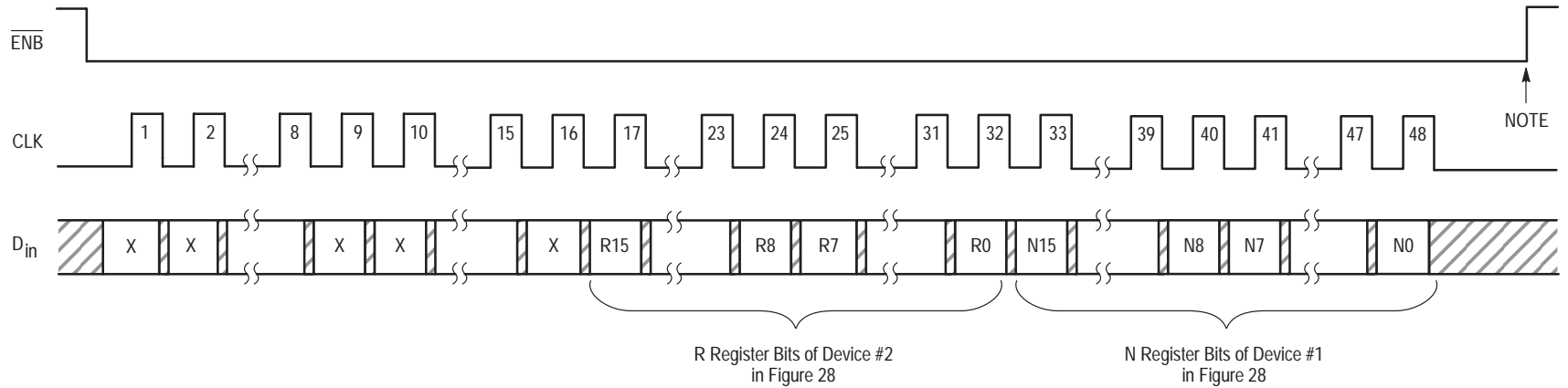
NOTE: At this point, the new data is transferred to the C registers of both devices and stored. No other registers are affected.

Figure 30. Accessing the A and R Registers of Two Different Device Types



NOTE: At this point, the new data is transferred to the A register of Device #2 and R register of Device #1 and stored. No other registers are affected.

Figure 31. Accessing the R and N Registers of Two Different Device Types



NOTE: At this point, the new data is transferred to the R register of Device #2 and N register of Device #1 and stored. No other registers are affected.

1.1 GHz PLL Frequency Synthesizer

The MC145193 is recommended for new designs and offers reduced power consumption. The counters are programmed via a synchronous serial port which is SPI compatible. The serial port is byte-oriented to facilitate control via an MCU. Due to the innovative BitGrabber Plus™ registers, the MC145193 may be cascaded with other peripherals featuring BitGrabber Plus without requiring leading dummy bits or address bits in the serial data stream. In addition, BitGrabber Plus peripherals may be cascaded with existing BitGrabber™ peripherals.

The device features a single-ended current source/sink phase detector A output and a double-ended phase detector B output. Both phase detectors have linear transfer functions (no dead zones). The maximum current of the single-ended phase detector output is determined by an external resistor tied from the Rx pin to ground. This current can be varied via the serial port.

Slew-rate control is provided by a special driver designed for the REF_{out} pin. This minimizes interference caused by REF_{out}.

This part includes a differential RF input that may be operated in a single-ended mode. Also featured are on-board support of an external crystal and a programmable reference output. The R, A, and N counters are fully programmable. The C register (configuration register) allows the part to be configured to meet various applications. A patented feature allows the C register to shut off unused outputs, thereby minimizing system noise and interference.

In order to have consistent lock times and prevent erroneous data from being loaded into the counters, on-board circuitry synchronizes the update of the A register if the A or N counters are loading. Similarly, an update of the R register is synchronized if the R counter is loading.

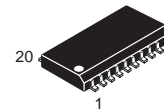
The double-buffered R register allows new divide ratios to be presented to the three counters (R, A, and N) simultaneously.

- Maximum Operating Frequency: 1100 MHz @ – 10 dBm
- Operating Supply Current: 3 mA Nominal at 3.0 V
- Operating Supply Voltage Range (V_{DD} , V_{CC} , V_{PD} Pins): 2.7 to 5.5 V
- Current Source/Sink Phase Detector Output:
1.7 mA @ 5.0 V or 1.0 mA @ 3.0 V
- Gain of Current Source/Sink Phase/Frequency Detector Controllable via Serial Port
- R Counter Division Range: 1 and 5 to 8191
- Dual-Modulus Capability Provides Total Division up to 262,143
- High-Speed Serial Interface: 4 Mbps
- Output A Pin, When Configured as Data Out, Permits Cascading of Devices
- Two General-Purpose Digital Outputs:
Output A: Totem-Pole (Push-Pull) with Four Output Modes
Output B: Open-Drain
- Patented Power-Saving Standby Feature with Orderly Recovery for Minimizing Lock Times, Standby Current: 30 μ A
- See App Note AN1253/D for Low-Pass Filter Design, and AN1277/D for Offset Reference PLLs for Fine Resolution or Fast Hopping

MC145193

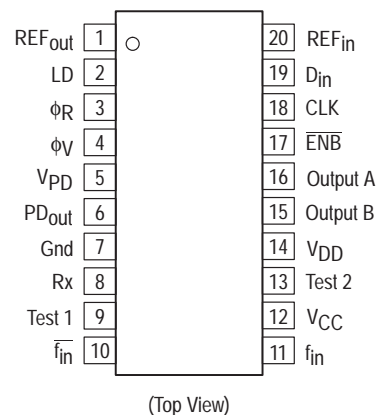
PLL FREQUENCY SYNTHESIZER

SEMICONDUCTOR TECHNICAL DATA



F SUFFIX
PLASTIC PACKAGE
CASE 751J
(SO-20)

PIN CONNECTIONS



EVALUATION KIT

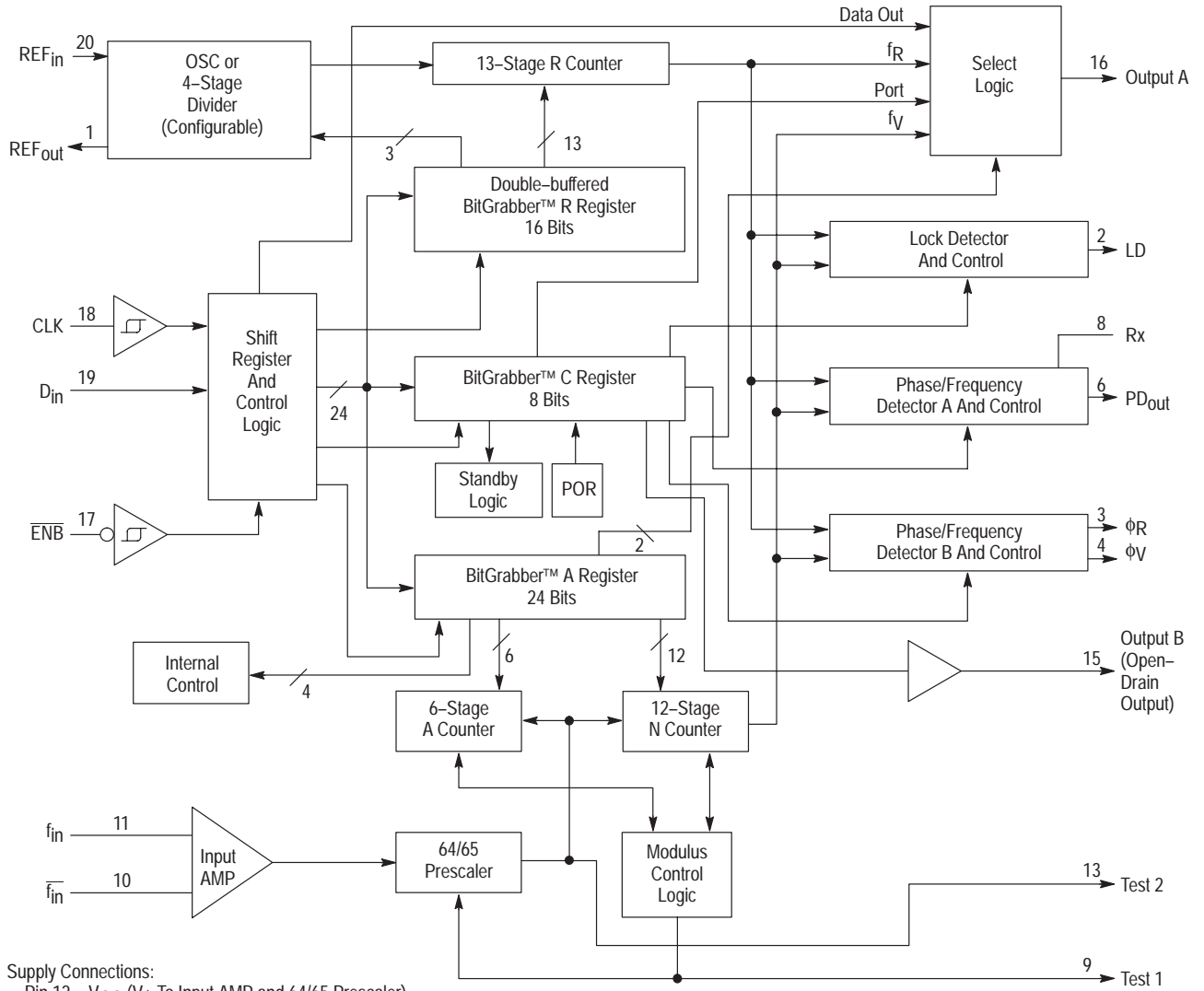
The MC145193EVK, which contains hardware and software, is available.

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC145193F	$T_A = -40$ to 85°C	SO-20

MC145193

BLOCK DIAGRAM



Supply Connections:
 Pin 12 = V_{CC} ($V+$ To Input AMP and 64/65 Prescaler)
 Pin 5 = V_{PD} ($V+$ To Phase/Frequency Detectors A and B)
 Pin 14 = V_{DD} ($V+$ To Balance Of Circuit)
 Pin 7 = Gnd (Common Ground)

This device contains 7,278 active transistors.

MC145193

MAXIMUM RATINGS* (Voltages Referenced to Gnd, unless otherwise stated)

Parameter	Symbol	Value	Unit
DC Supply Voltage (Pins 12 and 14)	V_{CC}, V_{DD}	-0.5 to 6.0	V
DC Supply Voltage (Pin 5)	V_{PD}	$V_{DD} - 0.5$ to 6.0	V
DC Input Voltage	V_{in}	-0.5 to $V_{DD} + 0.5$	V
DC Output Voltage (except Output B, PD_{out} , ϕ_R , ϕ_V)	V_{out}	-0.5 to $V_{DD} + 0.5$	V
DC Output Voltage (Output B, PD_{out} , ϕ_R , ϕ_V)	V_{out}	-0.5 to $V_{PD} + 0.5$	V
DC Input Current, per Pin (Includes V_{PD})	I_{in}, I_{PD}	± 10	mA
DC Output Current, per Pin	I_{out}	± 20	mA
DC Supply Current, V_{DD} and Gnd Pins	I_{DD}	± 30	mA
Power Dissipation, per Package	P_D	300	mW
Storage Temperature	T_{stg}	-65 to 150	°C
Lead Temperature, 1 mm from Case for 10 Seconds	T_L	260	°C

This device contains protection circuitry to guard against damage due to high static voltages or electric fields. However, precautions must be taken to avoid applications of any voltage higher than maximum rated voltages to this high-impedance circuit.

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section.
 2. ESD (electrostatic discharge) immunity meets Human Body Model (HBM) ≤ 2000 V and Machine Model (MM) ≤ 200 V. Additional ESD data available upon request.

ELECTRICAL CHARACTERISTICS

($V_{DD} = V_{CC} = 2.7$ to 5.5 V, Voltages Referenced to Gnd, unless otherwise stated; $V_{PD} = 2.7$ to 5.5 V, $T_A = -40$ to 85°C)

Parameter	Test Condition	Symbol	Guaranteed Limit	Unit
Maximum Low-Level Input Voltage (D_{in} , CLK, \overline{ENB})		V_{IL}	$0.3 \times V_{DD}$	V
Minimum High-Level Input Voltage (D_{in} , CLK, \overline{ENB})		V_{IH}	$0.7 \times V_{DD}$	V
Minimum Hysteresis Voltage (CLK, \overline{ENB})	$V_{DD} = 2.7$ V $V_{DD} = 4.5$ V	V_{Hys}	100 250	mV
Maximum Low-Level Output Voltage (REF_{out} , Output A)	$I_{out} = 20 \mu\text{A}$, Device in Reference Mode	V_{OL}	0.1	V
Minimum High-Level Output Voltage (REF_{out} , Output A)	$I_{out} = -20 \mu\text{A}$, Device in Reference Mode	V_{OH}	$V_{DD} - 0.1$	V
Minimum Low-Level Output Current (REF_{out} , LD)	$V_{out} = 0.3$ V	I_{OL}	0.36	mA
Minimum Low-Level Output Current (ϕ_R , ϕ_V)	$V_{out} = 0.3$ V	I_{OL}	0.36	mA
Minimum Low-Level Output Current (Output A)	$V_{out} = 0.4$ V $V_{DD} = 4.5$ V	I_{OL}	1.0	mA
Minimum Low-Level Output Current (Output B)	$V_{out} = 0.4$ V	I_{OL}	1.0	mA
Minimum High-Level Output Current (REF_{out} , LD)	$V_{out} = V_{DD} - 0.3$ V	I_{OH}	-0.36	mA
Minimum High-Level Output Current (ϕ_R , ϕ_V)	$V_{out} = V_{PD} - 0.3$ V	I_{OH}	-0.36	mA
Minimum High-Level Output Current (Output A Only)	$V_{out} = V_{DD} - 0.4$ V $V_{DD} = 4.5$ V	I_{OH}	-0.6	mA

(continued)

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test Condition	Symbol	Guaranteed Limit	Unit
Maximum Input Leakage Current (D _{in} , CLK, $\overline{\text{ENB}}$, REF _{in})	V _{in} = V _{DD} or Gnd, Device in XTAL Mode	I _{in}	±1.0	μA
Maximum Input Current (REF _{in})	V _{in} = V _{DD} or Gnd, Device in Reference Mode	I _{in}	±100	μA
Maximum Output Leakage Current (PD _{out}) (Output B)	V _{out} = V _{PD} or Gnd, Output in Floating State	I _{OZ}	±130	nA
	V _{out} = V _{PD} or Gnd, Output in High-Impedance State		±1	μA
Maximum Standby Supply Current (V _{DD} + V _{PD} Pins)	V _{in} = V _{DD} or Gnd; Outputs Open; Device in Standby Mode, Shut-Down Crystal Mode or REF _{out} -Static-Low Reference Mode; Output B Controlling V _{CC} per Figure 21	I _{STBY}	30	μA
Maximum Phase Detector Quiescent Current (V _{PD} Pin)	Bit C6 = High Which Selects Phase Detector A, PD _{out} = Open, PD _{out} = Static State, Bit C4 = Low Which is not Standby, I _{Rx} = 170 μA, V _{PD} = 5.5 V	I _{PD}	750	μA
	Bit C6 = Low Which Selects Phase Detector B, φ _R and φ _V = Open, φ _R and φ _V = Static Low or High, Bit C4 = Low Which is not Standby		30	
Total Operating Supply Current (V _{DD} + V _{PD} + V _{CC} Pins)	f _{in} = 2.0 GHz; REF _{in} = 13 MHz @ 1 V _{pp} ; Output A = Inactive and No Connect; V _{DD} = V _{CC} , REF _{out} , φ _V , φ _R , PD _{out} , LD = No Connect; D _{in} , $\overline{\text{ENB}}$, CLK = V _{DD} or Gnd, Phase Detector B Selected (Bit C6 = Low)	I _T	[Note]	mA

NOTE: The nominal value is: 3 mA at V_{DD} = V_{CC} = V_{PD} = 3.0 V. This is not a guaranteed limit.

ANALOG CHARACTERISTICS — CURRENT SOURCE/SINK OUTPUT — PD_{out}

(I_{out} ≤ 1 mA @ V_{DD} = 2.7 V and I_{out} ≤ 1.7mA @ V_{DD} ≥ 4.5 V, V_{DD} = V_{CC} = 2.7 to 5.5 V, Voltages Referenced to Gnd)

Parameter	Test Condition	V _{PD}	Guaranteed Limit	Unit
Maximum Source Current Variation (Part-to-Part)	V _{out} = 0.5 x V _{PD}	2.7	±15	%
		4.5	±15	
		5.5	±15	
Maximum Sink-vs-Source Mismatch [Note 3]	V _{out} = 0.5 x V _{PD}	2.7	11	%
		4.5	11	
		5.5	11	
Output Voltage Range [Note 3]	I _{out} Variation ≤ 15%	2.7	0.5 to 2.2	V
	I _{out} Variation ≤ 20%	4.5	0.5 to 3.7	
	I _{out} Variation ≤ 22%	5.5	0.5 to 4.7	

NOTES: 1. Percentages calculated using the following formula: (Maximum Value – Minimum Value)/Maximum Value.

2. See Rx Pin Description for external resistor values.

3. This parameter is guaranteed for a given temperature within –40 to 85°C.

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AC INTERFACE CHARACTERISTICS

($V_{DD} = V_{CC} = 2.7$ to 5.5 V, $T_A = -40$ to $+85^\circ\text{C}$, $C_L = 25$ pF, Input $t_r = t_f = 10$ ns; $V_{PD} = 2.7$ to 5.5 V)

Parameter	Figure No.	Symbol	Guaranteed Limit	Unit
Serial Data Clock Frequency (Note: Refer to Clock t_w below)	1	f_{clk}	dc to 4.0	MHz
Maximum Propagation Delay, CLK to Output A (Selected as Data Out)	1, 5	t_{PLH} , t_{PHL}	100	ns
Maximum Propagation Delay, $\overline{\text{ENB}}$ to Output A (Selected as Port)	2, 5	t_{PLH} , t_{PHL}	150	ns
Maximum Propagation Delay, $\overline{\text{ENB}}$ to Output B	2, 6	t_{PZL} , t_{PLZ}	150	ns
Maximum Output Transition Time, Output A and Output B; t_{THL} only, on Output B	1, 5, 6	t_{TLH} , t_{THL}	50	ns
Maximum Input Capacitance – D_{in} , $\overline{\text{ENB}}$, CLK		C_{in}	10	pF

TIMING REQUIREMENTS

($V_{DD} = V_{CC} = 2.7$ to 5.5 V, $T_A = -40$ to $+85^\circ\text{C}$, Input $t_r = t_f = 10$ ns, unless otherwise indicated)

Parameter	Figure No.	Symbol	Guaranteed Limit	Unit
Minimum Setup and Hold Times, D_{in} vs CLK	3	t_{su} , t_{h}	50	ns
Minimum Setup, Hold and Recovery Times, $\overline{\text{ENB}}$ vs CLK	4	t_{su} , t_{h} , t_{rec}	100	ns
Minimum Pulse Width, $\overline{\text{ENB}}$	4	t_w	[Note]	cycles
Minimum Pulse Width, CLK	1	t_w	125	ns
Maximum Input Rise and Fall Times, CLK	1	t_r , t_f	100	μs

NOTE: The minimum limit is 3 REF_{in} cycles or 195 f_{in} cycles, whichever is greater.

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SWITCHING WAVEFORMS

Figure 1.

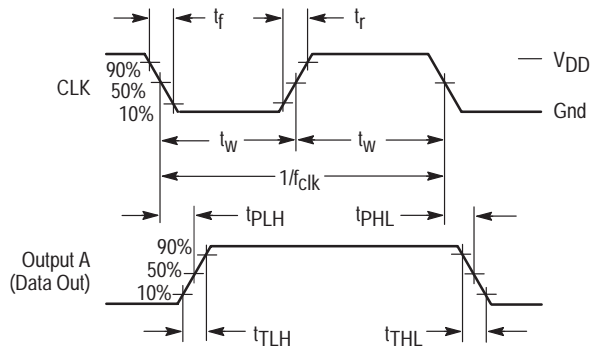


Figure 2.

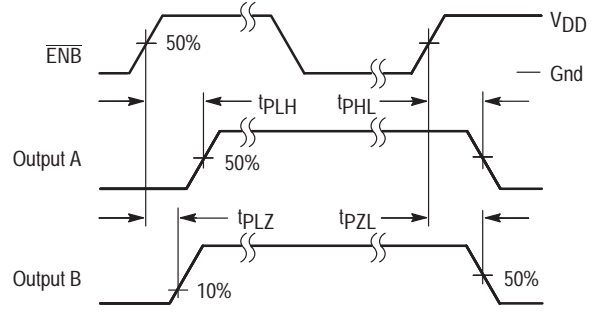


Figure 3.

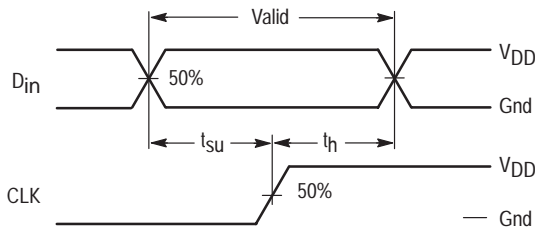


Figure 4.

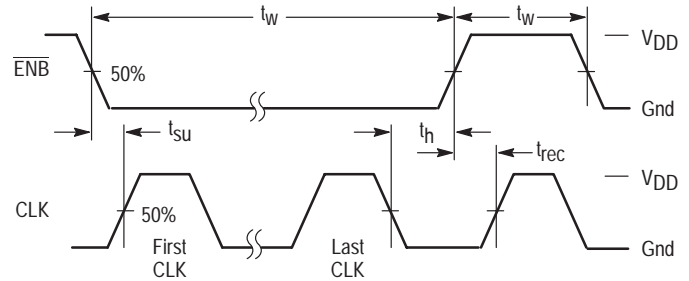
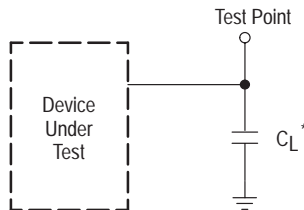
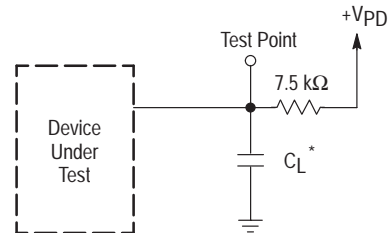


Figure 5.



* Includes all probe and fixture capacitance.

Figure 6.



* Includes all probe and fixture capacitance.

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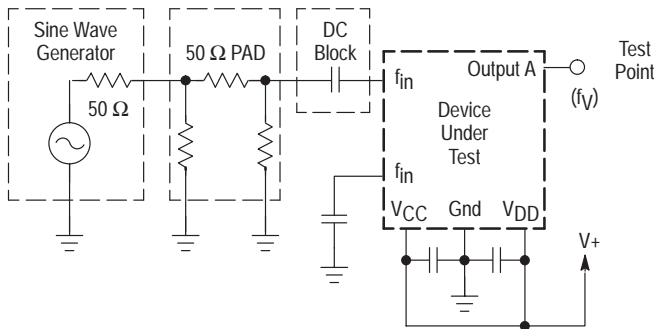
LOOP SPECIFICATIONS ($V_{DD} = V_{CC} = 2.7$ to 5.5 V unless otherwise indicated, $T_A = -40$ to 85°C)

Parameter	Test Condition	Fig. No.	Symbol	Guaranteed Operating Range		Unit
				Min	Max	
Input Sensitivity Range, f_{in}	$100 \text{ MHz} \leq f_{in} \leq 1100 \text{ MHz}$	7	P_{in}	-10	4	dBm*
Input Frequency, REF_{in} Externally Driven in Reference Mode	$V_{in} \geq 400 \text{ mVpp}$ $2.7 \leq V_{DD} < 4.5 \text{ V}$ $4.5 \leq V_{DD} \leq 5.5 \text{ V}$	8	f_{ref}	1.5	20	MHz
Crystal Frequency, Crystal Mode	$C_1 \leq 30 \text{ pF}$, $C_2 \leq 30 \text{ pF}$, Includes Stray Capacitance	9	f_{XTAL}	2	15	MHz
Output Frequency, REF_{out}	$C_L = 20 \text{ pF}$, $V_{out} \geq 1 \text{ Vpp}$	10, 12	f_{out}	dc	10	MHz
Operating Frequency of the Phase Detectors			f_ϕ	dc	2	MHz
Output Pulse Width (ϕ_R , ϕ_V , and LD)	f_R in Phase with f_V , $C_L = 20 \text{ pF}$, ϕ_R and ϕ_V active for LD measurement, ** $V_{PD} = 2.7$ to 5.5 V	11, 12	t_w			ns
Output Transition Times (LD, ϕ_V , and ϕ_R)	$C_L = 20 \text{ pF}$, $V_{PD} = 2.7 \text{ V}$, $V_{DD} = V_{CC} = 2.7 \text{ V}$	11, 12	t_{TLH} , t_{THL}	—	80	ns
Input Capacitance, REF_{in}			C_{in}	—	7	pF

* Power level at the input to the dc block.

** When PD_{out} is active, LD minimum pulse width is approximately 5 ns.

Figure 7. Test Circuit



NOTE: Alternately, the 50 Ω pad may be a T network.

Figure 8. Test Circuit — Reference Mode

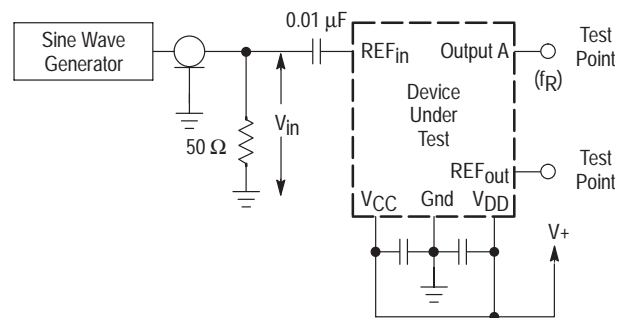


Figure 9. Test Circuit — Crystal Mode

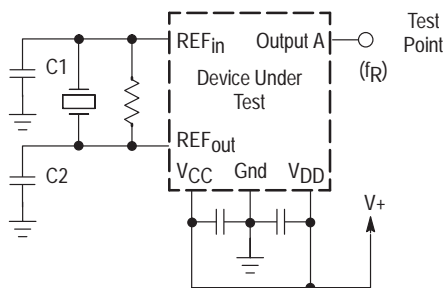


Figure 10. Switching Waveform

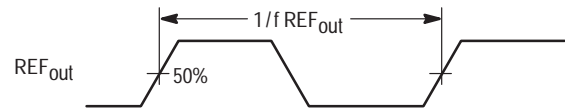


Figure 11. Switching Waveform

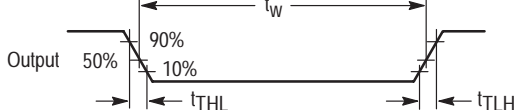
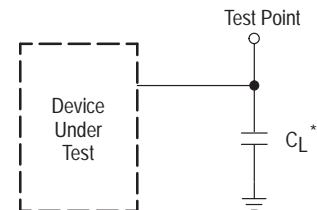


Figure 12. Test Circuit



* Includes all probe and fixture capacitance.

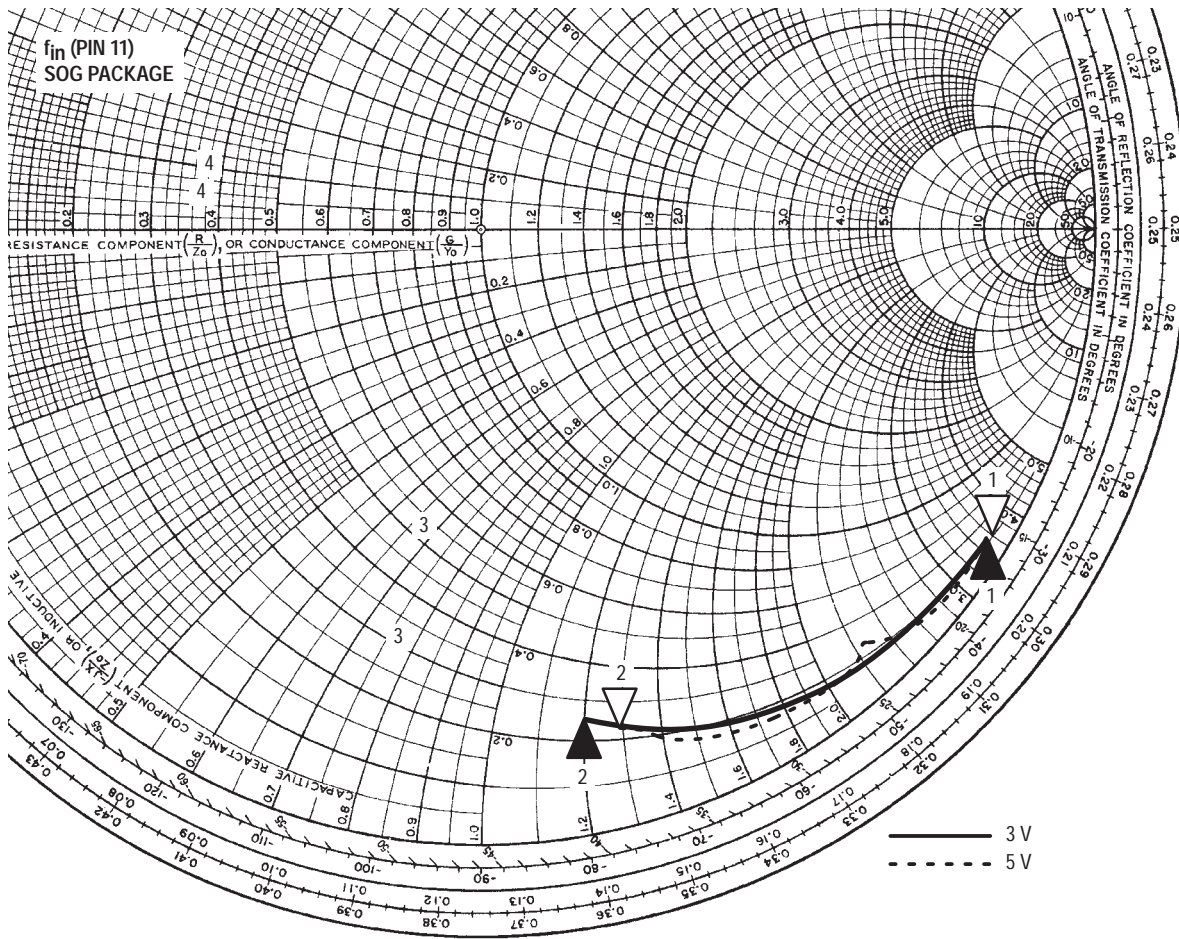


Figure 13. Normalized Input Impedance at f_{in} — Series Format ($R + jx$)

Table 1. Input Impedance at f_{in} — Series Format ($R + jx$), $V_{CC} = 3\text{ V}$

Marker	Frequency (GHz)	Resistance (Ω)	Reactance (Ω)	Capacitance/Inductance
1	0.5	11.4	-168	1.9 pF
2	1	12.4	-59.4	2.68 pF

Table 2. Input Impedance at f_{in} — Series Format ($R + jx$), $V_{CC} = 5\text{ V}$

Marker	Frequency (GHz)	Resistance (Ω)	Reactance (Ω)	Capacitance/Inductance
1	0.5	11.8	-175	1.82 pF
2	1	11.5	-64.4	2.47 pF

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PIN DESCRIPTIONS

DIGITAL INTERFACE PINS

D_{in} Serial Data Input (Pin 19)

The bit stream begins with the most significant bit (MSB) and is shifted in on the low-to-high transition of CLK. The bit pattern is 1 byte (8 bits) long to access the C or configuration register, 2 bytes (16 bits) to access the first buffer of the R register, or 3 bytes (24 bits) to access the A register (see Table 3). The values in the C, R, and A registers do not change during shifting because the transfer of data to the registers is controlled by $\overline{\text{ENB}}$.

CAUTION

The value programmed for the N counter must be greater than or equal to the value of the A counter.

The 13 least significant bits (LSBs) of the R register are double-buffered. As indicated above, data is latched into the first buffer on a 16-bit transfer. (The 3 MSBs are not double-buffered and have an immediate effect after a 16-bit transfer.) The second buffer of the R register contains the 13 bits for the R counter. This second buffer is loaded with the contents of the first buffer when the A register is loaded (a 24-bit transfer). This allows presenting new values to the R, A, and N counters simultaneously. If this is not required, then the 16-bit transfer may be followed by pulsing $\overline{\text{ENB}}$ low with no signal on the CLK pin. This is an alternate method of transferring data to the second buffer of the R register (see Figure 16).

The bit stream needs neither address nor steering bits due to the innovative BitGrabber Plus registers. Therefore, all bits in the stream are available to be data for the three registers. Random access of any register is provided (i.e., the registers may be accessed in any sequence). Data is retained in the registers over a supply range of 2.7 to 5.5 V. The formats are shown in Figures 14, 15, and 16.

D_{in} typically switches near 50% of V_{DD} to maximize noise immunity. This input can be directly interfaced to CMOS devices with outputs guaranteed to switch near rail-to-rail. When interfacing to NMOS or TTL devices, either a level shifter (MC74HC14A, MC14504B) or pull-up resistor of 1 k Ω to 10 k Ω must be used. Parameters to consider when sizing the resistor are worst-case I_{OL} of the driving device, maximum tolerable power consumption, and maximum data rate.

Table 3. Register Access

(MSBs are shifted in first; C0, R0, and A0 are the LSBs)

Number of Clocks	Accessed Register	Bit Nomenclature
8	C Register	C7, C6, C5, . . . , C0
16	R Register	R15, R14, R13, . . . , R0
24	A Register	A23, A22, A21, . . . , A0
Other Values \leq 32 Values $>$ 32	Not Allowed See Figures 22 – 25	

CLK Serial Data Clock Input (Pin 18)

Low-to-high transitions on CLK shift bits available at the D_{in} pin, while high-to-low transitions shift bits from Output A (when configured as Data Out, see Pin 16). The 24-1/2-stage shift register is static, allowing clock rates down to dc in a continuous or intermittent mode.

Eight clock cycles are required to access the C register. Sixteen clock cycles are needed for the first buffer of the R register. Twenty-four cycles are used to access the A register. See Table 3 and Figures 14, 15, and 16. The number of clocks required for cascaded devices is shown in Figures 23 through 25.

CLK typically switches near 50% of V_{DD} and has a Schmitt-triggered input buffer. Slow CLK rise and fall times are allowed. See the last paragraph of D_{in} for more information.

NOTE

To guarantee proper operation of the power-on reset (POR) circuit, the CLK pin must be held at Gnd (with $\overline{\text{ENB}}$ being a don't care) or $\overline{\text{ENB}}$ must be held at the potential of the V+ pin (with CLK being a don't care) during power-up. Floating, toggling, or having these pins in the wrong state during power-up does not harm the chip, but causes two potentially undesirable effects. First, the outputs of the device power up in an unknown state. Second, if two devices are cascaded, the A Registers must be written twice after power up. After these two accesses, the two cascaded chips perform normally.

$\overline{\text{ENB}}$ Active Low Enable Input (Pin 17)

This pin is used to activate the serial interface to allow the transfer of data to/from the device. When $\overline{\text{ENB}}$ is in an inactive high state, shifting is inhibited and the port is held in the initialized state. To transfer data to the device, $\overline{\text{ENB}}$ (which must start inactive high) is taken low, a serial transfer is made via D_{in} and CLK, and $\overline{\text{ENB}}$ is taken back high. The low-to-high transition on $\overline{\text{ENB}}$ transfers data to the C or A registers and first buffer of the R register, depending on the data stream length per Table 3.

Transitions on $\overline{\text{ENB}}$ must not be attempted while CLK is high. This puts the device out of synchronization with the microcontroller. Resynchronization occurs when $\overline{\text{ENB}}$ is high and CLK is low.

This input is also Schmitt-triggered and switches near 50% of V_{DD}, thereby minimizing the chance of loading erroneous data into the registers. See the last paragraph of D_{in} for more information.

For POR information, see the note for the CLK pin.

Output A**Configurable Digital Output (Pin 16)**

Output A is selectable as f_R , f_V , Data Out, or Port. Bits A22 and A23 in the A register control the selection; see Figure 15.

If A23 = A22 = high, Output A is configured as f_R . This signal is the buffered output of the 13-stage R counter. The f_R signal appears as normally low and pulses high. The f_R signal can be used to verify the divide ratio of the R counter. This ratio extends from 5 to 8191 and is determined by the binary value loaded into bits R0–R12 in the R register. Also, direct access to the phase detectors via the REF_{in} pin is allowed by choosing a divide value of 1 (see Figure 16). The maximum frequency at which the phase detectors operate is 2 MHz. Therefore, the frequency of f_R should not exceed 2 MHz.

If A23 = high and A22 = low, Output A is configured as f_V . This signal is the buffered output of the 12-stage N counter. The f_V signal appears as normally low and pulses high. The f_V signal can be used to verify the operation of the prescaler, A counter, and N counter. The divide ratio between the f_{in} input and the f_V signal is $N \times 64 + A$. N is the divide ratio of the N counter and A is the divide ratio of the A counter. These ratios are determined by bits loaded into the A register. See Figure 15. The maximum frequency at which the phase detectors operate is 2 MHz. Therefore, the frequency of f_V should not exceed 2 MHz.

If A23 = low and A22 = high, Output A is configured as Data Out. This signal is the serial output of the 24–1/2-stage shift register. The bit stream is shifted out on the high-to-low transition of the CLK input. Upon power up, Output A is automatically configured as Data Out to facilitate cascading devices.

If A23 = A22 = low, Output A is configured as Port. This signal is a general-purpose digital output which may be used as an MCU port expander. This signal is low when the Port bit (C1) of the C register is low, and high when the Port bit is high.

Output B**Open-Drain Digital Output (Pin 15)**

This signal is a general-purpose digital output which may be used as an MCU port expander. This signal is low when the Out B bit (C0) of the C register is low. When the Out B bit is high, Output B assumes the high-impedance state. Output B may be pulled up through an external resistor or active circuitry to any voltage less than or equal to the potential of the V_{PD} pin. **Note:** the maximum voltage allowed on the V_{PD} pin is 5.5 V.

Upon power-up, power-on reset circuitry forces Output B to a low level.

REFERENCE PINS **REF_{in} and REF_{out}** **Reference Input and Reference Output (Pins 20 and 1)**

Configurable pins for a Crystal or an External Reference. This pair of pins can be configured in one of two modes: the crystal mode or the reference mode. Bits R13, R14, and R15 in the R register control the modes as shown in Figure 16.

In crystal mode, these pins form a reference oscillator when connected to terminals of an external parallel-resonant

crystal. Frequency-setting capacitors of appropriate values, as recommended by the crystal supplier, are connected from each of the two pins to ground (up to a maximum of 30 pF each, including stray capacitance). An external resistor of 1 M Ω to 15 M Ω is connected directly across the pins to ensure linear operation of the amplifier. The required connections for the components are shown in Figure 9.

To turn on the oscillator, bits R15, R14, and R13 must have an octal value of one (001 in binary, respectively). This is the active-crystal mode shown in Figure 16. In this mode, the crystal oscillator runs and the R Counter divides the crystal frequency, unless the part is in standby. If the part is placed in standby via the C register, the oscillator runs, but the R counter is stopped. However, if bits R15 to R13 have a value of 0, the oscillator is stopped, which saves additional power. This is the shut-down crystal mode (shown in Figure 16) and can be engaged whether in standby or not.

In the reference mode, REF_{in} (Pin 20) accepts a signal from an external reference oscillator, such as a TCXO. A signal swinging from at least the V_{IL} to V_{IH} levels listed in the Electrical Characteristics table may be directly coupled to the pin. If the signal is less than this level, ac coupling must be used as shown in Figure 8. Due to an on-board resistor which is engaged in the reference modes, an external biasing resistor tied between REF_{in} and REF_{out} is not required.

With the reference mode, the REF_{out} pin is configured as the output of a divider. As an example, if bits R15, R14, and R13 have an octal value of seven, the frequency at REF_{out} is the REF_{in} frequency divided by 16. In addition, Figure 16 shows how to obtain ratios of eight, four, and two. A ratio of one-to-one can be obtained with an octal value of three. Upon power up, a ratio of eight is automatically initialized. The maximum frequency capability of the REF_{out} pin is listed in the Loop Specifications table for an output swing of 1 V_{pp} and 20 pF loads. Therefore, for higher REF_{in} frequencies, the one-to-one ratio may not be used for this magnitude of signal swing and loading requirements. Likewise, for REF_{in} frequencies above two times the highest rated frequency, the ratio must be more than two.

The output has a special on-board driver that has slew-rate control. This feature minimizes interference in the application.

If REF_{out} is unused, an octal value of two should be used for R15, R14, and R13 and the REF_{out} pin should be floated. A value of two allows REF_{in} to be functional while disabling REF_{out} , which minimizes dynamic power consumption.

LOOP PINS **f_{in} and $\overline{f_{in}}$
Frequency Inputs (Pins 11 and 10)**

These pins are frequency inputs from the VCO. These pins feed the on-board RF amplifier which drives the 64/65 prescaler. These inputs may be fed differentially. However, they are usually used in a single-ended configuration (shown in Figure 7). Note that f_{in} is driven while $\overline{f_{in}}$ must be tied to ground via a capacitor.

Motorola does not recommend driving $\overline{f_{in}}$ while terminating f_{in} because this configuration is not tested for sensitivity. The sensitivity is dependent on the frequency as shown in the Loop Specifications table.

PD_{out} Single-Ended Phase/Frequency Detector Output (Pin 6)

This is a three-state current-source/sink output for use as a loop error signal when combined with an external low-pass filter. The phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detector is described below and is shown in Figure 17.

POL bit (C7) in the C register = low (see Figure 14)

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : current-sinking pulses from a floating state

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : current-sourcing pulses from a floating state

Frequency and Phase of $f_V = f_R$: essentially a floating state; voltage at pin determined by loop filter

POL bit (C7) = high

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : current-sourcing pulses from a floating state

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : current-sinking pulses from a floating state

Frequency and Phase of $f_V = f_R$: essentially a floating state; voltage at pin determined by loop filter

This output can be enabled, disabled, and inverted via the C register. If desired, PD_{out} can be forced to the high-impedance state by utilization of the disable feature in the C register (bit C6). This is a patented feature. Similarly, PD_{out} is forced to the high-impedance state when the device is put into standby (STBY bit C4 = high).

The PD_{out} circuit is powered by V_{PD}. The phase detector gain is controllable by bits C3, C2, and C1: gain (in amps per radian) = PD_{out} current divided by 2π .

ϕ_R and ϕ_V (Pins 3 and 4) Double-Ended Phase/Frequency Detector Outputs

These outputs can be combined externally to generate a loop error signal. Through use of a Motorola patented technique, the detector's dead zone has been eliminated. Therefore, the phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detector is described below and is shown in Figure 17.

POL bit (C7) in the C register = low (see Figure 14)

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : ϕ_V = negative pulses, ϕ_R = essentially high

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : ϕ_V = essentially high, ϕ_R = negative pulses

Frequency and Phase of $f_V = f_R$: ϕ_V and ϕ_R remain essentially high, except for a small minimum time period when both pulse low in phase

POL bit (C7) = high

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : ϕ_R = negative pulses, ϕ_V = essentially high

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : ϕ_R = essentially high, ϕ_V = negative pulses

Frequency and Phase of $f_V = f_R$: ϕ_V and ϕ_R remain essentially high, except for a small minimum time period when both pulse low in phase

These outputs can be enabled, disabled, and interchanged via C register bits C6 or C4. This is a patented

feature. Note that when disabled or in standby, ϕ_R and ϕ_V are forced to their rest condition (high state).

The ϕ_R and ϕ_V output signal swing is approximately from Gnd to V_{PD}.

LD Lock Detector Output (Pin 2)

This output is essentially at a high level with narrow low-going pulses when the loop is locked (f_R and f_V of the same phase and frequency). The output pulses low when f_V and f_R are out of phase or different frequencies. LD is the logical ANDING of ϕ_R and ϕ_V (see Figure 17).

This output can be enabled and disabled via the C register. This is a patented feature. Upon power up, on-chip initialization circuitry disables LD to a static low logic level to prevent a false "lock" signal. If unused, LD should be disabled and left open.

The LD output signal swing is approximately from Gnd to V_{DD}.

Rx External Resistor (Pin 8)

A resistor tied between this pin and Gnd, in conjunction with bits in the C register, determines the amount of current that the PD_{out} pin sinks and sources. When bits C2 and C3 are both set high, the maximum current is obtained at PD_{out}; see Tables 4 and 5 for other current values. The recommended value for Rx is 3.9 k Ω (preliminary). A value of 3.9 k Ω provides current at the PD_{out} pin of approximately 1 mA @ V_{DD} = 3 V and approximately 1.7 mA @ V_{DD} = 5 V in the 100% current mode. Note that V_{DD}, not V_{PD}, is a factor in determining the current.

When the ϕ_R and ϕ_V outputs are used, the Rx pin may be floated.

Table 4. PD_{out} Current*, C1 = Low with Output A not Selected as "Port"; Also, Default Mode When Output A Selected as "Port"

Bit C3	Bit C2	PD _{out} Current*
0	0	70%
0	1	80%
1	0	90%
1	1	100%

* At the time the data sheet was printed, only the 100% current mode was guaranteed. The reduced current modes were for experimentation only.

Table 5. PD_{out} Current*, C1 = High with Output A not Selected as "Port"

Bit C3	Bit C2	PD _{out} Current*
0	0	25%
0	1	50%
1	0	75%
1	1	100%

* At the time the data sheet was printed, only the 100% current mode was guaranteed. The reduced current modes were for experimentation only.

TEST POINT PINS**Test 1****Modulus Control Signal (Pin 9)**

This pin may be used in conjunction with the Test 2 pin for access to the on-board 64/65 prescaler. When Test 1 is low, the prescaler divides by 65. When high, the prescaler divides by 64.

CAUTION

This pin is an unbuffered output and must be floated in an actual application. This pin must be attached to an isolated pad with no trace.

Test 2**Prescaler Output (Pin 13)**

This pin may be used to access the on-board 64/65 prescaler output.

CAUTION

This pin is an unbuffered output and must be floated in an actual application. This pin must be attached to an isolated pad with no trace.

POWER SUPPLY PINS**V_{DD}****Positive Power Supply (Pin 14)**

This pin supplies power to the main CMOS digital portion of the device. Also, this pin, in conjunction with the Rx resistor, determines the internal reference current for the PD_{out} pin. The voltage range is 2.7 to 5.5 V with respect to the Gnd pin.

For optimum performance, V_{DD} should be bypassed to Gnd using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

V_{CC}**Positive Power Supply (Pin 12)**

This pin supplies power to the RF amp and 64/65 prescaler. The voltage range is 2.7 to 5.5 V with respect to the Gnd pin. In standby mode, the V_{CC} pin still draws a few milliamps from the power supply. This current drain can be eliminated with the use of transistor Q1 as shown in Figure 21.

For optimum performance, V_{CC} should be bypassed to Gnd using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

V_{PD}**Positive Power Supply (Pin 5)**

This pin supplies power to both phase/frequency detectors A and B. The voltage applied on this pin may be more or less than the potential applied to the V_{DD} and V_{CC} pins. The voltage range for V_{PD} is 2.7 to 5.5 V with respect to the Gnd pin.

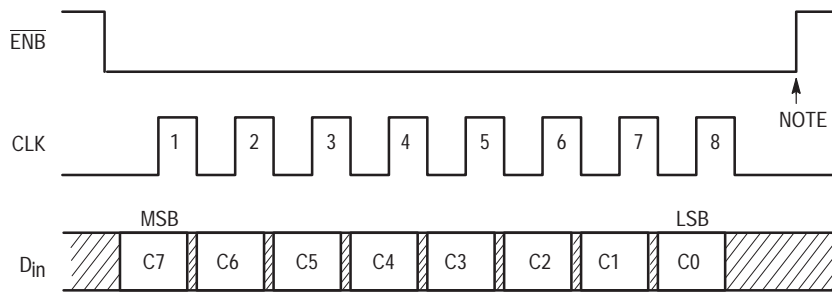
For optimum performance, V_{PD} should be bypassed to Gnd using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

Gnd**Ground (Pin 7)**

Common ground.

MC145193

Figure 14. C Register Access and Format
(8 Clock Cycles are Used)



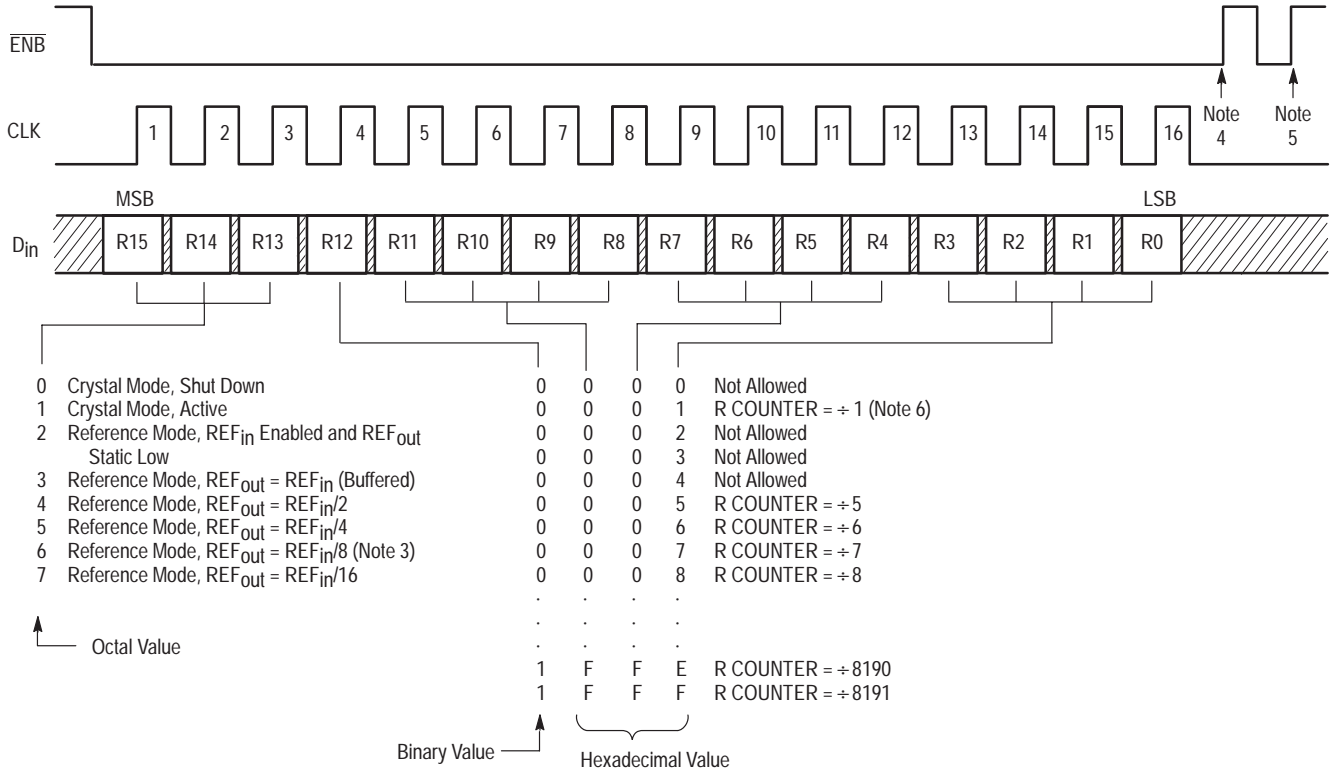
NOTE: At this point, the new byte is transferred to the C register and stored. No other registers are affected.

- C7 – POL: Selects the output polarity of the phase/frequency detectors. When set high, this bit inverts PD_{out} and interchanges the ϕ_R function with ϕ_V as depicted in Figure 17. Also see the phase detector output pin descriptions for more information. This bit is cleared low at power up.
- C6 – PDA/B: Selects which phase/frequency detector is to be used. When set high, enables the output of phase/frequency detector A (PD_{out}) and disables phase/frequency detector B by forcing ϕ_R and ϕ_V to the static high state. When cleared low, phase/frequency detector B is enabled (ϕ_R and ϕ_V) and phase/frequency detector A is disabled with PD_{out} forced to the high-impedance state. This bit is cleared low at power up.
- C5 – LDE: Enables the lock detector output when set high. When the bit is cleared low, the LD output is forced to a static low level. This bit is cleared low at power up.
- C4 – STBY: When set, places the CMOS section of device, which is powered by the V_{DD} and V_{PD} pins, in the standby mode for reduced power consumption: PD_{out} is forced to the high-impedance state, ϕ_R and ϕ_V are forced high, the A, N, and R counters are inhibited from counting, and the Rx current is shut off. In standby, the state of LD is determined by bit C5. C5 low forces LD low (no change). C5 high forces LD static high. During standby, data is retained in the A, R, and C registers. The condition of REF/OSC circuitry is determined by the control bits in the R register: R13, R14, and R15. However, if REF_{out} = static low is selected, the internal feedback resistor is disconnected and the input is inhibited when in standby; in addition, the REF_{in} input only presents a capacitive load. NOTE: Standby does not affect the other modes of the REF/OSC circuitry.

When C4 is reset low, the part is taken out of standby in two steps. First, the REF_{in} (only in one mode) resistor is reconnected, all counters are enabled, and the Rx current is enabled. Any f_R and f_V signals are inhibited from toggling the phase/frequency detectors and lock detector. Second, when the first f_V pulse occurs, the R counter is jam loaded, and the phase/frequency and lock detectors are initialized. Immediately after the jam load, the A, N, and R counters begin counting down together. At this point, the f_R and f_V pulses are enabled to the phase and lock detectors. (Patented feature.)
- C3, C2 – I2, I1: Controls the PD_{out} source/sink current per Tables 4 and 5. With both bits high, the maximum current is available. Also, see C1 bit description.
- C1 – Port: When the Output A pin is selected as "Port" via bits A22 and A23, C1 determines the state of Output A. When C1 is set high, Output A is forced high; C1 low forces Output A low. When Output A is **not** selected as "Port," C1 controls whether the PD_{out} step size is 10% or 25%. (See Tables 4 and 5.) When low, steps are 10%. When high, steps are 25%. Default is 10% steps when Output A is selected as "Port." The Port bit is not affected by the standby mode.
- C0 – Out B: Determines the state of Output B. When C0 is set high, Output B is high-impedance; C0 low forces Output B low. The Out B bit is not affected by the standby mode. This bit is cleared low at power up.

MC145193

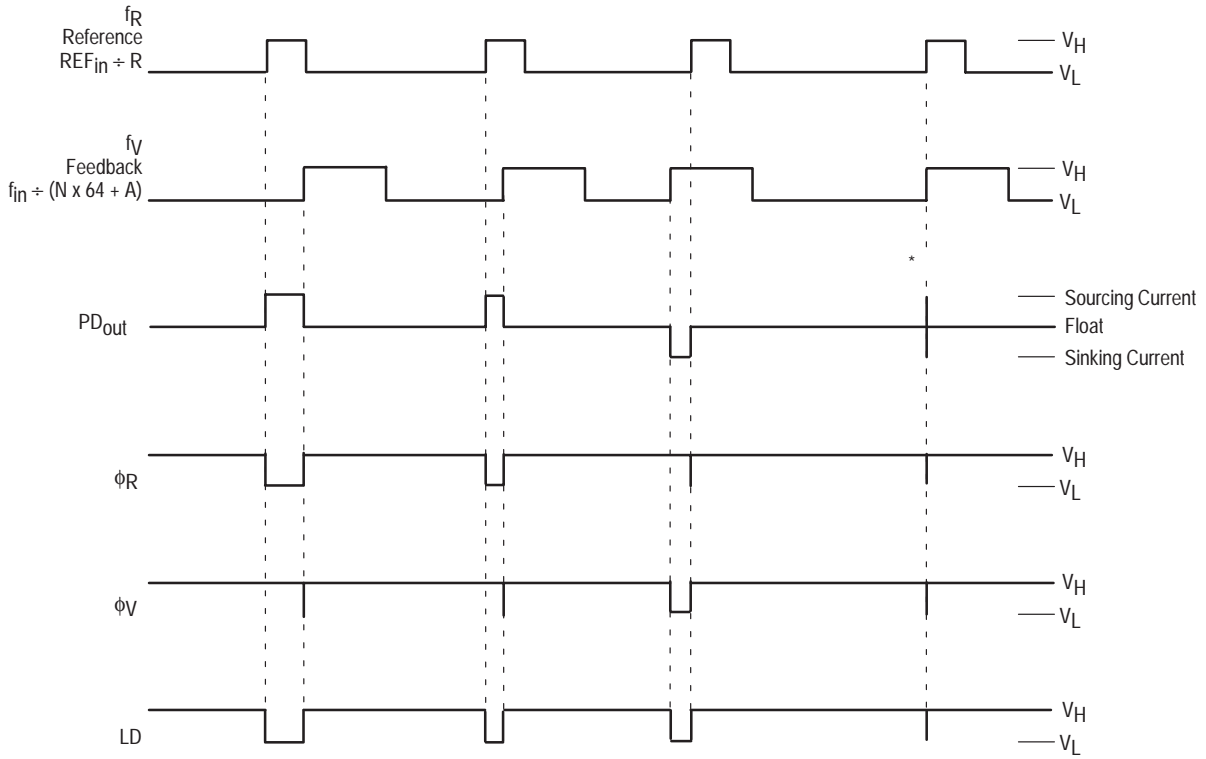
Figure 16. R Register Access and Format
(16 Clock Cycles are Used)



NOTES:

- Bits R15 through R13 control the configurable “OSC or 4–stage divider” block (see Block Diagram).
- Bits R12 through R0 control the “13–stage R counter” block (see Block Diagram).
- A power–on initialize circuit forces a default REF_{in} to REF_{out} ratio of eight.
- At this point, bits R13, R14, and R15 are stored and sent to the “OSC or 4–Stage Divider” block in the Block Diagram. Bits R0 – R12 are loaded into the first buffer in the double–buffered section of the R register. Therefore, the R counter divide ratio is not altered yet and retains the previous ratio loaded. The C and A registers are not affected.
- Optional load pulse. At this point, bits R0 – R12 are transferred to the second buffer of the R register. The R counter begins dividing by the new ratio after completing the rest of the present count cycle. CLK must be low during the ENB pulse, as shown. The C and A registers are not affected. The first buffer of the R register is not affected. Also, see Note 3 of Figure 15 for an alternate method of loading the second buffer in the R register.
- Allows direct access to reference input of phase/frequency detectors.

Figure 17. Phase/Frequency Detectors and Lock Detector Output Waveforms



V_H = High voltage level

V_L = Low voltage level

*At this point, when both f_R and f_V are in phase, the output source and sink circuits are turned on for a short interval.

NOTE: The PD_{out} either sources or sinks current during out-of-lock conditions. When locked in phase and frequency, the output is in the floating condition and the voltage at that pin is determined by the low-pass filter capacitor. PD_{out} , ϕ_R , and ϕ_V are shown with the polarity bit (POL) = low; see Figure 14 for POL.

Crystal Oscillator Considerations

The following options may be considered to provide a reference frequency to Motorola's CMOS frequency synthesizers.

Use of a Hybrid Crystal Oscillator

Commercially available temperature-compensated crystal oscillators (TCXOs) or crystal-controlled data clock oscillators provide very stable reference frequencies. An oscillator capable of CMOS logic levels at the output may be direct or dc coupled to REF_{in}. If the oscillator does not have CMOS logic levels on the outputs, capacitive or ac coupling to REF_{in} may be used (see Figure 8).

For additional information about TCXOs and data clock oscillators, please consult the latest version of the *eem Electronic Engineers Master Catalog*, the *Gold Book*, or similar publications.

Design an Off-Chip Reference

The user may design an off-chip crystal oscillator using discrete transistors or ICs specifically developed for crystal oscillator applications. The reference signal is usually ac coupled to REF_{in} (see Figure 8). For large amplitude signals (standard CMOS logic levels), dc coupling may be used.

Use of the On-Chip Oscillator Circuitry

The on-chip amplifier (a digital inverter) along with an appropriate crystal may be used to provide a reference source frequency. A fundamental mode crystal, parallel resonant at the desired operating frequency, should be connected as shown in Figure 18.

The crystal should be specified for a loading capacitance (C_L) which does not exceed approximately 20 pF when used at the highest operating frequencies listed in the Loop Specifications table. Assuming R1 = 0 Ω, the shunt load capacitance (C_L) presented across the crystal can be estimated to be:

$$C_L = \frac{C_{in}C_{out}}{C_{in} + C_{out}} + C_a + C_{stray} + \frac{C_1 \cdot C_2}{C_1 + C_2}$$

where

C_{in} = 5 pF (see Figure 19)

C_{out} = 6 pF (see Figure 19)

C_a = 1 pF (see Figure 19)

C1 and C2 = external capacitors (see Figure 18)

C_{stray} = the total equivalent external circuit stray capacitance appearing across the crystal terminals

The oscillator can be "trimmed" on-frequency by making a portion or all of C1 variable. The crystal and associated components must be located as close as possible to the REF_{in} and REF_{out} pins to minimize distortion, stray capacitance, stray inductance, and startup stabilization time. Circuit stray capacitance can also be handled by adding the appropriate stray value to the values for C_{in} and C_{out}. For this approach, the term C_{stray} becomes 0 in the above expression for C_L.

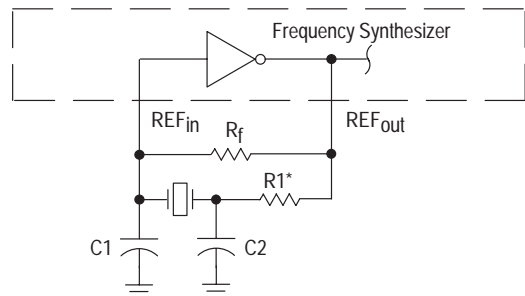
Power is dissipated in the effective series resistance of the crystal, R_e, in Figure 20. The maximum drive level specified by the crystal manufacturer represents the maximum stress that the crystal can withstand without damage or excessive

shift in operating frequency. R1 in Figure 18 limits the drive level. The use of R1 is not necessary in most cases.

To verify that the maximum dc supply voltage does not cause the crystal to be overdriven, monitor the output frequency (f_R) at Output A as a function of supply voltage. (REF_{out} is not used because loading impacts the oscillator.) The frequency should increase very slightly as the dc supply voltage is increased. An overdriven crystal decreases in frequency or becomes unstable with an increase in supply voltage. The operating supply voltage must be reduced or R1 must be increased in value if the overdriven condition exists. The user should note that the oscillator start-up time is proportional to the value of R1.

Through the process of supplying crystals for use with CMOS inverters, many crystal manufacturers have developed expertise in CMOS oscillator design with crystals. Discussions with such manufacturers can prove very helpful (see Table 2).

Figure 18. Pierce Crystal Oscillator Circuit



* May be needed in certain cases. See text.

Figure 19. Parasitic Capacitances of the Amplifier and C_{stray}

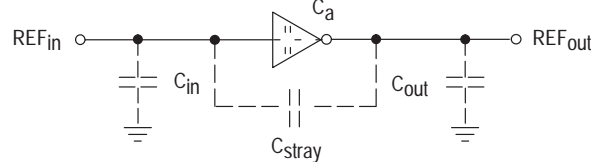
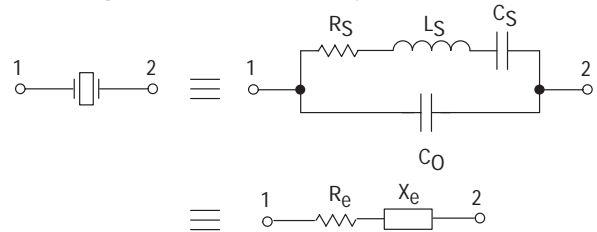


Figure 20. Equivalent Crystal Networks



NOTE: Values are supplied by crystal manufacturer (parallel resonant crystal).

MC145193

RECOMMENDED READING

Technical Note TN-24, Statek Corp.
Technical Note TN-7, Statek Corp.
E. Hafner, "The Piezoelectric Crystal Unit—Definitions and Method of Measurement", *Proc. IEEE*, Vol. 57, No. 2, Feb. 1969.
D. Kemper, L. Rosine, "Quartz Crystals for Frequency Control", *Electro-Technology*, June 1969.

P. J. Ottowitz, "A Guide to Crystal Selection", *Electronic Design*, May 1966.
D. Babin, "Designing Crystal Oscillators", *Machine Design*, March 7, 1985.
D. Babin, "Guidelines for Crystal Oscillator Design", *Machine Design*, April 25, 1985.

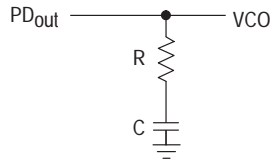
Table 6. Partial List of Crystal Manufacturers

CTS Corp.
United States Crystal Corp.
Crystek Crystal
Statek Corp.
Fox Electronics

NOTE: Motorola cannot recommend one supplier over another and in no way suggests that this is a complete listing of crystal manufacturers.

PHASE-LOCKED LOOP — LOW-PASS FILTER DESIGN

(A)



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NC}}$$

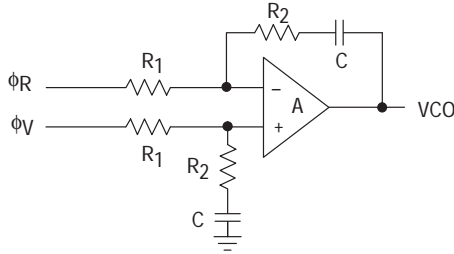
$$\zeta = \frac{R}{2} \sqrt{\frac{K_\phi K_{VCO} C}{N}} = \frac{\omega_n RC}{2}$$

$$Z(s) = \frac{1 + sRC}{sC}$$

NOTE:

For (A), using K_ϕ in amps per radian with the filter's impedance transfer function, $Z(s)$, maintains units of volts per radian for the detector/filter combination. Additional sideband filtering can be accomplished by adding a capacitor C' across R . The corner $\omega_c = 1/RC'$ should be chosen such that ω_n is not significantly affected.

(B)



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NCR_1}}$$

$$\zeta = \frac{\omega_n R_2 C}{2}$$

Assuming Gain A is very large, then:

$$F(s) = \frac{R_2 s C + 1}{R_1 s C}$$

NOTE:

For (B), R_1 is frequently split into two series resistors; each resistor is equal to R_1 divided by 2. A capacitor C_C is then placed from the midpoint to ground to further filter the error pulses. The value of C_C should be such that the corner frequency of this network does not significantly affect ω_n .

DEFINITIONS:

N = Total Division Ratio in Feedback Loop

K_ϕ (Phase Detector Gain) = $I_{PDout}/2\pi$ amps per radian for PD_{out}

K_ϕ (Phase Detector Gain) = $V_{PD}/2\pi$ volts per radian for ϕ_V and ϕ_R

K_{VCO} (VCO Transfer Function) = $\frac{2\pi\Delta f_{VCO}}{\Delta V_{VCO}}$ radians per volt

For a nominal design starting point, the user might consider a damping factor $\zeta \approx 0.7$ and a natural loop frequency $\omega_n \approx (2\pi f_R/50)$ where f_R is the frequency at the phase detector input. Larger ω_n values result in faster loop lock times and, for similar sideband filtering, higher f_R -related VCO sidebands.

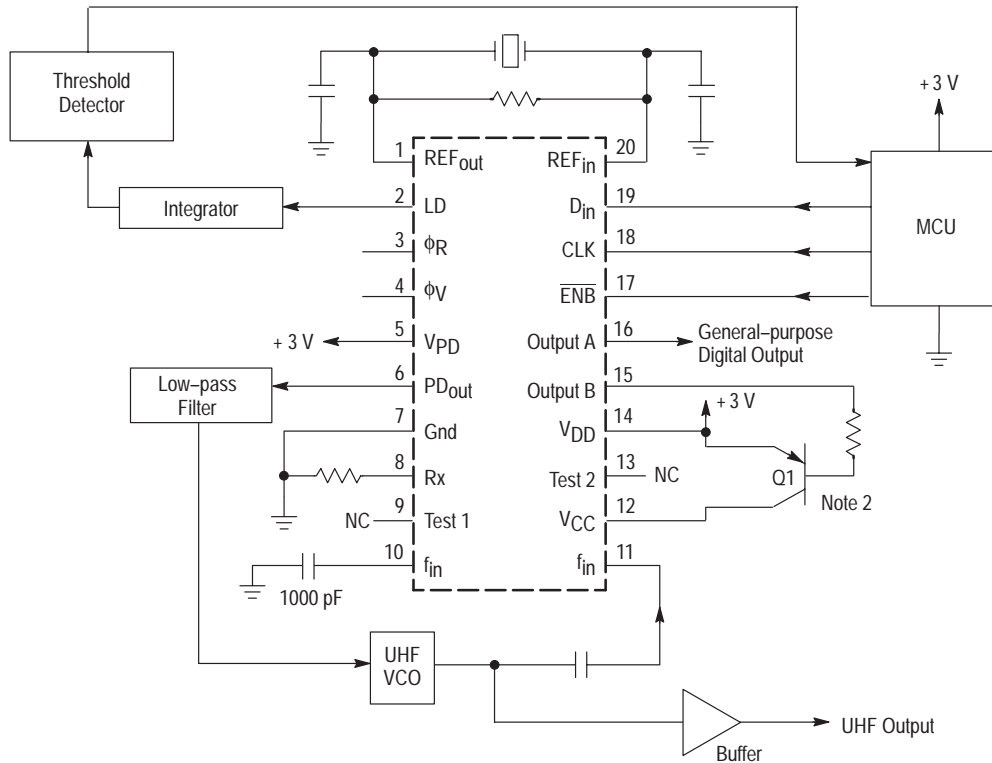
Either loop filter (A) or (B) is frequently followed by additional sideband filtering to further attenuate f_R -related VCO sidebands. This additional filtering may be active or passive.

RECOMMENDED READING:

Gardner, Floyd M., *Phaselock Techniques (second edition)*. New York, Wiley-Interscience, 1979.
 Manassewitsch, Vadim, *Frequency Synthesizers: Theory and Design (second edition)*. New York, Wiley-Interscience, 1980.
 Blanchard, Alain, *Phase-Locked Loops: Application to Coherent Receiver Design*. New York, Wiley-Interscience, 1976.
 Egan, William F., *Frequency Synthesis by Phase Lock*. New York, Wiley-Interscience, 1981.
 Rohde, Ulrich L., *Digital PLL Frequency Synthesizers Theory and Design*. Englewood Cliffs, NJ, Prentice-Hall, 1983.
 Berlin, Howard M., *Design of Phase-Locked Loop Circuits, with Experiments*. Indianapolis, Howard W. Sams and Co., 1978.
 Kinley, Harold, *The PLL Synthesizer Cookbook*. Blue Ridge Summit, PA, Tab Books, 1980.
 Seidman, Arthur H., *Integrated Circuits Applications Handbook*, Chapter 17, pp. 538-586. New York, John Wiley & Sons.
 Fadrhons, Jan, "Design and Analyze PLLs on a Programmable Calculator," *EDN*. March 5, 1980.
 AN535, Phase-Locked Loop Design Fundamentals, Motorola Semiconductor Products, Inc., 1970.
 AR254, Phase-Locked Loop Design Articles, Motorola Semiconductor Products, Inc., Reprinted with permission from *Electronic Design*, 1987.
 AN1253, An Improved PLL Design Method Without ω_n and ζ , Motorola Semiconductor Products, Inc., 1995.

MC145193

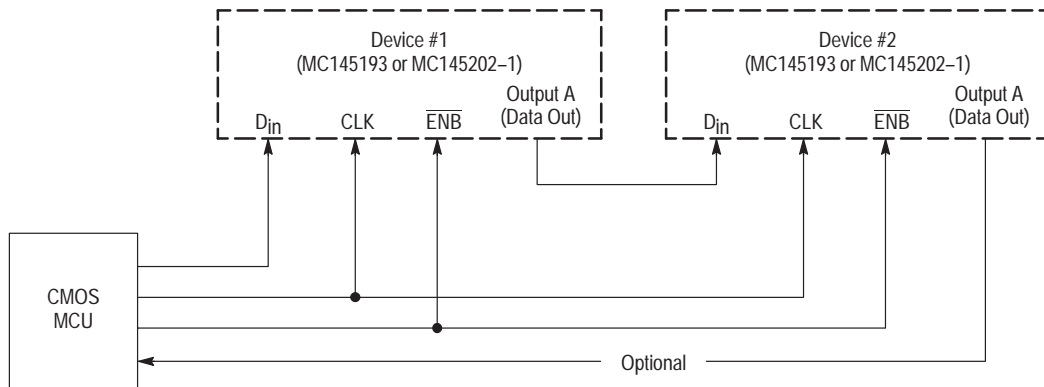
Figure 21. Example Application



NOTES:

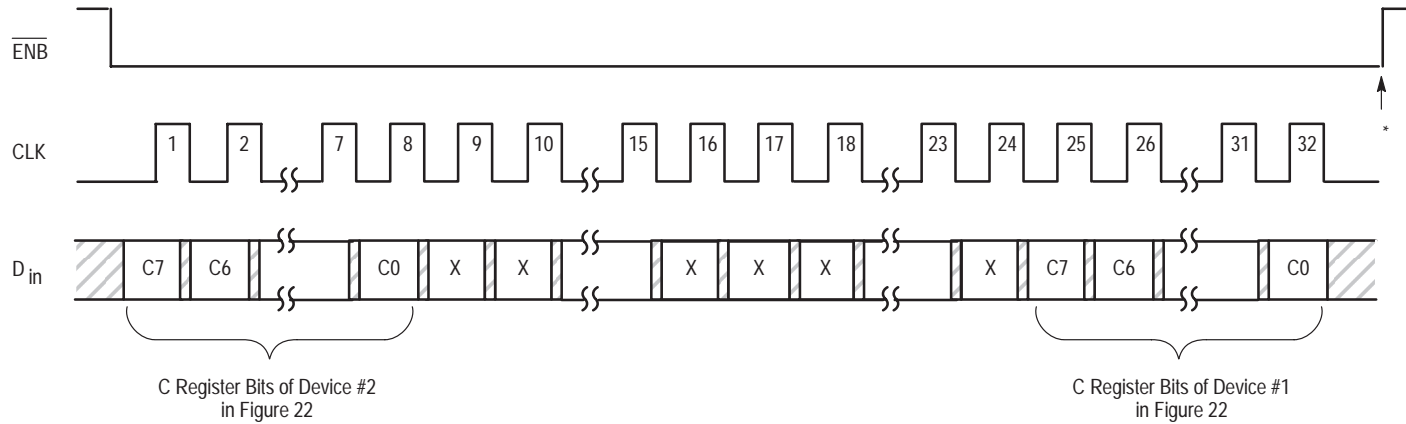
- 1 When used, the ϕ_R and ϕ_V outputs are fed to an external combiner/loop filter. See the Phase-Locked Loop — Low-Pass Filter Design (Page 4.2–142) for additional information.
- 2 Transistor Q1 is required only if the standby feature is needed. Q1 permits the bipolar section of the device to be shut down via use of the general-purpose digital pin, Output B. If the standby feature is not needed, tie Pin 12 directly to the power supply.
- 3 For optimum performance, bypass the V_{CC} , V_{DD} , and V_{PD} pins to Gnd with low-inductance capacitors.
- 4 The R counter is programmed for a divide value = REF_{in}/f_R . Typically, f_R is the tuning resolution required for the VCO. Also, the VCO frequency divided by $f_R = N_T = N \times 64 + A$; this determines the values (N, A) that must be programmed into the N and A counters, respectively.

Figure 22. Cascading Two Devices



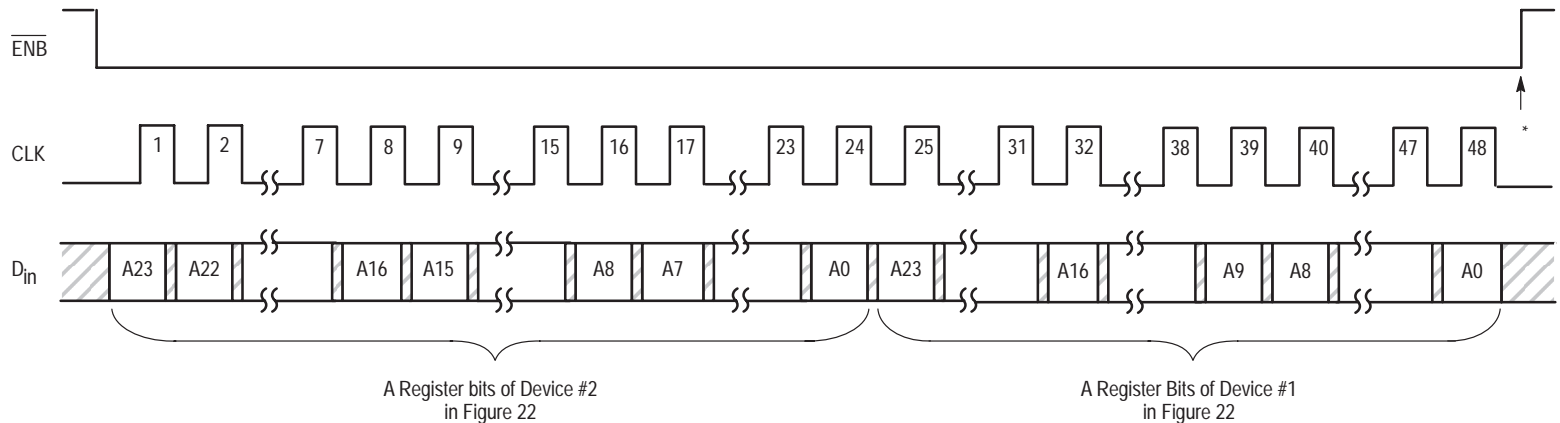
NOTE: See related Figures 23, 24, and 25.

Figure 23. Accessing the C Registers of Two Cascaded MC145193 or MC145202-1 Devices



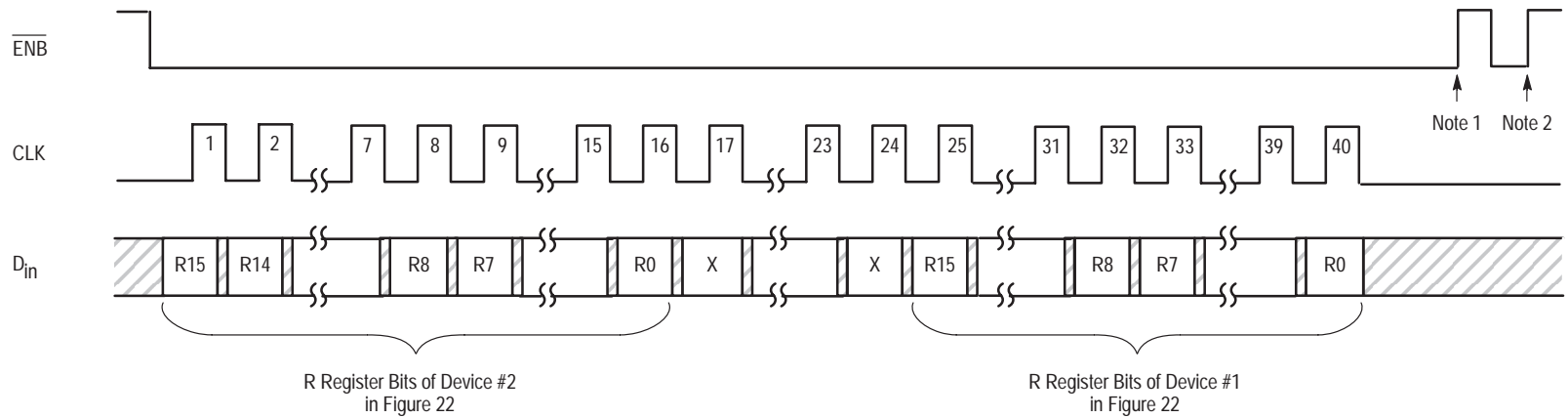
*At this point, the new bytes are transferred to the C registers of both devices and stored. No other registers are affected.

Figure 24. Accessing the A Registers of Two Cascaded MC145193 or MC145202-1 Devices



* At this point, the new bytes are transferred to the A registers of both devices and stored. Additionally, for both devices, the 13 LSBs in each of the first buffers of the R registers are transferred to the respective R register's second buffer. Thus, the R, N, and A counter can be presented new divide ratios at the same time. The first buffer of each R register is not affected. Neither C register is affected.

Figure 25. Accessing the R Registers of Two Cascaded MC145193 or MC145202-1 Devices



Notes Applicable to Each Device:

1. At this point, bits R13, R14 and R15 are stored and sent to the "OSC or 4-Stage Divider" block in the Block Diagram. Bits R0 through R12 are loaded into the first buffer in the double-buffered section of the R register. Therefore, the R counter divide is not altered yet and retains the previous ratio loaded. The C and A registers are not affected.
2. Optional load pulse. At this point, the bits R0 through R12 are transferred to the second buffer of the R register. The R counter begins dividing by the new ratio after completing the rest of the present count cycle. CLK must be low during the ENB pulse, as shown. The C and A registers are not affected. The first buffer of the R register is not affected. Also, see note of Figure 24 for an alternate method of loading the second buffer in the R register.

2.0 GHz PLL Frequency Synthesizer

The MC145202-1 is recommended for new designs and has improved suppression of reference sideband spurs. The counters are programmed via a synchronous serial port which is SPI compatible. The serial port is byte-oriented to facilitate control via an MCU. Due to the innovative BitGrabber Plus™ registers, the MC145202-1 may be cascaded with other peripherals featuring BitGrabber Plus without requiring leading dummy bits or address bits in the serial data stream. In addition, BitGrabber Plus peripherals may be cascaded with existing BitGrabber™ peripherals.

The device features a single-ended current source/sink phase detector A output and a double-ended phase detector B output. Both phase detectors have linear transfer functions (no dead zones). The maximum current of the single-ended phase detector output is determined by an external resistor tied from the Rx pin to ground. This current can be varied via the serial port.

Slew-rate control is provided by a special driver designed for the REF_{out} pin. This minimizes interference caused by REF_{out}.

This part includes a differential RF input that may be operated in a single-ended mode. Also featured are on-board support of an external crystal and a programmable reference output. The R, A, and N counters are fully programmable. The C register (configuration register) allows the part to be configured to meet various applications. A patented feature allows the C register to shut off unused outputs, thereby minimizing system noise and interference.

In order to have consistent lock times and prevent erroneous data from being loaded into the counters, on-board circuitry synchronizes the update of the A register if the A or N counters are loading. Similarly, an update of the R register is synchronized if the R counter is loading.

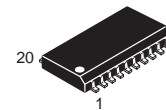
The double-buffered R register allows new divide ratios to be presented to the three counters (R, A, and N) simultaneously.

- Maximum Operating Frequency: 2000 MHz @ - 10 dBm
- Operating Supply Current: 4 mA Nominal at 3.0 V
- Operating Supply Voltage Range (V_{DD} , V_{CC} , V_{PD} Pins): 2.7 to 5.5 V
- Current Source/Sink Phase Detector Output:
1.7 mA @ 5.0 V or 1.0 mA @ 3.0 V
- Gain of Current Source/Sink Phase/Frequency Detector Controllable via Serial Port
- R Counter Division Range: 1 and 5 to 8191
- Dual-Modulus Capability Provides Total Division up to 262,143
- High-Speed Serial Interface: 4 Mbps
- Output A Pin, When Configured as Data Out, Permits Cascading of Devices
- Two General-Purpose Digital Outputs:
Output A: Totem-Pole (Push-Pull) with Four Output Modes
Output B: Open-Drain
- Patented Power-Saving Standby Feature with Orderly Recovery for Minimizing Lock Times, Standby Current: 30 μ A
- See App Note AN1253/D for Low-Pass Filter Design, and AN1277/D for Offset Reference PLLs for Fine Resolution or Fast Hopping

MC145202-1

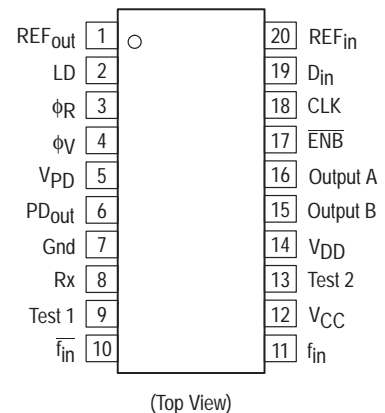
PLL FREQUENCY SYNTHESIZER

SEMICONDUCTOR TECHNICAL DATA



F SUFFIX
PLASTIC PACKAGE
CASE 751J
(SO-20)

PIN CONNECTIONS



EVALUATION KIT

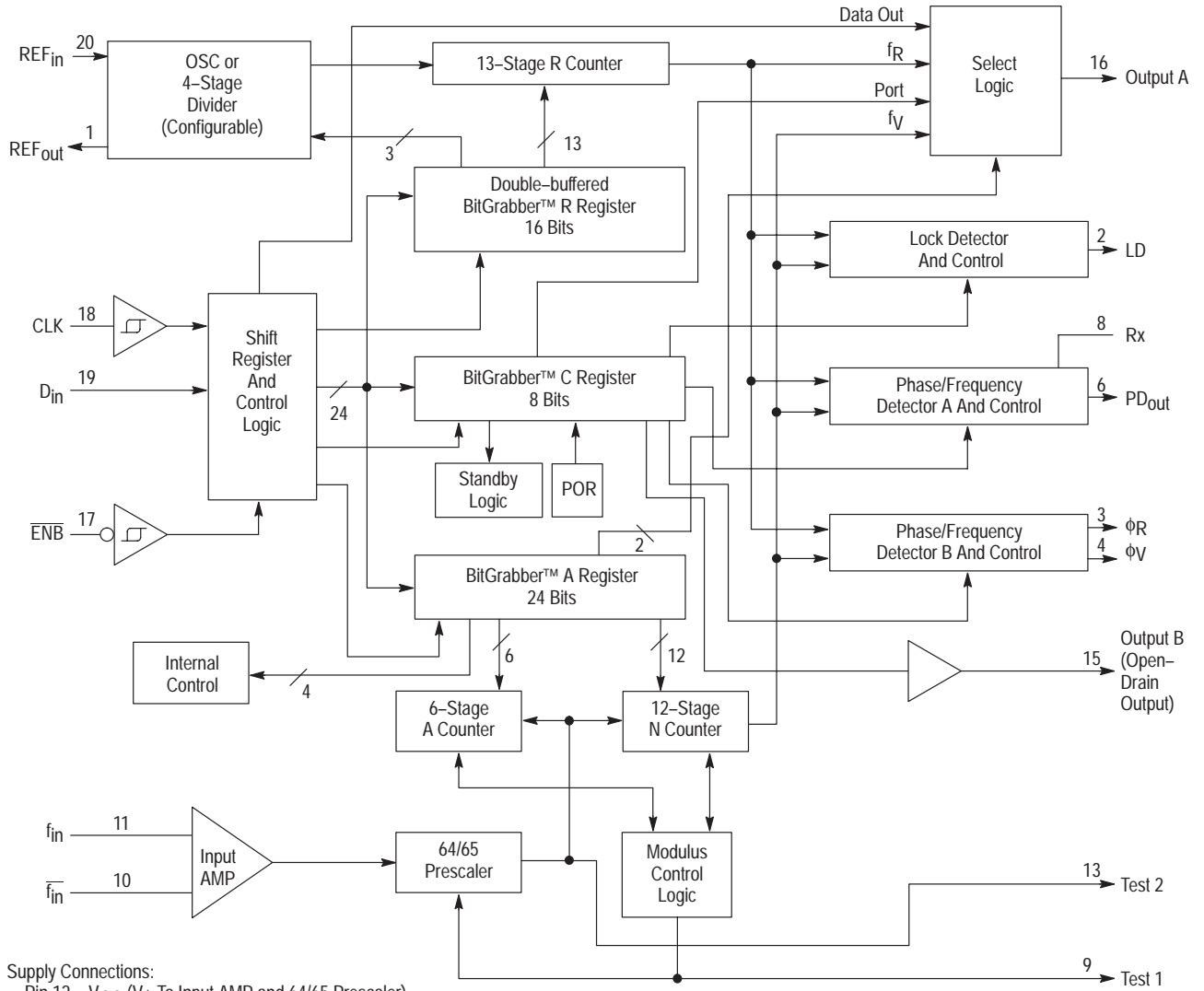
The P/N MC145202-1EVK, which contains hardware and software, is available.

ORDERING INFORMATION

Device	Operating Temperature Range	Package
MC145202F1	$T_A = -40$ to 85°C	SO-20

MC145202-1

BLOCK DIAGRAM



Supply Connections:
 Pin 12 = V_{CC} ($V+$ To Input AMP and 64/65 Prescaler)
 Pin 5 = V_{PD} ($V+$ To Phase/Frequency Detectors A and B)
 Pin 14 = V_{DD} ($V+$ To Balance Of Circuit)
 Pin 7 = Gnd (Common Ground)

This device contains 7,278 active transistors.

MC145202-1

MAXIMUM RATINGS* (Voltages Referenced to Gnd, unless otherwise stated)

Parameter	Symbol	Value	Unit
DC Supply Voltage (Pins 12 and 14)	V_{CC}, V_{DD}	-0.5 to 6.0	V
DC Supply Voltage (Pin 5)	V_{PD}	$V_{DD} - 0.5$ to 6.0	V
DC Input Voltage	V_{in}	-0.5 to $V_{DD} + 0.5$	V
DC Output Voltage (except Output B, PD_{out} , ϕ_R , ϕ_V)	V_{out}	-0.5 to $V_{DD} + 0.5$	V
DC Output Voltage (Output B, PD_{out} , ϕ_R , ϕ_V)	V_{out}	-0.5 to $V_{PD} + 0.5$	V
DC Input Current, per Pin (Includes V_{PD})	I_{in}, I_{PD}	± 10	mA
DC Output Current, per Pin	I_{out}	± 20	mA
DC Supply Current, V_{DD} and Gnd Pins	I_{DD}	± 30	mA
Power Dissipation, per Package	P_D	300	mW
Storage Temperature	T_{stg}	-65 to 150	°C
Lead Temperature, 1 mm from Case for 10 Seconds	T_L	260	°C

This device contains protection circuitry to guard against damage due to high static voltages or electric fields. However, precautions must be taken to avoid applications of any voltage higher than maximum rated voltages to this high-impedance circuit.

- NOTES:** 1. Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section.
 2. ESD (electrostatic discharge) immunity meets Human Body Model (HBM) ≤ 2000 V and Machine Model (MM) ≤ 200 V. Additional ESD data available upon request.

ELECTRICAL CHARACTERISTICS

($V_{DD} = V_{CC} = 2.7$ to 5.5 V, Voltages Referenced to Gnd, unless otherwise stated; $V_{PD} = 2.7$ to 5.5 V, $T_A = -40$ to 85°C)

Parameter	Test Condition	Symbol	Guaranteed Limit	Unit
Maximum Low-Level Input Voltage (D_{in} , CLK, \overline{ENB})		V_{IL}	$0.3 \times V_{DD}$	V
Minimum High-Level Input Voltage (D_{in} , CLK, \overline{ENB})		V_{IH}	$0.7 \times V_{DD}$	V
Minimum Hysteresis Voltage (CLK, \overline{ENB})	$V_{DD} = 2.7$ V $V_{DD} = 4.5$ V	V_{Hys}	100 250	mV
Maximum Low-Level Output Voltage (REF_{out} , Output A)	$I_{out} = 20 \mu\text{A}$, Device in Reference Mode	V_{OL}	0.1	V
Minimum High-Level Output Voltage (REF_{out} , Output A)	$I_{out} = -20 \mu\text{A}$, Device in Reference Mode	V_{OH}	$V_{DD} - 0.1$	V
Minimum Low-Level Output Current (REF_{out} , LD)	$V_{out} = 0.3$ V	I_{OL}	0.36	mA
Minimum Low-Level Output Current (ϕ_R , ϕ_V)	$V_{out} = 0.3$ V	I_{OL}	0.36	mA
Minimum Low-Level Output Current (Output A)	$V_{out} = 0.4$ V $V_{DD} = 4.5$ V	I_{OL}	1.0	mA
Minimum Low-Level Output Current (Output B)	$V_{out} = 0.4$ V	I_{OL}	1.0	mA
Minimum High-Level Output Current (REF_{out} , LD)	$V_{out} = V_{DD} - 0.3$ V	I_{OH}	-0.36	mA
Minimum High-Level Output Current (ϕ_R , ϕ_V)	$V_{out} = V_{PD} - 0.3$ V	I_{OH}	-0.36	mA
Minimum High-Level Output Current (Output A Only)	$V_{out} = V_{DD} - 0.4$ V $V_{DD} = 4.5$ V	I_{OH}	-0.6	mA

(continued)

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ELECTRICAL CHARACTERISTICS (continued)

Parameter	Test Condition	Symbol	Guaranteed Limit	Unit
Maximum Input Leakage Current (D _{in} , CLK, $\overline{\text{ENB}}$, REF _{in})	V _{in} = V _{DD} or Gnd, Device in XTAL Mode	I _{in}	±1.0	μA
Maximum Input Current (REF _{in})	V _{in} = V _{DD} or Gnd, Device in Reference Mode	I _{in}	±100	μA
Maximum Output Leakage Current (PD _{out}) (Output B)	V _{out} = V _{PD} or Gnd, Output in Floating State	I _{OZ}	±130	nA
	V _{out} = V _{PD} or Gnd, Output in High-Impedance State		±1	μA
Maximum Standby Supply Current (V _{DD} + V _{PD} Pins)	V _{in} = V _{DD} or Gnd; Outputs Open; Device in Standby Mode, Shut-Down Crystal Mode or REF _{out} -Static-Low Reference Mode; Output B Controlling V _{CC} per Figure 21	I _{STBY}	30	μA
Maximum Phase Detector Quiescent Current (V _{PD} Pin)	Bit C6 = High Which Selects Phase Detector A, PD _{out} = Open, PD _{out} = Static State, Bit C4 = Low Which is not Standby, I _{Rx} = 170 μA, V _{PD} = 5.5 V	I _{PD}	750	μA
	Bit C6 = Low Which Selects Phase Detector B, φ _R and φ _V = Open, φ _R and φ _V = Static Low or High, Bit C4 = Low Which is not Standby		30	
Total Operating Supply Current (V _{DD} + V _{PD} + V _{CC} Pins)	f _{in} = 2.0 GHz; REF _{in} = 13 MHz @ 1 V _{pp} ; Output A = Inactive and No Connect; V _{DD} = V _{CC} , REF _{out} , φ _V , φ _R , PD _{out} , LD = No Connect; D _{in} , $\overline{\text{ENB}}$, CLK = V _{DD} or Gnd, Phase Detector B Selected (Bit C6 = Low)	I _T	[Note]	mA

NOTE: The nominal values are: 4 mA at V_{DD} = V_{CC} = V_{PD} = 3.0 V; 6 mA at V_{DD} = V_{CC} = V_{PD} = 5.0 V. These are not guaranteed limits.

ANALOG CHARACTERISTICS — CURRENT SOURCE/SINK OUTPUT — PD_{out}

(I_{out} ≤ 1 mA @ V_{DD} = 2.7 V and I_{out} ≤ 1.7mA @ V_{DD} ≥ 4.5 V, V_{DD} = V_{CC} = 2.7 to 5.5 V, Voltages Referenced to Gnd)

Parameter	Test Condition	V _{PD}	Guaranteed Limit	Unit
Maximum Source Current Variation (Part-to-Part)	V _{out} = 0.5 x V _{PD}	2.7	±15	%
		4.5	±15	
		5.5	±15	
Maximum Sink-vs-Source Mismatch [Note 3]	V _{out} = 0.5 x V _{PD}	2.7	11	%
		4.5	11	
		5.5	11	
Output Voltage Range [Note 3]	I _{out} Variation ≤ 15%	2.7	0.5 to 2.2	V
	I _{out} Variation ≤ 20%	4.5	0.5 to 3.7	
	I _{out} Variation ≤ 22%	5.5	0.5 to 4.7	

- NOTES:** 1. Percentages calculated using the following formula: (Maximum Value – Minimum Value)/Maximum Value.
 2. See Rx Pin Description for external resistor values.
 3. This parameter is guaranteed for a given temperature within –40 to 85°C.

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AC INTERFACE CHARACTERISTICS

($V_{DD} = V_{CC} = 2.7$ to 5.5 V, $T_A = -40$ to $+85^\circ\text{C}$, $C_L = 25$ pF, Input $t_r = t_f = 10$ ns; $V_{PD} = 2.7$ to 5.5 V)

Parameter	Figure No.	Symbol	Guaranteed Limit	Unit
Serial Data Clock Frequency (Note: Refer to Clock t_w below)	1	f_{clk}	dc to 4.0	MHz
Maximum Propagation Delay, CLK to Output A (Selected as Data Out)	1, 5	t_{PLH} , t_{PHL}	100	ns
Maximum Propagation Delay, $\overline{\text{ENB}}$ to Output A (Selected as Port)	2, 5	t_{PLH} , t_{PHL}	150	ns
Maximum Propagation Delay, $\overline{\text{ENB}}$ to Output B	2, 6	t_{PZL} , t_{PLZ}	150	ns
Maximum Output Transition Time, Output A and Output B; t_{THL} only, on Output B	1, 5, 6	t_{TLH} , t_{THL}	50	ns
Maximum Input Capacitance – D_{in} , $\overline{\text{ENB}}$, CLK		C_{in}	10	pF

TIMING REQUIREMENTS

($V_{DD} = V_{CC} = 2.7$ to 5.5 V, $T_A = -40$ to $+85^\circ\text{C}$, Input $t_r = t_f = 10$ ns, unless otherwise indicated)

Parameter	Figure No.	Symbol	Guaranteed Limit	Unit
Minimum Setup and Hold Times, D_{in} vs CLK	3	t_{su} , t_{h}	50	ns
Minimum Setup, Hold and Recovery Times, $\overline{\text{ENB}}$ vs CLK	4	t_{su} , t_{h} , t_{rec}	100	ns
Minimum Pulse Width, $\overline{\text{ENB}}$	4	t_w	[Note]	cycles
Minimum Pulse Width, CLK	1	t_w	125	ns
Maximum Input Rise and Fall Times, CLK	1	t_r , t_f	100	μs

NOTE: The minimum limit is 3 REF_{in} cycles or 195 f_{in} cycles, whichever is greater.

MC145202-1 SWITCHING WAVEFORMS

Figure 1.

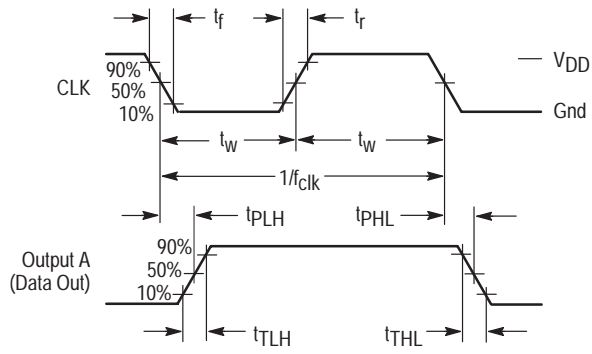


Figure 2.

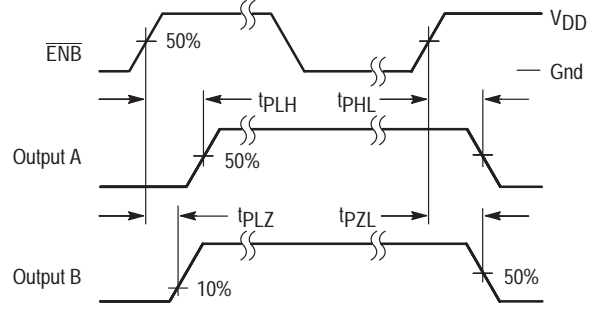


Figure 3.

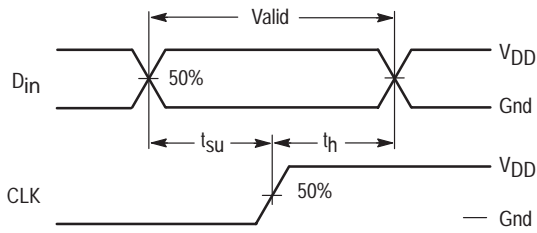


Figure 4.

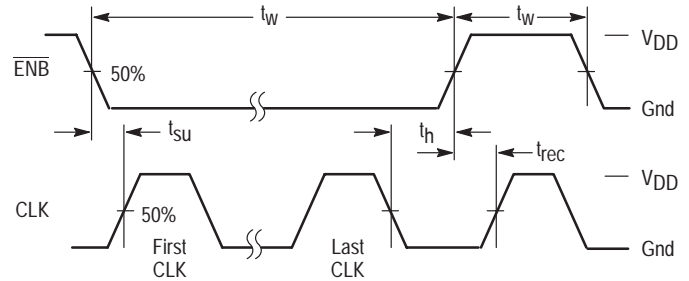
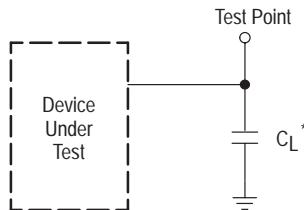
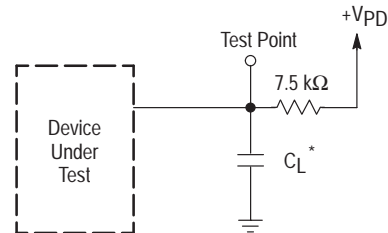


Figure 5.



* Includes all probe and fixture capacitance.

Figure 6.



* Includes all probe and fixture capacitance.

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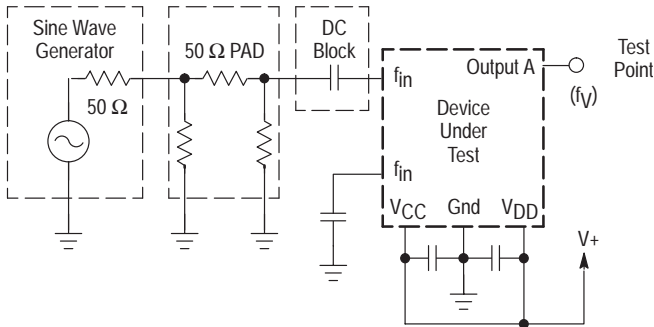
LOOP SPECIFICATIONS ($V_{DD} = V_{CC} = 2.7$ to 5.5 V unless otherwise indicated, $T_A = -40$ to 85°C)

Parameter	Test Condition	Fig. No.	Symbol	Guaranteed Operating Range		Unit
				Min	Max	
Input Sensitivity Range, f_{in}	$500 \text{ MHz} \leq f_{in} \leq 2000 \text{ MHz}$	7	P_{in}	-10	4	dBm*
Input Frequency, REF_{in} Externally Driven in Reference Mode	$V_{in} \geq 400 \text{ mVpp}$ $2.7 \leq V_{DD} < 4.5 \text{ V}$ $4.5 \leq V_{DD} \leq 5.5 \text{ V}$	8	f_{ref}	1.5 1.5	20 30	MHz
Crystal Frequency, Crystal Mode	$C1 \leq 30 \text{ pF}$, $C2 \leq 30 \text{ pF}$, Includes Stray Capacitance	9	f_{XTAL}	2	15	MHz
Output Frequency, REF_{out}	$C_L = 20 \text{ pF}$, $V_{out} \geq 1 \text{ Vpp}$	10, 12	f_{out}	dc	10	MHz
Operating Frequency of the Phase Detectors			f_ϕ	dc	2	MHz
Output Pulse Width (ϕ_R , ϕ_V , and LD)	f_R in Phase with f_V , $C_L = 20 \text{ pF}$, ϕ_R and ϕ_V active for LD measurement, ** $V_{PD} = 2.7$ to 5.5 V $V_{DD} = 2.7 \text{ V}$ $V_{DD} = 4.5 \text{ V}$ $V_{DD} = 5.5 \text{ V}$	11, 12	t_w	40 18 14	120 60 50	ns
Output Transition Times (LD, ϕ_V , and ϕ_R)	$C_L = 20 \text{ pF}$, $V_{PD} = 2.7 \text{ V}$, $V_{DD} = V_{CC} = 2.7 \text{ V}$	11, 12	t_{TLH} , t_{THL}	—	80	ns
Input Capacitance, REF_{in}			C_{in}	—	7	pF

* Power level at the input to the dc block.

** When PD_{out} is active, LD minimum pulse width is approximately 5 ns.

Figure 7. Test Circuit



NOTE: Alternately, the 50 Ω pad may be a T network.

Figure 8. Test Circuit — Reference Mode

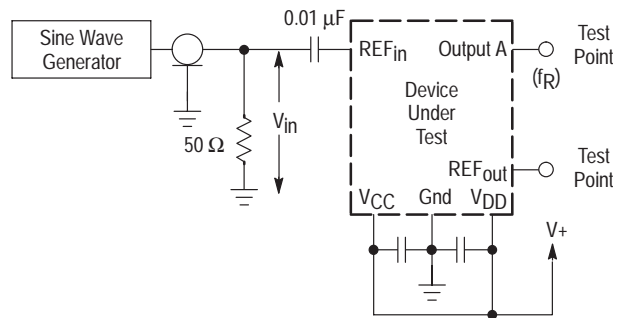


Figure 9. Test Circuit — Crystal Mode

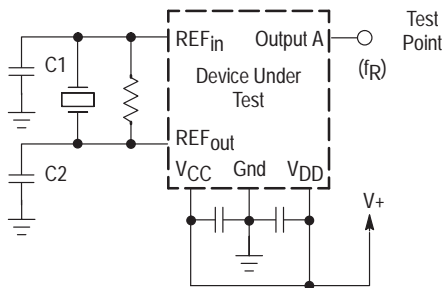


Figure 10. Switching Waveform

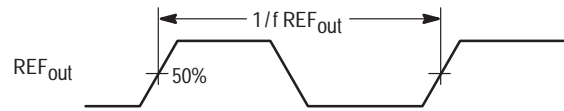


Figure 11. Switching Waveform

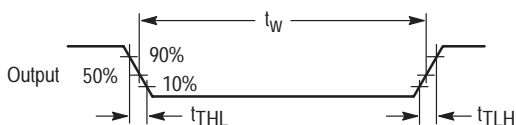
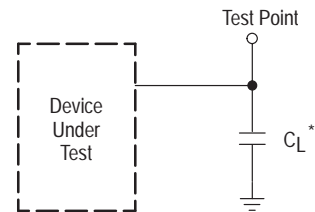


Figure 12. Test Circuit



* Includes all probe and fixture capacitance.

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Figure 13. Normalized Input Impedance at f_{in} — Series Format ($R + jx$)

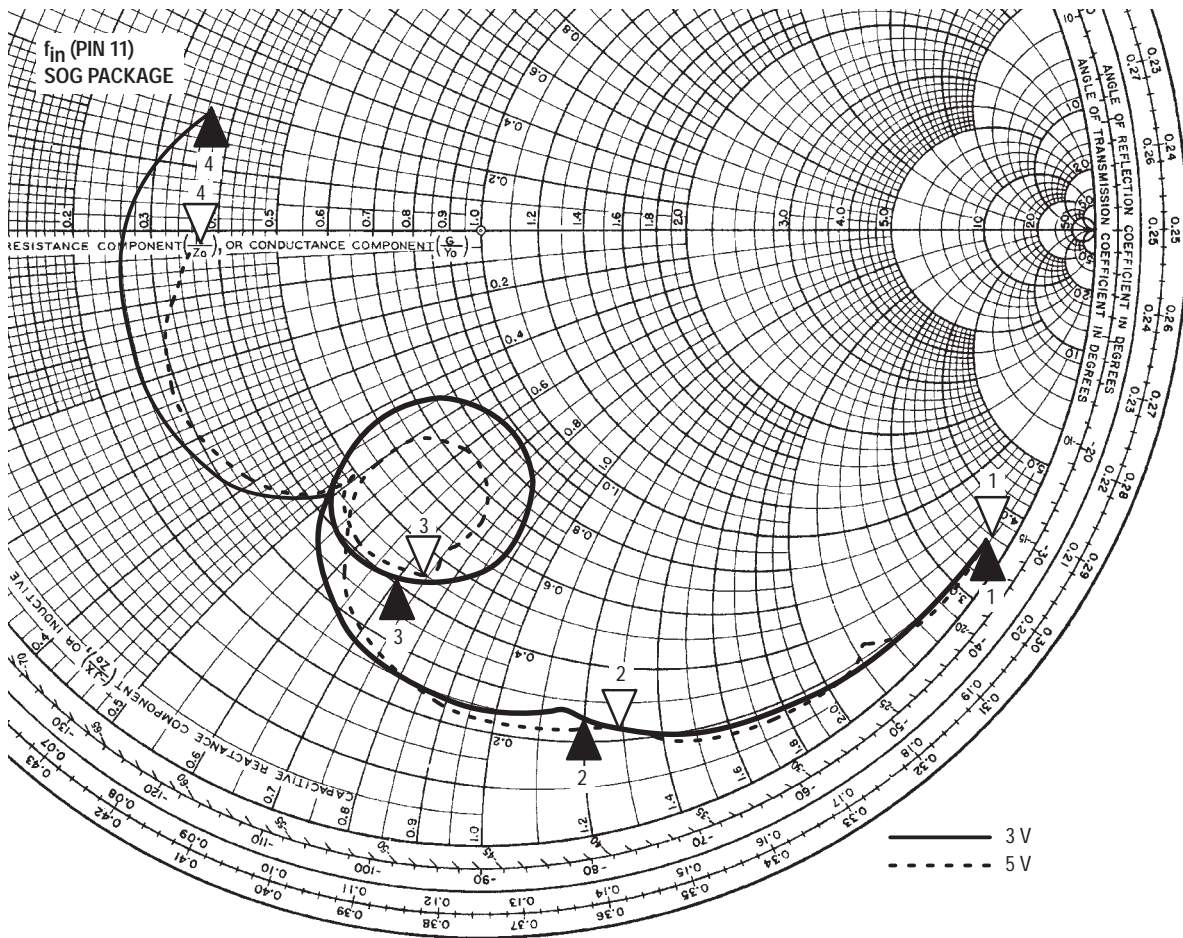


Table 1. Input Impedance at f_{in} — Series Format ($R + jx$), $V_{CC} = 3 V$

Marker	Frequency (GHz)	Resistance (Ω)	Reactance (Ω)	Capacitance/Inductance
1	0.5	11.4	-168	1.9 pF
2	1	12.4	-59.4	2.68 pF
3	1.5	19.8	-34.9	3.04 pF
4	2	18.1	9.43	751 pH

Table 2. Input Impedance at f_{in} — Series Format ($R + jx$), $V_{CC} = 5 V$

Marker	Frequency (GHz)	Resistance (Ω)	Reactance (Ω)	Capacitance/Inductance
1	0.5	11.8	-175	1.82 pF
2	1	11.5	-64.4	2.47 pF
3	1.5	22.2	-36.5	2.91 pF
4	2	18.4	1.14	90.4 pH

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PIN DESCRIPTIONS

DIGITAL INTERFACE PINS

D_{in} Serial Data Input (Pin 19)

The bit stream begins with the most significant bit (MSB) and is shifted in on the low-to-high transition of CLK. The bit pattern is 1 byte (8 bits) long to access the C or configuration register, 2 bytes (16 bits) to access the first buffer of the R register, or 3 bytes (24 bits) to access the A register (see Table 3). The values in the C, R, and A registers do not change during shifting because the transfer of data to the registers is controlled by $\overline{\text{ENB}}$.

CAUTION

The value programmed for the N counter must be greater than or equal to the value of the A counter.

The 13 least significant bits (LSBs) of the R register are double-buffered. As indicated above, data is latched into the first buffer on a 16-bit transfer. (The 3 MSBs are not double-buffered and have an immediate effect after a 16-bit transfer.) The second buffer of the R register contains the 13 bits for the R counter. This second buffer is loaded with the contents of the first buffer when the A register is loaded (a 24-bit transfer). This allows presenting new values to the R, A, and N counters simultaneously. If this is not required, then the 16-bit transfer may be followed by pulsing $\overline{\text{ENB}}$ low with no signal on the CLK pin. This is an alternate method of transferring data to the second buffer of the R register (see Figure 16).

The bit stream needs neither address nor steering bits due to the innovative BitGrabber Plus registers. Therefore, all bits in the stream are available to be data for the three registers. Random access of any register is provided (i.e., the registers may be accessed in any sequence). Data is retained in the registers over a supply range of 2.7 to 5.5 V. The formats are shown in Figures 14, 15, and 16.

D_{in} typically switches near 50% of V_{DD} to maximize noise immunity. This input can be directly interfaced to CMOS devices with outputs guaranteed to switch near rail-to-rail. When interfacing to NMOS or TTL devices, either a level shifter (MC74HC14A, MC14504B) or pull-up resistor of 1 k Ω to 10 k Ω must be used. Parameters to consider when sizing the resistor are worst-case I_{OL} of the driving device, maximum tolerable power consumption, and maximum data rate.

Table 3. Register Access

(MSBs are shifted in first; C0, R0, and A0 are the LSBs)

Number of Clocks	Accessed Register	Bit Nomenclature
8	C Register	C7, C6, C5, . . . , C0
16	R Register	R15, R14, R13, . . . , R0
24	A Register	A23, A22, A21, . . . , A0
Other Values \leq 32 Values $>$ 32	Not Allowed See Figures 22 – 25	

CLK Serial Data Clock Input (Pin 18)

Low-to-high transitions on CLK shift bits available at the D_{in} pin, while high-to-low transitions shift bits from Output A (when configured as Data Out, see Pin 16). The 24-1/2-stage shift register is static, allowing clock rates down to dc in a continuous or intermittent mode.

Eight clock cycles are required to access the C register. Sixteen clock cycles are needed for the first buffer of the R register. Twenty-four cycles are used to access the A register. See Table 3 and Figures 14, 15, and 16. The number of clocks required for cascaded devices is shown in Figures 23 through 25.

CLK typically switches near 50% of V_{DD} and has a Schmitt-triggered input buffer. Slow CLK rise and fall times are allowed. See the last paragraph of D_{in} for more information.

NOTE

To guarantee proper operation of the power-on reset (POR) circuit, the CLK pin must be held at Gnd (with $\overline{\text{ENB}}$ being a don't care) or $\overline{\text{ENB}}$ must be held at the potential of the V+ pin (with CLK being a don't care) during power-up. Floating, toggling, or having these pins in the wrong state during power-up does not harm the chip, but causes two potentially undesirable effects. First, the outputs of the device power up in an unknown state. Second, if two devices are cascaded, the A Registers must be written twice after power up. After these two accesses, the two cascaded chips perform normally.

$\overline{\text{ENB}}$ Active Low Enable Input (Pin 17)

This pin is used to activate the serial interface to allow the transfer of data to/from the device. When $\overline{\text{ENB}}$ is in an inactive high state, shifting is inhibited and the port is held in the initialized state. To transfer data to the device, $\overline{\text{ENB}}$ (which must start inactive high) is taken low, a serial transfer is made via D_{in} and CLK, and $\overline{\text{ENB}}$ is taken back high. The low-to-high transition on $\overline{\text{ENB}}$ transfers data to the C or A registers and first buffer of the R register, depending on the data stream length per Table 3.

Transitions on $\overline{\text{ENB}}$ must not be attempted while CLK is high. This puts the device out of synchronization with the microcontroller. Resynchronization occurs when $\overline{\text{ENB}}$ is high and CLK is low.

This input is also Schmitt-triggered and switches near 50% of V_{DD}, thereby minimizing the chance of loading erroneous data into the registers. See the last paragraph of D_{in} for more information.

For POR information, see the note for the CLK pin.

Output A**Configurable Digital Output (Pin 16)**

Output A is selectable as f_R , f_V , Data Out, or Port. Bits A22 and A23 in the A register control the selection; see Figure 15.

If A23 = A22 = high, Output A is configured as f_R . This signal is the buffered output of the 13-stage R counter. The f_R signal appears as normally low and pulses high. The f_R signal can be used to verify the divide ratio of the R counter. This ratio extends from 5 to 8191 and is determined by the binary value loaded into bits R0–R12 in the R register. Also, direct access to the phase detectors via the REF_{in} pin is allowed by choosing a divide value of 1 (see Figure 16). The maximum frequency at which the phase detectors operate is 2 MHz. Therefore, the frequency of f_R should not exceed 2 MHz.

If A23 = high and A22 = low, Output A is configured as f_V . This signal is the buffered output of the 12-stage N counter. The f_V signal appears as normally low and pulses high. The f_V signal can be used to verify the operation of the prescaler, A counter, and N counter. The divide ratio between the f_{in} input and the f_V signal is $N \times 64 + A$. N is the divide ratio of the N counter and A is the divide ratio of the A counter. These ratios are determined by bits loaded into the A register. See Figure 15. The maximum frequency at which the phase detectors operate is 2 MHz. Therefore, the frequency of f_V should not exceed 2 MHz.

If A23 = low and A22 = high, Output A is configured as Data Out. This signal is the serial output of the 24-1/2-stage shift register. The bit stream is shifted out on the high-to-low transition of the CLK input. Upon power up, Output A is automatically configured as Data Out to facilitate cascading devices.

If A23 = A22 = low, Output A is configured as Port. This signal is a general-purpose digital output which may be used as an MCU port expander. This signal is low when the Port bit (C1) of the C register is low, and high when the Port bit is high.

Output B**Open-Drain Digital Output (Pin 15)**

This signal is a general-purpose digital output which may be used as an MCU port expander. This signal is low when the Out B bit (C0) of the C register is low. When the Out B bit is high, Output B assumes the high-impedance state. Output B may be pulled up through an external resistor or active circuitry to any voltage less than or equal to the potential of the V_{PD} pin. **Note:** the maximum voltage allowed on the V_{PD} pin is 5.5 V.

Upon power-up, power-on reset circuitry forces Output B to a low level.

REFERENCE PINS **REF_{in} and REF_{out}** **Reference Input and Reference Output (Pins 20 and 1)**

Configurable pins for a Crystal or an External Reference. This pair of pins can be configured in one of two modes: the crystal mode or the reference mode. Bits R13, R14, and R15 in the R register control the modes as shown in Figure 16.

In crystal mode, these pins form a reference oscillator when connected to terminals of an external parallel-resonant

crystal. Frequency-setting capacitors of appropriate values, as recommended by the crystal supplier, are connected from each of the two pins to ground (up to a maximum of 30 pF each, including stray capacitance). An external resistor of 1 M Ω to 15 M Ω is connected directly across the pins to ensure linear operation of the amplifier. The required connections for the components are shown in Figure 9.

To turn on the oscillator, bits R15, R14, and R13 must have an octal value of one (001 in binary, respectively). This is the active-crystal mode shown in Figure 16. In this mode, the crystal oscillator runs and the R Counter divides the crystal frequency, unless the part is in standby. If the part is placed in standby via the C register, the oscillator runs, but the R counter is stopped. However, if bits R15 to R13 have a value of 0, the oscillator is stopped, which saves additional power. This is the shut-down crystal mode (shown in Figure 16) and can be engaged whether in standby or not.

In the reference mode, REF_{in} (Pin 20) accepts a signal from an external reference oscillator, such as a TCXO. A signal swinging from at least the V_{IL} to V_{IH} levels listed in the Electrical Characteristics table may be directly coupled to the pin. If the signal is less than this level, ac coupling must be used as shown in Figure 8. Due to an on-board resistor which is engaged in the reference modes, an external biasing resistor tied between REF_{in} and REF_{out} is not required.

With the reference mode, the REF_{out} pin is configured as the output of a divider. As an example, if bits R15, R14, and R13 have an octal value of seven, the frequency at REF_{out} is the REF_{in} frequency divided by 16. In addition, Figure 16 shows how to obtain ratios of eight, four, and two. A ratio of one-to-one can be obtained with an octal value of three. Upon power up, a ratio of eight is automatically initialized. The maximum frequency capability of the REF_{out} pin is listed in the Loop Specifications table for an output swing of 1 V_{pp} and 20 pF loads. Therefore, for higher REF_{in} frequencies, the one-to-one ratio may not be used for this magnitude of signal swing and loading requirements. Likewise, for REF_{in} frequencies above two times the highest rated frequency, the ratio must be more than two.

The output has a special on-board driver that has slew-rate control. This feature minimizes interference in the application.

If REF_{out} is unused, an octal value of two should be used for R15, R14, and R13 and the REF_{out} pin should be floated. A value of two allows REF_{in} to be functional while disabling REF_{out} , which minimizes dynamic power consumption.

LOOP PINS **f_{in} and $\overline{f_{in}}$
Frequency Inputs (Pins 11 and 10)**

These pins are frequency inputs from the VCO. These pins feed the on-board RF amplifier which drives the 64/65 prescaler. These inputs may be fed differentially. However, they are usually used in a single-ended configuration (shown in Figure 7). Note that f_{in} is driven while $\overline{f_{in}}$ must be tied to ground via a capacitor.

Motorola does not recommend driving $\overline{f_{in}}$ while terminating f_{in} because this configuration is not tested for sensitivity. The sensitivity is dependent on the frequency as shown in the Loop Specifications table.

PD_{Out} Single-Ended Phase/Frequency Detector Output (Pin 6)

This is a three-state current-source/sink output for use as a loop error signal when combined with an external low-pass filter. The phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detector is described below and is shown in Figure 17.

POL bit (C7) in the C register = low (see Figure 14)

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : current-sinking pulses from a floating state

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : current-sourcing pulses from a floating state

Frequency and Phase of $f_V = f_R$: essentially a floating state; voltage at pin determined by loop filter

POL bit (C7) = high

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : current-sourcing pulses from a floating state

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : current-sinking pulses from a floating state

Frequency and Phase of $f_V = f_R$: essentially a floating state; voltage at pin determined by loop filter

This output can be enabled, disabled, and inverted via the C register. If desired, PD_{Out} can be forced to the high-impedance state by utilization of the disable feature in the C register (bit C6). This is a patented feature. Similarly, PD_{Out} is forced to the high-impedance state when the device is put into standby (STBY bit C4 = high).

The PD_{Out} circuit is powered by V_{PD}. The phase detector gain is controllable by bits C3, C2, and C1: gain (in amps per radian) = PD_{Out} current divided by 2π .

ϕ_R and ϕ_V (Pins 3 and 4) Double-Ended Phase/Frequency Detector Outputs

These outputs can be combined externally to generate a loop error signal. Through use of a Motorola patented technique, the detector's dead zone has been eliminated. Therefore, the phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detector is described below and is shown in Figure 17.

POL bit (C7) in the C register = low (see Figure 14)

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : ϕ_V = negative pulses, ϕ_R = essentially high

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : ϕ_V = essentially high, ϕ_R = negative pulses

Frequency and Phase of $f_V = f_R$: ϕ_V and ϕ_R remain essentially high, except for a small minimum time period when both pulse low in phase

POL bit (C7) = high

Frequency of $f_V > f_R$ or Phase of f_V Leading f_R : ϕ_R = negative pulses, ϕ_V = essentially high

Frequency of $f_V < f_R$ or Phase of f_V Lagging f_R : ϕ_R = essentially high, ϕ_V = negative pulses

Frequency and Phase of $f_V = f_R$: ϕ_V and ϕ_R remain essentially high, except for a small minimum time period when both pulse low in phase

These outputs can be enabled, disabled, and interchanged via C register bits C6 or C4. This is a patented

feature. Note that when disabled or in standby, ϕ_R and ϕ_V are forced to their rest condition (high state).

The ϕ_R and ϕ_V output signal swing is approximately from Gnd to V_{PD}.

LD Lock Detector Output (Pin 2)

This output is essentially at a high level with narrow low-going pulses when the loop is locked (f_R and f_V of the same phase and frequency). The output pulses low when f_V and f_R are out of phase or different frequencies. LD is the logical ANDING of ϕ_R and ϕ_V (see Figure 17).

This output can be enabled and disabled via the C register. This is a patented feature. Upon power up, on-chip initialization circuitry disables LD to a static low logic level to prevent a false "lock" signal. If unused, LD should be disabled and left open.

The LD output signal swing is approximately from Gnd to V_{DD}.

Rx External Resistor (Pin 8)

A resistor tied between this pin and Gnd, in conjunction with bits in the C register, determines the amount of current that the PD_{Out} pin sinks and sources. When bits C2 and C3 are both set high, the maximum current is obtained at PD_{Out}; see Tables 4 and 5 for other current values. The recommended value for Rx is 3.9 k Ω (preliminary). A value of 3.9 k Ω provides current at the PD_{Out} pin of approximately 1 mA @ V_{DD} = 3 V and approximately 1.7 mA @ V_{DD} = 5 V in the 100% current mode. Note that V_{DD}, not V_{PD}, is a factor in determining the current.

When the ϕ_R and ϕ_V outputs are used, the Rx pin may be floated.

Table 4. PD_{Out} Current*, C1 = Low with Output A not Selected as "Port"; Also, Default Mode When Output A Selected as "Port"

Bit C3	Bit C2	PD _{Out} Current*
0	0	70%
0	1	80%
1	0	90%
1	1	100%

* At the time the data sheet was printed, only the 100% current mode was guaranteed. The reduced current modes were for experimentation only.

Table 5. PD_{Out} Current*, C1 = High with Output A not Selected as "Port"

Bit C3	Bit C2	PD _{Out} Current*
0	0	25%
0	1	50%
1	0	75%
1	1	100%

* At the time the data sheet was printed, only the 100% current mode was guaranteed. The reduced current modes were for experimentation only.

TEST POINT PINS**Test 1****Modulus Control Signal (Pin 9)**

This pin may be used in conjunction with the Test 2 pin for access to the on-board 64/65 prescaler. When Test 1 is low, the prescaler divides by 65. When high, the prescaler divides by 64.

CAUTION

This pin is an unbuffered output and must be floated in an actual application. This pin must be attached to an isolated pad with no trace.

Test 2**Prescaler Output (Pin 13)**

This pin may be used to access the on-board 64/65 prescaler output.

CAUTION

This pin is an unbuffered output and must be floated in an actual application. This pin must be attached to an isolated pad with no trace.

POWER SUPPLY PINS**V_{DD}****Positive Power Supply (Pin 14)**

This pin supplies power to the main CMOS digital portion of the device. Also, this pin, in conjunction with the Rx resistor, determines the internal reference current for the PD_{Out} pin. The voltage range is 2.7 to 5.5 V with respect to the Gnd pin.

For optimum performance, V_{DD} should be bypassed to Gnd using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

V_{CC}**Positive Power Supply (Pin 12)**

This pin supplies power to the RF amp and 64/65 prescaler. The voltage range is 2.7 to 5.5 V with respect to the Gnd pin. In standby mode, the V_{CC} pin still draws a few milliamps from the power supply. This current drain can be eliminated with the use of transistor Q1 as shown in Figure 21.

For optimum performance, V_{CC} should be bypassed to Gnd using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

V_{PD}**Positive Power Supply (Pin 5)**

This pin supplies power to both phase/frequency detectors A and B. The voltage applied on this pin may be more or less than the potential applied to the V_{DD} and V_{CC} pins. The voltage range for V_{PD} is 2.7 to 5.5 V with respect to the Gnd pin.

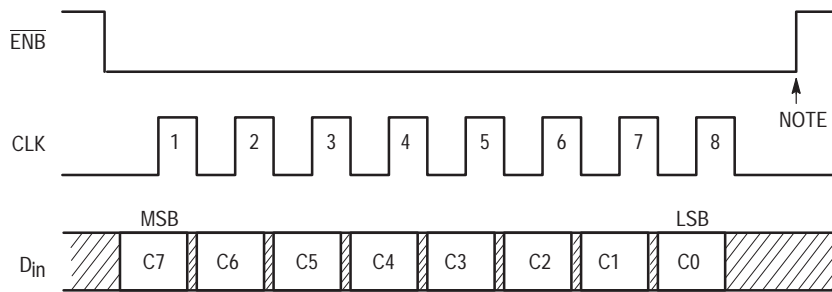
For optimum performance, V_{PD} should be bypassed to Gnd using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

Gnd**Ground (Pin 7)**

Common ground.

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Figure 14. C Register Access and Format
(8 Clock Cycles are Used)

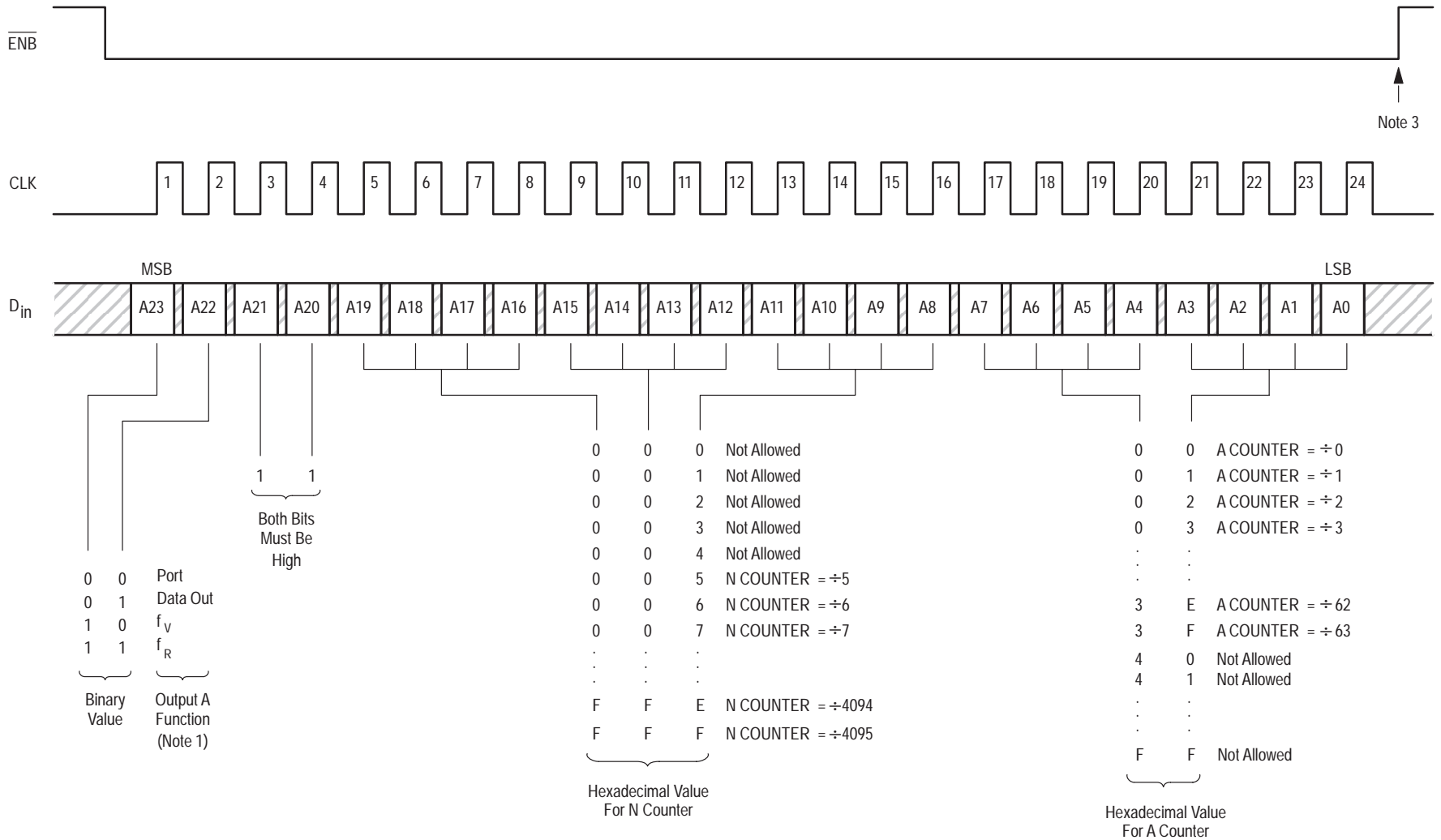


NOTE: At this point, the new byte is transferred to the C register and stored. No other registers are affected.

- C7 – POL: Selects the output polarity of the phase/frequency detectors. When set high, this bit inverts PD_{Out} and interchanges the ϕ_R function with ϕ_V as depicted in Figure 17. Also see the phase detector output pin descriptions for more information. This bit is cleared low at power up.
- C6 – PDA/B: Selects which phase/frequency detector is to be used. When set high, enables the output of phase/frequency detector A (PD_{Out}) and disables phase/frequency detector B by forcing ϕ_R and ϕ_V to the static high state. When cleared low, phase/frequency detector B is enabled (ϕ_R and ϕ_V) and phase/frequency detector A is disabled with PD_{Out} forced to the high-impedance state. This bit is cleared low at power up.
- C5 – LDE: Enables the lock detector output when set high. When the bit is cleared low, the LD output is forced to a static low level. This bit is cleared low at power up.
- C4 – STBY: When set, places the CMOS section of device, which is powered by the V_{DD} and V_{PD} pins, in the standby mode for reduced power consumption: PD_{Out} is forced to the high-impedance state, ϕ_R and ϕ_V are forced high, the A, N, and R counters are inhibited from counting, and the Rx current is shut off. In standby, the state of LD is determined by bit C5. C5 low forces LD low (no change). C5 high forces LD static high. During standby, data is retained in the A, R, and C registers. The condition of REF/OSC circuitry is determined by the control bits in the R register: R13, R14, and R15. However, if REF_{Out} = static low is selected, the internal feedback resistor is disconnected and the input is inhibited when in standby; in addition, the REF_{In} input only presents a capacitive load. NOTE: Standby does not affect the other modes of the REF/OSC circuitry.

When C4 is reset low, the part is taken out of standby in two steps. First, the REF_{In} (only in one mode) resistor is reconnected, all counters are enabled, and the Rx current is enabled. Any f_R and f_V signals are inhibited from toggling the phase/frequency detectors and lock detector. Second, when the first f_V pulse occurs, the R counter is jam loaded, and the phase/frequency and lock detectors are initialized. Immediately after the jam load, the A, N, and R counters begin counting down together. At this point, the f_R and f_V pulses are enabled to the phase and lock detectors. (Patented feature.)
- C3, C2 – I2, I1: Controls the PD_{Out} source/sink current per Tables 4 and 5. With both bits high, the maximum current is available. Also, see C1 bit description.
- C1 – Port: When the Output A pin is selected as "Port" via bits A22 and A23, C1 determines the state of Output A. When C1 is set high, Output A is forced high; C1 low forces Output A low. When Output A is **not** selected as "Port," C1 controls whether the PD_{Out} step size is 10% or 25%. (See Tables 4 and 5.) When low, steps are 10%. When high, steps are 25%. Default is 10% steps when Output A is selected as "Port." The Port bit is not affected by the standby mode.
- C0 – Out B: Determines the state of Output B. When C0 is set high, Output B is high-impedance; C0 low forces Output B low. The Out B bit is not affected by the standby mode. This bit is cleared low at power up.

Figure 15. A Register Access and Format
(24 Clock Cycles are Used)



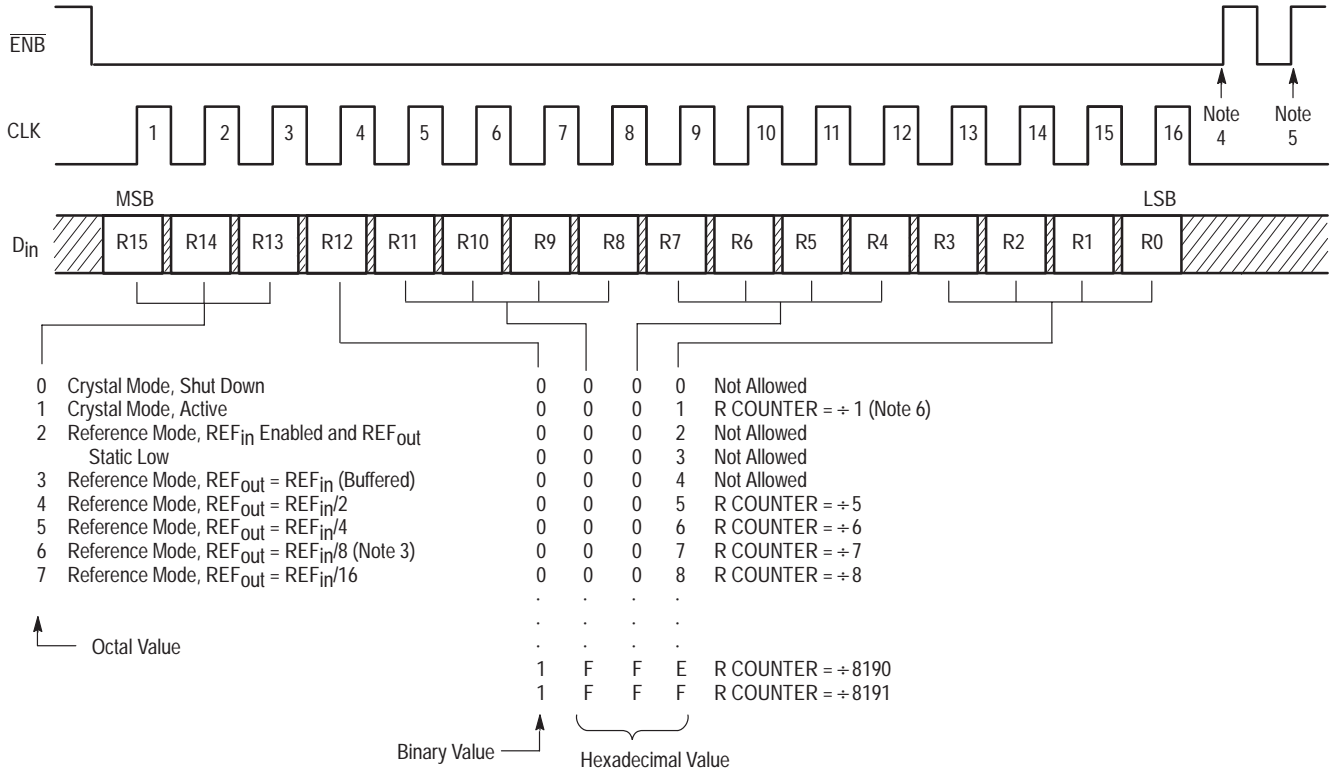
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NOTES:

1. A power-on initialize circuit forces the Output A function to default to Data Out.
2. The values programmed for the N counter must be greater than or equal to the values programmed for the A counter. This results in a total divide value = N x 64 + A.
3. At this point, the three new bytes are transferred to the A register. In addition, the 13 LSBs in the first buffer of the R register are transferred to the R register's second buffer. Thus, the R, N, and A counters can be presented new divide ratios at the same time. The first buffer of the R register is not affected. The C register is not affected.

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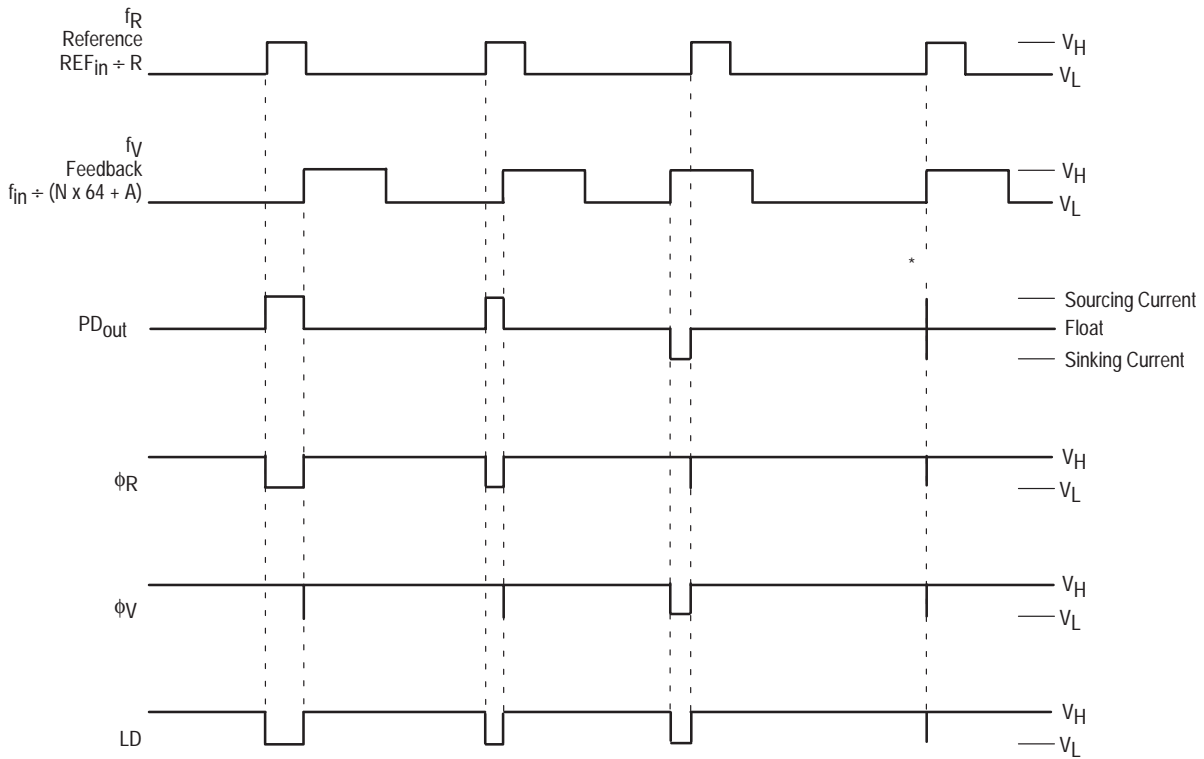
Figure 16. R Register Access and Format
(16 Clock Cycles are Used)



NOTES:

- Bits R15 through R13 control the configurable “OSC or 4-stage divider” block (see Block Diagram).
- Bits R12 through R0 control the “13-stage R counter” block (see Block Diagram).
- A power-on initialize circuit forces a default REF_{in} to REF_{out} ratio of eight.
- At this point, bits R13, R14, and R15 are stored and sent to the “OSC or 4-Stage Divider” block in the Block Diagram. Bits R0 – R12 are loaded into the first buffer in the double-buffered section of the R register. Therefore, the R counter divide ratio is not altered yet and retains the previous ratio loaded. The C and A registers are not affected.
- Optional load pulse. At this point, bits R0 – R12 are transferred to the second buffer of the R register. The R counter begins dividing by the new ratio after completing the rest of the present count cycle. CLK must be low during the ENB pulse, as shown. The C and A registers are not affected. The first buffer of the R register is not affected. Also, see Note 3 of Figure 15 for an alternate method of loading the second buffer in the R register.
- Allows direct access to reference input of phase/frequency detectors.

Figure 17. Phase/Frequency Detectors and Lock Detector Output Waveforms



V_H = High voltage level

V_L = Low voltage level

*At this point, when both f_R and f_V are in phase, the output source and sink circuits are turned on for a short interval.

NOTE: The PD_{out} either sources or sinks current during out-of-lock conditions. When locked in phase and frequency, the output is in the floating condition and the voltage at that pin is determined by the low-pass filter capacitor. PD_{out}, ϕ_R , and ϕ_V are shown with the polarity bit (POL) = low; see Figure 14 for POL.

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DESIGN CONSIDERATIONS

Crystal Oscillator Considerations

The following options may be considered to provide a reference frequency to Motorola's CMOS frequency synthesizers.

Use of a Hybrid Crystal Oscillator

Commercially available temperature-compensated crystal oscillators (TCXOs) or crystal-controlled data clock oscillators provide very stable reference frequencies. An oscillator capable of CMOS logic levels at the output may be direct or dc coupled to REF_{in}. If the oscillator does not have CMOS logic levels on the outputs, capacitive or ac coupling to REF_{in} may be used (see Figure 8).

For additional information about TCXOs and data clock oscillators, please consult the latest version of the *eem Electronic Engineers Master Catalog*, the *Gold Book*, or similar publications.

Design an Off-Chip Reference

The user may design an off-chip crystal oscillator using discrete transistors or ICs specifically developed for crystal oscillator applications. The reference signal is usually ac coupled to REF_{in} (see Figure 8). For large amplitude signals (standard CMOS logic levels), dc coupling may be used.

Use of the On-Chip Oscillator Circuitry

The on-chip amplifier (a digital inverter) along with an appropriate crystal may be used to provide a reference source frequency. A fundamental mode crystal, parallel resonant at the desired operating frequency, should be connected as shown in Figure 18.

The crystal should be specified for a loading capacitance (C_L) which does not exceed approximately 20 pF when used at the highest operating frequencies listed in the Loop Specifications table. Assuming R1 = 0 Ω, the shunt load capacitance (C_L) presented across the crystal can be estimated to be:

$$C_L = \frac{C_{in}C_{out}}{C_{in} + C_{out}} + C_a + C_{stray} + \frac{C_1 \cdot C_2}{C_1 + C_2}$$

where

C_{in} = 5 pF (see Figure 19)

C_{out} = 6 pF (see Figure 19)

C_a = 1 pF (see Figure 19)

C1 and C2 = external capacitors (see Figure 18)

C_{stray} = the total equivalent external circuit stray capacitance appearing across the crystal terminals

The oscillator can be "trimmed" on-frequency by making a portion or all of C1 variable. The crystal and associated components must be located as close as possible to the REF_{in} and REF_{out} pins to minimize distortion, stray capacitance, stray inductance, and startup stabilization time. Circuit stray capacitance can also be handled by adding the appropriate stray value to the values for C_{in} and C_{out}. For this approach, the term C_{stray} becomes 0 in the above expression for C_L.

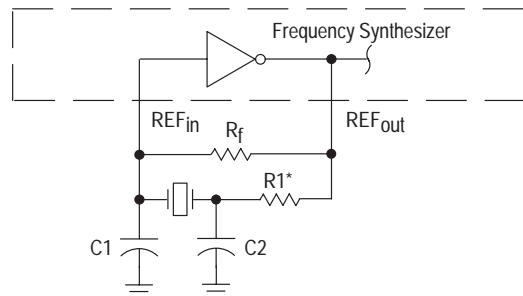
Power is dissipated in the effective series resistance of the crystal, R_e, in Figure 20. The maximum drive level specified by the crystal manufacturer represents the maximum stress that the crystal can withstand without damage or excessive

shift in operating frequency. R1 in Figure 18 limits the drive level. The use of R1 is not necessary in most cases.

To verify that the maximum dc supply voltage does not cause the crystal to be overdriven, monitor the output frequency (f_R) at Output A as a function of supply voltage. (REF_{out} is not used because loading impacts the oscillator.) The frequency should increase very slightly as the dc supply voltage is increased. An overdriven crystal decreases in frequency or becomes unstable with an increase in supply voltage. The operating supply voltage must be reduced or R1 must be increased in value if the overdriven condition exists. The user should note that the oscillator start-up time is proportional to the value of R1.

Through the process of supplying crystals for use with CMOS inverters, many crystal manufacturers have developed expertise in CMOS oscillator design with crystals. Discussions with such manufacturers can prove very helpful (see Table 2).

Figure 18. Pierce Crystal Oscillator Circuit



* May be needed in certain cases. See text.

Figure 19. Parasitic Capacitances of the Amplifier and C_{stray}

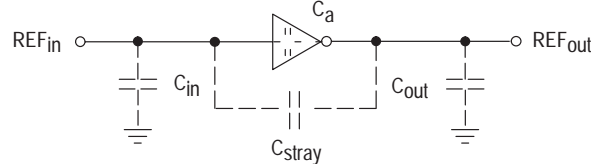
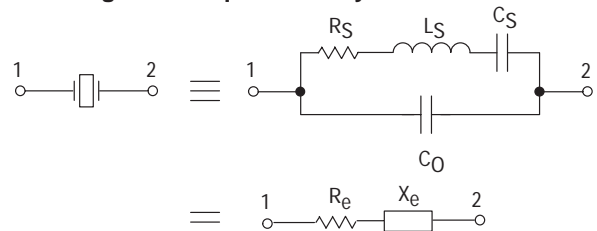


Figure 20. Equivalent Crystal Networks



NOTE: Values are supplied by crystal manufacturer (parallel resonant crystal).

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RECOMMENDED READING

Technical Note TN-24, Statek Corp.
Technical Note TN-7, Statek Corp.
E. Hafner, "The Piezoelectric Crystal Unit-Definitions and Method of Measurement", *Proc. IEEE*, Vol. 57, No. 2, Feb. 1969.
D. Kemper, L. Rosine, "Quartz Crystals for Frequency Control", *Electro-Technology*, June 1969.

P. J. Ottowitz, "A Guide to Crystal Selection", *Electronic Design*, May 1966.

D. Babin, "Designing Crystal Oscillators", *Machine Design*, March 7, 1985.

D. Babin, "Guidelines for Crystal Oscillator Design", *Machine Design*, April 25, 1985.

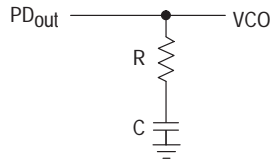
Table 6. Partial List of Crystal Manufacturers

CTS Corp.
United States Crystal Corp.
Crystek Crystal
Statek Corp.
Fox Electronics

NOTE: Motorola cannot recommend one supplier over another and in no way suggests that this is a complete listing of crystal manufacturers.

PHASE-LOCKED LOOP — LOW-PASS FILTER DESIGN

(A)



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NC}}$$

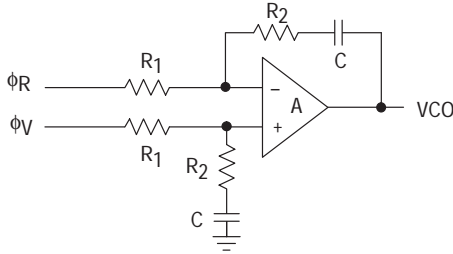
$$\zeta = \frac{R}{2} \sqrt{\frac{K_\phi K_{VCO} C}{N}} = \frac{\omega_n RC}{2}$$

$$Z(s) = \frac{1 + sRC}{sC}$$

NOTE:

For (A), using K_ϕ in amps per radian with the filter's impedance transfer function, $Z(s)$, maintains units of volts per radian for the detector/filter combination. Additional sideband filtering can be accomplished by adding a capacitor C' across R . The corner $\omega_c = 1/RC'$ should be chosen such that ω_n is not significantly affected.

(B)



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NCR_1}}$$

$$\zeta = \frac{\omega_n R_2 C}{2}$$

Assuming Gain A is very large, then:

$$F(s) = \frac{R_2 s C + 1}{R_1 s C}$$

NOTE:

For (B), R_1 is frequently split into two series resistors; each resistor is equal to R_1 divided by 2. A capacitor C_C is then placed from the midpoint to ground to further filter the error pulses. The value of C_C should be such that the corner frequency of this network does not significantly affect ω_n .

DEFINITIONS:

N = Total Division Ratio in Feedback Loop

K_ϕ (Phase Detector Gain) = $I_{PDout}/2\pi$ amps per radian for PD_{out}

K_ϕ (Phase Detector Gain) = $V_{PD}/2\pi$ volts per radian for ϕ_V and ϕ_R

K_{VCO} (VCO Transfer Function) = $\frac{2\pi\Delta f_{VCO}}{\Delta V_{VCO}}$ radians per volt

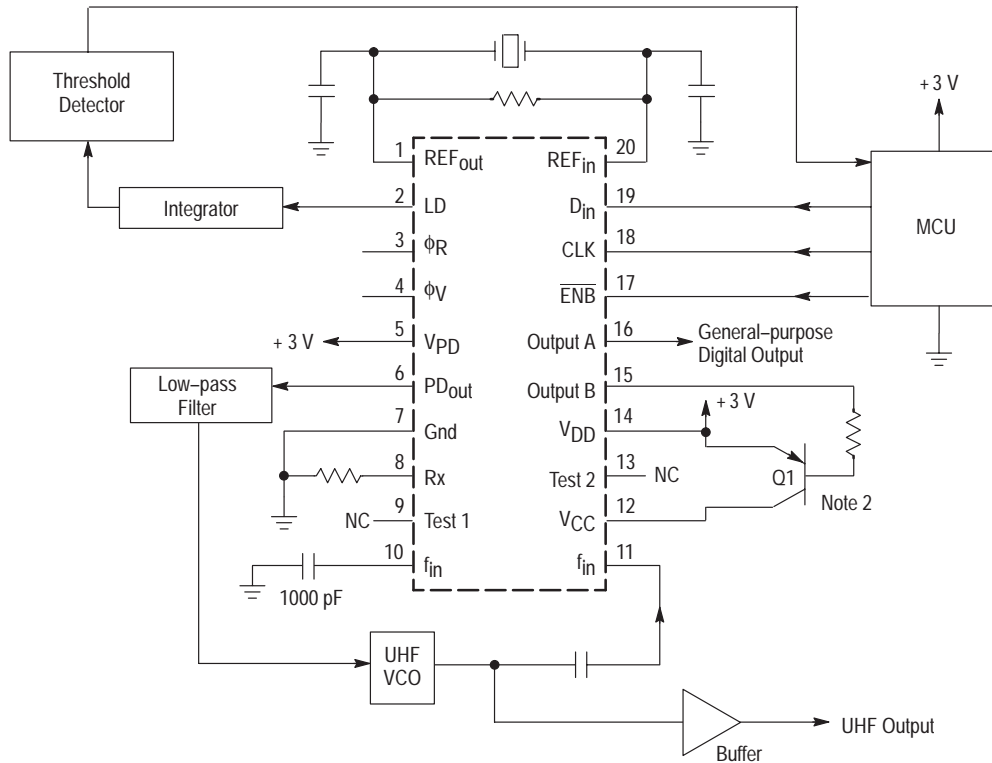
For a nominal design starting point, the user might consider a damping factor $\zeta \approx 0.7$ and a natural loop frequency $\omega_n \approx (2\pi f_R/50)$ where f_R is the frequency at the phase detector input. Larger ω_n values result in faster loop lock times and, for similar sideband filtering, higher f_R -related VCO sidebands.

Either loop filter (A) or (B) is frequently followed by additional sideband filtering to further attenuate f_R -related VCO sidebands. This additional filtering may be active or passive.

RECOMMENDED READING:

Gardner, Floyd M., *Phaselock Techniques (second edition)*. New York, Wiley-Interscience, 1979.
 Manassewitsch, Vadim, *Frequency Synthesizers: Theory and Design (second edition)*. New York, Wiley-Interscience, 1980.
 Blanchard, Alain, *Phase-Locked Loops: Application to Coherent Receiver Design*. New York, Wiley-Interscience, 1976.
 Egan, William F., *Frequency Synthesis by Phase Lock*. New York, Wiley-Interscience, 1981.
 Rohde, Ulrich L., *Digital PLL Frequency Synthesizers Theory and Design*. Englewood Cliffs, NJ, Prentice-Hall, 1983.
 Berlin, Howard M., *Design of Phase-Locked Loop Circuits, with Experiments*. Indianapolis, Howard W. Sams and Co., 1978.
 Kinley, Harold, *The PLL Synthesizer Cookbook*. Blue Ridge Summit, PA, Tab Books, 1980.
 Seidman, Arthur H., *Integrated Circuits Applications Handbook*, Chapter 17, pp. 538-586. New York, John Wiley & Sons.
 Fadrhons, Jan, "Design and Analyze PLLs on a Programmable Calculator," *EDN*. March 5, 1980.
 AN535, Phase-Locked Loop Design Fundamentals, Motorola Semiconductor Products, Inc., 1970.
 AR254, Phase-Locked Loop Design Articles, Motorola Semiconductor Products, Inc., Reprinted with permission from *Electronic Design*, 1987.
 AN1253, An Improved PLL Design Method Without ω_n and ζ , Motorola Semiconductor Products, Inc., 1995.

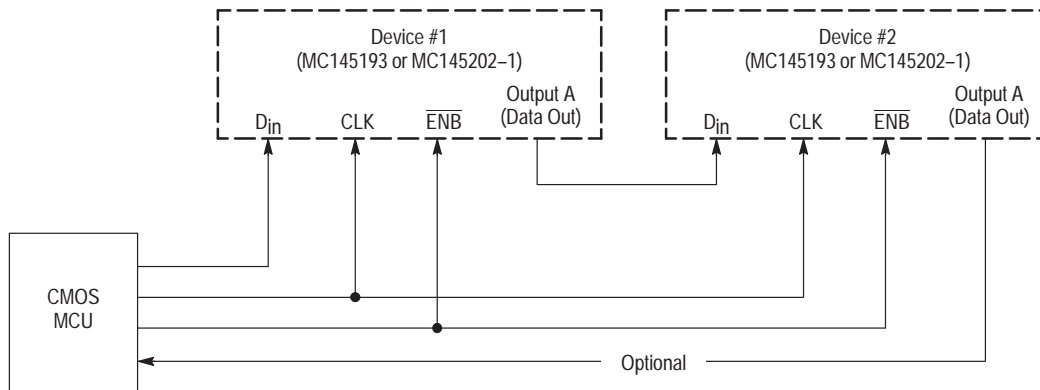
Figure 21. Example Application



NOTES:

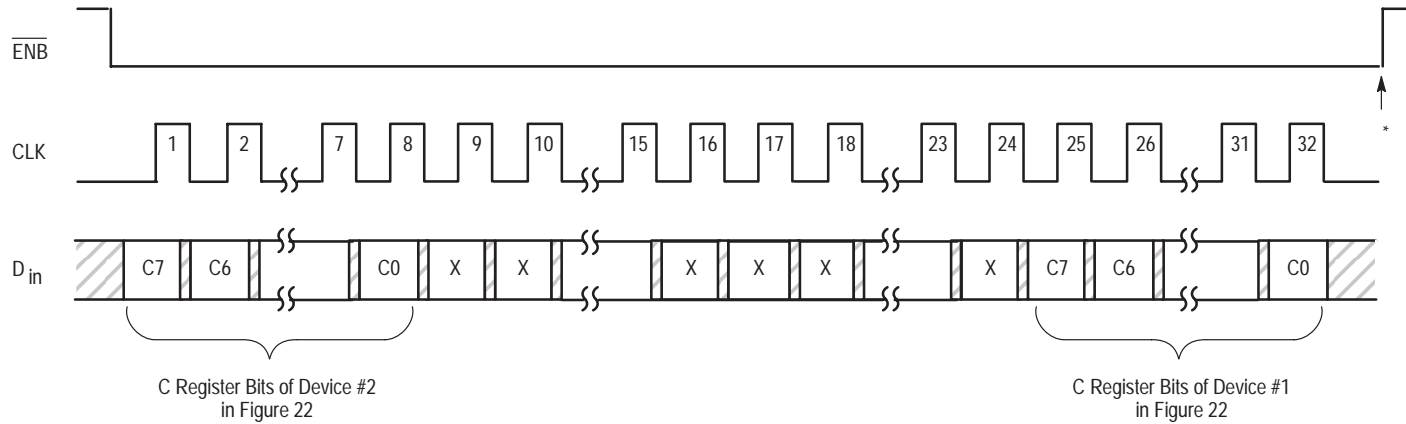
- 1 When used, the ϕ_R and ϕ_V outputs are fed to an external combiner/loop filter. See the Phase-Locked Loop — Low-Pass Filter Design (Page 4.2-142) for additional information.
- 2 Transistor Q1 is required only if the standby feature is needed. Q1 permits the bipolar section of the device to be shut down via use of the general-purpose digital pin, Output B. If the standby feature is not needed, tie Pin 12 directly to the power supply.
- 3 For optimum performance, bypass the V_{CC} , V_{DD} , and V_{PD} pins to Gnd with low-inductance capacitors.
- 4 The R counter is programmed for a divide value = REF_{in}/f_R . Typically, f_R is the tuning resolution required for the VCO. Also, the VCO frequency divided by $f_R = N_T = N \times 64 + A$; this determines the values (N, A) that must be programmed into the N and A counters, respectively.

Figure 22. Cascading Two Devices



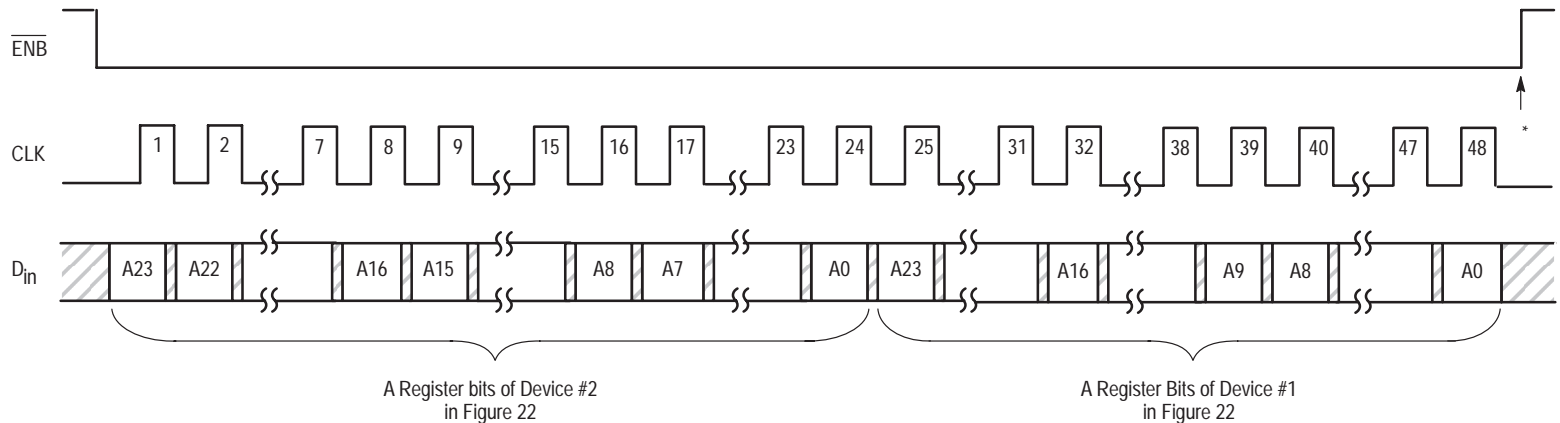
NOTE: See related Figures 23, 24, and 25.

Figure 23. Accessing the C Registers of Two Cascaded MC145193 or MC145202-1 Devices



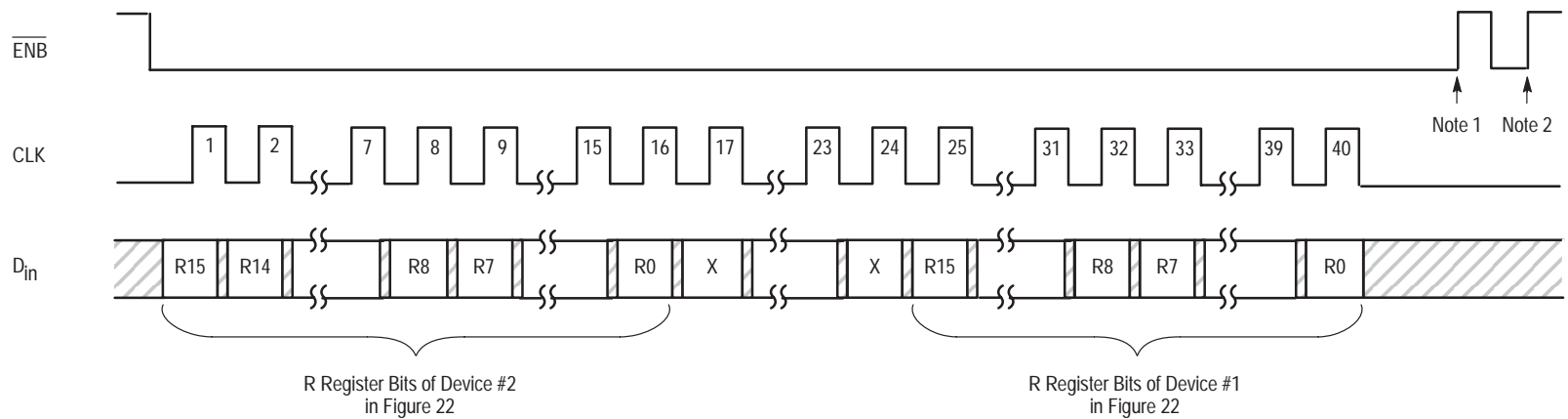
*At this point, the new bytes are transferred to the C registers of both devices and stored. No other registers are affected.

Figure 24. Accessing the A Registers of Two Cascaded MC145193 or MC145202-1 Devices



* At this point, the new bytes are transferred to the A registers of both devices and stored. Additionally, for both devices, the 13 LSBs in each of the first buffers of the R registers are transferred to the respective R register's second buffer. Thus, the R, N, and A counter can be presented new divide ratios at the same time. The first buffer of each R register is not affected. Neither C register is affected.

Figure 25. Accessing the R Registers of Two Cascaded MC145193 or MC145202-1 Devices



Notes Applicable to Each Device:

1. At this point, bits R13, R14 and R15 are stored and sent to the "OSC or 4-Stage Divider" block in the Block Diagram. Bits R0 through R12 are loaded into the first buffer in the double-buffered section of the R register. Therefore, the R counter divide is not altered yet and retains the previous ratio loaded. The C and A registers are not affected.
2. Optional load pulse. At this point, the bits R0 through R12 are transferred to the second buffer of the R register. The R counter begins dividing by the new ratio after completing the rest of the present count cycle. CLK must be low during the ENB pulse, as shown. The C and A registers are not affected. The first buffer of the R register is not affected. Also, see note of Figure 24 for an alternate method of loading the second buffer in the R register.

Dual 1.1 GHz PLL Frequency Synthesizer

BiCMOS

The MC145220 is a low-voltage, single-chip frequency synthesizer with serial interface capable of direct usage up to 1.1 GHz. The device simultaneously supports two loops. The two on-chip dual-modulus prescalers may be independently programmed to divide by either 32/33 or 64/65.

The device consists of two dual-modulus prescalers, two 6-stage A counters, two 12-stage N counters, two fully programmable 13-stage R (reference) counters, and two lock detectors. Four phase/frequency detectors are included: two with current source/sink outputs and two with double-ended outputs.

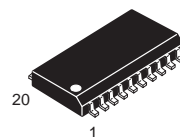
The counters are programmed via a synchronous serial port which is SPI compatible. The serial port is byte-oriented to facilitate control via an MCU. Due to the innovative BitGrabber Plus™ registers, the MC145220 may be cascaded with other peripherals featuring BitGrabber Plus without requiring leading dummy bits or multiple address bits in the serial data stream. In addition, BitGrabber Plus peripherals may be cascaded with existing BitGrabber™ peripherals. Because this device is a dual synthesizer, a single steering bit is used in the serial data stream to direct the data to either side of the chip.

The phase/frequency detectors have linear transfer functions (no dead zones). The current delivered by the current source/sink outputs is controllable via the serial port.

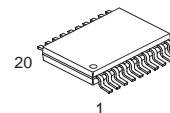
Also featured are low-power standby for either one or both loops and on-board support of an external crystal. In addition, the part may be configured such that the REF_{IN} pin accepts an external reference signal. In this configuration, the REF_{OUT} pin may be programmed to output the REF_{IN} frequency divided by 1, 2, 4, 8, or 16.

- Operating Frequency: 40 to 1100 MHz
- Operating Supply Voltage Range: 2.7 to 5.5 V
- Supply Current: Both PLLs Operating — 12 mA Nominal
One PLL Operating, One on Standby — 6.5 mA Nominal
Both PLLs on Standby — 30 µA Maximum
- Phase Detector Output Current: Up to 2 mA @ 5 V
Up to 1 mA @ 3 V
- Operating Temperature Range: – 40 to 85°C
- Independent R Counters Allow Use of Different Step Sizes for Each Loop
- Double-Buffered R Register — Reference and Loop Divide Ratios Updated Simultaneously
- R Counter Division Range: 1 and 10 to 8,191
- Dual-Modulus Capability Provides Total Division of the VCO Frequency up to 262,143
- Direct Interface to Motorola SPI Data Port
- Evaluation Kit Available (Part Number MC145220EVK)
- See Application Note AN1253/D for Low-Pass Filter Design, and AN1277/D for Offset Reference PLLs for Fine Resolution or Fast Hopping

MC145220



F SUFFIX
SOG PACKAGE
CASE 803C



DT SUFFIX
TSSOP
CASE 948D

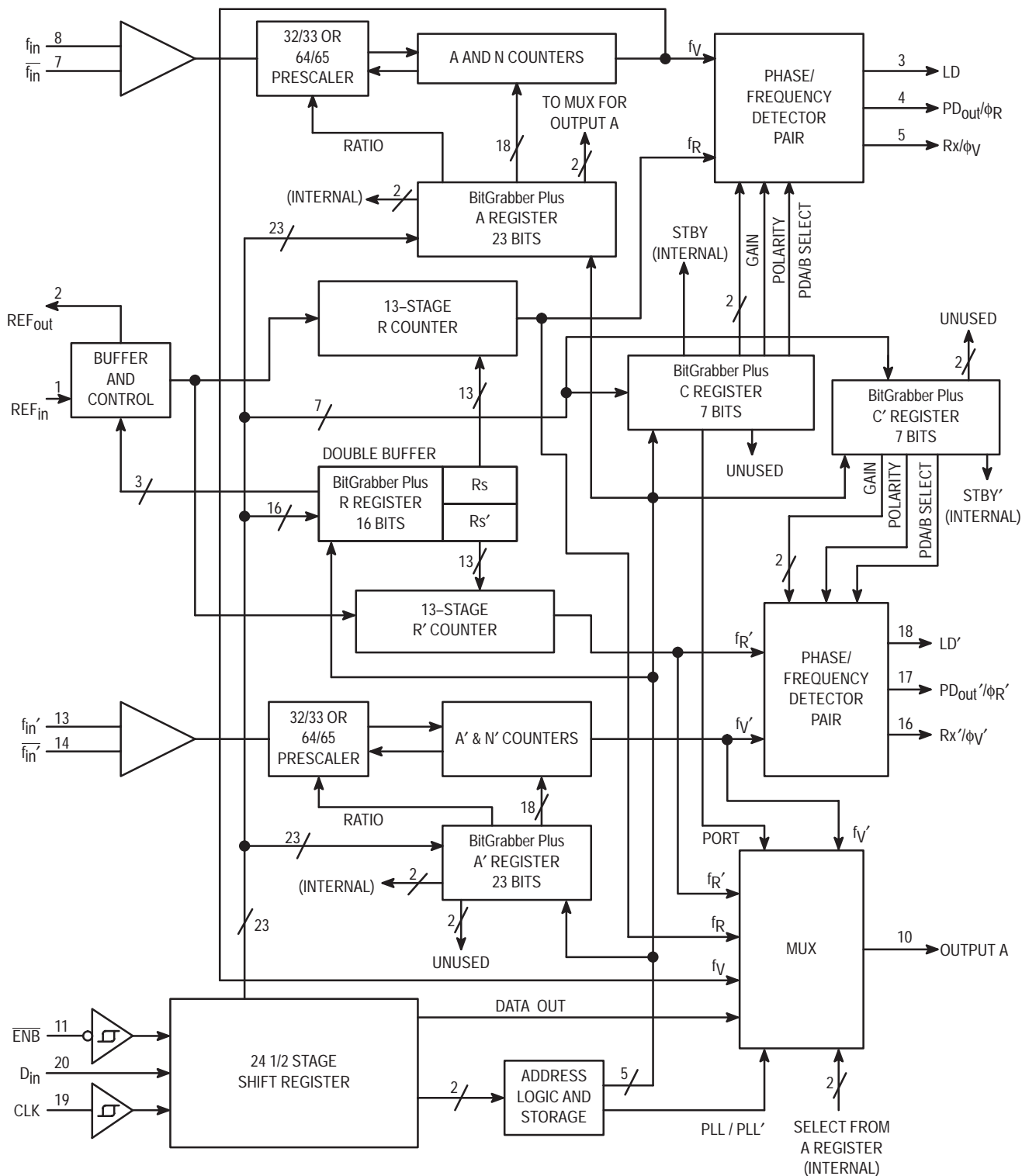
ORDERING INFORMATION

MC145220F SOG Package
MC145220DT TSSOP

PIN ASSIGNMENT

REF _{IN}	1	20	D _{IN}
REF _{OUT}	2	19	CLK
LD	3	18	LD'
PD _{OUT} /φ _R	4	17	PD _{OUT} '/φ _R '
R _X /φ _V	5	16	R _X '/φ _V '
GND	6	15	GND'
f _{IN}	7	14	f _{IN} '
f _{IN}	8	13	f _{IN} '
V+	9	12	V+'
OUTPUT A	10	11	ENB

BLOCK DIAGRAM



- PIN 9 = V+ (Positive Power to the main PLL, Reference Circuit, and a portion of the Serial Port)
- PIN 6 = GND (Ground to the main PLL, Reference Circuit, and a portion of the Serial Port)
- PIN 12 = V+' (Positive Power to PLL' and a portion of the Serial Port)
- PIN 15 = GND' (Ground to PLL' and a portion of the Serial Port)

MAXIMUM RATINGS* (Voltages Referenced to GND, unless otherwise stated)

Symbol	Parameter	Value	Unit
V+, V+'	DC Supply Voltage	- 0.5 to + 6.0	V
V _{in}	DC Input Voltage	- 0.5 to V+ + 0.5	V
V _{out}	DC Output Voltage	- 0.5 to V+ + 0.5	V
I _{in}	DC Input Current, per Pin	± 10	mA
I _{out}	DC Output Current, per Pin	± 20	mA
I	DC Supply Current, V+, V+', GND, and GND' Pins	30	mA
P _D	Power Dissipation, per Package	300	mW
T _{stg}	Storage Temperature	- 65 to + 150	°C
T _L	Lead Temperature, 1 mm from Case for 10 Seconds	260	°C

This device contains protection circuitry to guard against damage due to high static voltages or electric fields. However, precautions must be taken to avoid applications of any voltage higher than maximum rated voltages to this high-impedance circuit.

* Maximum Ratings are those values beyond which damage to the device may occur. Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section.

ELECTRICAL CHARACTERISTICS

(V+ = V+ ' = 2.7 to 5.5 V, GND = GND', Voltages Referenced to GND, T_A = - 40 to 85°C, unless otherwise stated)

Symbol	Parameter	Test Condition	Guaranteed Limit	Unit
V _{IL}	Maximum Low-Level Input Voltage (D _{in} , CLK, $\overline{\text{ENB}}$, REF _{in})	Device in Reference Mode, dc Coupled	0.3 x V+	V
V _{IH}	Minimum High-Level Input Voltage (D _{in} , CLK, $\overline{\text{ENB}}$, REF _{in})	Device in Reference Mode, dc Coupled	0.7 x V+	V
V _{Hys}	Minimum Hysteresis Voltage (CLK, $\overline{\text{ENB}}$)		100	mV
V _{OL}	Maximum Low-Level Output Voltage (LD, LD', REF _{out} , Output A)	I _{out} = 20 μA, Device in Reference Mode; Output A Not Selected as Port	0.1	V
V _{OH}	Minimum High-Level Output Voltage (REF _{out} , Output A)	I _{out} = - 20 μA, Device in Reference Mode; Output A Not Selected as Port	V+ - 0.1	V
I _{OL}	Minimum Low-Level Output Current (REF _{out})	V _{out} = 0.3 V	0.5	mA
I _{OL}	Minimum Low-Level Output Current (PD _{out} /φ _R , PD _{out} '/φ _R ', Rx/φ _V , Rx'/φ _V ')	V _{out} = 0.3 V; Phase/Frequency Detectors Configured with φ _R , φ _V Outputs	0.5	mA
I _{OL}	Minimum Low-Level Output Current (Output A)	V _{out} = 0.3 V	0.5	mA
I _{OL}	Minimum Low-Level Output Current (LD, LD')	V _{out} = 0.3 V	0.5	mA
I _{OH}	Minimum High-Level Output Current (REF _{out})	V _{out} = V+ - 0.3 V	- 0.4	mA
I _{OH}	Minimum High-Level Output Current (PD _{out} /φ _R , PD _{out} '/φ _R ', Rx/φ _V , Rx'/φ _V ')	V _{out} = V+ - 0.3 V; Phase/Frequency Detectors Configured with φ _R , φ _V Outputs	- 0.4	mA
I _{OH}	Minimum High-Level Output Current (Output A)	V _{out} = V+ - 0.3 V; Output A Not Selected as Port	- 0.4	mA
I _{in}	Maximum Input Leakage Current (D _{in} , CLK, $\overline{\text{ENB}}$, REF _{in})	V _{in} = V+ or GND; Device in XTAL Mode	± 1.0	μA
I _{in}	Maximum Input Current (REF _{in})	V _{in} = V+ or GND; Device in Reference Mode	± 150	μA
I _{OZ}	Maximum Output Leakage Current (PD _{out} /φ _R , PD _{out} '/φ _R ')	V _{out} = V+ or GND; Phase/Frequency Detectors Configured with PD _{out} Output, Output in High- Impedance State	± 150	nA
I _{OZ}	Maximum Output Leakage Current (Output A, LD, LD')	V _{out} = V+ or GND; Output A Selected as Port; Output in High-Impedance State	± 5	μA
I _{STBY}	Maximum Standby Supply Current	V _{in} = V+ or GND; Outputs Open; Both PLLs in Standby Mode, Shut-Down Crystal Mode or REF _{out} -Static-Low Reference Mode	30	μA
I _T	Total Operating Supply Current	f _{in} = f _{in} ' = 1.1 GHz; both loops active; REF _{in} = 13 MHz @ 1 V p-p; Output A = Inactive; All Outputs = No Connect; D _{in} , ENB, CLK = V+ or GND; Phase/Frequency Detectors Configured with φ _R , φ _V Outputs	*	mA

* The nominal value is 12 mA. This is not a guaranteed limit.

ANALOG CHARACTERISTICS — CURRENT SOURCE/SINK OUTPUTS — PD_{out}/ϕ_R AND PD_{out}'/ϕ_R'

(Phase/Frequency Detectors Configured with PD_{out} Outputs, $I_{out} \leq 2 \text{ mA}$ @ $V_+ = V_+' = 4.5$ to 5.5 V , $I_{out} \leq 1 \text{ mA}$ @ $V_+ = V_+' = 2.7$ to 4.4 V , $GND = GND'$, Voltages Referenced to GND)

Parameter	Test Condition	Guaranteed Limit	Unit
Maximum Source Current Variation Part-to-Part (Notes 3 and 4)	$V_{out} = 0.5 \times V_+$	± 20	%
Maximum Sink-versus-Source Mismatch (Note 3)	$V_{out} = 0.5 \times V_+$	12	%
Output Voltage Range (Note 3)	I_{out} variation $\leq 20\%$	0.5 to $V_+ - 0.5 \text{ V}$	V

NOTES:

- Percentages calculated using the following formula: (Maximum Value – Minimum Value)/Maximum Value.
- See Rx Pin Description for external resistor values.
- This parameter is guaranteed for a given temperature within -40 to 85°C and given supply voltage within 2.7 to 5.5 V .
- Applicable for the Rx/ϕ_V or Rx'/ϕ_V' reference pin tied to the GND or GND' pin through a resistor. See Pin Descriptions for suggested resistor values.

AC INTERFACE CHARACTERISTICS

($V_+ = V_+' = 2.7$ to 5.5 V , $GND = GND'$, $T_A = -40$ to 85°C , $C_L = 25 \text{ pF}$, Input $t_r = t_f = 10 \text{ ns}$)

Symbol	Parameter	Guaranteed Limit	Unit
f_{clk}	Serial Data CLK Frequency (Figure 1) NOTE: Refer to Clock t_w below	dc to 2.0	MHz
t_{PLH} , t_{PHL}	Maximum Propagation Delay, CLK to Output A (Selected as Data Out) (Figures 1 and 5)	200	ns
t_{PZL} , t_{PLZ}	Maximum Propagation Delay, \overline{ENB} to Output A (Selected as Port) (Figures 2 and 6)	200	ns
t_{TLH} , t_{THL}	Maximum Output Transition Time, Output A; t_{THL} only, on Output A when Selected as Port (Figures 1, 5, and 6)	200	ns
C_{in}	Maximum Input Capacitance — D_{in} , CLK, \overline{ENB}	10	pF

TIMING REQUIREMENTS ($V_+ = V_+' = 2.7$ to 5.5 V , $GND = GND'$, $T_A = -40$ to 85°C , Input $t_r = t_f = 10 \text{ ns}$ unless otherwise indicated)

Symbol	Parameter	Guaranteed Limit	Unit
t_{su} , t_h	Minimum Setup and Hold Times, D_{in} versus CLK (Figure 3)	50	ns
t_{su} , t_h , t_{rec}	Minimum Setup, Hold, and Recovery Times, \overline{ENB} versus CLK (Figure 4)	100	ns
t_w	Minimum Pulse Width, \overline{ENB} (Figure 4)	*	cycles
t_w	Minimum Pulse Width, CLK (Figure 1)	250	ns
t_r , t_f	Maximum Input Rise and Fall Times — CLK (Figure 1)	100	μs

* The minimum limit is 3 REF_{in} cycles or $195 f_{in}$ or f_{in}' cycles with selection of a 64/65 prescale ratio or $99 f_{in}$ or f_{in}' cycles with selection of a 32/33 prescale ratio, whichever is greater.

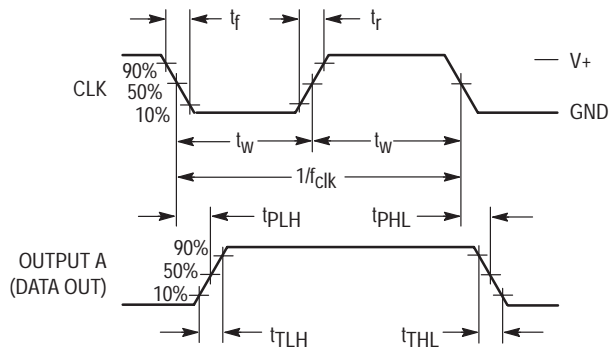


Figure 1.

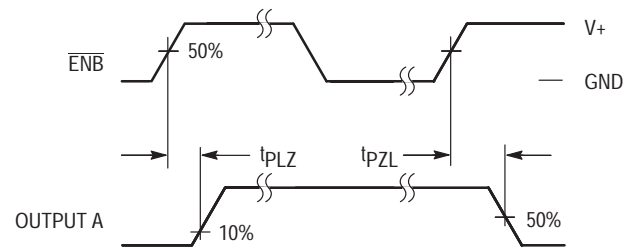


Figure 2.

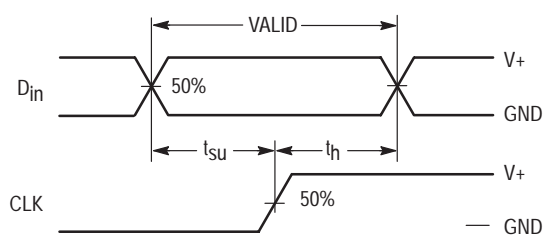


Figure 3.

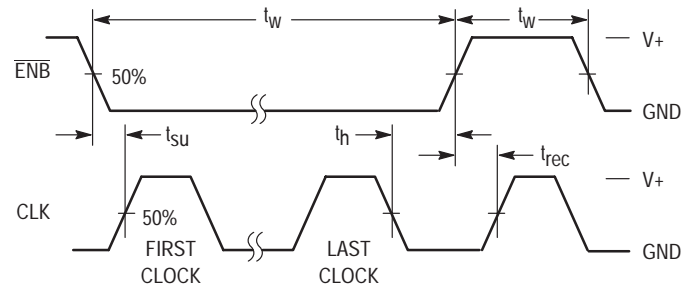


Figure 4.

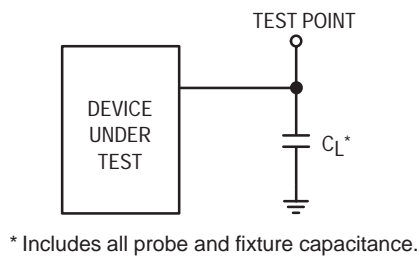


Figure 5.

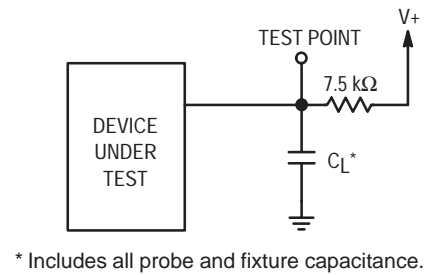
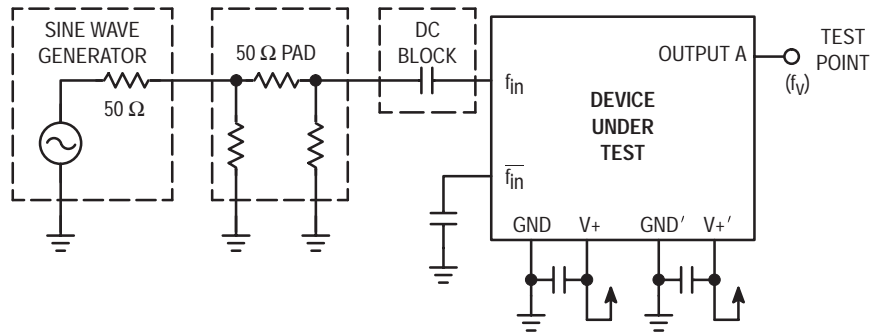


Figure 6.

LOOP SPECIFICATIONS ($V_+ = V_+' = 2.7$ to 5.5 V unless otherwise indicated, $GND = GND'$, $T_A = -40$ to 85°C)

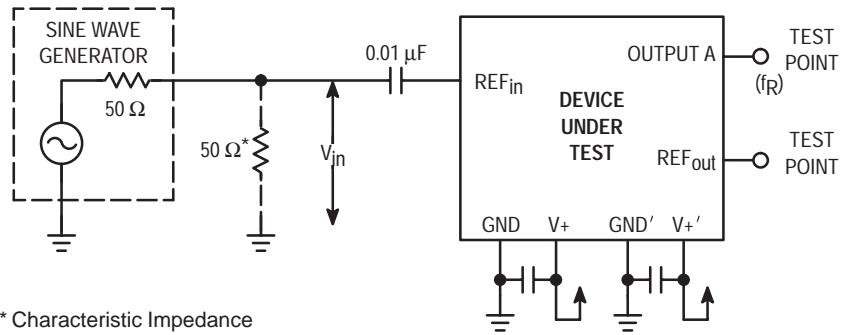
Symbol	Parameter	Test Condition	Guaranteed Operating Range		Unit
			Min	Max	
P_{in}	Input Sensitivity Range, f_{in} or f_{in}' (Figure 7)	40 MHz \leq frequency < 300 MHz 300 MHz \leq frequency < 700 MHz 700 MHz \leq frequency < 1100 MHz	-2 -5 -16	8 6 4	dBm*
ΔP_{in}	Difference Allowed Between f_{in} and f_{in}'			10	dB
—	Isolation Between f_{in} and f_{in}'		15		dB
f_{ref}	Input Frequency, REF _{in} Externally Driven in Reference Mode (Figure 8)	$V_{in} \geq 400$ mV p-p, R Counter set to divide ratio such that $f_R \leq 1$ MHz, REF Counter set to divide ratio such that REF _{out} ≤ 5 MHz	4	27	MHz
f_{XTAL}	Crystal Frequency, Crystal Mode (Figure 9)	$C_1 \leq 30$ pF, $C_2 \leq 30$ pF, Includes Stray Capacitance; R Counter and REF Counter same as above $V_+ = 2.7$ V $V_+ = 3.5$ V $V_+ = 4.5$ V $V_+ = 5.5$ V	2 2 2 2	10 13 15 15	MHz
f_{out}	Output Frequency, REF _{out} (Figures 10 and 12)	$C_L = 25$ pF	dc	5	MHz
f	Operating Frequency of the Phase Detectors		dc	1	MHz
t_w	Output Pulse Width, ϕ_R , ϕ_V , ϕ_R' , ϕ_V' (Figures 11 and 12)	f_R in Phase with f_V , $C_L = 25$ pF	16	125	ns
C_{in}	Input Capacitance, REF _{in}		—	5	pF

* Power level at the input to the dc block.



NOTE: Alternately, the 50 Ω pad may be a T network.

Figure 7. Test Circuit



* Characteristic Impedance

Figure 8. Test Circuit — Reference Mode

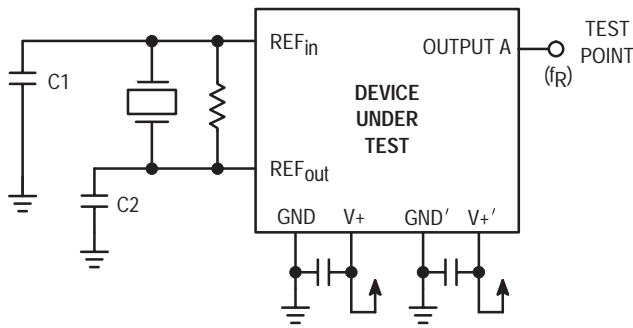


Figure 9. Test Circuit — Crystal Mode

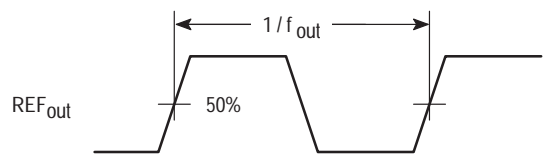


Figure 10. Switching Waveform

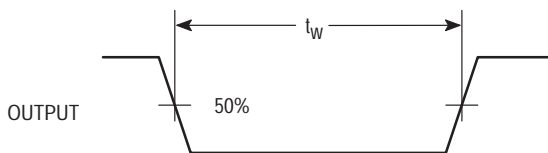
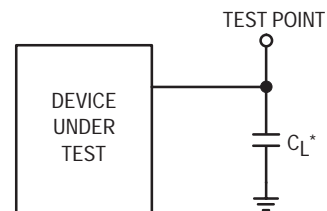
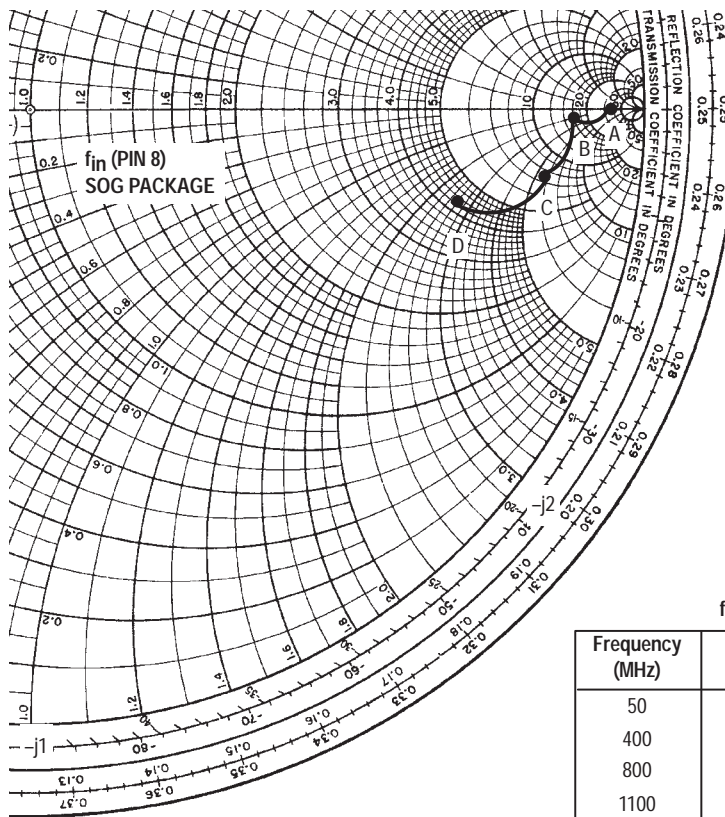


Figure 11. Switching Waveform



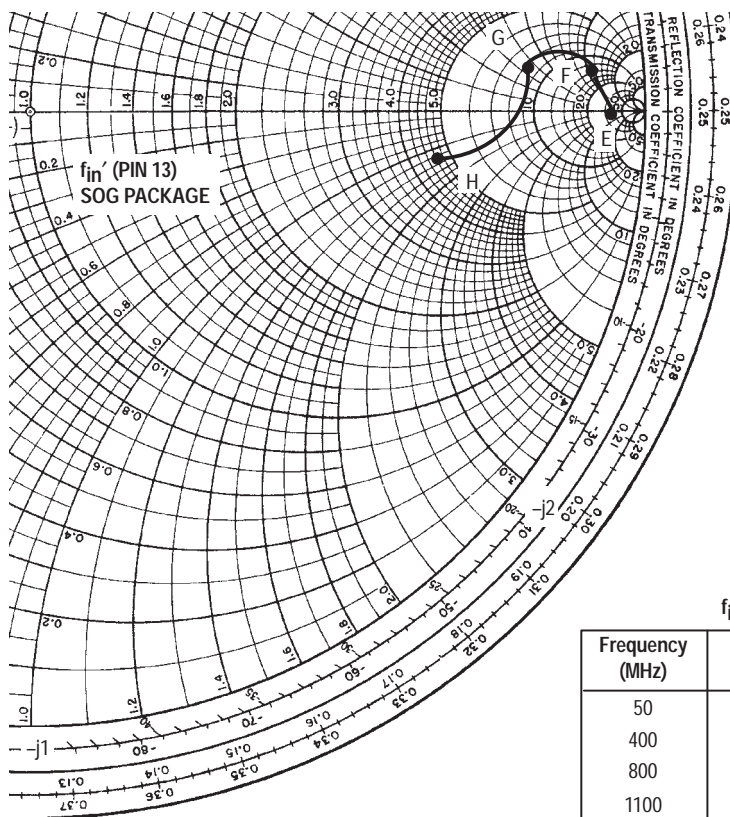
* Includes all probe and fixture capacitance.

Figure 12. Test Circuit



f_{in} (PIN 8) – SOG PACKAGE

Frequency (MHz)	Point	Impedance (Ω)	
		3 V Supply	5 V Supply
50	A	1900 - j 157	1970 - j 102
400	B	1440 - j 228	1510 + j 19
800	C	552 - j 380	671 - j 334
1100	D	196 - j 141	223 - j 147



f_{in}' (PIN 13) – SOG PACKAGE

Frequency (MHz)	Point	Impedance (Ω)	
		3 V Supply	5 V Supply
50	E	1900 + j 149	1930 + j 214
400	F	878 + j 703	746 + j 741
800	G	705 + j 208	626 + j 327
1100	H	215 - j 69.3	243 - j 61.3

Figure 13. Nominal Input Impedance of f_{in} and f_{in}' — Series Format ($R + jX$)
(50 – 1100 MHz)

PIN DESCRIPTIONS

DIGITAL INTERFACE PINS

D_{in}

Serial Data Input (Pin 20)

The bit stream begins with the MSB and is shifted in on the low-to-high transition of CLK. The bit pattern is 1 byte (8 bits) long to access the C or configuration registers, 2 bytes (16 bits) to access the first buffer of the R registers, or 3 bytes (24 bits) to access the A registers (see Table 1). The values in the registers do not change during shifting because the transfer of data to the registers is controlled by $\overline{\text{ENB}}$.

NOTE

The value programmed for the N counter must be greater than or equal to the value of the A counter.

The 13 LSBs of the R registers are double-buffered. As indicated above, data is latched into the first buffer on a 16-bit transfer. (The 3 MSBs are not double-buffered and have an immediate effect after a 16-bit transfer.) The two second buffers of the R register contain the two 13-bit divide ratios for the R counters. These second buffers are loaded with the contents of the first buffer as follows. Whenever the A register is loaded, the Rs (second) buffer is loaded from the R (first) buffer. Similarly, whenever the A' register is loaded, the Rs' (second) buffer is updated from the R (first) buffer. This allows presenting new values to the R, A, and N counters simultaneously. Note that two different R counter divide ratios may be established: one for the main PLL and another for PLL'.

The bit stream does not need address bits due to the innovative BitGrabber Plus registers. A steering bit is used to direct data to either the main PLL or PLL' section of the chip. Data is retained in the registers over a supply range of 2.7 to 5.5 V. The formats are shown in Figures 14, 15, and 16.

D_{in} typically switches near 50% of V₊ to maximize noise immunity. This input can be directly interfaced to CMOS devices with outputs guaranteed to switch near rail-to-rail. When interfacing to NMOS or TTL devices, either a level shifter (MC74HC14A, MC14504B) or pull-up resistor of 1 kΩ to 10 kΩ must be used. Parameters to consider when sizing the resistor are worst-case I_{OL} of the driving device, maximum tolerable power consumption, and maximum data rate.

Table 1. Register Access

(MSBs are shifted in first; C0, R0, and A0 are the LSBs)

Number of Clocks	Accessed Register	Bit Nomenclature
8	C Registers	C7, C6, C5, . . . , C0
16	R Register, First Buffer	R15, R14, R13, . . . , R0
24	A Registers	A23, A22, A21, . . . , A0
Other Values ≤ 32 Values > 32	Not Allowed See Figures 24 to 27	

CLK

Serial Data Clock Input (Pin 19)

Low-to-high transitions on CLK shift bits available at the D_{in} pin, while high-to-low transitions shift bits from Output A (when configured as Data Out, see Pin 10). The 24–1/2 stage shift register is static, allowing clock rates down to dc in a continuous or intermittent mode.

Eight clock cycles are required to access the C registers. Sixteen clock cycles are needed for the first buffer of the R register. Twenty-four cycles are used to access the A registers. See Table 1 and Figures 14, 15, and 16. The number of clocks required for cascaded devices is shown in Figures 25 through 27.

CLK typically switches near 50% of V₊ and has a Schmitt-triggered input buffer. Slow CLK rise and fall times are allowed. See the last paragraph of D_{in} for more information.

NOTE

To guarantee proper operation of the power-on reset (POR) circuit, the CLK pin must be held at GND (with $\overline{\text{ENB}}$ being a don't care) or $\overline{\text{ENB}}$ must be held at the potential of the V₊ pin (with CLK being a don't care) during power-up. Floating, toggling, or having these pins in the wrong state during power-up does not harm the chip, but causes two potentially undesirable effects. First, the outputs of the device power up in an unknown state. Second, if two devices are cascaded, the A Registers must be written twice after power up. After these two accesses, the two cascaded chips perform normally.

$\overline{\text{ENB}}$

Active-Low Enable Input (Pin 11)

This pin is used to activate the serial interface to allow the transfer of data to/from the device. When $\overline{\text{ENB}}$ is in an inactive high state, shifting is inhibited and the port is held in the initialized state. To transfer data to the device, $\overline{\text{ENB}}$ (which must start inactive high) is taken low, a serial transfer is made via D_{in} and CLK, and $\overline{\text{ENB}}$ is taken back high. The low-to-high transition on $\overline{\text{ENB}}$ transfers data to the C or A registers and first buffer of the R register, depending on the data stream length per Table 1.

NOTE

Transitions on $\overline{\text{ENB}}$ must not be attempted while CLK is high. This puts the device out of synchronization with the microcontroller. Resynchronization occurs whenever $\overline{\text{ENB}}$ is high and CLK is low.

This input is Schmitt-triggered and switches near 50% of V₊, thereby minimizing the chance of loading erroneous data into the registers. See the last paragraph of D_{in} for more information.

For POR information, see the note for the CLK pin.

OUTPUT A Configurable Digital Output (Pin 10)

Output A is selectable as f_R , f_V , $f_{R'}$, $f_{V'}$, Data Out, or Port. Bits A21 and A22 and the steering bit (A23) control the selection; see Figure 15. When selected as Port, the pin becomes an open-drain N-channel MOSFET output. As such, a pullup device is needed for pin 10. With all other selections, the pin is a totem-pole (push-pull) output.

If A22 = A21 = high, Output A is configured as f_R when the steering bit is low and $f_{R'}$ when the bit is high. These signals are the buffered outputs of the 13-stage R counters. The signals appear as normally low and pulse high. The signals can be used to verify the divide ratios of the R counters. These ratios extend from 10 to 8191 and are determined by the binary value loaded into bits R0 – R12 in the R register. Also, direct access to the phase detectors via the REF_{IN} pin is allowed by choosing a divide value of one. See Figure 16. The maximum frequency at which the phase detectors operate is 1 MHz. Therefore, the frequency of f_R and $f_{R'}$ should not exceed 1 MHz.

If A22 = high and A21 = low, Output A is configured as f_V when the steering bit is low and $f_{V'}$ when the bit is high. These signals are the buffered outputs of the 12-stage N counters. The signals appear as normally low and pulse high. The signals can be used to verify the operation of the prescalers, A counters, and N counters. The divide ratio between the f_{IN} or $f_{IN'}$ input and the f_V or $f_{V'}$ signal is $N \times P + A$. N is the divide ratio of the N counter, P is 32 with a 32/33 prescale ratio or 64 with a 64/65 prescale ratio, and A is the divide ratio of the A counter. These ratios are determined by bits loaded into the A registers. See Figure 15. The maximum frequency at which the phase detectors operate is 1 MHz. Therefore, the frequency of f_V and $f_{V'}$ should not exceed 1 MHz.

If A22 = low and A21 = high, Output A is configured as Data Out. This signal is the serial output of the 24-1/2 stage shift register. The bit stream is shifted out on the high-to-low transition of the CLK input. Upon power up, Output A is automatically configured as Data Out to facilitate cascading devices.

If A22 = A21 = low, Output A is configured as Port. This signal is a general-purpose digital output which may be used as an MCU port expander. This signal is low when the Port bit (C1) of the C register is low, and high impedance when the Port bit is high. See Figure 14.

REFERENCE PINS

REF_{IN} and REF_{OUT} Reference Oscillator Input and Output (Pins 1 and 2)

Configurable Pins for a Crystal or an External Reference. This pair of pins can be configured in one of two modes: the crystal mode or the reference mode. Bits R13, R14, and R15 in the R register control the modes as shown in Figure 16.

In the crystal mode, these pins form a reference oscillator when connected to terminals of an external parallel-resonant crystal. Frequency-setting capacitors of appropriate

values, as recommended by the crystal supplier, are connected from each of the two pins to ground (up to a maximum of 30 pF each, including stray capacitance). An external resistor of 1 M Ω to 15 M Ω is connected directly across the pins to ensure linear operation of the amplifier. The required connections for the crystal are shown in Figure 9. To turn on the oscillator, bits R15, R14, and R13 must have an octal value of one (001 in binary). This is the active-crystal mode shown in Figure 16. In this mode, the crystal oscillator runs and the R Counter divides the crystal frequency, unless the part is in standby. If the part is placed in standby via the C or C' register, the oscillator runs, but the R or R' counter is stopped, respectively. However, if bits R15 to R13 have a value of 0, the oscillator is stopped, which saves additional power. This is the shut-down crystal mode shown in Figure 16, and can be engaged whether in standby or not.

In the reference mode, REF_{IN} (pin 1) accepts a signal from an external reference oscillator, such as a TCXO. A signal swinging from at least the V_{IL} to V_{IH} levels listed in the **Electrical Characteristics** table may be directly coupled to the pin. If the signal is less than this level, ac coupling must be used as shown in Figure 8. The ac-coupled signal must be at least 400 mV p-p. Due to an on-board resistor which is engaged in the reference modes, an external biasing resistor tied between REF_{IN} and REF_{OUT} is not required.

With the reference mode, the REF_{OUT} pin is configured as the output of a divider. As an example, if bits R15, R14, and R13 have an octal value of seven, the frequency at REF_{OUT} is the REF_{IN} frequency divided by 16. In addition, Figure 16 shows how to obtain ratios of eight, four, and two. A ratio of one-to-one can be obtained with an octal value of three. Upon power up, a ratio of eight is automatically initialized. The maximum frequency capability of the REF_{OUT} pin is 5 MHz for large output swings (V_{OH} to V_{OL}) and 25 pF loads. Therefore, for REF_{IN} frequencies above 5 MHz, the one-to-one ratio may not be used for these large signal swing and large C_L requirements. Likewise, for REF_{IN} frequencies above 10 MHz, the ratio must be more than two.

If REF_{OUT} is unused, an octal value of two should be used for R15, R14, and R13 and the REF_{OUT} pin should be floated. A value of two allows REF_{IN} to be functional while disabling REF_{OUT} , which minimizes dynamic power consumption and electromagnetic interference (EMI).

LOOP PINS

f_{IN} , $\overline{f_{IN}}$ and $f_{IN'}$, $\overline{f_{IN'}}$ Frequency Inputs (Pins 8, 7 and 13, 14)

These pins feed the onboard RF amplifiers which drive the prescalers. These inputs may be fed differentially. However, they usually are used in single-ended configurations (shown in Figure 7). Note that f_{IN} is driven while $\overline{f_{IN}}$ must be tied to ac ground (via capacitor). The signal sources driving these pins originate from external VCOs.

Motorola does not recommend driving $\overline{f_{IN}}$ while terminating f_{IN} because this configuration is not tested for sensitivity. The sensitivity is dependent on the frequency as shown in the **Loop Specifications** table.

**PD_{out}/φ_R, PD_{out}'/φ_R'
Single-Ended Phase/Frequency Detector Outputs
(Pins 4 and 17)**

When the C2 bits in the C or C' registers are low, these pins are independently configured as single-ended outputs PD_{out} or PD_{out}', respectively. As such, each pin is a three-state current-source/sink output for use as a loop error signal when combined with an external low-pass filter. The phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detector is described below and is shown in Figure 17.

POL bit (C0) in the C register = low (see Figure 14)

Frequency of f_V > f_R or Phase of f_V Leading f_R: current-sinking pulses from a floating state

Frequency of f_V < f_R or Phase of f_V Lagging f_R: current-sourcing pulses from a floating state

Frequency and Phase of f_V = f_R: essentially a floating state; voltage at pin determined by loop filter

POL bit (C0) = high

Frequency of f_V > f_R or Phase of f_V Leading f_R: current-sourcing pulses from a floating state

Frequency of f_V < f_R or Phase of f_V Lagging f_R: current-sinking pulses from a floating state

Frequency and Phase of f_V = f_R: essentially a floating state; voltage at pin determined by loop filter

These outputs can be enabled, disabled, and inverted via the C and C' registers. If desired, these pins can be forced to the floating state by utilization of the standby feature in the C or C' registers (bit C6). This is a patented feature.

The phase detector gain is controllable by bits C4 and C5: gain (in amps per radian) = PD_{out} current in amps divided by 2π.

**PD_{out}/φ_R, Rx/φ_V and PD_{out}'/φ_R', Rx'/φ_V'
Double-Ended Phase/Frequency Detector Outputs
(Pins 4, 5 and 17, 16)**

When the C2 bits in the C or C' registers are high, these two pairs of pins are independently configured as double-ended outputs φ_R, φ_V or φ_R', φ_V', respectively. As such, these outputs can be combined externally to generate a loop error signal. Through use of a Motorola patented technique, the detector's dead zone has been eliminated. Therefore, the phase/frequency detector is characterized by a linear transfer function. The operation of the phase/frequency detectors are described below and are shown in Figure 17.

POL bit (C0) in the C register = low (see Figure 14)

Frequency of f_V > f_R or Phase of f_V Leading f_R: φ_V = negative pulses, φ_R = essentially high

Frequency of f_V < f_R or Phase of f_V Lagging f_R: φ_V = essentially high, φ_R = negative pulses

Frequency and Phase of f_V = f_R: φ_V and φ_R remain essentially high, except for a small minimum time period when both pulse low in phase

POL bit (C0) = high

Frequency of f_V > f_R or Phase of f_V Leading f_R: φ_R = negative pulses, φ_V = essentially high

Frequency of f_V < f_R or Phase of f_V Lagging f_R: φ_R = essentially high, φ_V = negative pulses

Frequency and Phase of f_V = f_R: φ_V and φ_R remain essentially high, except for a small minimum time period when both pulse low in phase

These outputs can be enabled, disabled, or interchanged via C register bits C6 or C0. This is a patented feature. Note that when disabled in standby, these outputs are forced to their rest condition (high state). See Figure 14.

The φ_R and φ_V output signals swing from approximately GND to V+.

**LD and LD'
Lock Detector Outputs (Pins 3 and 18)**

Each output is essentially at a high-impedance state with very narrow low-going pulses of a few nanoseconds when the respective loop is locked (f_R and f_V of the same phase and frequency). The output pulses low when f_V and f_R are out of phase or different frequencies. LD is the logical ANDing of φ_R and φ_V, while LD' is the logical ANDing of φ_R' and φ_V'. See Figure 17.

Upon power up, on-chip initialization circuitry forces LD and LD' to the high-impedance state. These pins are low during standby. If unused, LD should be tied to GND and LD' should be tied to GND'.

These outputs have open-drain N-channel MOSFET drivers. This facilitates a wired-OR function. See Figure 21.

**Rx/φ_V and Rx'/φ_V'
External Current Setting Resistors (Pins 5 and 16)**

When the C2 bits in the C or C' registers are low, these two pins are independently configured as current setting pins Rx or Rx', respectively. As such, resistors tied between each of these pins and GND and GND', in conjunction with bits C4 and C5 in the C and C' registers, determine the amount of current that the PD_{out} pins sink and source. When bits C4 and C5 are both set high, the maximum current is obtained; see Table 2 for other values of current.

Table 2. PD_{out} or PD_{out}' Current

C5	C4	Current
0	0	5%
0	1	50%
1	0	80%
1	1	100%

The formula for determining the value of Rx or Rx' is as follows.

$$R_x = \frac{V1 - V2}{I}$$

where Rx is the value of external resistor in ohms, V1 is the supply voltage, V2 is 1.5 V for a reference current through Rx of 100 μA or 1.745 V for a reference current of 200 μA, and I is the reference current flowing through Rx or Rx'.

The reference current flowing through Rx or Rx' is multiplied by a factor of approximately 10 (in the 100% current mode) and delivered by the PD_{out} or PD_{out}' pin, respectively. To achieve a maximum phase detector output current of 1 mA, the resistor should be about 15 kΩ when a 3 V supply is employed. See Table 3.

Table 3. Rx Values

Supply Voltage	Rx	PD _{out} or PD _{out} ' Current in 100% Mode
3 V	15 kΩ	1 mA
5 V	16 kΩ	2 mA

Do not use a decoupling capacitor on the Rx or Rx' pin. Use of a capacitor causes undesirable current spikes to appear on the phase detector output when invoking the standby mode.

POWER SUPPLY PINS

V+ and V+'

Positive Supply Potentials (Pins 9 and 12)

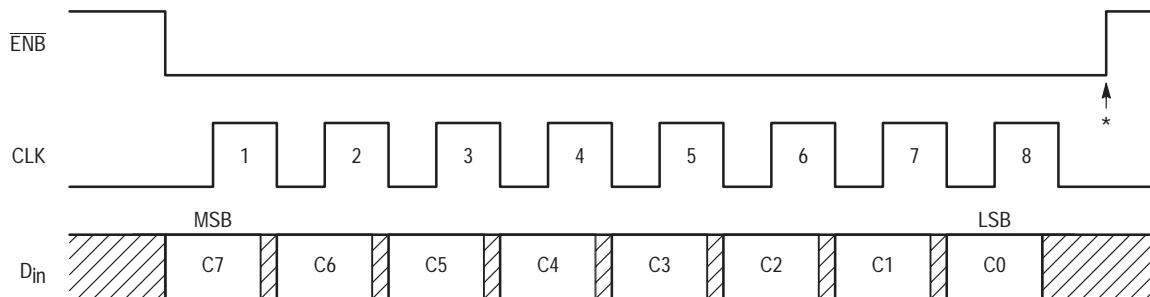
V+ supplies power to the main PLL, reference circuit, and a portion of the serial port. V+' supplies power to PLL' and a portion of the serial port. Both V+ and V+' must be at the same voltage level and may range from 2.7 V to 5.5 V with respect to the GND and GND' pins.

For optimum performance, V+ should be bypassed to GND and V+' bypassed to GND' using separate low-inductance capacitors mounted very close to the MC145220. Lead lengths and printed circuit board traces to the capacitors should be minimized. (The very fast switching speed of the device can cause excessive current spikes on the power leads if they are improperly bypassed.)

GND and GND'

Grounds (Pins 6 and 15)

The GND pin is the ground for the main PLL and GND' is the ground for PLL'.

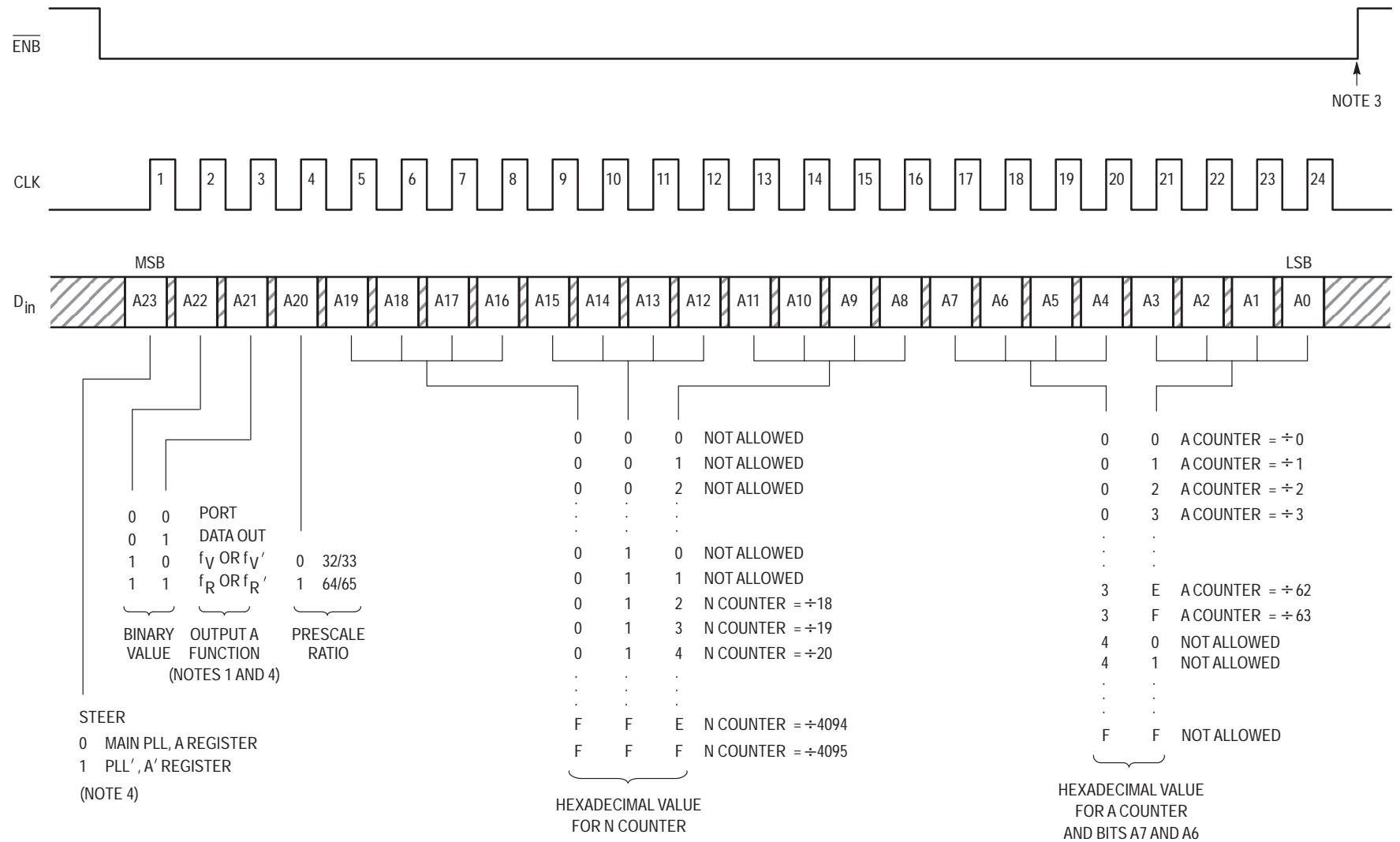


* At this point, the new byte is transferred to the C or C' register and stored. No other registers are affected.

- C7 – Steer: Used to direct the data to either the C or C' register. A low level directs data to the C register; a high level is for the C' register.
- C6 – Standby: When set high, places both the main PLL and PLL' (when C6 is set in the C register) or PLL' only (when C6 is set in the C' register) in the standby mode for reduced power consumption. The associated PD_{OUT} is forced to the floating state, the associated counters (A, N, and R) are inhibited from counting, the associated Rx current is shut off, and the associated prescaler stops counting and is placed in a low current mode. The associated double-ended phase/frequency detector outputs are forced to a high level. In standby, the associated LD output is placed in the low-state, thus indicating “not locked” (open loop). During standby, data is retained in all registers and any register may be accessed.
- In standby, the condition of the REF/OSC circuitry is determined by bits R13, R14, and R15 in the R register per Figure 16. However, if REF_{OUT} = *static low* is selected, the internal feedback resistor is disconnected and the REF_{IN} is inhibited when both PLL and PLL' are placed in standby via the C register. Thus, the REF_{IN} only presents a capacitive load. **Note:** PLL/PLL' standby does not affect the other modes of the REF/OSC circuitry as determined by bits R13, R14, and R15 in the R register. The PLL' standby mode (controlled from the C' register) has no effect on the REF/OSC circuit.
- When C6 is reset low, the associated PLL (or PLLs) is (are) taken out of standby in two steps. First, the REF_{IN} (only in 1 mode, PLL/PLL' in standby) resistor is reconnected, REF_{IN} (only 1 mode) is gated on, all counters are enabled, and the Rx current is enabled. Any f_R and f_V signals are inhibited from toggling the phase/frequency detectors and lock detectors. Second, when the appropriate f_R pulse occurs, the A and N counters are jam loaded, the prescaler is gated on, and the phase/frequency and lock detectors are initialized. Immediately after the jam load, the A, N, and R counters begin counting down together. At this point, the f_R and f_V pulses are enabled to the phase and lock detectors. (Patented feature.)
- C5, C4 – I2, I1: Independently controls the PD_{OUT} or PD_{OUT}' source/sink current per Table 2. With both bits high, the maximum current (as set by Rx or Rx') is available. POR forces C5 and C4 to high levels.
- C3 – Spare: Unused
- C2 – PDA/B: Independently selects which phase/frequency detector is to be used. When set high, the double-ended detector is selected with outputs φ_R and φ_V or φ_R' and φ_V'. When reset low, the current source/sink detector is selected with outputs PD_{OUT} or PD_{OUT}'. In the second case, the appropriate Rx or Rx' pin is tied to an external resistor. POR forces C2 low.
- C1 – Port: When the Output A pin is selected as “Port” via bits A22 and A21, C1 of the C register determines the state of Output A. When C1 is set high, Output A is forced to the high-impedance state; C1 low forces Output A low. The Port bit is not affected by the standby mode. **Note:** C1 of the C' register is not used in any mode.
- C0 – POL: Selects the output polarity of the associated phase/frequency detectors. When set high, this bit inverts the associated current source/sink output and interchanges the associated double-ended output relative to the waveforms in Figure 17. Also, see the phase detector output pin descriptions for more information. This bit is cleared low at power up.

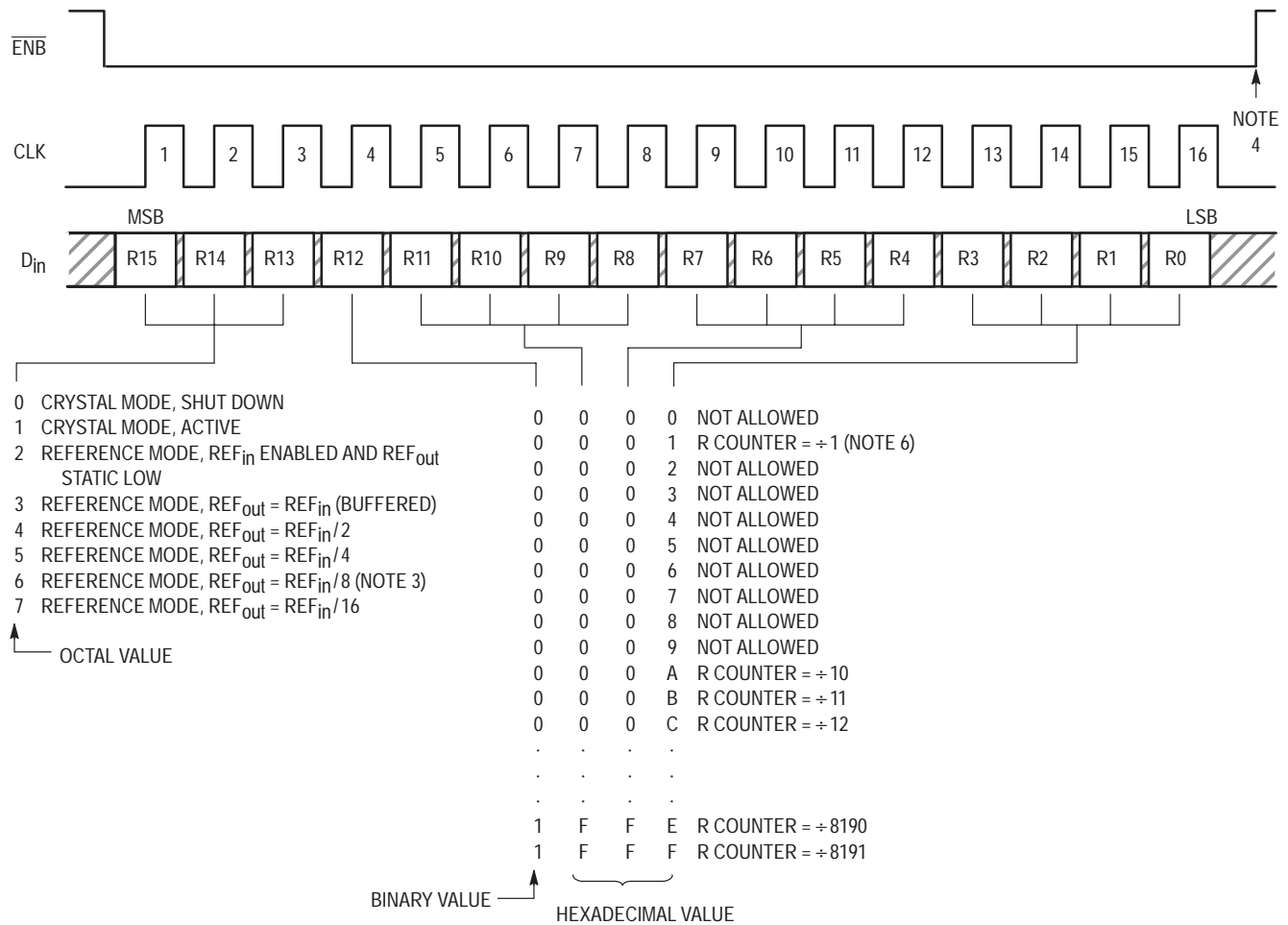
Figure 14. C and C' Register Accesses and Format (8 Clock Cycles are Used)

Figure 15. A and A' Register Accesses and Format (24 Clock Cycles are Used)



NOTES:

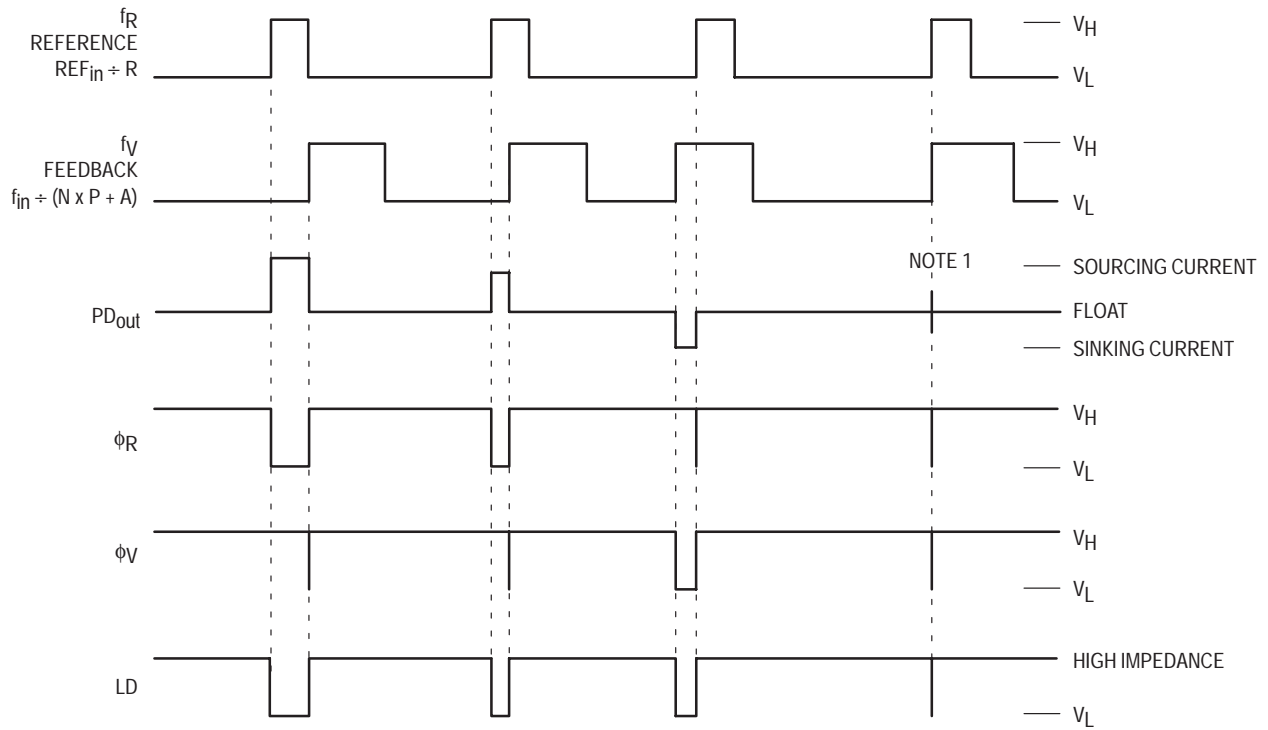
1. A power-on initialize circuit forces the Output A function to default to Data Out.
2. The values programmed for the N counter must be greater than or equal to the values programmed for the A counter. This results in a total divide value = N x P + A where N is the value programmed for the N counter, P is 32 if bit A20 is low or 64 if A20 is high, and A is the value programmed for the A counter.
3. At this point, the three new bytes are transferred to the A register if bit A23 is a "0" or A' register if A23 is a "1". In addition, the 13 LSBs in the first buffer of the R register are transferred to the R register's relative second buffer, Rs or Rs'. Thus, the R, N, and A (or R', N', and A') counters can be presented new divide ratios at the same time. The first buffer of the R register is not affected. The C or C registers are not affected.
4. A "0" for the Steering bit allows selection of f_R , f_V , Data Out, or Port by bits A21 and A22. A "1" for the Steering bit allows selection of $f_{R'}$, $f_{V'}$, Data Out, or Port.



NOTES:

1. Bits R15 – R13 control the configurable “Buffer and Control” block (see Block Diagram).
2. Bits R12 – R0 control the “13-stage R counter” blocks (see Block Diagram).
3. A power-on initialize circuit forces a default REF_{in} to REF_{out} ratio of eight.
4. At this point, bits R13, R14, and R15 are stored and sent to the “Buffer and Control” block in the Block Diagram. Bits R0 – R12 are loaded into the first buffer in the double-buffered section of the R register. Therefore, the R or R’ counter divide ratio is not altered yet and retains the previous ratio loaded. The C, C’, A, and A’ registers are not affected.
5. Bits R0 – R12 are transferred to the second buffer of the R register (Rs in the Block Diagram) on a subsequent 24-bit write to the A register. The bits are transferred to Rs’ on a subsequent 24-bit write to the A’ register. The respective R counter begins dividing by the new ratio after completing the rest of its present count cycle.
6. Allows direct access to reference input of phase/frequency detectors.

Figure 16. R Register Access and Format (16 Clock Cycles are Used)



NOTES:

1. At this point, when both f_R and f_V are in phase, the output source and sink circuits are turned on for a short interval.
2. The PD_{out} either sources or sinks current during out-of-lock conditions. When locked in phase and frequency, the output is mostly in a floating condition and the voltage at that pin is determined by the low-pass filter capacitor. PD_{out} , ϕ_R , and ϕ_V are shown with the polarity bit (POL) = low; see Figure 14 for POL.
3. V_H = High voltage level, V_L = Low voltage level.
4. The waveforms are applicable to both the main PLL and PLL'.

Figure 17. Phase/Frequency Detectors and Lock Detector Output Waveforms

DESIGN CONSIDERATIONS

CRYSTAL OSCILLATOR CONSIDERATIONS

The following options may be considered to provide a reference frequency to Motorola's CMOS frequency synthesizers.

Use of a Hybrid Crystal Oscillator

Commercially available temperature-compensated crystal oscillators (TCXOs) or crystal-controlled data clock oscillators provide very stable reference frequencies. An oscillator capable of CMOS logic levels at the output may be direct or dc coupled to REF_{in}. If the oscillator does not have CMOS logic levels on the outputs, capacitive or ac coupling to REF_{in} must be used. See Figure 8.

For additional information about TCXOs and data clock oscillators, please consult the latest version of the *eem Electronic Engineers Master Catalog*, the *Gold Book*, or similar publications.

Design an Off-Chip Reference

The user may design an off-chip crystal oscillator using discrete transistors or ICs specifically developed for crystal oscillator applications, such as the MC12061 MECL device. The reference signal from the MECL device is ac coupled to REF_{in}. (See Figure 8.) For large amplitude signals (standard CMOS logic levels), dc coupling may be used.

Use of the On-Chip Oscillator Circuitry

The on-chip amplifier (a digital inverter) along with an appropriate crystal may be used to provide a reference source frequency. A fundamental mode crystal, parallel resonant at the desired operating frequency, should be connected as shown in Figure 18.

The crystal should be specified for a loading capacitance, C_L, which does not exceed approximately 20 pF when used near the highest operating frequency of the MC145220. Assuming R1 = 0 Ω, the shunt load capacitance, C_L, presented across the crystal can be estimated to be:

$$C_L = \frac{C_{in}C_{out}}{C_{in} + C_{out}} + C_a + C_{stray} + \frac{C1 \cdot C2}{C1 + C2}$$

where

$$C_{in} = 5 \text{ pF (see Figure 19)}$$

$$C_{out} = 6 \text{ pF (see Figure 19)}$$

$$C_a = 1 \text{ pF (see Figure 19)}$$

C1 and C2 = external capacitors (see Figure 18)

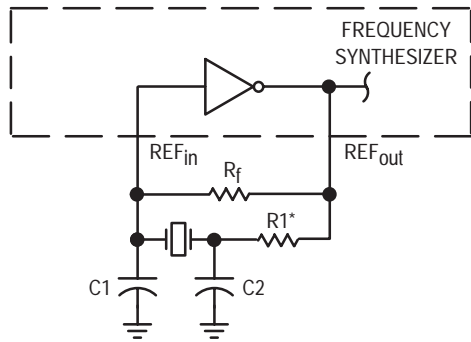
C_{stray} = the total equivalent external circuit stray capacitance appearing across the crystal terminals

The oscillator can be "trimmed" on-frequency by making either a portion or all of C1 variable. The crystal and associated components must be located as close as possible to the REF_{in} and REF_{out} pins to minimize distortion, stray capacitance, stray inductance, and startup stabilization time. Circuit stray capacitance can also be handled by adding the appropriate stray value to the values for C_{in} and C_{out}. For this approach, the term C_{stray} becomes zero in the above expression for C_L.

Power is dissipated in the effective series resistance of the crystal, R_e, in Figure 20. The maximum drive level specified by the crystal manufacturer represents the maximum stress that the crystal can withstand without damage or excessive shift in operating frequency. R1 in Figure 18 limits the drive level. The use of R1 is not necessary in most cases.

To verify that the maximum dc supply voltage does not cause the crystal to be overdriven, monitor the output frequency (f_R) at Output A as a function of supply voltage. (REF_{out} is not used because loading impacts the oscillator.) The frequency should increase very slightly as the dc supply voltage is increased. An overdriven crystal decreases in frequency or becomes unstable with an increase in supply voltage. The operating supply voltage must be reduced or R1 must be increased in value if the overdriven condition exists. Note that the oscillator start-up time is proportional to the value of R1.

Through the process of supplying crystals for use with CMOS inverters, many crystal manufacturers have developed expertise in CMOS oscillator design with crystals. Discussions with such manufacturers can prove very helpful. See Table 4.



* May be needed in certain cases. See text.

Figure 18. Pierce Crystal Oscillator Circuit

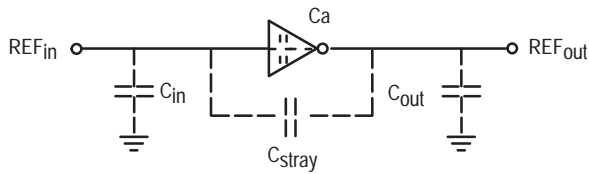
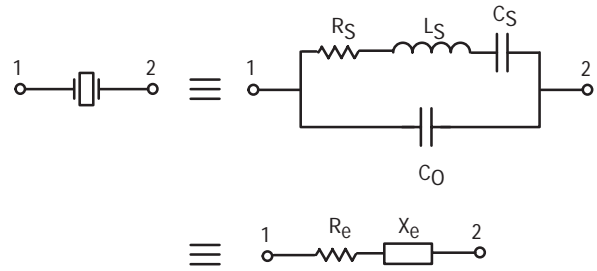


Figure 19. Parasitic Capacitances of the Amplifier and C_{stray}



NOTE: Values are supplied by crystal manufacturer (parallel resonant crystal).

Figure 20. Equivalent Crystal Networks

RECOMMENDED READING

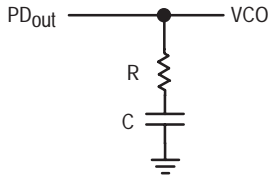
- Technical Note TN-24, Statek Corp.
- Technical Note TN-7, Statek Corp.
- E. Hafner, "The Piezoelectric Crystal Unit – Definitions and Method of Measurement", *Proc. IEEE*, Vol. 57, No. 2, Feb. 1969.
- D. Kemper, L. Rosine, "Quartz Crystals for Frequency Control", *Electro-Technology*, June 1969.
- P. J. Ottowitz, "A Guide to Crystal Selection", *Electronic Design*, May 1966.
- D. Babin, "Designing Crystal Oscillators", *Machine Design*, March 7, 1985.
- D. Babin, "Guidelines for Crystal Oscillator Design", *Machine Design*, April 25, 1985.

Table 4. Partial List of Crystal Manufacturers

United States Crystal Corp.
Crystek Crystal
Statek Corp.
Fox Electronics

PHASE-LOCKED LOOP — LOW-PASS FILTER DESIGN

(A)



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NC}}$$

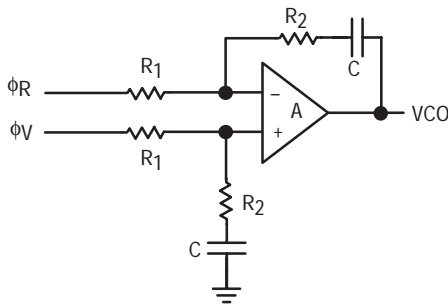
$$\zeta = \frac{R}{2} \sqrt{\frac{K_\phi K_{VCO} C}{N}} = \frac{\omega_n RC}{2}$$

$$Z(s) = \frac{1 + sRC}{sC}$$

NOTE:

For (A), using K_ϕ in amps per radian with the filter's impedance transfer function, $Z(s)$, maintains units of volts per radian for the detector/filter combination. Additional sideband filtering can be accomplished by adding a capacitor C' across R . The corner $\omega_c = 1/RC'$ should be chosen such that ω_n is not significantly affected.

(B)



$$\omega_n = \sqrt{\frac{K_\phi K_{VCO}}{NCR_1}}$$

$$\zeta = \frac{\omega_n R_2 C}{2}$$

ASSUMING GAIN A IS VERY LARGE, THEN:

$$Z(s) = \frac{R_2 s C + 1}{R_1 s C}$$

NOTE:

For (B), R_1 is frequently split into two series resistors; each resistor is equal to R_1 divided by 2. A capacitor C_C is then placed from the midpoint to ground to further filter the error pulses. The value of C_C should be such that the corner frequency of this network does not significantly affect ω_n .

DEFINITIONS:

N = Total Division Ratio in Feedback Loop

K_ϕ (Phase Detector Gain) = $I_{PDout}/2\pi$ amps per radian for PD_{out}

K_ϕ (Phase Detector Gain) = $V+/2\pi$ volts per radian for ϕ_V and ϕ_R

K_{VCO} (VCO Transfer Function) = $\frac{2\pi\Delta f_{VCO}}{\Delta V_{VCO}}$ radians per volt

For a nominal design starting point, the user might consider a damping factor $\zeta \approx 0.7$ and a natural loop frequency $\omega_n \approx (2\pi f_R/50)$ where f_R is the frequency at the phase detector input. Larger ω_n values result in faster loop lock times and, for similar sideband filtering, higher f_R -related VCO sidebands.

Either loop filter (A) or (B) is frequently followed by additional sideband filtering to further attenuate f_R -related VCO sidebands. This additional filtering may be active or passive.

RECOMMENDED READING:

Gardner, Floyd M., *Phaselock Techniques (second edition)*. New York, Wiley-Interscience, 1979.

Manassewitsch, Vadim, *Frequency Synthesizers: Theory and Design (second edition)*. New York, Wiley-Interscience, 1980.

Blanchard, Alain, *Phase-Locked Loops: Application to Coherent Receiver Design*. New York, Wiley-Interscience, 1976.

Egan, William F., *Frequency Synthesis by Phase Lock*. New York, Wiley-Interscience, 1981.

Rohde, Ulrich L., *Digital PLL Frequency Synthesizers Theory and Design*. Englewood Cliffs, NJ, Prentice-Hall, 1983.

Berlin, Howard M., *Design of Phase-Locked Loop Circuits, with Experiments*. Indianapolis, Howard W. Sams and Co., 1978.

Kinley, Harold, *The PLL Synthesizer Cookbook*. Blue Ridge Summit, PA, Tab Books, 1980.

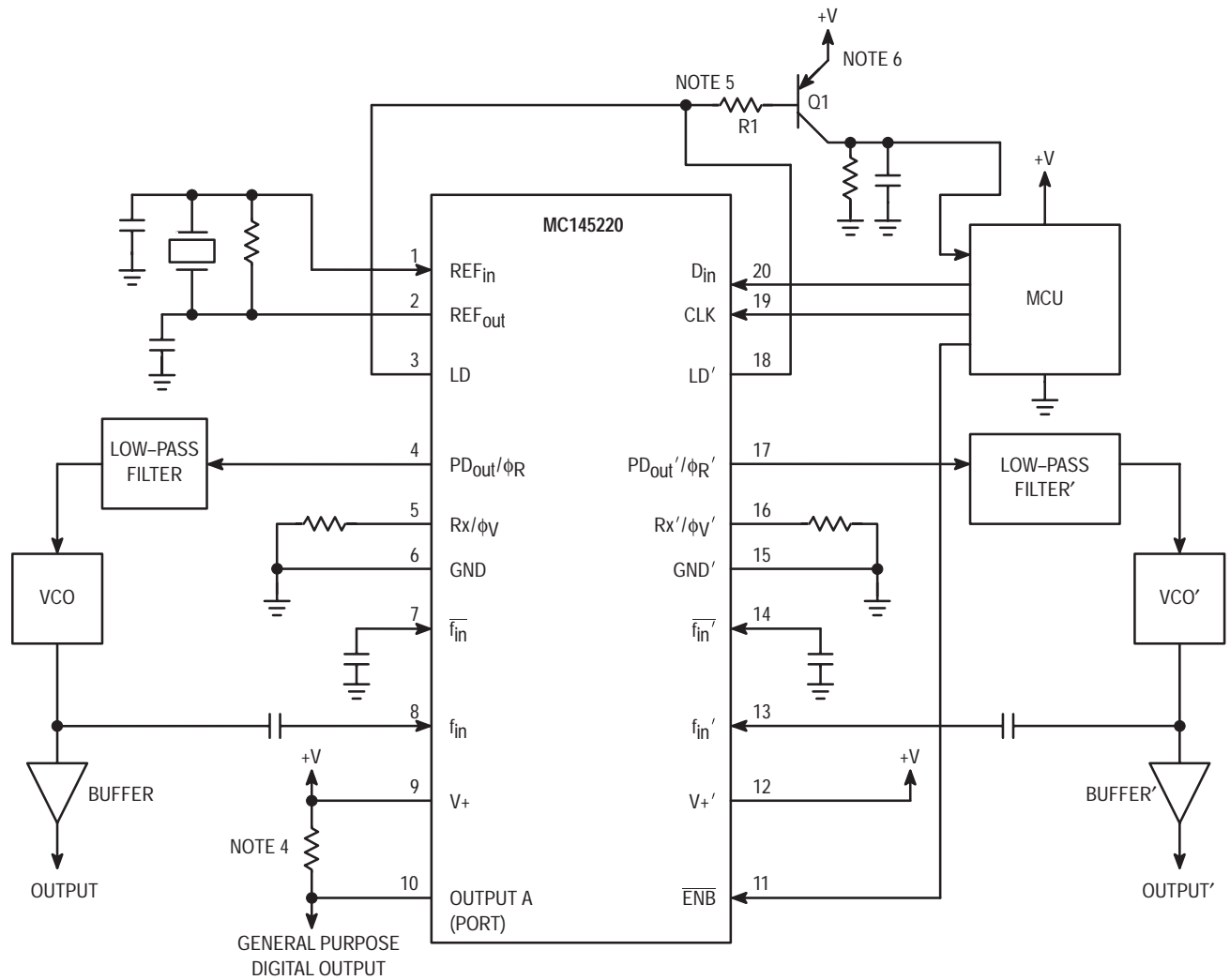
Seidman, Arthur H., *Integrated Circuits Applications Handbook*, Chapter 17, pp. 538-586. New York, John Wiley & Sons.

Fadrhons, Jan, "Design and Analyze PLLs on a Programmable Calculator," *EDN*. March 5, 1980.

AN535, Phase-Locked Loop Design Fundamentals, Motorola Semiconductor Products, Inc., 1970.

AR254, Phase-Locked Loop Design Articles, Motorola Semiconductor Products, Inc., Reprinted with permission from *Electronic Design*, 1987.

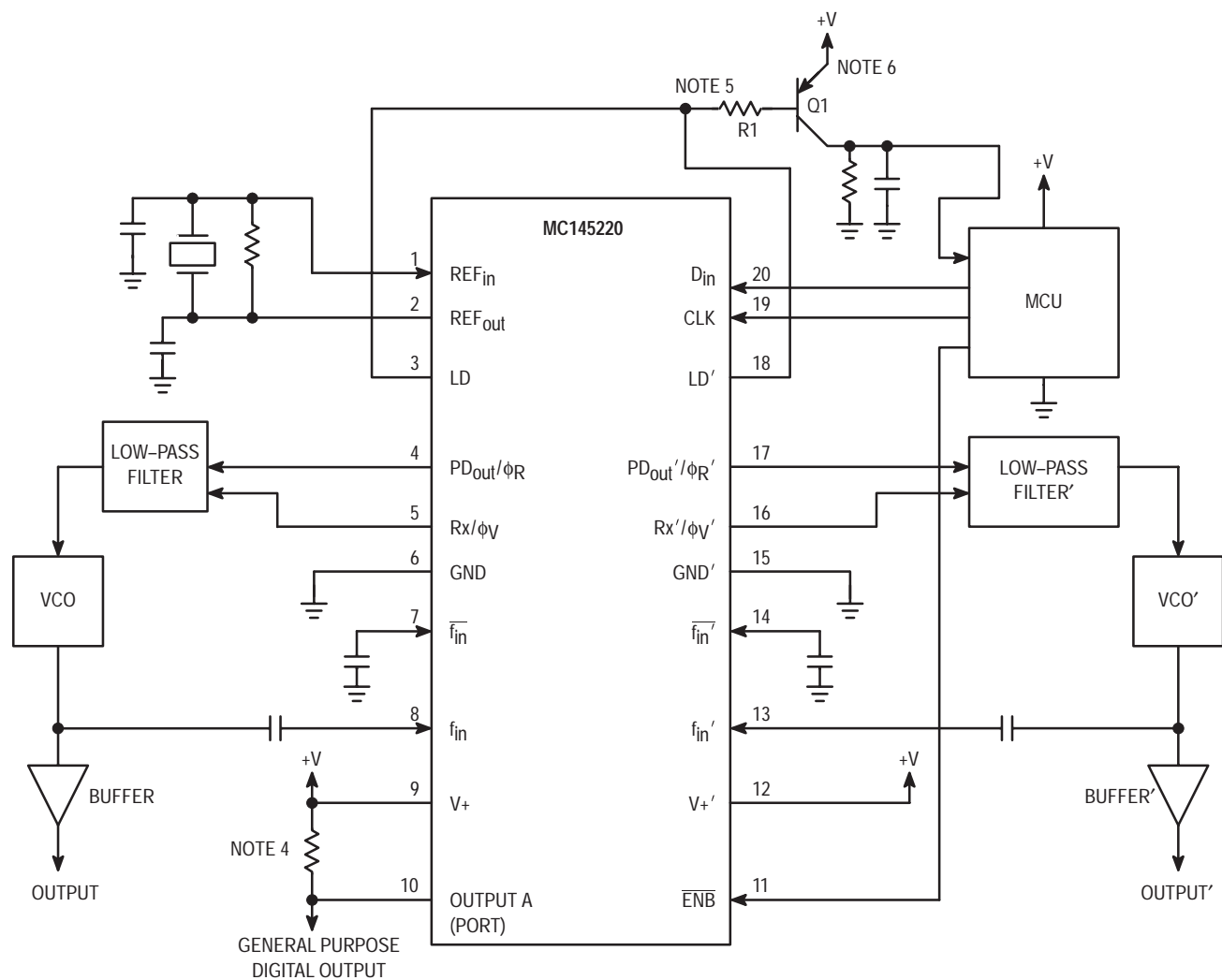
AN1253, An Improved PLL Design Method Without ω_n and ζ , Motorola Semiconductor Products, Inc., 1995.



NOTES:

1. The PD_{Out} output is fed to an external loop filter. See the Phase-Locked Loop — Low-Pass Filter Design page for additional information.
2. For optimum performance, bypass the V+ and V+' pins to GND and GND' with low-inductance capacitors.
3. The R counter is programmed for a divide value = REF_{in} / f_R. Typically, f_R is the tuning resolution required for the VCO. Also, the VCO frequency divided by f_R = N_T = N • P + A; this determines the values (N, A) that must be programmed into the N and A counters, respectively. P is the lower divide ratio of the dual-modulus prescaler (i.e., 32 or 64).
4. Pull-up voltage must be at the same potential as the V+ pin or less. Pull-up device other than a resistor may be used. (Pull-up device not required when Output A is configured as f_R, f_{R'}, f_V, f_{V'}, DATA OUT.)
5. LD and LD' are open-drain outputs. This allows the wired-OR configuration shown. Note that R1 and Q1 form the "pull-up device".
6. Use of Q1 is optional and depends on loading.

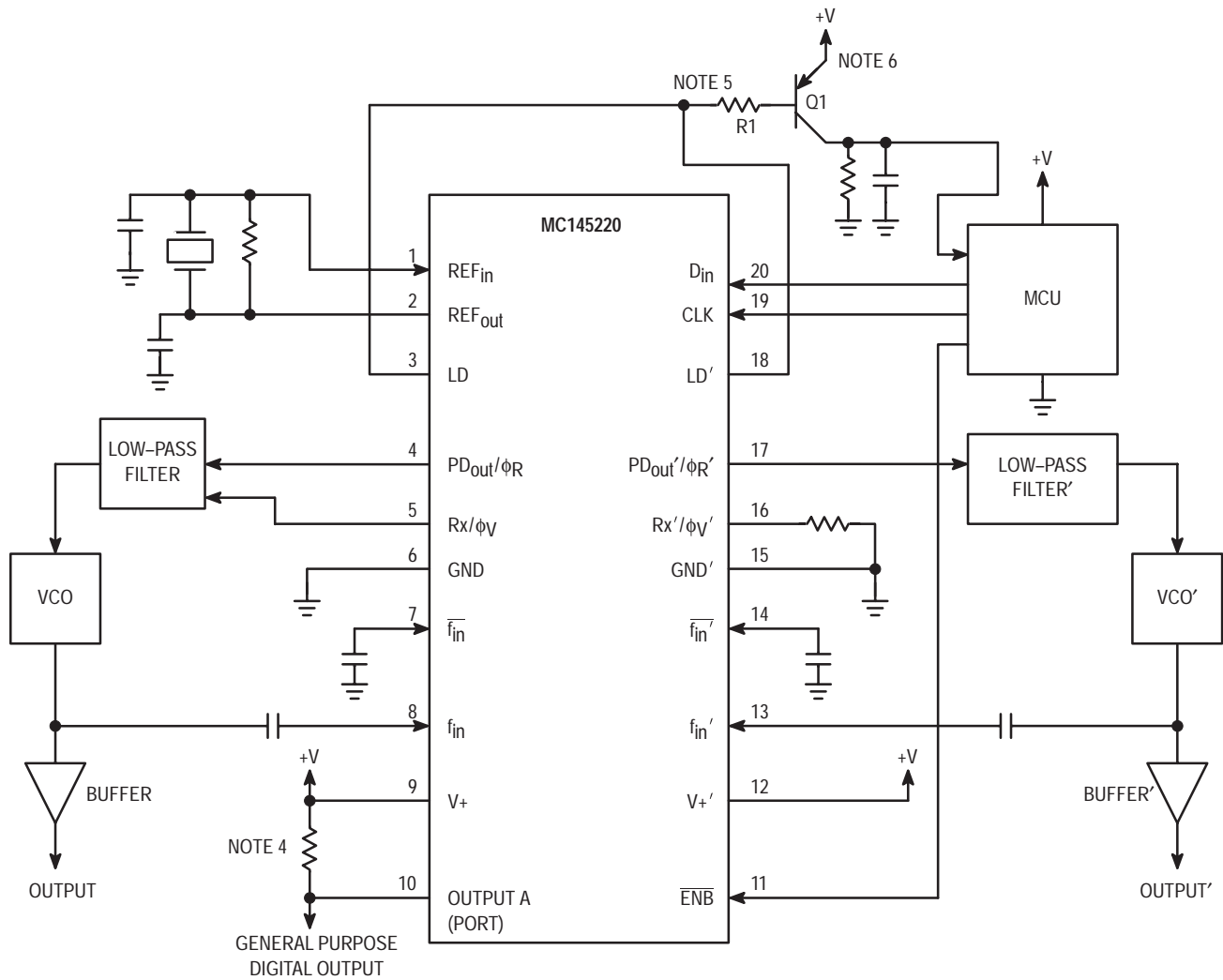
Figure 21. Application Showing Use of the Two Single-Ended Phase/Frequency Detectors



NOTES:

1. The ϕ_R and ϕ_V outputs are fed to an external combiner/loop filter. See the Phase-Locked Loop — Low-Pass Filter Design page for additional information. The ϕ_R and ϕ_V outputs swing rail-to-rail. Therefore, the user should be careful not to exceed the common mode input range of the op amp used in the combiner/loop filter.
2. For optimum performance, bypass the V_+ and V_+' pins to GND and GND' with low-inductance capacitors.
3. The R counter is programmed for a divide value = REF_{in} / f_R . Typically, f_R is the tuning resolution required for the VCO. Also, the VCO frequency divided by $f_R = N_T = N \cdot P + A$; this determines the values (N, A) that must be programmed into the N and A counters, respectively. P is the lower divide ratio of the dual-modulus prescaler (i.e., 32 or 64).
4. Pull-up voltage must be at the same potential as the V_+ pin or less. Pull-up device other than a resistor may be used. (Pull-up device not required when Output A is configured as f_R , f_R' , f_V , f_V' , DATA OUT.)
5. LD and LD' are open-drain outputs. This allows the wired-OR configuration shown. Note that R1 and Q1 form the "pull-up device".
6. Use of Q1 is optional and depends on loading.

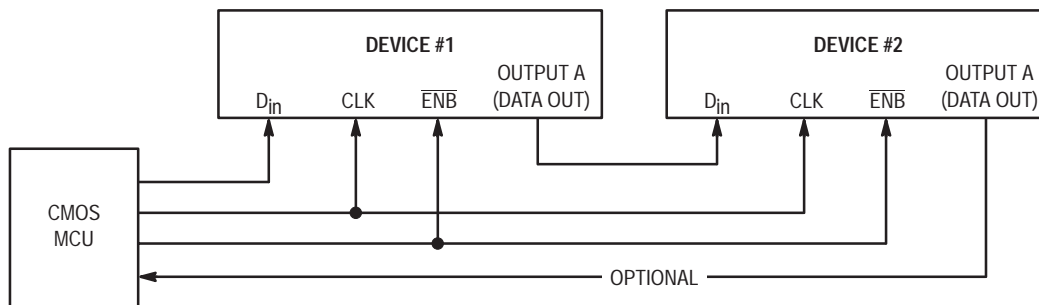
Figure 22. Application Showing Use of the Two Double-Ended Phase/Frequency Detectors



NOTES:

1. See the Phase-Locked Loop — Low-Pass Filter Design page for additional information.
2. For optimum performance, bypass the V+ and V+' pins to GND and GND' with low-inductance capacitors.
3. The R counter is programmed for a divide value = REF_{in} / f_R . Typically, f_R is the tuning resolution required for the VCO. Also, the VCO frequency divided by $f_R = N_T = N \cdot P + A$; this determines the values (N, A) that must be programmed into the N and A counters, respectively. P is the lower divide ratio of the dual-modulus prescaler (i.e., 32 or 64).
4. Pull-up voltage must be at the same potential as the V+ pin or less. Pull-up device other than a resistor may be used. (Pull-up device not required when Output A is configured as f_R , f_R' , f_V , f_V' , DATA OUT.)
5. LD and LD' are open-drain outputs. This allows the wired-OR configuration shown. Note that R1 and Q1 form the "pull-up device".
6. Use of Q1 is optional and depends on loading.

Figure 23. Application Showing Use of Both the Single- and Double-Ended Phase/Frequency Detectors



NOTE: See related Figures 25, 26, and 27.

Figure 24. Cascading Two Devices

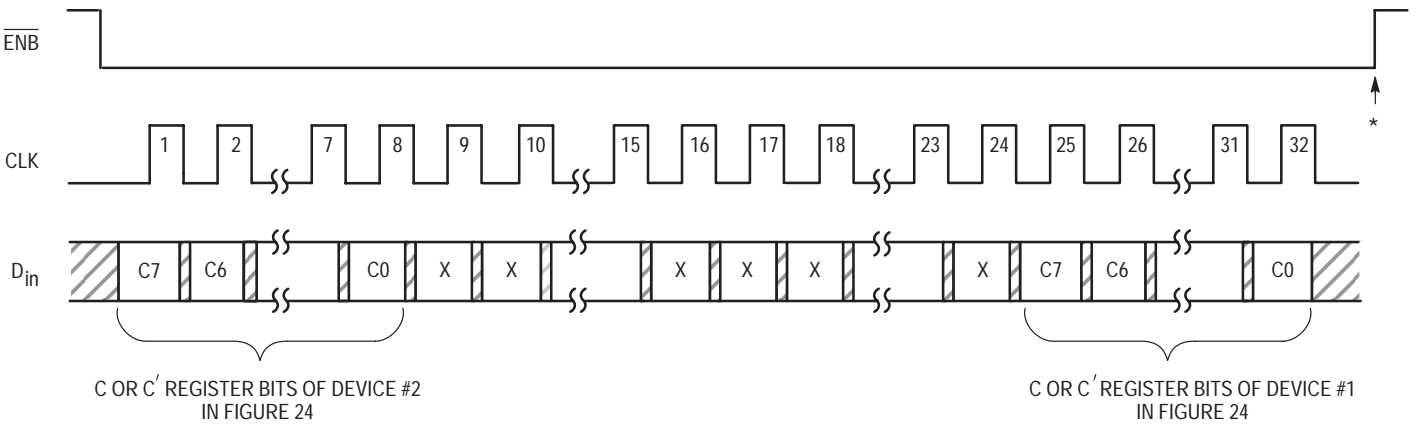
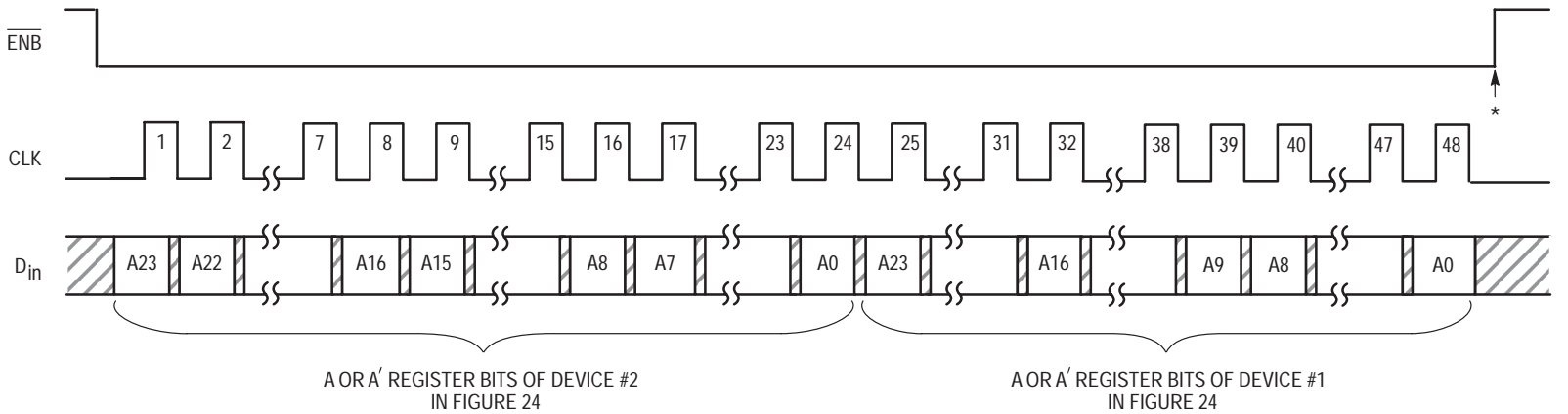


Figure 25. Accessing the C or C' Registers of Two Cascaded MC145220 Devices (32 Clock Cycles are Used)

*At this point, the new bytes are transferred to the C or C' registers of both devices and stored. No other registers are affected.

Figure 26. Accessing the A or A' Registers of Two Cascaded MC145220 Devices (48 Clock Cycles are Used)



*At this point, the new bytes are transferred to the A or A' registers of both devices and stored. Additionally, for both devices, the 13 LSBs in each of the first buffers of the R Registers are transferred to the respective R register's second buffer. Thus, the R, N, and A (R', N', and A') counters can be presented new divide ratios at the same time. The first buffer of each R register is not affected. None of the C or C' registers are affected.

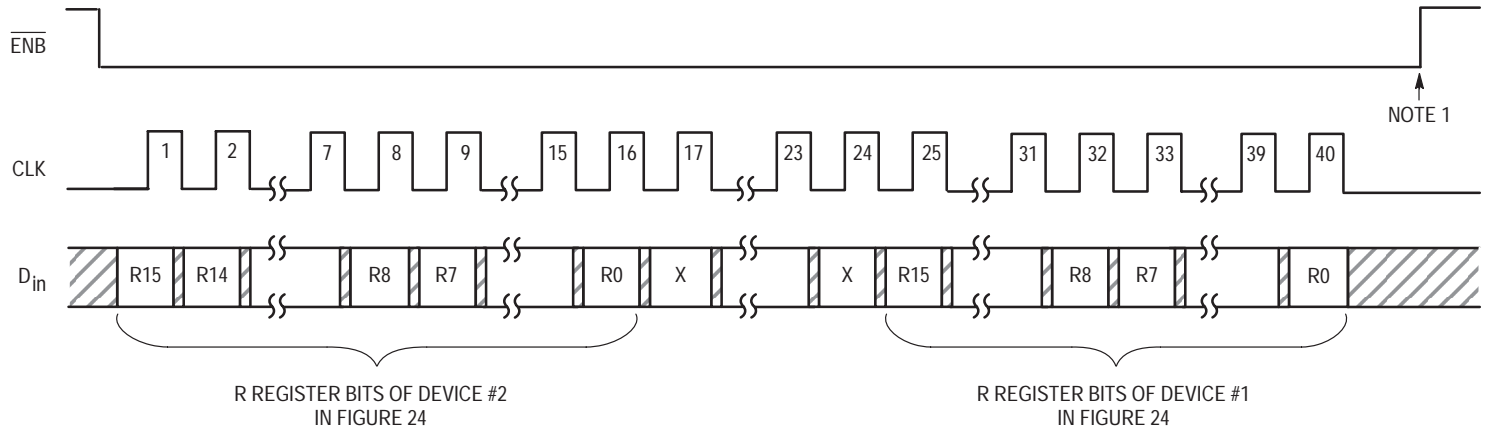


Figure 27. Accessing the R Registers of Two Cascaded MC145220 Devices (40 Clock Cycles are Used)

NOTES APPLICABLE TO EACH DEVICE:

1. At this point, bits R13, R14, and R15 are stored and sent to the Buffer and Control block in the Block Diagram. Bits R0 through R12 are loaded into the first buffer in the double-buffered section of the R register. Therefore, the R and R' counter divide ratios are not altered yet and retain the previous ratios loaded. The other registers are not affected.
2. See note of Figure 26 for the method of loading the second buffers in the R register to achieve new divide ratios.

MC145220EVK

Technical Summary
MC145220 Evaluation Board

INTRODUCTION

The MC145220EVK makes it easy to exercise features of the MC145220 and build PLLs which meet individual performance requirements. The EVK is controlled through menu driven software operating on an IBM PC or compatible. Other Motorola PLL EVKs (MC145190, MC145191, MC145192, MC145200, MC145201, MC145202) in up to three-board cascades can use the same program. Frequency defaults that apply to each are automatically selected. All board functions are controlled through the printer port of an IBM PC. Up to three different EVKs may be controlled at the same time from one printer port. The functional block diagram is given in Figure 1.

This technical summary contains the hardware description for the evaluation board and a summary of the software section. For complete information, consult the manual that is provided in the evaluation kit.

ORDERING INFORMATION

These kits may be ordered through your local Motorola Semiconductor sales office or authorized distributor. Ask your Motorola representative to order the kits from the finished goods warehouse, not the literature distribution center. Request the part number shown below.

Part Number	Description
MC145220EVK	Kit with the MC145220 installed.

This document contains information on a new product. Specifications and information herein are subject to change without notice.

SECTION 1 – HARDWARE

FEATURES

1. The EVK is a complete working synthesizer, including VCOs.
2. Board is controlled by an IBM PC-compatible computer through the printer port.
3. Up to three boards can be operated independently through one printer port.
4. A prototype area and mounting holes are provided for VCOs, mixers, and amplifiers.
5. External reference input can be used.
6. Five element loop filter is included.
7. Frequency range of operation, step size and reference frequency can be changed in the control program.
8. Lock Detect, Out A, and Out B on any single board are accessible through the printer port.

CONTENTS OF EVALUATION KIT

1. Assembled evaluation board.
2. Nine-foot flat cable with four DB-25 male connectors.
3. MC145220EVK manual.
4. 3.5" PC-compatible disk containing compiled program.
5. PLL device data sheets.

GETTING STARTED

To perform basic functions, do the following:

1. Plug in 12 volts at J8, observing the polarity marked on the board.
2. Short circuit section 1 of the DIP switch (S1) and open circuit all other sections.
3. Connect the supplied flat cable between the computer printer port and the DB-25 connector on the board (J9).
4. Type PLL at the DOS prompt. Then press enter.
5. Type the number that corresponds with the type of board given in the on-screen menu. The MC145220 may operate in single loop or dual loop mode. Then press Q.

You should now see the main menu displayed. There should be a signal present at J5 if single loop, or J12 if dual loop. The frequency will be the current output frequency given in the main menu. If the signal is not on the correct frequency, check to see if your printer port address is \$278 (hexadecimal 278). If not, then select the P menu item and enter the correct address. After returning to the main menu, select the I menu item to send data to the board. You should now be on frequency.

MODIFICATIONS

The user may modify the hardware, such as utilizing a different VCO, by using the prototyping area of the board. After such modifications are made, the default values in the software may need to be changed. This is facilitated from the 'Select from the available options' screen.

Note that the on-board voltage regulators allow for a maximum VCO control voltage range of 0.5 – 4.5 volts.

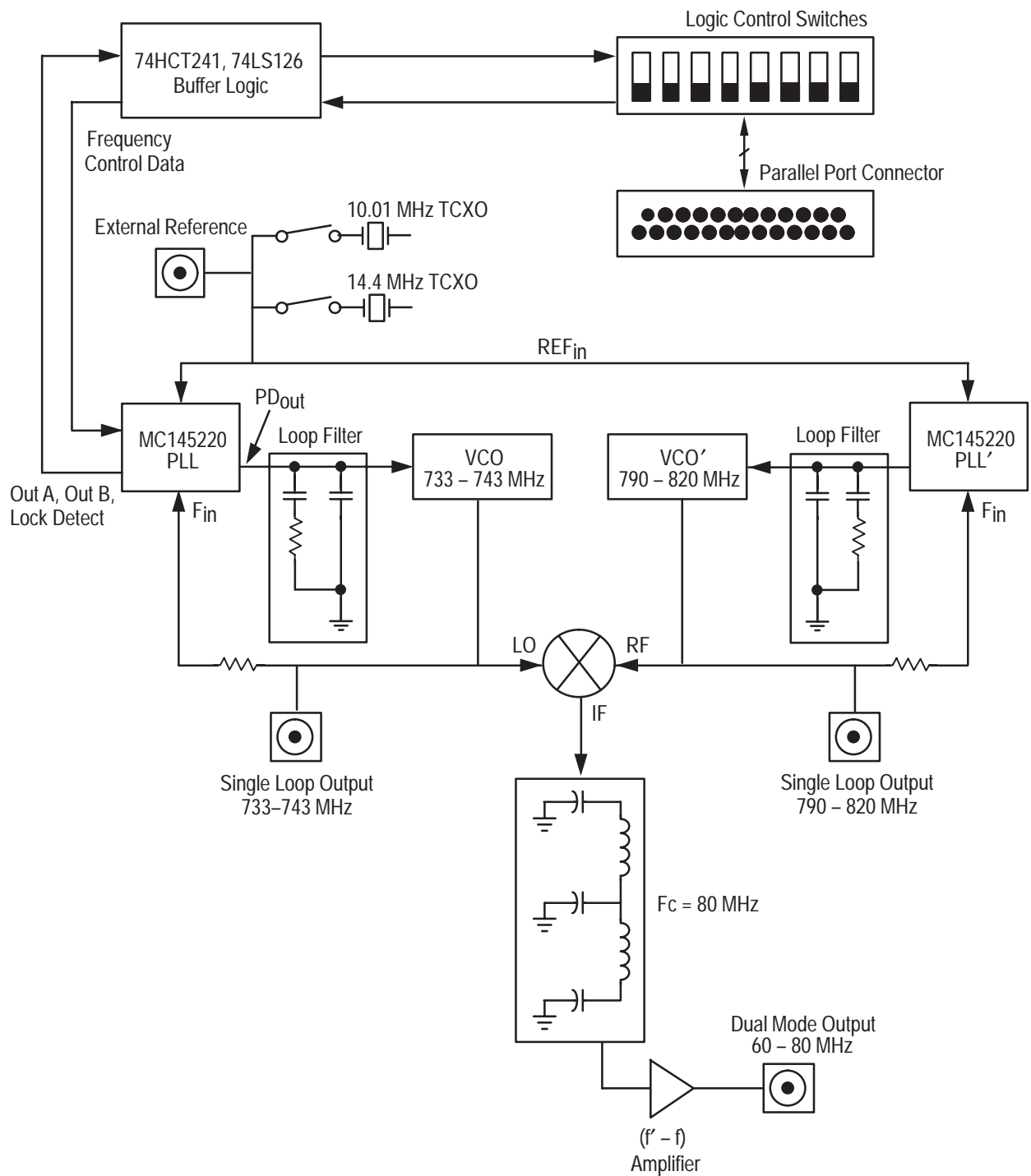


Figure 1. Evaluation Kit Block Diagram

TYPICAL PERFORMANCE

Typical performance applies only to the configuration as shipped. The MC145220EVK is shipped with $V+ = 5$ V. For lowest phase noise in single or dual loop mode, a $50\ \Omega$ load must be connected to J12.

	Single Loop PLL	Single Loop PLL'	Dual Loop PLL
Supply Voltage (J8)	11.5 – 12.5 V		
Supply Current (J8) (Note 1)	177 mA		
Available Current (Note 2)	45 mA		
Frequency Range (Note 3)	733 – 743 MHz	790 – 820 MHz	60 – 80 MHz
Reference Frequency (M1)	10.01 MHz		
Temperature Stability (M1, – 30°C to + 70°C)	< ± 2.5 ppm		
Reference Frequency (M5)	14.4 MHz		N/A
Temperature Stability (M5, – 30°C to + 85°C)	< ± 2 ppm		N/A
TCXO Aging (M1, M5)	< ± 1 ppm / year		
Step Size	10 kHz		10 Hz
Power Output	– 3.0 dBm	– 5.0 dBm	4.5 – 7.5 dBm
Frequency Accuracy	± 1.5 kHz	± 1.5 kHz	± 50 Hz
Reference Sidebands (Note 4)	– 57 dB	– 74 dB	– 57 dB
Phase Noise (100 Hz)	– 65 dBc/Hz	– 56 dBc/Hz	– 50 dBc/Hz
Phase Noise (10 kHz) (Note 5)	– 104 dBc/Hz	– 90 dBc/Hz	– 89 dBc/Hz
Switching Time (Note 6)	24 ms	40 ms	45 ms

NOTES:

- Supply current is current the board requires without user modifications.
- Available current is the sum of currents available to the user (in the prototype area) from the 5 V and 8.5 V supply. The 12 V supply is not regulated. Current at 12 V is limited by the external power supply. If the on-board VCO and amplifier are disconnected from the power bus, more current can be drawn in the prototype area. The current flowing into U5 (the 8.5 V regulator) should not exceed 180 mA. This will limit temperature rise in U5.
- Frequency ranges require use of the 5 V default charge pump supply voltage.
- VCO sidebands on PLL at low step sizes (10 kHz) are limited by control line leakage of the VCO. Up to 24 nA of leakage has been seen. At higher step sizes (100 kHz and above), this effect is much less noticeable. This did not affect PLL' because its VCO leakage was less than 10 pA.
- 10 kHz phase noise is limited by the PLL device noise. For low noise designs, the loop bandwidth is made narrower and the VCO is relied upon to provide the 10 kHz phase noise. This can be seen on the EVKs since the VCOs have much lower noise.
- 10 MHz step, within ± 1 kHz of final frequency ('220).
Due to the software architecture, when the user is measuring the switching time of a single board in dual loop mode, it takes 20 ms to load the data as compared to single loop mode, which takes 8 ms to load the data. This is a limitation of the software, not the IC. To find the actual PLL switching time, subtract 8 or 20 ms from the switching time stated in the table.

SUPPORT MATERIAL

The following documents are included in the appendix:

1. Schematic diagram of MC145220EVK.
2. Bill of materials.
3. Parts layout diagram.
4. Mechanical drawing of board.
5. MC145220 data sheet.
6. Typical signal plots.

PRODUCTION TEST

After assembly is complete, the following alignment and test is performed:

1. The control program is started in '220 single loop mode.
2. [L]! is selected to set PLL frequency to 733 MHz.
3. Power is applied to the board. DIP switch section 1 is closed circuit with all others being open circuit.
4. After attaching computer cable, [I]! is selected.
5. Trim resistor VR1 is adjusted to obtain an output frequency at J5 of 733 MHz \pm 500 Hz.
6. Voltage at the control voltage test point (TP2) is measured. It must be > 0.5 V.
7. [H]! is selected.
8. Voltage at the control voltage test point (TP2) is measured. It must be < 4.4 V.
9. [T]! is selected to toggle to PLL'.
10. [L]! is selected to set PLL' frequency to 790 MHz.
11. Voltage at the control voltage test point (TP9) is measured. It must be > 0.5 V.
12. [H]! is selected to set PLL' frequency to 820 MHz.
13. Voltage at the control voltage test point (TP9) is measured. It must be < 4.4 V.
14. [G] is selected and the board type is changed to '220 dual loop mode.
15. [Q]!, then [I]!, is selected to initialize the dual mode output (J12) to 70 MHz. The frequency should be 70 MHz \pm 50 Hz.

If in step 5 it isn't possible to obtain a signal on frequency, the adjustment screw in M1 may be turned for further frequency adjustment range. If neither adjustment works, [P] should be selected and the correct printer port address entered. [I]! is then selected to reload the data.

BOARD OPERATION

A computer is connected to the DB-25 connector J9. Data is output from the printer port. The printer card is in slot 0 using the default address in the control program. Data is sent to the PLL device (U1) through the DIP switch (S1), and 74HCT241 buffer (U2). D1, D2, D3, R7, R8, and R12 are in the data path between the 'HCT241 and PLL device. This limits the high level output voltage of the buffer. Voltage on PLL device inputs must be no greater than 0.5 V above V+. A '220 PLL has three output lines which are routed through a 74LS126 line driver (U3) back to the computer.

U2, the 74HCT241, provides isolation and logic translation for PLL input lines. Logic translation is needed from the TTL levels on the printer port to the CMOS levels on the '220 inputs.

A 12 V power supply should be used to power the board at J8 (Augat 2SV-02 connector). The 2SV-02 will accept 18-24 AWG bare copper power leads. No tools are needed for connection. If power is properly connected, LED D4 will be lit.

Power passes from J8 to U5 (LM317 regulator) configured as an 8.5 V regulator. 8.5 V powers the VCOs. Regulators U6 and U7 use the 8.5 V supply to produce 3 V and 5 V. The '220 board can use either to power the logic and charge pump. V+ voltage is selected by J11. U6 and U7 are cascaded with U5 to equalize their individual voltage drops.

The '220 operates in both a single loop and dual loop mode. There are no component changes between the two modes. The differences are in the programming of the counters and the SMA connector that is used.

The PLL loop is composed of the MC145220 (U1), 733 – 743 MHz VCO (M2), and a passive loop filter (R4, R5, C6, C7, C8). In single loop mode, output is taken from J5. A passive loop filter was used to keep the design simple, reduce noise, and reduce the quantity of traces susceptible to stray pickup. The PLL' loop is composed of the MC145220 (U1), 790 – 820 MHz VCO (M3), and a passive loop filter (R22, R25, C24, C26, C30). In single loop mode, output is taken from J10.

Dual mode output is the $(f' - f)$ frequency output from the mixer. It is low pass filtered (L1, L2, C15, C21, C22) then amplified (U4). The output is available at J12.

Phase detector current is 2 mA. J1 is a removable jumper used for current measurement of V+.

Two TCXOs, a Motorola Saber 14.4 MHz (M5), and Raltron 10.01 MHz (M1) are supplied. As shipped from the factory, the 10.01 MHz TCXO is in use. This allows both the 10 kHz and 10 Hz step sizes to be used with one TCXO. 10.01 MHz cannot be divided for larger step sizes such as 100 kHz. For larger step sizes use the Saber. Jumpers J3, J4, J13, and J14 determine which TCXO or the external reference input is in use.

DUAL MODE OUTPUT

The dual mode output (J12) is the difference frequency from mixing PLL and PLL'. By using a reference frequency of 10.01 MHz, PLL can be operated with a 10.01 kHz step size and PLL' with a 10 kHz step size. If both PLL and PLL' step down in frequency, the mixed output will step up by 10 Hz. More information on the offset reference technique is in **AN1277/D, Offset Reference PLLs for Fine Resolution or Fast Hopping**. The block diagram, formulas, and an example are shown in Figure 2.

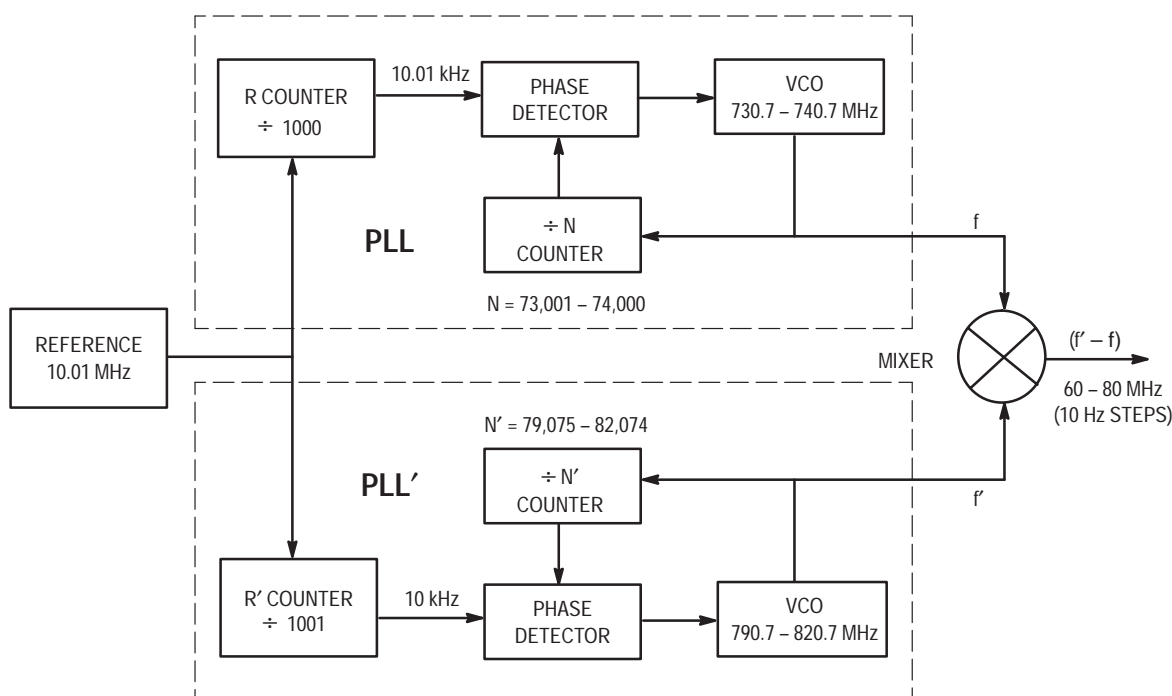


Figure 2. Dual Mode Block Diagram

PLL	PLL'
$f = N (10.01 \text{ kHz})$	$f' = N' (10 \text{ kHz})$
$f = 10.01 \text{ kHz} \left[74,000 - \frac{r(f' - f)}{10 \text{ Hz}} \right]$	$f' = 10 \text{ kHz} \left[\frac{w(f' - f) + 740 \text{ kHz}}{10 \text{ kHz}} + N \right]$
$N = 74,000 - \frac{r(f' - f)}{10 \text{ Hz}}$	$N' = N + 74 + \frac{w(f' - f)}{10 \text{ kHz}}$
$(f' - f) = w(f' - f) + r(f' - f)$	
$(f' - f) = \text{Desired Output Frequency}$	
$w(f' - f) = \text{Output Frequency Portion that Divides Evenly by 10 kHz}$	
$r(f' - f) = \text{Remainder from Output Frequency Division by 10 kHz}$	

Dual Mode Formulas

Example: Synthesize 76.849 930 MHz

$$r(f' - f) = 9.930 \text{ kHz},$$

$$w(f' - f) = 76.840 \text{ MHz}$$

$$N = 74,000 - \frac{9.930 \text{ kHz}}{10 \text{ Hz}} = 73,007$$

$$f = 73,007 (10.01 \text{ kHz}) = 730.800 070 \text{ MHz}$$

$$N' = 73,007 + 74 + \frac{76.840 \text{ MHz}}{10 \text{ kHz}} = 80,765$$

$$f' = 80,765 (10 \text{ kHz}) = 807.650 000 \text{ MHz}$$

$$(f' - f) = 807.650 000 \text{ MHz} - 730.800 070 \text{ MHz} = 76.849 930 \text{ MHz}$$

EXTERNAL REFERENCE INPUT

To use an external reference, disconnect J3, J4, J13, and J14. Use a reference signal at J2 which complies with data sheet requirements. Then modify the reference frequency in the program main menu to reflect the changes made (F menu item).

DATA TRANSFER FROM COMPUTER TO EVK

To control the serial input EVK with the parallel printer port, a conversion is done. Printer cards are designed to output eight bits through eight lines. A bit mask is used to obtain the bit combination for the three required output lines (Data, Clock, Load). As bytes are sent to the printer card in sequence, it appears to be a serial transfer. The printer port is used because data transfer using the serial port would be much slower. A standard IBM PC can support a parallel port data rate of 4.77 MHz.

IBM PCs and compatibles can accept up to three printer port configurations. These ports are called LPT1, LPT2, and LPT3. Each printer port has a unique address. Two sets of addresses are in common use. One set applies to IBM PC XT, AT, and clones. The other is for the PS 2 line. To load data into the EVK, the correct address must be selected. The program default is \$278. If \$278 is not the address in use, it must be modified by entering the P menu item in the main menu. All allowed addresses given in hexadecimal are as follows:

Label	IBM PC and Clones	PS 2
LPT1	278	3BC
LPT2	378	378
LPT3	3BC	278

Up to three EVK boards can operate independently from one printer port. All lines on the printer port are connected to every EVK. Even with three boards operating, only three output lines (Clock, Data, and Load) from the printer card are used. If two boards are controlled together, data for the second board is received from the Output A of the first. Output A is a configurable output on '220 devices, which in this case is used to shift data through chip 1 into chip 2. Output A and Data are connected using a printer port input line. This was done to avoid connecting extra wires. Fortunately not all port input lines are needed for computer input. Load and Clock are common to both boards.

A three-board cascade is handled similarly to a two-board cascade. Out A on the first board is fed to Data on the second. Out A on the second connects to Data on the third. Instructing the program on the quantity of boards connected together allows it to modify the number of bits sent.

All boards have a DIP switch S1 which gives each a unique address. The configuration menu is used to tell the program what type of board is connected at a board address. Switch positions for all possible addresses are given in Figure 2.

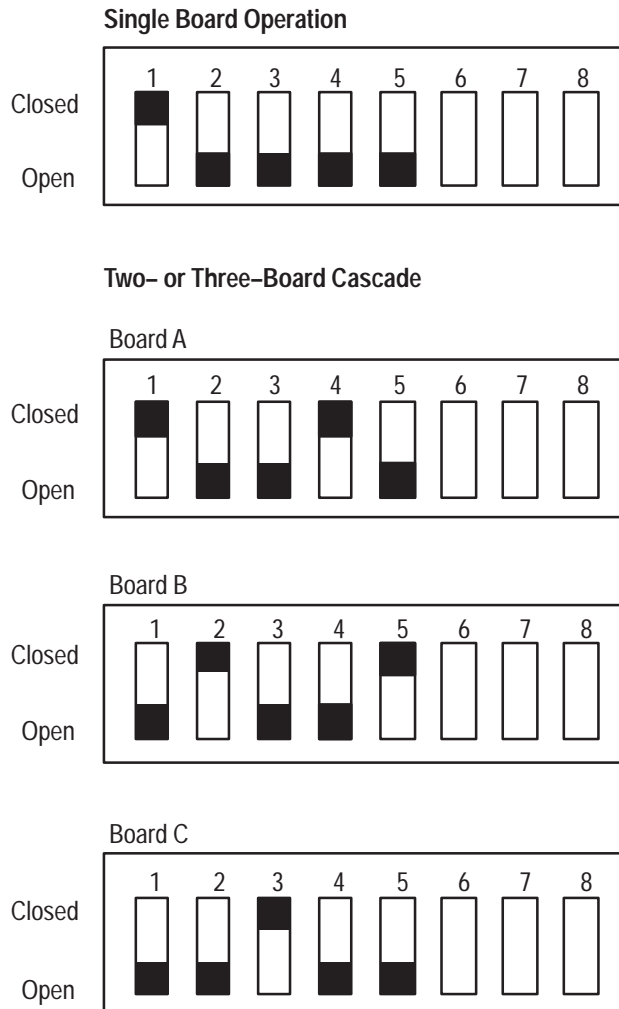


Figure 3. Switch Positions

In Figure 2, DIP switch sections 6, 7, and 8 allow the computer to read Out A, Lock Detect, or Lock Detect from the PLL device. Each of the inputs can only be read on one board at a time, but each item could be read on a different board. In a three-board cascade, Out A could be read from the first board, Out B from the second, and Lock Detect from the third. There is no way to determine the board address of a particular input with software. The control program does not make use of these inputs; however, source code could be modified as required. Pin assignment on the printer port connector is:

Label	Pin Number
Out A	12
Out B	13
Lock Detect	15

PRINTER PORT CONFIGURATION

Printer port outputs on an IBM PC or clone use TTL–LS logic levels. Inputs are one TTL–LS load. Signal lines can be used for any purpose. The standard names, direction of data flow, true and inverted data are shown in Figure 3.

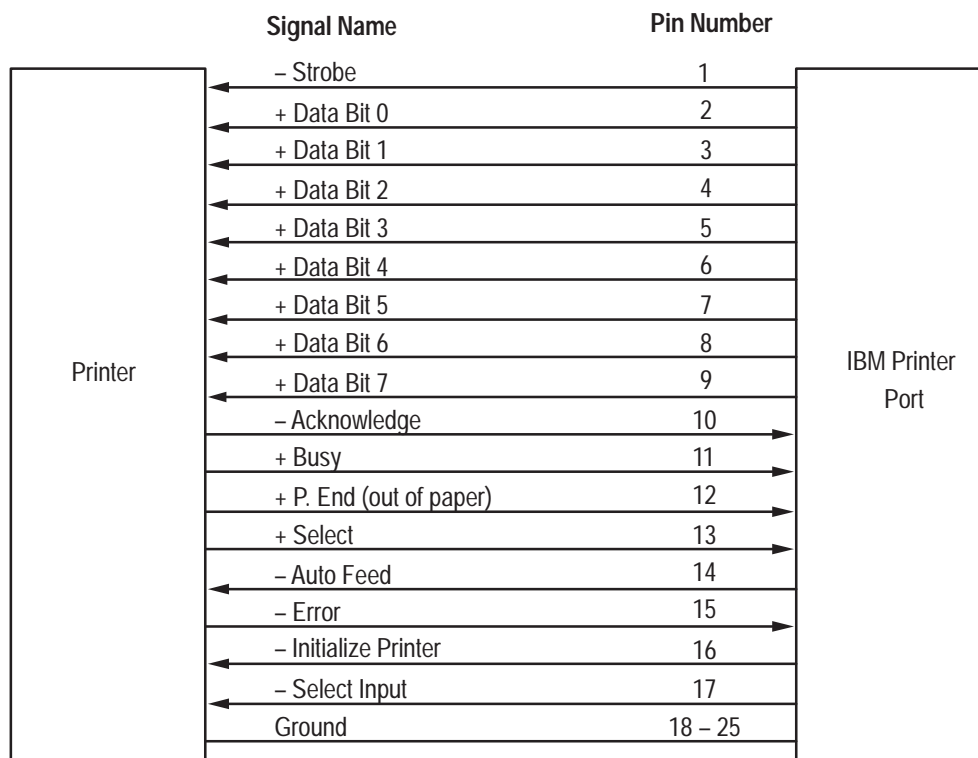


Figure 4. Printer Port Data Lines

Pin numbers for the port connector are shown in Figure 4.

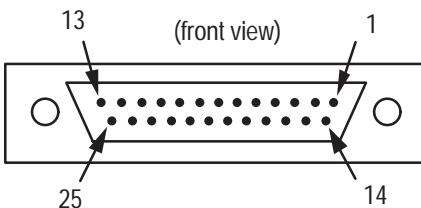


Figure 5. DB–25 Male Connector

SECTION 2 – SOFTWARE DESCRIPTIONS SUMMARY

INTRODUCTION

The MC145xxx EVK control program is used to program all PLL evaluation kits. It will simultaneously control up to three different boards independently from one printer port. All features of the PLL device may be accessed. Default frequencies can be modified to allow use of different channel spacings and VCOs.

User input errors are detected and appropriate messages are displayed.

To show the format of the program, a sample screen is shown below:

'Select from the available options'

```

                                Welcome to MC145xxx EVK Demonstration Program, rev 4.0
                                Select from the available options

Available Boards - Current target board is: A, MC145220 Dual
  Brd [A]!: MC145220 Dual   Brd [-]!: N/A           Brd [-]!: N/A
-----

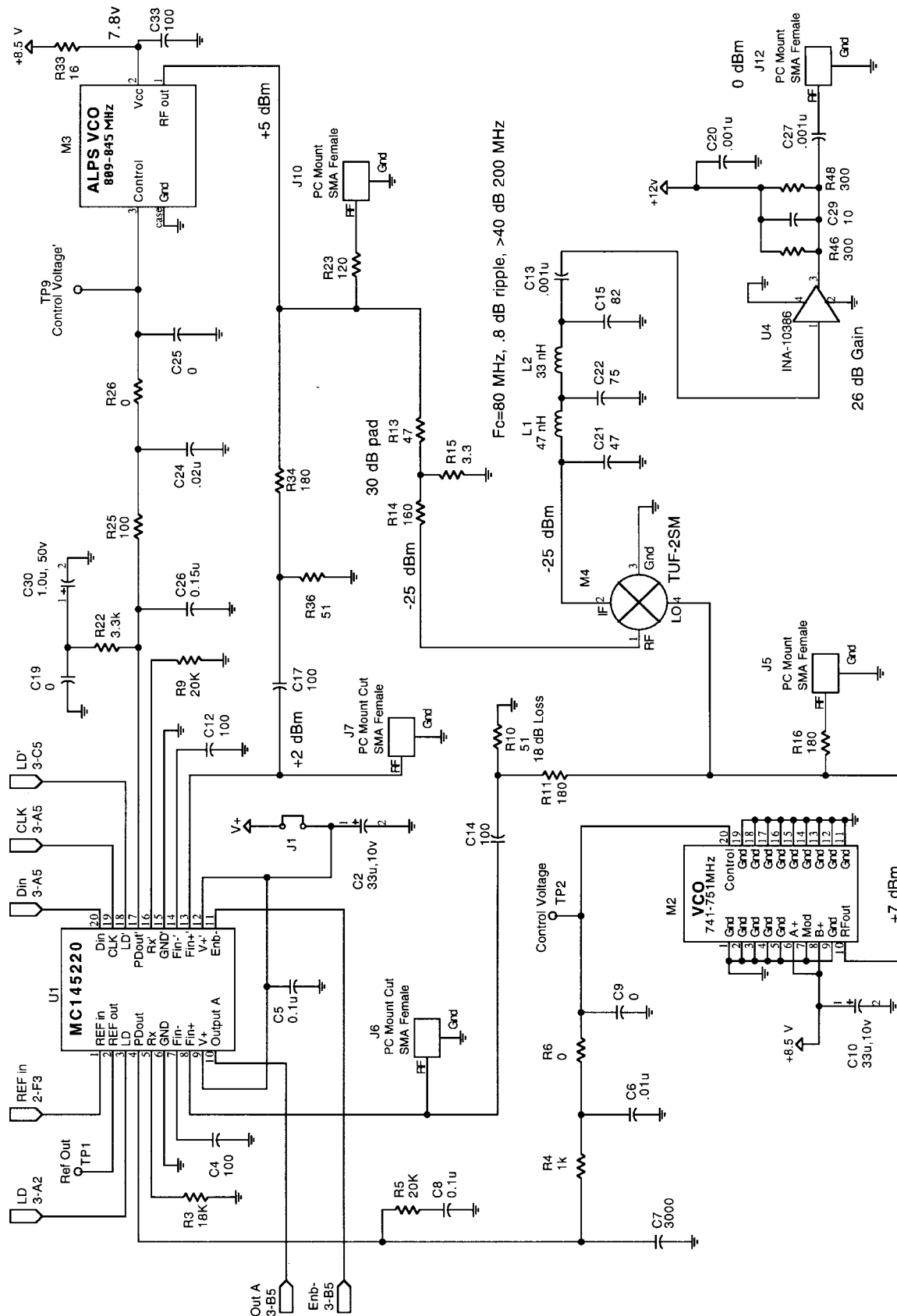
MC145xxx Frequency Commands - Current Output Frequency is 70 MHz
[L]! Set to low freq.      60 MHz [W] Change default low freq.
[M]! Set to med. freq.     70 MHz [Y] Change default med. freq.
[H]! Set to high freq.     80 MHz [Z] Change default high freq.
[U]! Step frequency up by step size   [O] Set PLL output frequency
[D]! Step frequency down by step size  [F] REFin freq. & channel spacing
MC145xxx Additional Commands
[E] Set function of output A           [N] Change C register and Prescale
[R] Set crystal/reference mode - Current mode is Ref. mode, REFOut low
-----

Initialization/System Setup Commands:
[P] Set output port address - Current address is $278
[G] Change board definitions
[I] Initialize board(s), Write all registers

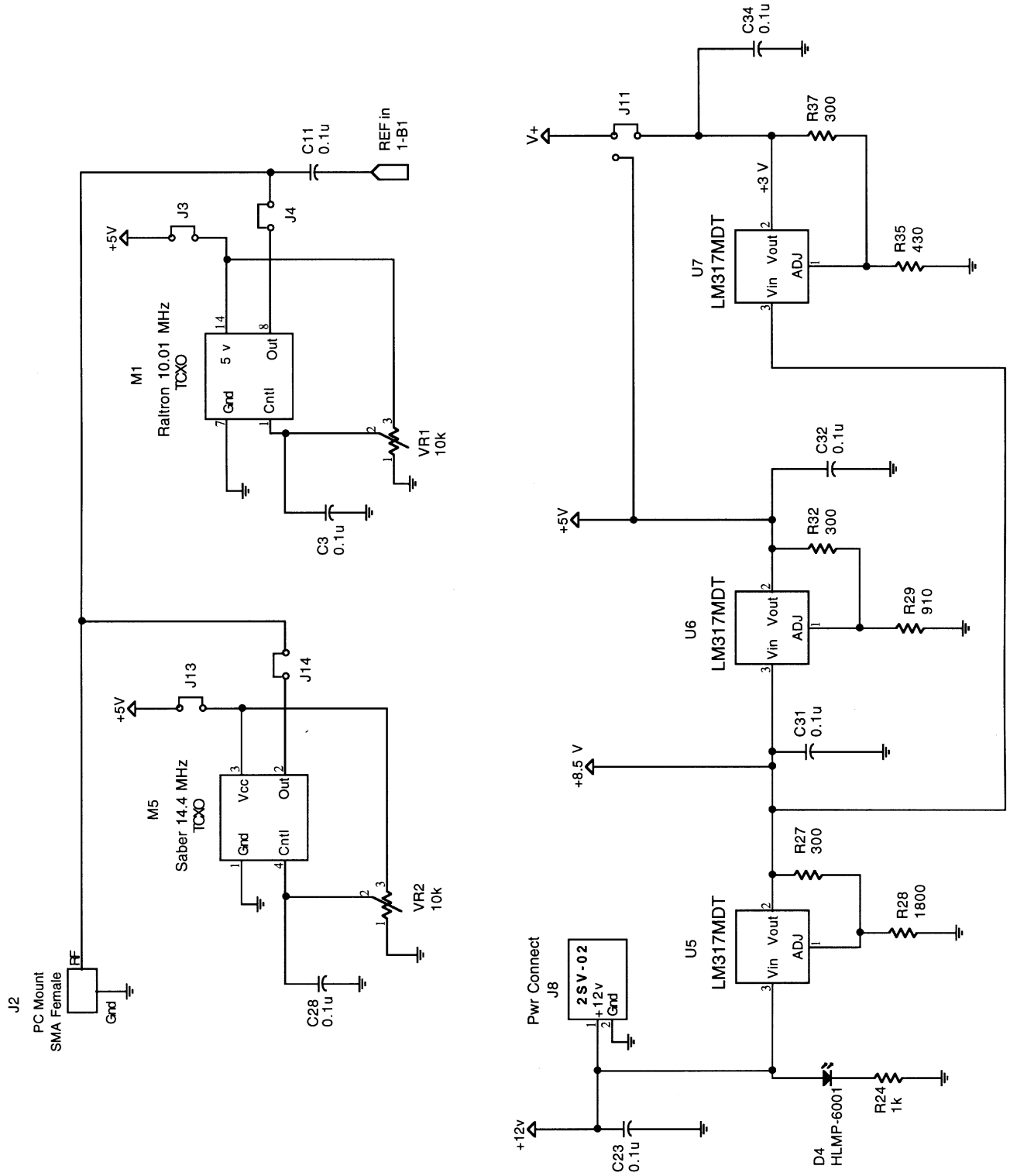
                                [X]! Terminate demonstration program. [?!] View help screen.
```

APPENDIX

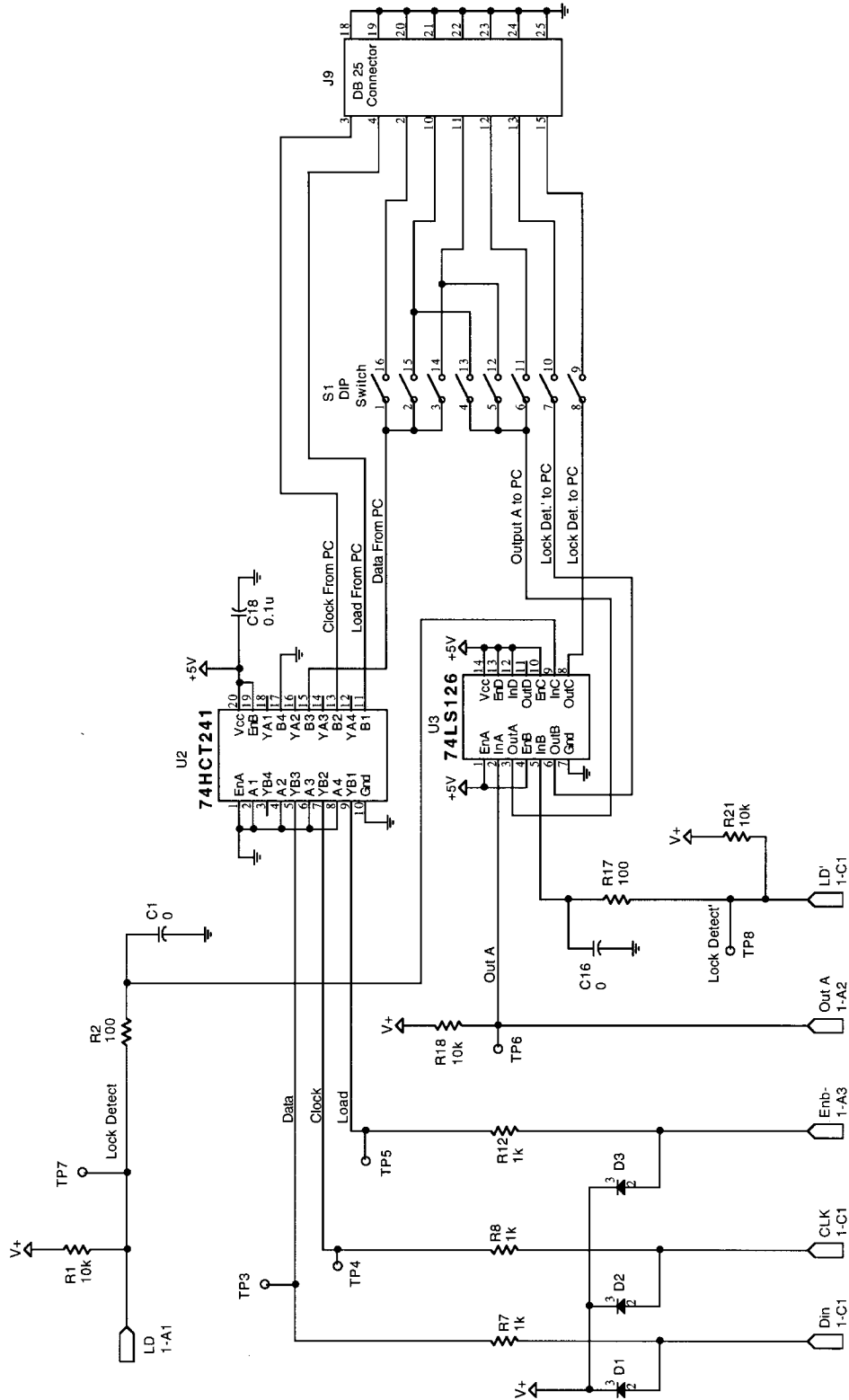
MC145220 PLL Evaluation Board



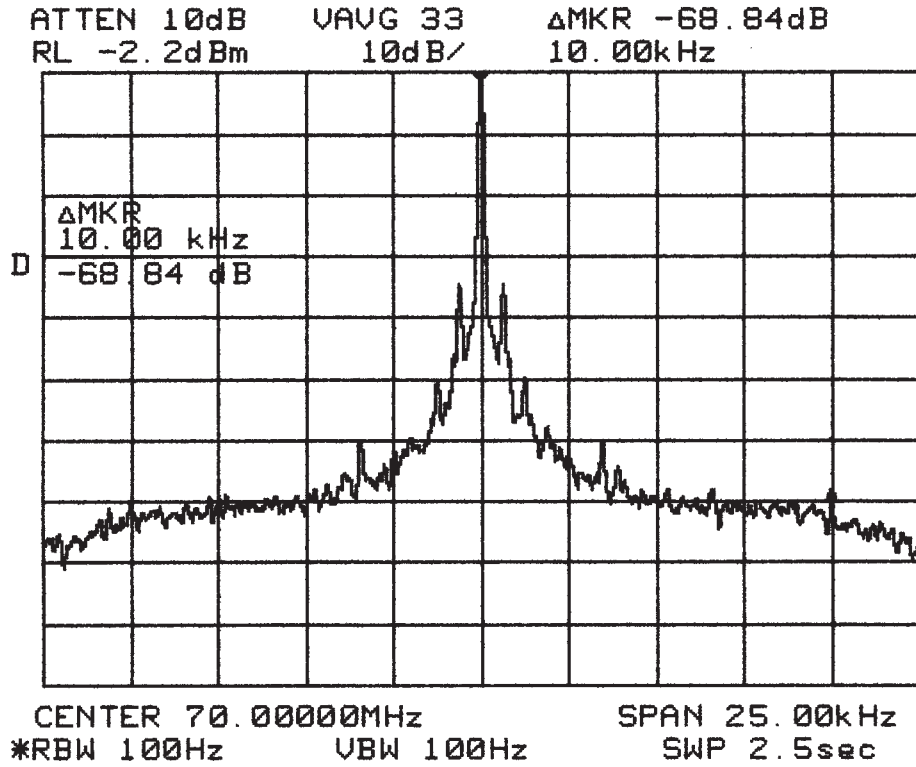
MC145220 Power Supply and Reference



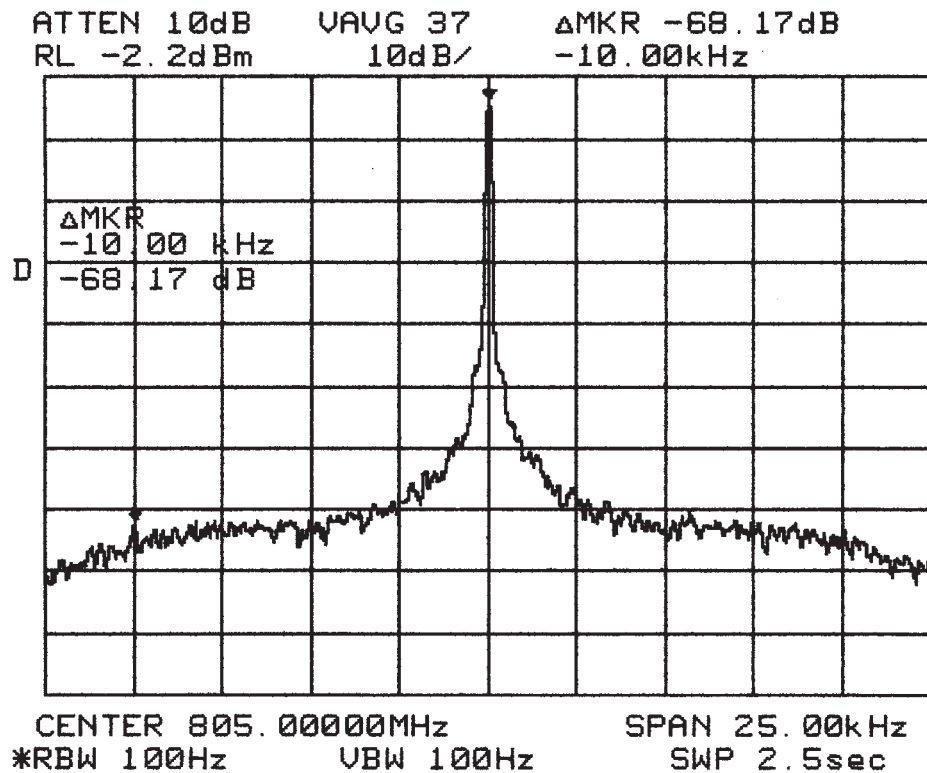
MC145220EVK Bus Interface



MC145220EVK Signal Plot — Dual Loop Mode Output at 70 MHz

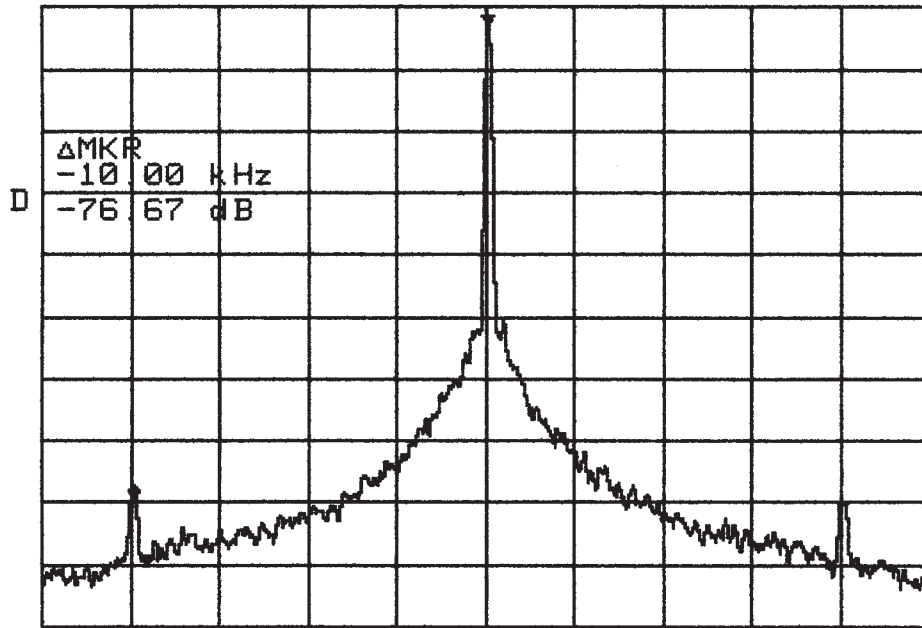


MC145220EVK Signal Plot — Single Loop Mode PLL on 805 MHz



MC145220EVK Signal Plot — Single Loop Mode PLL on 738 MHz

ATTEN 10dB VAUG 21 ΔMKR -76.67dB
RL -2.2dBm 10dB/ -10.00kHz



CENTER 737.99987MHz SPAN 25.00kHz
*RBW 100Hz VBW 100Hz SWP 2.5sec

Chapter Five

RF Discrete Transistors

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Section One Selector Guide

Motorola RF Discrete Transistors

Motorola offers the most extensive group of RF Discrete Transistors offered by any semiconductor manufacturer anywhere in the world today.

From Bipolar to FET, the user can choose from a variety of packages. They include plastic and ceramic that are microstrip circuit compatible or surface mountable. Many are designed for automated assembly equipment.

Major sub-headings are Power MOSFETs, Power GaAs and Bipolar Transistors.

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Motorola RF High Power Transistors

RF Power MOSFETs

Motorola RF Power MOSFETs are constructed using a planar process to enhance manufacturing repeatability. They are *N-channel field effect transistors* with an oxide insulated gate which controls vertical current flow.

Compared with bipolar transistors, RF Power FETs exhibit higher gain, higher input impedance, enhanced thermal stability and lower noise. The FETs listed in this section are specified for operation in RF Power Amplifiers and are grouped by frequency range of operation and type of application. Arrangement within each group is first by order of voltage then by increasing output power.

Table 1. 2 to 150 MHz HF/SSB – Vertical MOSFETs

For military and commercial HF/SSB fixed, mobile and marine transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	V _{DD} Volts	Class	Gain (Typ) @ 30 MHz dB	Typical IMD		θ _{JC} °C/W	Package/Style
							d ₃ dB	d ₁₁ dB		
MRF171A	U	2–225	30	28	AB	20	–32	—	1.52	211–07/2
MRF148A	U	2–225	30	50	AB	18	–35	–60	1.5	211–07/2
MRF150	U	2–150	150	50	AB	17	–32	–60	0.6	211–11/2
MRF154	U	2–100	600	50	AB	17	–25	—	0.13	368/2
MRF157	U	2–100	600	50	AB	20	–25	—	0.13	368/2

Table 2. 2 to 225 MHz VHF AM/FM – Vertical MOSFETs

For VHF military and commercial aircraft radio transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	V _{DD} Volts	Class	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Package/Style
MRF134	U	30–225	5	28	AB	14/150	55	10	211–07/2
MRF136	U	30–225	15	28	AB	16/150	60	3.2	211–07/2
MRF171A	U	30–225	45	28	AB	19.5/150	65	1.52	211–07/2
MRF173	U	30–225	80	28	AB	13/150	65	0.8	211–11/2
MRF174	U	30–225	125	28	AB	11.8/150	60	0.65	211–11/2
MRF141	U	2–175	150	28	AB	10/175	55	0.6	211–11/2
MRF141G	U	2–175	300	28	AB	13/175	55	0.35	375/2
MRF151	U	2–175	150	50	AB	13/175	45	0.6	211–11/2
MRF151G	U	2–175	300	50	AB	16/175	55	0.35	375/2

Table 3. 30 to 512 MHz VHF/UHF AM/FM – Vertical MOSFETs

For VHF/UHF military and commercial aircraft radio transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	V _{DD} Volts	Class	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Package/Style
MRF158	U	30–512	2	28	AB	17.5/500	52	13.2	305A/2
MRF160	U	30–512	4	28	AB	17/500	55	7.2	249/3
MRF166C	U	30–512	20	28	AB	16/500	55	2.5	319/3
MRF166W	U	30–512	40	28	AB	16/500	55	1.0	412/1
MRF177	U	100–400	100	28	AB	12/400	60	0.65	744A/2
MRF275L	U	150–512	100	28	AB	8.8/500	55	0.65	333/2
MRF275G	U	150–512	150	28	AB	11.2/500	55	0.44	375/2

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

RF Power MOSFETs (continued)

Table 4. Mobile – To 520 MHz

Designed for broadband VHF & UHF commercial and industrial applications. The high gain and broadband performance of these devices make them ideal for large-signal, common-source amplifier applications in 12.5/7.5 volt mobile, portable and base station operation.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Package/Style
VHF & UHF, Land Mobile Radio, Class AB – LDMOS Die							
MRF1511T1(18f)★	U	136–175	8	7.5	11.5/175	55	466/1
MRF1517T1(18f)★	U	430–520	8	7.5	11/520	55	466/1
MRF1513T1(18f)★	U	400–520	3	7.5/12.5	11/520	55	466/1
MRF1518T1(18f)★	U	400–520	8	12.5	11/520	55	466/1
MRF1535T1(18j)★	U	400–520	35	12.5	10(Min)/520	50(Min)	1264/1
MRF1550T1(18j)★	U	136–175	50	12.5	10(Min)/175	50(Min)	1264/1

Table 5. Broadcast – To 1.0 GHz – Lateral MOSFETs

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	IMD dBc	Package/Style
470 – 1000 MHz, Class AB – LDMOS Die								
MRF373A(46a)	U	470–860	75 CW	32	18/860	60	—	360B/1
MRF373AS(46a)	U	470–860	75 CW	32	18/860	60	—	360C/1
MRF374A(46a)	U	470–860	130 PEP	32	17.3/860	41	–31	375F/2
MRF372★	M	470–860	180 PEP	32	17/860	36	–35	375G/2
MRF377 ⁽⁹⁾	M	470–860	180 PEP	32	18/860	40	–30	375G/2
MRF376 ⁽⁹⁾	M	470–860	400 Pulsed	50	16/860	50	—	375G/2

Table 6. Cellular – To 1.0 GHz – Lateral MOSFETs

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/Style
800 – 1.0 GHz, Class AB – LDMOS Die								
MRF9002R2(18e,46a)	U	960	2 PEP	26	16/960	35	9	978/–
MRF9030MR1(18a,46b)	U	945	30 PEP	26	17/945	41	—	1265/1
MRF9030(46b)	U	945	30 PEP	26	17/945	40	1.9	360B/1
MRF9030S(18a,46b)	U	945	30 PEP	26	17/945	40	1.5	360C/1
MRF9045MR1(18a)★	U	945	45 PEP	28	18.5/945	41	0.8 ⁽⁵⁰⁾	1265/1
MRF9045★	U	945	45 PEP	28	18.8/945	42	1.4	360B/1
MRF9045S(18a)★	U	945	45 PEP	28	18.8/945	42	1.0	360C/1
MRF9060MR1(18a,46b)	U	945	60 PEP	26	17/945	40	—	1265/1
MRF9060(46a)	U	945	60 PEP	26	17/945	40	1.1	360B/1
MRF9060S(18a,46a)	U	945	60 PEP	26	17/945	40	0.8	360C/1
MRF6522–70(18i)	M	921–960	70 CW	26	16/921,960	58	1.1	465D/1
MRF9080★	M	921–960	75 CW	26	18.5/921,960	55	0.7	465/1
MRF9080S★	M	921–960	75 CW	26	18.5/921,960	55	0.7	465A/1
MRF9085★	M	880	90 PEP	26	17.9/880	40	0.7	465/1
MRF9085S★	M	880	90 PEP	26	17.9/880	40	0.7	465A/1

⁽⁹⁾In development.

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units;

f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

⁽⁵⁰⁾Simulated

★New Product

RF Power MOSFETs (continued)

Table 6. Cellular – To 1.0 GHz – Lateral MOSFETs (continued)

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style	
800 – 1.0 GHz, Class AB – LDMOS Die (continued)									
MRF9120 ^(46a)	M	880	120 PEP	2-Tone	26	16/880	39	0.7	375B/2
MRF9120S ^(46a)	M	880	120 PEP	2-Tone	26	16/880	39	0.7	375H/2
MRF9180★	M	880	170 PEP	2-Tone	26	17.5/880	39	0.45	375D/2
MRF9180S★	M	880	170 PEP	2-Tone	26	17.5/880	39	0.45	375E/2

Table 7. PCS and 3G – To 2.1 GHz – Lateral MOSFETs

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style	
1805 – 1990 MHz, Class AB – LDMOS Die (GSM1800, GSM1900, GSM EDGE and PCS TDMA)									
MRF18060A	M	1805–1880	60 CW	1-Tone	26	13/1805,1880	45	0.97	465/1
MRF18060AS	M	1805–1880	60 CW	1-Tone	26	13/1805,1880	45	0.97	465A/1
MRF18060B	M	1930–1990	60 CW	1-Tone	26	13/1930,1990	45	0.97	465/1
MRF18060BS	M	1930–1990	60 CW	1-Tone	26	13/1930,1990	45	0.97	465A/1
MRF18085A ^(46a)	M	1805–1880	85 CW	1-Tone	26	13/1805,1880	52	0.64	465/1
MRF18085AS ^(46a)	M	1805–1880	85 CW	1-Tone	26	13/1805,1880	53	0.64	465A/1
MRF18085B ^(46a)	M	1930–1990	85 CW	1-Tone	26	13/1930,1990	53	0.64	465/1
MRF18085BS ^(46a)	M	1930–1990	85 CW	1-Tone	26	13/1930,1990	52	0.64	465A/1
MRF18090A	M	1805–1880	90 CW	1-Tone	26	13.5/1805,1880	52	0.7	465B/1
MRF18090AS	M	1805–1880	90 CW	1-Tone	26	13.5/1805,1880	52	0.7	465C/1
MRF18090B	M	1930–1990	90 CW	1-Tone	26	13.5/1930,1990	45	0.7	465B/1
MRF18090BS	M	1930–1990	90 CW	1-Tone	26	13.5/1930,1990	45	0.7	465C/1

1.9 GHz, Class AB – LDMOS Die (2-CH N-CDMA)

MRF19030★	M	1930–1990	30 PEP	2-Tone	26	13/1990	36	2.1	465E/1
MRF19030S★	M	1930–1990	30 PEP	2-Tone	26	13/1990	36	2.1	465F/1
MRF19045 ^(46a)	M	1930–1990	9.5 AVG	N-CDMA	26	14.5/1990	23.5	1.97	465E/1
MRF19045S ^(46a)	M	1930–1990	9.5 AVG	N-CDMA	26	14.5/1990	23.5	1.97	465F/1
MRF19060	M	1930–1990	60 PEP	2-Tone	26	12.5/1990	36	0.97	465/1
MRF19060S	M	1930–1990	60 PEP	2-Tone	26	12.5/1990	36	0.97	465A/1
MRF19090	M	1930–1990	90 PEP	2-Tone	26	11.5/1990	35	0.65	465B/1
MRF19090S	M	1930–1990	90 PEP	2-Tone	26	11.5/1990	35	0.65	465C/1
MRF19085★	M	1930–1990	18 AVG	N-CDMA	26	13/1990	23	0.64	465/1
MRF19085S★	M	1930–1990	18 AVG	N-CDMA	26	13/1990	23	0.64	465A/1
MRF19120 ⁽³⁾ ★	M	1930–1990	120 PEP	2-Tone	26	11.7/1990	34	0.45	375D/2
MRF19120S ⁽³⁾ ★	M	1930–1990	120 PEP	2-Tone	26	11.7/1990	34	0.45	375E/2
MRF19125★	M	1930–1990	24 AVG	N-CDMA	26	13.5/1990	22	0.53	465B/1
MRF19125S★	M	1930–1990	24 AVG	N-CDMA	26	13.5/1990	22	0.53	465C/1

⁽³⁾Internal Impedance Matched Push-Pull Transistors

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units; f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Power MOSFETs (continued)

Table 7. PCS and 3G – To 2.1 GHz – Lateral MOSFETs (continued)

Device	Frequency Band ⁽³⁷⁾	Pout Watts	Test Signal	VDD Volts	Gain (Typ)/Freq. dB/MHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style
2.0 GHz, Class A, AB – LDMOS Die								
MRF281SR1 ^(18a) ★	U	1930–2000	4 PEP	2–Tone	26	12.5/2000	33	458B/1
MRF281ZR1 ^(18a) ★	U	1930–2000	4 PEP	2–Tone	26	12.5/2000	33	458C/1
MRF282SR1 ^(18a) ★	U	1930–2000	10 PEP	2–Tone	26	11.5/2000	28(min)	458B/1
MRF282ZR1 ^(18a) ★	U	1930–2000	10 PEP	2–Tone	26	11.5/2000	28(min)	458C/1
MRF284	U	1930–2000	30 PEP	2–Tone	26	10.5/2000	35	360B/1
MRF284SR1 ^(18a)	U	1930–2000	30 PEP	2–Tone	26	10.5/2000	35	360C/1
MRF286 ^(46a)	M	1930–2000	60 PEP	2–Tone	26	10.5/2000	32	465/1
MRF286S ^(46a)	M	1930–2000	60 PEP	2–Tone	26	10.5/2000	32	465A/1
2.1 GHz, Class AB – LDMOS Die (2–CH W–CDMA, UMTS)								
MRF21010★	U	2110–2170	10 PEP	2–Tone	28	13.5/2170	35	360B/1
MRF21010S ^(46a)	U	2110–2170	10 PEP	2–Tone	28	13.5/2170	35	360C/1
MRF21030★	M	2110–2170	30 PEP	2–Tone	28	13/2170	33	465E/1
MRF21030S★	M	2110–2170	30 PEP	2–Tone	28	13/2170	33	465F/1
MRF21045★	M	2110–2170	10 AVG	W–CDMA	28	15/2170	23.5	465E/1
MRF21045S★	M	2110–2170	10 AVG	W–CDMA	28	15/2170	23.5	465F/1
MRF21060	M	2110–2170	60 PEP	2–Tone	28	12.5/2170	34	465/1
MRF21060S	M	2110–2170	60 PEP	2–Tone	28	12.5/2170	34	465A/1
MRF21085★	M	2110–2170	19 AVG	W–CDMA	28	13.6/2170	23	465/1
MRF21085S★	M	2110–2170	19 AVG	W–CDMA	28	13.6/2170	23	465A/1
MRF21090★	M	2110–2170	90 PEP	2–Tone	28	11.7/2170	33	465B/1
MRF21090S★	M	2110–2170	90 PEP	2–Tone	28	11.7/2170	33	465C/1
MRF21120 ⁽³⁾ ★	M	2110–2170	120 PEP	2–Tone	28	11.4/2170	34.5	375D/2
MRF21120S ⁽³⁾ ★	M	2110–2170	120 PEP	2–Tone	28	11.2/2170	34.5	375E/2
MRF21125	M	2110–2170	20 AVG	W–CDMA	28	13/2170	18	465B/1
MRF21125S	M	2110–2170	20 AVG	W–CDMA	28	13/2170	18	465C/1
MRF21180 ^(3,46a)	M	2110–2170	38 AVG	W–CDMA	28	12.5/2170	22	375D/2
MRF21180S ^(3,46a)	M	2110–2170	38 AVG	W–CDMA	28	12.5/2170	22	375E/2

⁽³⁾Internal Impedance Matched Push-Pull Transistors

⁽¹⁸⁾Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units;

f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

RF Power GaAs Transistors

Motorola power GaAs transistors are made using an InGaAs PHEMT epitaxial structure for superior RF efficiency and linearity. The FETs listed in this section are designed for operation in base station infrastructure RF power amplifiers and are grouped according to frequency range and type of application. Parts are listed first by order of operating voltage, then by increasing output power.

Table 1. 3.5 GHz – Linear Transistors

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Test Signal	V _{DD} Volts	Gain (Typ)/Freq. dB/GHz	η Eff. (Typ) %	θ _{JC} °C/W	Pkg/ Style
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3.5 GHz, Class AB – GaAs (WLL, BWA, W-CDMA)

MRFG35010 ⁽⁹⁾	U	3.5 G	1 AVG	W-CDMA	12	10/3.5	26	6	—
MRFG35030 ⁽⁹⁾	M	3.5 G	4 AVG	W-CDMA	12	10/3.5	24	—	—

⁽⁹⁾In development.

RF Power Bipolar Transistors

Motorola's broad line of bipolar RF power transistors are characterized for operation in RF power amplifiers. Typical applications are in base stations, military and commercial landmobile, avionics and marine radio transmitters. Groupings are by frequency band and type of application. Within each group, the arrangement of devices is by major supply voltage rating, then in the order of increasing output power. All devices are NPN polarity except where otherwise noted.

UHF Transistors

Table 1. 100 – 500 MHz Band

Designed for UHF military and commercial aircraft radio transmitters.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	Gain (Min)/Freq. dB/MHz	θ _{JC} °C/W	Package/Style
V_{CC} = 28 Volts, Class C						
MRF392 ⁽³⁾	M	100–400	125	8/400	0.65	744A/1
MRF393 ⁽³⁾	M	100–512	100	7.5/500	0.65	744A/1

900 MHz Transistors

Table 2. 900 – 960 MHz Band

Designed specifically for the 900 MHz mobile radio band, these devices offer superior gain, ruggedness, stability and broadband operation. Devices are for mobile and base station applications.

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	Class	Gain (Min)/Freq. dB/MHz	θ _{JC} °C/W	Package/Style
V_{CC} = 24 Volts — Si Bipolar							
MRF858S	U	840–900	3.6 CW	A	11/900	6.9	319A/2
MRF897 ⁽³⁾	M	900	30	AB	10/900	1.7	395B/1
MRF897R ⁽³⁾	M	900	30	AB	10.5/900	1.7	395E/1
MRF898 ⁽²⁾	M	850–900	60 CW	C	7/900	1	333A/1
V_{CC} = 26 Volts — Si Bipolar							
MRF6409	M	921–960	20	AB	10/960	3.8	319/2
MRF6414	M	921–960	50	AB	8.5/960	1.3	333A/2
MRF899 ⁽³⁾	M	900	150	AB	8/900	0.8	375A/1

1.5 GHz Transistors

Table 3. 1600 – 1640 MHz Band

Device	Frequency Band ⁽³⁷⁾		P _{out} Watts	Class	Gain (Min)/Freq. dB/MHz	η Eff. (Min) %	θ _{JC} °C/W	Package/Style
MRF16006	M	1600–1640	6	C	7.4/1600	40	6.8	395C/2
MRF16030	M	1600–1640	30	C	7.5/1600	40	1.7	395C/2

⁽²⁾Internal Impedance Matched

⁽³⁾Internal Impedance Matched Push-Pull Transistors

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

Microwave Transistors

Table 4. L-Band Long Pulse Power

These products are designed for pulse power amplifier applications in the 960–1215 MHz frequency range. They are capable of handling up to 10 μ s pulses in long pulse trains resulting in up to a 50% duty cycle over a 3.5 millisecond interval. Overall duty cycle is limited to 25% maximum. The primary applications for devices of this type are military systems, specifically JTIDS and commercial systems, specifically Mode S. Package types are hermetic.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Gain (Min) @ 1215 MHz dB	θ_{JC} °C/W	Package/Style
V_{CC} = 28 Volts — Class C Common Base					
MRF10005	M 960–1215	5	8.5	8	336E/1
V_{CC} = 36 Volts — Class C Common Base					
MRF10031	M 960–1215	30	10	3	376B/1
MRF10120	M 960–1215	120	8	0.6	355C/1
V_{CC} = 50 Volts — Class C Common Base					
MRF10150	M 1025–1150	150	10 ⁽⁷⁾	0.25	376B/1
MRF10350	M 1025–1150	350	9 ⁽⁷⁾	0.11	355E/1
MRF10502	M 1025–1150	500	9 ⁽⁷⁾	0.12	355J/1

Linear Transistors

The following sections describe a wide variety of devices specifically characterized for linear amplification. Included are medium power and high power parts covering frequencies to 2.0 GHz.

Table 5. UHF Ultra Linear For TV Applications

The following device has been characterized for ultra-linear applications such as low-power TV transmitters in Band IV and Band V and features diffused ballast resistors and an all-gold metal system to provide enhanced reliability and ruggedness.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Gain (Typ)/Freq. Small Signal Gain dB/MHz	θ_{JC} °C/W	Package/Style
V_{CC} = 28 Volts, Class AB					
TPV8100B	M 470–860	100 ⁽¹¹⁾	9.5/860	0.7	398/1

Table 6. Microwave Linear for PCN Applications

The following devices have been developed for linear amplifiers in the 1.5–2 GHz region and have characteristics particularly suitable for PDC, PCS or DCS1800 base station applications.

Device	Frequency Band ⁽³⁷⁾	P _{out} Watts	Class	Gain (Typ)/Freq. dB/MHz	θ_{JC} °C/W	Package/Style
V_{CC} = 26 Volts–Bipolar Die						
MRF6404 ⁽¹⁶⁾	M 1860–1900	30	AB	8.2/1880	1.4	395C/1
MRF20030R	M 2000	30	AB	11/2000	1.4	395C/1
MRF20060R	M 2000	60	AB	9.8/2000	0.7	451/1
MRF20060RS	M 2000	60	AB	9.8/2000	0.7	451A/1

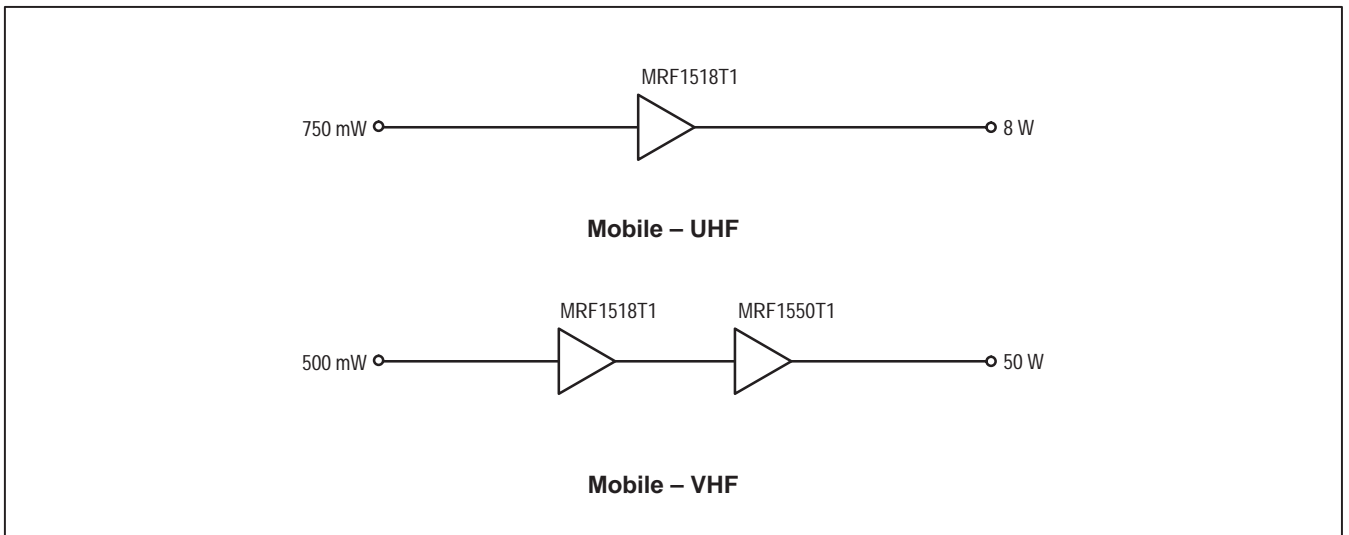
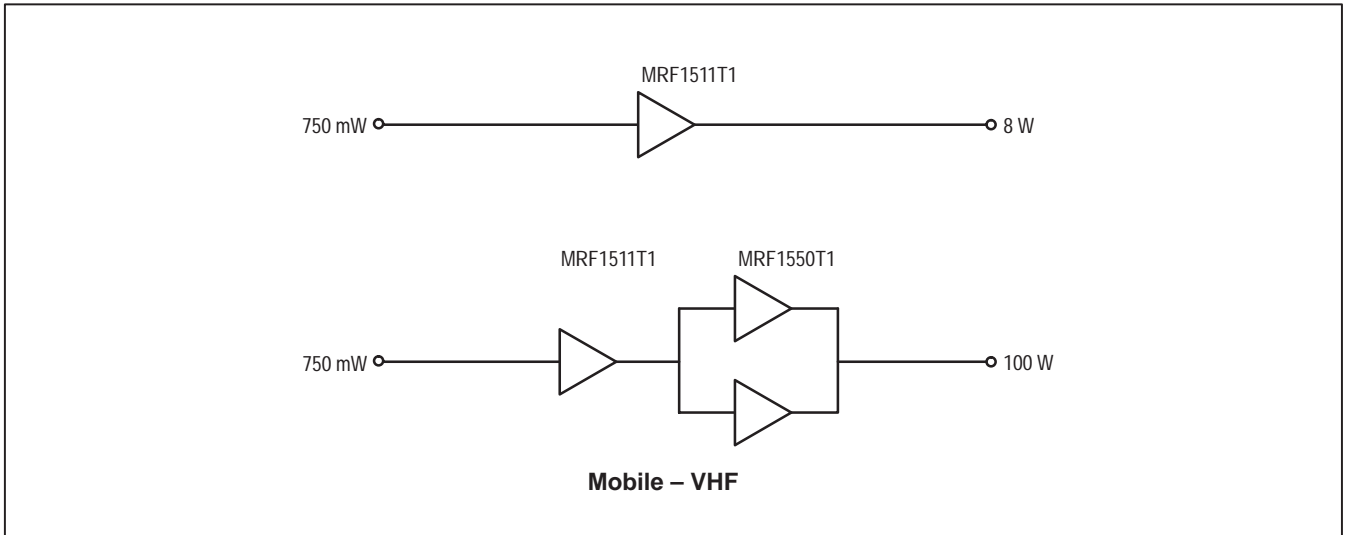
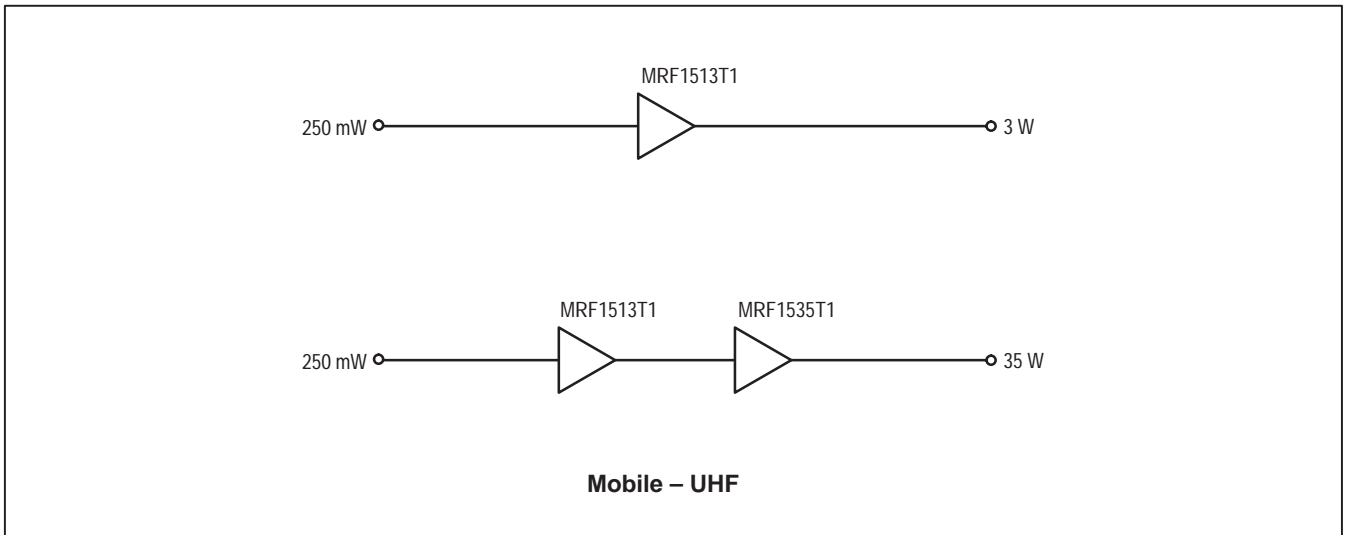
⁽⁷⁾Typical @ 1090 MHz

⁽¹¹⁾Output power at 1 dB compression in Class AB

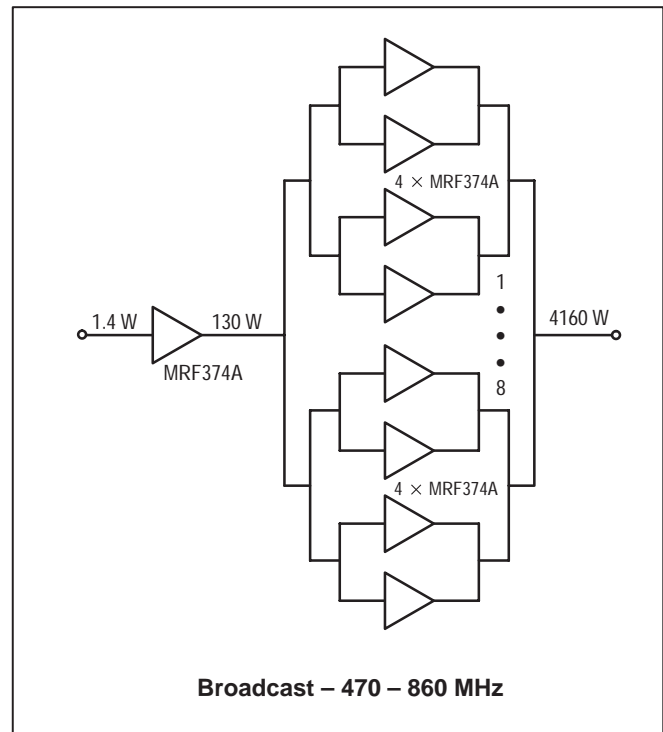
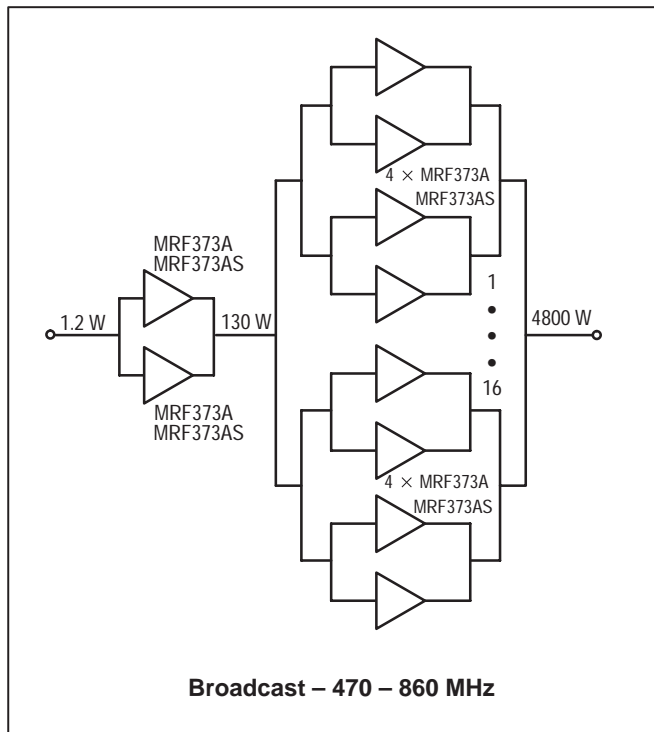
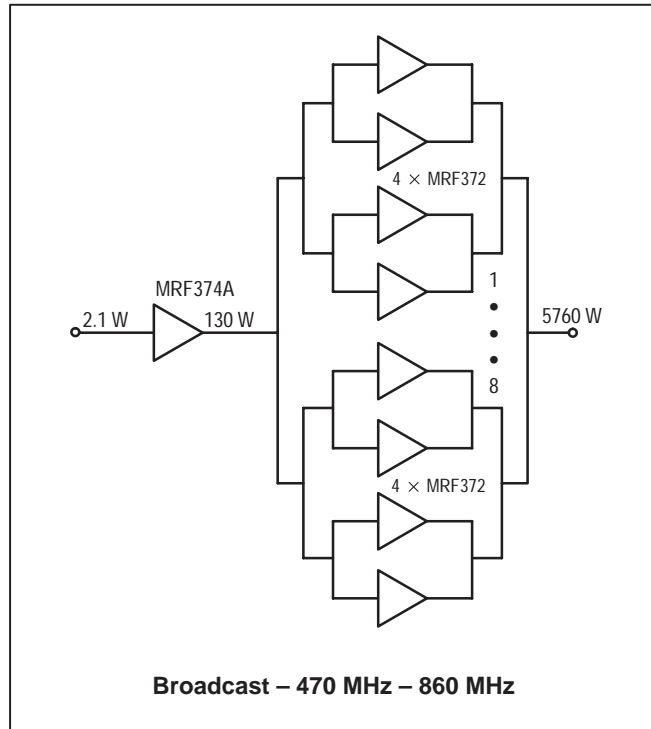
⁽¹⁶⁾Formerly known as "TP4035"

⁽³⁷⁾M = Matched Frequency Band; U = Unmatched Frequency Band.

RF LDMOS High Power Transistor Amplifier Line-ups

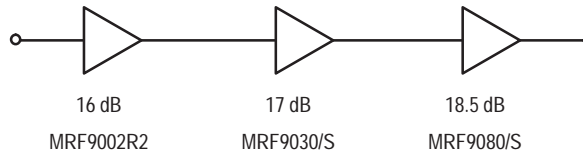


RF LDMOS High Power Transistor Amplifier Line-ups (continued)



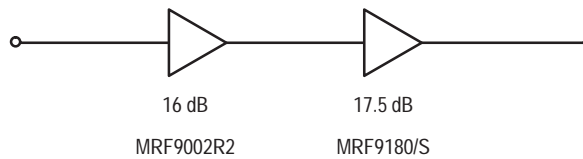
RF LDMOS High Power Transistor Amplifier Line-ups (continued)

GSM EDGE – 900 MHz



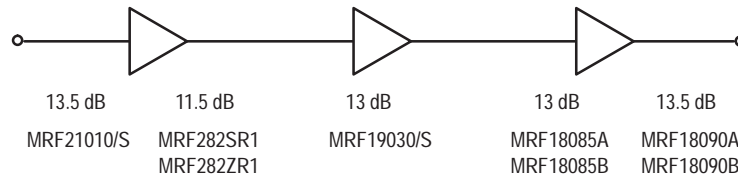
P _{in}	Amp1	Amp2	Amp3	P _{out}
0.602 mW	MRF9002R2	MRF9030/S	MRF9080/S	75 W

Cellular – 1.0 GHz



P _{in}	Amp1	Amp2	P _{out}
80 mW	MRF9002R2	MRF9180/S	170 W

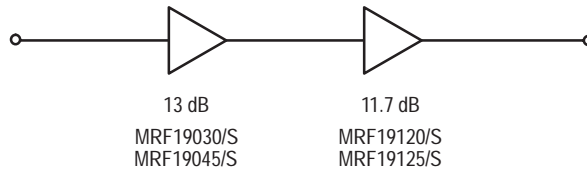
GSM1800, GSM1900, GSM EDGE and PCS TDMA – 1.8 – 1.9 GHz



P _{in}	Amp1	Amp2	Amp3	P _{out}
9.5 mW	MRF21010/S	MRF19030/S	MRF18085A	85 W
9.0 mW	MRF21010/S	MRF19030/S	MRF18090A	90 W
9.5 mW	MRF21010/S	MRF19030/S	MRF18085B	85 W
9.0 mW	MRF21010/S	MRF19030/S	MRF18090B	90 W
15 mW	MRF282SR1/ZR1	MRF19030/S	MRF18085A	85 W
14.2 mW	MRF282SR1/ZR1	MRF19030/S	MRF18090A	90 W
15 mW	MRF282SR1/ZR1	MRF19030/S	MRF18085B	85 W
14.2 mW	MRF282SR1/ZR1	MRF19030/S	MRF18090B	90 W

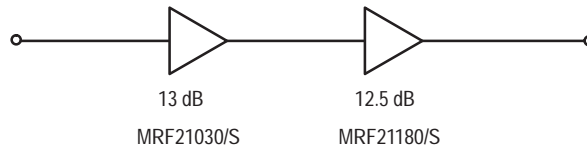
RF LDMOS High Power Transistor Amplifier Line-ups (continued)

2-CH N-CDMA – 1.9 GHz



P _{in}	Amp1	Amp2	P _{out}
406 mW	MRF19030/S	MRF19120/S	120 W
406 mW	MRF19045/S	MRF19125/S	120 W

2-CH W-CDMA, UMTS – 2.1 GHz

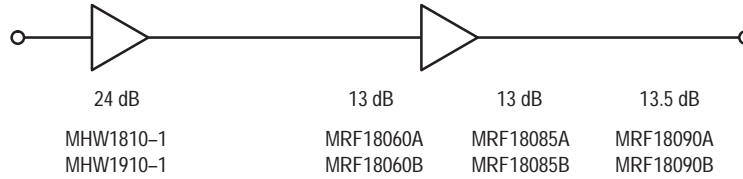


P _{in}	Amp1	Amp2	P _{out}
500 mW	MRF21030/S	MRF21180/S	180 W

RF LDMOS High Power Transistor Amplifier Line-ups (continued)

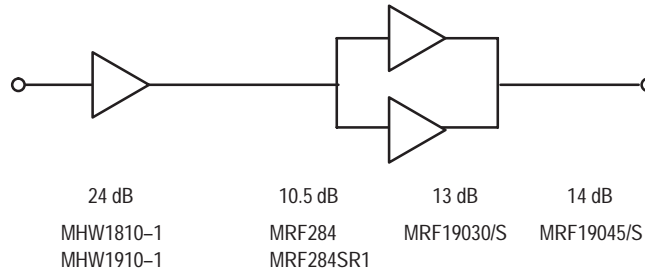
GSM1800, GSM1900 Base Station – Class 1: 30 – 90 Watts, 24 – 26 Volts

60 – 90 W Output



P _{in}	Amp1	Amp2	P _{out}
12 mW	MHW1810-1	MRF18060A	60 W
17 mW	MHW1810-1	MRF18085A	85 W
16 mW	MHW1810-1	MRF18090A	90 W
12 mW	MHW1910-1	MRF18060B	60 W
17 mW	MHW1910-1	MRF18085B	85 W
16 mW	MHW1910-1	MRF18090B	90 W

30 – 40 W Output



P _{in}	Amp1	Amp2	P _{out}
10.6 mW	MHW1810-1	MRF284/SR1	30 W
6.0 mW	MHW1810-1	MRF19030/S	30 W
7.13 mW	MHW1810-1	MRF19045/S	45 W
10.6 mW	MHW1910-1	MRF284/SR1	30 W
6.0 mW	MHW1910-1	MRF19030/S	30 W
7.13 mW	MHW1910-1	MRF19045/S	45 W

RF LDMOS High Power Transistor Amplifier Line-ups (continued)

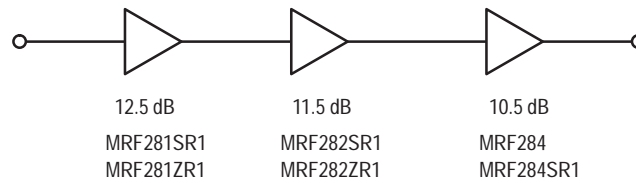
GSM1800, GSM1900 Base Station – Class 2: 30 – 45 Watts, 24 – 26 Volts

30 W Output



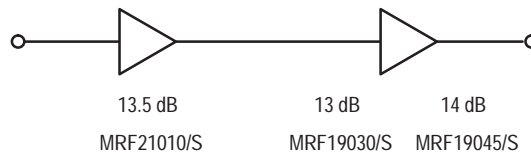
P _{in}	Amp1	Amp2	P _{out}
10.6 mW	MHW1810-1	MRF284/SR1	30 W
10.6 mW	MHW1910-1	MRF284/SR1	30 W

30 W Output



P _{in}	Amp1	Amp2	Amp3	P _{out}
10.6 mW	MRF281SR1/ZR1	MRF282SR1/ZR1	MRF284/SR1	30 W

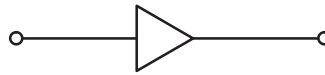
30 – 45 W Output



P _{in}	Amp1	Amp2	P _{out}
67 mW	MRF21010/S	MRF19030/S	30 W
80 mW	MRF21010/S	MRF19045/S	45 W

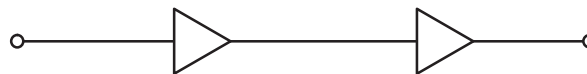
RF LDMOS High Power Transistor Amplifier Line-ups (continued)

GSM1800, GSM1900 Base Station – Class 3: 5 – 10 Watts, 24 – 26 Volts Microcell



24 dB
MHW1810-1
MHW1910-1

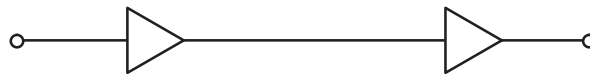
P _{in}	Amp1	P _{out}
40 mW	MHW1810-1	10 W
40 mW	MHW1910-1	10 W



12.5 dB 13.5 dB 11.5 dB
MRF281SR1 MRF21010/S MRF282SR1
MRF281ZR1 MRF282ZR1

P _{in}	Amp1	Amp2	P _{out}
25 mW	MRF281SR1/ZR1	MRF21010/S	10 W
40 mW	MRF281SR1/ZR2	MRF282SR1/ZR2	10 W

GSM900 Base Station – Class 4: 85 – 120 Watts, 24 – 26 Volts

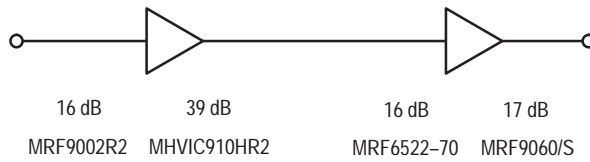


16 dB 39 dB 17.9 dB 16 dB
MRF9002R2 MHVIC910HR2 MRF9085/S MRF9120/S

P _{in}	Amp1	Amp2	P _{out}
37 mW	MRF9002R2	MRF9085/S	90 W
76 mW	MRF9002R2	MRF9120/S	120 W
0.183 mW	MHVIC910HR2	MRF9085/S	90 W
0.379 mW	MHVIC910HR2	MRF9120/S	120 W

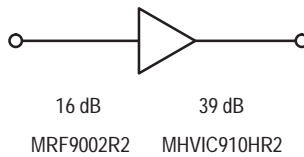
RF LDMOS High Power Transistor Amplifier Line-ups (continued)

GSM900 Base Station – Class 5: 60 – 70 Watts, 24 – 26 Volts



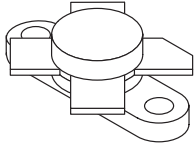
P _{in}	Amp1	Amp2	P _{out}
44 mW	MRF9002R2	MRF6522-70	70 W
30 mW	MRF9002R2	MRF9060/S	60 W
0.221 mW	MHVIC910HR2	MRF6522-70	70 W
0.151 mW	MHVIC910HR2	MRF9060/S	60 W

GSM900 Base Station – Class 7: 5 – 10 Watts, 24 – 26 Volts

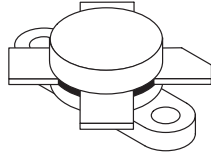


P _{in}	Amp1	P _{out}
252 mW	MRF9002R2	10 W
1.3 mW	MHVIC910HR2	10 W

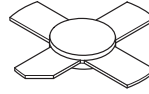
RF Power MOSFETs and Bipolar Transistors Packages



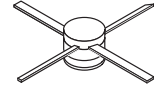
CASE 211-07
STYLE 2
(.380" FLANGE)



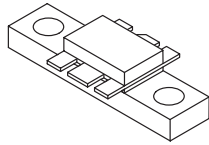
CASE 211-11
STYLE 2
(.500" FLANGE)



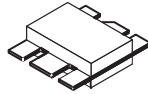
CASE 249
STYLE 3
(.280" PILL)



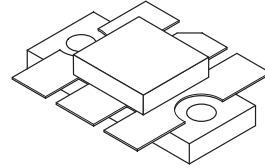
CASE 305A
STYLE 2
(.204" PILL)



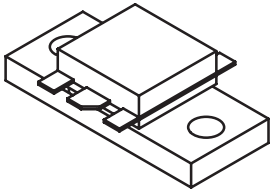
CASE 319
STYLE 2, 3
(CS-12)



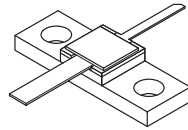
CASE 319A
STYLE 2



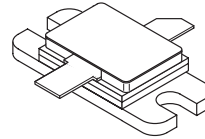
CASE 333
STYLE 2



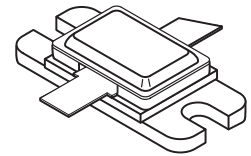
CASE 333A
STYLE 1, 2
(MAAC PAC)



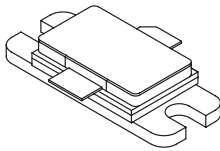
CASE 336E
STYLE 1



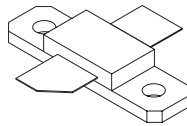
CASE 355C
STYLE 1



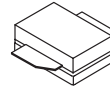
CASE 355E
STYLE 1



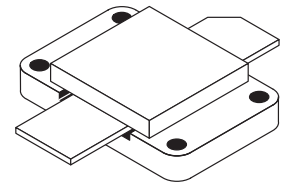
CASE 355J-02
STYLE 1



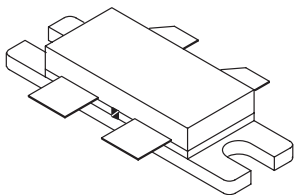
CASE 360B
STYLE 1
(Micro 250)



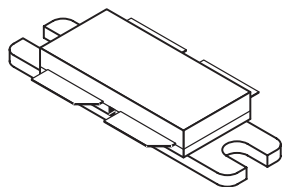
CASE 360C
STYLE 1
(Micro 250S)



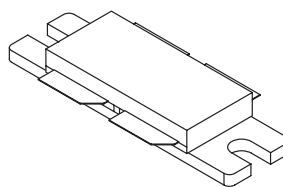
CASE 368
STYLE 2
(HOG PAC)



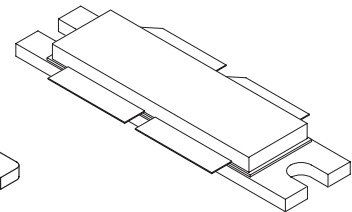
CASE 375
STYLE 2



CASE 375A
STYLE 1

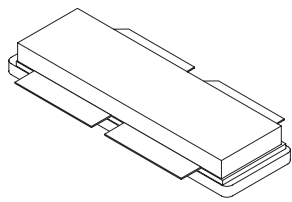


CASE 375B
STYLE 2
(Micro 860)

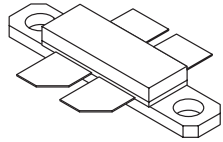


CASE 375D
STYLE 2

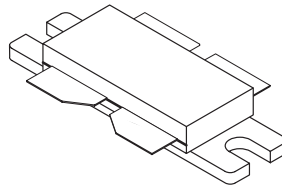
SCALE 1:1



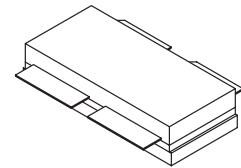
CASE 375E
STYLE 2



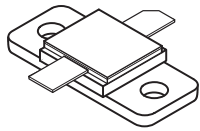
CASE 375F
STYLE 2



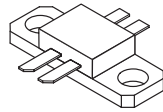
CASE 375G
STYLE 2



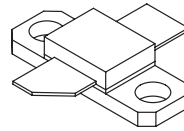
CASE 375H
STYLE 2



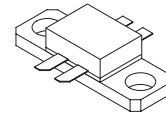
CASE 376B
STYLE 1



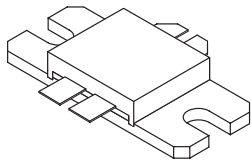
CASE 395B
STYLE 1



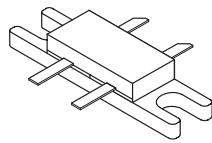
CASE 395C
STYLE 1, 2



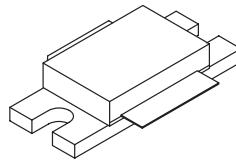
CASE 395E
STYLE 1



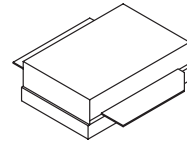
CASE 398
STYLE 1



CASE 412
STYLE 1



CASE 451
STYLE 1



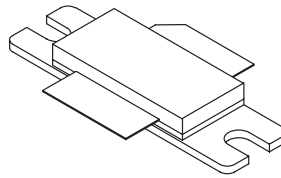
CASE 451A
STYLE 1



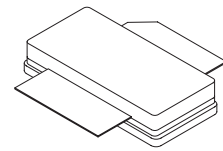
CASE 458B
STYLE 1
(Micro 200S)



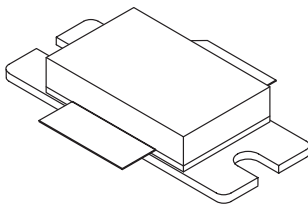
CASE 458C
STYLE 1
(Micro 200Z)



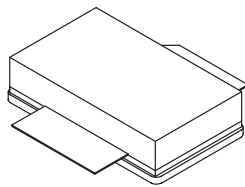
CASE 465
STYLE 1



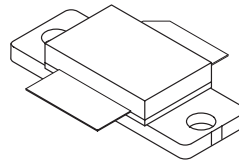
CASE 465A
STYLE 1



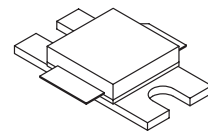
CASE 465B
STYLE 1



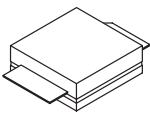
CASE 465C
STYLE 1



CASE 465D
STYLE 1



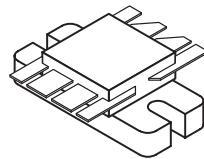
CASE 465E
STYLE 1



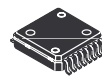
CASE 465F
STYLE 1



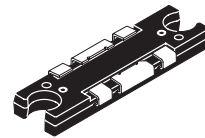
CASE 466
STYLE 1
PLASTIC
(PLD 1.5)



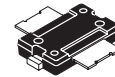
CASE 744A
STYLE 1, 2



CASE 978



CASE 1264
PLASTIC
(TO-272)
STYLE 1



CASE 1265
PLASTIC
(TO-270)
STYLE 1

SCALE 1:1

Section Two

Motorola RF Discrete Transistors – Data Sheets

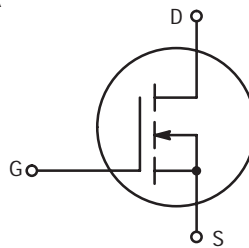
Device Number	Page Number	Device Number	Page Number
MRF134	5.2-3	MRF373	5.2-258
MRF136	5.2-12	MRF373S	5.2-258
MRF141	5.2-22	MRF374	5.2-267
MRF141G	5.2-31	MRF392	5.2-275
MRF148A	5.2-39	MRF393	5.2-278
MRF150	5.2-44	MRF858S	5.2-281
MRF151	5.2-51	MRF897	5.2-286
MRF151G	5.2-58	MRF897R	5.2-290
MRF154	5.2-66	MRF898	5.2-295
MRF157	5.2-72	MRF899	5.2-298
MRF158	5.2-78	MRF1511T1	5.2-303
MRF160	5.2-93	MRF1513T1	5.2-313
MRF166C	5.2-101	MRF1517T1	5.2-325
MRF166W	5.2-109	MRF1518T1	5.2-337
MRF171A	5.2-118	MRF1535T1	5.2-349
MRF173	5.2-129	MRF1550T1	5.2-359
MRF174	5.2-136	MRF6404	5.2-368
MRF177	5.2-144	MRF6409	5.2-377
MRF181SR1, MRF181ZR1	5.2-152	MRF6414	5.2-382
MRF182	5.2-160	MRF6522-10R1	5.2-387
MRF182S	5.2-160	MRF6522-70	5.2-394
MRF182SR1	5.2-160	MRF6522-70R3	5.2-394
MRF183	5.2-166	MRF9045	5.2-401
MRF183S	5.2-166	MRF9045S	5.2-401
MRF183SR1	5.2-166	MRF9045SR1	5.2-401
MRF184	5.2-175	MRF9045MR1	5.2-408
MRF184S	5.2-175	MRF9080	5.2-414
MRF184SR1	5.2-175	MRF9080S	5.2-414
MRF185	5.2-183	MRF9085	5.2-420
MRF186	5.2-185	MRF9085S	5.2-420
MRF187	5.2-192	MRF9180	5.2-426
MRF187S	5.2-192	MRF9180S	5.2-426
MRF275G	5.2-198	MRF10005	5.2-434
MRF275L	5.2-213	MRF10031	5.2-437
MRF281SR1, MRF281ZR1	5.2-225	MRF10120	5.2-440
MRF282SR1, MRF282ZR1	5.2-229	MRF10150	5.2-443
MRF284	5.2-236	MRF10350	5.2-446
MRF284SR1	5.2-236	MRF10502	5.2-449
MRF372	5.2-247	MRF16006	5.2-452

Device Number	Page Number	Device Number	Page Number
MRF16030	5.2-456	MRF19125S	5.2-516
MRF18060A	5.2-460	MRF20030R	5.2-524
MRF18060AS	5.2-460	MRF20060R	5.2-531
MRF18060B	5.2-466	MRF20060RS	5.2-531
MRF18060BS	5.2-466	MRF21010	5.2-538
MRF18090A	5.2-472	MRF21030	5.2-543
MRF18090AS	5.2-472	MRF21030S	5.2-543
MRF18090B	5.2-478	MRF21045	5.2-548
MRF18090BS	5.2-478	MRF21045S	5.2-548
MRF19030	5.2-484	MRF21060	5.2-556
MRF19030S	5.2-484	MRF21060S	5.2-556
MRF19060	5.2-489	MRF21085	5.2-562
MRF19060S	5.2-489	MRF21085S	5.2-562
MRF19085	5.2-495	MRF21090	5.2-570
MRF19085S	5.2-495	MRF21090S	5.2-570
MRF19090	5.2-503	MRF21120	5.2-575
MRF19090S	5.2-503	MRF21120S	5.2-575
MRF19120	5.2-509	MRF21125	5.2-582
MRF19120S	5.2-509	MRF21125S	5.2-582
MRF19125	5.2-516	TPV8100B	5.2-589

The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode

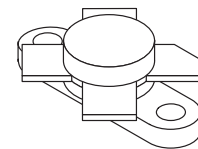
. . . designed for wideband large-signal amplifier and oscillator applications up to 400 MHz range.

- Guaranteed 28 Volt, 150 MHz Performance
Output Power = 5.0 Watts
Minimum Gain = 11 dB
Efficiency — 55% (Typical)
- Small-Signal and Large-Signal Characterization
- Typical Performance at 400 MHz, 28 Vdc, 5.0 W
Output = 10.6 dB Gain
- 100% Tested For Load Mismatch At All Phase Angles
With 30:1 VSWR
- Low Noise Figure — 2.0 dB (Typ) at 200 mA, 150 MHz
- Excellent Thermal Stability, Ideally Suited For Class A Operation



MRF134

5.0 W, to 400 MHz
N-CHANNEL MOS
BROADBAND RF POWER
FET



CASE 211-07, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1.0 M\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	0.9	Adc
Total Device Dissipation @ $T_C = 25^\circ C$ Derate above $25^\circ C$	P_D	17.5 0.1	Watts W/ $^\circ C$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ C$

THERMAL CHARACTERISTICS

Rating	Symbol	Value	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	10	$^\circ C/W$

Handling and Packaging — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 5.0\text{ mA}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	1.0	mAdc
Gate–Source Leakage Current ($V_{GS} = 20\text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS

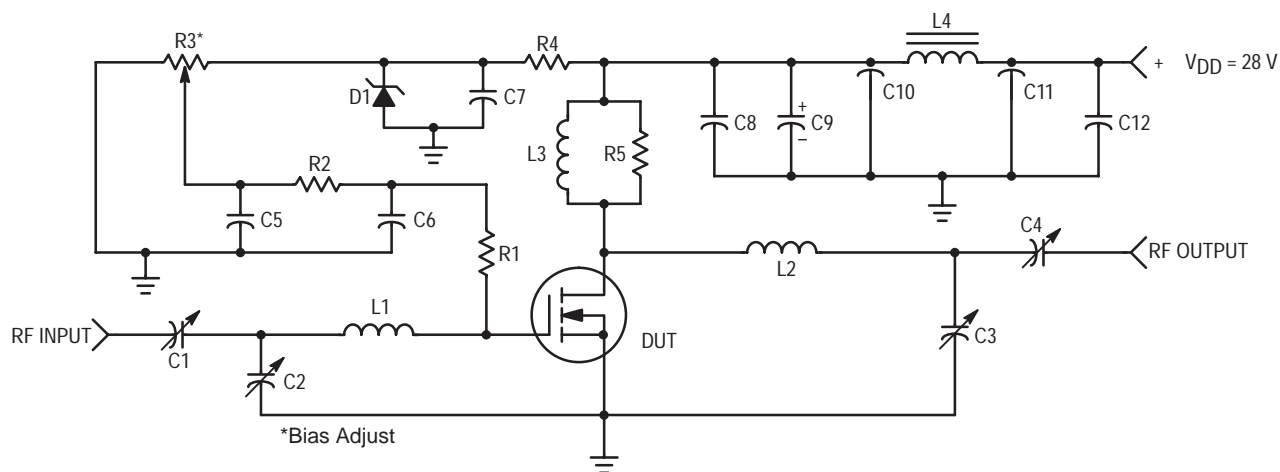
Gate Threshold Voltage ($I_D = 10\text{ mA}, V_{DS} = 10\text{ V}$)	$V_{GS(th)}$	1.0	3.5	6.0	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}, I_D = 100\text{ mA}$)	g_{fs}	80	110	—	mmhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{iss}	—	7.0	—	pF
Output Capacitance ($V_{DS} = 28\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{oss}	—	9.7	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{rss}	—	2.3	—	pF

FUNCTIONAL CHARACTERISTICS

Noise Figure ($V_{DS} = 28\text{ Vdc}, I_D = 200\text{ mA}, f = 150\text{ MHz}$)	NF	—	2.0	—	dB
Common Source Power Gain ($V_{DD} = 28\text{ Vdc}, P_{out} = 5.0\text{ W}, I_{DQ} = 50\text{ mA}$) $f = 150\text{ MHz}$ (Fig. 1) $f = 400\text{ MHz}$ (Fig. 14)	G_{ps}	11	14	—	dB
Drain Efficiency (Fig. 1) ($V_{DD} = 28\text{ Vdc}, P_{out} = 5.0\text{ W}, f = 150\text{ MHz}, I_{DQ} = 50\text{ mA}$)	η	50	55	—	%
Electrical Ruggedness (Fig. 1) ($V_{DD} = 28\text{ Vdc}, P_{out} = 5.0\text{ W}, f = 150\text{ MHz}, I_{DQ} = 50\text{ mA},$ $VSWR\ 30:1$ at all Phase Angles)	ψ	No Degradation in Output Power			



- C1, C4 — Arco 406, 15–115 pF
- C2 — Arco 403, 3.0–35 pF
- C3 — Arco 402, 1.5–20 pF
- C5, C6, C7, C8, C12 — 0.1 μF Erie Redcap
- C9 — 10 μF , 50 V
- C10, C11 — 680 pF Feedthru
- D1 — 1N5925A Motorola Zener
- L1 — 3 Turns, 0.310" ID, #18 AWG Enamel, 0.2" Long
- L2 — 3–1/2 Turns, 0.310" ID, #18 AWG Enamel, 0.25" Long

- L3 — 20 Turns, #20 AWG Enamel Wound on R5
- L4 — Ferroxcube VK–200 — 19/4B
- R1 — 68 Ω , 1.0 W Thin Film
- R2 — 10 k Ω , 1/4 W
- R3 — 10 Turns, 10 k Ω Beckman Instruments 8108
- R4 — 1.8 k Ω , 1/2 W
- R5 — 1.0 M Ω , 2.0 W Carbon
- Board — G10, 62 mils

Figure 1. 150 MHz Test Circuit

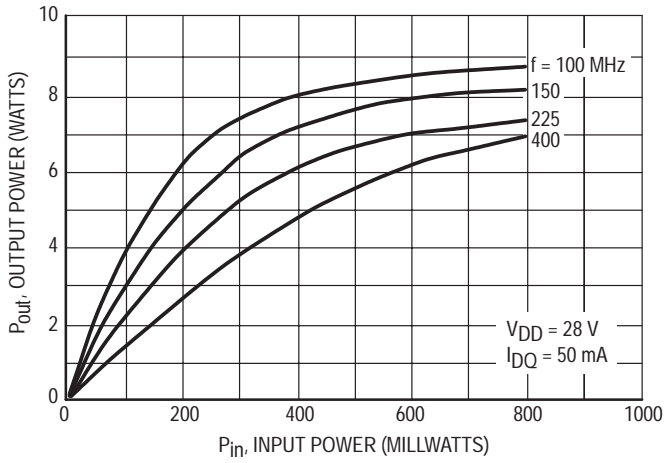


Figure 2. Output Power versus Input Power

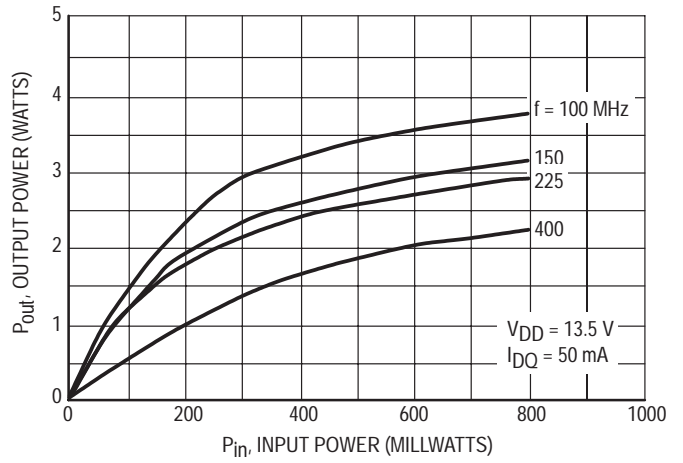


Figure 3. Output Power versus Input Power

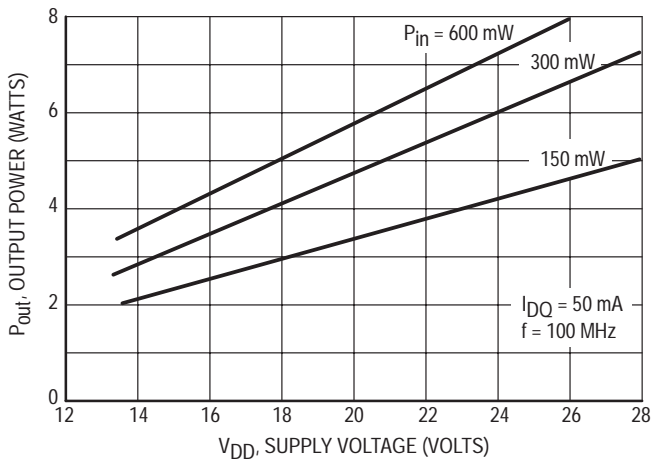


Figure 4. Output Power versus Supply Voltage

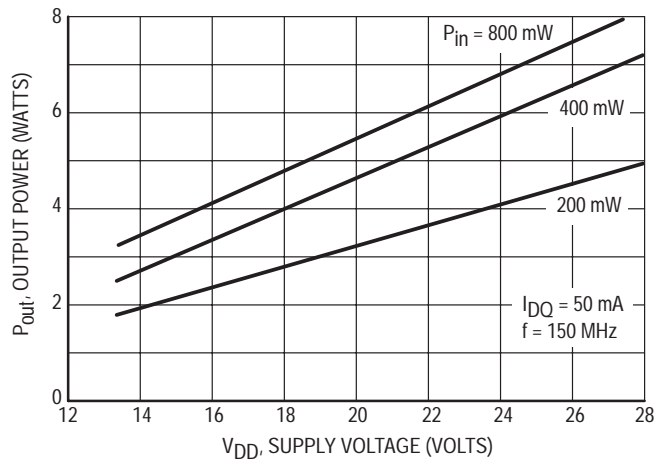


Figure 5. Output Power versus Supply Voltage

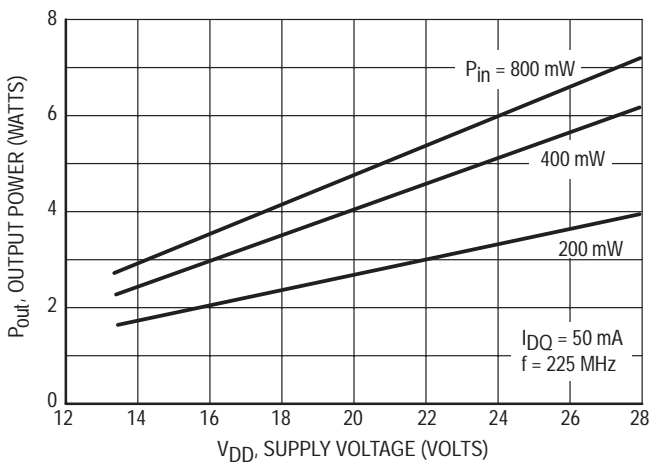


Figure 6. Output Power versus Supply Voltage

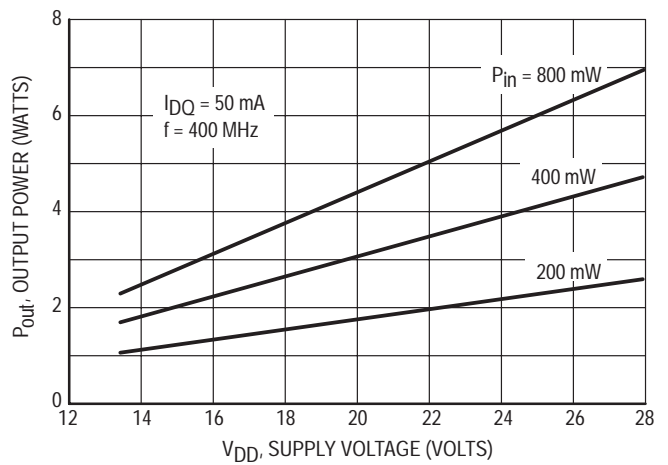


Figure 7. Output Power versus Supply Voltage

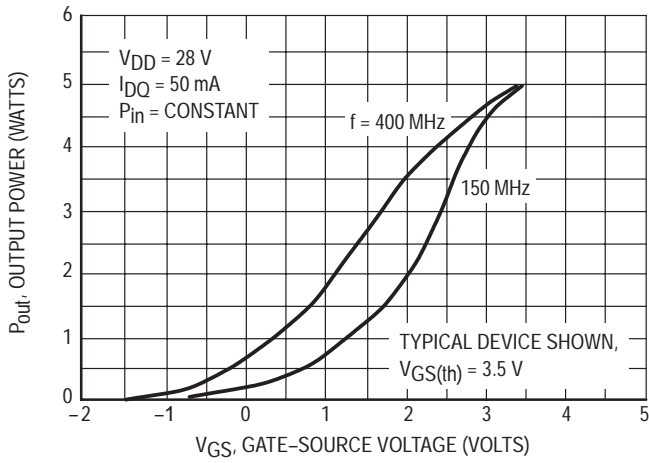


Figure 8. Output Power versus Gate Voltage

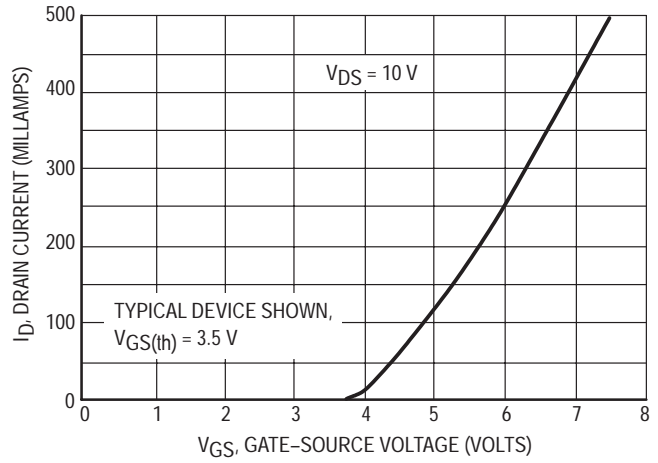


Figure 9. Drain Current versus Gate Voltage (Transfer Characteristics)

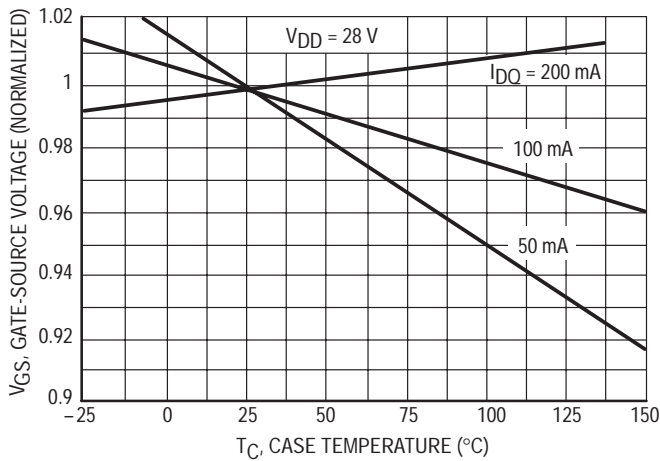


Figure 10. Gate-Source Voltage versus Case Temperature

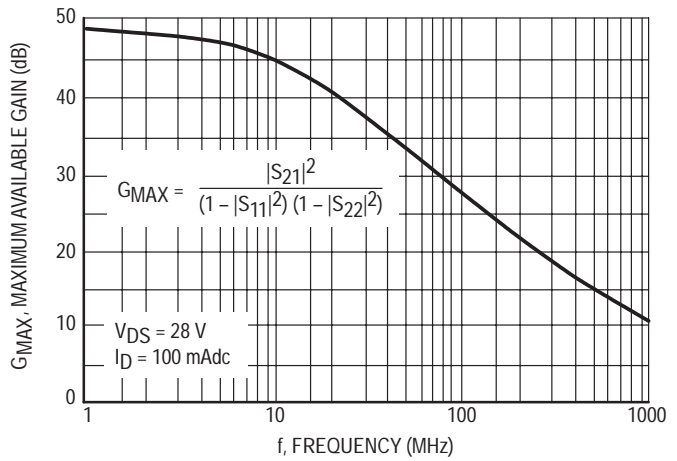


Figure 11. Maximum Available Gain versus Frequency

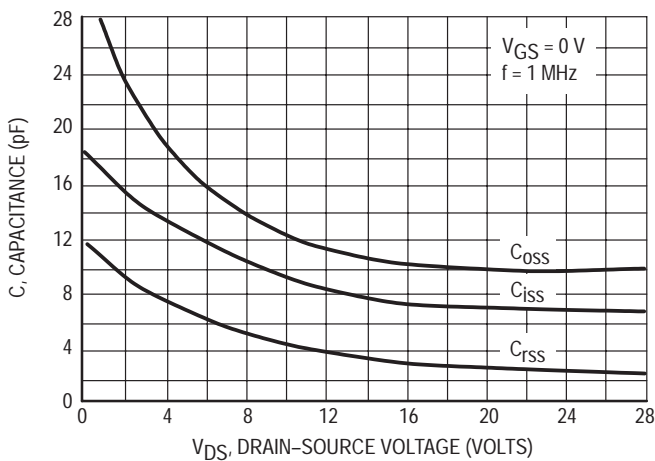


Figure 12. Capacitance versus Voltage

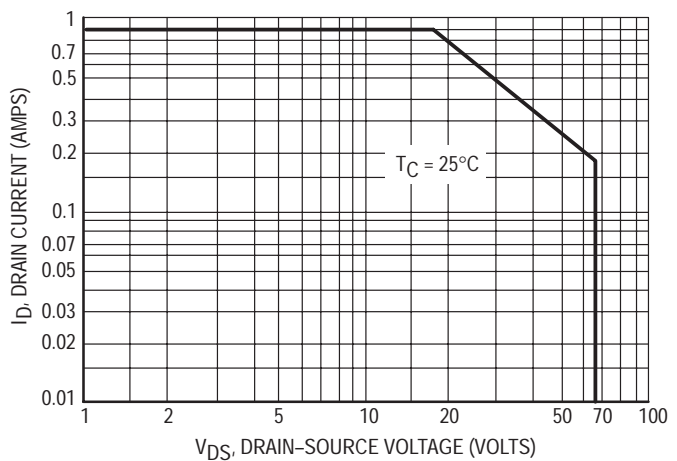
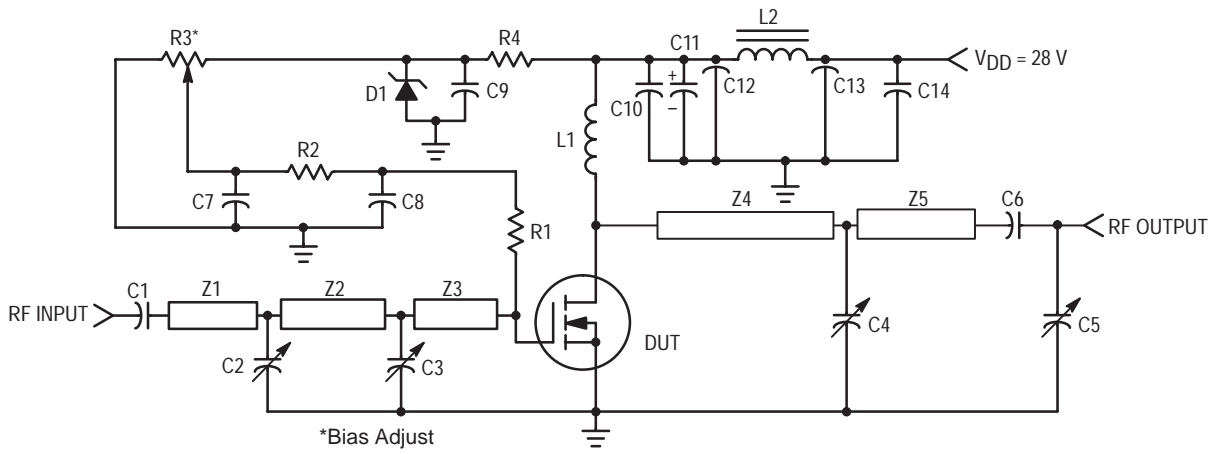


Figure 13. Maximum Rated Forward Biased Safe Operating Area



C1, C6 — 270 pF, ATC 100 mils
 C2, C3, C4, C5 — 0–20 pF Johanson
 C7, C9, C10, C14 — 0.1 μ F Erie Redcap, 50 V
 C8 — 0.001 μ F
 C11 — 10 μ F, 50 V
 C12, C13 — 680 pF Feedthru
 D1 — 1N5925A Motorola Zener
 L1 — 6 Turns, 1/4" ID, #20 AWG Enamel
 L2 — Ferroxcube VK-200 — 19/4B
 R1 — 68 Ω , 1.0 W Thin Film

R2 — 10 k Ω , 1/4 W
 R3 — 10 Turns, 10 k Ω Beckman Instruments 8108
 R4 — 1.8 k Ω , 1/2 W
 Z1 — 1.4" x 0.166" Microstrip
 Z2 — 1.1" x 0.166" Microstrip
 Z3 — 0.95" x 0.166" Microstrip
 Z4 — 2.2" x 0.166" Microstrip
 Z5 — 0.85" x 0.166" Microstrip
 Board — Glass Teflon, 62 mils

Figure 14. 400 MHz Test Circuit

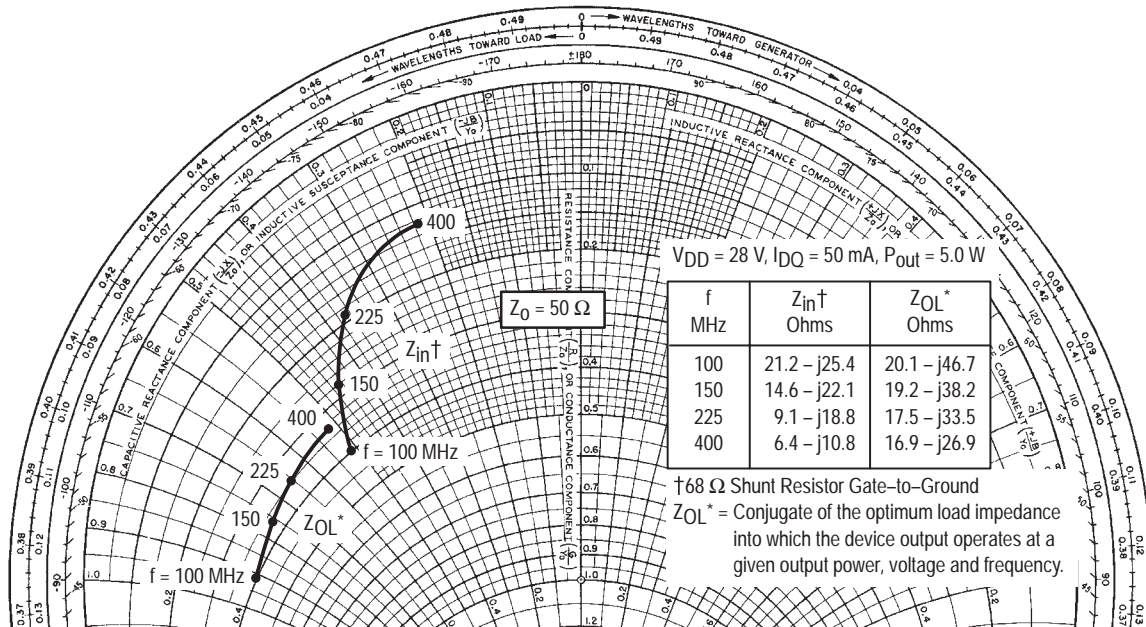


Figure 15. Large-Signal Series Equivalent Input/Output Impedances, Z_{in}[†], Z_{OL}^{*}

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
1.0	0.989	-1.0	11.27	179	0.0014	89	0.954	-1.0
2.0	0.989	-2.0	11.27	179	0.0028	89	0.954	-2.0
5.0	0.988	-5.0	11.26	176	0.0069	86	0.954	-4.0
10	0.985	-10	11.20	173	0.014	83	0.951	-9.0
20	0.977	-20	10.99	166	0.027	76	0.938	-18
30	0.965	-30	10.66	159	0.039	69	0.918	-26
40	0.950	-39	10.25	153	0.051	63	0.895	-34
50	0.931	-47	9.777	147	0.060	57	0.867	-42
60	0.912	-53	9.359	142	0.069	53	0.846	-49
70	0.892	-58	8.960	138	0.077	49	0.828	-56
80	0.874	-62	8.583	135	0.085	46	0.815	-62
90	0.855	-66	8.190	131	0.091	43	0.801	-68
100	0.833	-70	7.808	128	0.096	40	0.785	-74
110	0.827	-73	7.661	125	0.101	38	0.784	-77
120	0.821	-76	7.515	122	0.107	36	0.784	-82
130	0.814	-79	7.368	119	0.113	34	0.784	-85
140	0.808	-82	7.222	116	0.119	32	0.783	-88
150	0.802	-86	7.075	114	0.125	31	0.783	-90
160	0.788	-89	6.810	112	0.127	30	0.780	-92
170	0.774	-92	6.540	110	0.128	28	0.774	-94
180	0.763	-94	6.220	108	0.130	26	0.762	-98
190	0.751	-97	5.903	106	0.132	24	0.760	-100
200	0.740	-100	5.784	104	0.134	23	0.758	-103
225	0.719	-104	5.334	100	0.136	20	0.757	-107
250	0.704	-108	4.904	97	0.139	19	0.758	-110
275	0.687	-113	4.551	92	0.141	16	0.757	-114
300	0.673	-117	4.219	89	0.141	14	0.750	-117
325	0.668	-120	3.978	86	0.142	12	0.757	-120
350	0.669	-123	3.737	83	0.142	10	0.766	-121
375	0.662	-125	3.519	80	0.143	9.0	0.768	-123
400	0.654	-127	3.325	77	0.142	8.0	0.772	-124
425	0.650	-129	3.170	75	0.140	7.0	0.772	-125
450	0.638	-131	3.048	72	0.141	6.0	0.783	-125
475	0.614	-132	2.898	71	0.136	6.0	0.786	-126
500	0.641	-133	2.833	68	0.136	5.0	0.795	-127
525	0.638	-135	2.709	66	0.135	5.0	0.801	-127
550	0.633	-137	2.574	64	0.133	4.0	0.802	-128
575	0.628	-138	2.481	62	0.131	5.0	0.805	-128
600	0.625	-140	2.408	60	0.129	5.0	0.814	-128

The Power RF characterization data were measured with a 68 ohm resistor shunting the MRF134 input port.
The scattering parameters were measured on the MRF134 device alone with no external components.

(continued)

Table 1. Common Source Scattering Parameters
V_{DS} = 28 V, I_D = 100 mA

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
625	0.619	-142	2.334	58	0.128	5.0	0.818	-129
650	0.617	-144	2.259	56	0.125	6.0	0.824	-130
675	0.618	-146	2.192	55	0.123	7.0	0.834	-130
700	0.619	-147	2.124	53	0.122	8.0	0.851	-131
725	0.618	-150	2.061	51	0.120	9.0	0.859	-132
750	0.614	-152	1.983	49	0.118	11	0.857	-133
775	0.609	-154	1.908	48	0.119	13	0.865	-133
800	0.562	-155	1.877	49	0.118	15	0.872	-133
825	0.587	-156	1.869	46	0.119	16	0.869	-134
850	0.593	-158	1.794	44	0.118	18	0.875	-135
875	0.597	-160	1.749	43	0.119	18	0.881	-135
900	0.598	-162	1.700	41	0.118	18	0.889	-136
925	0.592	-164	1.641	40	0.115	18	0.888	-138
950	0.588	-166	1.590	39	0.112	20	0.877	-138
975	0.586	-168	1.572	39	0.108	23	0.864	-137
1000	0.590	-171	1.551	37	0.107	28	0.863	-137

The Power RF characterization data were measured with a 68 ohm resistor shunting the MRF134 input port. The scattering parameters were measured on the MRF134 device alone with no external components.

Table 1. Common Source Scattering Parameters (continued)
V_{DS} = 28 V, I_D = 100 mA

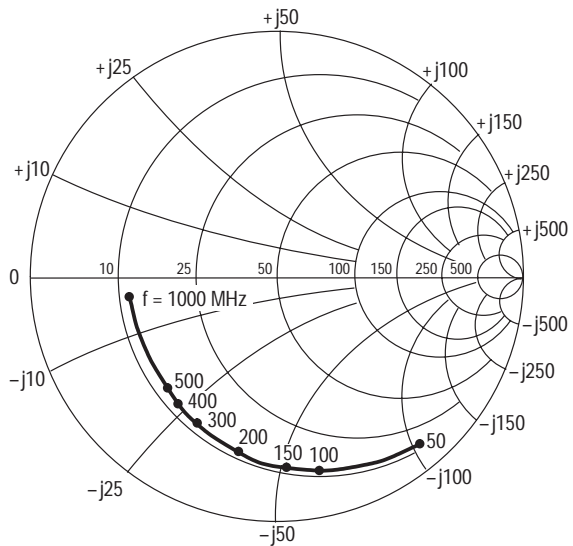


Figure 16. S₁₁, Input Reflection Coefficient versus Frequency
V_{DS} = 28 V I_D = 100 mA

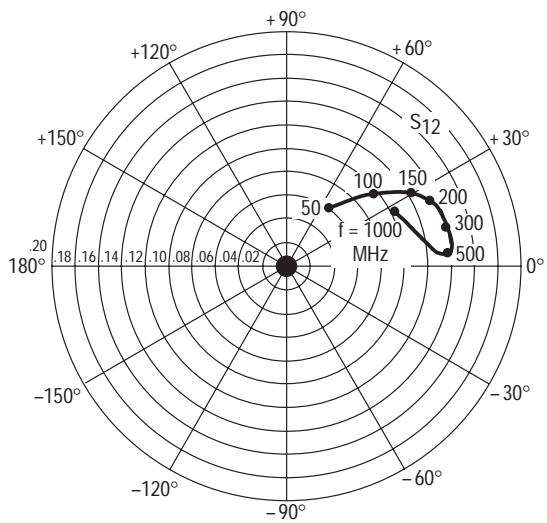


Figure 17. S₁₂, Reverse Transmission Coefficient versus Frequency
V_{DS} = 28 V I_D = 100 mA

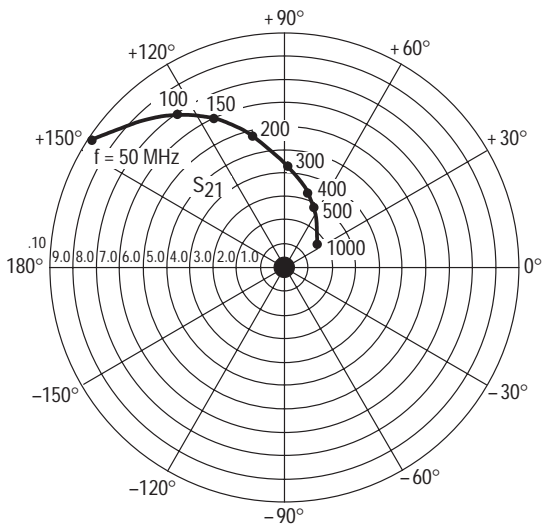


Figure 18. S₂₁, Forward Transmission Coefficient versus Frequency
V_{DS} = 28 V I_D = 100 mA

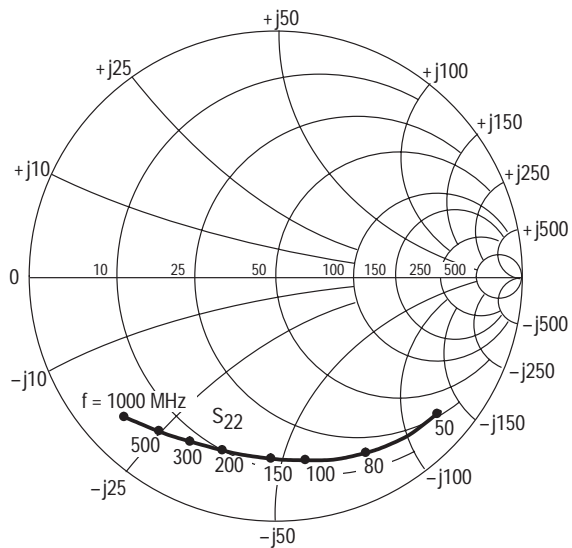


Figure 19. S₂₂, Output Reflection Coefficient versus Frequency
V_{DS} = 28 V I_D = 100 mA

DESIGN CONSIDERATIONS

The MRF134 is a RF power N-Channel enhancement mode field-effect transistor (FET) designed especially for VHF power amplifier and oscillator applications. Motorola RF MOS FETs feature a vertical structure with a planar design, thus avoiding the processing difficulties associated with V-groove vertical power FETs.

Motorola Application Note AN-211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power FETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal, thus facilitating manual gain control, ALC and modulation.

DC BIAS

The MRF134 is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. See Figure 9 for a typical plot of drain current versus gate voltage. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF134 was characterized at $I_{DQ} = 50$ mA, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of the MRF134 may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems. (See Figure 8.)

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar VHF transistors are suitable for MRF134. See Motorola Application Note AN721, Impedance Matching Networks Applied to RF Power Transistors. The higher input impedance of RF MOS FETs helps ease the task of broadband network design. Both small signal scattering parameters and large signal impedances are provided. While the s-parameters will not produce an exact design solution for high power operation, they do yield a good first approximation. This is an additional advantage of RF MOS power FETs.

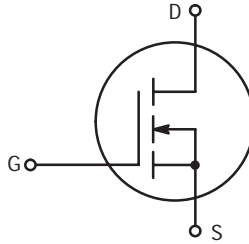
RF power FETs are triode devices and, therefore, not unilateral. This, coupled with the very high gain of the MRF134, yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The MRF134 was characterized with a 68-ohm input shunt loading resistor. Two port parameter stability analysis with the MRF134 s-parameters provides a useful-tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A for a discussion of two port network theory and stability.

Input resistive loading is not feasible in low noise applications. The MRF134 noise figure data was generated in a circuit with drain loading and a low loss input network.

The RF MOSFET Line
RF Power
Field-Effect Transistors
N-Channel Enhancement-Mode MOSFET

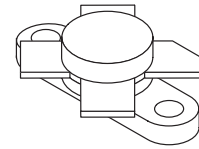
Designed for wideband large-signal amplifier and oscillator applications up to 400 MHz range, in single ended configuration.

- Guaranteed 28 Volt, 150 MHz Performance
Output Power = 15 Watts
Narrowband Gain = 16 dB (Typ)
Efficiency = 60% (Typical)
- Small-Signal and Large-Signal Characterization
- 100% Tested For Load Mismatch At All Phase Angles With 30:1 VSWR
- Excellent Thermal Stability, Ideally Suited For Class A Operation
- Facilitates Manual Gain Control, ALC and Modulation Techniques



MRF136

15 W, to 400 MHz
N-CHANNEL
MOS BROADBAND
RF POWER FET



CASE 211-07, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1.0 \text{ M}\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	2.5	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	55 0.314	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	3.2	$^\circ\text{C/W}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS (1)

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 5.0 \text{ mA}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero–Gate Voltage Drain Current ($V_{DS} = 28 \text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	2.0	mAdc
Gate–Source Leakage Current ($V_{GS} = 40 \text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS (1)

Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 25 \text{ mA}$)	$V_{GS(th)}$	1.0	3.0	6.0	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 250 \text{ mA}$)	g_{fs}	250	400	—	mmhos

DYNAMIC CHARACTERISTICS (1)

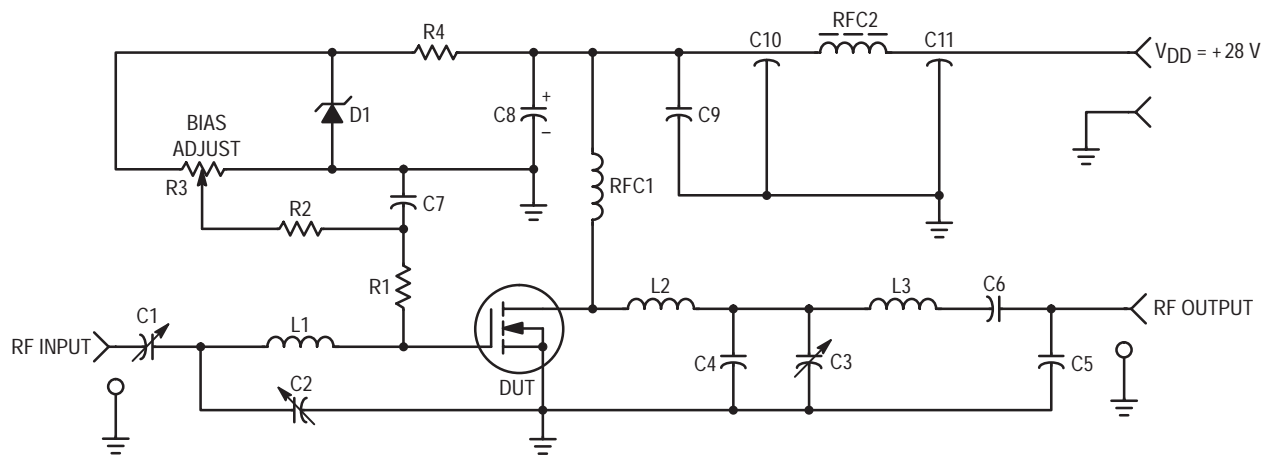
Input Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{iss}	—	24	—	pF
Output Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{oss}	—	27	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{rss}	—	5.5	—	pF

FUNCTIONAL CHARACTERISTICS

Noise Figure ($V_{DS} = 28 \text{ Vdc}, I_D = 500 \text{ mA}, f = 150 \text{ MHz}$)	NF	—	1.0	—	dB
Common Source Power Gain (Figure 1) ($V_{DD} = 28 \text{ Vdc}, P_{out} = 15 \text{ W}, f = 150 \text{ MHz}, I_{DQ} = 25 \text{ mA}$)	G_{ps}	13	16	—	dB
Drain Efficiency (Figure 1) ($V_{DD} = 28 \text{ Vdc}, P_{out} = 15 \text{ W}, f = 150 \text{ MHz}, I_{DQ} = 25 \text{ mA}$)	η	50	60	—	%
Electrical Ruggedness (Figure 1) ($V_{DD} = 28 \text{ Vdc}, P_{out} = 15 \text{ W}, f = 150 \text{ MHz}, I_{DQ} = 25 \text{ mA},$ $V_{SWR} 30:1$ at all Phase Angles)	ψ	No Degradation in Output Power			

NOTES:

- Each side measured separately.



- C1, C2 — Arco 406, 15–115 pF or Equivalent
- C3 — Arco 404, 8–60 pF or Equivalent
- C4 — 43 pF Mini–Unelco or Equivalent
- C5 — 24 pF Mini–Unelco or Equivalent
- C6 — 680 pF, 100 Mils Chip
- C7 — 0.01 μ F Ceramic
- C8 — 100 μ F, 40 V
- C9 — 0.1 μ F Ceramic
- C10, C11 — 680 pF Feedthru
- D1 — 1N5925A Motorola Zener

- L1 — 2 Turns, 0.29" ID, #18 AWG, 0.10" Long
- L2 — 2 Turns, 0.23" ID, #18 AWG, 0.10" Long
- L3 — 2–1/4 Turns, 0.29" ID, #18 AWG, 0.125" Long
- RFC1 — 20 Turns, 0.30" ID, #20 AWG Enamel Closewound
- RFC2 — Ferroxcube VK–200 — 19/4B
- R1 — 27 Ω , 1 W Thin Film
- R2 — 10 k Ω , 1/4 W
- R3 — 10 Turns, 10 k Ω
- R4 — 1.8 k Ω , 1/2 W
- Board Material — 0.062" G10, 1 oz. Cu Clad, Double Sided

Figure 1. 150 MHz Test Circuit

TYPICAL CHARACTERISTICS

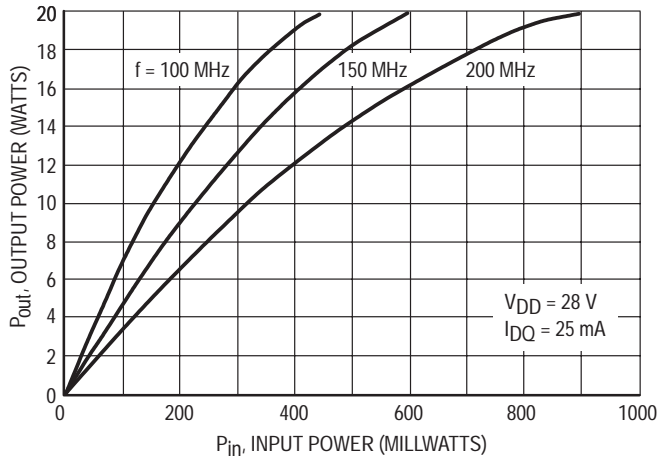


Figure 2. Output Power versus Input Power

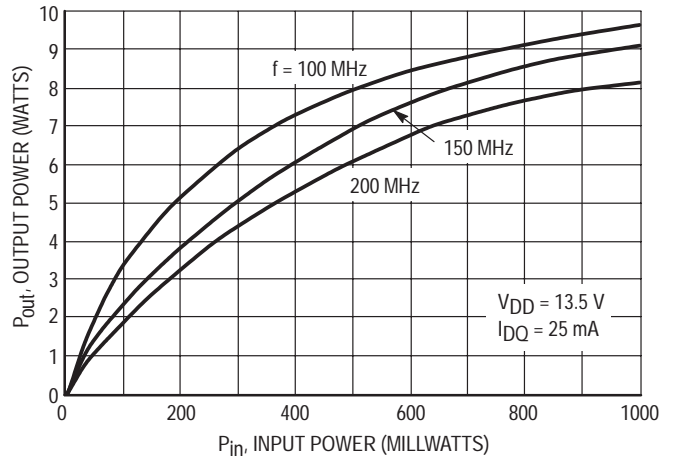


Figure 3. Output Power versus Input Power

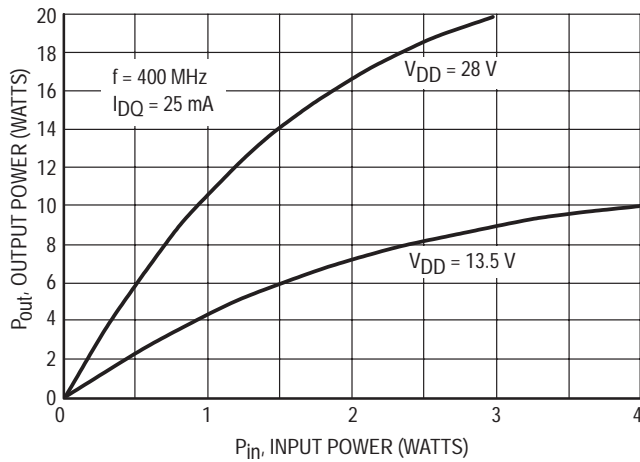


Figure 4. Output Power versus Input Power

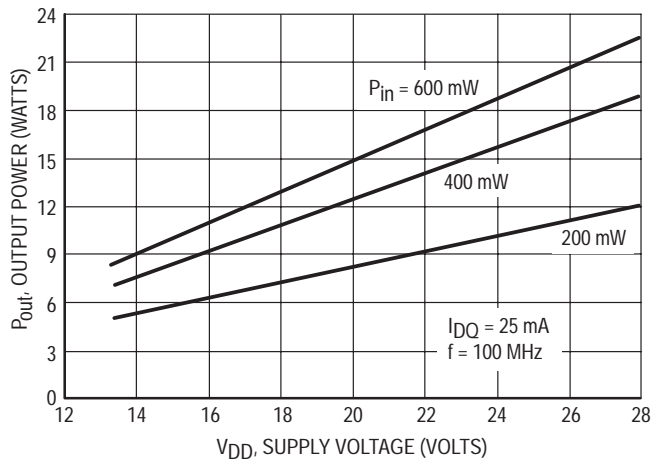


Figure 5. Output Power versus Supply Voltage

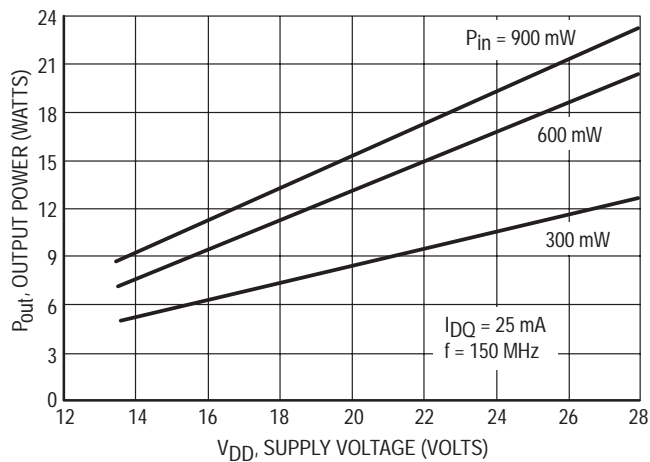


Figure 6. Output Power versus Supply Voltage

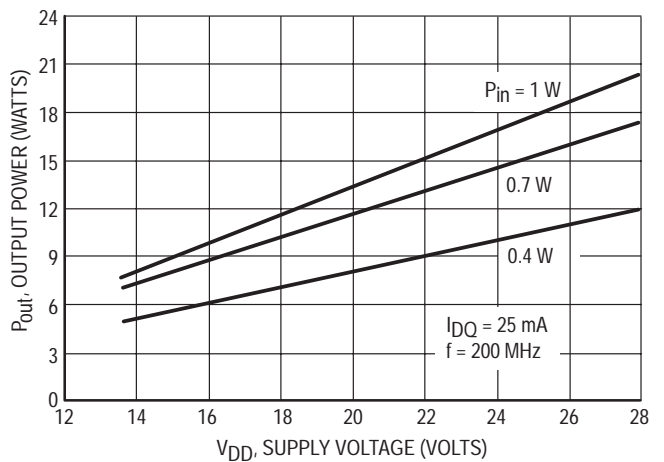


Figure 7. Output Power versus Supply Voltage

TYPICAL CHARACTERISTICS

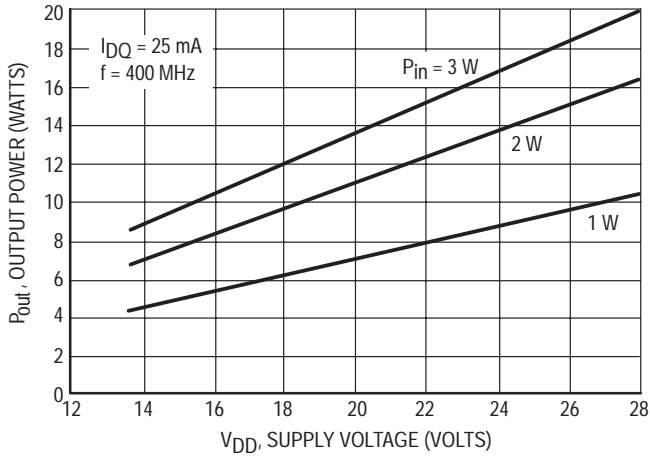


Figure 8. Output Power versus Supply Voltage

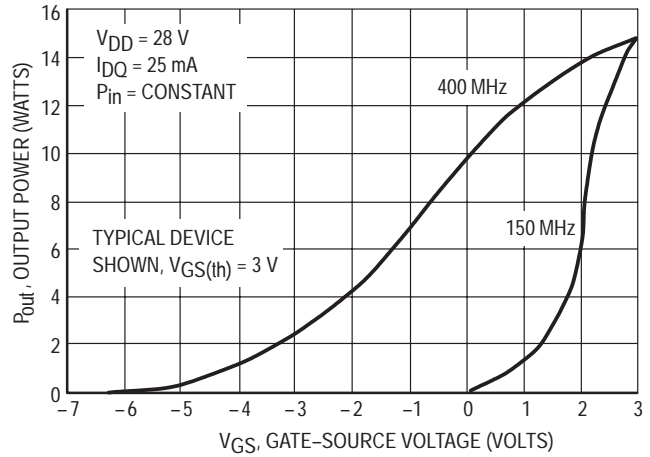


Figure 9. Output Power versus Gate Voltage

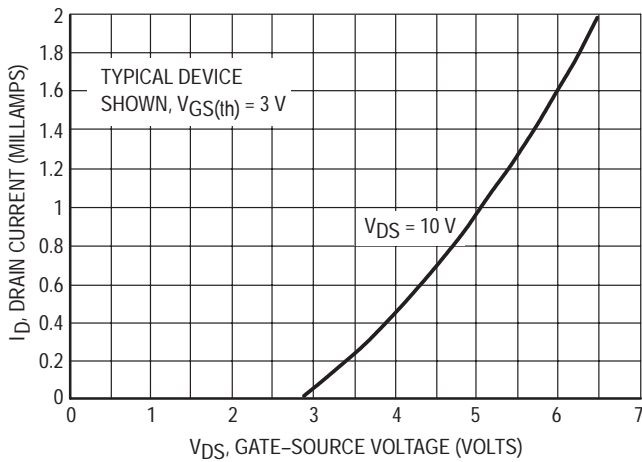


Figure 10. Drain Current versus Gate Voltage (Transfer Characteristics)

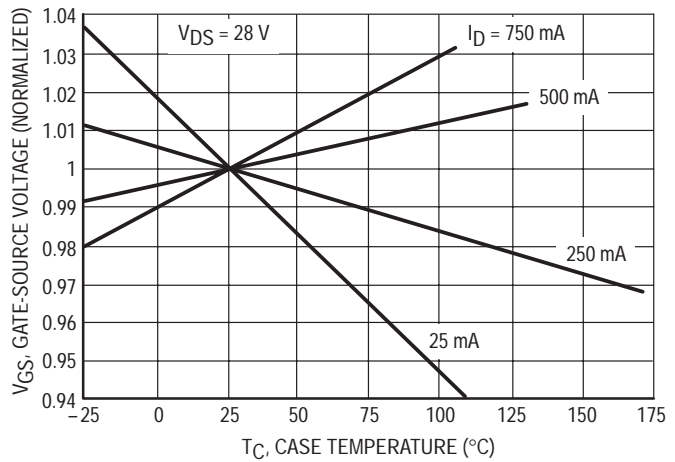


Figure 11. Gate-Source Voltage versus Case Temperature

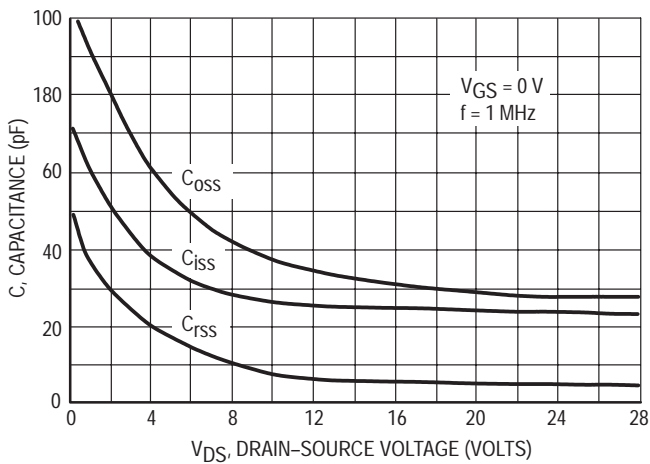


Figure 12. Capacitance versus Drain-Source Voltage

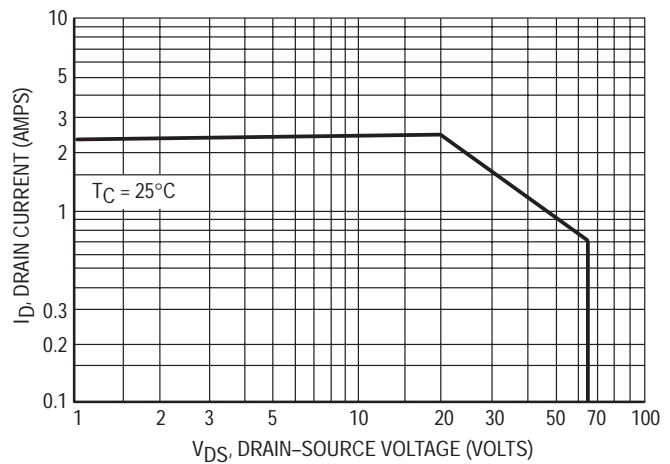


Figure 13. DC Safe Operating Area

TYPICAL CHARACTERISTICS

TYPICAL 400 MHz PERFORMANCE

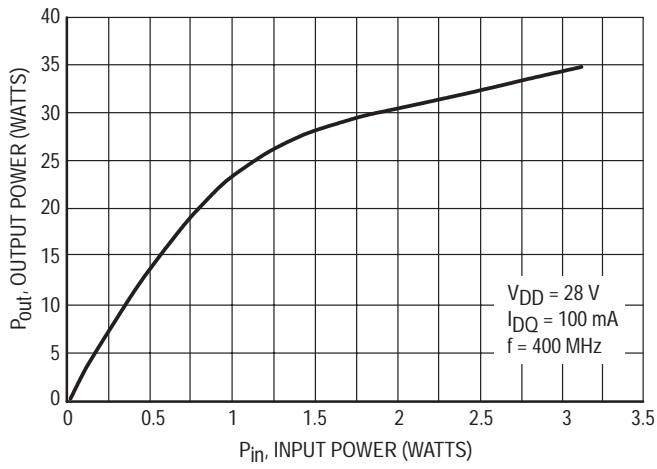


Figure 14. Output Power versus Input Power

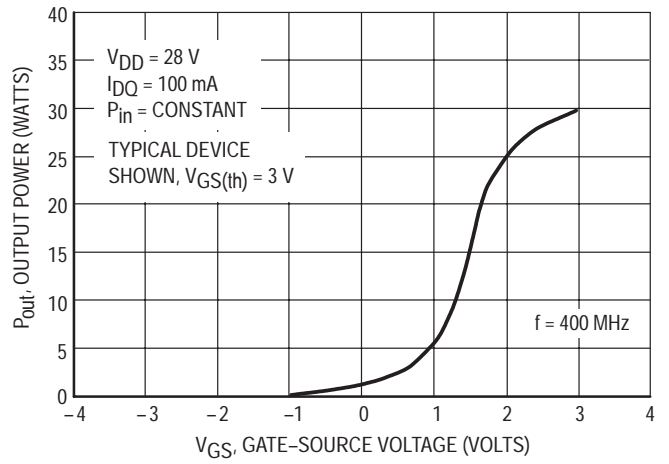


Figure 15. Output Power versus Gate Voltage

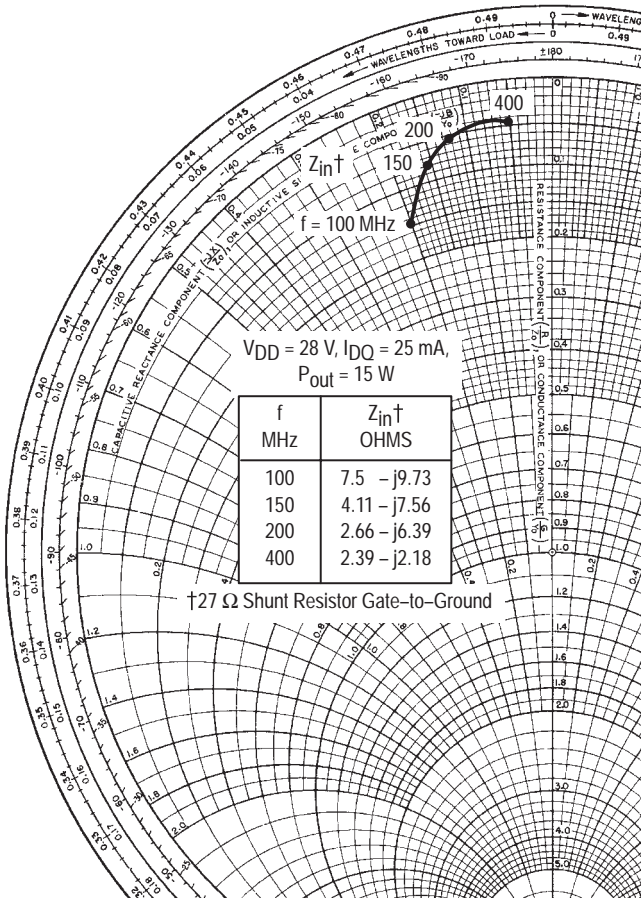


Figure 16. Large-Signal Series Equivalent Input Impedance, Z_{in}^\dagger

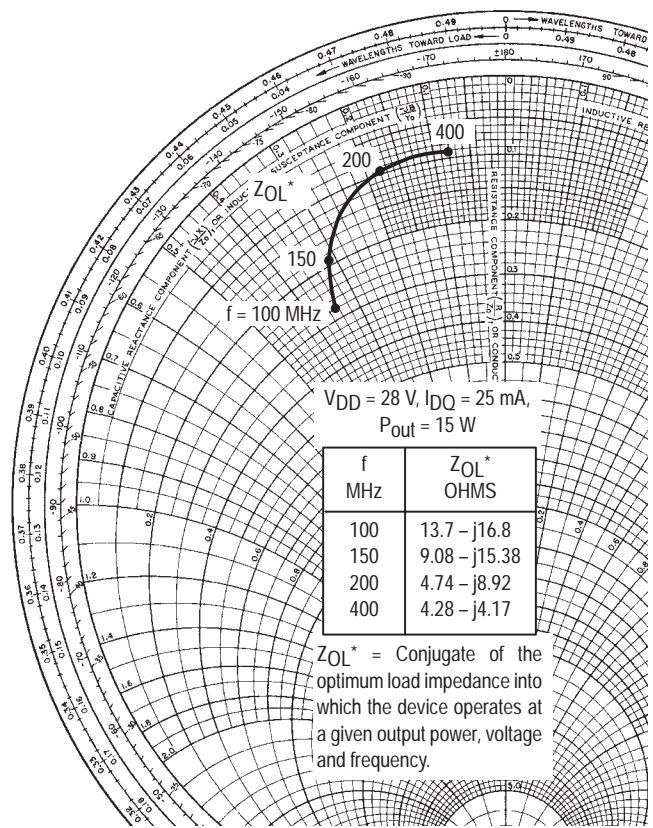
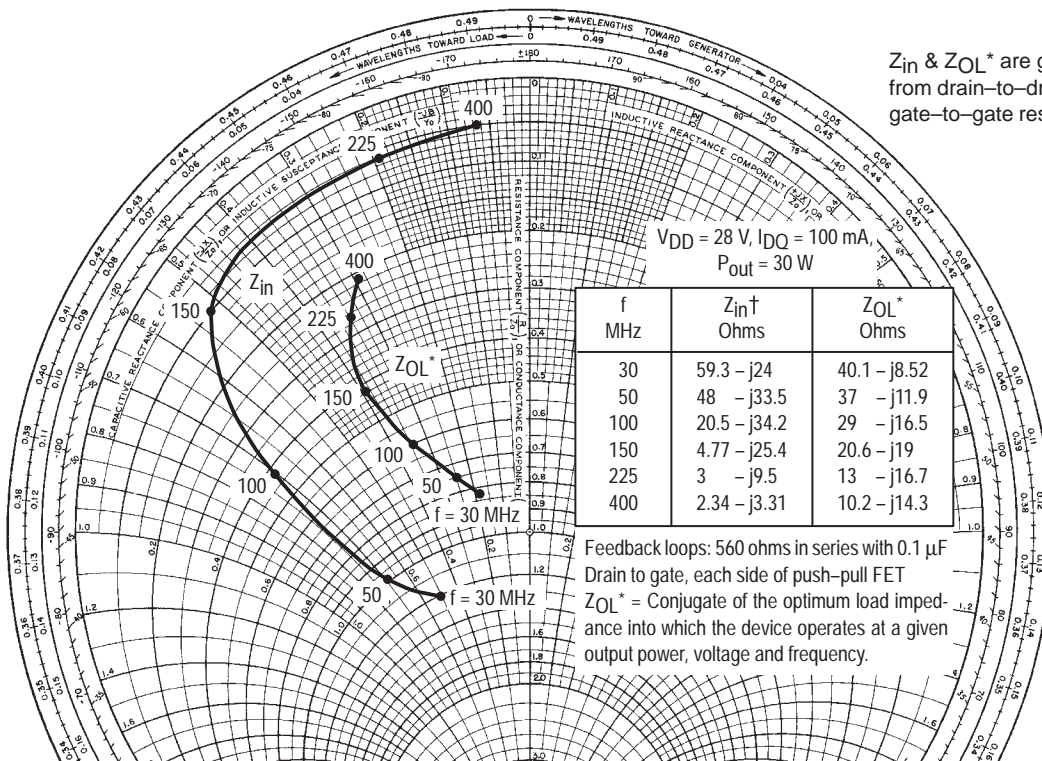


Figure 17. Large-Signal Series Equivalent Output Impedance, Z_{OL}^*



Z_{in} & Z_{OL}^* are given from drain-to-drain and gate-to-gate respectively.

Figure 18. Input and Output Impedance

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
2.0	0.988	-11	41.19	173	0.006	67	0.729	-12
5.0	0.970	-27	40.07	164	0.014	62	0.720	-31
10	0.923	-52	35.94	149	0.026	54	0.714	-58
20	0.837	-88	27.23	129	0.040	36	0.690	-96
30	0.784	-111	20.75	117	0.046	27	0.684	-118
40	0.751	-125	16.49	108	0.048	22	0.680	-131
50	0.733	-135	13.41	103	0.050	19	0.679	-139
60	0.720	-142	11.43	99	0.050	16	0.678	-145
70	0.709	-147	9.871	96	0.050	14	0.679	-149
80	0.707	-152	8.663	93	0.051	13	0.683	-153
90	0.706	-155	7.784	91	0.051	13	0.682	-155
100	0.708	-157	7.008	88	0.051	13	0.680	-157
110	0.711	-159	6.435	86	0.051	14	0.681	-158
120	0.714	-161	5.899	85	0.051	15	0.682	-159
130	0.717	-163	5.439	82	0.052	16	0.684	-160
140	0.720	-164	5.068	80	0.052	17	0.684	-161
150	0.723	-165	4.709	80	0.052	18	0.686	-161
160	0.727	-166	4.455	78	0.052	18	0.690	-161
170	0.732	-167	4.200	77	0.052	18	0.694	-162
180	0.735	-168	3.967	75	0.052	19	0.699	-162
190	0.738	-169	3.756	74	0.052	19	0.703	-163
200	0.740	-170	3.545	73	0.052	20	0.706	-163
225	0.746	-171	3.140	69	0.053	22	0.717	-163
250	0.742	-172	2.783	67	0.053	25	0.724	-163
275	0.744	-173	2.540	64	0.054	27	0.724	-163
300	0.751	-174	2.323	60	0.055	29	0.736	-163
325	0.757	-175	2.140	58	0.058	32	0.749	-163
350	0.760	-176	1.963	54	0.059	35	0.758	-163
375	0.762	-177	1.838	52	0.062	38	0.768	-163
400	0.774	-179	1.696	50	0.065	41	0.783	-163
425	0.775	-179	1.590	48	0.068	43	0.793	-163
450	0.781	+179	1.493	46	0.071	46	0.805	-163
475	0.787	+177	1.415	43	0.074	47	0.813	-164
500	0.792	+176	1.332	40	0.079	48	0.825	-164
525	0.797	+175	1.259	38	0.083	50	0.831	-164
550	0.801	+175	1.185	37	0.088	51	0.843	-164
575	0.810	+174	1.145	36	0.094	52	0.855	-164
600	0.816	+173	1.091	34	0.101	52	0.869	-165
625	0.818	+171	1.041	32	0.106	53	0.871	-165
650	0.825	+170	0.994	30	0.112	53	0.884	-165
675	0.834	+169	0.962	29	0.119	53	0.890	-165
700	0.837	+168	0.922	27	0.127	53	0.906	-166
725	0.836	+167	0.879	25	0.133	52	0.909	-167
750	0.841	+166	0.838	25	0.140	53	0.917	-167
775	0.844	+165	0.824	24	0.148	52	0.933	-167
800	0.846	+163	0.785	21	0.154	50	0.941	-168

Table 1. Common Source Scattering Parameters
V_{DS} = 28 V, I_D = 0.5 A

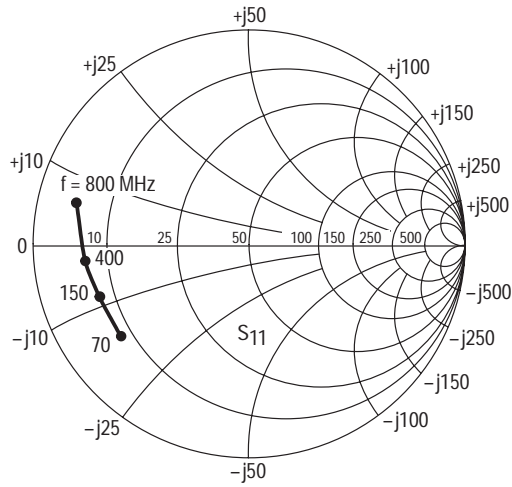


Figure 19. S_{11} , Input Reflection Coefficient versus Frequency
 $V_{DS} = 28\text{ V}$ $I_D = 0.5\text{ A}$

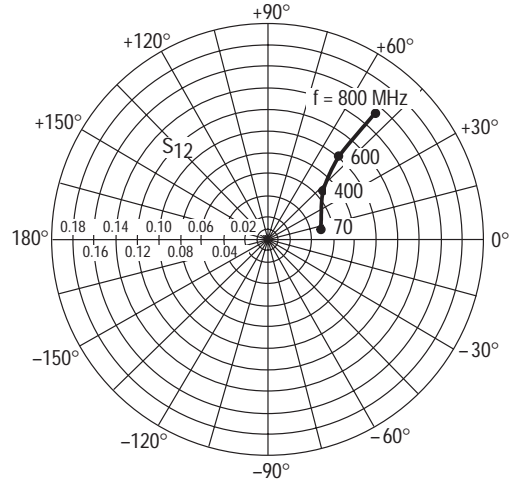


Figure 20. S_{12} , Reverse Transmission Coefficient versus Frequency
 $V_{DS} = 28\text{ V}$ $I_D = 0.5\text{ A}$

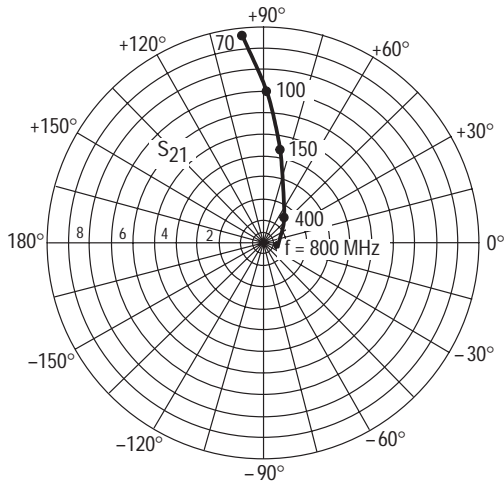


Figure 21. S_{21} , Forward Transmission Coefficient versus Frequency
 $V_{DS} = 28\text{ V}$ $I_D = 0.5\text{ A}$

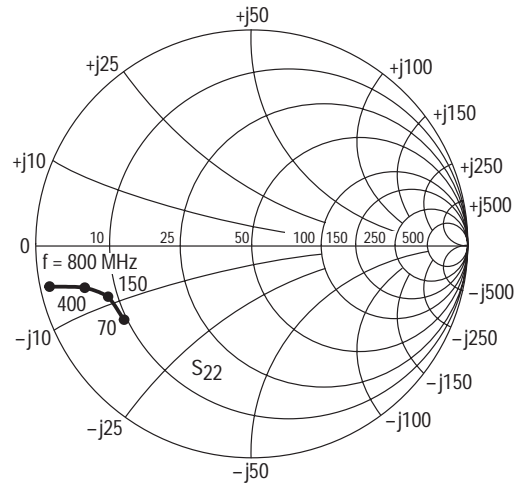


Figure 22. S_{22} , Output Reflection Coefficient versus Frequency
 $V_{DS} = 28\text{ V}$ $I_D = 0.5\text{ A}$

DESIGN CONSIDERATIONS

The MRF136 is an RF power N-Channel enhancement mode field-effect transistor (FET) designed especially for HF and VHF power amplifier applications. Motorola RF MOS FETs feature planar design for optimum manufacturability.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power FETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal, thus facilitating manual gain control, ALC and modulation.

DC BIAS

The MRF136 is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied without gate bias. A positive gate voltage causes drain current to flow (see Figure 10). RF power FETs require forward bias for optimum gain and power output. A Class AB condition with quiescent drain current (I_{DQ}) in the 25–100 mA range is sufficient for many applications. For special requirements such as linear amplification, I_{DQ} may have to be adjusted to optimize the critical parameters.

The MOS gate is a dc open circuit. Since the gate bias circuit does not have to deliver any current to the FET, a simple resistive divider arrangement may sometimes suffice for this function. Special applications may require more elaborate gate bias systems.

GAIN CONTROL

Power output of the MRF136 may be controlled from rated values down to the milliwatt region (>20 dB reduction in power output with constant input power) by varying the dc gate

voltage. This feature, not available in bipolar RF power devices, facilitates the incorporation of manual gain control, AGC/ALC and modulation schemes into system designs. A full range of power output control may require dc gate voltage excursions into the negative region.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for MRF136. See Motorola Application Note AN721, Impedance Matching Networks Applied to RF Power Transistors. Both small signal scattering parameters and large signal impedance parameters are provided. Large signal impedances should be used for network designs wherever possible. While the s parameters will not produce an exact design solution for high power operation, they do yield a good first approximation. This is particularly useful at frequencies outside those presented in the large signal impedance plots.

RF power FETs are triode devices and are therefore not unilateral. This, coupled with the very high gain, yields a device capable of self oscillation. Stability may be achieved using techniques such as drain loading, input shunt resistive loading, or feedback. S parameter stability analysis can provide useful information in the selection of loading and/or feedback to insure stable operation. The MRF136 was characterized with a 27 ohm input shunt loading resistor.

For further discussion of RF amplifier stability and the use of two port parameters in RF amplifier design, see Motorola Application Note AN215A.

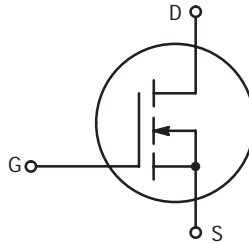
LOW NOISE OPERATION

Input resistive loading will degrade noise performance, and noise figure may vary significantly with gate driving impedance. A low loss input matching network with its gate impedance optimized for lowest noise is recommended.

The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode MOSFET

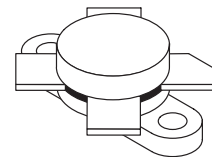
Designed for broadband commercial and military applications at frequencies to 175 MHz. The high power, high gain and broadband performance of this device makes possible solid state transmitters for FM broadcast or TV channel frequency bands.

- Guaranteed Performance at 30 MHz, 28 V:
Output Power — 150 W
Gain — 18 dB (22 dB Typ)
Efficiency — 40%
- Typical Performance at 175 MHz, 50 V:
Output Power — 150 W
Gain — 13 dB
- Low Thermal Resistance
- Ruggedness Tested at Rated Output Power
- Nitride Passivated Die for Enhanced Reliability
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://motorola.com/sps/rf/designtds/>



MRF141

150 W, 28 V, 175 MHz
N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 211-11, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage	V_{DGO}	65	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	16	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	300 1.71	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.6	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS (1)

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 100 \text{ mA}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	5.0	mAdc
Gate–Body Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS (1)

Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 100 \text{ mA}$)	$V_{GS(th)}$	1.0	3.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 10 \text{ A}$)	$V_{DS(on)}$	0.1	0.9	1.5	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 5.0 \text{ A}$)	g_{fs}	5.0	7.0	—	mhos

DYNAMIC CHARACTERISTICS (1)

Input Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{iss}	—	350	—	pF
Output Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{oss}	—	420	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{rss}	—	35	—	pF

FUNCTIONAL TESTS

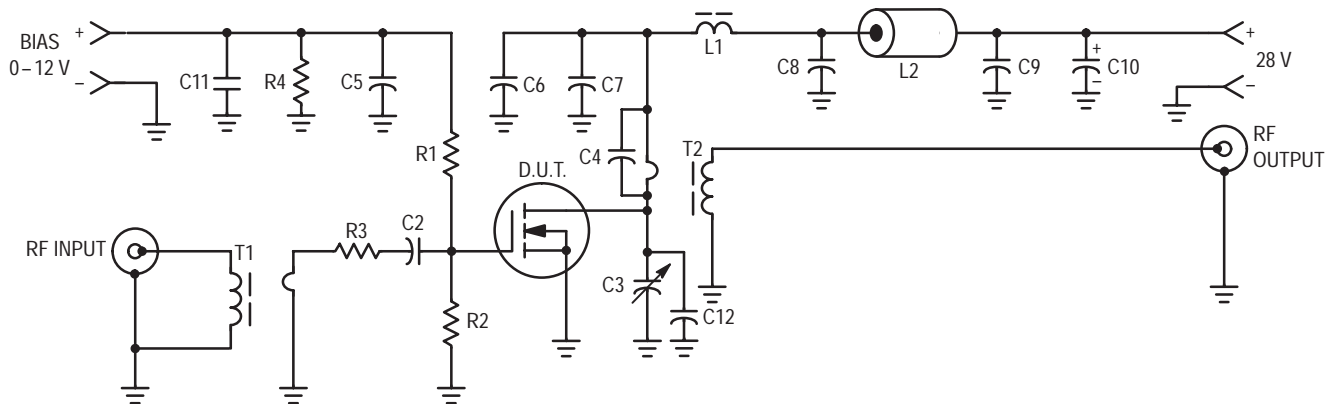
Common Source Amplifier Power Gain, $f = 30; 30.001 \text{ MHz}$ ($V_{DD} = 28 \text{ V}, P_{out} = 150 \text{ W (PEP)}, I_{DQ} = 250 \text{ mA}$) $f = 175 \text{ MHz}$	G_{ps}	16 —	20 10	— —	dB
Drain Efficiency ($V_{DD} = 28 \text{ V}, P_{out} = 150 \text{ W (PEP)}, f = 30; 30.001 \text{ MHz},$ $I_{DQ} = 250 \text{ mA}, I_D (\text{Max}) = 5.95 \text{ A}$)	η	40	45	—	%
Intermodulation Distortion (1) ($V_{DD} = 28 \text{ V}, P_{out} = 150 \text{ W (PEP)}, f = 30 \text{ MHz},$ $f_2 = 30.001 \text{ MHz}, I_{DQ} = 250 \text{ mA}$)	$IMD_{(d3)}$ $IMD_{(d11)}$	— —	-30 -60	-28 —	dB
Load Mismatch ($V_{DD} = 28 \text{ V}, P_{out} = 150 \text{ W (PEP)}, f_1 = 30; 30.001 \text{ MHz},$ $I_{DQ} = 250 \text{ mA}, VSWR 30:1$ at all Phase Angles)	ψ	No Degradation in Output Power			

CLASS A PERFORMANCE

Intermodulation Distortion (1) and Power Gain ($V_{DD} = 28 \text{ V}, P_{out} = 50 \text{ W (PEP)}, f_1 = 30 \text{ MHz},$ $f_2 = 30.001 \text{ MHz}, I_{DQ} = 4.0 \text{ A}$)	G_{PS} $IMD_{(d3)}$ $IMD_{(d9-13)}$	— — —	23 -50 -75	— — —	dB
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NOTE:

- To MIL–STD–1311 Version A, Test Method 2204B, Two Tone, Reference Each Tone.



- C2, C5, C6, C7, C8, C9 — 0.1 μF Ceramic Chip or Monolithic with Short Leads
- C3 — Arco 469
- C4 — 820 pF Unencapsulated Mica or Dipped Mica with Short Leads
- C10 — 10 $\mu\text{F}/100 \text{ V}$ Electrolytic
- C11 — 1 $\mu\text{F}, 50 \text{ V}$, Tantalum
- C12 — 330 pF, Dipped Mica (Short leads)

- L1 — VK200/4B Ferrite Choke or Equivalent, 3.0 μH
- L2 — Ferrite Bead(s), 2.0 μH
- R1, R2 — 51 $\Omega/1.0 \text{ W}$ Carbon
- R3 — 1.0 $\Omega/1.0 \text{ W}$ Carbon or Parallel Two 2 $\Omega, 1/2 \text{ W}$ Resistors
- R4 — 1 k $\Omega/1/2 \text{ W}$ Carbon
- T1 — 16:1 Broadband Transformer
- T2 — 1:25 Broadband Transformer
- Board Material — 0.062" Fiberglass (G10), 1 oz. Copper Clad, 2 Sides, $\epsilon_r = 5$

Figure 1. 30 MHz Test Circuit (Class AB)

TYPICAL CHARACTERISTICS

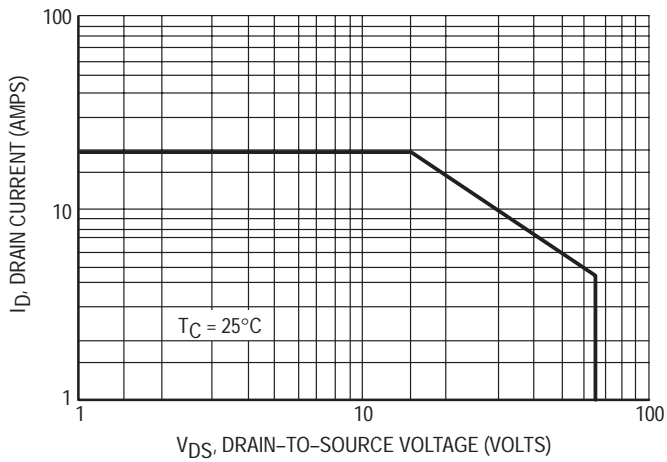


Figure 2. DC Safe Operating Area

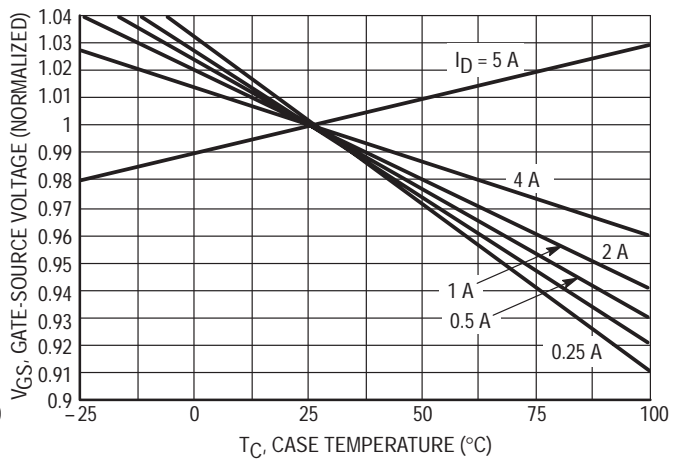


Figure 3. Gate-Source Voltage versus Case Temperature

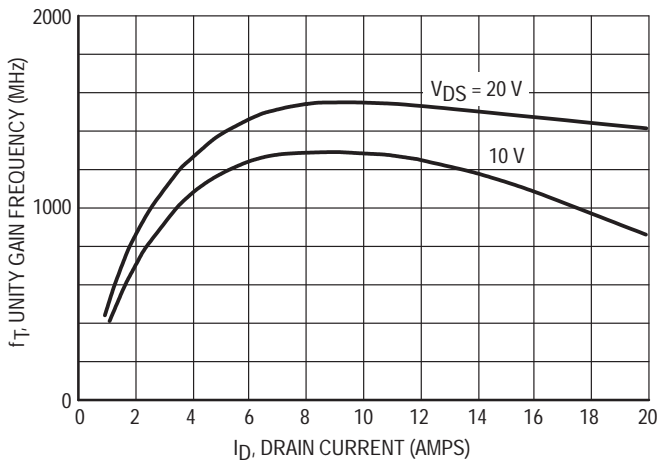


Figure 4. Common Source Unity Gain Frequency versus Drain Current

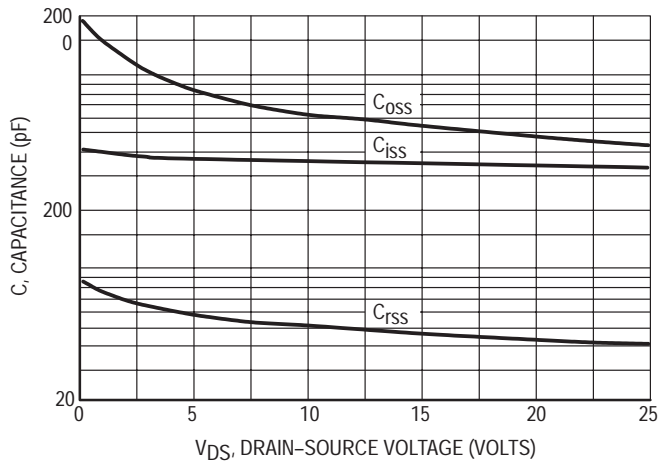


Figure 5. Capacitance versus Drain-Source Voltage

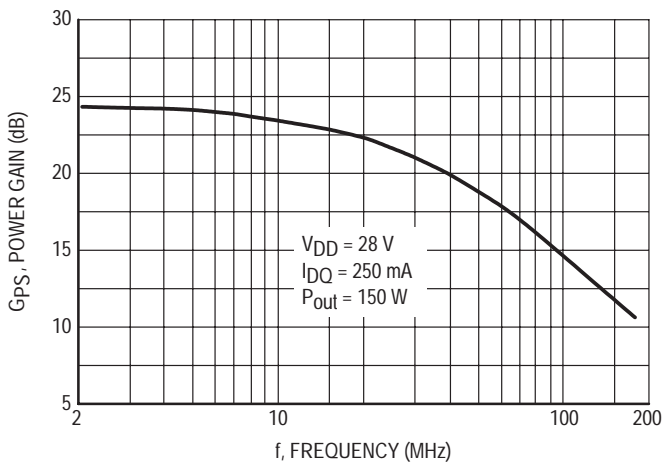


Figure 6. Power Gain versus Frequency

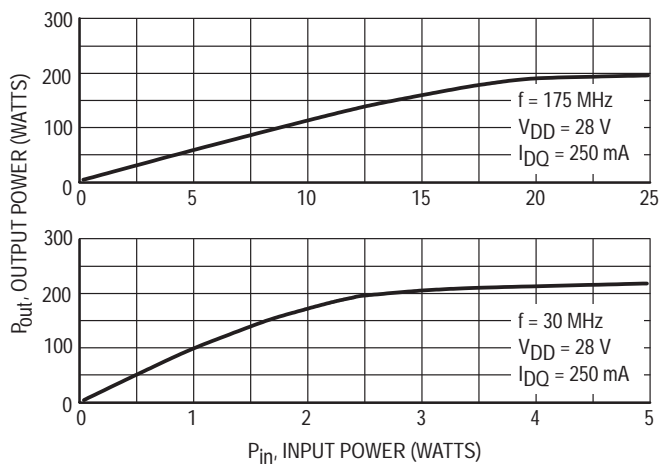


Figure 7. Output Power versus Input Power

TYPICAL CHARACTERISTICS

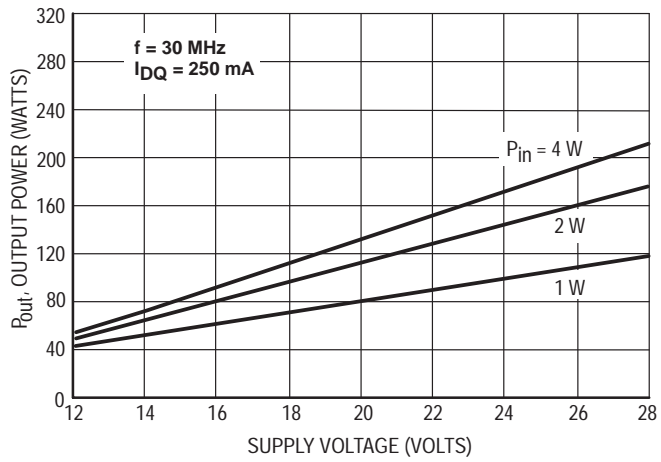


Figure 8. Output Power versus Supply Voltage

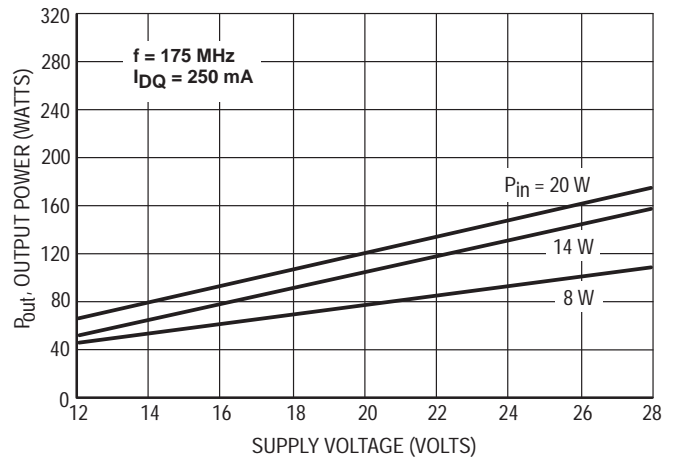


Figure 9. Output Power versus Supply Voltage

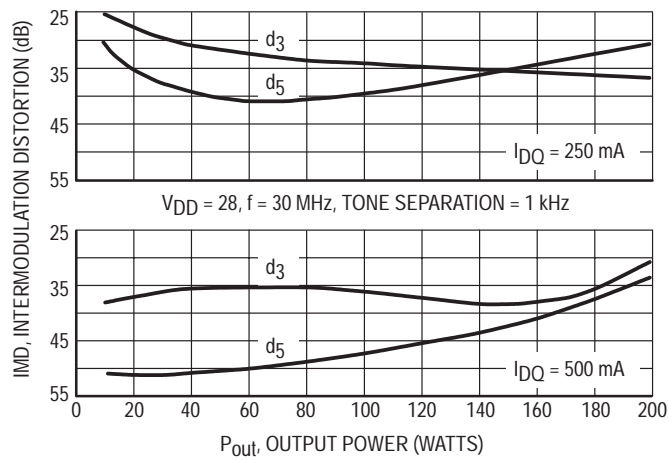


Figure 10. IMD versus P_{out} (PEP)

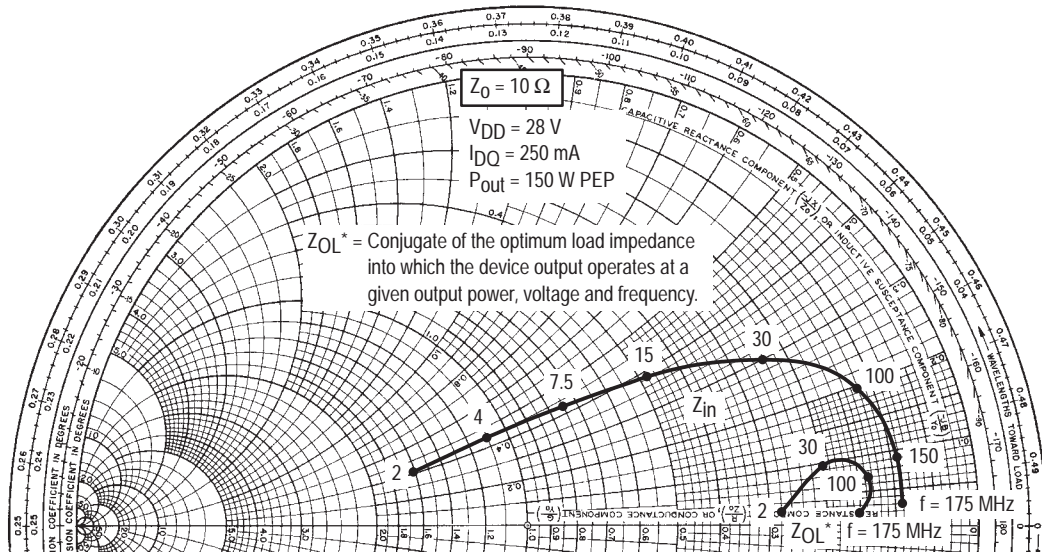
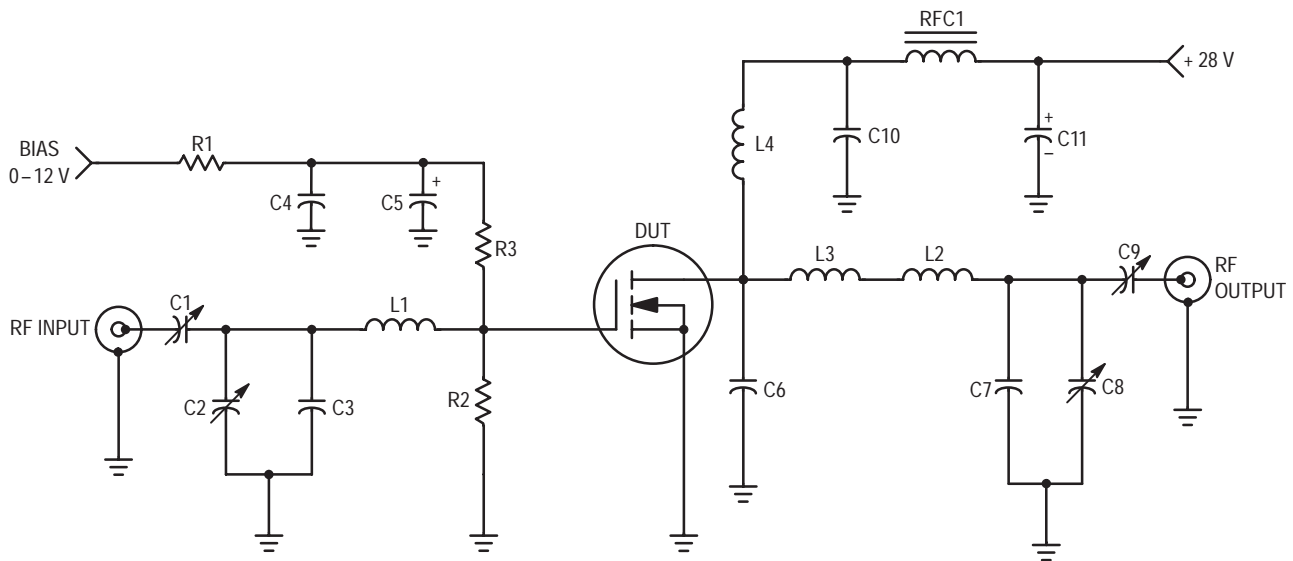


Figure 11. Input and Output Impedances



- C1, C2, C8 — Arco 463 or equivalent
- C3 — 25 pF, Unelco
- C4 — 0.1 μ F, Ceramic
- C5 — 1.0 μ F, 15 WV Tantalum
- C6 — 25 pF, Unelco J101
- C7 — 25 pF, Unelco J101
- C9 — Arco 262 or equivalent
- C10 — 0.05 μ F, Ceramic
- C11 — 15 μ F, 35 WV Electrolytic

- L1 — 3/4", #18 AWG into Hairpin
- L2 — Printed Line, 0.200" x 0.500"
- L3 — 7/8", #16 AWG into Hairpin
- L4 — 2 Turns, #16 AWG, 5/16 ID
- RFC1 — 5.6 μ H, Molded Choke
- RFC2 — VK200-4B
- R1 — 150 Ω , 1.0 W Carbon
- R2 — 10 k Ω , 1/2 W Carbon
- R3 — 120 Ω , 1/2 W Carbon

Figure 12. 175 MHz Test Circuit (Class AB)

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 5\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.916	-177	4.23	83	0.008	32	0.876	-177
40	0.919	-178	3.23	76	0.009	39	0.885	178
50	0.922	-178	2.55	72	0.010	45	0.914	-180
60	0.923	-179	2.14	68	0.010	46	0.893	179
70	0.927	-179	1.77	63	0.011	48	0.878	179
80	0.929	-179	1.48	61	0.013	53	0.864	180
90	0.931	-180	1.28	60	0.015	61	0.850	180
100	0.934	-180	1.15	55	0.016	66	0.893	178
110	0.935	180	1.05	53	0.016	69	0.913	177
120	0.939	180	0.91	51	0.017	69	0.930	180
130	0.941	179	0.82	48	0.019	67	0.916	-180
140	0.943	179	0.76	46	0.022	68	0.926	179
150	0.946	179	0.67	42	0.024	70	0.940	177
160	0.946	179	0.63	40	0.025	73	0.915	178
170	0.948	178	0.57	39	0.024	78	0.891	178
180	0.949	178	0.52	37	0.026	75	0.906	178
190	0.950	178	0.49	37	0.028	74	0.899	176
200	0.950	177	0.45	35	0.030	78	0.915	176
210	0.938	177	0.43	31	0.043	108	0.966	174
220	0.958	178	0.39	33	0.029	61	0.972	175
230	0.961	177	0.36	27	0.038	77	1.033	174
240	0.960	177	0.36	28	0.036	76	0.943	174
250	0.961	176	0.32	30	0.038	77	0.912	175
260	0.962	176	0.30	31	0.040	76	0.918	174
270	0.961	176	0.27	30	0.044	77	0.933	171
280	0.963	176	0.26	30	0.045	79	0.943	172
290	0.964	175	0.25	25	0.045	78	0.940	172
300	0.965	175	0.26	27	0.047	77	0.930	172
310	0.966	175	0.25	27	0.051	78	0.977	172
320	0.964	175	0.24	26	0.053	75	0.947	171
330	0.966	174	0.22	21	0.056	75	0.946	170
340	0.967	174	0.23	26	0.056	75	0.944	170
350	0.967	174	0.22	24	0.058	78	0.946	171
360	0.965	174	0.21	28	0.062	74	0.956	171
370	0.966	174	0.20	28	0.048	61	0.968	170
380	0.968	173	0.20	27	0.053	74	0.931	168
390	0.970	173	0.18	31	0.063	74	0.962	168
400	0.970	173	0.17	26	0.071	79	0.965	172
410	0.970	172	0.17	29	0.076	78	0.982	169
420	0.971	172	0.17	30	0.076	76	0.956	167
430	0.970	172	0.15	29	0.070	76	0.912	165
440	0.970	171	0.13	32	0.074	76	0.933	167

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 5\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
450	0.970	171	0.15	31	0.081	76	0.967	167
460	0.970	171	0.15	32	0.090	73	0.982	164
470	0.969	170	0.15	30	0.095	77	0.945	165
480	0.964	170	0.16	34	0.099	80	0.956	165
490	0.960	170	0.15	31	0.107	75	0.947	163
500	0.959	170	0.15	23	0.103	68	0.962	163

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 5\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.914	-177	4.60	82	0.007	25	0.874	-176
40	0.915	-178	3.51	76	0.008	26	0.879	-179
50	0.918	-178	2.76	71	0.009	34	0.888	-179
60	0.920	-178	2.32	67	0.010	45	0.881	179
70	0.924	-179	1.92	62	0.010	56	0.887	179
80	0.927	-179	1.61	60	0.009	62	0.899	-179
90	0.930	-179	1.39	58	0.010	61	0.874	-177
100	0.933	-180	1.23	53	0.012	57	0.875	-179
110	0.934	-180	1.13	51	0.015	63	0.884	179
120	0.938	180	0.98	49	0.017	73	0.926	179
130	0.940	180	0.88	46	0.018	81	0.959	-179
140	0.942	179	0.81	44	0.018	82	0.966	-179
150	0.945	179	0.71	40	0.018	77	0.961	-179
160	0.946	179	0.67	38	0.021	73	0.910	-179
170	0.948	178	0.61	37	0.023	77	0.871	179
180	0.950	178	0.54	35	0.026	78	0.912	178
190	0.950	178	0.52	34	0.029	76	0.959	177
200	0.952	178	0.47	33	0.034	64	0.971	178
210	0.949	177	0.46	28	0.067	17	1.023	-178
220	0.953	178	0.41	31	0.019	94	0.954	177
230	0.959	177	0.38	26	0.037	76	1.014	174
240	0.960	177	0.37	25	0.040	79	0.943	174
250	0.961	177	0.33	27	0.042	84	0.972	175
260	0.962	176	0.30	27	0.041	86	0.969	176
270	0.961	176	0.29	27	0.041	83	0.951	175
280	0.963	176	0.27	27	0.042	80	0.929	174
290	0.964	175	0.26	23	0.045	79	0.930	172
300	0.965	175	0.27	25	0.051	81	0.963	171
310	0.966	175	0.26	24	0.052	83	1.012	173
320	0.965	175	0.25	23	0.053	81	0.984	171
330	0.966	174	0.23	19	0.055	78	0.955	172
340	0.967	174	0.24	25	0.054	76	0.929	171
350	0.967	174	0.22	22	0.057	79	0.917	170

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 5\text{ A}$) (continued)

f MHz	S11		S21		S12		S22	
	S11	ϕ	S21	ϕ	S12	ϕ	S22	ϕ
360	0.967	174	0.21	26	0.060	91	0.978	169
370	0.967	174	0.20	26	0.084	89	1.030	167
380	0.969	173	0.20	23	0.081	82	0.994	170
390	0.970	173	0.19	29	0.072	80	0.963	170
400	0.970	173	0.17	25	0.069	80	0.951	172
410	0.970	172	0.17	27	0.072	71	0.985	167
420	0.972	172	0.16	28	0.078	68	0.970	165
430	0.971	172	0.15	27	0.084	70	0.953	165
440	0.971	171	0.13	29	0.086	74	0.949	168
450	0.971	171	0.15	29	0.087	79	0.962	167
460	0.970	171	0.15	32	0.081	72	0.976	164
470	0.969	170	0.15	29	0.079	65	0.969	164
480	0.964	170	0.16	32	0.081	57	0.972	165
490	0.959	170	0.15	29	0.081	54	0.976	165
500	0.958	170	0.15	21	0.086	58	0.953	167

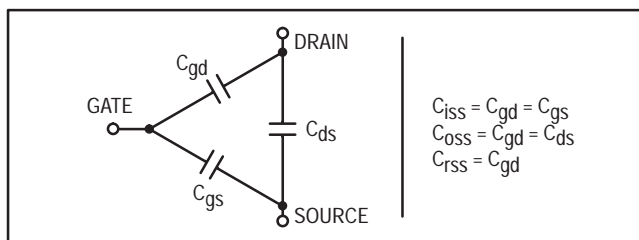
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal anode gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the MOSFET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iSS}), output (C_{OSS}) and reverse transfer (C_{RSS}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iSS} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 4 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors.

Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gate of this device is essentially capacitor. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the device due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — This device does not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

Using a resistor to keep the gate-to-source impedance low also helps damp transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

HANDLING CONSIDERATIONS

When shipping, the devices should be transported only in antistatic bags or conductive foam. Upon removal from the packaging, careful handling procedures should be adhered to. Those handling the devices should wear grounding straps and devices not in the antistatic packaging should be kept in metal tote bins. MOSFETs should be handled by the case and not by the leads, and when testing the device, all leads should make good electrical contact before voltage is applied. As a final note, when placing the FET into the system it is designed for, soldering should be done with a grounded iron.

DESIGN CONSIDERATIONS

The MRF141 is an RF Power, MOS, N-channel enhancement mode field-effect transistor (FET) designed for HF and VHF power amplifier applications.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power MOSFETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal.

DC BIAS

The MRF141 is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF141 was characterized at $I_{DQ} = 250$ mA, each side, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may be just a simple resistive divider network. Some applications may require a more elaborate bias system.

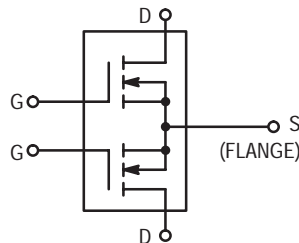
GAIN CONTROL

Power output of the MRF141 may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems.

The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode MOSFET

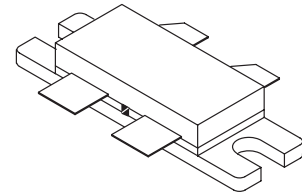
Designed for broadband commercial and military applications at frequencies to 175 MHz. The high power, high gain and broadband performance of this device makes possible solid state transmitters for FM broadcast or TV channel frequency bands.

- Guaranteed Performance at 175 MHz, 28 V:
Output Power — 300 W
Gain — 12 dB (14 dB Typ)
Efficiency — 50%
- Low Thermal Resistance — 0.35°C/W
- Ruggedness Tested at Rated Output Power
- Nitride Passivated Die for Enhanced Reliability
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://motorola.com/sps/rf/designtds/>



MRF141G

300 W, 28 V, 175 MHz
N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 375-04, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage	V_{DGO}	65	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	32	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	500 2.85	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.35	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS (1)

Drain–Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 100$ mA)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28$ V, $V_{GS} = 0$)	I_{DSS}	—	—	5.0	mAdc
Gate–Body Leakage Current ($V_{GS} = 20$ V, $V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS (1)

Gate Threshold Voltage ($V_{DS} = 10$ V, $I_D = 100$ mA)	$V_{GS(th)}$	1.0	3.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10$ V, $I_D = 10$ A)	$V_{DS(on)}$	0.1	0.9	1.5	Vdc
Forward Transconductance ($V_{DS} = 10$ V, $I_D = 5.0$ A)	g_{fs}	5.0	7.0	—	mhos

DYNAMIC CHARACTERISTICS (1)

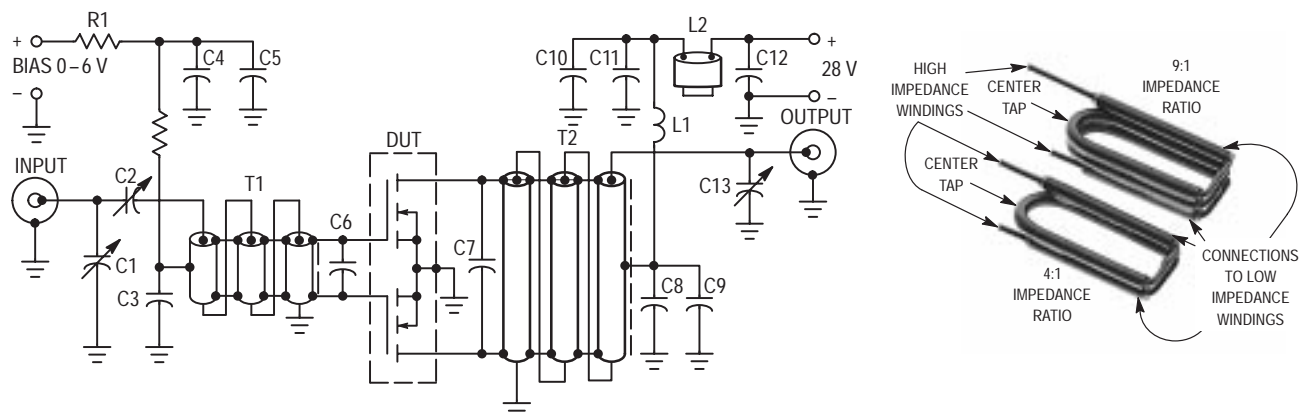
Input Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1.0$ MHz)	C_{iss}	—	350	—	pF
Output Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1.0$ MHz)	C_{oss}	—	420	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1.0$ MHz)	C_{rss}	—	35	—	pF

FUNCTIONAL TESTS (2)

Common Source Amplifier Power Gain ($V_{DD} = 28$ V, $P_{out} = 300$ W, $I_{DQ} = 500$ mA, $f = 175$ MHz)	G_{ps}	12	14	—	dB
Drain Efficiency ($V_{DD} = 28$ V, $P_{out} = 300$ W, $f = 175$ MHz, I_D (Max) = 21.4 A)	η	45	55	—	%
Load Mismatch ($V_{DD} = 28$ V, $P_{out} = 300$ W, $I_{DQ} = 500$ mA, $f = 175$ MHz, VSWR 5:1 at all Phase Angles)	ψ	No Degradation in Output Power			

NOTES:

1. Each side measured separately.
2. Measured in push–pull configuration.



- C1 — Arco 402, 1.5–20 pF
- C2 — Arco 406, 15–115 pF
- C3, C4, C8, C9, C10 — 1000 pF Chip
- C5, C11 — 0.1 μ F Chip
- C6 — 330 pF Chip
- C7 — 200 pF and 180 pF Chips in Parallel
- C12 — 0.47 μ F Ceramic Chip, Kemet 1215 or Equivalent
- C13 — Arco 403, 3.0–35 pF
- L1 — 10 Turns AWG #16 Enameled Wire, Close Wound, 1/4" I.D.
- L2 — Ferrite Beads of Suitable Material for 1.5–2.0 μ H Total Inductance
- R1 — 100 Ohms, 1/2 W
- R2 — 1.0 kOhm, 1/2 W

- T1 — 9:1 RF Transformer. Can be made of 15–18 Ohms Semirigid Co-Ax, 62–90 Mils O.D.
- T2 — 1:9 RF Transformer. Can be made of 15–18 Ohms Semirigid Co-Ax, 70–90 Mils O.D.

Board Material — 0.062" Fiberglass (G10), 1 oz. Copper Clad, 2 Sides, $\epsilon_r = 5$

NOTE: For stability, the input transformer T1 must be loaded with ferrite toroids or beads to increase the common mode inductance. For operation below 100 MHz. The same is required for the output transformer.

See pictures for construction details.

Unless Otherwise Noted, All Chip Capacitors are ATC Type 100 or Equivalent.

Figure 1. 175 MHz Test Circuit

TYPICAL CHARACTERISTICS

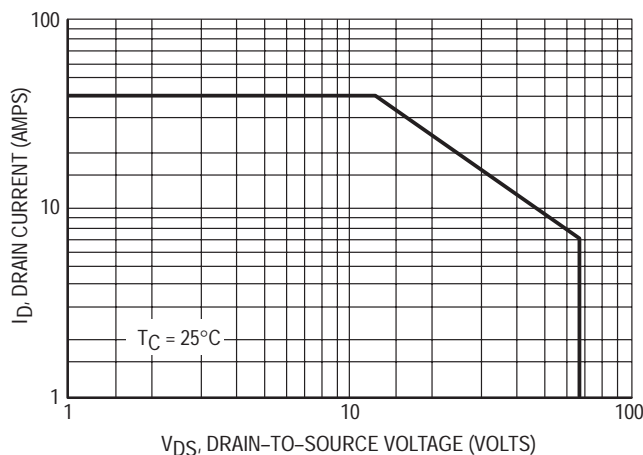


Figure 2. DC Safe Operating Area

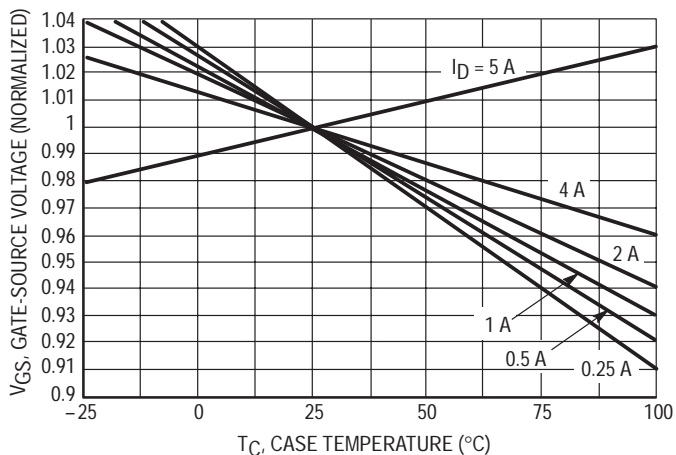
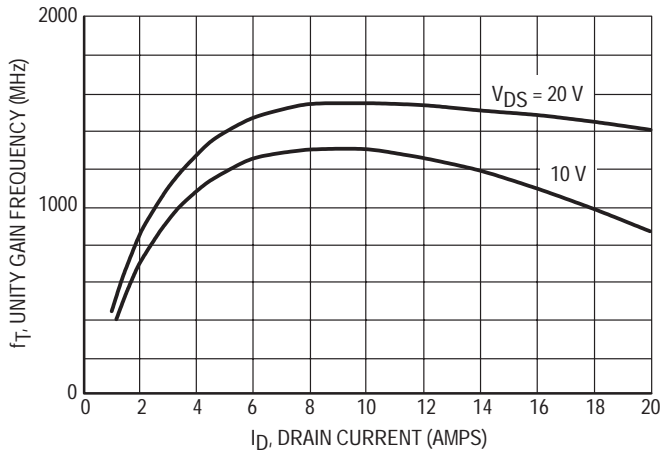


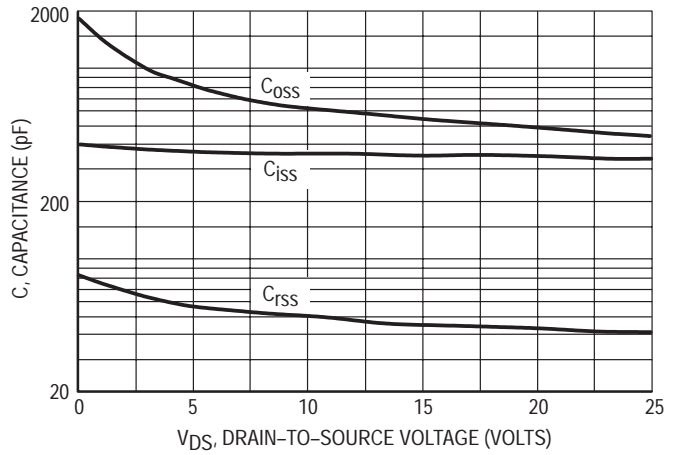
Figure 3. Gate-Source Voltage versus Case Temperature

TYPICAL CHARACTERISTICS



NOTE: Data shown applies to each half of MRF141G.

Figure 4. Common Source Unity Gain Frequency versus Drain Current



NOTE: Data shown applies to each half of MRF141G.

Figure 5. Capacitance versus Drain-Source Voltage

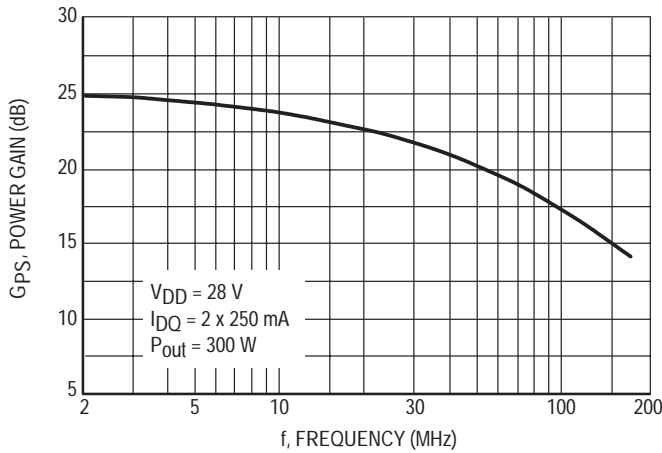


Figure 6. Power Gain versus Frequency

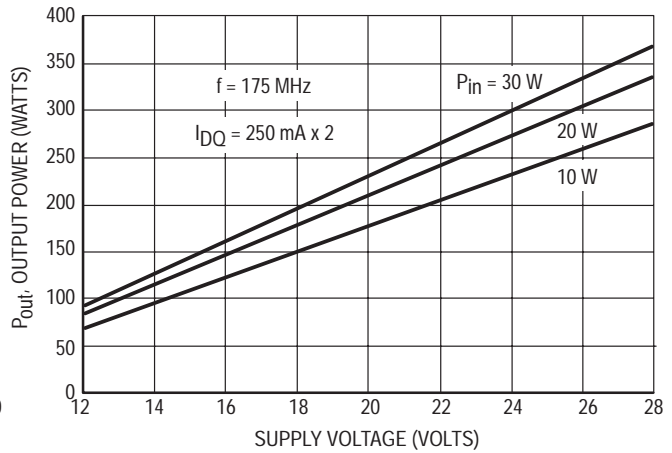
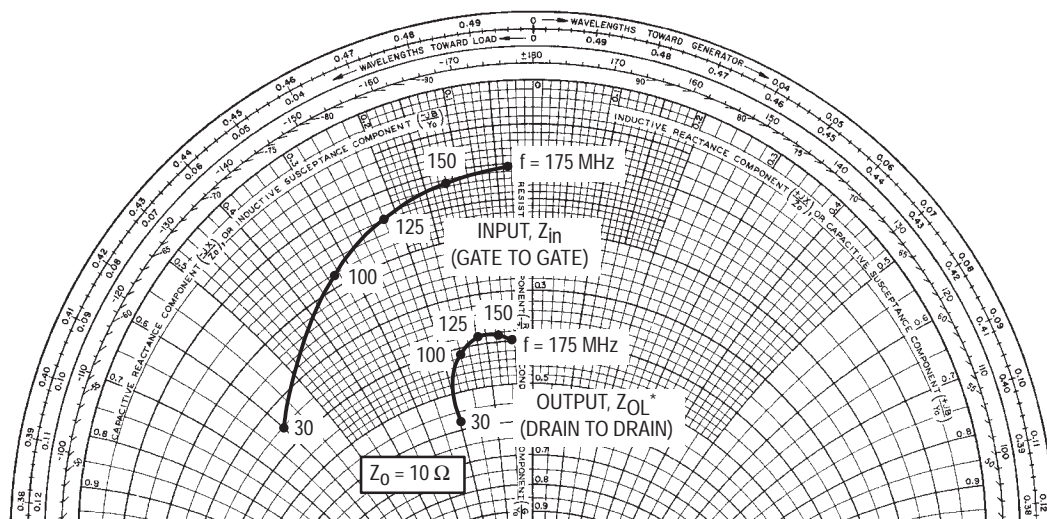


Figure 7. Output Power versus Supply Voltage



Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

Figure 8. Input and Output Impedances

NOTE: S-Parameter data represents measurements taken from one chip only.

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 0.57\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.845	-174	4.88	78	0.014	-5	0.939	-174
40	0.867	-174	3.23	66	0.013	-14	0.856	-172
50	0.876	-174	2.62	62	0.013	-17	0.868	-175
60	0.883	-174	2.12	59	0.012	-15	0.938	-176
70	0.890	-175	1.85	58	0.012	-12	1.036	-177
80	0.899	-175	1.57	56	0.011	-10	1.110	-177
90	0.909	-175	1.36	50	0.010	-11	1.190	-176
100	0.920	-176	1.13	43	0.009	-13	1.160	-176
110	0.930	-176	0.95	37	0.007	-16	1.100	-177
120	0.938	-176	0.78	33	0.007	-11	1.010	-175
130	0.944	-176	0.67	31	0.006	-3	0.954	-176
140	0.948	-177	0.60	31	0.006	10	0.964	-177
150	0.951	-177	0.56	32	0.005	23	1.023	-178
160	0.954	-178	0.52	32	0.005	31	1.130	-179
170	0.958	-178	0.48	29	0.006	37	1.190	-178
180	0.962	-178	0.45	24	0.006	39	1.260	-179
190	0.965	-179	0.40	17	0.007	41	1.200	180
200	0.968	-179	0.34	15	0.008	49	1.090	-179
210	0.970	-179	0.30	15	0.008	60	0.980	-178
220	0.972	-180	0.27	15	0.008	68	0.960	-177
230	0.973	-180	0.25	17	0.008	68	1.045	-179
240	0.974	180	0.24	20	0.009	67	1.030	179
250	0.975	180	0.24	19	0.011	68	1.100	179
260	0.977	179	0.21	17	0.012	69	1.200	179
270	0.978	179	0.22	13	0.013	72	1.210	177
280	0.979	179	0.19	13	0.012	72	1.170	177
290	0.979	178	0.17	1	0.012	68	1.040	180
300	0.980	178	0.16	8	0.013	65	0.998	179
310	0.980	178	0.16	13	0.015	70	0.977	179
320	0.981	178	0.16	15	0.017	76	0.979	178
330	0.982	177	0.13	10	0.017	83	1.033	178
340	0.982	177	0.15	19	0.016	81	1.110	176
350	0.982	177	0.13	16	0.016	73	1.140	177
360	0.983	177	0.13	8	0.020	63	1.150	177
370	0.982	176	0.10	6	0.023	65	1.120	176
380	0.982	176	0.10	7	0.023	72	1.050	177
390	0.982	176	0.10	10	0.021	81	0.993	177
400	0.982	176	0.09	14	0.018	83	0.959	179
410	0.983	175	0.10	12	0.020	71	1.040	176
420	0.983	175	0.09	16	0.025	65	1.090	174
430	0.984	175	0.09	15	0.028	70	1.100	174

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 0.57\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
440	0.983	174	0.09	12	0.028	77	1.100	175
450	0.983	174	0.09	13	0.025	82	1.090	176
460	0.983	174	0.07	14	0.022	66	1.080	174
470	0.983	174	0.07	13	0.024	56	0.992	175
480	0.983	174	0.07	16	0.032	60	0.970	175
490	0.984	173	0.07	13	0.036	74	0.996	174
500	0.984	173	0.07	18	0.035	85	1.040	174

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.65\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.849	-174	5.41	79	0.013	-6	0.934	-174
40	0.869	-174	3.59	67	0.013	-16	0.849	-172
50	0.878	-174	2.91	62	0.012	-17	0.859	-174
60	0.884	-174	2.36	60	0.011	-13	0.928	-176
70	0.890	-175	2.06	59	0.010	-11	1.029	-177
80	0.899	-175	1.75	56	0.009	-14	1.110	-177
90	0.910	-176	1.52	51	0.009	-18	1.190	-175
100	0.920	-176	1.26	43	0.009	-19	1.150	-175
110	0.929	-176	1.07	37	0.008	-15	1.100	-177
120	0.937	-176	0.88	34	0.006	-4	1.000	-175
130	0.943	-176	0.75	32	0.004	5	0.953	-176
140	0.947	-177	0.67	32	0.003	6	0.966	-177
150	0.950	-177	0.63	32	0.004	6	1.030	-178
160	0.953	-178	0.58	32	0.005	18	1.120	-178
170	0.957	-178	0.54	29	0.006	36	1.180	-178
180	0.961	-178	0.51	24	0.006	53	1.250	-179
190	0.964	-179	0.45	18	0.006	65	1.200	180
200	0.967	-179	0.39	15	0.005	69	1.110	-179
210	0.969	-179	0.35	15	0.005	63	1.030	-178
220	0.971	-180	0.31	15	0.006	59	0.975	-177
230	0.972	-180	0.28	17	0.009	66	1.040	-179
240	0.973	180	0.27	20	0.010	78	1.030	179
250	0.974	180	0.27	19	0.010	88	1.090	180
260	0.976	179	0.24	17	0.009	85	1.200	179
270	0.977	179	0.24	12	0.010	73	1.220	177
280	0.978	179	0.21	12	0.011	66	1.170	178
290	0.979	178	0.19	2	0.013	70	1.040	180
300	0.979	178	0.18	8	0.013	78	1.000	179
310	0.979	178	0.17	13	0.013	89	0.975	179
320	0.980	178	0.17	14	0.012	88	0.988	177

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.65\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
330	0.981	177	0.14	9	0.013	80	1.050	177
340	0.982	177	0.16	17	0.015	75	1.110	176
350	0.982	177	0.15	14	0.018	80	1.130	177
360	0.982	177	0.14	8	0.018	82	1.160	177
370	0.982	176	0.12	6	0.017	82	1.120	176
380	0.982	176	0.12	6	0.015	77	1.060	177
390	0.982	176	0.11	9	0.016	72	0.992	177
400	0.982	176	0.10	13	0.018	78	0.958	179
410	0.983	175	0.11	11	0.021	83	1.050	176
420	0.983	175	0.10	15	0.021	87	1.070	175
430	0.983	175	0.10	14	0.019	85	1.090	175
440	0.983	174	0.10	10	0.018	76	1.130	175
450	0.983	174	0.10	9	0.021	71	1.130	176
460	0.982	174	0.08	10	0.024	70	1.080	174
470	0.983	174	0.08	11	0.023	82	0.996	175
480	0.983	174	0.08	15	0.021	90	0.974	176
490	0.983	173	0.08	12	0.019	87	0.971	175
500	0.983	173	0.08	17	0.021	78	1.010	174

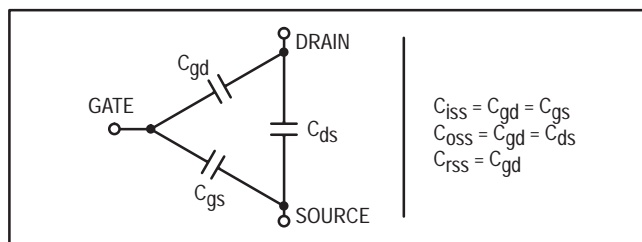
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal anode gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the MOSFET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 4 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors. Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gate of this device is essentially a capacitor. Circuits that leave the gate open-circuited or float-

ing should be avoided. These conditions can result in turn-on of the device due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — This device does not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

Using a resistor to keep the gate-to-source impedance low also helps damp transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

HANDLING CONSIDERATIONS

When shipping, the devices should be transported only in antistatic bags or conductive foam. Upon removal from the packaging, careful handling procedures should be adhered to. Those handling the devices should wear grounding straps and devices not in the antistatic packaging should be kept in metal tote bins. MOSFETs should be handled by the case and not by the leads, and when testing the device, all leads should make good electrical contact before voltage is applied. As a final note, when placing the FET into the system it is designed for, soldering should be done with a grounded iron.

DESIGN CONSIDERATIONS

The MRF141G is an RF Power, MOS, N-channel enhancement mode field-effect transistor (FET) designed for HF and VHF power amplifier applications.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power MOSFETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal.

DC BIAS

The MRF141G is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF141G was characterized at $I_{DQ} = 250$ mA, each side, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may be just a simple resistive divider network. Some applications may require a more elaborate bias system.

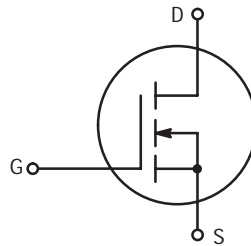
GAIN CONTROL

Power output of the MRF141G may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems.

The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode

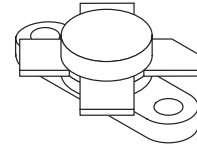
Designed for power amplifier applications in industrial, commercial and amateur radio equipment to 175 MHz.

- Superior High Order IMD
- Specified 50 Volts, 30 MHz Characteristics
Output Power = 30 Watts
Power Gain = 18 dB (Typ)
Efficiency = 40% (Typ)
- $IMD_{(d3)}$ (30 W PEP) — -35 dB (Typ)
- $IMD_{(d11)}$ (30 W PEP) — -60 dB (Typ)
- 100% Tested For Load Mismatch At All Phase Angles With 30:1 VSWR
- Lower Reverse Transfer Capacitance (3.0 pF Typical)



MRF148A

30 W, to 175 MHz
N-CHANNEL MOS
LINEAR RF POWER
FET



CASE 211-07, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	120	Vdc
Drain-Gate Voltage	V_{DGO}	120	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	6.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	115 0.66	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.52	$^\circ\text{C/W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 10\text{ mA}$)	$V_{(BR)DSS}$	125	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 50\text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	1.0	mAdc
Gate–Body Leakage Current ($V_{GS} = 20\text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	100	nAdc

ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}, I_D = 10\text{ mA}$)	$V_{GS(th)}$	1.0	2.5	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}, I_D = 2.5\text{ A}$)	$V_{DS(on)}$	1.0	3.0	5.0	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}, I_D = 2.5\text{ A}$)	g_{fs}	0.8	1.2	—	mhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{iss}	—	62	—	pF
Output Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{oss}	—	35	—	pF
Reverse Transfer Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{rss}	—	3.0	—	pF

FUNCTIONAL TESTS (SSB)

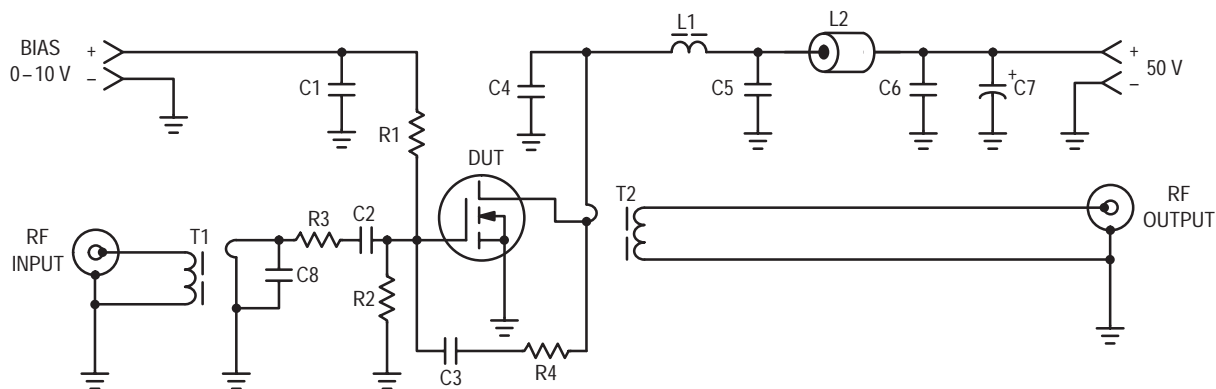
Common Source Amplifier Power Gain ($V_{DD} = 50\text{ V}, P_{out} = 30\text{ W (PEP)}, I_{DQ} = 100\text{ mA}$)	(30 MHz) (175 MHz)	G_{ps}	— —	18 15	— —	dB
Drain Efficiency ($V_{DD} = 50\text{ V}, f = 30\text{ MHz}, I_{DQ} = 100\text{ mA}$)	(30 W PEP) (30 W CW)	η	— —	40 50	— —	%
Intermodulation Distortion ($V_{DD} = 50\text{ V}, P_{out} = 30\text{ W (PEP)}, f = 30; 30.001\text{ MHz}, I_{DQ} = 100\text{ mA}$)		IMD(d3) IMD(d11)	— —	-35 -60	— —	dB
Load Mismatch ($V_{DD} = 50\text{ V}, P_{out} = 30\text{ W (PEP)}, f = 30; 30.001\text{ MHz}, I_{DQ} = 100\text{ mA}, VSWR 30:1$ at all Phase Angles)		ψ	No Degradation in Output Power			

CLASS A PERFORMANCE

Intermodulation Distortion (1) and Power Gain ($V_{DD} = 50\text{ V}, P_{out} = 10\text{ W (PEP)}, f_1 = 30\text{ MHz}, f_2 = 30.001\text{ MHz}, I_{DQ} = 1.0\text{ A}$)	G_{ps} IMD(d3) IMD(d9–13)	— — —	20 -50 -70	— — —	dB
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NOTE:

- To MIL–STD–1311 Version A, Test Method 2204B, Two Tone, Reference Each Tone.



C1, C2, C3, C4, C5, C6 — 0.1 μF Ceramic Chip or Equivalent
 C7 — 10 μF , 100 V Electrolytic
 C8 — 100 pF Dipped Mica
 L1 — VK200 20/4B Ferrite Choke or Equivalent (3.0 μH)
 L2 — Ferrite Bead(s), 2.0 μH

R1, R2 — 200 Ω , 1/2 W Carbon
 R3 — 4.7 Ω , 1/2 W Carbon
 R4 — 470 Ω , 1.0 W Carbon
 T1 — 4:1 Impedance Transformer
 T2 — 1:2 Impedance Transformer

Figure 1. 2.0 to 50 MHz Broadband Test Circuit

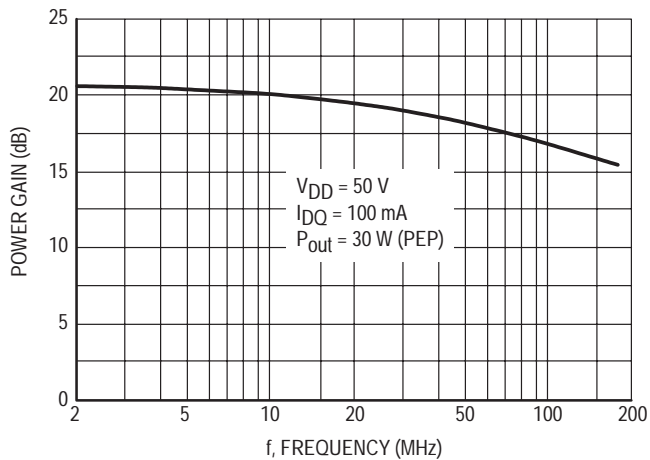


Figure 2. Power Gain versus Frequency

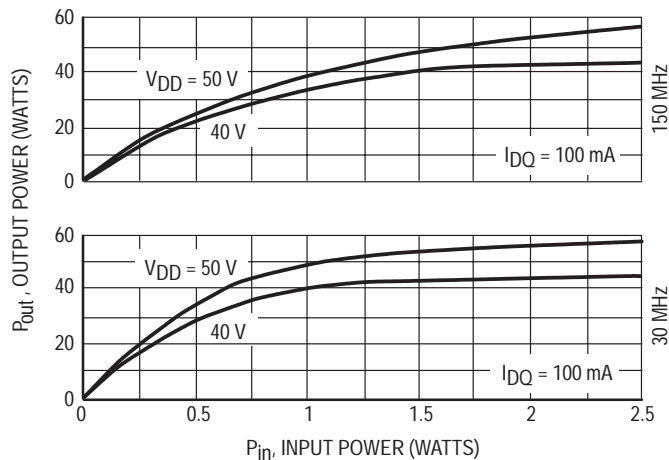


Figure 3. Output Power versus Input Power

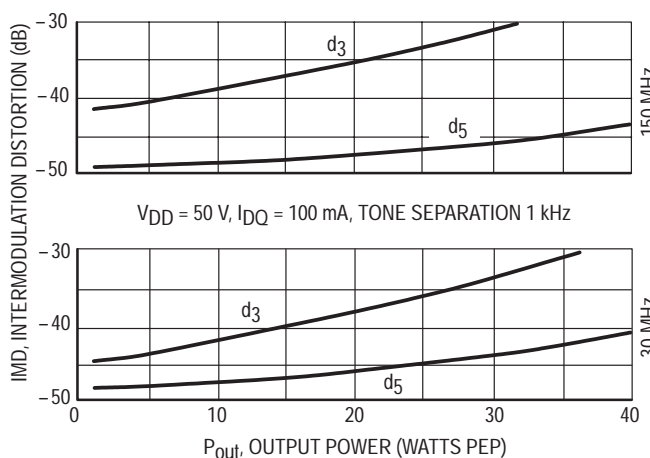


Figure 4. IMD versus Pout

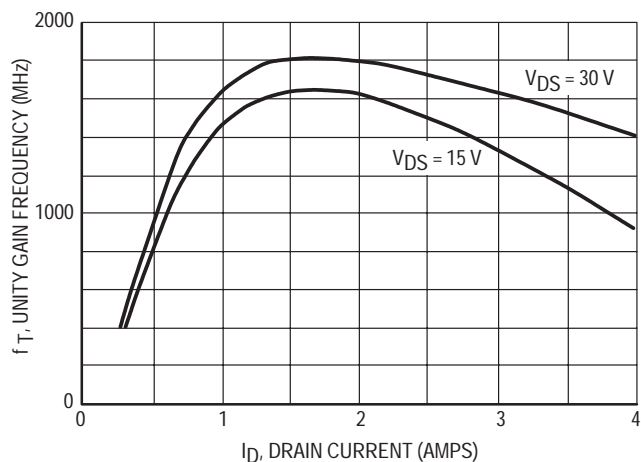


Figure 5. Common Source Unity Gain Frequency versus Drain Current

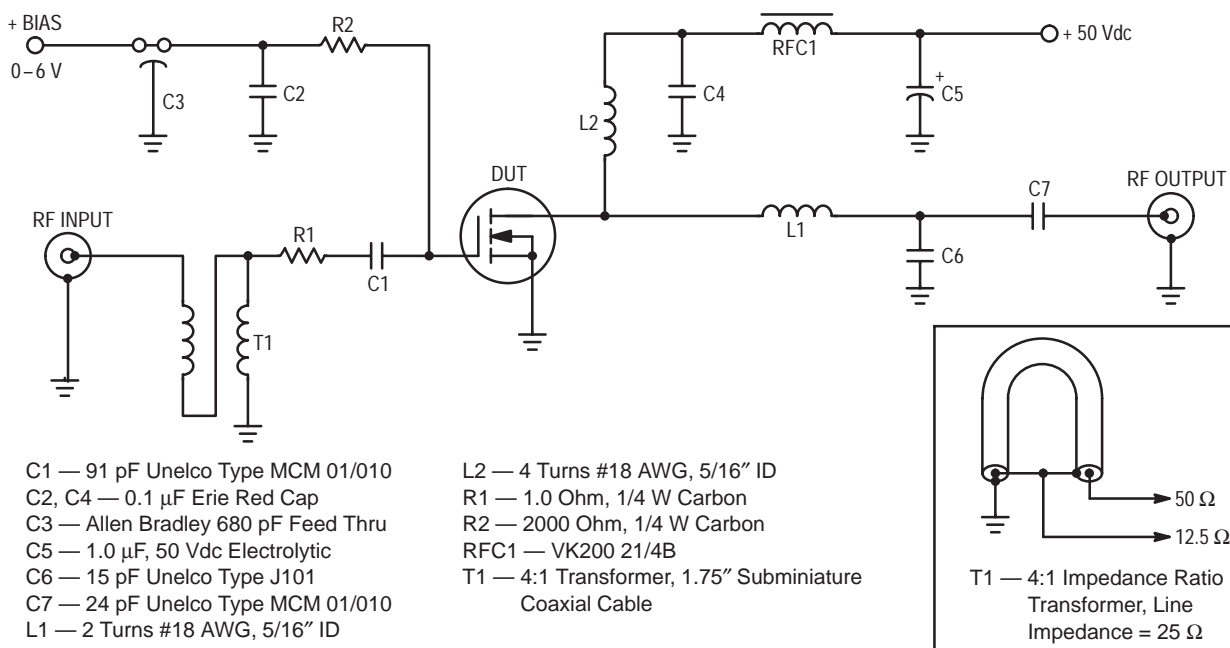


Figure 6. 150 MHz Test Circuit

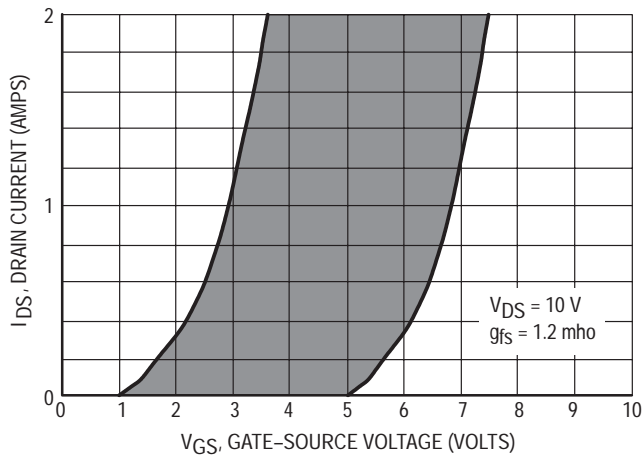


Figure 7. Gate Voltage versus Drain Current

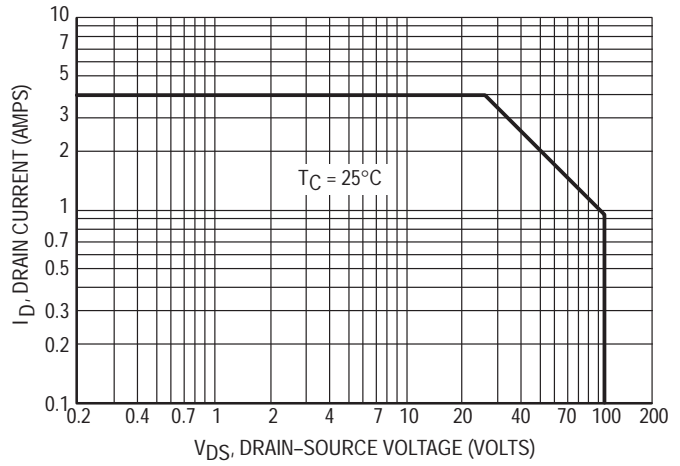
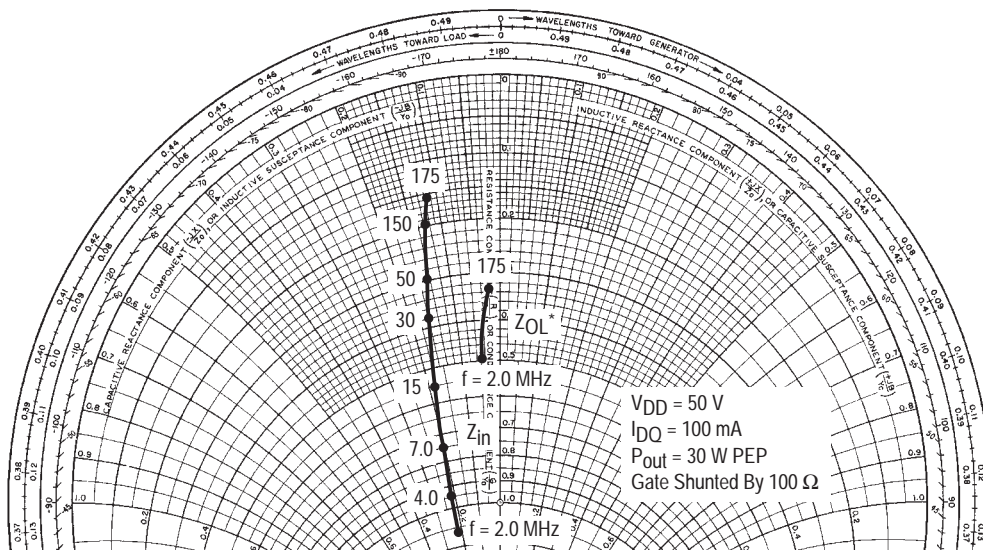


Figure 8. DC Safe Operating Area (SOA)



Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

Figure 9. Impedance Coordinates — 50 Ohm Characteristic Impedance

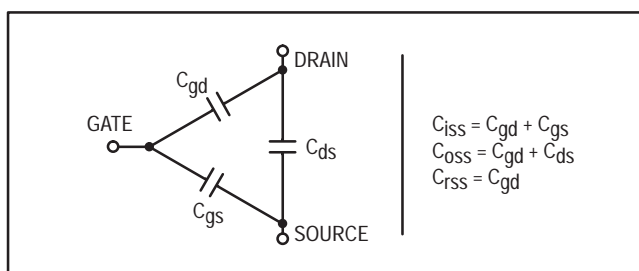
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 5 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors.

Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

EQUIVALENT TRANSISTOR PARAMETER TERMINOLOGY

Collector	Drain
Emitter	Source
Base	Gate
$V_{(BR)CES}$	$V_{(BR)DSS}$
V_{CBO}	V_{DGO}
I_C	I_D
I_{CES}	I_{DSS}
I_{EBO}	I_{GSS}
$V_{BE(on)}$	$V_{GS(th)}$
$V_{CE(sat)}$	$V_{DS(on)}$
C_{ib}	C_{iss}
C_{ob}	C_{oss}
h_{fe}	g_{fs}
$R_{CE(sat)} = \frac{V_{CE(sat)}}{I_C}$	$r_{DS(on)} = \frac{V_{DS(on)}}{I_D}$

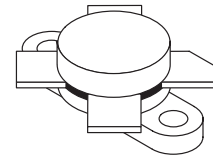
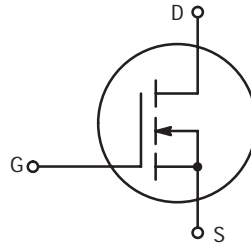
The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode

Designed primarily for linear large-signal output stages up to 150 MHz frequency range.

- Specified 50 Volts, 30 MHz Characteristics
Output Power = 150 Watts
Power Gain = 17 dB (Typ)
Efficiency = 45% (Typ)
- Superior High Order IMD
- IMD(d3) (150 W PEP) — -32 dB (Typ)
- IMD(d11) (150 W PEP) — -60 dB (Typ)
- 100% Tested For Load Mismatch At All Phase Angles With 30:1 VSWR
- S-Parameters Available for Download into Frequency Domain Simulators. See <http://motorola.com/sps/rf/designrtds/>

MRF150

150 W, to 150 MHz
N-CHANNEL MOS
LINEAR RF POWER
FET



CASE 211-11, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	125	Vdc
Drain-Gate Voltage	V_{DGO}	125	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	16	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	300 1.71	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.6	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 100\text{ mA}$)	$V_{(BR)DSS}$	125	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 50\text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	5.0	mAdc
Gate–Body Leakage Current ($V_{GS} = 20\text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}, I_D = 100\text{ mA}$)	$V_{GS(th)}$	1.0	3.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}, I_D = 10\text{ A}$)	$V_{DS(on)}$	1.0	3.0	5.0	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}, I_D = 5.0\text{ A}$)	g_{fs}	4.0	7.0	—	mhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{iss}	—	400	—	pF
Output Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{oss}	—	240	—	pF
Reverse Transfer Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{rss}	—	40	—	pF

FUNCTIONAL TESTS (SSB)

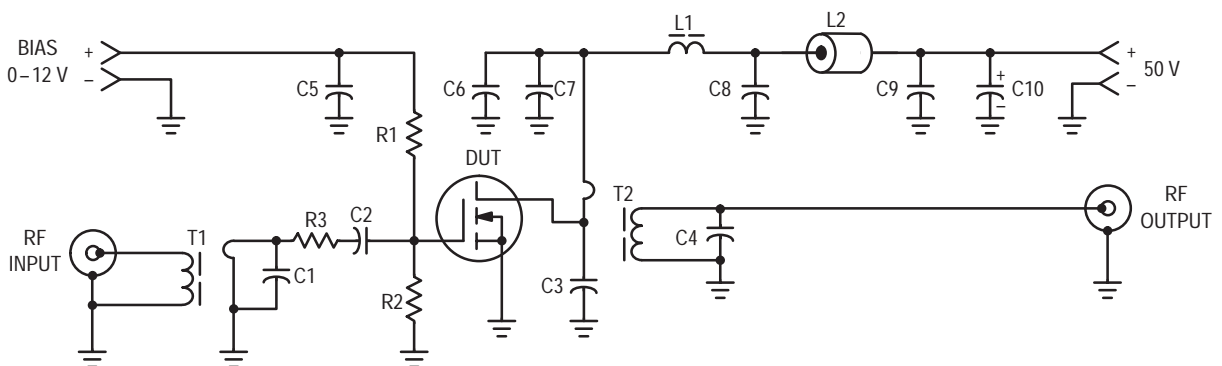
Common Source Amplifier Power Gain ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, I_{DQ} = 250\text{ mA}$)	G_{ps}	—	17 8.0	—	dB
Drain Efficiency ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, f = 30; 30.001\text{ MHz}, I_D(\text{Max}) = 3.75\text{ A}$)	η	—	45	—	%
Intermodulation Distortion (1) ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, f_1 = 30\text{ MHz}, f_2 = 30.001\text{ MHz}, I_{DQ} = 250\text{ mA}$)	IMD(d3) IMD(d11)	—	—32 —60	—	dB
Load Mismatch ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, f = 30; 30.001\text{ MHz}, I_{DQ} = 250\text{ mA}, V_{SWR} 30:1$ at all Phase Angles)	ψ	No Degradation in Output Power			

CLASS A PERFORMANCE

Intermodulation Distortion (1) and Power Gain ($V_{DD} = 50\text{ V}, P_{out} = 50\text{ W (PEP)}, f_1 = 30\text{ MHz}, f_2 = 30.001\text{ MHz}, I_{DQ} = 3.0\text{ A}$)	G_{PS} IMD(d3) IMD(d9–13)	—	20 —50 —75	—	dB
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NOTE:

- To MIL–STD–1311 Version A, Test Method 2204B, Two Tone, Reference Each Tone.



- | | |
|--|--|
| C1 — 470 pF Dipped Mica | C10 — 10 $\mu\text{F}/100\text{ V}$ Electrolytic |
| C2, C5, C6, C7, C8, C9 — 0.1 μF Ceramic Chip or Monolithic with Short Leads | L1 — VK200/4B Ferrite Choke or Equivalent, 3.0 μH |
| C3 — 200 pF Unencapsulated Mica or Dipped Mica with Short Leads | L2 — Ferrite Bead(s), 2.0 μH |
| C4 — 15 pF Unencapsulated Mica or Dipped Mica with Short Leads | R1, R2 — 51 $\Omega/1.0\text{ W}$ Carbon |
| | R3 — 3.3 $\Omega/1.0\text{ W}$ Carbon (or 2.0 x 6.8 $\Omega/1/2\text{ W}$ in Parallel) |
| | T1 — 9:1 Broadband Transformer |
| | T2 — 1:9 Broadband Transformer |

Figure 1. 30 MHz Test Circuit (Class AB)

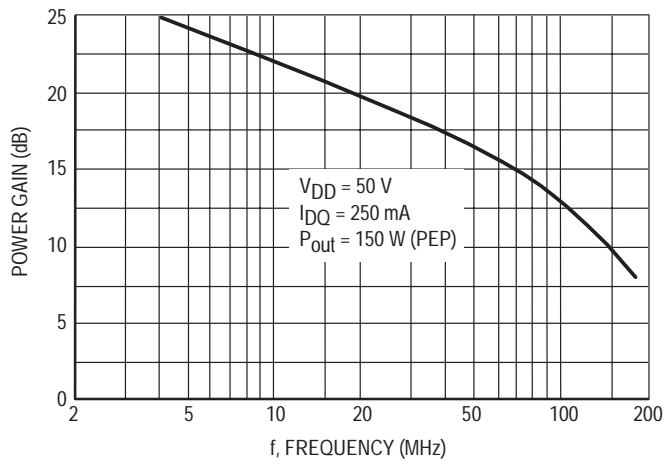


Figure 2. Power Gain versus Frequency

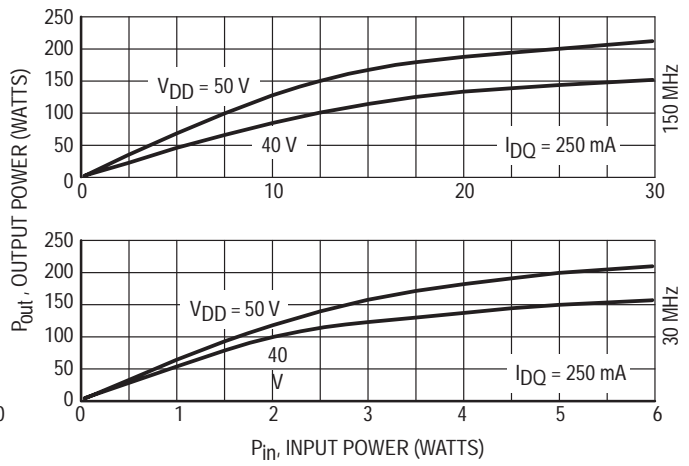


Figure 3. Output Power versus Input Power

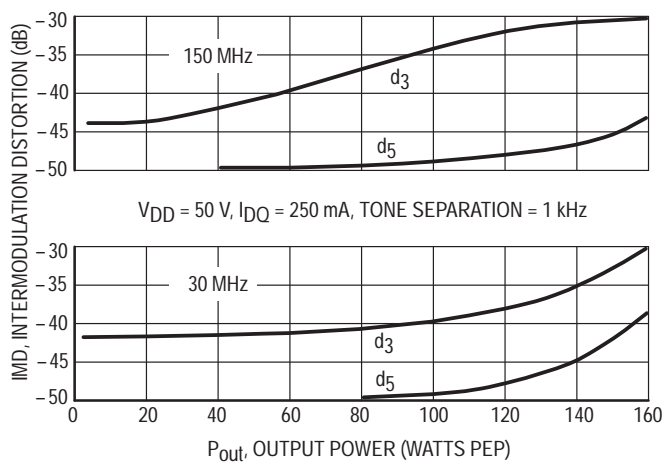


Figure 4. IMD versus P_{out}

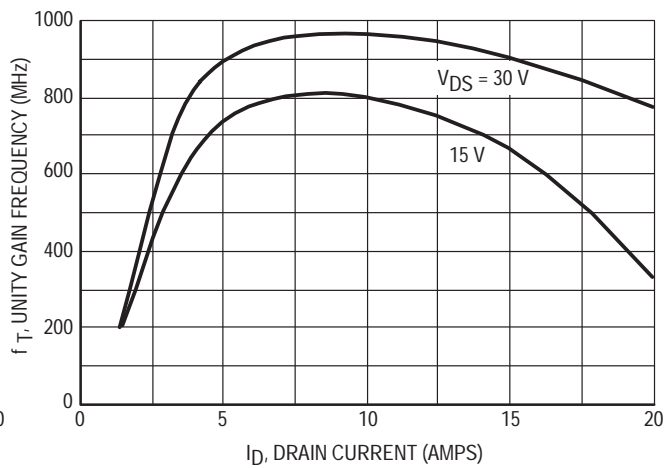


Figure 5. Common Source Unity Gain Frequency versus Drain Current

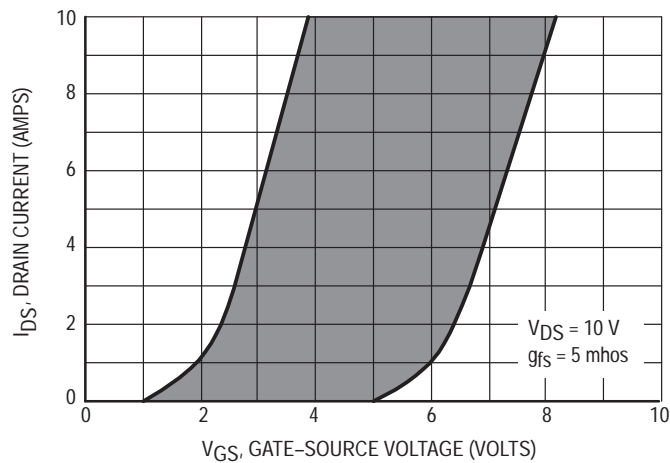
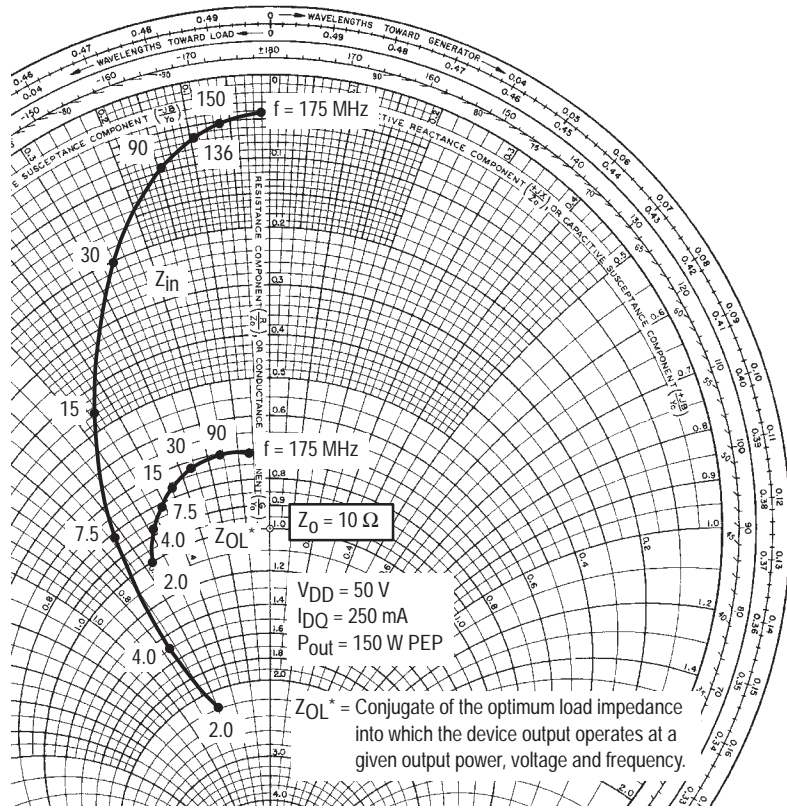
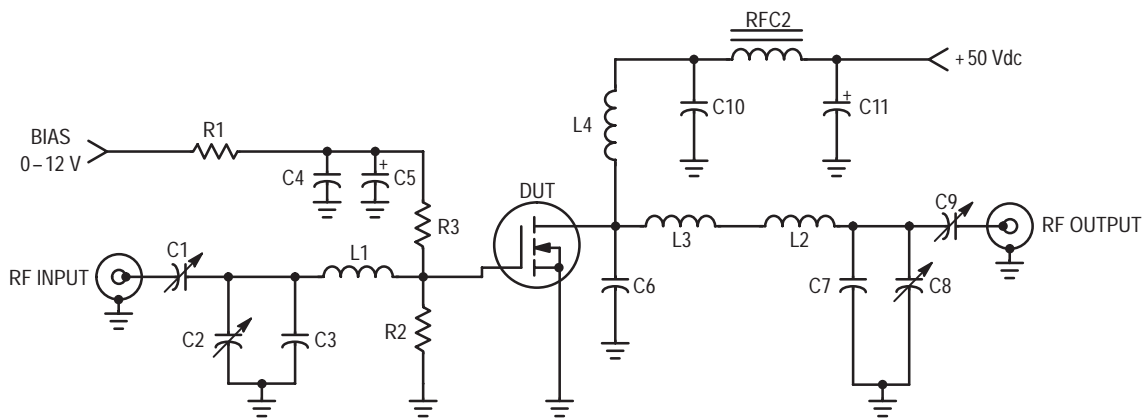


Figure 6. Gate Voltage versus Drain Current



NOTE: Gate Shunted by 25 Ohms.

Figure 7. Series Equivalent Impedance



- C1, C2, C8 — Arco 463 or equivalent
- C3 — 25 pF, Unelco
- C4 — 0.1 μF , Ceramic
- C5 — 1.0 μF , 15 WV Tantalum
- C6 — 25 pF, Unelco J101
- C7 — 25 pF, Unelco J101
- C9 — Arco 262 or equivalent
- C10 — 0.05 μF , Ceramic
- C11 — 15 μF , 60 WV Electrolytic

- L1 — 3/4", 18 AWG into Hairpin
- L2 — Printed Line, 0.200" x 0.500"
- L3 — 1", #16 AWG into Hairpin
- L4 — 2 Turns #16 AWG, 5/16 ID
- RFC1 — 5.6 μH , Choke
- RFC2 — VK200-4B
- R1 — 150 Ω , 1.0 W Carbon
- R2 — 10 k Ω , 1/2 W Carbon
- R3 — 120 Ω , 1/2 W Carbon

Figure 8. 150 MHz Test Circuit (Class AB)

Table 1. Common Source S-Parameters ($V_{DS} = 50\text{ V}$, $I_D = 2\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.936	-179	4.13	84	0.011	22	0.844	-176
40	0.936	-179	3.16	79	0.012	23	0.842	-180
50	0.936	-180	2.52	75	0.013	29	0.855	-179
60	0.937	180	2.13	72	0.014	36	0.854	179
70	0.939	179	1.81	68	0.013	42	0.870	179
80	0.940	179	1.53	67	0.013	45	0.868	-179
90	0.941	179	1.34	65	0.014	46	0.855	-178
100	0.942	179	1.21	60	0.016	46	0.874	180
110	0.942	179	1.11	58	0.018	52	0.875	178
120	0.945	178	0.99	56	0.019	61	0.893	180
130	0.946	178	0.88	53	0.019	67	0.902	-179
140	0.947	178	0.83	52	0.019	68	0.919	-179
150	0.949	177	0.74	49	0.020	63	0.910	-179
160	0.949	177	0.71	46	0.024	62	0.889	-180
170	0.952	177	0.65	44	0.026	68	0.878	179
180	0.953	177	0.59	42	0.029	72	0.921	179
190	0.954	176	0.57	41	0.029	75	0.949	178
200	0.956	176	0.52	39	0.028	74	0.929	178
210	0.955	176	0.51	38	0.030	71	0.934	179
220	0.957	175	0.49	35	0.034	70	0.918	177
230	0.960	175	0.43	32	0.039	71	0.977	175
240	0.959	175	0.42	32	0.040	74	0.941	175
250	0.961	175	0.39	32	0.040	77	0.944	176
260	0.961	175	0.36	31	0.040	76	0.948	177
270	0.960	174	0.35	29	0.043	74	0.947	175
280	0.963	174	0.34	29	0.046	73	0.929	174
290	0.963	174	0.32	25	0.048	74	0.918	172
300	0.965	173	0.32	28	0.051	78	0.925	174
310	0.966	173	0.29	27	0.052	79	0.953	174
320	0.963	173	0.28	26	0.054	76	0.954	172
330	0.965	172	0.26	22	0.057	74	0.914	171
340	0.966	172	0.26	27	0.058	72	0.925	171
350	0.965	172	0.26	25	0.062	75	0.934	171
360	0.968	171	0.25	25	0.065	74	0.979	171
370	0.967	171	0.23	24	0.064	73	0.993	168
380	0.967	171	0.24	22	0.068	74	0.952	172
390	0.969	170	0.22	26	0.069	74	0.942	170
400	0.968	170	0.21	23	0.072	76	0.936	172
410	0.968	170	0.21	24	0.076	73	0.984	168
420	0.970	169	0.20	25	0.078	71	0.977	167
430	0.969	169	0.18	25	0.082	72	0.959	168
440	0.970	169	0.19	25	0.082	73	0.953	169

Table 1. Common Source S-Parameters ($V_{DS} = 50\text{ V}$, $I_D = 2\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	ϕ	S ₂₁	ϕ	S ₁₂	ϕ	S ₂₂	ϕ
450	0.971	168	0.19	24	0.085	75	0.960	168
460	0.972	168	0.17	26	0.086	70	0.960	164
470	0.972	168	0.17	23	0.087	70	0.952	165
480	0.969	167	0.18	26	0.093	70	0.977	166
490	0.969	167	0.18	25	0.099	71	0.966	166
500	0.969	166	0.17	26	0.101	71	0.972	164

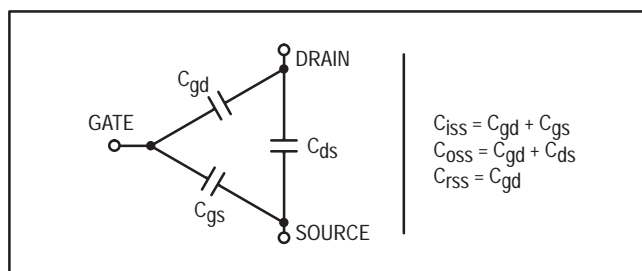
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 5 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors.

Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

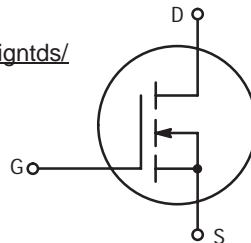
EQUIVALENT TRANSISTOR PARAMETER TERMINOLOGY

Collector	Drain
Emitter	Source
Base	Gate
$V_{(BR)CES}$	$V_{(BR)DSS}$
V_{CBO}	V_{DGO}
I_C	I_D
I_{CES}	I_{DSS}
I_{EBO}	I_{GSS}
$V_{BE(on)}$	$V_{GS(th)}$
$V_{CE(sat)}$	$V_{DS(on)}$
C_{ib}	C_{iss}
C_{ob}	C_{oss}
h_{fe}	g_{fs}
$R_{CE(sat)} = \frac{V_{CE(sat)}}{I_C}$	$r_{DS(on)} = \frac{V_{DS(on)}}{I_D}$

The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode MOSFET

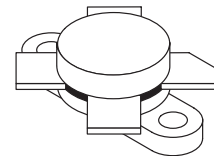
Designed for broadband commercial and military applications at frequencies to 175 MHz. The high power, high gain and broadband performance of this device makes possible solid state transmitters for FM broadcast or TV channel frequency bands.

- Guaranteed Performance at 30 MHz, 50 V:
Output Power — 150 W
Gain — 18 dB (22 dB Typ)
Efficiency — 40%
- Typical Performance at 175 MHz, 50 V:
Output Power — 150 W
Gain — 13 dB
- Low Thermal Resistance
- Ruggedness Tested at Rated Output Power
- Nitride Passivated Die for Enhanced Reliability
- S-Parameters Available for Download into Frequency Domain Simulators. See <http://motorola.com/sps/ef/designtds/>



MRF151

150 W, 50 V, 175 MHz
N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 211-11, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	125	Vdc
Drain-Gate Voltage	V_{DGO}	125	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	16	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	300 1.71	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.6	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0, I_D = 100\text{ mA}$)	$V_{(BR)DSS}$	125	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 50\text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	5.0	mAdc
Gate-Body Leakage Current ($V_{GS} = 20\text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}, I_D = 100\text{ mA}$)	$V_{GS(th)}$	1.0	3.0	5.0	Vdc
Drain-Source On-Voltage ($V_{GS} = 10\text{ V}, I_D = 10\text{ A}$)	$V_{DS(on)}$	1.0	3.0	5.0	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}, I_D = 5.0\text{ A}$)	g_{fs}	5.0	7.0	—	mhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{iss}	—	350	—	pF
Output Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{oss}	—	220	—	pF
Reverse Transfer Capacitance ($V_{DS} = 50\text{ V}, V_{GS} = 0, f = 1.0\text{ MHz}$)	C_{rss}	—	15	—	pF

FUNCTIONAL TESTS

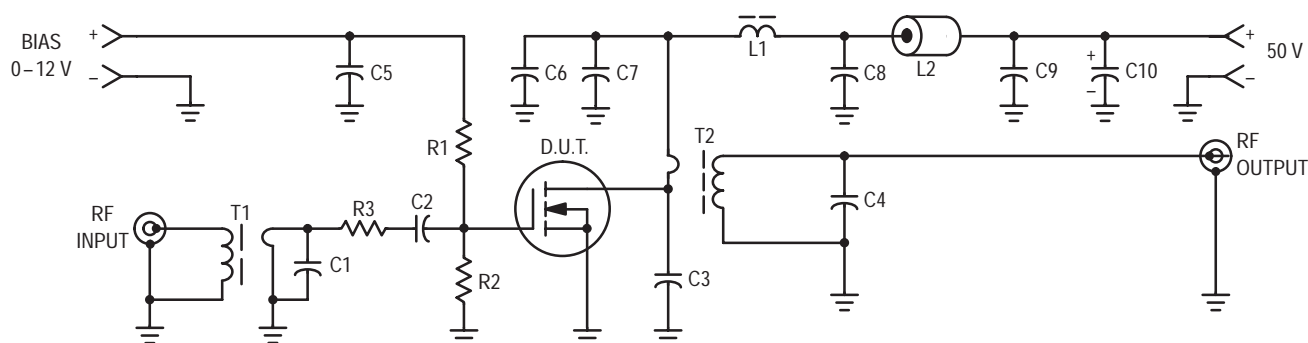
Common Source Amplifier Power Gain, $f = 30; 30.001\text{ MHz}$ ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, I_{DQ} = 250\text{ mA}$) $f = 175\text{ MHz}$	G_{ps}	18	22	—	dB
Drain Efficiency ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, f = 30; 30.001\text{ MHz}, I_D (\text{Max}) = 3.75\text{ A}$)	η	40	45	—	%
Intermodulation Distortion (1) ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, f = 30\text{ MHz}, f_2 = 30.001\text{ MHz}, I_{DQ} = 250\text{ mA}$)	IMD(d3) IMD(d11)	—	-32 -60	-30 —	dB
Load Mismatch ($V_{DD} = 50\text{ V}, P_{out} = 150\text{ W (PEP)}, f_1 = 30; 30.001\text{ MHz}, I_{DQ} = 250\text{ mA}, \text{VSWR } 30:1 \text{ at all Phase Angles}$)	ψ	No Degradation in Output Power			

CLASS A PERFORMANCE

Intermodulation Distortion (1) and Power Gain ($V_{DD} = 50\text{ V}, P_{out} = 50\text{ W (PEP)}, f_1 = 30\text{ MHz}, f_2 = 30.001\text{ MHz}, I_{DQ} = 3.0\text{ A}$)	G_{PS} IMD(d3) IMD(d9-13)	—	23 -50 -75	— — —	dB
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NOTE:

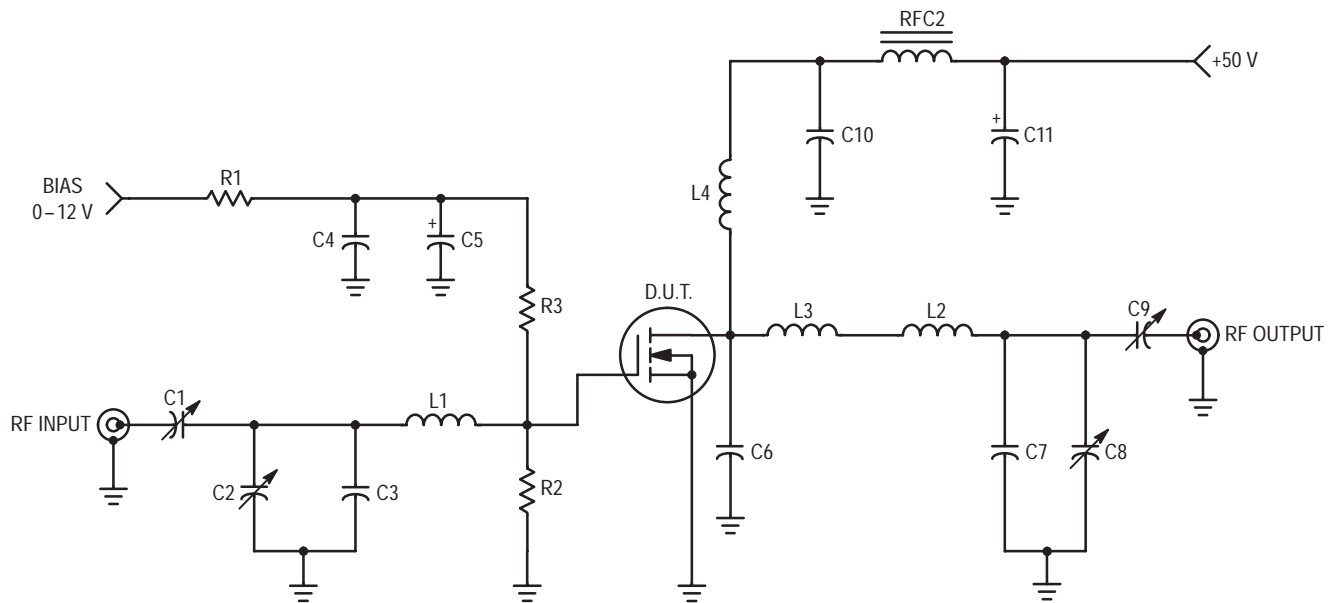
- To MIL-STD-1311 Version A, Test Method 2204B, Two Tone, Reference Each Tone.



- C1 — 470 pF Dipped Mica
- C2, C5, C6, C7, C8, C9 — 0.1 μF Ceramic Chip or Monolithic with Short Leads
- C3 — 200 pF Unencapsulated Mica or Dipped Mica with Short Leads
- C4 — 15 pF Unencapsulated Mica or Dipped Mica with Short Leads
- C10 — 10 $\mu\text{F}/100\text{ V}$ Electrolytic

- L1 — VK200/4B Ferrite Choke or Equivalent, 3.0 μH
- L2 — Ferrite Bead(s), 2.0 μH
- R1, R2 — 51 $\Omega/1.0\text{ W}$ Carbon
- R3 — 3.3 $\Omega/1.0\text{ W}$ Carbon (or 2.0 x 6.8 $\Omega/1/2\text{ W}$ in Parallel)
- T1 — 9:1 Broadband Transformer
- T2 — 1:9 Broadband Transformer
- Board Material — 0.062" Fiberglass (G10), 1 oz. Copper Clad, 2 Sides, $\epsilon_r = 5$

Figure 1. 30 MHz Test Circuit



- C1, C2, C8 — Arco 463 or equivalent
- C3 — 25 pF, Unelco
- C4 — 0.1 μ F, Ceramic
- C5 — 1.0 μ F, 15 WV Tantalum
- C6 — 15 pF, Unelco J101
- C7 — 25 pF, Unelco J101
- C9 — Arco 262 or equivalent
- C10 — 0.05 μ F, Ceramic
- C11 — 15 μ F, 60 WV Electrolytic
- D1 — 1N5347 Zener Diode

- L1 — 3/4", #18 AWG into Hairpin
- L2 — Printed Line, 0.200" x 0.500"
- L3 — 1", #16 AWG into Hairpin
- L4 — 2 Turns, #16 AWG, 5/16 ID
- RFC1 — 5.6 μ H, Choke
- RFC2 — VK200-4B
- R1 — 150 Ω , 1.0 W Carbon
- R2 — 10 k Ω , 1/2 W Carbon
- R3 — 120 Ω , 1/2 W Carbon
- Board Material — 0.062" Fiberglass (G10),
1 oz. Copper Clad, 2 Sides, $\epsilon_r = 5.0$

Figure 2. 175 MHz Test Circuit

TYPICAL CHARACTERISTICS

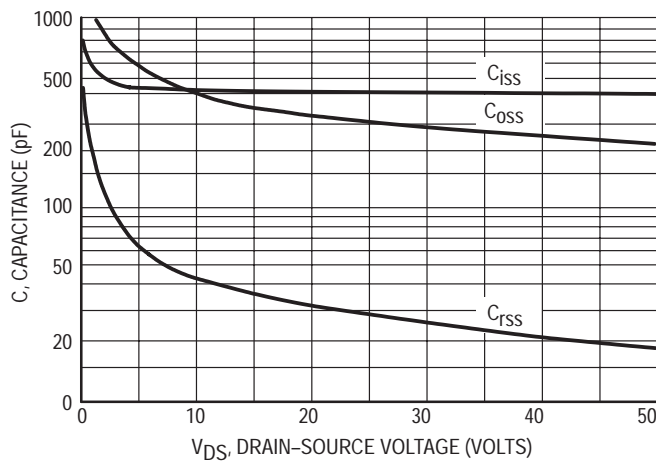


Figure 3. Capacitance versus Drain-Source Voltage

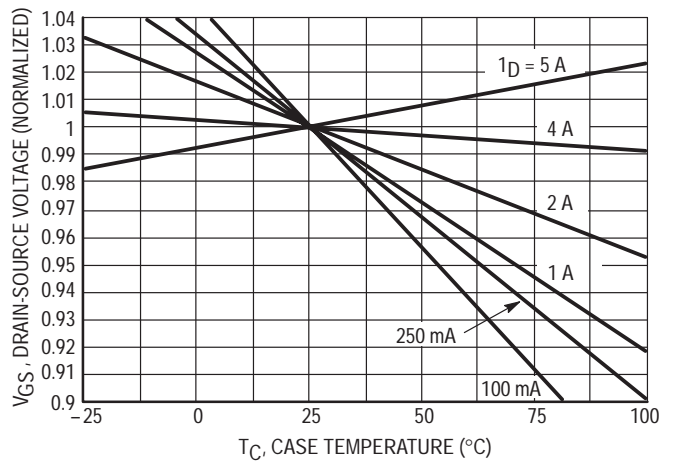


Figure 4. Gate-Source Voltage versus Case Temperature

TYPICAL CHARACTERISTICS

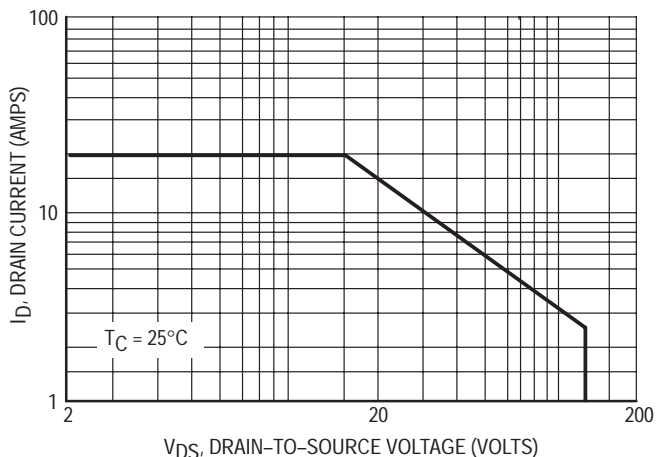


Figure 5. DC Safe Operating Area

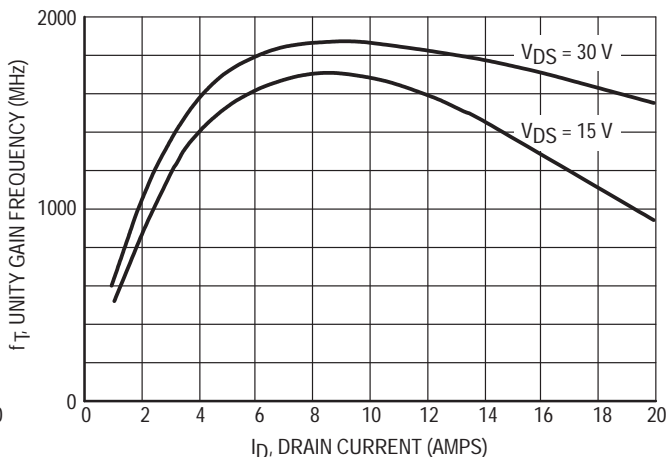


Figure 6. Common Source Unity Gain Frequency versus Drain Current

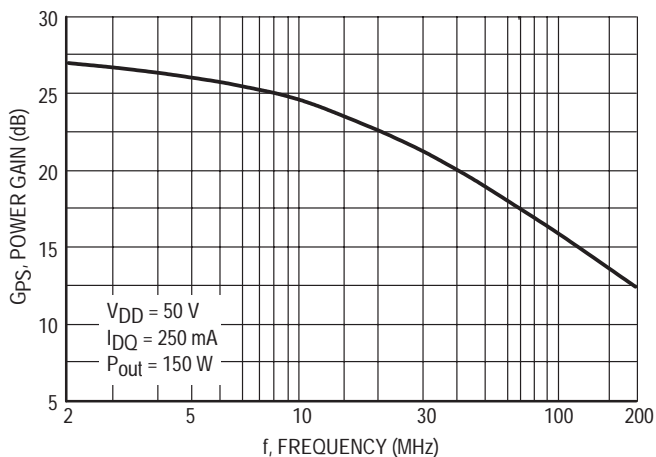


Figure 7. Power Gain versus Frequency

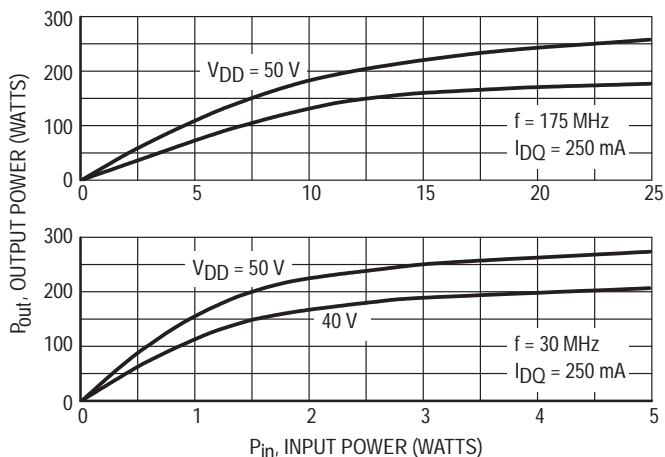


Figure 8. Output Power versus Input Power

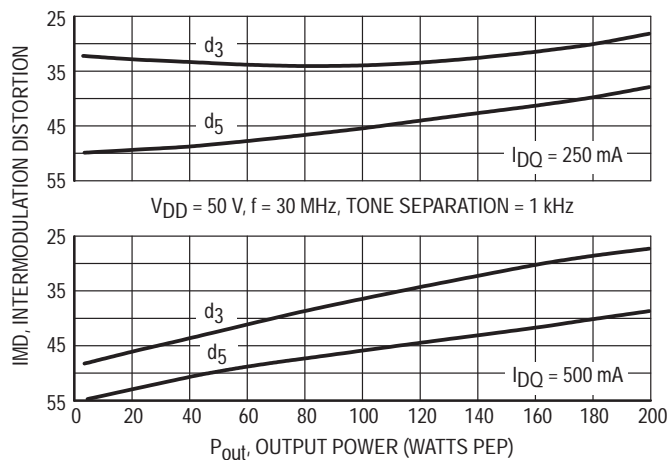


Figure 9. IMD versus Pout

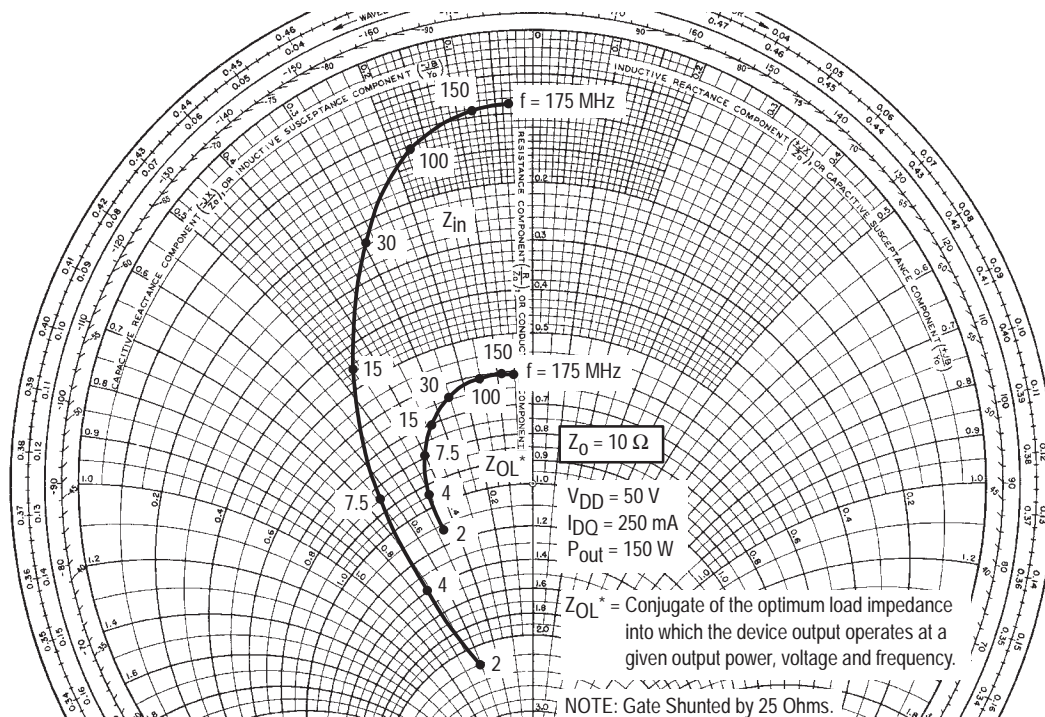


Figure 10. Series Equivalent Impedance

Table 1. Common Source S-Parameters ($V_{DS} = 50$ V, $I_D = 2$ A)

f MHz	S11		S21		S12		S22	
	S11	ϕ	S21	ϕ	S12	ϕ	S22	ϕ
30	0.877	-174	10.10	77	0.008	19	0.707	-169
40	0.886	-175	7.47	69	0.009	24	0.715	-172
50	0.895	-175	5.76	63	0.008	33	0.756	-171
60	0.902	-176	4.73	58	0.009	39	0.764	-171
70	0.912	-176	3.86	52	0.009	46	0.784	-172
80	0.918	-177	3.19	48	0.010	54	0.802	-171
90	0.925	-177	2.69	45	0.011	62	0.808	-171
100	0.932	-177	2.34	40	0.013	67	0.850	-173
110	0.936	-178	2.06	37	0.014	72	0.865	-175
120	0.942	-178	1.77	35	0.015	76	0.875	-173
130	0.946	-179	1.55	32	0.017	77	0.874	-172
140	0.950	-179	1.39	30	0.019	77	0.884	-174
150	0.954	-180	1.23	27	0.021	78	0.909	-175
160	0.957	-180	1.13	24	0.023	79	0.911	-176
170	0.960	180	1.01	22	0.024	82	0.904	-177
180	0.962	179	0.90	20	0.026	82	0.931	-176
190	0.964	179	0.84	19	0.028	80	0.929	-178
200	0.967	179	0.75	18	0.030	79	0.922	-179
210	0.967	178	0.71	16	0.032	80	0.937	-180
220	0.969	178	0.67	14	0.035	82	0.949	180
230	0.971	178	0.60	12	0.038	81	0.950	179
240	0.970	177	0.57	12	0.037	80	0.950	179
250	0.972	177	0.51	12	0.039	80	0.935	179

Table 1. Common Source S-Parameters ($V_{DS} = 50\text{ V}$, $I_D = 2\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
260	0.973	177	0.47	11	0.041	79	0.954	178
270	0.972	176	0.45	9	0.044	80	0.953	176
280	0.974	176	0.41	9	0.046	80	0.965	175
290	0.974	176	0.40	6	0.046	79	0.944	175
300	0.975	176	0.39	10	0.048	82	0.929	176
310	0.976	175	0.36	9	0.049	82	0.943	176
320	0.974	175	0.33	7	0.053	78	0.954	173
330	0.975	174	0.31	4	0.056	78	0.935	172
340	0.976	174	0.30	10	0.056	77	0.948	172
350	0.975	174	0.29	7	0.058	80	0.950	174
360	0.977	174	0.28	8	0.059	79	0.978	172
370	0.976	173	0.26	8	0.061	76	0.981	170
380	0.976	173	0.26	7	0.065	75	0.944	171
390	0.977	173	0.24	10	0.066	76	0.960	171
400	0.976	172	0.23	7	0.068	80	0.955	173
410	0.976	172	0.22	9	0.071	77	0.999	170
420	0.977	172	0.21	9	0.071	76	0.962	168
430	0.976	171	0.19	10	0.073	76	0.950	168
440	0.976	171	0.20	12	0.075	75	0.953	168
450	0.978	171	0.19	10	0.080	77	0.982	168
460	0.978	170	0.18	13	0.082	74	0.990	165
470	0.978	170	0.18	10	0.081	77	0.953	168
480	0.974	170	0.18	13	0.085	78	0.944	167
490	0.973	169	0.17	13	0.086	75	0.966	165
500	0.972	169	0.17	14	0.089	73	0.980	165

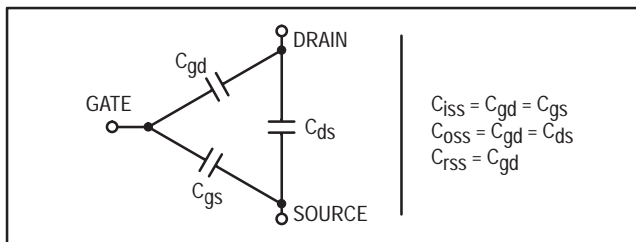
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal anode gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the MOSFET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iSS}), output (C_{oSS}) and reverse transfer (C_{rSS}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iSS} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 6 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors. Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gate of this device is essentially capacitor. Circuits that leave the gate open-circuited or float-

ing should be avoided. These conditions can result in turn-on of the device due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — This device does not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

Using a resistor to keep the gate-to-source impedance low also helps damp transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

HANDLING CONSIDERATIONS

When shipping, the devices should be transported only in antistatic bags or conductive foam. Upon removal from the packaging, careful handling procedures should be adhered to. Those handling the devices should wear grounding straps and devices not in the antistatic packaging should be kept in metal tote bins. MOSFETs should be handled by the case and not by the leads, and when testing the device, all leads should make good electrical contact before voltage is applied. As a final note, when placing the FET into the system it is designed for, soldering should be done with a grounded iron.

DESIGN CONSIDERATIONS

The MRF151 is an RF Power, MOS, N-channel enhancement mode field-effect transistor (FET) designed for HF and VHF power amplifier applications.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power MOSFETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal.

DC BIAS

The MRF151 is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF151 was characterized at $I_{DQ} = 250$ mA, each side, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may be just a simple resistive divider network. Some applications may require a more elaborate bias system.

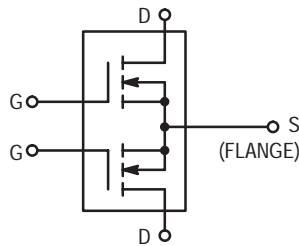
GAIN CONTROL

Power output of the MRF151 may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems.

The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode MOSFET

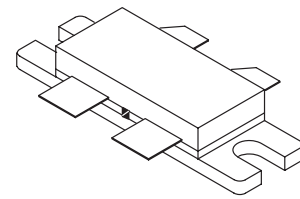
Designed for broadband commercial and military applications at frequencies to 175 MHz. The high power, high gain and broadband performance of this device makes possible solid state transmitters for FM broadcast or TV channel frequency bands.

- Guaranteed Performance at 175 MHz, 50 V:
Output Power — 300 W
Gain — 14 dB (16 dB Typ)
Efficiency — 50%
- Low Thermal Resistance — 0.35°C/W
- Ruggedness Tested at Rated Output Power
- Nitride Passivated Die for Enhanced Reliability
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://motorola.com/sps/rf/designtds/>



MRF151G

300 W, 50 V, 175 MHz
N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 375-04, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	125	Vdc
Drain-Gate Voltage	V_{DGO}	125	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	40	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	500 2.85	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.35	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS (Each Side)

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 100 \text{ mA}$)	$V_{(BR)DSS}$	125	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 50 \text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	5.0	mAdc
Gate–Body Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS (Each Side)

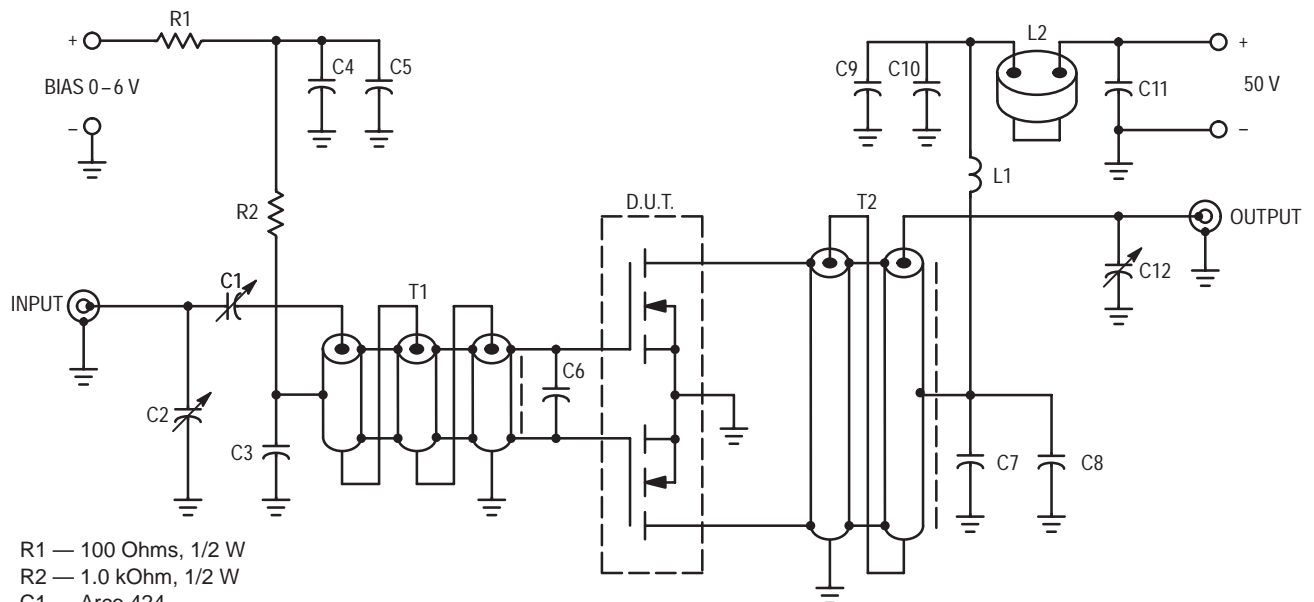
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 100 \text{ mA}$)	$V_{GS(th)}$	1.0	3.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 10 \text{ A}$)	$V_{DS(on)}$	1.0	3.0	5.0	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 5.0 \text{ A}$)	g_{fs}	5.0	7.0	—	mhos

DYNAMIC CHARACTERISTICS (Each Side)

Input Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{iss}	—	350	—	pF
Output Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{oss}	—	220	—	pF
Reverse Transfer Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{rss}	—	15	—	pF

FUNCTIONAL TESTS

Common Source Amplifier Power Gain ($V_{DD} = 50 \text{ V}, P_{Out} = 300 \text{ W}, I_{DQ} = 500 \text{ mA}, f = 175 \text{ MHz}$)	G_{ps}	14	16	—	dB
Drain Efficiency ($V_{DD} = 50 \text{ V}, P_{Out} = 300 \text{ W}, f = 175 \text{ MHz}, I_D (\text{Max}) = 11 \text{ A}$)	η	50	55	—	%
Load Mismatch ($V_{DD} = 50 \text{ V}, P_{Out} = 300 \text{ W}, I_{DQ} = 500 \text{ mA},$ VSWR 5:1 at all Phase Angles)	ψ	No Degradation in Output Power			



- R1 — 100 Ohms, 1/2 W
 - R2 — 1.0 kOhm, 1/2 W
 - C1 — Arco 424
 - C2 — Arco 404
 - C3, C4, C7, C8, C9 — 1000 pF Chip
 - C5, C10 — 0.1 μF Chip
 - C6 — 330 pF Chip
 - C11 — 0.47 μF Ceramic Chip, Kemet 1215 or Equivalent (100 V)
 - C12 — Arco 422
 - L1 — 10 Turns AWG #18 Enameled Wire, Close Wound, 1/4" I.D.
 - L2 — Ferrite Beads of Suitable Material for 1.5–2.0 μH Total Inductance
- Unless Otherwise Noted, All Chip Capacitors are ATC Type 100 or Equivalent.

- T1 — 9:1 RF Transformer. Can be made of 15–18 Ohms Semirigid Co–Ax, 62–90 Mils O.D.
 - T2 — 1:4 RF Transformer. Can be made of 16–18 Ohms Semirigid Co–Ax, 70–90 Mils O.D.
- Board Material — 0.062" Fiberglass (G10), 1 oz. Copper Clad, 2 Sides, $\epsilon_r = 5.0$

NOTE: For stability, the input transformer T1 must be loaded with ferrite toroids or beads to increase the common mode inductance. For operation below 100 MHz. The same is required for the output transformer.

See Figure 6 for construction details of T1 and T2.

Figure 1. 175 MHz Test Circuit

TYPICAL CHARACTERISTICS

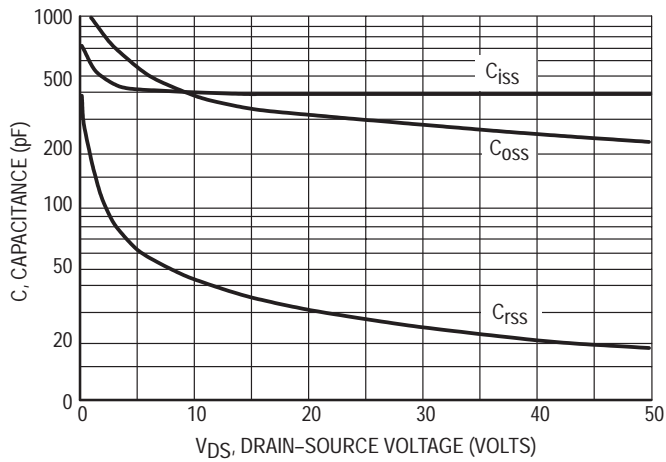


Figure 2. Capacitance versus Drain-Source Voltage*

*Data shown applies to each half of MRF151G.

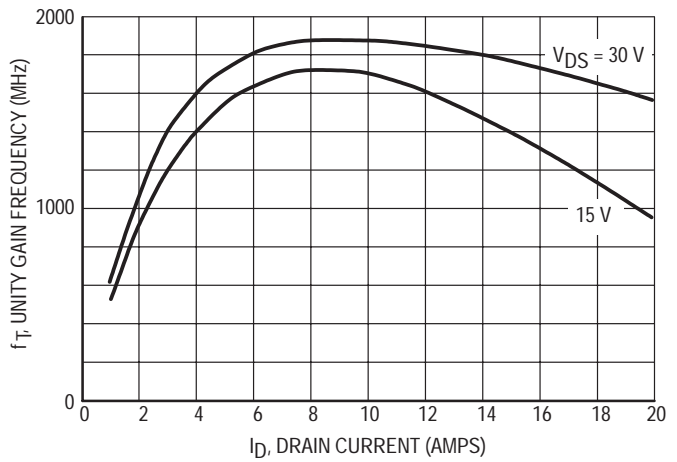


Figure 3. Common Source Unity Gain Frequency versus Drain Current*

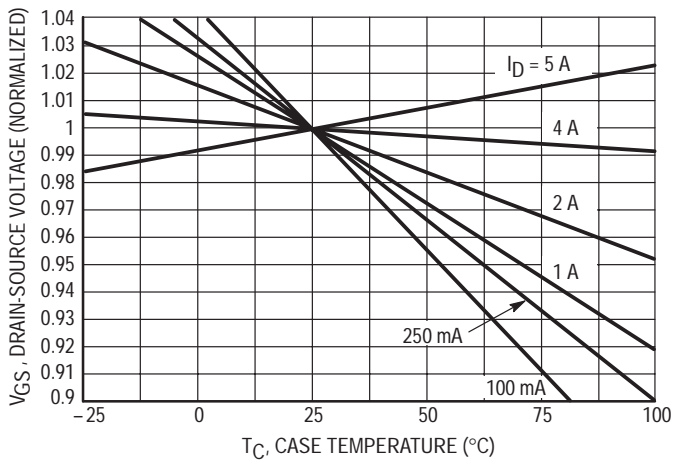


Figure 4. Gate-Source Voltage versus Case Temperature*

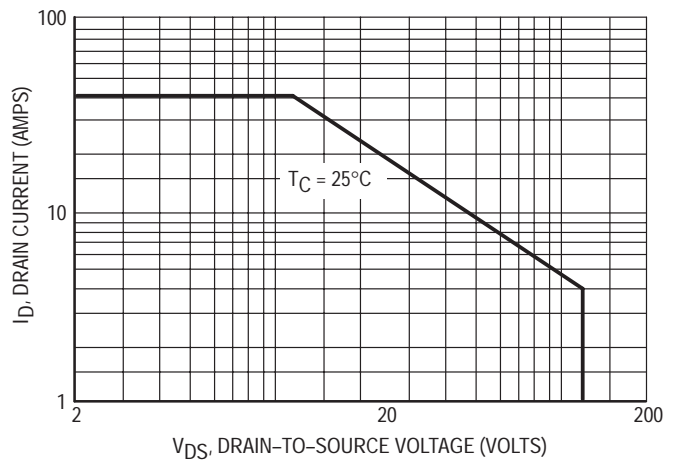


Figure 5. DC Safe Operating Area

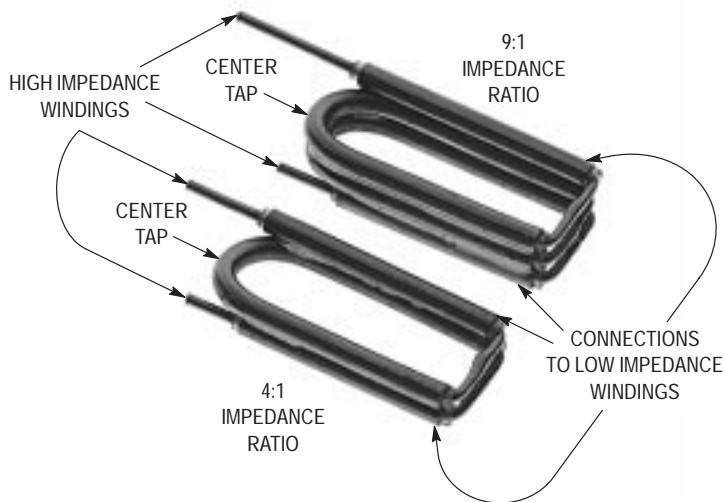


Figure 6. RF Transformer

TYPICAL CHARACTERISTICS

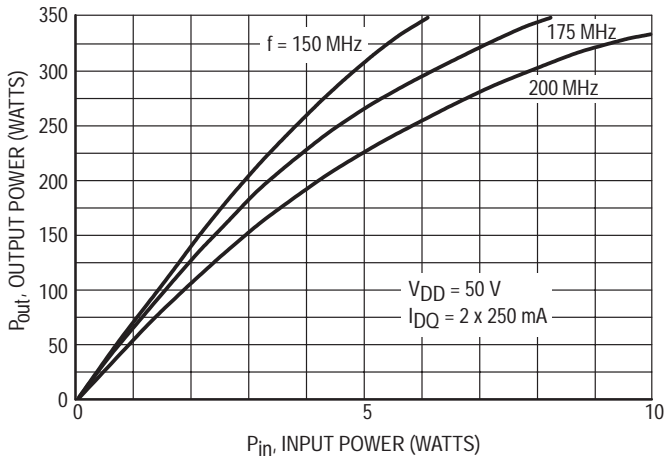


Figure 7. Output Power versus Input Power

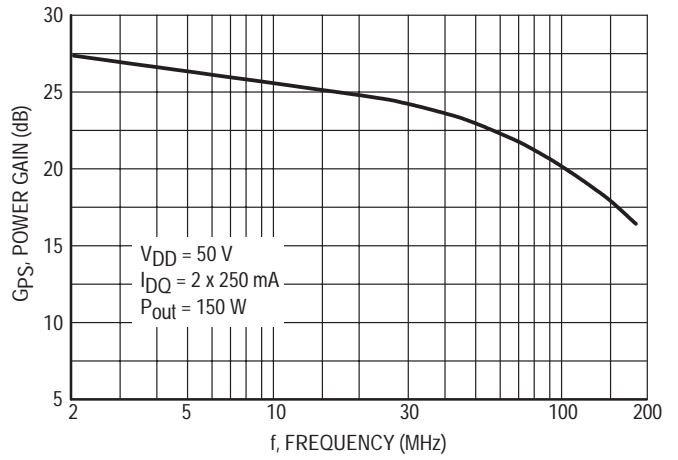
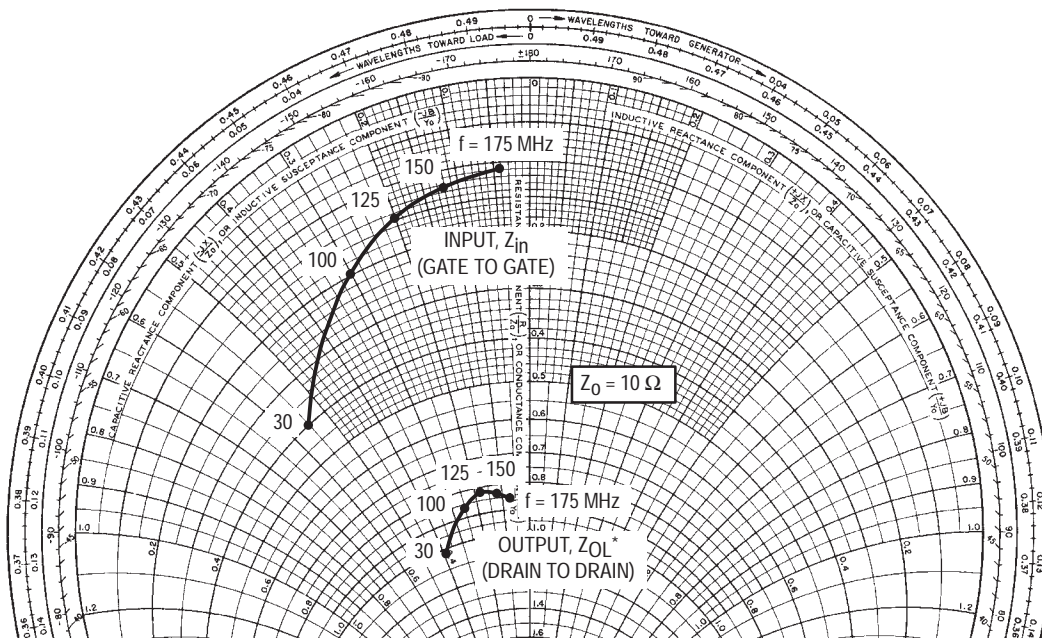


Figure 8. Power Gain versus Frequency



Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

Figure 9. Input and Output Impedance

NOTE: S-Parameter data represents measurements taken from one chip only.

Table 1. Common Source S-Parameters ($V_{DS} = 50\text{ V}$, $I_D = 2\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.877	-174	10.10	77	0.008	19	0.707	-169
40	0.886	-175	7.47	69	0.009	24	0.715	-172
50	0.895	-175	5.76	63	0.008	33	0.756	-171
60	0.902	-176	4.73	58	0.009	39	0.764	-171
70	0.912	-176	3.86	52	0.009	46	0.784	-172
80	0.918	-177	3.19	48	0.010	54	0.802	-171
90	0.925	-177	2.69	45	0.011	62	0.808	-171
100	0.932	-177	2.34	40	0.013	67	0.850	-173
110	0.936	-178	2.06	37	0.014	72	0.865	-175
120	0.942	-178	1.77	35	0.015	76	0.875	-173
130	0.946	-179	1.55	32	0.017	77	0.874	-172
140	0.950	-179	1.39	30	0.019	77	0.884	-174
150	0.954	-180	1.23	27	0.021	78	0.909	-175
160	0.957	-180	1.13	24	0.023	79	0.911	-176
170	0.960	180	1.01	22	0.024	82	0.904	-177
180	0.962	179	0.90	20	0.026	82	0.931	-176
190	0.964	179	0.84	19	0.028	80	0.929	-178
200	0.967	179	0.75	18	0.030	79	0.922	-179
210	0.967	178	0.71	16	0.032	80	0.937	-180
220	0.969	178	0.67	14	0.035	82	0.949	180
230	0.971	178	0.60	12	0.038	81	0.950	179
240	0.970	177	0.57	12	0.037	80	0.950	179
250	0.972	177	0.51	12	0.039	80	0.935	179
260	0.973	177	0.47	11	0.041	79	0.954	178
270	0.972	176	0.45	9	0.044	80	0.953	176
280	0.974	176	0.41	9	0.046	80	0.965	175
290	0.974	176	0.40	6	0.046	79	0.944	175
300	0.975	176	0.39	10	0.048	82	0.929	176
310	0.976	175	0.36	9	0.049	82	0.943	176
320	0.974	175	0.33	7	0.053	78	0.954	173
330	0.975	174	0.31	4	0.056	78	0.935	172
340	0.976	174	0.30	10	0.056	77	0.948	172
350	0.975	174	0.29	7	0.058	80	0.950	174
360	0.977	174	0.28	8	0.059	79	0.978	172
370	0.976	173	0.26	8	0.061	76	0.981	170
380	0.976	173	0.26	7	0.065	75	0.944	171
390	0.977	173	0.24	10	0.066	76	0.960	171
400	0.976	172	0.23	7	0.068	80	0.955	173
410	0.976	172	0.22	9	0.071	77	0.999	170
420	0.977	172	0.21	9	0.071	76	0.962	168
430	0.976	171	0.19	10	0.073	76	0.950	168

Table 1. Common Source S-Parameters ($V_{DS} = 50\text{ V}$, $I_D = 2\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
440	0.976	171	0.20	12	0.075	75	0.953	168
450	0.978	171	0.19	10	0.080	77	0.982	168
460	0.978	170	0.18	13	0.082	74	0.990	165
470	0.978	170	0.18	10	0.081	77	0.953	168
480	0.974	170	0.18	13	0.085	78	0.944	167
490	0.973	169	0.17	13	0.086	75	0.966	165
500	0.972	169	0.17	14	0.089	73	0.980	165

Table 2. Common Source S-Parameters ($V_{DS} = 50\text{ V}$, $I_D = 0.38\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.834	-168	9.70	74	0.014	-10	0.747	-162
40	0.869	-169	6.47	62	0.013	-19	0.731	-159
50	0.883	-170	5.13	55	0.012	-24	0.754	-161
60	0.892	-171	4.03	51	0.011	-24	0.823	-164
70	0.901	-172	3.39	50	0.010	-20	0.912	-167
80	0.911	-173	2.80	47	0.009	-16	0.996	-168
90	0.924	-173	2.39	42	0.008	-14	1.100	-167
100	0.935	-174	1.99	35	0.006	-15	1.100	-167
110	0.945	-174	1.67	29	0.005	-17	1.070	-169
120	0.953	-175	1.36	25	0.004	-10	0.988	-167
130	0.958	-175	1.14	23	0.004	4	0.934	-169
140	0.962	-176	1.01	23	0.004	26	0.935	-170
150	0.964	-177	0.93	24	0.004	45	0.983	-172
160	0.966	-177	0.85	24	0.004	58	1.080	-173
170	0.969	-178	0.79	21	0.005	61	1.170	-173
180	0.972	-178	0.74	17	0.006	57	1.250	-173
190	0.975	-178	0.65	10	0.007	56	1.210	-174
200	0.977	-179	0.56	8	0.008	63	1.110	-174
210	0.979	-179	0.50	7	0.008	72	1.010	-174
220	0.980	-179	0.44	9	0.008	81	0.958	-172
230	0.980	-180	0.41	9	0.009	79	1.020	-175
240	0.981	180	0.38	12	0.009	74	1.020	-178
250	0.982	180	0.38	11	0.011	74	1.060	-176
260	0.983	179	0.34	8	0.014	76	1.180	-179
270	0.984	179	0.34	4	0.014	80	1.220	-180
280	0.984	179	0.30	3	0.013	79	1.180	-179
290	0.984	178	0.27	-4	0.012	73	1.040	-177
300	0.984	178	0.25	0	0.014	69	0.996	-178
310	0.984	178	0.24	4	0.017	74	0.951	-178
320	0.985	177	0.23	7	0.019	83	0.964	179
330	0.985	177	0.20	3	0.019	90	1.060	180
340	0.986	177	0.22	7	0.017	87	1.100	179

Table 2. Common Source S-Parameters ($V_{DS} = 50\text{ V}$, $I_D = 0.38\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
350	0.986	177	0.20	5	0.017	76	1.140	-180
360	0.986	176	0.19	-2	0.021	67	1.160	180
370	0.985	176	0.17	-3	0.024	69	1.100	180
380	0.985	176	0.16	-3	0.024	77	1.070	-180
390	0.985	176	0.15	0	0.021	85	0.993	-180
400	0.985	175	0.14	3	0.018	85	0.962	-180
410	0.985	175	0.14	2	0.021	72	1.040	179
420	0.986	175	0.13	5	0.027	68	1.060	177
430	0.986	174	0.13	4	0.031	73	1.100	177
440	0.986	174	0.13	0	0.030	81	1.140	177
450	0.985	174	0.13	-1	0.025	87	1.110	178
460	0.984	174	0.11	-2	0.022	68	1.090	176
470	0.984	174	0.10	-1	0.025	59	1.020	177
480	0.985	173	0.10	3	0.034	66	0.993	179
490	0.986	173	0.10	1	0.038	79	1.020	178
500	0.986	173	0.10	6	0.035	93	1.010	177

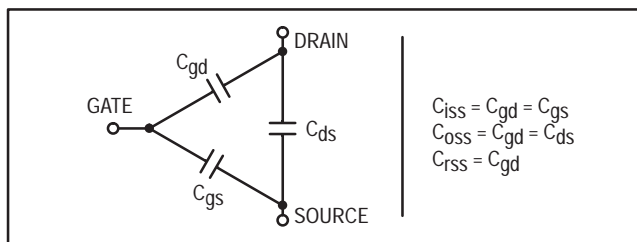
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

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These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 3 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors. Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-cir-

cuted or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

Using a resistor to keep the gate-to-source impedance low also helps damp transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

HANDLING CONSIDERATIONS

When shipping, the devices should be transported only in antistatic bags or conductive foam. Upon removal from the packaging, careful handling procedures should be adhered to. Those handling the devices should wear grounding straps and devices not in the antistatic packaging should be kept in metal tote bins. MOSFETs should be handled by the case and not by the leads, and when testing the device, all leads should make good electrical contact before voltage is applied. As a final note, when placing the FET into the system it is designed for, soldering should be done with a grounded iron.

DESIGN CONSIDERATIONS

The MRF151G is an RF Power, MOS, N-channel enhancement mode field-effect transistor (FET) designed for HF and VHF power amplifier applications.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power MOSFETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal.

DC BIAS

The MRF151G is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF151G was characterized at $I_{DQ} = 250$ mA, each side, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may be just a simple resistive divider network. Some applications may require a more elaborate bias system.

GAIN CONTROL

Power output of the MRF151G may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems.

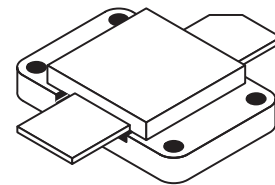
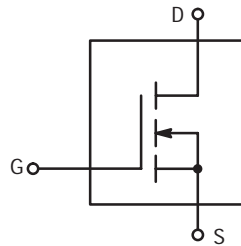
The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode MOSFET

Designed primarily for linear large-signal output stages in the 2.0–100 MHz frequency range.

- Specified 50 Volts, 30 MHz Characteristics
Output Power = 600 Watts
Power Gain = 17 dB (Typ)
Efficiency = 45% (Typ)

MRF154

600 W, 50 V, 80 MHz
N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 368-03, STYLE 2
(HOG PAC)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	125	Vdc
Drain-Gate Voltage	V_{DGO}	125	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	60	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	1350 7.7	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.13	$^\circ\text{C}/\text{W}$

Handling and Packaging — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 100 \text{ mA}$)	$V_{(BR)DSS}$	125	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 50 \text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	20	mAdc
Gate–Body Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	5.0	μAdc

ON CHARACTERISTICS

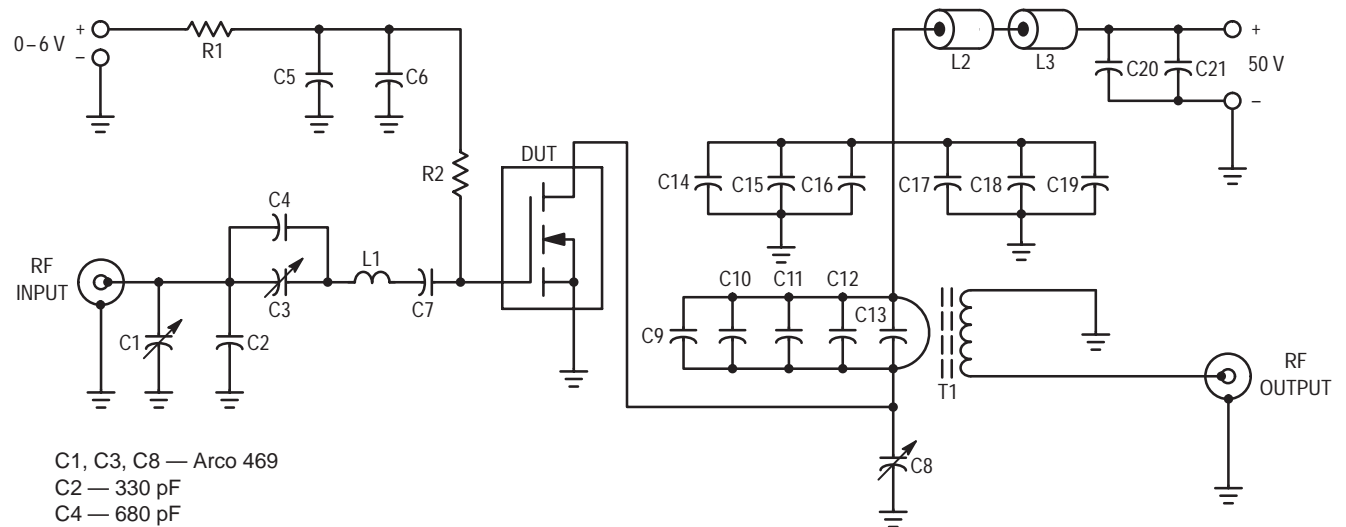
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 100 \text{ mA}$)	$V_{GS(th)}$	1.0	3.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 40 \text{ A}$)	$V_{DS(on)}$	1.0	3.0	5.0	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 20 \text{ A}$)	g_{fs}	16	20	—	mhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{iss}	—	1600	—	pF
Output Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{oss}	—	950	—	pF
Reverse Transfer Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{rss}	—	175	—	pF

FUNCTIONAL TESTS

Common Source Amplifier Power Gain ($V_{DD} = 50 \text{ V}, P_{out} = 600 \text{ W}, I_{DQ} = 800 \text{ mA}, f = 30 \text{ MHz}$)	G_{ps}	—	17	—	dB
Drain Efficiency ($V_{DD} = 50 \text{ V}, P_{out} = 600 \text{ W}, I_{DQ} = 800 \text{ mA}, f = 30 \text{ MHz}$)	η	—	45	—	%
Intermodulation Distortion ($V_{DD} = 50 \text{ V}, P_{out} = 600 \text{ W (PEP)},$ $f_1 = 30 \text{ MHz}, f_2 = 30.001 \text{ MHz}, I_{DQ} = 800 \text{ mA}$)	IMD(d3)	—	-25	—	dB



- C1, C3, C8 — Arco 469
- C2 — 330 pF
- C4 — 680 pF
- C5, C19, C20 — 0.47 μF , RMC Type 2225C
- C6, C7, C14, C15, C16 — 0.1 μF
- C9, C10, C11 — 470 pF
- C12 — 1000 pF
- C13 — Two Unencapsulated 1000 pF Mica, in Series
- C17, C18 — 0.039 μF
- C21 — 10 $\mu\text{F}/100 \text{ V}$ Electrolytic
- L1 — 2 Turns #16 AWG, 1/2" ID, 3/8" Long
- L2, L3 — Ferrite Beads, Fair-Rite Products Corp. #2673000801

- R1, R2 — 10 Ohms/2.0 W Carbon
- T1 — RF Transformer, 1:25 Impedance Ratio. See Motorola Application Note AN749, Figure 4 for details.
Ferrite Material: 2 Each, Fair-Rite Products Corp. #2667540001

All capacitors ATC type 100/200 chips or equivalent unless otherwise noted.

Figure 1. 30 MHz Test Circuit

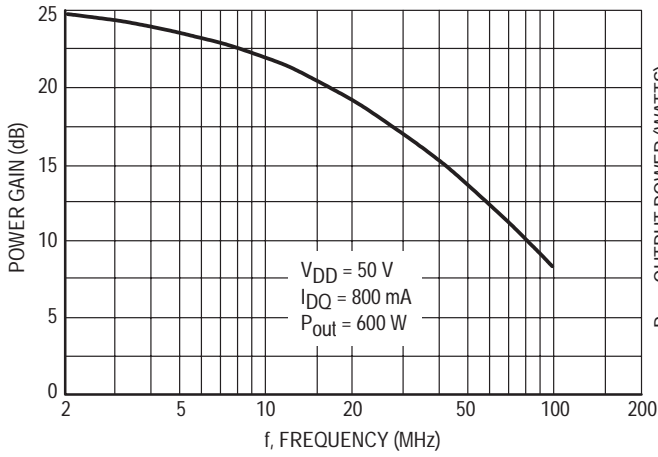


Figure 2. Power Gain versus Frequency

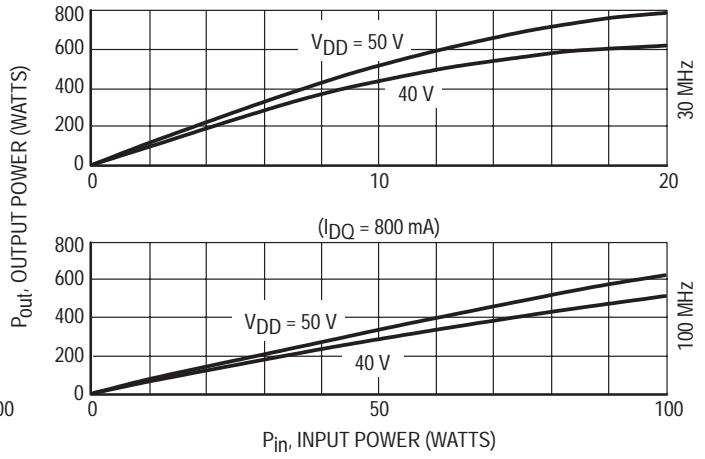


Figure 3. Output Power versus Input Power

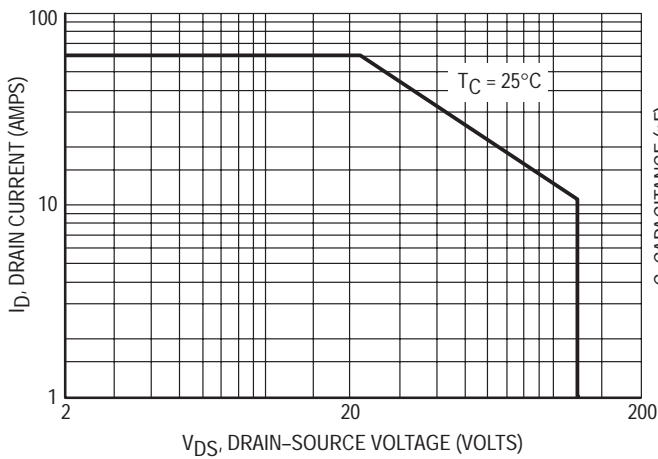


Figure 4. DC Safe Operating Area

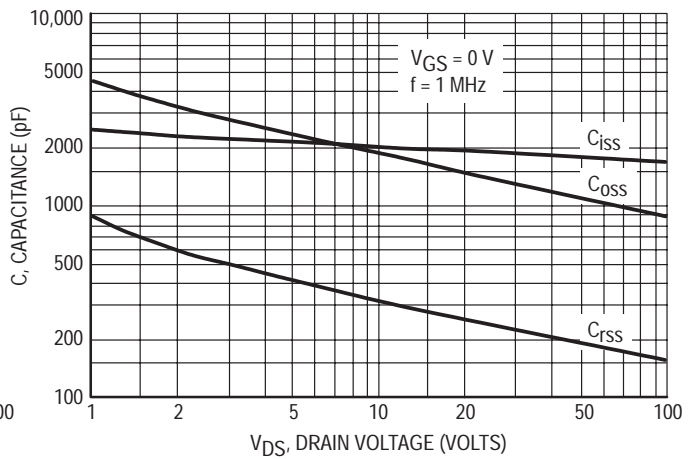


Figure 5. Capacitance versus Drain Voltage

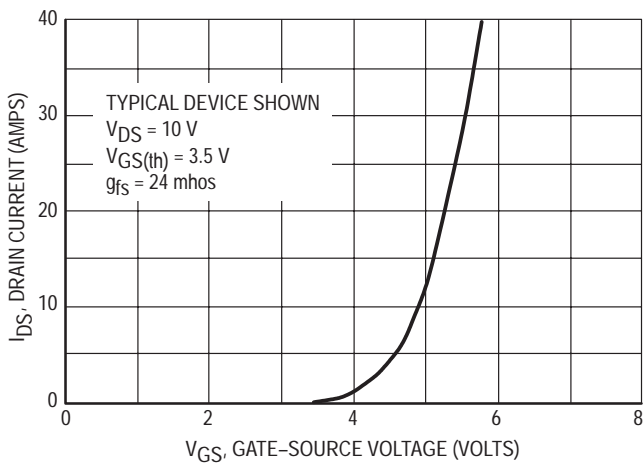


Figure 6. Gate Voltage versus Drain Current

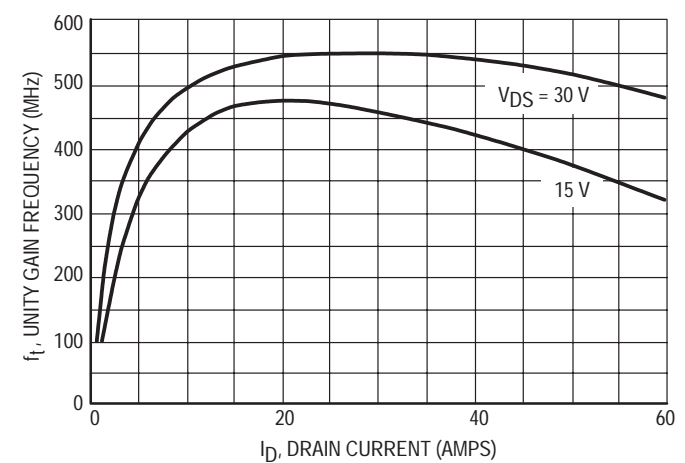


Figure 7. Common Source Unity Gain Frequency versus Drain Current

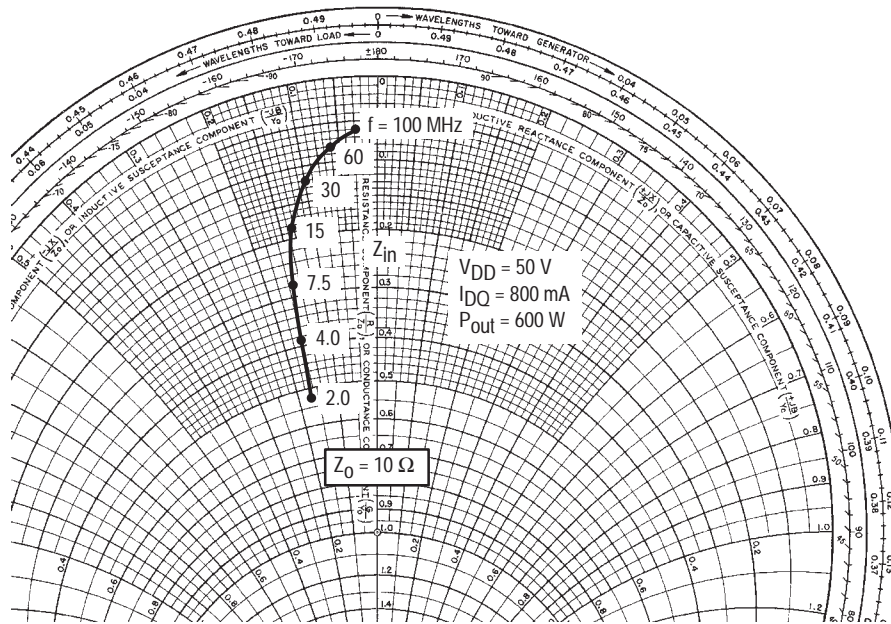
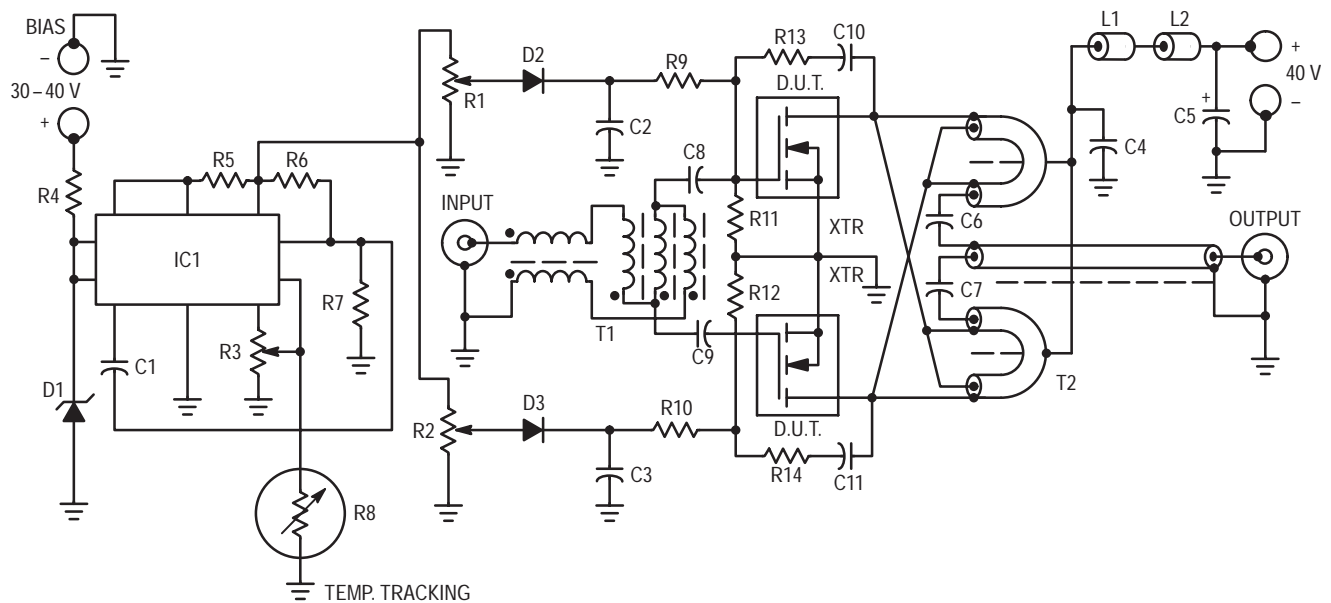


Figure 8. Series Equivalent Impedance



- C1 — 1000 pF Ceramic
- C2, C3, C4, C8, C9, C10, C11 — 0.1 μ F Ceramic
- C5 — 10 μ F/100 V Electrolytic
- C6, C7 — 0.1 μ F Ceramic, (ATC 200/823 or Equivalent)
- D1 — 28 V Zener, 1N5362 or Equivalent
- D3 — 1N4148
- IC1 — MC1723
- L1, L2 — Fair-Rite Products Corp. Ferrite Beads #2673000801
- R1, R2, R3 — 10 k Trimpot
- R4 — 1.0 k/1.0 W
- R5 — 10 Ohms
- R6 — 2.0 k

- R7 — 10 k
- R8 — Thermistor, 10 k (25°C), 2.5 k (75°C)
- R9, R10 — 100 Ohms
- R11, R12 — 1.0 k
- R13, R14 — 50–100 Ohms, 4.0 x 2.0 W Carbon in Parallel
- T1 — 9:1 Transformer, Trifilar and Balun Wound on Separate Fair-Rite Products Corp. Balun Cores #286100012, 5 Turns Each.
- T2 — 1:9 Transformer, Balun 50 Ohm CO-AX Cable RG-188, Low Impedance Lines W.L. Gore 16 Ohms CO-AX Type CXN 1837. Each Winding Threaded Through Two Fair-Rite Products Corp. #2661540001 Ferrite Sleeves (6 Each).
- XTR — MRF154

Figure 9. 20–80 MHz 1.0 kW Broadband Amplifier

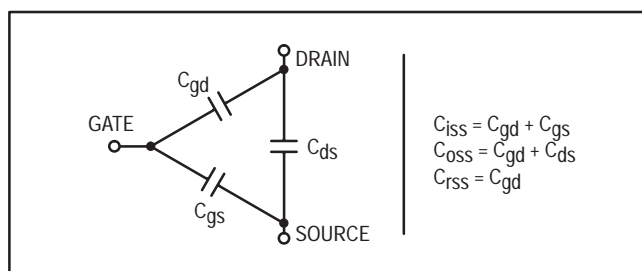
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 5 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors. Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

MOUNTING OF HIGH POWER RF POWER TRANSISTORS

The package of this device is designed for conduction cooling. It is extremely important to minimize the thermal resistance between the device flange and the heat dissipator.

Since the device mounting flange is made of soft copper, it may be deformed during various stages of handling or during transportation. It is recommended that the user makes a final inspection on this before the device installation. $\pm 0.0005''$ is considered sufficient for the flange bottom.

The same applies to the heat dissipator in the device mounting area. If copper heatsink is not used, a copper head spreader is strongly recommended between the device mounting surfaces and the main heatsink. It should be at least $1/4''$ thick and extend at least one inch from the flange edges. A thin layer of thermal compound in all interfaces is, of course, essential. The recommended torque on the 4–40 mounting screws should be in the area of 4–5 lbs.-inch, and spring type lock washers along with flat washers are recommended.

For die temperature calculations, the Δ temperature from a corner mounting screw area to the bottom center of the flange is approximately 5°C and 10°C under normal operating conditions (dissipation 150 W and 300 W respectively).

The main heat dissipator must be sufficiently large and have low R_θ for moderate air velocity, unless liquid cooling is employed.

CIRCUIT CONSIDERATIONS

At high power levels (500 W and up), the circuit layout becomes critical due to the low impedance levels and high RF currents associated with the output matching. Some of the components, such as capacitors and inductors must also withstand these currents. The component losses are directly proportional to the operating frequency. The manufacturers

specifications on capacitor ratings should be consulted on these aspects prior to design.

Push-pull circuits are less critical in general, since the ground referenced RF loops are practically eliminated, and the impedance levels are higher for a given power output. High power broadband transformers are also easier to design than comparable LC matching networks.

EQUIVALENT TRANSISTOR PARAMETER TERMINOLOGY

Collector	Drain
Emitter	Source
Base	Gate
$V_{(BR)CES}$	$V_{(BR)DSS}$
V_{CBO}	V_{DGO}
I_C	I_D
I_{CES}	I_{DSS}
I_{EBO}	I_{GSS}
$V_{BE(on)}$	$V_{GS(th)}$
$V_{CE(sat)}$	$V_{DS(on)}$
C_{ib}	C_{iss}
C_{ob}	C_{oss}
h_{fe}	g_{fs}
$R_{CE(sat)} = \frac{V_{CE(sat)}}{I_C}$	$r_{DS(on)} = \frac{V_{DS(on)}}{I_D}$

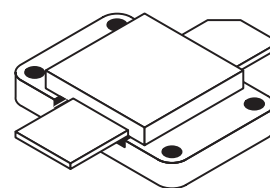
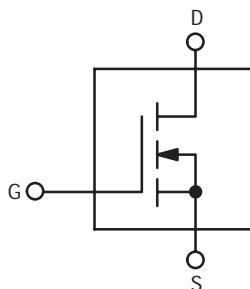
The RF Power MOS Line
Power Field Effect Transistor
N-Channel Enhancement Mode

Designed primarily for linear large-signal output stages to 80 MHz.

- Specified 50 Volts, 30 MHz Characteristics
 - Output Power = 600 Watts
 - Power Gain = 21 dB (Typ)
 - Efficiency = 45% (Typ)

MRF157

600 W, to 80 MHz
MOS LINEAR
RF POWER FET



CASE 368-03, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	125	Vdc
Drain-Gate Voltage	V_{DGO}	125	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	60	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	1350 7.7	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.13	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 100 \text{ mA}$)	$V_{(BR)DSS}$	125	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 50 \text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	20	mAdc
Gate–Body Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	5.0	μAdc

ON CHARACTERISTICS

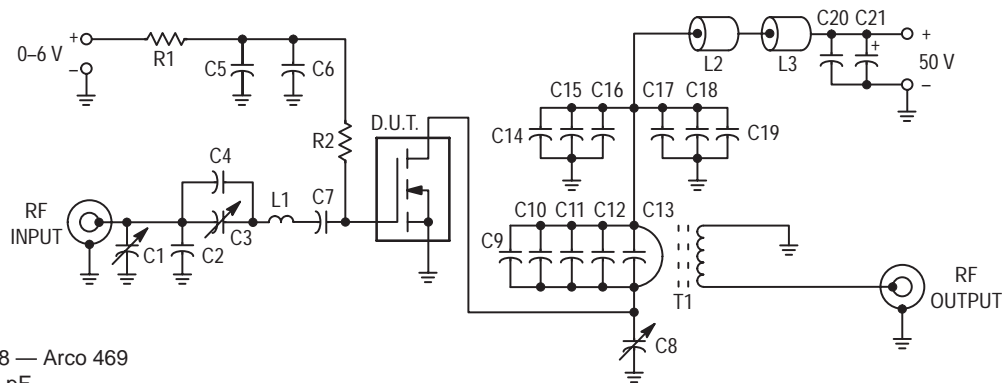
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 100 \text{ mA}$)	$V_{GS(th)}$	1.0	3.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 40 \text{ A}$)	$V_{DS(on)}$	1.0	3.0	5.0	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 20 \text{ A}$)	g_{fs}	16	24	—	mhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0 \text{ V}, f = 1.0 \text{ MHz}$)	C_{iss}	—	1800	—	pF
Output Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{oss}	—	750	—	pF
Reverse Transfer Capacitance ($V_{DS} = 50 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{rss}	—	75	—	pF

FUNCTIONAL TESTS

Common Source Amplifier Power Gain ($V_{DD} = 50 \text{ V}, P_{out} = 600 \text{ W}, I_{DQ} = 800 \text{ mA}, f = 30 \text{ MHz}$)	G_{ps}	15	21	—	dB
Drain Efficiency ($V_{DD} = 50 \text{ V}, P_{out} = 600 \text{ W}, f = 30 \text{ MHz}, I_{DQ} = 800 \text{ mA}$)	h	40	45	—	%
Intermodulation Distortion ($V_{DD} = 50 \text{ V}, P_{out} = 600 \text{ W(PEP)}, f_1 = 30 \text{ MHz}, f_2 = 30.001 \text{ MHz}, I_{DQ} = 800 \text{ mA}$)	$IMD(d3)$	—	-25	—	dB



- C1, C3, C8 — Arco 469
- C2 — 330 pF
- C4 — 680 pF
- C5, C19, C20 — 0.47 μF , RMC Type 2225C
- C6, C7, C14, C15, C16 — 0.1 μF
- C9, C10, C11 — 470 pF
- C12 — 1000 pF
- C13 — Two Unencapsulated 1000 pF Mica, in Series
- C17, C18 — 0.039 μF
- C21 — 10 $\mu\text{F}/100 \text{ V}$ Electrolytic
- L1 — 2 Turns #16 AWG, 1/2" ID, 3/8" Long
- L2, L3 — Ferrite Beads, Fair–Rite Products Corp. #2673000801

- R1, R2 — 10 Ohms/2W Carbon
- T1 — RF Transformer, 1:25 Impedance Ratio. See Motorola Application Note AN749, Figure 4 for details.
Ferrite Material: 2 Each, Fair–Rite Products Corp. #2667540001

All capacitors ATC type 100/200 chips or equivalent unless otherwise noted.

Figure 1. 30 MHz Test Circuit

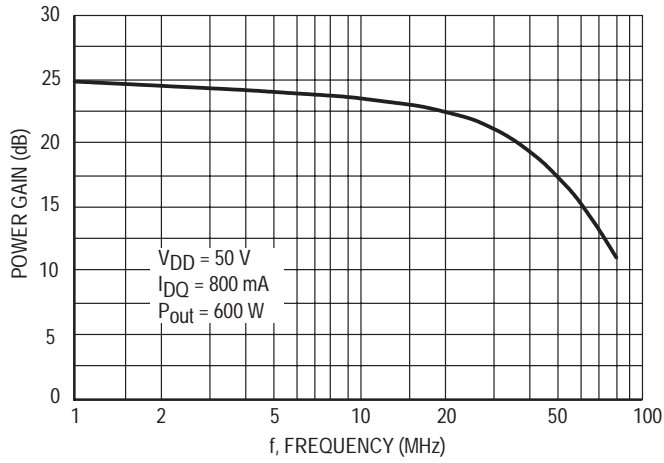


Figure 2. Power Gain versus Frequency

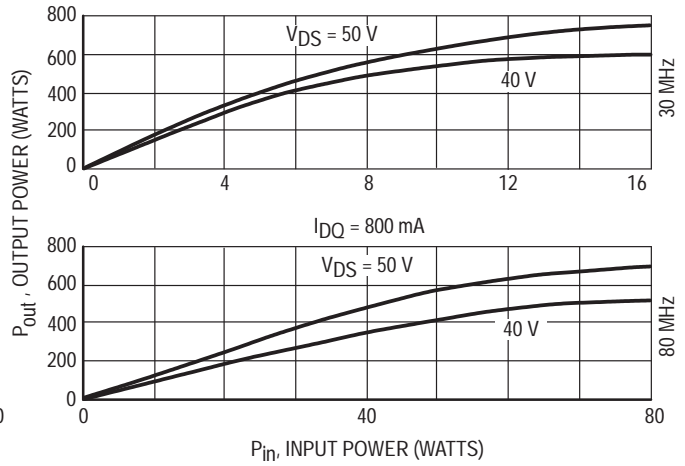


Figure 3. Output Power versus Input Power

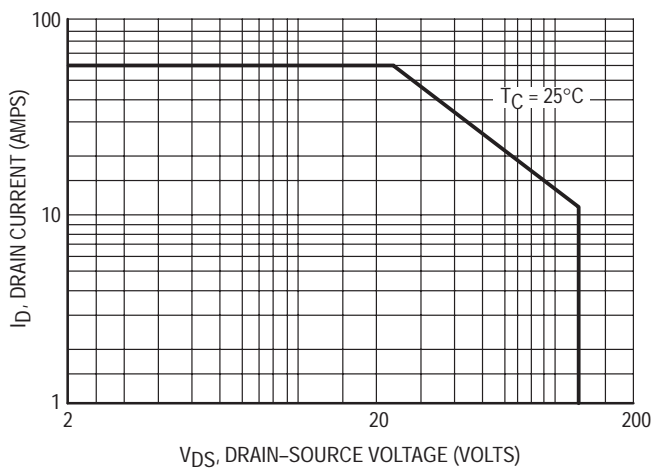


Figure 4. DC Safe Operating Area

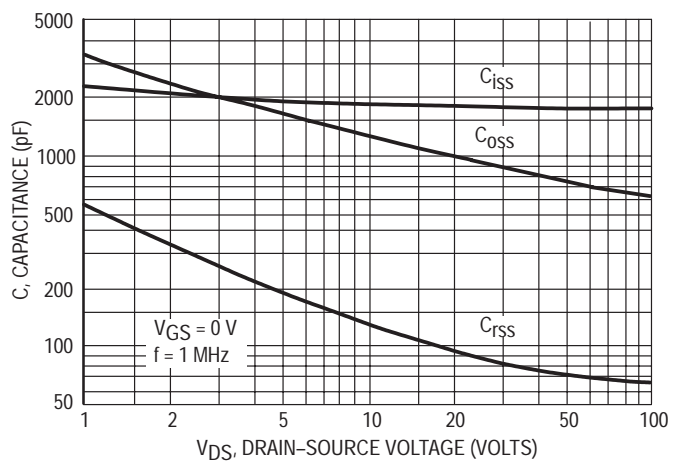


Figure 5. Capacitance versus Drain Voltage

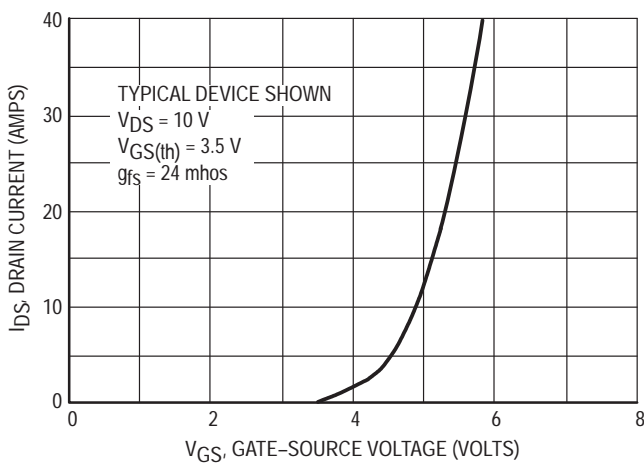


Figure 6. Gate Voltage versus Drain Current

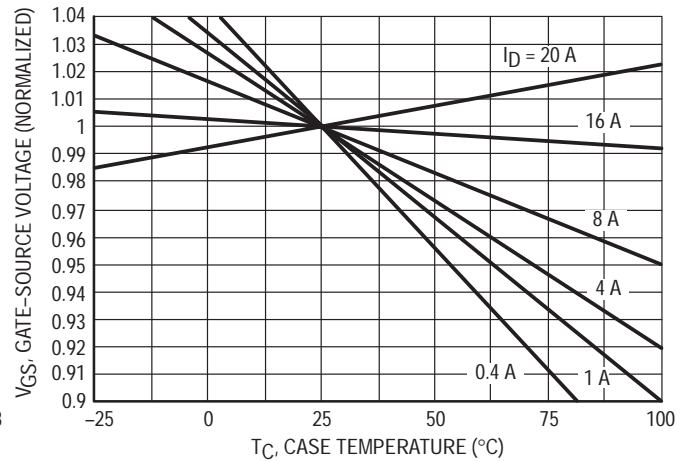


Figure 7. Gate-Source Voltage versus Case Temperature

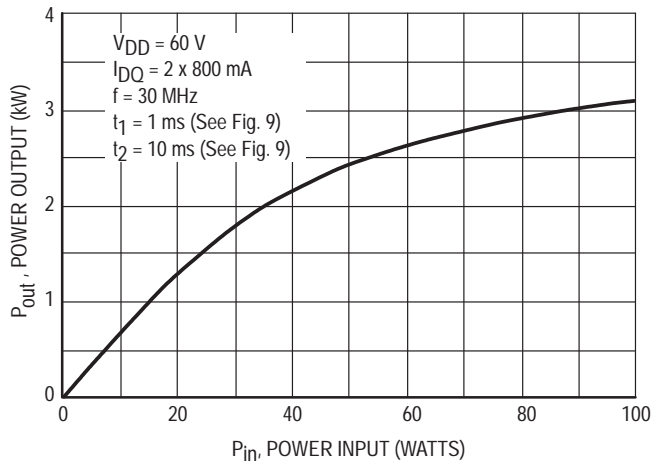


Figure 8. Output Power versus Input Power Under Pulse Conditions (2 x MRF157)

Note: Pulse data for this graph was taken in a push-pull circuit similar to the one shown. However, the output matching network was modified for the higher level of peak power.

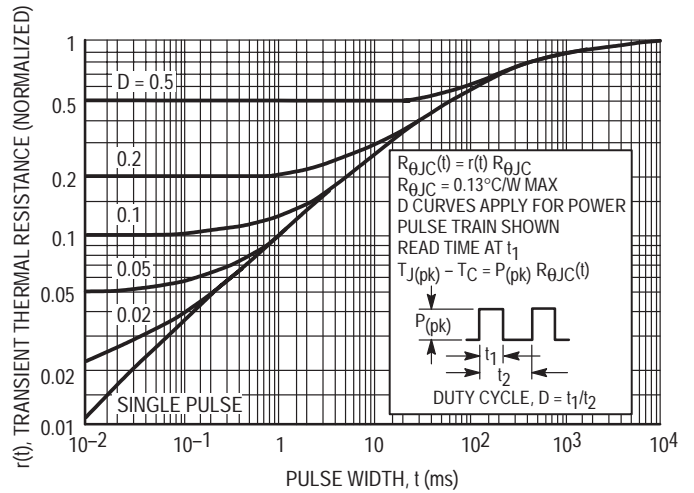
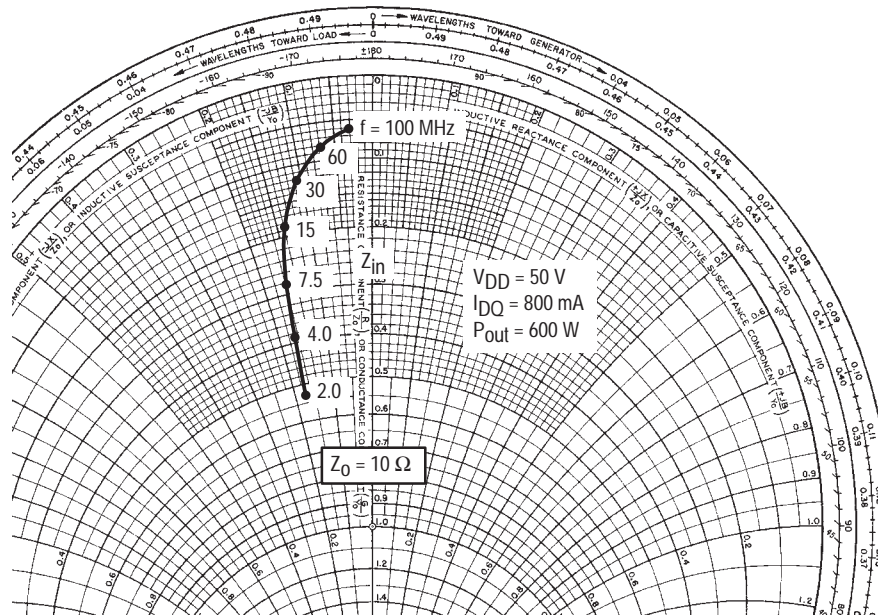
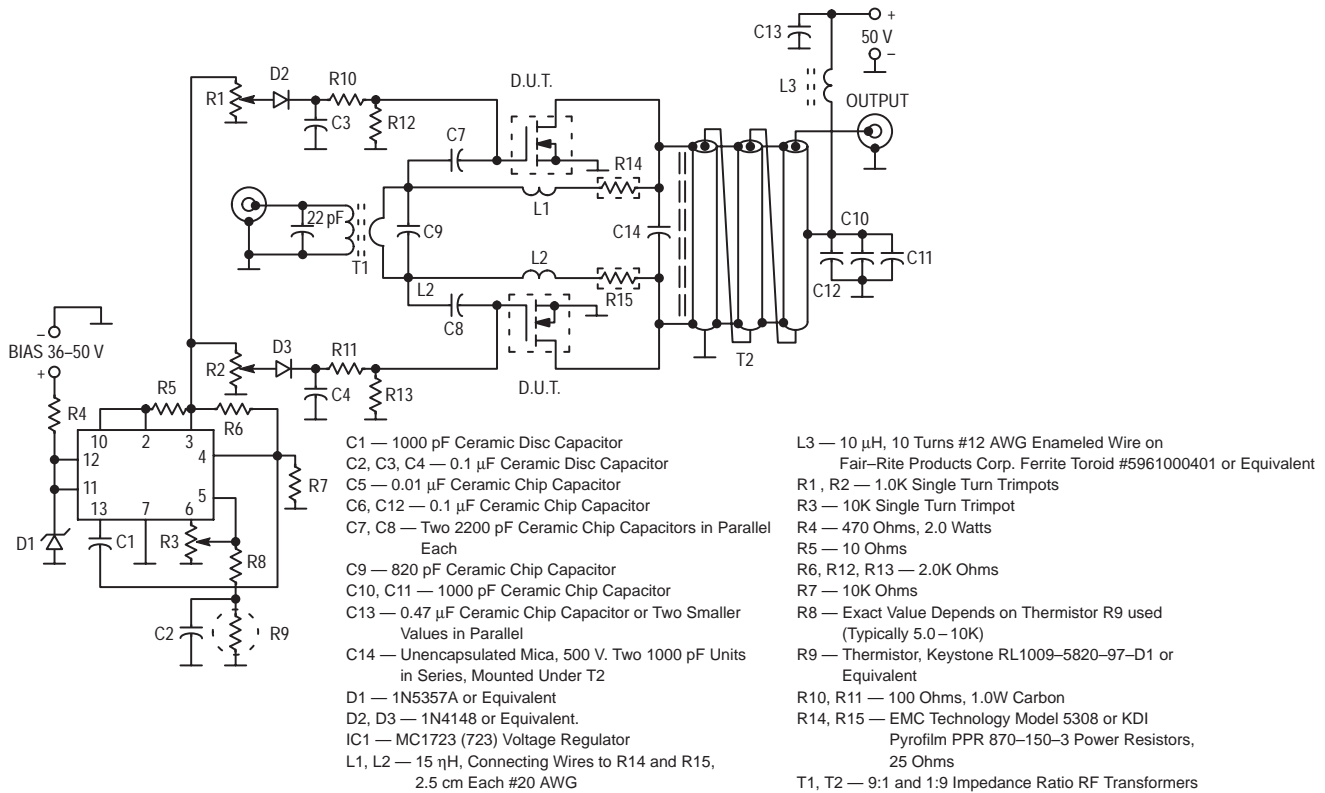


Figure 9. Thermal Response versus Pulse Width



Note: To determine Z_{OL}^* , use formula $\frac{(V_{CC} - V_{sat})^2}{2 P_0} = Z_{OL}^*$

Figure 10. Series Equivalent Impedance



Unless otherwise noted, all resistors are 1/2 watt metal film type. All chip capacitors except C13 are ATC type 100/200B or Dielectric Laboratories type C17.

Figure 11. 2.0 to 50 MHz, 1.0 kW Wideband Amplifier

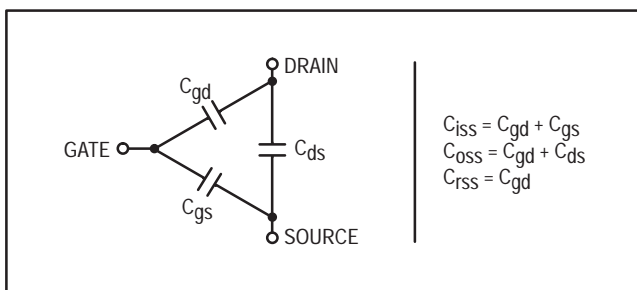
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the TMOS[®] FET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iSS}), output (C_{oSS}) and reverse transfer (C_{rSS}) capacitances on data sheets. The relationships between the interterminal capacitances and those given on data sheets are shown below. The C_{iSS} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



LINEARITY AND GAIN CHARACTERISTICS

In addition to the typical IMD and power gain data presented, Figure 5 may give the designer additional information on the capabilities of this device. The graph represents the small signal unity current gain frequency at a given drain current level. This is equivalent to f_T for bipolar transistors. Since this test is performed at a fast sweep speed, heating of the device does not occur. Thus, in normal use, the higher temperatures may degrade these characteristics to some extent.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the TMOS FET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. The addition of an internal zener diode may result in detrimental effects on the reliability of a power MOSFET. If gate protection is required, an external zener diode is recommended.

IMPEDANCE CHARACTERISTICS

Device input and output impedances are normally obtained by measuring their conjugates in an optimized narrow band test circuit. These test circuits are designed and constructed for a number of frequency points depending on the frequency coverage of characterization. For low frequencies the circuits consist of standard LC matching networks including variable capacitors for peak tuning. At increasing power levels the output impedance decreases, resulting in higher RF currents in the matching network. This makes the practicality of output impedance measurements in the manner described questionable at power levels higher than 200–300 W for devices operated at 50 V and 150–200 W for devices operated at 28 V. The physical sizes and values required for the components to withstand the RF currents increase to a point where physical construction of the output matching network gets difficult if not impossible. For this reason the output impedances are not given for high power devices such as the MRF154 and MRF157. However, formulas like $\frac{(V_{DS} - V_{sat})^2}{2P_{out}}$ for a single ended design or $\frac{2((V_{DS} - V_{sat})^2)}{P_{out}}$ for a push-pull design can be used to obtain reasonably close approximations to actual values.

MOUNTING OF HIGH POWER RF POWER TRANSISTORS

The package of this device is designed for conduction cooling. It is extremely important to minimize the thermal resistance between the device flange and the heat dissipator.

If a copper heatsink is not used, a copper head spreader is strongly recommended between the device mounting surfaces and the main heatsink. It should be at least 1/4" thick and extend at least one inch from the flange edges. A thin layer of thermal compound in all interfaces is, of course, essential. The recommended torque on the 4–40 mounting screws should be in the area of 4–5 lbs.-inch, and spring type lock washers along with flat washers are recommended.

For die temperature calculations, the Δ temperature from a corner mounting screw area to the bottom center of the flange is approximately 5°C and 10°C under normal operating conditions (dissipation 150 W and 300 W respectively).

The main heat dissipator must be sufficiently large and have low R_{θ} for moderate air velocity, unless liquid cooling is employed.

CIRCUIT CONSIDERATIONS

At high power levels (500 W and up), the circuit layout becomes critical due to the low impedance levels and high RF currents associated with the output matching. Some of the components, such as capacitors and inductors must also withstand these currents. The component losses are directly proportional to the operating frequency. The manufacturers specifications on capacitor ratings should be consulted on these aspects prior to design.

Push-pull circuits are less critical in general, since the ground referenced RF loops are practically eliminated, and the impedance levels are higher for a given power output. High power broadband transformers are also easier to design than comparable LC matching networks.

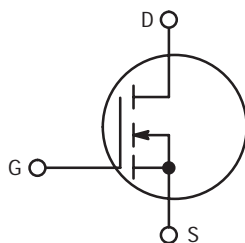
EQUIVALENT TRANSISTOR PARAMETER TERMINOLOGY

Collector	Drain
Emitter	Source
Base	Gate
$V_{(BR)CES}$	$V_{(BR)DSS}$
V_{CBO}	V_{DGO}
I_C	I_D
I_{CES}	I_{DSS}
I_{EBO}	I_{GSS}
$V_{BE(on)}$	$V_{GS(th)}$
$V_{CE(sat)}$	$V_{DS(on)}$
C_{ib}	C_{iss}
C_{ob}	C_{oss}
h_{fe}	g_{fs}
$R_{CE(sat)} = \frac{V_{CE(sat)}}{I_C}$	$R_{DS(on)} = \frac{V_{DS(on)}}{I_D}$

The RF TMOS® Line
Power Field Effect Transistor
N-Channel Enhancement Mode

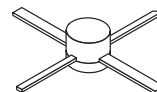
Designed for wideband large-signal amplifier and oscillator applications to 500 MHz.

- Guaranteed 28 Volt, 500 MHz Performance
Output Power = 2.0 Watts
Minimum Gain = 16 dB (Min)
Efficiency = 55% (Typ)
- Facilitates Manual Gain Control, ALC and Modulation Techniques
- 100% Tested for Load Mismatch at All Phase Angles with 30:1 VSWR
- Excellent Thermal Stability, Ideally Suited for Class A Operation
- Circuit board sample available upon request by contacting RF Tactical Marketing in Tempe, AZ.
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://mot-sps.com/rf/designtds/>



MRF158

To 500 MHz, 2 W, 28 V
TMOS
BROADBAND
RF POWER FET



CASE 305A-01, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1.0 \text{ M}\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current — Continuous	I_D	0.5	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	8.0 45	Watts mW/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	13.2	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 1.0$ mA)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28$ V, $V_{GS} = 0$)	I_{DSS}	—	—	0.5	mAdc
Gate–Source Leakage Current ($V_{GS} = 20$ V, $V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS

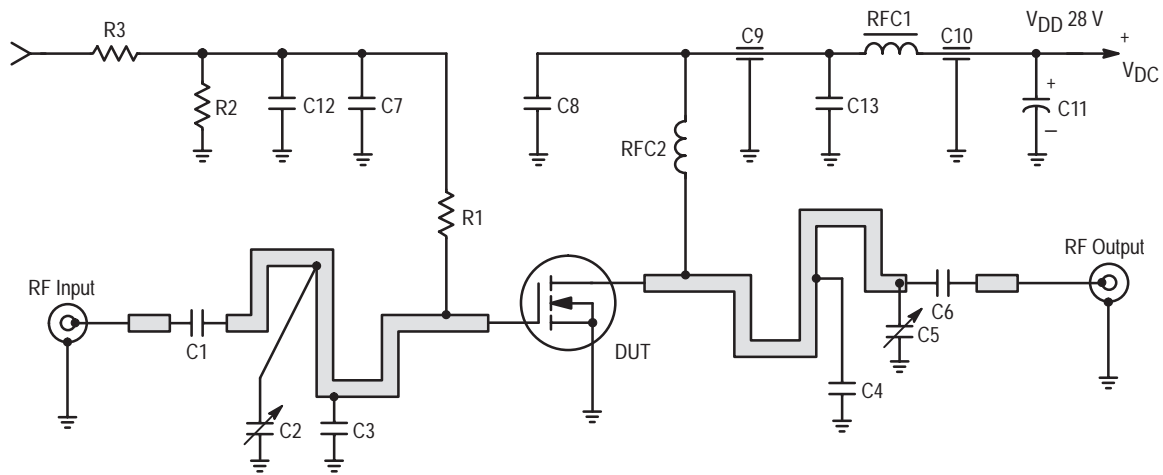
Gate Threshold Voltage ($I_D = 10$ mA, $V_{DS} = 10$ V)	$V_{GS(th)}$	2.0	4.0	5.0	Vdc
Forward Transconductance ($V_{DS} = 10$ V, $I_D = 100$ mA)	g_{fs}	80	110	—	mmhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1.0$ MHz)	C_{iss}	—	3.0	—	pF
Output Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1.0$ MHz)	C_{oss}	—	4.0	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1.0$ MHz)	C_{rss}	—	0.45	—	pF

FUNCTIONAL CHARACTERISTICS (Figure 1)

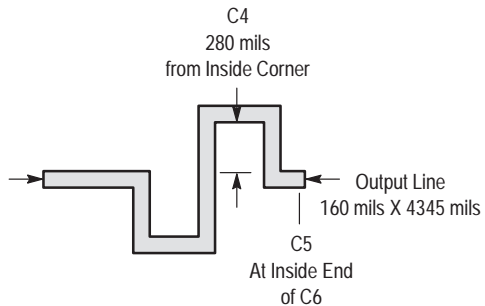
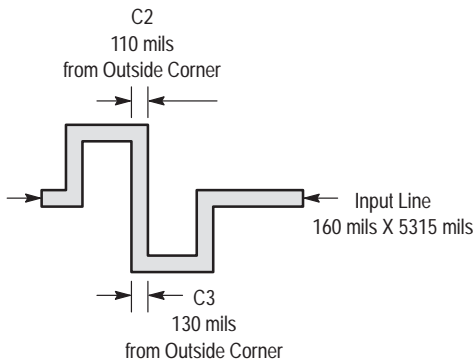
Common Source Power Gain ($V_{DD} = 28$ Vdc, $P_{out} = 2.0$ W, $f = 500$ MHz, $I_{DQ} = 25$ mA)	G_{ps}	16	18	—	dB
Drain Efficiency (Figure 1) ($V_{DD} = 28$ Vdc, $P_{out} = 2.0$ W, $f = 500$ MHz, $I_{DQ} = 25$ mA)	η	50	55	—	%
Electrical Ruggedness (Figure 1) ($V_{DD} = 28$ Vdc, $P_{out} = 2.0$ W, $f = 500$ MHz, $I_{DQ} = 25$ mA, VSWR 30:1 at all Phase Angles)	ψ	No Degradation in Output Power			
Series Equivalent Input Impedance ($V_{DD} = 28$ V, $P_{out} = 2.0$ W, $f = 500$ MHz, $I_{DQ} = 25$ mA)	Z_{in}	—	$5.9 - j19.4$	—	Ohms
Series Equivalent Output Impedance ($V_{DD} = 28$ V, $P_{out} = 2.0$ W, $f = 500$ MHz, $I_{DQ} = 25$ mA)	Z_{out}	—	$14.5 - j29$	—	Ohms



- C1, C6, C12 270 pF, Chip Capacitors
- C2, C5 1–10 pF, Johanson Trimmer Capacitors
- C3 30 pF, 100 mil ATC Chip Capacitor
- C4 3.9 pF, 100 mil ATC Chip Capacitor
- C7, C8 0.1 μ F, Blue Capacitors
- C9, C10 680 pF, Feed Through Capacitors
- C11 50 μ F, 50 V Electrolytic Capacitor
- C13 240 pF, 100 mil ATC Chip Capacitor

- R1 150 Ω , 1/2 Watt
- R2 10 k Ω , 1/2 Watt
- R3 1 k Ω , 1/2 Watt
- RFC1 Ferroxcube VK200–19/4B
- RFC2 8 Turns, #20 AWG, Enameled, ID 110 mils

Board Material — 0.062", Teflon[®] Fiberglass, 1 oz.,
Copper clad both sides, $\epsilon_r = 2.55$



NOTE: Due to variation in Chip Capacitor values and board material, these are approximate positions.

Figure 1. MRF158 500 MHz Test Circuit

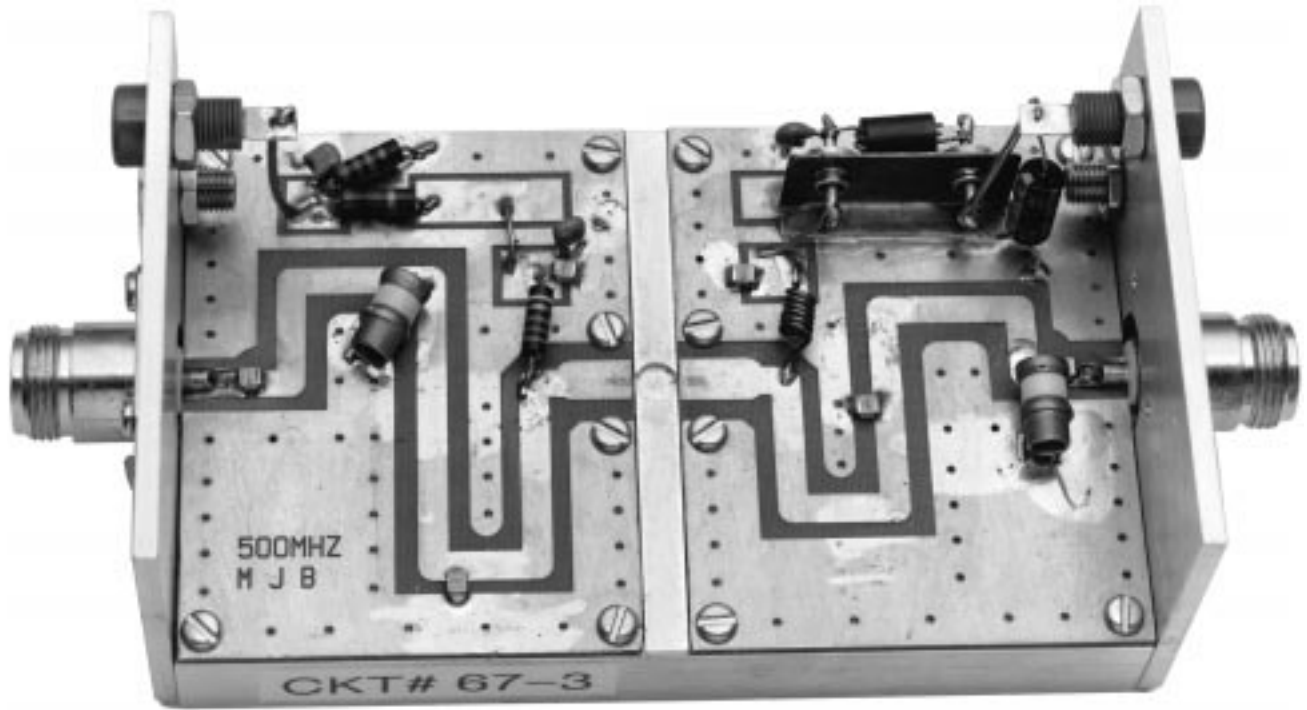


Figure 2. MRF158 Broadband Test Fixture

TYPICAL CHARACTERISTICS

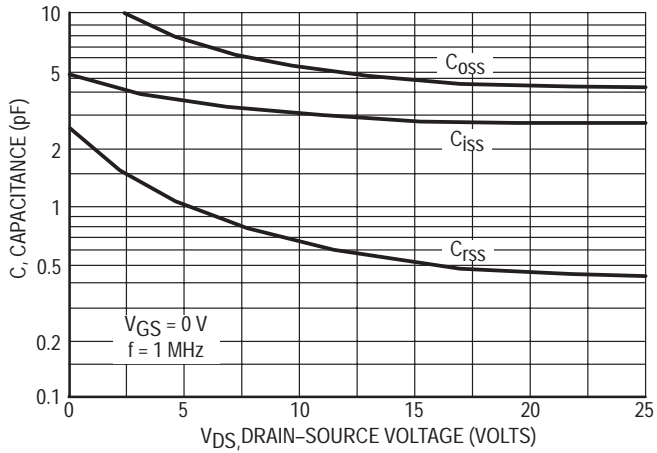


Figure 3. Capacitance versus Drain-Source Voltage

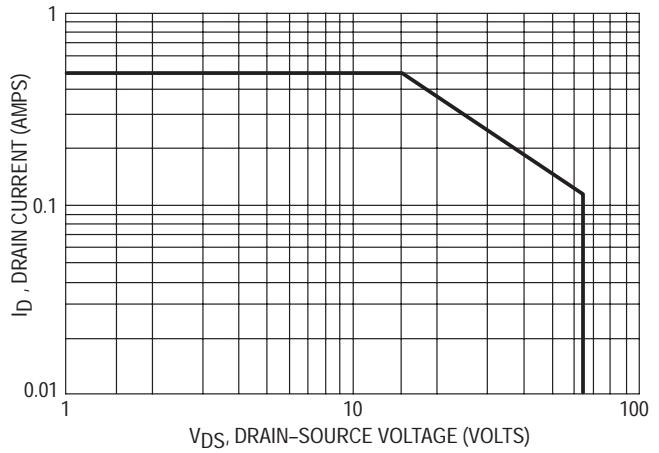


Figure 4. DC Safe Operating Area

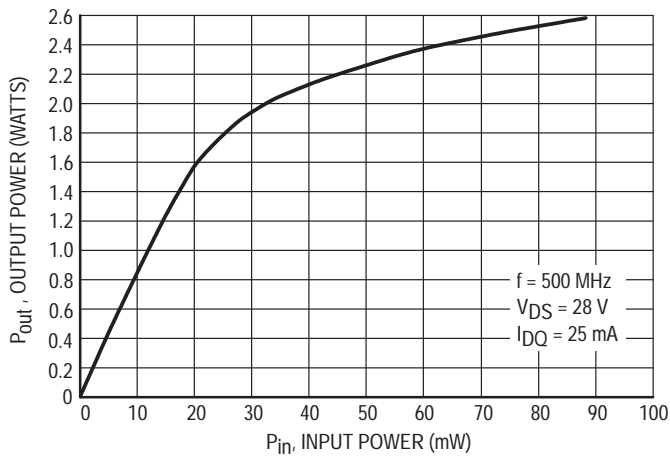


Figure 5. Output Power versus Input Power

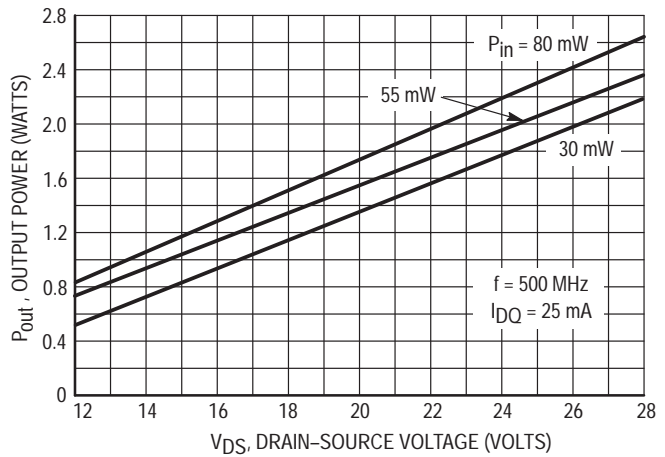


Figure 6. Output Power versus Voltage

Table 1. Common Source S-Parameters ($V_{DS} = 13\text{ V}$, $I_D = 100\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
5	1.000	-2	9.45	179	0.000	89	0.965	-1
10	0.997	-4	9.45	177	0.005	92	0.969	-3
15	0.999	-5	9.50	176	0.007	86	0.962	-5
20	0.997	-7	9.45	174	0.009	91	0.958	-6
25	0.997	-9	9.44	173	0.012	88	0.958	-7
30	0.996	-10	9.40	172	0.014	82	0.960	-8
35	0.994	-12	9.38	170	0.016	78	0.956	-10
40	0.993	-14	9.35	169	0.016	77	0.958	-11
45	0.990	-15	9.34	167	0.020	79	0.957	-12
50	0.988	-17	9.29	166	0.021	76	0.957	-14
55	0.985	-19	9.25	165	0.023	77	0.955	-15
60	0.983	-21	9.26	163	0.026	75	0.952	-17
65	0.980	-22	9.19	162	0.028	74	0.947	-18
70	0.977	-24	9.15	160	0.029	74	0.943	-20
75	0.973	-25	9.11	159	0.031	74	0.942	-21
80	0.970	-27	9.04	158	0.034	70	0.935	-22
85	0.967	-29	8.98	157	0.035	71	0.932	-24
90	0.963	-30	8.91	155	0.037	67	0.929	-25
95	0.961	-32	8.90	154	0.039	68	0.924	-26
100	0.957	-33	8.81	153	0.040	67	0.917	-27
105	0.953	-35	8.77	151	0.041	64	0.916	-28
109	0.950	-36	8.69	150	0.042	65	0.914	-30
114	0.943	-38	8.62	149	0.045	63	0.906	-31
119	0.940	-40	8.56	148	0.045	62	0.907	-32
124	0.933	-41	8.49	146	0.049	61	0.901	-33
129	0.933	-43	8.46	145	0.049	60	0.901	-35
134	0.923	-44	8.37	144	0.052	59	0.896	-36
139	0.921	-45	8.29	143	0.052	58	0.890	-37
144	0.917	-47	8.22	142	0.055	57	0.885	-39
149	0.913	-48	8.16	140	0.055	55	0.878	-40
154	0.911	-50	8.11	140	0.057	53	0.874	-41
159	0.905	-51	8.02	138	0.059	54	0.868	-42
164	0.902	-52	7.94	137	0.059	53	0.863	-43
169	0.896	-54	7.87	136	0.062	52	0.856	-44
174	0.893	-55	7.79	135	0.063	50	0.851	-45
179	0.890	-56	7.71	134	0.062	50	0.846	-46
184	0.882	-58	7.64	133	0.065	48	0.845	-47
189	0.881	-59	7.59	132	0.065	47	0.840	-48
194	0.874	-60	7.53	131	0.066	47	0.834	-49
199	0.868	-61	7.43	130	0.067	47	0.828	-50
204	0.864	-62	7.36	129	0.068	46	0.829	-51
209	0.861	-63	7.31	128	0.070	45	0.824	-52

Table 1. Common Source S-Parameters ($V_{DS} = 13\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
214	0.856	-65	7.24	127	0.070	44	0.820	-53
219	0.853	-66	7.17	126	0.070	43	0.813	-54
224	0.848	-67	7.10	125	0.072	41	0.806	-55
229	0.847	-68	7.02	124	0.074	41	0.803	-56
234	0.841	-69	6.94	124	0.075	40	0.800	-57
239	0.839	-70	6.92	122	0.074	39	0.789	-58
244	0.832	-71	6.80	122	0.076	40	0.783	-59
249	0.828	-72	6.73	121	0.077	38	0.780	-60
254	0.825	-73	6.68	120	0.077	39	0.778	-60
259	0.820	-74	6.60	119	0.078	36	0.772	-61
264	0.816	-75	6.54	118	0.078	35	0.769	-62
269	0.813	-76	6.48	117	0.078	36	0.765	-63
274	0.810	-77	6.42	117	0.079	34	0.765	-64
279	0.806	-78	6.34	116	0.080	35	0.762	-64
284	0.799	-79	6.29	115	0.080	34	0.757	-65
289	0.800	-80	6.23	114	0.081	31	0.756	-66
294	0.795	-81	6.18	113	0.081	33	0.753	-67
299	0.789	-82	6.12	113	0.084	31	0.750	-67
304	0.791	-83	6.07	112	0.082	31	0.742	-68
308	0.790	-84	5.99	111	0.084	30	0.742	-69
313	0.787	-85	5.95	110	0.084	29	0.737	-70
318	0.784	-85	5.88	109	0.083	30	0.729	-70
323	0.779	-86	5.80	109	0.084	28	0.726	-71
328	0.778	-87	5.77	108	0.085	27	0.723	-72
333	0.773	-88	5.69	107	0.085	28	0.720	-72
338	0.771	-89	5.64	107	0.084	26	0.716	-73
343	0.766	-89	5.60	106	0.086	25	0.716	-74
348	0.766	-90	5.55	106	0.086	25	0.712	-74
353	0.763	-91	5.50	105	0.086	24	0.708	-75
358	0.761	-92	5.43	104	0.086	24	0.708	-75
363	0.761	-93	5.41	104	0.086	24	0.706	-76
368	0.755	-94	5.35	103	0.086	23	0.702	-77
373	0.753	-94	5.29	102	0.087	23	0.704	-77
378	0.752	-95	5.25	101	0.086	23	0.700	-78
383	0.750	-96	5.20	101	0.087	22	0.697	-79
388	0.747	-96	5.15	100	0.089	21	0.692	-79
393	0.742	-97	5.08	100	0.087	21	0.693	-80
398	0.741	-98	5.04	99	0.088	20	0.689	-81
403	0.743	-98	5.01	98	0.088	20	0.684	-81
408	0.740	-99	4.97	98	0.088	19	0.682	-81
413	0.734	-100	4.90	97	0.089	19	0.682	-82
418	0.738	-100	4.87	97	0.088	18	0.677	-83

Table 1. Common Source S-Parameters ($V_{DS} = 13\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
423	0.733	-101	4.82	96	0.089	18	0.676	-83
428	0.735	-102	4.80	96	0.089	17	0.674	-84
433	0.731	-102	4.74	95	0.088	16	0.672	-84
438	0.732	-103	4.70	94	0.088	17	0.673	-85
443	0.728	-104	4.67	94	0.089	16	0.670	-85
448	0.729	-105	4.64	93	0.090	16	0.671	-86
453	0.727	-105	4.59	93	0.088	16	0.668	-86
458	0.723	-105	4.56	92	0.089	15	0.668	-87
463	0.721	-106	4.50	91	0.088	15	0.668	-87
468	0.720	-107	4.46	91	0.088	15	0.665	-87
473	0.719	-107	4.42	90	0.089	13	0.662	-88
478	0.717	-107	4.38	90	0.089	13	0.662	-89
483	0.717	-108	4.35	89	0.088	13	0.658	-89
488	0.715	-109	4.32	89	0.088	13	0.660	-89
493	0.714	-109	4.28	88	0.090	13	0.655	-90
498	0.714	-110	4.25	88	0.090	12	0.655	-91
503	0.713	-110	4.22	87	0.089	12	0.652	-91
507	0.712	-111	4.17	87	0.090	11	0.650	-91
512	0.711	-111	4.15	86	0.089	11	0.649	-92
517	0.706	-112	4.11	86	0.090	11	0.650	-92
522	0.705	-112	4.07	85	0.089	10	0.650	-93
527	0.706	-113	4.07	85	0.089	10	0.648	-93
532	0.705	-113	4.02	84	0.088	10	0.649	-93
537	0.704	-114	4.00	84	0.088	9	0.645	-94
542	0.704	-114	3.95	83	0.089	9	0.646	-94
547	0.704	-115	3.93	82	0.087	10	0.646	-95
552	0.704	-116	3.90	82	0.090	8	0.645	-95
557	0.702	-116	3.87	82	0.089	8	0.646	-96
562	0.699	-117	3.83	81	0.088	8	0.646	-96
567	0.699	-117	3.80	81	0.089	8	0.641	-96
572	0.700	-117	3.76	80	0.088	7	0.640	-97
577	0.699	-118	3.74	80	0.087	7	0.640	-97
582	0.698	-118	3.70	80	0.088	7	0.641	-98
587	0.699	-118	3.69	79	0.087	7	0.637	-98
592	0.697	-119	3.67	79	0.088	6	0.638	-98
597	0.698	-119	3.64	78	0.088	6	0.633	-99
602	0.698	-119	3.62	78	0.087	6	0.638	-99
607	0.695	-120	3.58	77	0.087	6	0.637	-99
612	0.696	-120	3.57	77	0.087	6	0.637	-100
617	0.694	-121	3.54	76	0.086	5	0.636	-100
622	0.695	-121	3.52	76	0.087	5	0.635	-100
627	0.692	-121	3.48	75	0.088	5	0.637	-101

Table 1. Common Source S-Parameters ($V_{DS} = 13\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
632	0.691	-122	3.46	75	0.085	4	0.634	-101
637	0.691	-122	3.44	74	0.087	4	0.641	-102
642	0.689	-123	3.41	74	0.087	3	0.637	-102
647	0.687	-123	3.38	74	0.087	3	0.634	-103
652	0.689	-124	3.36	73	0.085	3	0.636	-103
657	0.686	-124	3.34	73	0.086	1	0.635	-103
662	0.688	-125	3.30	72	0.086	3	0.634	-104
667	0.689	-125	3.28	72	0.086	2	0.634	-104
672	0.693	-125	3.27	72	0.086	2	0.631	-104
677	0.687	-126	3.24	71	0.086	1	0.632	-104
682	0.689	-126	3.22	71	0.083	1	0.629	-105
687	0.687	-126	3.20	70	0.083	1	0.630	-105
692	0.686	-127	3.17	70	0.083	1	0.630	-105
697	0.690	-127	3.16	70	0.083	0	0.630	-106
702	0.687	-127	3.14	69	0.084	0	0.627	-106
706	0.688	-128	3.12	69	0.083	1	0.630	-106
711	0.685	-128	3.10	68	0.083	0	0.632	-107
716	0.686	-128	3.08	68	0.085	0	0.636	-107
721	0.688	-128	3.08	68	0.084	-1	0.634	-107
726	0.685	-129	3.05	67	0.083	0	0.634	-108
731	0.685	-130	3.02	67	0.083	-1	0.634	-108
736	0.684	-130	3.01	66	0.083	-1	0.635	-108
741	0.680	-130	2.98	66	0.082	-1	0.631	-109
746	0.681	-130	2.97	65	0.083	-2	0.636	-109
751	0.682	-131	2.96	65	0.082	-2	0.631	-110
756	0.683	-131	2.93	65	0.082	-2	0.632	-109
761	0.681	-132	2.90	64	0.082	-1	0.630	-110
766	0.683	-132	2.89	64	0.083	-3	0.632	-110
771	0.684	-132	2.87	64	0.082	-3	0.631	-110
776	0.682	-133	2.85	63	0.081	-4	0.628	-111
781	0.684	-133	2.85	63	0.080	-3	0.630	-111
786	0.686	-133	2.83	63	0.079	-4	0.629	-111
791	0.684	-134	2.81	62	0.080	-3	0.632	-112
796	0.685	-134	2.79	62	0.080	-4	0.631	-112
801	0.683	-134	2.77	62	0.079	-4	0.634	-112
806	0.685	-134	2.75	61	0.079	-2	0.632	-112
811	0.683	-135	2.75	61	0.078	-4	0.635	-113
816	0.684	-135	2.73	60	0.079	-4	0.637	-113
821	0.683	-135	2.70	60	0.077	-3	0.633	-113
826	0.682	-135	2.69	60	0.078	-5	0.637	-114
831	0.682	-136	2.67	59	0.077	-4	0.635	-114
836	0.681	-136	2.66	59	0.077	-5	0.638	-114

Table 1. Common Source S-Parameters ($V_{DS} = 13\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
841	0.681	-136	2.64	58	0.079	-4	0.635	-115
846	0.679	-137	2.63	58	0.078	-4	0.637	-115
851	0.678	-137	2.61	58	0.077	-5	0.634	-115
856	0.682	-137	2.59	57	0.077	-5	0.635	-115
861	0.680	-137	2.59	57	0.077	-4	0.634	-115
866	0.681	-138	2.57	57	0.077	-6	0.635	-116
871	0.682	-138	2.55	56	0.075	-6	0.633	-116
876	0.684	-139	2.54	56	0.075	-5	0.631	-116
881	0.683	-139	2.53	56	0.075	-5	0.635	-117
886	0.681	-139	2.52	55	0.074	-6	0.633	-117
891	0.685	-140	2.50	55	0.074	-6	0.633	-117
896	0.683	-140	2.49	55	0.075	-6	0.638	-117
901	0.680	-140	2.47	54	0.073	-5	0.640	-118
905	0.681	-140	2.46	54	0.074	-7	0.637	-118
910	0.684	-140	2.44	54	0.074	-8	0.639	-118
915	0.683	-141	2.43	53	0.073	-6	0.639	-119
920	0.686	-141	2.42	53	0.074	-6	0.643	-119
925	0.683	-141	2.40	53	0.073	-7	0.641	-119
930	0.684	-141	2.39	52	0.072	-7	0.640	-120
935	0.682	-142	2.38	52	0.073	-6	0.638	-120
940	0.685	-142	2.37	52	0.072	-6	0.639	-120
945	0.683	-142	2.36	51	0.072	-7	0.638	-120
950	0.683	-143	2.34	51	0.071	-7	0.639	-120
955	0.683	-143	2.33	51	0.070	-7	0.638	-120
960	0.683	-143	2.32	51	0.073	-8	0.640	-121
965	0.683	-143	2.31	50	0.070	-8	0.640	-121
970	0.684	-144	2.30	50	0.071	-7	0.643	-121
975	0.684	-144	2.28	50	0.069	-8	0.640	-121
980	0.682	-144	2.27	49	0.068	-6	0.641	-122
985	0.685	-144	2.26	49	0.069	-9	0.643	-122
990	0.684	-145	2.25	48	0.067	-8	0.644	-122
995	0.683	-145	2.24	48	0.069	-8	0.644	-123
1000	0.684	-145	2.23	48	0.068	-8	0.643	-123

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
5	1.002	-1	7.98	179	0.001	80	0.966	-1
10	0.999	-3	7.99	178	0.003	105	0.969	-2
15	0.999	-4	8.03	176	0.005	87	0.962	-3
20	0.998	-6	7.99	175	0.007	72	0.959	-4
25	0.999	-7	8.00	174	0.008	82	0.959	-5
30	0.997	-9	7.97	173	0.010	89	0.962	-6
35	0.999	-10	7.95	172	0.012	85	0.961	-7
40	0.996	-12	7.94	170	0.014	74	0.962	-8
45	0.994	-13	7.95	169	0.015	77	0.960	-9
50	0.991	-15	7.91	168	0.017	79	0.959	-10
55	0.990	-16	7.88	167	0.017	83	0.959	-11
60	0.988	-18	7.91	165	0.021	77	0.957	-12
65	0.989	-19	7.85	164	0.020	76	0.957	-13
70	0.983	-20	7.83	163	0.022	74	0.954	-15
75	0.981	-22	7.80	162	0.025	78	0.952	-16
80	0.980	-23	7.76	161	0.026	73	0.948	-17
85	0.979	-25	7.72	160	0.026	72	0.946	-18
90	0.977	-26	7.67	158	0.029	72	0.944	-19
95	0.973	-28	7.68	157	0.030	68	0.939	-19
100	0.970	-29	7.62	156	0.031	68	0.934	-20
105	0.970	-30	7.60	155	0.031	68	0.932	-21
109	0.967	-32	7.54	154	0.034	66	0.931	-22
114	0.961	-33	7.49	153	0.034	67	0.926	-23
119	0.960	-34	7.46	152	0.036	66	0.925	-24
124	0.956	-36	7.42	150	0.038	65	0.923	-25
129	0.954	-37	7.41	149	0.039	65	0.923	-26
134	0.948	-38	7.35	148	0.041	63	0.920	-27
139	0.946	-40	7.29	147	0.042	61	0.916	-28
144	0.944	-41	7.25	146	0.044	61	0.913	-29
149	0.939	-42	7.20	145	0.044	60	0.909	-30
154	0.939	-43	7.17	144	0.046	60	0.904	-31
159	0.935	-45	7.11	143	0.046	58	0.900	-32
164	0.932	-46	7.06	142	0.048	57	0.897	-33
169	0.928	-47	7.01	141	0.049	59	0.891	-34
174	0.927	-48	6.94	140	0.049	55	0.885	-34
179	0.922	-49	6.89	139	0.051	55	0.882	-35
184	0.918	-51	6.85	138	0.052	54	0.883	-36
189	0.915	-52	6.82	137	0.053	53	0.878	-36
194	0.912	-53	6.78	136	0.053	50	0.874	-37
199	0.904	-54	6.71	135	0.054	52	0.867	-38
204	0.902	-55	6.65	134	0.054	51	0.868	-39
209	0.902	-56	6.62	133	0.056	50	0.866	-39

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
214	0.898	-58	6.57	132	0.058	50	0.863	-40
219	0.896	-59	6.52	132	0.059	49	0.858	-41
224	0.888	-60	6.47	131	0.059	48	0.850	-42
229	0.887	-61	6.42	130	0.060	46	0.847	-43
234	0.885	-62	6.36	129	0.061	46	0.846	-44
239	0.882	-63	6.35	128	0.062	46	0.837	-45
244	0.876	-64	6.25	127	0.062	45	0.833	-45
249	0.872	-65	6.19	126	0.063	43	0.829	-46
254	0.869	-66	6.15	125	0.064	43	0.828	-47
259	0.867	-67	6.09	125	0.065	43	0.823	-47
264	0.863	-68	6.06	124	0.065	42	0.818	-48
269	0.860	-69	6.01	123	0.065	42	0.816	-48
274	0.856	-70	5.95	122	0.067	41	0.815	-49
279	0.854	-71	5.91	121	0.068	40	0.812	-50
284	0.848	-72	5.87	120	0.068	39	0.809	-50
289	0.849	-73	5.84	120	0.068	38	0.807	-51
294	0.845	-74	5.78	119	0.069	38	0.805	-52
299	0.840	-75	5.73	118	0.070	36	0.800	-53
304	0.839	-75	5.68	117	0.068	37	0.795	-53
308	0.840	-76	5.63	117	0.069	35	0.793	-54
313	0.835	-77	5.59	116	0.071	35	0.790	-55
318	0.832	-78	5.54	115	0.071	35	0.784	-55
323	0.829	-79	5.48	114	0.070	34	0.783	-56
328	0.829	-80	5.45	114	0.072	33	0.778	-56
333	0.825	-81	5.39	113	0.071	33	0.776	-57
338	0.821	-82	5.35	112	0.073	32	0.771	-58
343	0.818	-82	5.31	111	0.072	32	0.770	-58
348	0.816	-83	5.25	111	0.074	30	0.765	-59
353	0.814	-84	5.23	110	0.074	31	0.764	-59
358	0.810	-85	5.18	110	0.073	30	0.764	-59
363	0.810	-85	5.16	109	0.074	30	0.761	-60
368	0.807	-86	5.11	108	0.074	29	0.756	-61
373	0.805	-87	5.07	107	0.075	29	0.760	-61
378	0.801	-88	5.03	107	0.075	27	0.753	-62
383	0.799	-88	4.98	106	0.075	27	0.752	-62
388	0.796	-89	4.94	105	0.074	27	0.748	-63
393	0.796	-90	4.88	105	0.077	26	0.748	-63
398	0.790	-91	4.85	104	0.075	26	0.743	-64
403	0.794	-91	4.82	103	0.076	25	0.739	-64
408	0.789	-92	4.78	103	0.077	26	0.738	-65
413	0.785	-92	4.73	102	0.076	25	0.736	-66
418	0.788	-93	4.70	102	0.076	24	0.732	-66

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
423	0.783	-94	4.66	101	0.077	24	0.730	-66
428	0.784	-95	4.64	101	0.079	23	0.728	-67
433	0.779	-95	4.60	100	0.078	23	0.727	-67
438	0.779	-96	4.55	99	0.078	22	0.727	-68
443	0.775	-97	4.52	99	0.077	21	0.725	-68
448	0.778	-98	4.51	98	0.078	21	0.725	-69
453	0.776	-98	4.46	98	0.078	21	0.719	-69
458	0.771	-99	4.43	97	0.078	21	0.720	-70
463	0.771	-99	4.39	96	0.079	20	0.723	-70
468	0.769	-100	4.36	95	0.079	19	0.716	-71
473	0.767	-100	4.31	95	0.079	18	0.716	-71
478	0.765	-101	4.28	95	0.078	20	0.716	-72
483	0.764	-101	4.24	94	0.079	19	0.710	-72
488	0.763	-102	4.22	94	0.079	19	0.711	-72
493	0.762	-103	4.18	93	0.079	18	0.709	-73
498	0.760	-103	4.15	93	0.080	17	0.706	-73
503	0.760	-104	4.12	92	0.079	16	0.705	-74
507	0.758	-104	4.10	91	0.079	17	0.701	-74
512	0.758	-105	4.08	91	0.079	16	0.700	-74
517	0.751	-105	4.03	90	0.078	16	0.700	-75
522	0.750	-106	4.00	90	0.080	15	0.700	-75
527	0.753	-106	4.00	89	0.079	16	0.698	-76
532	0.750	-107	3.96	89	0.079	14	0.699	-76
537	0.749	-107	3.94	88	0.079	15	0.696	-76
542	0.748	-108	3.90	87	0.080	13	0.696	-77
547	0.749	-109	3.88	87	0.080	13	0.697	-77
552	0.750	-109	3.85	87	0.079	14	0.693	-78
557	0.747	-110	3.82	86	0.078	13	0.697	-78
562	0.743	-110	3.78	86	0.079	12	0.695	-79
567	0.744	-111	3.75	85	0.079	12	0.689	-79
572	0.742	-111	3.73	85	0.078	11	0.690	-79
577	0.743	-112	3.70	84	0.080	12	0.689	-80
582	0.743	-112	3.67	84	0.080	11	0.691	-80
587	0.742	-112	3.64	83	0.078	11	0.688	-80
592	0.740	-113	3.62	83	0.080	10	0.685	-81
597	0.741	-113	3.61	82	0.078	10	0.682	-81
602	0.739	-114	3.59	82	0.078	10	0.685	-82
607	0.736	-114	3.56	82	0.079	9	0.682	-82
612	0.737	-115	3.53	81	0.077	9	0.684	-82
617	0.735	-115	3.52	81	0.078	10	0.682	-82
622	0.736	-115	3.50	80	0.078	9	0.680	-83
627	0.732	-116	3.47	80	0.078	8	0.681	-83

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
632	0.733	-117	3.45	79	0.077	8	0.682	-84
637	0.730	-117	3.41	79	0.078	8	0.684	-84
642	0.731	-117	3.40	78	0.077	8	0.683	-85
647	0.728	-118	3.37	78	0.077	7	0.679	-85
652	0.730	-118	3.35	77	0.077	8	0.679	-85
657	0.725	-119	3.32	77	0.077	7	0.679	-85
662	0.725	-119	3.29	76	0.079	6	0.679	-86
667	0.727	-120	3.27	76	0.078	5	0.677	-86
672	0.731	-120	3.26	75	0.077	6	0.676	-86
677	0.727	-120	3.24	75	0.077	5	0.675	-87
682	0.725	-121	3.21	75	0.077	4	0.673	-87
687	0.726	-121	3.19	74	0.078	6	0.672	-87
692	0.724	-121	3.17	74	0.076	6	0.672	-88
697	0.728	-122	3.17	74	0.075	6	0.672	-88
702	0.724	-122	3.13	73	0.075	5	0.672	-88
706	0.724	-122	3.12	73	0.077	5	0.670	-89
711	0.722	-123	3.10	72	0.077	5	0.674	-89
716	0.722	-123	3.09	72	0.076	4	0.676	-89
721	0.723	-124	3.08	71	0.075	2	0.674	-90
726	0.720	-124	3.05	71	0.075	4	0.672	-90
731	0.719	-124	3.03	70	0.075	4	0.676	-90
736	0.720	-125	3.02	70	0.076	3	0.675	-91
741	0.716	-125	2.99	70	0.075	2	0.672	-91
746	0.718	-126	2.98	69	0.075	3	0.677	-91
751	0.715	-126	2.97	69	0.075	3	0.670	-92
756	0.717	-126	2.94	68	0.075	3	0.673	-92
761	0.716	-127	2.92	68	0.075	2	0.668	-92
766	0.717	-127	2.90	67	0.075	2	0.673	-93
771	0.717	-128	2.88	67	0.073	2	0.669	-93
776	0.714	-128	2.86	67	0.076	1	0.668	-93
781	0.718	-128	2.86	66	0.074	1	0.668	-93
786	0.718	-129	2.85	66	0.073	1	0.670	-94
791	0.718	-129	2.82	66	0.073	1	0.670	-94
796	0.716	-129	2.81	65	0.072	0	0.668	-94
801	0.715	-130	2.79	65	0.073	-1	0.671	-95
806	0.718	-130	2.77	65	0.071	1	0.669	-95
811	0.714	-130	2.77	64	0.072	0	0.672	-95
816	0.714	-130	2.74	64	0.072	0	0.673	-96
821	0.714	-131	2.72	63	0.070	0	0.671	-96
826	0.715	-131	2.71	63	0.073	0	0.675	-96
831	0.713	-131	2.69	63	0.071	0	0.672	-96
836	0.713	-131	2.68	62	0.072	-1	0.672	-97

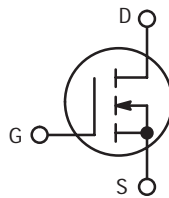
Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
841	0.712	-132	2.67	62	0.069	0	0.671	-97
846	0.710	-132	2.65	61	0.071	-1	0.672	-97
851	0.708	-132	2.63	61	0.071	-1	0.670	-97
856	0.712	-133	2.62	61	0.071	-2	0.669	-98
861	0.710	-133	2.61	61	0.071	-2	0.669	-98
866	0.710	-134	2.59	60	0.071	-2	0.669	-98
871	0.710	-134	2.58	60	0.071	-2	0.669	-98
876	0.713	-134	2.57	59	0.069	-3	0.666	-99
881	0.711	-135	2.56	59	0.068	-3	0.667	-99
886	0.710	-135	2.54	59	0.069	-3	0.666	-99
891	0.711	-135	2.52	58	0.067	-3	0.668	-100
896	0.711	-136	2.52	58	0.070	-2	0.670	-100
901	0.709	-136	2.50	57	0.069	-5	0.669	-101
905	0.711	-136	2.49	57	0.069	-3	0.671	-101
910	0.711	-136	2.47	57	0.068	-4	0.674	-101
915	0.710	-137	2.46	56	0.068	-2	0.673	-101
920	0.712	-137	2.45	56	0.066	-4	0.673	-102
925	0.708	-137	2.42	56	0.067	-4	0.673	-102
930	0.709	-137	2.42	55	0.068	-3	0.673	-102
935	0.709	-138	2.41	55	0.066	-4	0.670	-102
940	0.709	-138	2.40	55	0.066	-2	0.672	-102
945	0.709	-138	2.39	54	0.065	-3	0.672	-103
950	0.708	-139	2.38	54	0.066	-4	0.671	-103
955	0.711	-139	2.36	54	0.065	-5	0.669	-103
960	0.709	-139	2.35	54	0.064	-4	0.672	-103
965	0.708	-140	2.34	53	0.064	-3	0.671	-104
970	0.707	-140	2.33	53	0.065	-5	0.673	-104
975	0.706	-140	2.32	52	0.065	-4	0.671	-104
980	0.707	-140	2.30	52	0.065	-4	0.669	-104
985	0.707	-140	2.29	51	0.064	-6	0.674	-105
990	0.708	-141	2.28	51	0.063	-4	0.674	-105
995	0.708	-141	2.28	51	0.063	-5	0.674	-105
1000	0.710	-141	2.26	50	0.063	-5	0.676	-106

The RF MOSFET Line
Power Field Effect Transistor
N-Channel Enhancement-Mode MOSFET

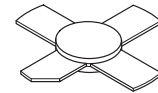
Designed primarily for wideband large-signal output and driver from 30–500 MHz.

- Guaranteed 28 Volt, 500 MHz Performance
Output Power = 4.0 Watts
Gain = 16 dB (Min)
Efficiency = 55% (Typ)
- Excellent Thermal Stability, Ideally Suited for Class A Operation
- Facilitates Manual Gain Control, ALC and Modulation Techniques
- 100% Tested for Load Mismatch at All Phase Angles with 30:1 VSWR
- Low C_{RSS} – 0.8 pF Typical at $V_{DS} = 28$ Volts
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://mot-sps.com/rf/designtds/>



MRF160

To 500 MHz, 4 W, 28 V
MOSFET BROADBAND
RF POWER FET



CASE 249-06, STYLE 3

MAXIMUM RATINGS ($T_J = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-Gate Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1.0\text{ M}\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current-Continuous	I_D	1.0	ADC
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate Above 25°C	P_D	24 0.14	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	- 65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Thermal Resistance — Junction to Case	$R_{\theta JC}$	7.2	$^\circ\text{C}/\text{W}$
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NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{DS} = 0\text{ Vdc}$, $V_{GS} = 0\text{ Vdc}$, $I_D = 1.0\text{ mA}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	—	—	0.5	mA
Gate–Source Leakage Current ($V_{GS} = 20\text{ Vdc}$, $V_{DS} = 0\text{ Vdc}$)	I_{GSS}	—	—	1.0	μA

ON CHARACTERISTICS

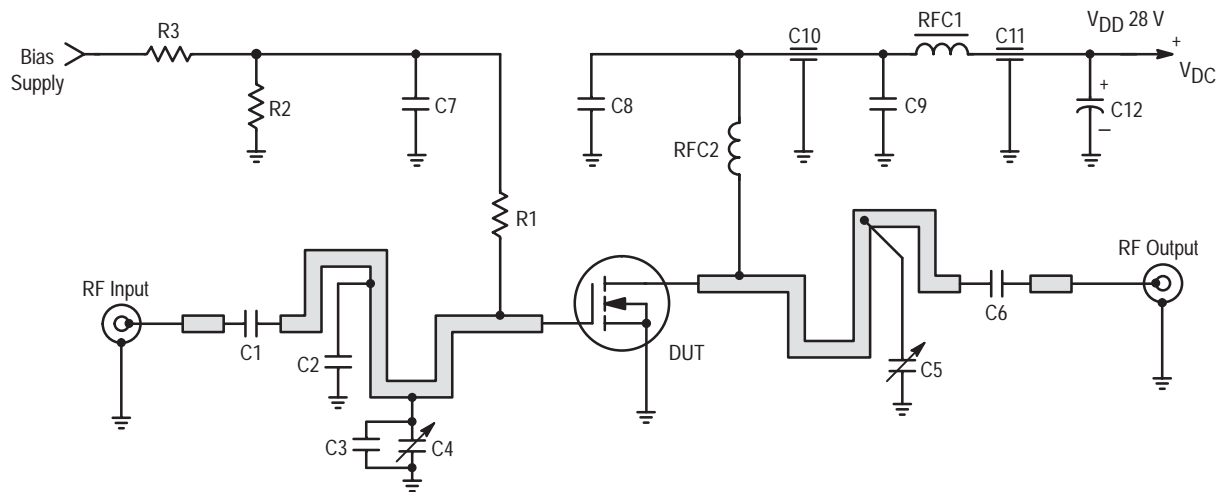
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 10\text{ mA}$)	$V_{GS(th)}$	1.5	3.0	4.5	Vdc
Drain Source On–Voltage ($V_{DS(on)}$, $V_{GS} = 10\text{ Vdc}$, $I_D = 500\text{ mA}$)	$V_{DS(on)}$	—	3.8	—	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 250\text{ mA}$)	g_{fs}	150	220	—	mS

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{iss}	—	6.0	—	pF
Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ Vdc}$, $f = 1.0\text{ MHz}$)	C_{oss}	—	6.5	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0\text{ Vdc}$, $f = 1.0\text{ MHz}$)	C_{rss}	—	0.8	—	pF

FUNCTIONAL CHARACTERISTICS

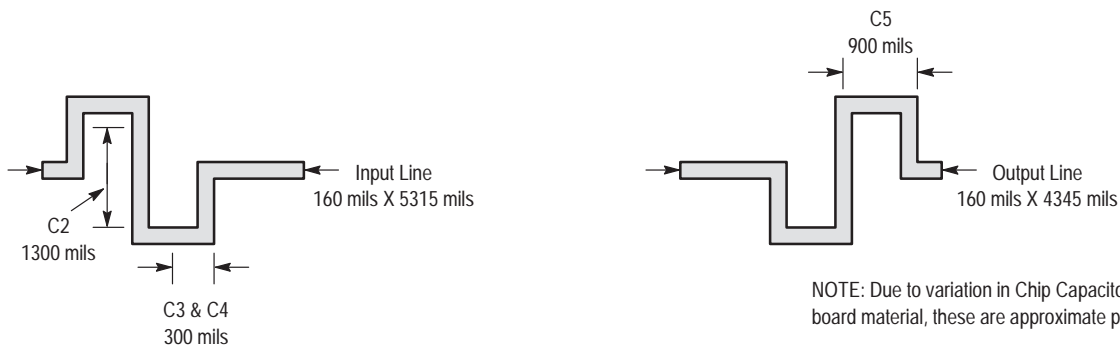
Common Source Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 4.0\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	G_{ps}	16	18	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 4.0\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	η	50	55	—	%
Electrical Ruggedness ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 4.0\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 50\text{ mA}$) Load VSWR = 30:1 at All Phase Angles at Frequency of Test	ψ	No Degradation in Output Power			
Series Equivalent Input Impedance ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 4.0\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	Z_{in}	—	$6.8 - j21$	—	Ohms
Series Equivalent Output Impedance ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 4.0\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	Z_{out}	—	$21 - j28$	—	Ohms



- C1, C6 240 pF, 100 mil Chip Capacitors
- C2 15 pF, 100 mil ATC Chip Capacitor
- C4, C5 1 – 10 pF, Johanson Trimmer Capacitors
- C3 24 pF, 100 mil ATC Chip Capacitor
- C7, C9 0.1 μ F, 100 mil Chip Capacitors
- C8 220 pF, 100 mil ATC Chip Capacitor
- C10, C11 680 pF, Feed Through Capacitors
- C12 50 μ F, 50 V Electrolytic Capacitor

- R1 200 Ω , 1/2 Watt
- R2 10 k Ω , 1/2 Watt
- R3 1 k Ω , 1/2 Watt
- RFC1 Ferroxcube VK200–19/4B
- RFC2 8 Turns, #20 AWG, Enameled, ID 110 mils

Board Material — 0.062", Teflon[®] Fiberglass, 1 oz.,
Copper clad both sides, $\epsilon_r = 2.55$



NOTE: Due to variation in Chip Capacitor values and board material, these are approximate positions.

Figure 1. MRF160 500 MHz Test Circuit

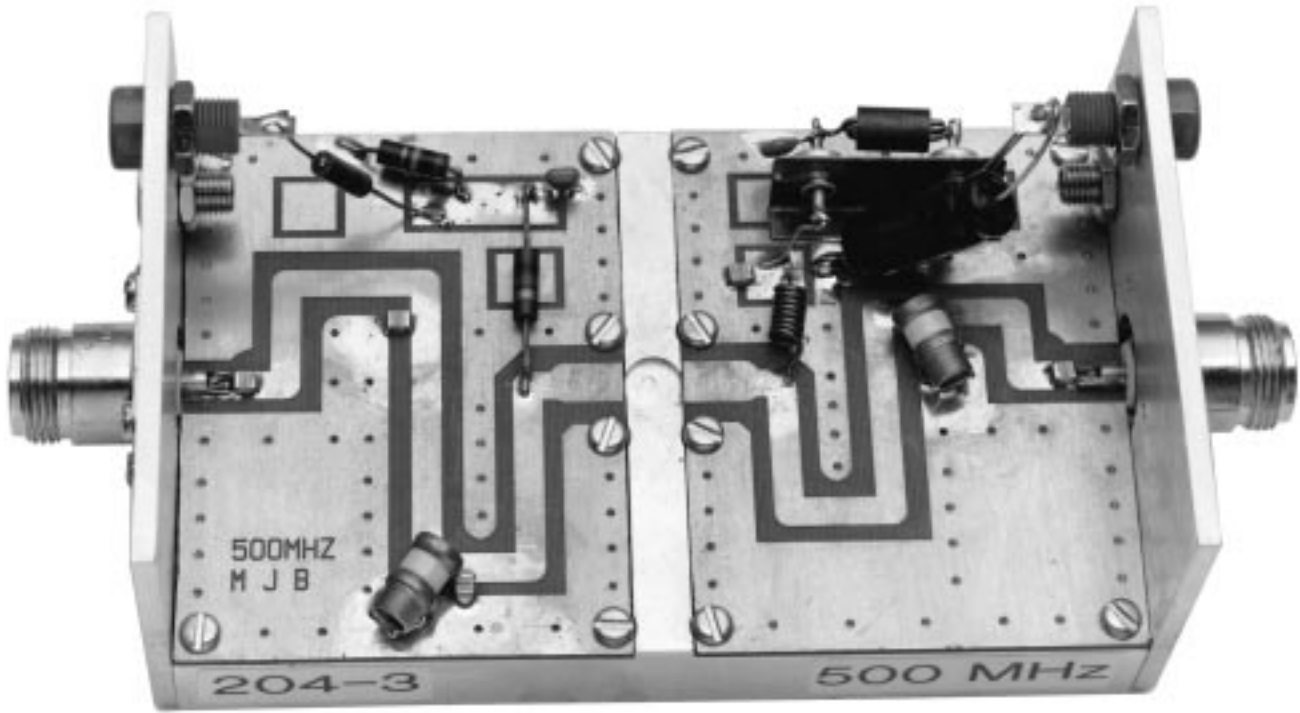


Figure 2. MRF160 Broadband Test Fixture

TYPICAL CHARACTERISTICS

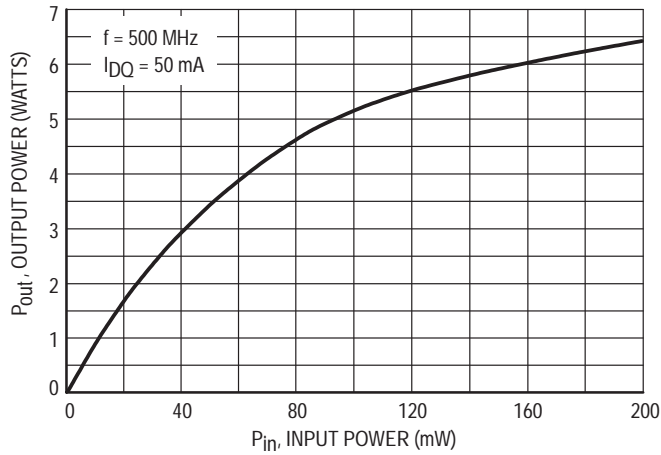


Figure 3. Output Power versus Input Power

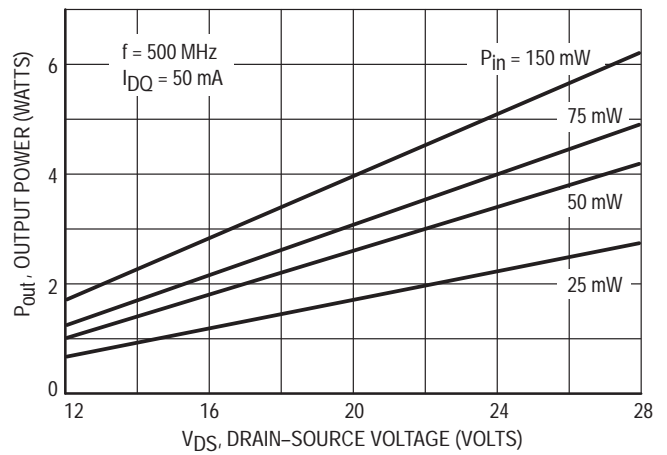


Figure 4. Output Power versus Voltage

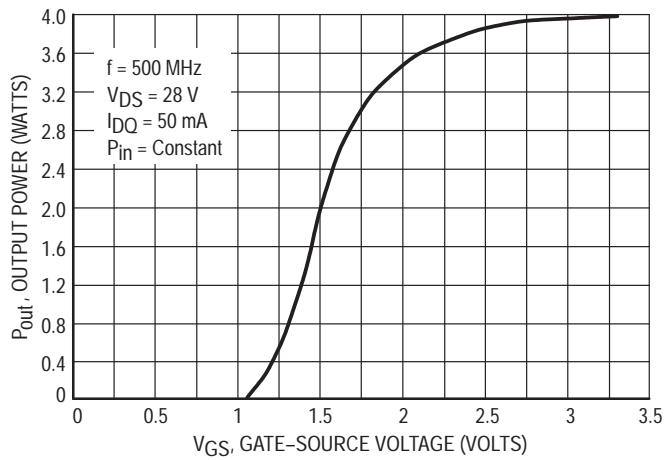


Figure 5. Output Power versus Gate Voltage

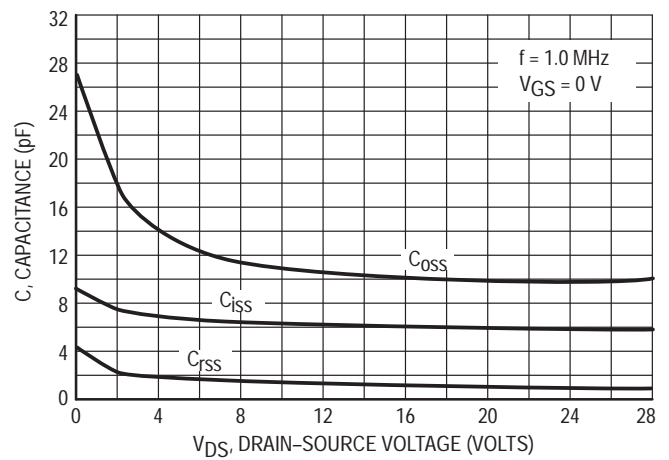


Figure 6. Capacitance versus Drain-Source Voltage

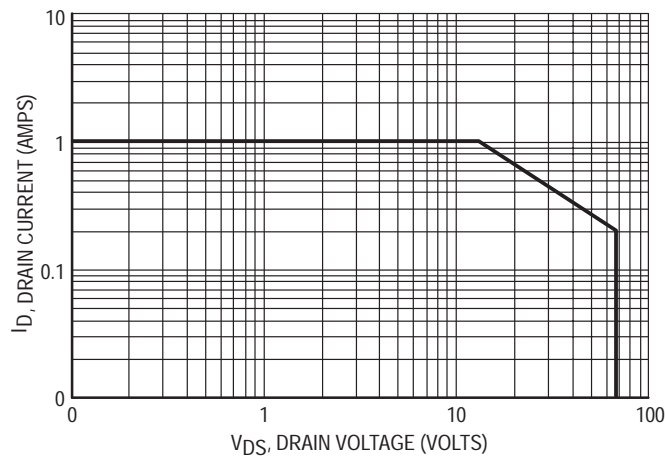


Figure 7. DC Safe Operating Area

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 120\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.991	-19	15.80	166	0.019	77	0.938	-19
40	0.970	-25	15.50	161	0.025	72	0.933	-25
50	0.959	-31	15.20	156	0.030	67	0.918	-31
60	0.943	-37	14.80	151	0.035	63	0.900	-37
70	0.925	-42	14.30	147	0.040	59	0.880	-42
80	0.912	-48	13.90	143	0.044	56	0.863	-47
85	0.903	-51	13.70	141	0.046	54	0.857	-49
90	0.896	-53	13.50	139	0.048	52	0.851	-52
100	0.872	-58	12.90	135	0.051	48	0.830	-57
110	0.853	-63	12.40	131	0.054	46	0.812	-60
120	0.841	-67	11.90	128	0.056	43	0.796	-63
130	0.831	-71	11.50	126	0.059	40	0.788	-67
140	0.814	-75	11.10	122	0.061	37	0.777	-70
150	0.797	-79	10.70	119	0.063	34	0.760	-74
160	0.782	-82	10.20	117	0.064	32	0.739	-78
170	0.776	-85	9.81	115	0.066	32	0.740	-79
180	0.769	-89	9.55	112	0.068	28	0.737	-83
190	0.754	-92	9.24	109	0.069	25	0.725	-87
200	0.737	-94	8.83	107	0.068	23	0.707	-90
210	0.731	-96	8.47	105	0.068	22	0.692	-92
220	0.730	-99	8.20	103	0.069	21	0.692	-94
230	0.724	-101	7.94	101	0.071	20	0.697	-95
240	0.713	-104	7.69	99	0.072	16	0.696	-99
250	0.705	-106	7.44	97	0.070	15	0.676	-100
260	0.699	-108	7.18	96	0.070	15	0.673	-102
270	0.697	-109	6.91	94	0.070	14	0.661	-103
280	0.697	-111	6.70	93	0.071	13	0.654	-104
290	0.693	-113	6.54	92	0.071	11	0.658	-106
300	0.686	-115	6.36	90	0.072	9	0.664	-108
310	0.679	-116	6.12	88	0.069	7	0.639	-111
320	0.679	-117	5.96	87	0.070	9	0.642	-110
330	0.679	-119	5.80	86	0.070	8	0.648	-112
340	0.679	-121	5.63	84	0.071	7	0.648	-114
350	0.674	-122	5.47	83	0.070	5	0.645	-114
360	0.669	-123	5.33	82	0.070	4	0.650	-116
370	0.667	-124	5.18	80	0.068	3	0.644	-118
380	0.672	-125	5.02	80	0.066	3	0.614	-119
390	0.675	-127	4.96	78	0.071	4	0.655	-116
400	0.672	-129	4.83	77	0.070	2	0.655	-119
410	0.668	-130	4.70	75	0.069	0	0.654	-121
420	0.666	-131	4.56	74	0.067	-1	0.644	-122
430	0.667	-131	4.48	74	0.066	-1	0.646	-122

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 120\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
440	0.671	-132	4.39	72	0.066	-1	0.651	-123
450	0.670	-134	4.29	71	0.068	-1	0.663	-123
460	0.662	-135	4.15	70	0.067	-6	0.677	-127
470	0.663	-135	4.05	69	0.065	-5	0.664	-127
480	0.666	-136	3.95	68	0.064	-5	0.663	-128
490	0.670	-137	3.88	67	0.064	-5	0.663	-128
500	0.670	-138	3.81	66	0.063	-6	0.670	-128
600	0.693	-147	3.06	55	0.053	-17	0.689	-136
700	0.708	-152	2.61	46	0.044	-14	0.723	-142
800	0.731	-158	2.22	40	0.037	-15	0.733	-146
900	0.724	-165	1.93	32	0.037	-32	0.760	-151
1000	0.748	-169	1.73	28	0.027	-6	0.778	-153

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 250\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.995	-18	15.00	167	0.014	78	0.919	-15
40	0.978	-24	14.70	162	0.018	73	0.913	-19
50	0.971	-30	14.50	158	0.022	69	0.900	-23
60	0.961	-36	14.20	153	0.026	65	0.885	-28
70	0.947	-41	13.80	149	0.029	62	0.867	-32
80	0.938	-46	13.40	145	0.033	58	0.851	-35
85	0.932	-49	13.30	143	0.034	56	0.845	-37
90	0.927	-51	13.10	141	0.036	55	0.839	-39
100	0.908	-56	12.70	138	0.038	51	0.825	-43
110	0.893	-61	12.20	134	0.040	49	0.802	-46
120	0.884	-65	11.80	131	0.043	46	0.788	-48
130	0.875	-69	11.40	128	0.045	44	0.781	-51
140	0.862	-74	11.10	125	0.047	40	0.772	-54
150	0.848	-78	10.70	122	0.048	37	0.754	-57
160	0.836	-81	10.30	119	0.049	35	0.733	-60
170	0.830	-84	9.86	117	0.050	35	0.718	-60
180	0.824	-88	9.64	115	0.053	31	0.729	-64
190	0.813	-91	9.38	112	0.053	29	0.719	-67
200	0.798	-94	9.00	109	0.053	26	0.701	-70
210	0.792	-96	8.63	107	0.053	25	0.682	-72
220	0.790	-98	8.36	105	0.054	24	0.677	-73
230	0.785	-101	8.10	104	0.055	22	0.677	-75
240	0.777	-104	7.92	101	0.057	19	0.694	-78
250	0.769	-106	7.65	99	0.055	18	0.663	-80
260	0.764	-108	7.40	97	0.055	18	0.662	-81
270	0.761	-109	7.13	96	0.055	17	0.649	-82
280	0.760	-111	6.91	95	0.055	16	0.640	-82

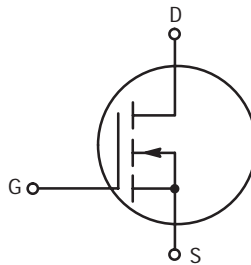
Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 250\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
290	0.757	-113	6.75	93	0.055	14	0.641	-84
300	0.751	-115	6.59	91	0.056	12	0.645	-86
310	0.743	-117	6.37	89	0.055	9	0.635	-90
320	0.744	-118	6.17	88	0.054	11	0.619	-89
330	0.744	-120	6.01	87	0.055	11	0.628	-90
340	0.743	-121	5.85	85	0.055	10	0.629	-92
350	0.738	-123	5.70	84	0.055	8	0.629	-92
360	0.733	-124	5.55	82	0.054	6	0.631	-94
370	0.730	-126	5.40	81	0.054	4	0.623	-96
380	0.732	-127	5.21	80	0.052	4	0.593	-98
390	0.737	-129	5.17	79	0.055	7	0.627	-93
400	0.734	-130	5.04	77	0.055	4	0.639	-97
410	0.731	-131	4.92	76	0.054	3	0.641	-99
420	0.728	-132	4.78	75	0.052	1	0.630	-100
430	0.729	-133	4.67	74	0.051	0	0.628	-101
440	0.731	-134	4.57	72	0.051	1	0.626	-102
450	0.731	-136	4.47	71	0.053	1	0.630	-102
460	0.723	-137	4.37	69	0.054	-4	0.673	-106
470	0.724	-137	4.24	68	0.050	-3	0.647	-107
480	0.727	-138	4.13	68	0.049	-3	0.642	-108
490	0.730	-139	4.05	67	0.048	-3	0.641	-107
500	0.730	-140	3.99	66	0.048	-4	0.647	-108
600	0.736	-150	3.54	56	0.037	-14	0.657	-118
700	0.745	-156	2.99	46	0.029	-9	0.699	-126
800	0.765	-161	2.54	39	0.025	-5	0.713	-131
900	0.759	-168	2.20	31	0.022	-34	0.742	-136
1000	0.769	-173	1.98	27	0.018	19	0.756	-139

The RF MOSFET Line
RF Power
Field Effect Transistors
N-Channel Enhancement Mode MOSFETs

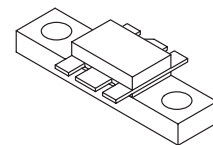
Designed primarily for wideband large-signal output and driver from 30–500 MHz.

- MRF166C — Guaranteed Performance at 500 MHz, 28 Vdc
Output Power = 20 W
Gain = 13.5 dB
Efficiency = 50%
- Replacement for Industry Standards such as MRF136, DV2820, BLF244, SD1902, and ST1001
- 100% Tested for Load Mismatch at all Phase Angles with 30:1 VSWR
- Facilitates Manual Gain Control, ALC and Modulation Techniques
- Excellent Thermal Stability, Ideally Suited for Class A Operation
- Low C_{rss} — 4.0 pF @ $V_{DS} = 28$ V
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://mot-sps.com/rf/designtds/>



MRF166C

20 W, 500 MHz
MOSFET
BROADBAND
RF POWER FETs



CASE 319-07, STYLE 3

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain–Gate Voltage	V_{DSS}	65	Vdc
Drain–Gate Voltage ($R_{GS} = 1.0$ M Ω)	V_{DGR}	65	Vdc
Gate–Source Voltage	V_{GS}	± 20	Adc
Drain Current — Continuous	I_D	4.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate Above 25°C	P_D	70 0.4	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to 150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

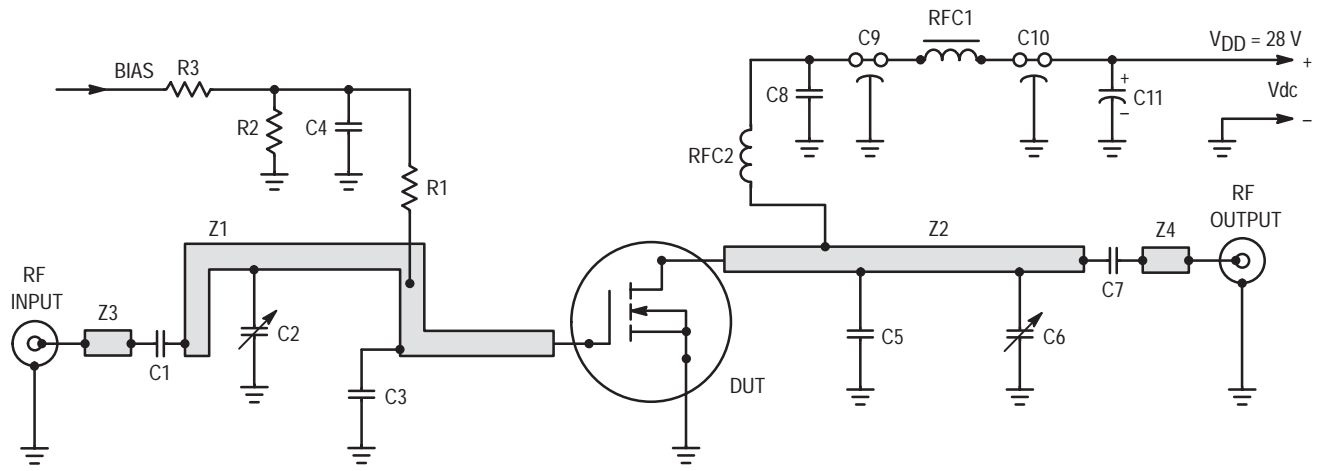
THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	2.5	$^\circ\text{C}/\text{W}$

NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

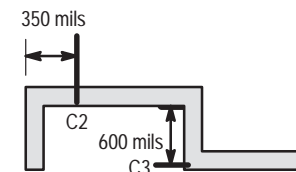
ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ V}$, $I_D = 5.0\text{ mA}$)	$V_{(BR)DSS}$	65	—	—	V
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	—	—	0.5	mA
Gate–Source Leakage Current ($V_{GS} = 20\text{ V}$, $V_{DS} = 0\text{ V}$)	I_{GSS}	—	—	1.0	μA
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 25\text{ mA}$)	$V_{GS(th)}$	1.5	3.0	4.5	V
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 1.5\text{ A}$)	g_{fs}	0.8	1.1	—	mhos
DYNAMIC CHARACTERISTICS					
Input Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{iss}	—	28	—	pF
Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{oss}	—	30	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{rss}	—	4.0	—	pF
FUNCTIONAL CHARACTERISTICS					
Common Source Power Gain ($V_{DD} = 28\text{ V}$, $P_{out} = 20\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 25\text{ mA}$)	G_{ps}	13.5	16	—	dB
Drain Efficiency ($V_{DD} = 28\text{ V}$, $P_{out} = 20\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 25\text{ mA}$)	η	50	55	—	%
Electrical Ruggedness ($V_{DD} = 28\text{ V}$, $P_{out} = 20\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 25\text{ mA}$, Load VSWR 30:1 at All Phase Angles)	ψ	No Degradation in Output Power			

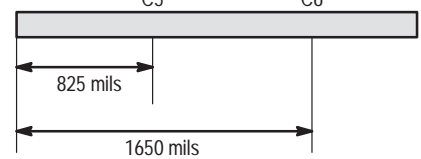


- C1, C7 200 pF, Chip Capacitor
- C2, C6 2–10 pF, Trimmer Capacitor, Johansen
- C3 27 pF, ATC 100 mil Chip Capacitor
- C4, C8 0.1 μF, Chip Capacitor
- C5 15 pF, ATC 100 mil Chip Capacitor
- C9, C10 680 pF, Feedthru Capacitor
- C11 50 μF, 50 V, Electrolytic Capacitor
- R1 120 Ω, 1/2 W Resistor
- R2 10 kΩ, 1/2 W Resistor
- R3 1 kΩ, 1/2 W Resistor
- RFC1 Ferroxcube VK200 19/4B
- RFC2 10 Turns AWG #18, 0.125" I.D., Enameled
- Board Material 0.062" Teflon® Fiberglass
- 1 oz. Copper Clad Both Sides
- $\epsilon_r = 2.56$

Z1 0.120" x 3.3", Microstrip Line



Z2 0.120" x 2.1", Microstrip Line



Z3, Z4 0.120" x 0.25", Microstrip Line

Figure 1. MRF166C 500 MHz Test Circuit

TYPICAL CHARACTERISTICS

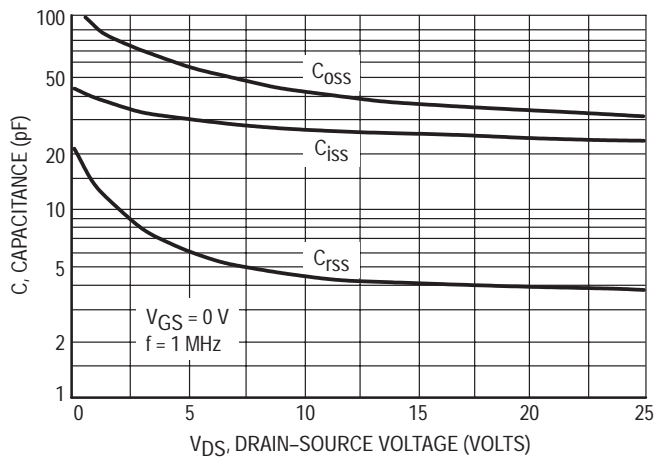


Figure 2. Capacitance versus Drain-Source Voltage

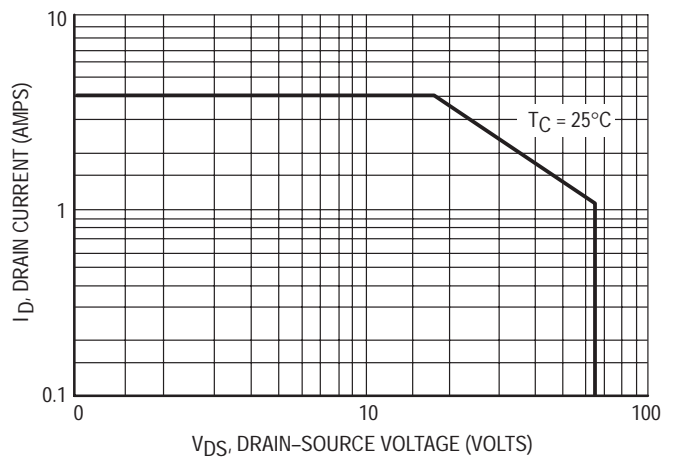


Figure 3. DC Safe Operating Area

TYPICAL CHARACTERISTICS

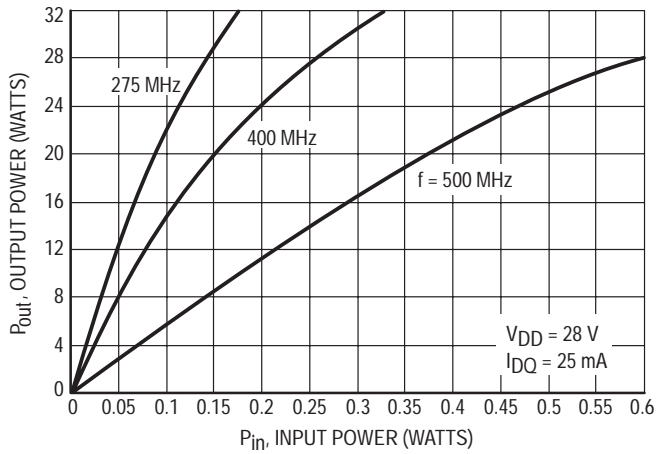


Figure 4. Output Power versus Input Power

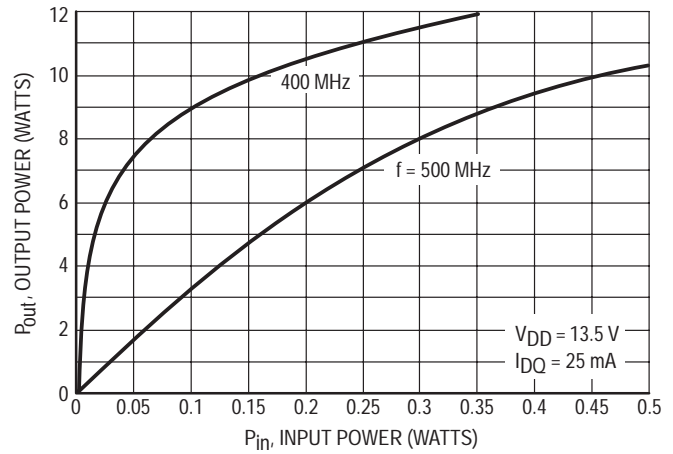


Figure 5. Output Power versus Input Power

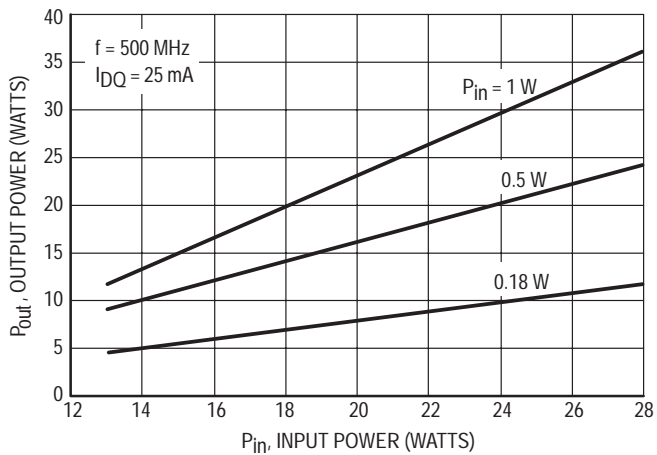


Figure 6. Output Power versus Supply Voltage

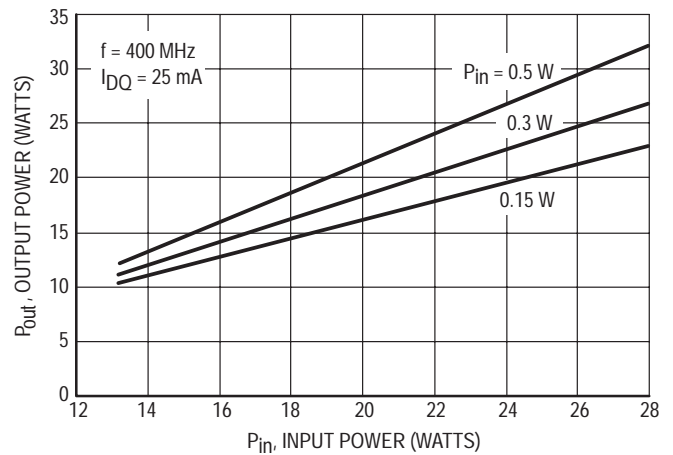
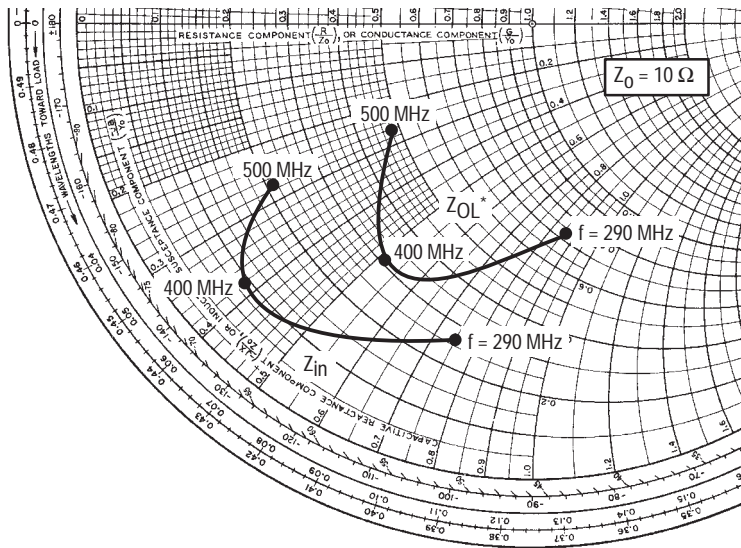


Figure 7. Output Power versus Supply Voltage



$V_{DD} = 28 \text{ V}$, $I_{DQ} = 25 \text{ mA}$, $P_{out} = 20 \text{ Watts}$

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
500	$2.09 - j2.77$	$4.87 - j2.63$
400	$0.93 - j3.80$	$3.09 - j5.24$
290	$2.63 - j7.58$	$7.35 - j8.67$

Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

Figure 8. Series Equivalent Input and Output Impedance

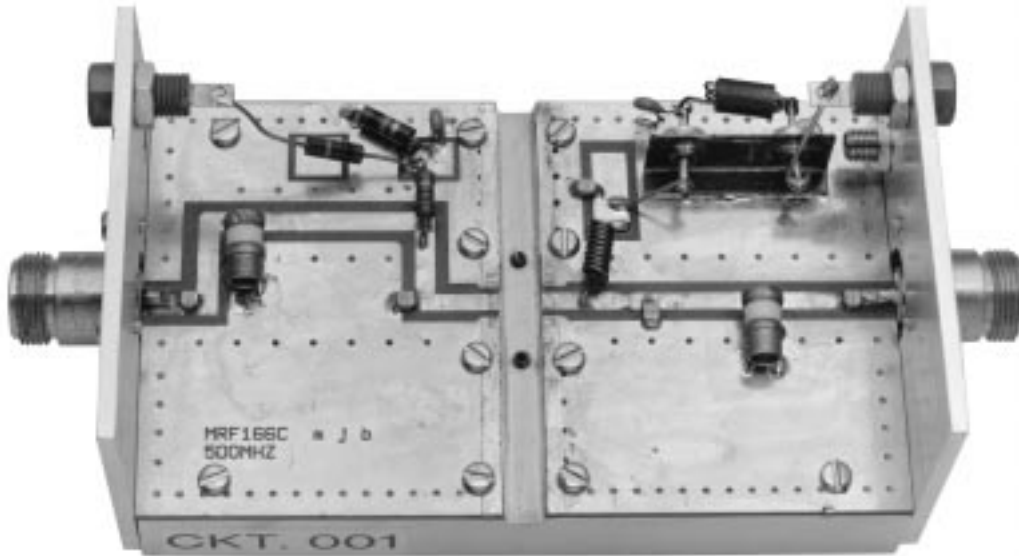


Figure 9. MRF166C Test Fixture

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 1.25\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.840	-142	22.59	105	0.025	20	0.727	-155
40	0.836	-151	17.4	100	0.025	17	0.743	-161
50	0.832	-156	14.1	97	0.026	15	0.751	-164
60	0.829	-159	12.0	94	0.026	14	0.764	-166
70	0.826	-162	10.4	91	0.026	14	0.763	-168
80	0.822	-164	9.09	90	0.026	14	0.763	-169
90	0.818	-165	8.07	89	0.027	14	0.765	-170
100	0.819	-167	7.28	87	0.027	14	0.774	-171
110	0.821	-168	6.61	85	0.027	14	0.773	-172
120	0.821	-169	6.00	83	0.026	15	0.771	-172
130	0.820	-169	5.56	83	0.027	16	0.778	-172
140	0.818	-170	5.22	82	0.027	17	0.785	-172
150	0.820	-170	4.86	80	0.027	17	0.786	-173
160	0.821	-171	4.52	79	0.027	17	0.781	-173
170	0.820	-171	4.23	79	0.027	20	0.774	-172
180	0.820	-171	4.03	78	0.027	20	0.799	-173
190	0.820	-172	3.86	76	0.027	20	0.799	-174
200	0.821	-172	3.62	75	0.027	20	0.784	-175
210	0.822	-173	3.39	75	0.027	22	0.780	-174
220	0.823	-173	3.25	74	0.027	24	0.795	-173
230	0.825	-173	3.12	72	0.028	23	0.823	-175
240	0.827	-173	2.96	71	0.026	24	0.791	-175
250	0.827	-174	2.83	70	0.027	26	0.789	-174
260	0.827	-174	2.71	70	0.026	27	0.791	-174
270	0.829	-174	2.62	69	0.027	28	0.801	-174
280	0.831	-174	2.52	68	0.027	29	0.807	-175
290	0.832	-174	2.42	66	0.027	30	0.788	-175
300	0.832	-174	2.32	66	0.027	32	0.792	-175
310	0.831	-174	2.25	66	0.027	33	0.797	-174
320	0.833	-175	2.18	65	0.027	34	0.810	-174
330	0.836	-175	2.10	63	0.028	35	0.812	-175
340	0.837	-175	2.00	62	0.027	35	0.789	-176
350	0.838	-175	1.95	62	0.028	39	0.806	-173
360	0.839	-175	1.90	61	0.028	39	0.817	-174
370	0.840	-176	1.84	60	0.028	40	0.817	-175
380	0.843	-176	1.77	59	0.028	41	0.811	-175
390	0.845	-176	1.71	59	0.028	42	0.805	-175
400	0.846	-176	1.66	58	0.029	46	0.801	-172
410	0.846	-176	1.64	57	0.030	46	0.845	-174
420	0.847	-176	1.59	56	0.030	46	0.836	-176
430	0.848	-176	1.52	56	0.030	47	0.823	-176
440	0.850	-176	1.48	56	0.030	49	0.816	-174

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 1.25\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
450	0.851	-176	1.47	54	0.032	51	0.851	-174
460	0.853	-177	1.42	53	0.032	48	0.849	-178
470	0.853	-177	1.37	53	0.031	51	0.830	-176
480	0.856	-177	1.34	53	0.032	53	0.834	-176
490	0.857	-177	1.32	52	0.033	54	0.841	-175
500	0.859	-177	1.28	51	0.034	54	0.847	-175
600	0.857	178	0.988	41	0.032	73	0.877	180
700	0.884	176	0.789	34	0.047	65	0.881	179
800	0.881	173	0.684	30	0.031	83	0.890	174
900	0.890	172	0.580	26	0.069	71	0.885	176
1000	0.897	170	0.503	24	0.090	60	0.931	173

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 1.25\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.842	-125	29.6	113	0.024	28	0.586	-136
40	0.831	-136	23.2	106	0.025	22	0.607	-145
50	0.822	-143	19.0	101	0.026	19	0.613	-151
60	0.816	-148	16.2	98	0.026	17	0.626	-155
70	0.812	-152	14.1	95	0.027	16	0.635	-157
80	0.806	-155	12.4	92	0.026	15	0.643	-159
90	0.801	-157	11.1	90	0.027	14	0.650	-160
100	0.802	-159	9.97	88	0.027	13	0.656	-161
110	0.805	-161	9.04	86	0.027	13	0.654	-163
120	0.805	-162	8.22	84	0.026	13	0.654	-163
130	0.803	-163	7.59	83	0.026	14	0.663	-163
140	0.801	-164	7.09	82	0.026	14	0.673	-164
150	0.803	-165	6.61	80	0.026	14	0.675	-164
160	0.804	-165	6.16	79	0.026	14	0.674	-164
170	0.803	-166	5.77	78	0.026	16	0.672	-164
180	0.804	-166	5.49	77	0.026	17	0.697	-164
190	0.806	-166	5.25	75	0.026	16	0.700	-165
200	0.806	-167	4.92	73	0.025	16	0.688	-166
210	0.807	-168	4.60	73	0.025	17	0.680	-165
220	0.809	-168	4.40	72	0.025	19	0.689	-165
230	0.812	-168	4.21	70	0.025	19	0.713	-167
240	0.814	-169	3.99	69	0.024	20	0.701	-167
250	0.815	-169	3.83	68	0.024	21	0.707	-166
260	0.816	-169	3.66	67	0.024	22	0.711	-166
270	0.818	-169	3.52	66	0.024	23	0.715	-166
280	0.821	-169	3.39	65	0.025	24	0.718	-167
290	0.822	-170	3.25	63	0.024	26	0.708	-168
300	0.823	-170	3.11	62	0.023	28	0.715	-167

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 1.25\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
310	0.822	-170	2.99	62	0.023	29	0.725	-166
320	0.825	-170	2.89	61	0.024	31	0.734	-166
330	0.828	-171	2.78	60	0.024	33	0.736	-167
340	0.830	-171	2.66	59	0.024	33	0.724	-168
350	0.832	-171	2.59	58	0.024	37	0.739	-166
360	0.834	-171	2.52	57	0.024	39	0.757	-166
370	0.836	-171	2.44	56	0.023	39	0.755	-167
380	0.839	-172	2.34	55	0.023	38	0.745	-167
390	0.840	-172	2.26	54	0.024	40	0.738	-168
400	0.841	-172	2.19	54	0.024	46	0.735	-166
410	0.842	-172	2.14	53	0.025	46	0.787	-167
420	0.844	-172	2.09	51	0.026	46	0.790	-168
430	0.845	-173	1.99	51	0.027	49	0.777	-168
440	0.846	-173	1.93	51	0.026	52	0.770	-167
450	0.849	-173	1.91	49	0.027	53	0.794	-167
460	0.853	-173	1.84	48	0.027	51	0.803	-171
470	0.855	-173	1.77	47	0.027	54	0.787	-170
480	0.857	-174	1.72	47	0.027	57	0.789	-169
490	0.857	-174	1.68	47	0.027	56	0.796	-168
500	0.859	-174	1.64	46	0.029	57	0.802	-169
600	0.862	-179	1.18	33	0.036	77	0.851	-173
700	0.893	178	0.921	26	0.043	75	0.856	-175
800	0.890	175	0.771	22	0.043	78	0.880	-178
900	0.895	173	0.635	17	0.065	74	0.882	-178
1000	0.905	171	0.544	14	0.086	69	0.931	178

The RF MOSFET Line

Power Field Effect Transistor

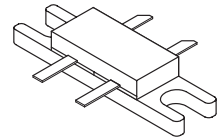
N-Channel Enhancement-Mode MOSFET

Designed primarily for wideband large-signal output and driver stages to 30 – 500 MHz.

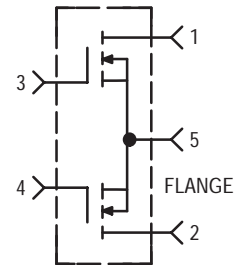
- Push-Pull Configuration Reduces Even Numbered Harmonics
- Guaranteed Performance at 500 MHz, 28 Vdc
 - Output Power = 40 Watts
 - Gain = 14 dB
 - Efficiency = 50%
- Typical Performance at 175 MHz, 28 Vdc
 - Output Power = 40 Watts
 - Gain = 17 dB
 - Efficiency = 60%
- Excellent Thermal Stability, Ideally Suited for Class A Operation
- Facilitates Manual Gain Control, ALC and Modulation Techniques
- 100% Tested for Load Mismatch at All Phase Angles with 30:1 VSWR
- Low C_{RSS} — 4.0 pF @ $V_{DS} = 28$ Volts
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.
- S-Parameters Available for Download into Frequency Domain Simulators. See <http://motorola.com/sps/rf/designtds/>

MRF166W

**40 W, 500 MHz
TMOS BROADBAND
RF POWER FET**



CASE 412-01, Style 1



MAXIMUM RATINGS ($T_J = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-Gate Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1.0 \text{ M}\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Adc
Drain Current — Continuous	I_D	8.0	ADC
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	175 1.0	Watts $^\circ\text{C/W}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Thermal Resistance — Junction to Case	$R_{\theta JC}$	1.0	$^\circ\text{C/W}$
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NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS (1)

Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 5.0\text{ mA}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0\text{ Vdc}$)	I_{DSS}	—	—	0.5	mA
Gate–Source Leakage Current ($V_{GS} = 20\text{ Vdc}$, $V_{DS} = 0\text{ Vdc}$)	I_{GSS}	—	—	1.0	μA

ON CHARACTERISTICS (1)

Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 25\text{ mA}$)	$V_{GS(th)}$	1.5	3.0	4.5	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 1.5\text{ A}$)	g_{fs}	0.9	1.1	—	mS

DYNAMIC CHARACTERISTICS (1)

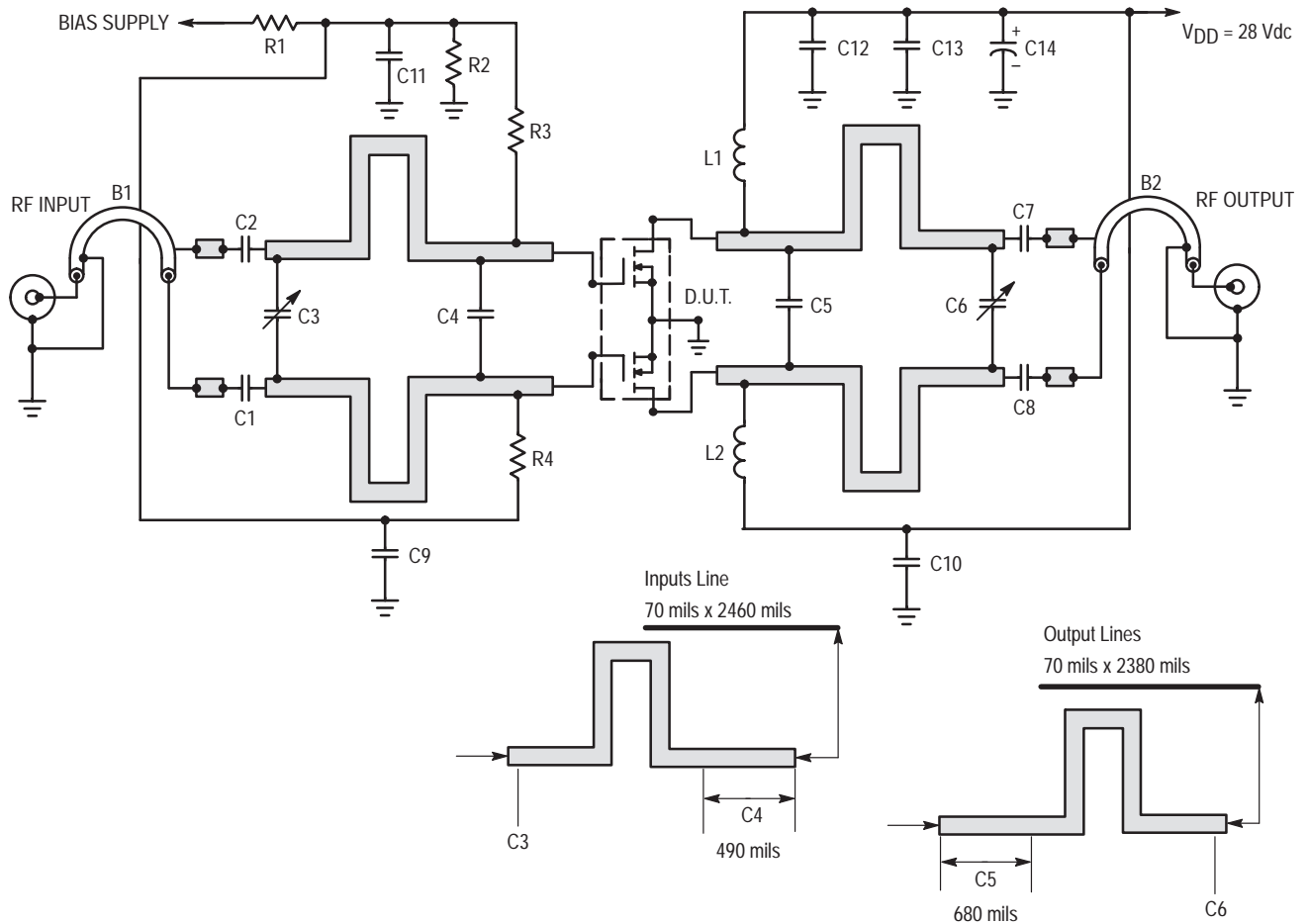
Input Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0\text{ Vdc}$, $f = 1.0\text{ MHz}$)	C_{iss}	—	28	—	pF
Output Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0\text{ Vdc}$, $f = 1.0\text{ MHz}$)	C_{oss}	—	30	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0\text{ Vdc}$, $f = 1.0\text{ MHz}$)	C_{rss}	—	4.0	—	pF

FUNCTIONAL CHARACTERISTICS (2)

Common Source Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 40\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	G_{ps}	14	16	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 40\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	η	50	55	—	%
Electrical Ruggedness ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 40\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$) Load VSWR = 30:1, All phase angles at frequency of test	Ψ	No Degradation in Output Power			
Series Equivalent Input Impedance ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 40\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	Z_{in}	—	$2.88 -j7.96$	—	Ohms
Series Equivalent Output Impedance ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 40\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	Z_{out}	—	$6.12 -j9.43$	—	Ohms

(1) Each transistor chip measured separately.

(2) Both transistor chips operating in a push–pull amplifier.



C1, C2, C7, C8	220 pF, 100 mil Chip Capacitor, ATC
C3, C6	0 – 10 pF, Johanson
C4	27 pF, 100 mil Chip Capacitor, ATC
C5	22 pF, 100 mil Chip Capacitor, ATC
C9, C10, C11, C12	0.01 μ F Blue Capacitor
C13	470 pF, 100 mil Chip Capacitor, ATC
C14	50 μ F, 50 V Electrolytic Capacitor
L1, L2	8 Turns #20 AWG, 0.100 mils ID
B1, B2	6" long, ID = 550 mils, 50 Ω Semi-Rigid Coax
R1	1.0 k Ω 1/2 Watt
R2	10 k Ω 1/2 Watt
R3, R4	45 Ω 1/2 Watt
Board Material – Teflon [®] Fiberglass	
Dielectric Thickness = 0.30", ϵ_r = 2.55 Copper Clad, 2.0 oz. Copper	

Figure 1. MRF166W 500 MHz Test Circuit Schematic

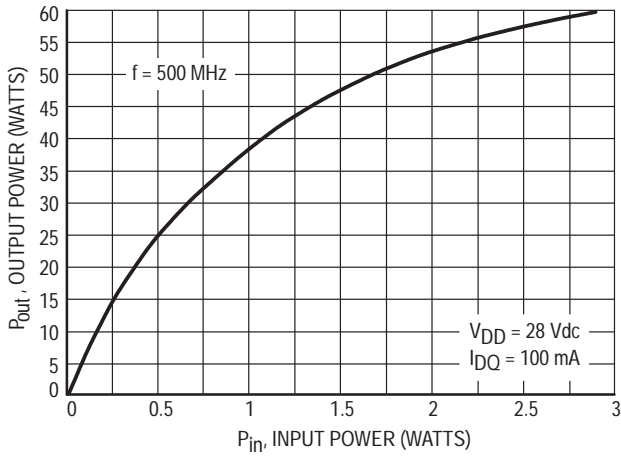


Figure 2. Output Power versus Input Power, 28 Vdc

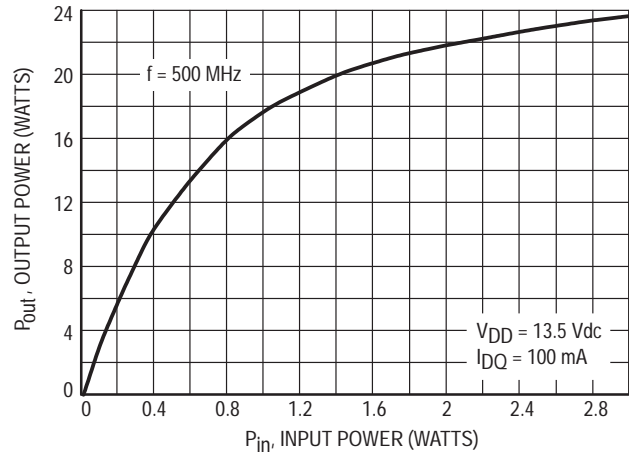


Figure 3. Output Power versus Input Power, 13.5 Vdc

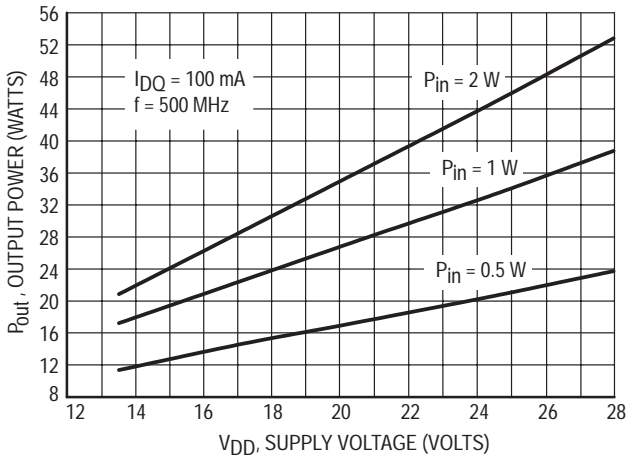


Figure 4. Output Power versus Supply Voltage

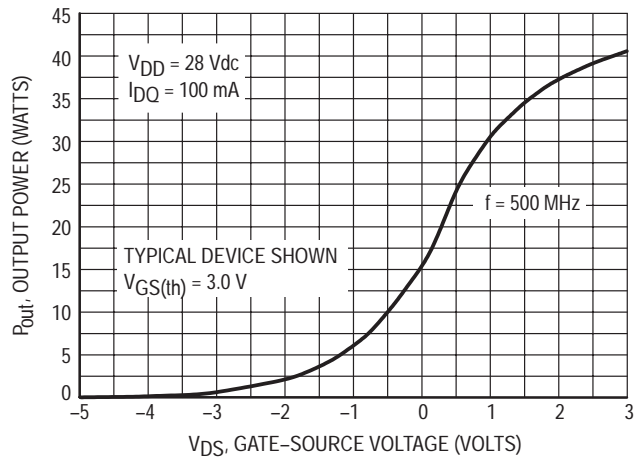


Figure 5. Output Power versus Gate Voltage

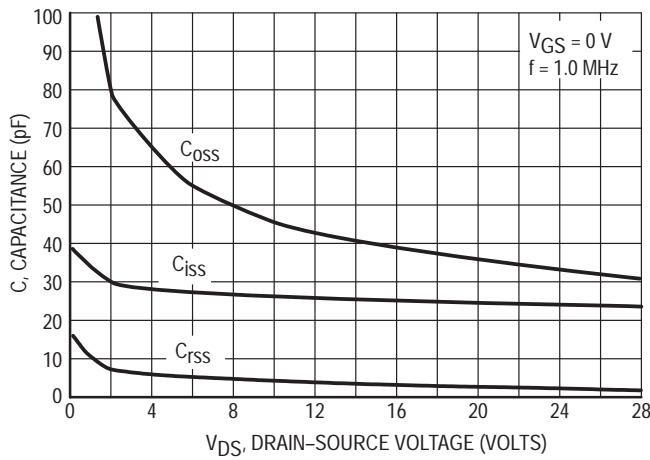
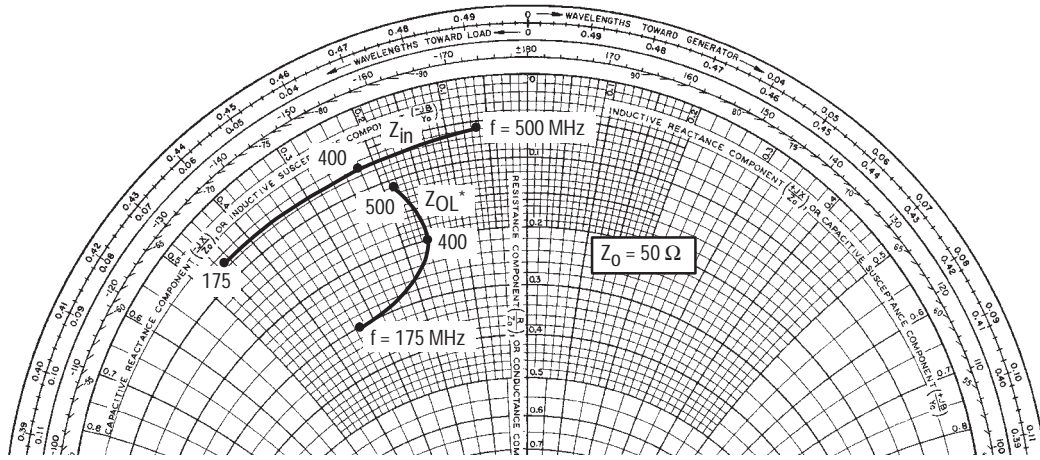


Figure 6. Capacitance versus Voltage



$V_{DD} = 28 \text{ Vdc}$, $I_{DQ} = 100 \text{ mA}$, $P_{out} = 40 \text{ W}$

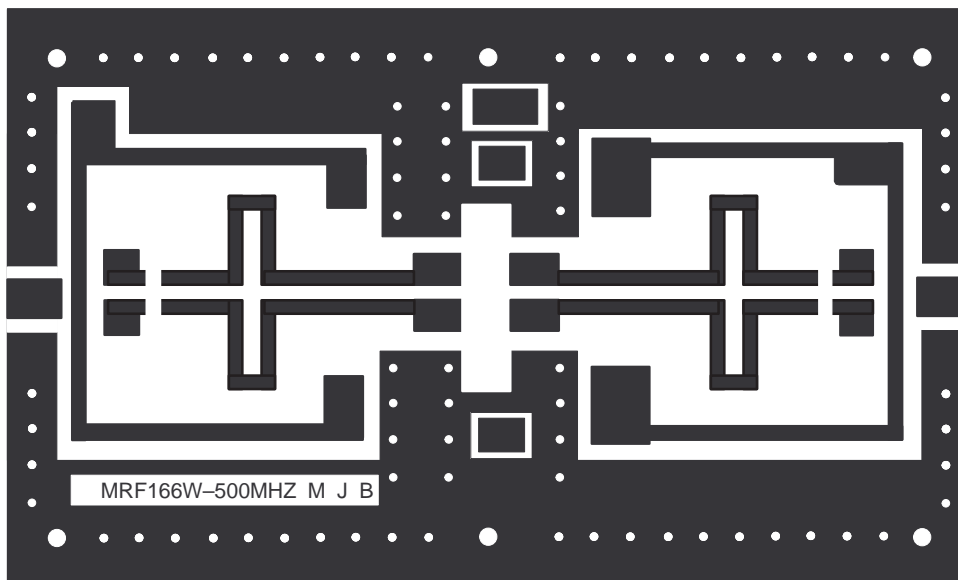
f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
175	$3.7 - j 22.4$	$15.2 - j 16.6$
400	$3.6 - j 10.99$	$10.3 - j 7.99$
500	$2.88 - j 7.96$	$6.12 - j 9.43$

Table 1. Input and Output Impedances

Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

NOTE: Input and output impedance values given are measured from gate to gate and drain to drain respectively.

Figure 7. Series Equivalent Input/Output Impedance



- NOTES: 1) 3 X 5 inch Glass Teflon[®] 32 Mil Board, Copper Both Sides
 2) Small Holes are 40 Mils ID and Plated Through
 3) Large Holes are 140 Mils ID and Plated Through

(Scale 1:1)

**Figure 8. MRF166W Circuit Board Photomaster
 (Reduced 18% in printed data book, DL110/D)**

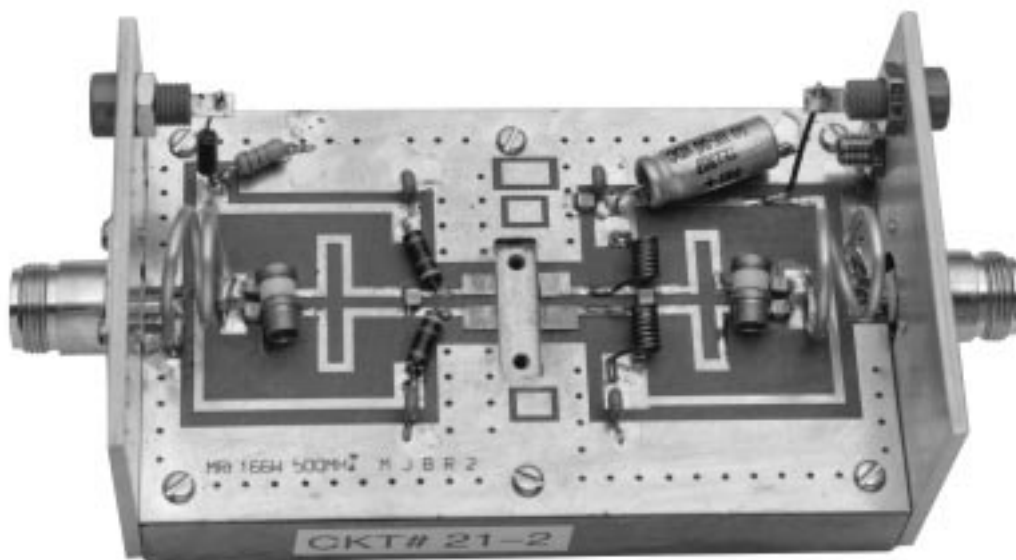


Figure 9. MRF166W Test Fixture

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 230\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.554	-85	20.30	128	0.044	28	0.628	-121
40	0.775	-113	20.00	113	0.040	26	0.632	-123
50	0.758	-124	17.50	107	0.041	20	0.652	-135
60	0.711	-132	14.60	100	0.050	20	0.570	-135
70	0.751	-139	12.70	100	0.042	11	0.666	-145
80	0.742	-143	11.30	95	0.043	9	0.666	-149
90	0.724	-146	10.00	92	0.042	8	0.657	-151
100	0.730	-149	8.97	90	0.042	6	0.663	-154
110	0.735	-151	8.29	87	0.043	3	0.683	-156
120	0.732	-153	7.53	84	0.042	2	0.666	-158
130	0.734	-155	7.01	83	0.042	1	0.688	-159
140	0.740	-156	6.57	81	0.043	0	0.701	-160
150	0.747	-157	6.01	78	0.042	-2	0.688	-162
160	0.748	-159	5.66	76	0.041	-4	0.715	-162
170	0.741	-160	5.22	76	0.040	-4	0.690	-161
180	0.746	-160	4.94	74	0.041	-4	0.719	-164
190	0.753	-161	4.67	73	0.041	-6	0.725	-165
200	0.756	-162	4.51	70	0.040	-7	0.729	-166
210	0.755	-162	4.15	69	0.039	-8	0.727	-165
220	0.759	-163	3.91	68	0.039	-8	0.724	-166
230	0.767	-163	3.75	65	0.039	-10	0.751	-169
240	0.769	-164	3.56	64	0.038	-12	0.733	-167
250	0.766	-164	3.41	63	0.037	-12	0.726	-167
260	0.767	-165	3.26	63	0.035	-10	0.725	-167
270	0.773	-165	3.07	61	0.035	-10	0.725	-167
280	0.777	-165	3.03	61	0.035	-11	0.753	-167
290	0.777	-166	2.89	58	0.034	-13	0.732	-169
300	0.782	-166	2.80	57	0.034	-11	0.744	-169
310	0.788	-166	2.66	57	0.034	-12	0.764	-169
320	0.794	-167	2.54	55	0.033	-12	0.760	-167
330	0.796	-167	2.47	54	0.032	-13	0.787	-169
340	0.795	-168	2.38	54	0.031	-13	0.753	-170
350	0.799	-168	2.27	52	0.030	-11	0.772	-168
360	0.804	-168	2.17	51	0.030	-11	0.782	-169
370	0.805	-168	2.15	50	0.030	-11	0.796	-169
380	0.807	-169	2.06	48	0.029	-12	0.782	-170
390	0.812	-169	2.00	48	0.028	-12	0.796	-170
400	0.818	-170	1.91	47	0.027	-10	0.784	-168
410	0.821	-170	1.86	46	0.029	-11	0.830	-170
420	0.821	-170	1.83	44	0.028	-11	0.823	-171
430	0.822	-171	1.74	44	0.026	-9	0.791	-170
440	0.826	-171	1.67	43	0.025	-7	0.788	-170

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 230\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
450	0.830	-171	1.68	42	0.025	-7	0.820	-170
460	0.831	-172	1.64	41	0.026	-10	0.843	-174
470	0.832	-172	1.54	41	0.025	-7	0.827	-173
480	0.835	-173	1.50	39	0.024	-3	0.836	-172
490	0.835	-173	1.43	38	0.024	1	0.835	-171
500	0.823	-174	1.43	37	0.025	3	0.849	-172
600	0.874	-176	1.12	29	0.003	-171	0.873	-176
700	0.910	-179	0.86	23	0.013	89	0.867	-177
800	0.932	179	0.74	18	0.035	61	0.904	178
900	0.966	176	0.63	12	0.029	68	0.897	179
1000	0.975	172	0.54	5	0.042	49	0.953	174

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 250\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.601	-86	22.20	128	0.040	29	0.796	-119
40	0.783	-112	21.20	114	0.037	27	0.616	-122
50	0.764	-122	18.50	108	0.038	21	0.637	-133
60	0.727	-131	15.50	101	0.045	21	0.574	-135
70	0.759	-138	13.50	100	0.039	12	0.648	-143
80	0.751	-142	12.10	95	0.040	9	0.649	-148
90	0.732	-146	10.70	93	0.040	8	0.641	-150
100	0.737	-149	9.55	90	0.040	6	0.648	-153
110	0.741	-150	8.81	88	0.040	4	0.670	-155
120	0.738	-153	8.01	85	0.040	3	0.654	-156
130	0.740	-154	7.47	83	0.040	2	0.675	-157
140	0.747	-156	7.01	82	0.040	1	0.684	-158
150	0.754	-157	6.43	79	0.040	-2	0.669	-161
160	0.757	-159	6.07	77	0.039	-3	0.693	-161
170	0.749	-159	5.59	76	0.038	-3	0.670	-161
180	0.753	-160	5.28	75	0.039	-4	0.701	-163
190	0.759	-161	4.99	73	0.039	-5	0.712	-164
200	0.761	-161	4.81	70	0.038	-7	0.719	-165
210	0.759	-162	4.44	70	0.037	-6	0.713	-163
220	0.762	-163	4.18	69	0.037	-7	0.709	-164
230	0.771	-164	4.03	66	0.037	-9	0.733	-167
240	0.775	-164	3.83	65	0.036	-10	0.715	-165
250	0.774	-165	3.69	64	0.035	-10	0.713	-166
260	0.775	-165	3.52	63	0.034	-10	0.715	-168
270	0.780	-165	3.29	61	0.034	-10	0.712	-168
280	0.782	-165	3.24	61	0.034	-11	0.741	-168
290	0.781	-166	3.10	59	0.032	-12	0.722	-168
300	0.785	-166	3.01	58	0.033	-11	0.733	-168

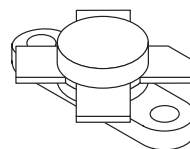
Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 250\text{ mA}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
310	0.792	-167	2.87	57	0.032	-12	0.750	-167
320	0.798	-167	2.75	56	0.032	-12	0.739	-166
330	0.801	-168	2.68	53	0.031	-13	0.760	-170
340	0.800	-168	2.58	53	0.030	-14	0.727	-172
350	0.803	-169	2.44	52	0.029	-12	0.755	-170
360	0.807	-169	2.33	50	0.029	-12	0.772	-171
370	0.808	-169	2.30	50	0.029	-12	0.787	-169
380	0.809	-169	2.19	48	0.028	-13	0.768	-170
390	0.813	-170	2.14	49	0.027	-13	0.775	-169
400	0.820	-170	2.06	47	0.026	-11	0.765	-167
410	0.823	-170	2.02	45	0.027	-12	0.805	-170
420	0.823	-171	1.98	44	0.026	-13	0.794	-173
430	0.824	-171	1.89	44	0.025	-12	0.778	-174
440	0.828	-172	1.83	43	0.024	-11	0.785	-173
450	0.832	-172	1.81	41	0.024	-10	0.812	-172
460	0.833	-172	1.75	41	0.025	-13	0.838	-175
470	0.835	-172	1.65	41	0.023	-11	0.817	-173
480	0.840	-172	1.60	40	0.022	-10	0.818	-172
490	0.844	-173	1.55	38	0.022	-10	0.819	-172
500	0.845	-173	1.56	37	0.022	-10	0.833	-173
600	0.879	-176	1.21	29	0.002	138	0.870	-176
700	0.912	-179	0.92	23	0.017	77	0.862	-176
800	0.935	179	0.79	18	0.039	58	0.887	179
900	0.966	176	0.67	11	0.030	69	0.892	179
1000	0.974	172	0.57	5	0.043	49	0.945	175

The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode MOSFET

MRF171A

45 W, 150 MHz
MOSFET BROADBAND
RF POWER FET



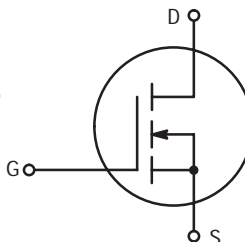
CASE 211-07, STYLE 2

Designed primarily for wideband large-signal output and driver stages from 30–200 MHz.

- Guaranteed Performance at 150 MHz, 28 Vdc
Output Power = 45 Watts
Power Gain = 17 dB (Min)
Efficiency = 60% (Min)
- Excellent Thermal Stability, Ideally Suited for Class A Operation
- Facilitates Manual Gain Control, ALC and Modulation Techniques
- 100% Tested for Load Mismatch At All Phase Angles with 30:1 VSWR
- Low Crss – 8 pF @ V_{DS} = 28 V
- Gold Top Metal

Typical Data For Power Amplifier Applications in Industrial, Commercial and Amateur Radio Equipment

- Typical Performance at 30 MHz, 28 Vdc
Output Power = 30 Watts (PEP)
Power Gain = 20 dB (Typ)
Efficiency = 50% (Typ)
IMD(d3) (30 Watts PEP) –32 dB (Typ)
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://motorola.com/sps/rf/designtds/>



MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Gate Voltage	V _{DSS}	65	Vdc
Drain-Gate Voltage (R _{GS} = 1.0 MΩ)	V _{DGR}	65	Vdc
Gate-Source Voltage	V _{GS}	±20	Adc
Drain Current — Continuous	I _D	4.5	Adc
Total Device Dissipation @ T _C = 25°C Derate above 25°C	P _D	115 0.66	Watts W/°C
Storage Temperature Range	T _{stg}	–65 to +150	°C
Operating Junction Temperature	T _J	200	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	1.52	°C/W

ELECTRICAL CHARACTERISTICS (T_C = 25°C unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain-Source Breakdown Voltage (I _D = 50 mA, V _{GS} = 0)	V _{(BR)DSS}	65	80	—	Vdc
Zero Gate Voltage Drain Current (V _{GS} = 0, V _{DS} = 28 V)	I _{DSS}	—	—	1.0	mA _{dc}
Gate-Source Leakage Current (V _{GS} = 20 V, V _{DS} = 0)	I _{GS}	—	—	1.0	μA _{dc}

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS – continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 50\text{ mA}$)	$V_{GS(th)}$	1.5	2.5	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 3\text{ A}$)	$V_{DS(on)}$	—	1.0	—	V
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 2\text{ A}$)	g_{fs}	1.4	1.8	—	mhos

DYNAMIC CHARACTERISTICS

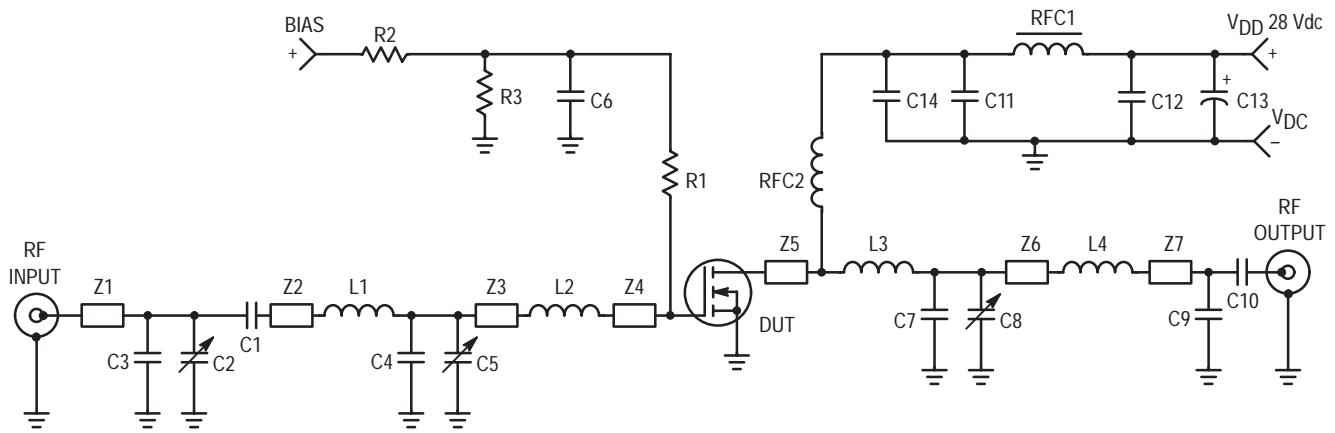
Input Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{iss}	—	60	—	pF
Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{oss}	—	70	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{rss}	—	8	—	pF

FUNCTIONAL CHARACTERISTICS

Common Source Power Gain ($V_{DD} = 28\text{ V}$, $P_{out} = 45\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 25\text{ mA}$)	G_{ps}	17	19.5	—	dB
Drain Efficiency ($V_{DD} = 28\text{ V}$, $P_{out} = 45\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 25\text{ mA}$)	η	60	70	—	%
Electrical Ruggedness ($V_{DD} = 28\text{ V}$, $P_{out} = 45\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 25\text{ mA}$, VSWR 30:1 at All Phase Angles)		No Degradation in Output Power			

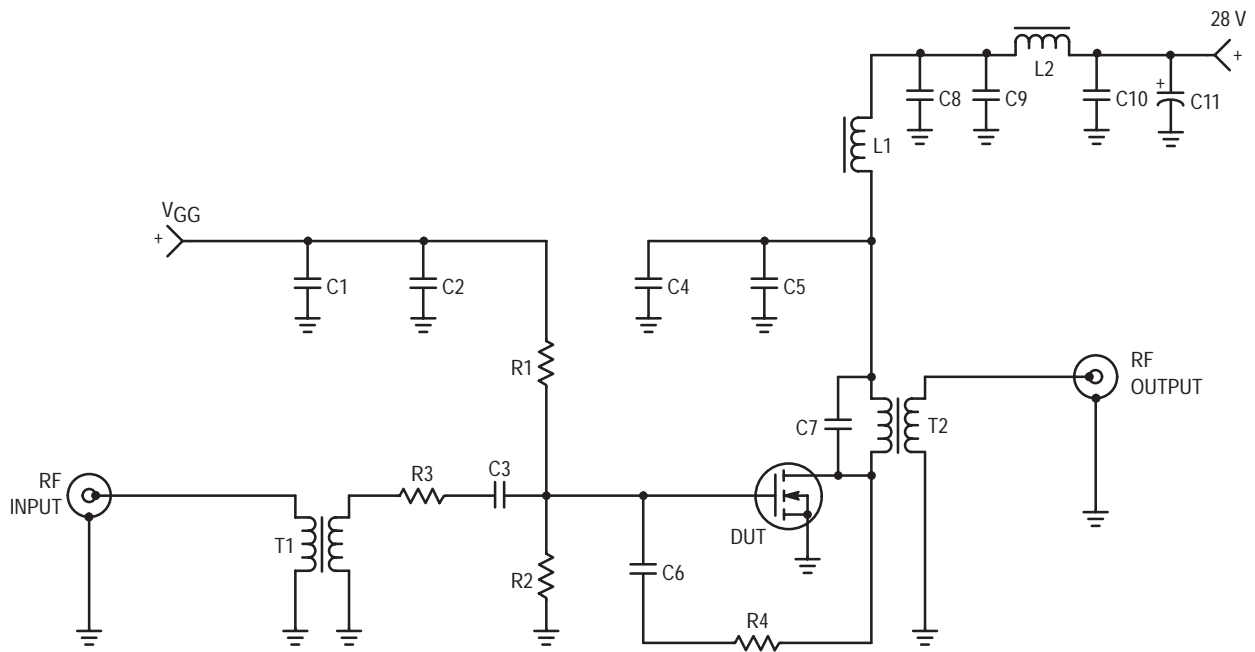
TYPICAL FUNCTIONAL TESTS (SSB)

Common Source Power Gain ($V_{DD} = 28\text{ V}$, $P_{out} = 30\text{ W (PEP)}$, $I_{DQ} = 100\text{ mA}$, $f = 30$; 30.001 MHz)	G_{ps}	—	20	—	dB
Drain Efficiency ($V_{DD} = 28\text{ V}$, $P_{out} = 30\text{ W (PEP)}$, $I_{DQ} = 100\text{ mA}$, $f = 30$; 30.001 MHz)	η	—	50	—	%
Intermodulation Distortion ($V_{DD} = 28\text{ V}$, $P_{out} = 30\text{ W (PEP)}$, $I_{DQ} = 100\text{ mA}$, $f = 30$; 30.001 MHz)	IMD(d3)	—	–32	—	dB



C1, C10	1000 pF, Chip Capacitor	R2	1 k Ω , 1/2 W Chip Resistor
C2, C5, C8	2–20 pF, Trimmer Capacitors, Johanson	R3	10 k Ω , 1/2 W Chip Resistor
C3	43 pF, 100 mil Chip Capacitor, ATC	Z1	0.160" x 0.400" Microstrip
C4	120 pF, 100 mil Chip Capacitor, ATC	Z2	0.160" x 0.600" Microstrip
C6, C14	0.1 μ F, Capacitors	Z3	0.160" x 0.600" Microstrip
C7	50 pF, 100 mil Chip Capacitor, ATC	Z4	0.160" x 0.900" Microstrip
C9	12 pF, 100 mil Chip Capacitor, ATC	Z5	0.160" x 0.800" Microstrip
C11, C12	680 pF, Feedthru Capacitors	Z6	0.160" x 0.800" Microstrip
C13	50 μ F, 50 V, Electrolytic Capacitor	Z7	0.160" x 0.400" Microstrip
L1	2 Turns, 0.297" ID, 18 AWG	RFC1	Ferroxcube VK200–19/4B
L2	1–1/2 Turns, 0.265" ID, 18 AWG	RFC2	10 Turns, 0.250" ID, 20 AWG, Enamel
L3	1–1/4 Turns, 0.234" ID, 18 AWG	Board	0.062", G10 1 oz. Copper Clad
L4	1–1/2 Turns, 0.250" ID, 18 AWG		Both Sides, $\epsilon_r = 2.56$
R1	68 Ω , 1/2 W Chip Resistor		

Figure 1. MRF171A 150 MHz Test Circuit



C1, C3, C5, C6	0.1 μ F, Chip Capacitors	L1, L2	VK200 20/4B Ferrite Choke
C2, C4	1000 pF, Chip Capacitors	R1, R2	200 Ω , 1/2 W Carbon
C7	68 pF, Dipped Mica	R3	3 Ω , 1/2 W Carbon
C8	0.1 μ F, Ceramic Cap or Equivalent	R4	270 Ω , 2 W Carbon
C9, C10	680 pF, Feedthru Capacitors	T1	4:1 Impedance Broadband Transformer
C11	250 μ F, 50 V, Electrolytic Capacitor	T2	1:4 Impedance Broadband Transformer

Figure 2. MRF171A 30 MHz Test Circuit

TYPICAL CHARACTERISTICS

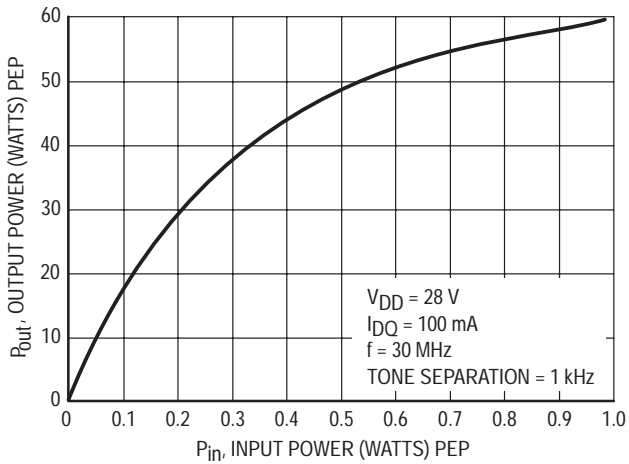


Figure 3. Output Power versus Input Power

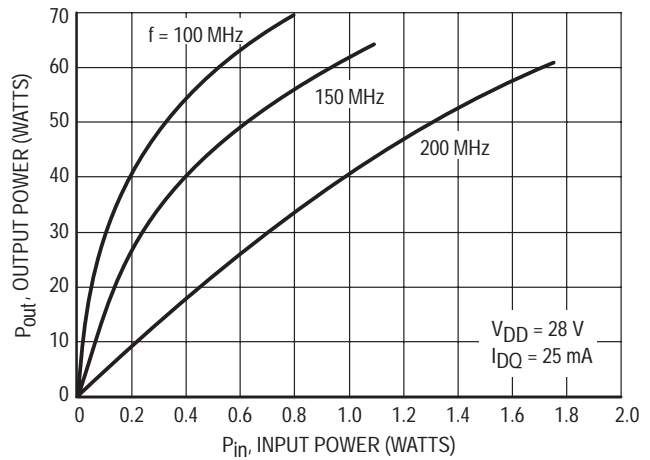


Figure 4. Output Power versus Input Power

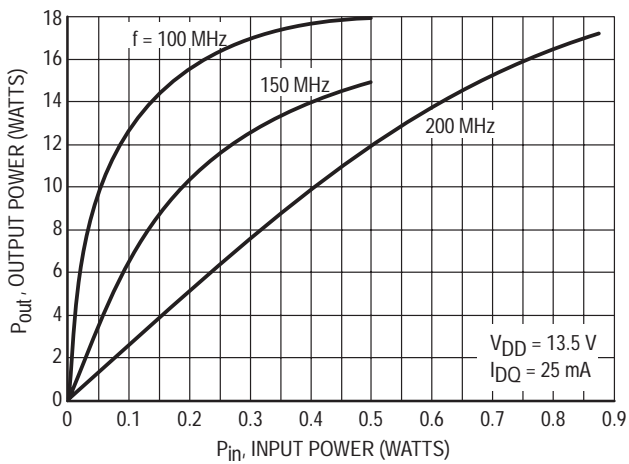


Figure 5. Output Power versus Input Power

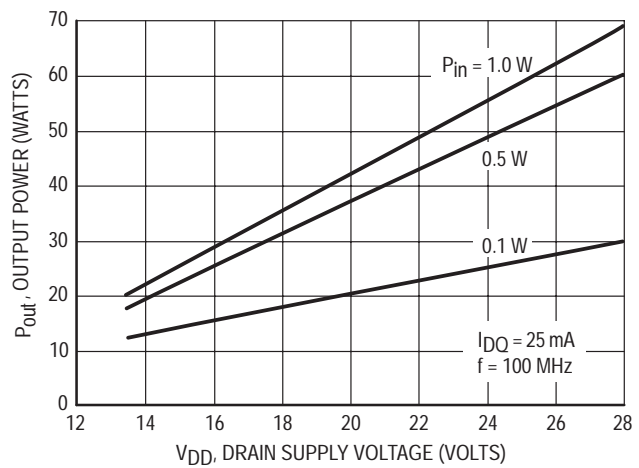


Figure 6. Output Power versus Supply Voltage

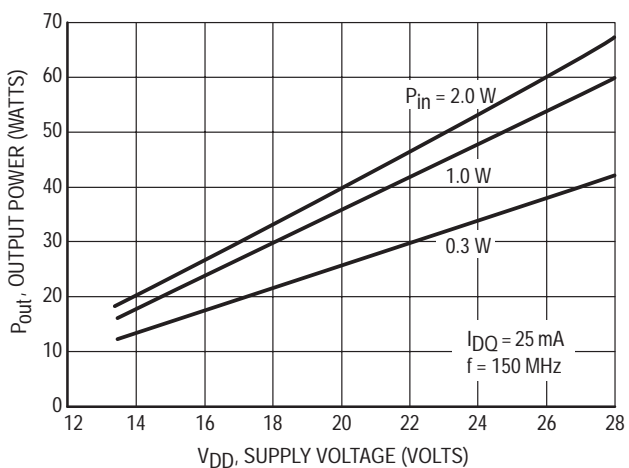


Figure 7. Output Power versus Supply Voltage

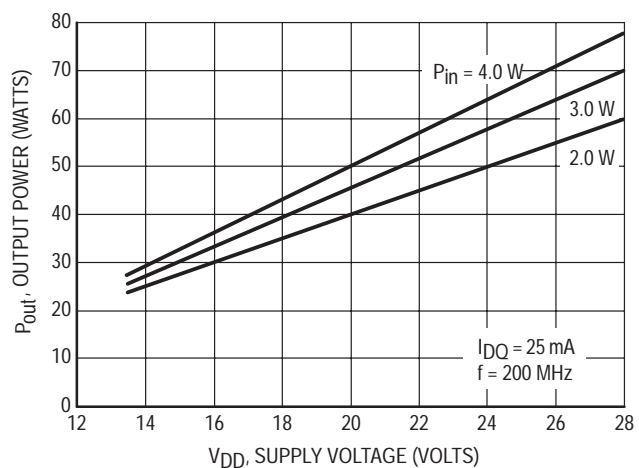


Figure 8. Output Power versus Supply Voltage

TYPICAL CHARACTERISTICS

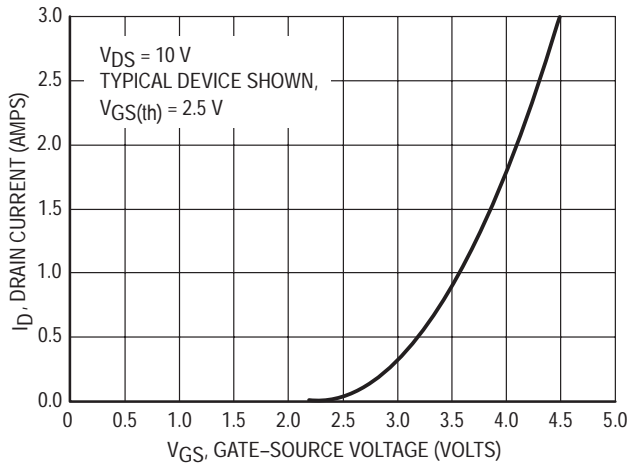


Figure 9. Drain Current versus Gate Voltage (Transfer Characteristics)

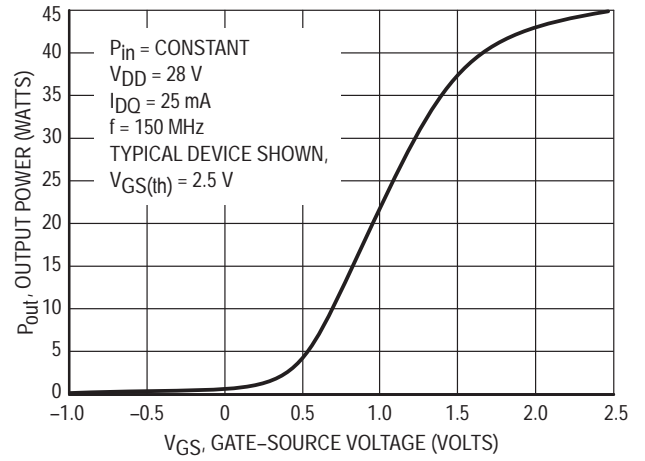


Figure 10. Output Power versus Gate Voltage

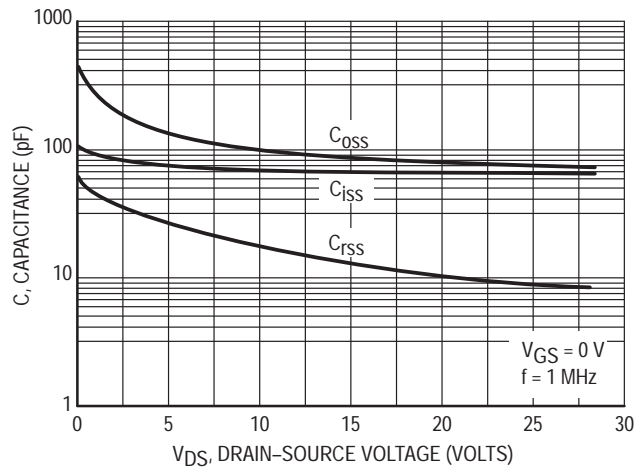
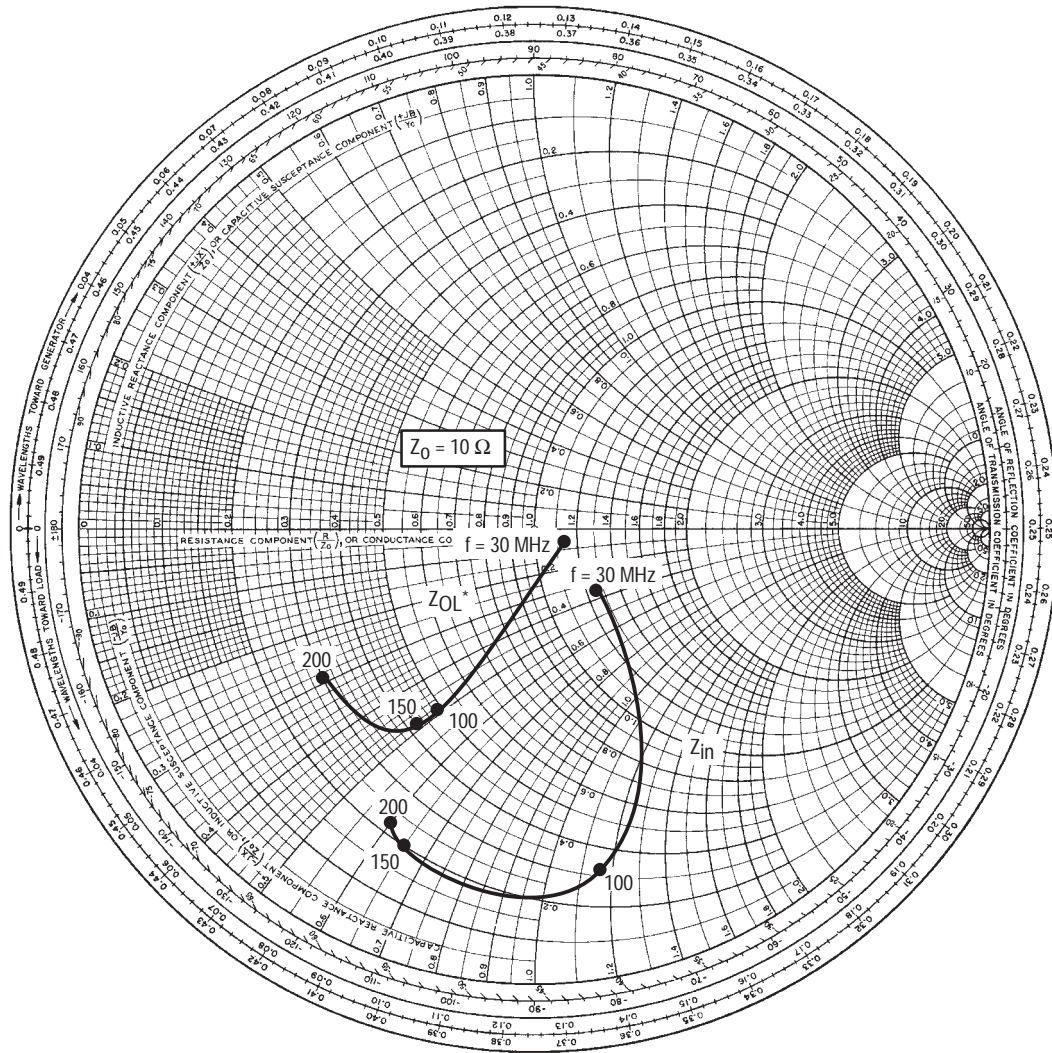


Figure 11. Capacitance versus Drain-Source Voltage



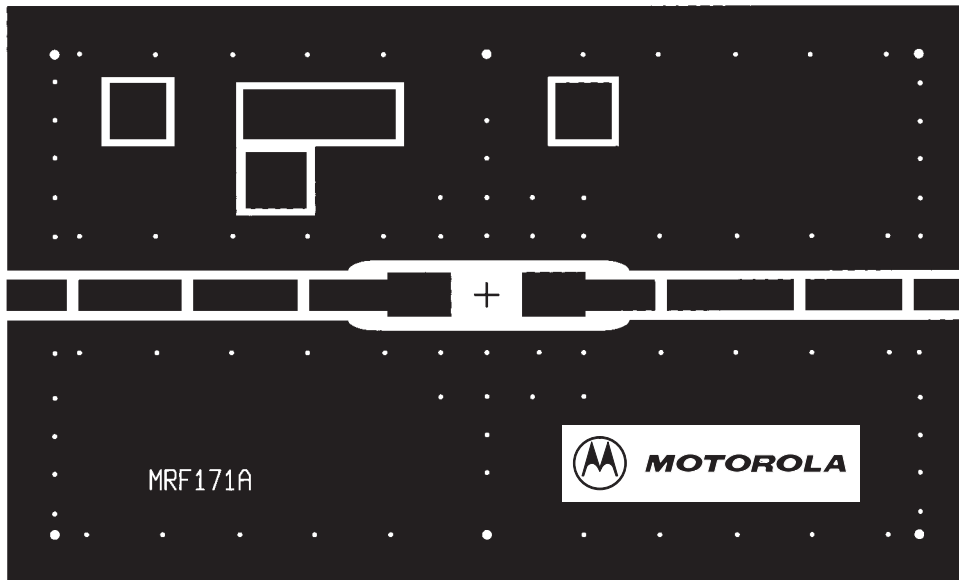
$V_{DD} = 28 \text{ V}$, $I_{DQ} = 25 \text{ mA}$, $P_{out} = 45 \text{ W}$

f MHz	$Z_{in}(1)$ Ω	$Z_{OL}(2)$ Ω
30	$12.8 - j3.6$	$11.5 - j0.99$
100	$3.1 - j11.6$	$4.9 - j4.9$
150	$2.0 - j6.5$	$4.2 - j4.9$
200	$2.2 - j6.0$	$3.0 - j2.9$

(1) 68 Ω shunt resistor gate-to-ground.

(2) Z_{OL} =Conjugate of the optimum load impedance into which the device operates at a given output power, voltage and frequency.

Figure 12. Large-Signal Series Equivalent Input/Output Impedance



(Scale 1:1)

Figure 13. MRF171A Circuit Board Photo Master
(Reduced 18% in printed data book, DL110/D)

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 0.5\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.801	-162	11.90	96	0.026	13	0.811	-166
40	0.809	-166	9.12	91	0.028	11	0.812	-171
50	0.810	-169	7.29	88	0.027	11	0.831	-172
60	0.808	-170	6.22	85	0.028	9	0.824	-174
70	0.814	-172	5.30	82	0.028	9	0.831	-176
80	0.811	-173	4.56	81	0.027	10	0.837	-175
90	0.811	-174	4.04	80	0.027	13	0.829	-174
100	0.814	-174	3.66	77	0.027	12	0.846	-176
110	0.812	-175	3.37	75	0.027	11	0.842	-177
120	0.816	-175	3.00	74	0.027	13	0.850	-176
130	0.816	-176	2.75	73	0.027	14	0.849	-175
140	0.817	-176	2.57	72	0.027	17	0.851	-176
150	0.821	-176	2.37	69	0.027	17	0.863	-177
160	0.820	-176	2.27	67	0.027	17	0.853	-177
170	0.821	-177	2.08	66	0.026	19	0.838	-177
180	0.824	-177	1.93	65	0.027	19	0.861	-177
190	0.825	-177	1.89	64	0.027	21	0.873	-177
200	0.830	-177	1.74	62	0.027	23	0.873	-178
210	0.831	-177	1.67	60	0.027	25	0.874	-177
220	0.831	-178	1.62	59	0.026	28	0.870	-178
230	0.836	-178	1.48	57	0.027	27	0.909	-179
240	0.836	-178	1.43	56	0.027	26	0.865	-180
250	0.839	-178	1.37	57	0.028	30	0.873	-178
260	0.844	-178	1.30	54	0.028	34	0.882	-179
270	0.842	-178	1.28	52	0.028	36	0.887	-180
280	0.845	-179	1.21	52	0.027	37	0.881	-180
290	0.849	-179	1.14	50	0.027	36	0.869	179
300	0.849	-179	1.12	50	0.029	39	0.852	-180
310	0.855	-179	1.06	49	0.029	42	0.891	-179
320	0.856	-179	1.03	46	0.030	43	0.889	180
330	0.856	-180	0.96	45	0.031	47	0.868	180
340	0.858	-180	0.96	46	0.030	47	0.888	179
350	0.860	180	0.93	44	0.031	49	0.875	-180
360	0.862	180	0.91	44	0.033	48	0.901	179
370	0.866	180	0.86	43	0.034	50	0.913	178
380	0.867	179	0.84	41	0.036	52	0.897	178
390	0.869	179	0.82	42	0.035	54	0.893	178
400	0.870	179	0.78	40	0.035	57	0.880	180
410	0.872	179	0.77	39	0.037	55	0.923	178
420	0.876	178	0.73	37	0.039	54	0.915	176
430	0.877	178	0.69	38	0.040	56	0.903	177
440	0.879	178	0.68	39	0.041	58	0.921	178

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 0.5\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
450	0.882	177	0.68	36	0.040	61	0.926	178
460	0.884	177	0.65	36	0.041	59	0.937	175
470	0.886	177	0.62	35	0.041	60	0.896	176
480	0.885	176	0.62	33	0.044	61	0.907	176
490	0.886	176	0.61	32	0.046	63	0.907	176
500	0.887	176	0.59	31	0.047	65	0.916	175

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.5\text{ A}$)

f MHz	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.783	-152	17.10	100	0.025	17	0.730	-158
40	0.793	-158	13.20	94	0.027	13	0.730	-164
50	0.793	-162	10.50	90	0.027	12	0.754	-167
60	0.791	-165	9.00	87	0.027	11	0.746	-169
70	0.798	-167	7.68	83	0.026	10	0.760	-171
80	0.795	-169	6.63	82	0.026	10	0.770	-170
90	0.795	-170	5.85	80	0.026	12	0.760	-170
100	0.799	-170	5.30	77	0.026	10	0.779	-172
110	0.798	-171	4.86	75	0.026	11	0.775	-174
120	0.802	-172	4.35	74	0.025	13	0.785	-172
130	0.801	-172	3.97	72	0.025	14	0.788	-171
140	0.803	-173	3.70	71	0.025	15	0.791	-172
150	0.809	-173	3.42	68	0.025	14	0.808	-173
160	0.808	-173	3.27	66	0.025	15	0.796	-172
170	0.809	-174	2.99	65	0.024	18	0.783	-174
180	0.814	-174	2.77	63	0.025	19	0.809	-173
190	0.815	-175	2.71	62	0.024	21	0.820	-174
200	0.822	-175	2.49	60	0.024	22	0.826	-175
210	0.824	-175	2.37	57	0.024	24	0.836	-175
220	0.825	-175	2.23	57	0.024	26	0.807	-175
230	0.831	-176	2.08	56	0.024	29	0.839	-175
240	0.830	-176	2.00	54	0.024	29	0.818	-176
250	0.832	-176	1.92	55	0.024	33	0.828	-174
260	0.838	-176	1.81	53	0.024	35	0.829	-175
270	0.837	-176	1.79	50	0.025	37	0.834	-175
280	0.840	-177	1.69	50	0.025	39	0.832	-176
290	0.844	-177	1.60	48	0.025	39	0.836	-177
300	0.844	-177	1.55	48	0.025	44	0.814	-175
310	0.849	-178	1.48	47	0.026	46	0.848	-175
320	0.852	-178	1.43	44	0.027	45	0.855	-177
330	0.852	-178	1.35	43	0.028	48	0.833	-177
340	0.855	-178	1.32	44	0.028	49	0.861	-177
350	0.856	-178	1.29	41	0.029	53	0.842	-176

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.5\text{ A}$) (continued)

f MHz	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
360	0.859	-179	1.25	42	0.030	54	0.872	-178
370	0.863	-179	1.18	39	0.030	55	0.886	-178
380	0.864	-179	1.15	38	0.031	55	0.864	-178
390	0.867	-179	1.12	39	0.032	57	0.862	-179
400	0.869	-180	1.07	37	0.032	60	0.853	-177
410	0.872	-180	1.05	35	0.035	60	0.898	-179
420	0.876	180	1.00	34	0.036	60	0.889	180
430	0.877	179	0.95	35	0.037	62	0.884	-179
440	0.879	179	0.93	34	0.038	64	0.902	-179
450	0.882	179	0.91	32	0.039	65	0.901	-180
460	0.884	178	0.88	32	0.041	64	0.922	179
470	0.885	178	0.84	32	0.040	66	0.877	179
480	0.885	178	0.83	30	0.042	66	0.892	179
490	0.886	177	0.81	29	0.044	68	0.891	179
500	0.887	177	0.80	28	0.045	68	0.900	178

The RF MOSFET Line
RF Power
Field Effect Transistor
N-Channel Enhancement Mode MOSFET

MRF173

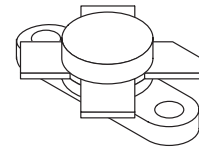
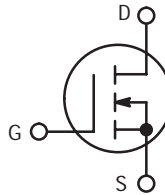
80 W, 28 V, 175 MHz
N-CHANNEL
BROADBAND
RF POWER MOSFET

Designed for broadband commercial and military applications up to 200 MHz frequency range. The high-power, high-gain and broadband performance of this device make possible solid state transmitters for FM broadcast or TV channel frequency bands.

- Guaranteed Performance at 150 MHz, 28 V:

Output Power = 80 W
Gain = 11 dB (13 dB Typ)
Efficiency = 55% Min. (60% Typ)

- Low Thermal Resistance
- Ruggedness Tested at Rated Output Power
- Nitride Passivated Die for Enhanced Reliability
- Low Noise Figure — 1.5 dB Typ at 2.0 A, 150 MHz
- Excellent Thermal Stability; Suited for Class A Operation
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://motorola.com/sps/rf/designnlds/>



CASE 211-11, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage	V_{DGO}	65	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	9.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	220 1.26	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Temperature Range	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.8	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{DS} = 0\text{ V}$, $V_{GS} = 0\text{ V}$) $I_D = 50\text{ mA}$	$V_{(BR)DSS}$	65	—	—	V
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	—	—	2.0	mA
Gate-Source Leakage Current ($V_{GS} = 40\text{ V}$, $V_{DS} = 0\text{ V}$)	I_{GSS}	—	—	1.0	μA

ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 50\text{ mA}$)	$V_{GS(th)}$	1.0	3.0	6.0	V
Drain-Source On-Voltage ($V_{DS(on)}$, $V_{GS} = 10\text{ V}$, $I_D = 3.0\text{ A}$)	$V_{DS(on)}$	—	—	1.4	V
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 2.0\text{ A}$)	g_{fs}	1.8	2.2	—	mhos

(continued)

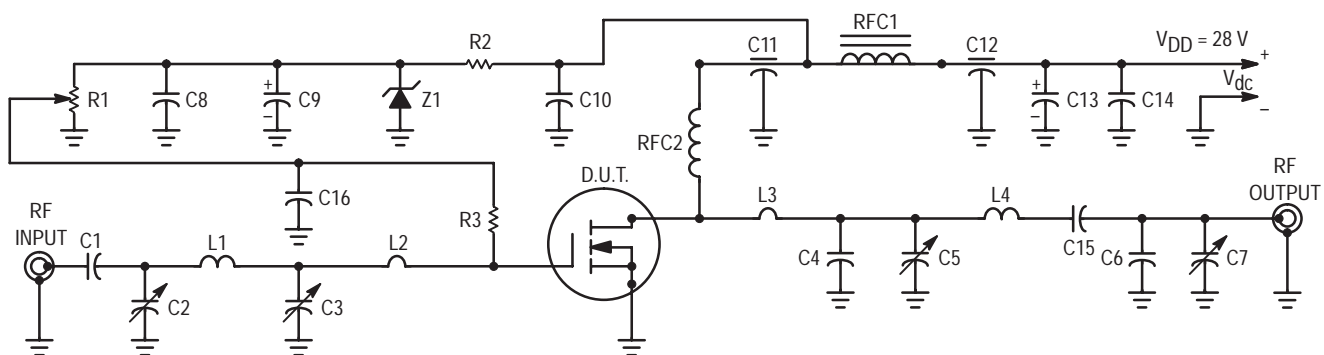
NOTE — **CAUTION** — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
DYNAMIC CHARACTERISTICS					
Input Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{iss}	—	110	—	pF
Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{oss}	—	105	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{rss}	—	10	—	pF

FUNCTIONAL CHARACTERISTICS

Noise Figure ($V_{DD} = 28\text{ V}$, $f = 150\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	NF	—	1.5	—	dB
Common Source Power Gain ($V_{DD} = 28\text{ V}$, $P_{out} = 80\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	G_{ps}	11	13	—	dB
Drain Efficiency ($V_{DD} = 28\text{ V}$, $P_{out} = 80\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	η	55	60	—	%
Electrical Ruggedness ($V_{DD} = 28\text{ V}$, $P_{out} = 80\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 50\text{ mA}$) Load VSWR 30:1 at all phase angles	ψ	No Degradation in Output Power			
Series Equivalent Input Impedance ($V_{DD} = 28\text{ V}$, $P_{out} = 80\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	Z_{in}	—	$2.99-j4.5$	—	Ohms
Series Equivalent Output Impedance ($V_{DD} = 28\text{ V}$, $P_{out} = 80\text{ W}$, $f = 150\text{ MHz}$, $I_{DQ} = 50\text{ mA}$)	Z_{out}	—	$2.68-j1.3$	—	Ohms



- | | |
|---------------------------------------|---|
| C1, C15 — 470 pF Unelco | L3 — #14 AWG Hairpin 0.8" long |
| C2, C3, C5 — 9–180 pF, Arco 463 | L4 — #14 AWG Hairpin 1.1" long |
| C4, C6 — 15 pF, Unelco | RFC1 — Ferroxcube VK200–19/4B |
| C7 — 5–80 pF, Arco 462 | RFC2 — 18 Turns #18 AWG Enameled, 0.3" ID |
| C8, C10, C14, C16 — 0.1 μF | R1 — 10 k Ω , 10 Turns Bourns |
| C9, C13 — 50 μF , 50 Vdc | R2 — 1.8 k Ω , 1/4 W |
| C11, C12 — 680 pF, Feed Through | R3 — 10 k Ω , 1/2 W |
| L1 — #16 AWG, 1–1/4 Turns, 0.3" ID | Z1 — 1N5925A Motorola Zener |
| L2 — #16 AWG Hairpin 1" long | |

Figure 1. 150 MHz Test Circuit

TYPICAL CHARACTERISTICS

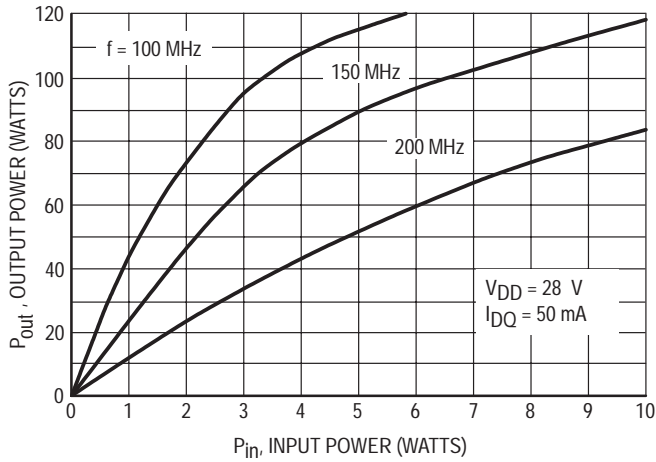


Figure 2. Output Power versus Input Power

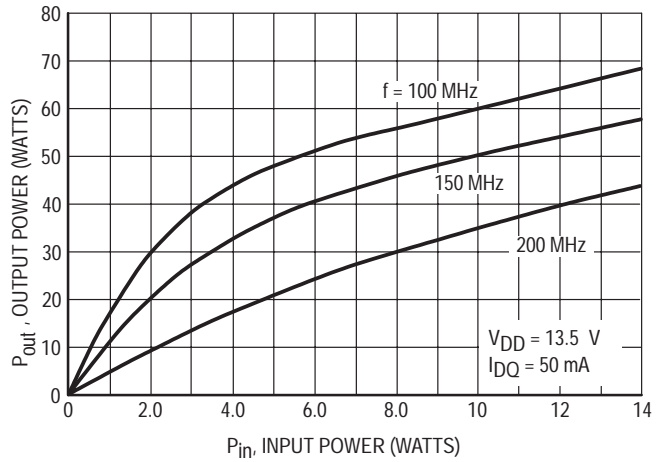


Figure 3. Output Power versus Input Power

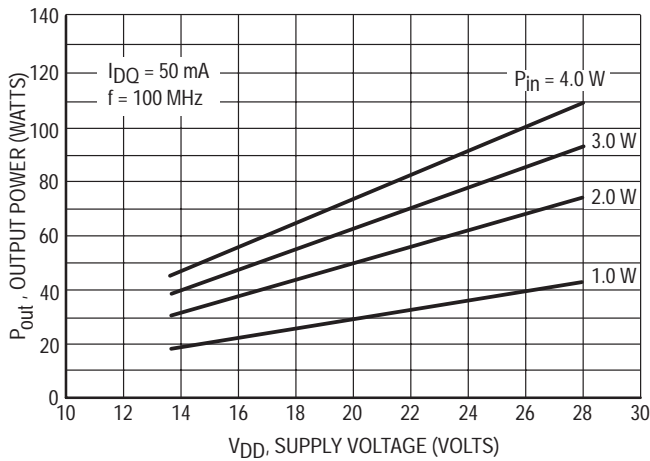


Figure 4. Output Power versus Supply Voltage

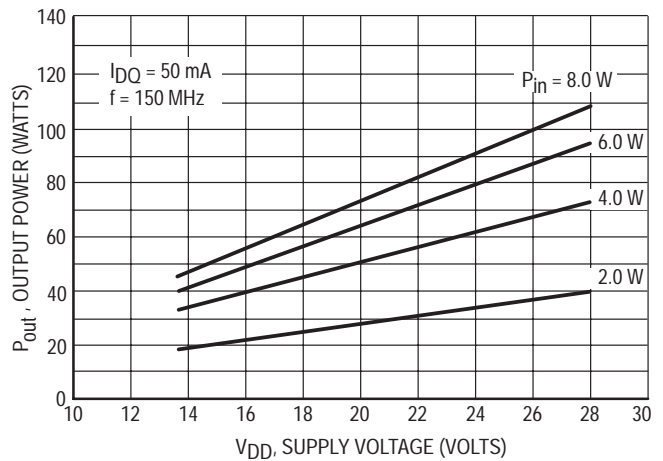


Figure 5. Output Power versus Supply Voltage

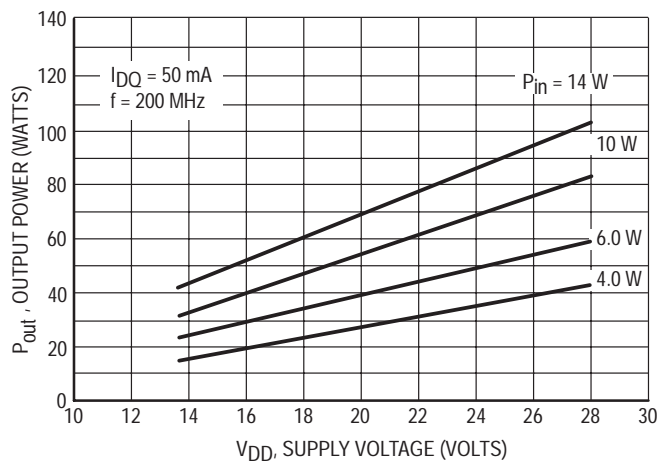


Figure 6. Output Power versus Supply Voltage

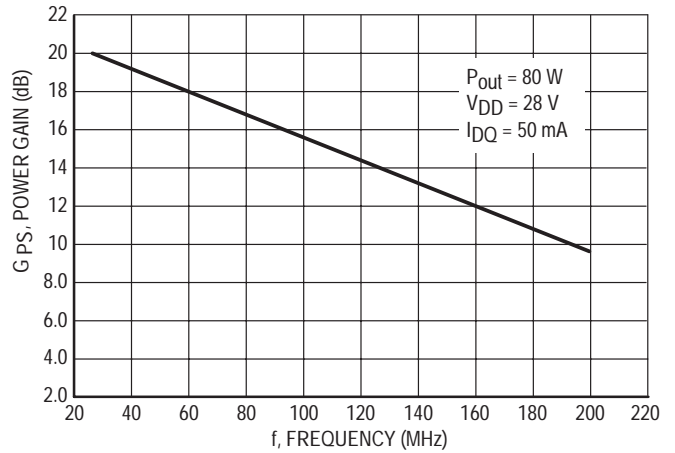


Figure 7. Power Gain versus Frequency

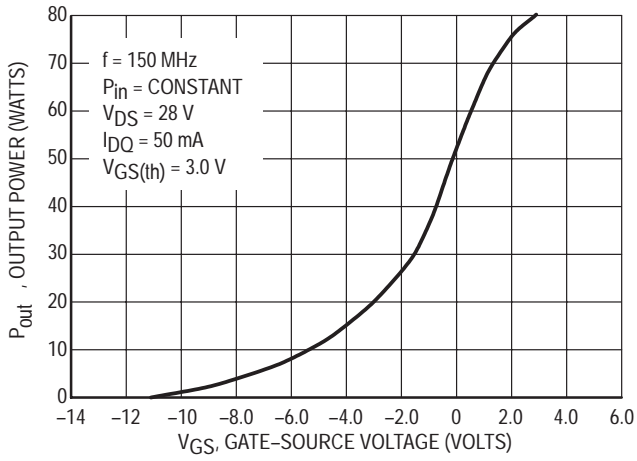


Figure 8. Output Power versus Gate Voltage

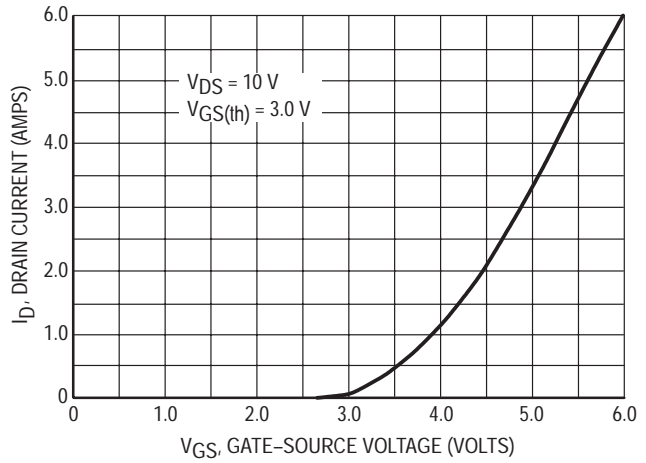


Figure 9. Drain Current versus Gate Voltage

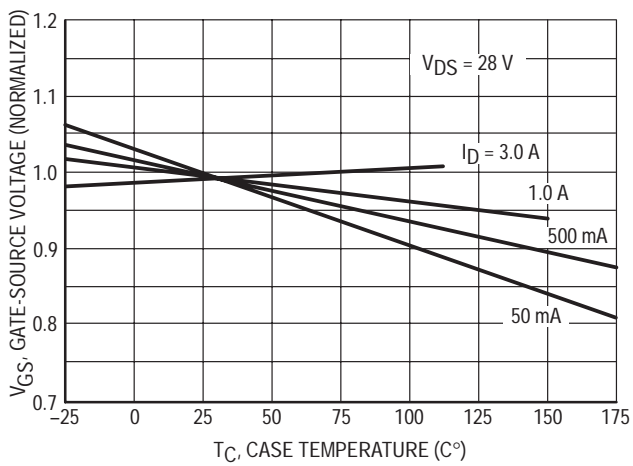


Figure 10. Gate-Source Voltage versus Case Temperature

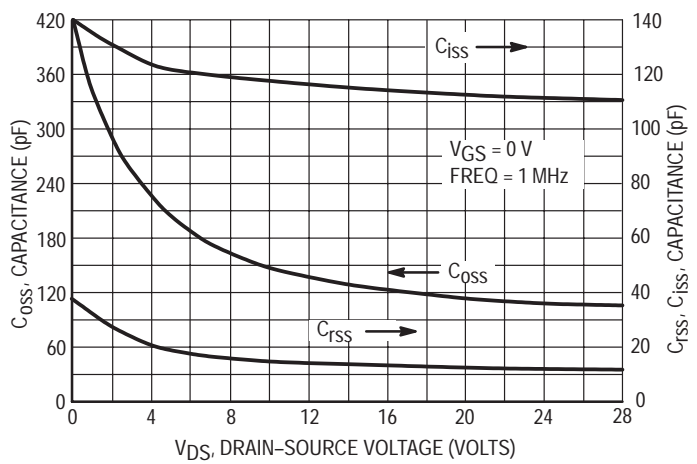


Figure 11. Capacitance versus Drain Voltage

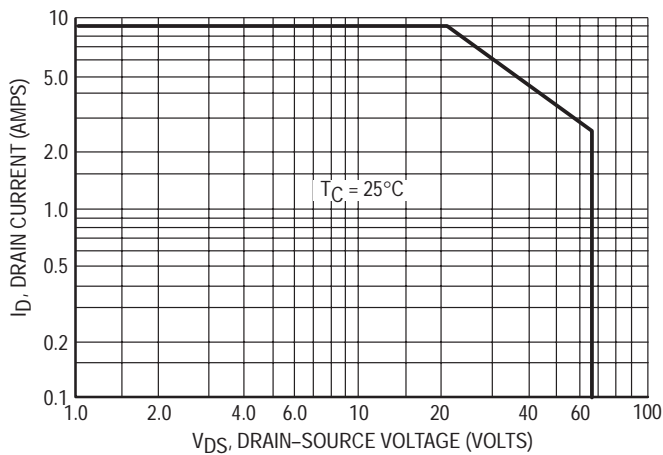


Figure 12. DC Safe Operating Area

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 4\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.879	-170	8.09	92	0.014	23	0.839	-174
40	0.883	-173	6.19	87	0.016	24	0.839	-179
50	0.885	-174	4.94	84	0.016	28	0.853	-178
60	0.885	-175	4.21	81	0.017	30	0.845	180
70	0.888	-176	3.57	77	0.017	34	0.849	179
80	0.888	-177	3.06	77	0.017	37	0.852	-179
90	0.888	-178	2.71	76	0.018	42	0.842	-179
100	0.890	-178	2.45	72	0.019	43	0.858	180
110	0.888	-179	2.28	70	0.020	46	0.859	179
120	0.892	-179	2.02	69	0.021	50	0.872	-180
130	0.893	-179	1.84	67	0.022	52	0.870	-179
140	0.894	-180	1.73	66	0.023	55	0.880	-180
150	0.896	-180	1.58	64	0.024	55	0.887	180
160	0.896	180	1.51	61	0.026	56	0.863	180
170	0.898	179	1.38	60	0.026	60	0.850	179
180	0.899	179	1.28	58	0.028	60	0.871	179
190	0.899	179	1.25	57	0.030	62	0.890	178
200	0.902	179	1.15	55	0.030	63	0.884	178
210	0.902	179	1.12	53	0.032	63	0.899	178
220	0.904	178	1.08	51	0.034	65	0.893	178
230	0.907	178	0.97	49	0.037	65	0.941	176
240	0.907	178	0.95	48	0.037	65	0.884	176
250	0.909	178	0.90	49	0.039	67	0.896	177
260	0.911	177	0.85	48	0.039	68	0.888	176
270	0.909	177	0.83	46	0.042	68	0.895	176
280	0.913	177	0.78	45	0.044	69	0.893	175
290	0.914	177	0.74	42	0.044	69	0.882	174
300	0.915	176	0.74	42	0.047	72	0.877	175
310	0.917	176	0.70	41	0.048	73	0.909	176
320	0.916	176	0.69	39	0.052	71	0.912	175
330	0.917	176	0.65	37	0.055	71	0.885	173
340	0.919	176	0.65	38	0.055	70	0.898	173
350	0.919	175	0.62	36	0.057	72	0.887	174
360	0.920	175	0.60	37	0.059	72	0.918	172
370	0.921	175	0.57	35	0.061	71	0.929	172
380	0.923	175	0.56	34	0.063	71	0.900	172
390	0.925	175	0.54	36	0.065	71	0.907	171
400	0.926	174	0.51	34	0.067	75	0.902	173
410	0.927	174	0.51	33	0.070	73	0.942	170
420	0.929	174	0.49	31	0.071	71	0.926	169
430	0.929	173	0.46	32	0.072	72	0.901	170
440	0.930	173	0.45	32	0.076	73	0.904	170

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 4\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
450	0.932	173	0.45	29	0.079	75	0.924	170
460	0.932	172	0.44	30	0.082	71	0.938	167
470	0.933	172	0.42	30	0.081	73	0.908	168
480	0.931	172	0.42	29	0.086	72	0.933	168
490	0.931	171	0.41	28	0.089	72	0.926	167
500	0.931	171	0.41	27	0.092	71	0.936	167

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 4\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.840	-163	11.48	92	0.016	20	0.718	-169
40	0.849	-167	8.80	86	0.017	22	0.713	-174
50	0.853	-170	6.99	82	0.017	24	0.748	-174
60	0.854	-171	5.92	79	0.017	23	0.746	-175
70	0.859	-172	5.00	74	0.018	25	0.746	-175
80	0.859	-174	4.29	73	0.018	30	0.741	-174
90	0.861	-174	3.77	71	0.019	38	0.735	-174
100	0.866	-175	3.39	67	0.018	40	0.768	-176
110	0.865	-175	3.12	64	0.018	41	0.782	-177
120	0.871	-176	2.75	63	0.019	42	0.794	-175
130	0.875	-176	2.49	60	0.021	45	0.783	-172
140	0.877	-177	2.31	59	0.023	51	0.776	-175
150	0.883	-177	2.10	56	0.023	55	0.806	-176
160	0.884	-177	1.99	53	0.023	58	0.807	-176
170	0.886	-178	1.82	51	0.023	61	0.806	-176
180	0.890	-178	1.66	49	0.025	59	0.820	-175
190	0.891	-179	1.62	48	0.027	60	0.815	-176
200	0.896	-179	1.47	46	0.030	63	0.819	-177
210	0.898	-179	1.41	43	0.031	67	0.842	-178
220	0.901	-179	1.36	41	0.032	70	0.855	-178
230	0.905	-180	1.22	38	0.033	70	0.906	-178
240	0.906	-180	1.19	38	0.034	67	0.845	-178
250	0.909	180	1.11	39	0.037	68	0.831	-178
260	0.913	180	1.03	37	0.038	70	0.837	-180
270	0.912	179	0.10	35	0.041	72	0.859	179
280	0.916	179	0.93	34	0.042	74	0.876	178
290	0.918	179	0.88	31	0.041	73	0.865	179
300	0.919	178	0.87	31	0.044	74	0.837	-180
310	0.922	178	0.83	31	0.046	74	0.863	180
320	0.922	178	0.80	27	0.051	73	0.879	177
330	0.924	177	0.75	26	0.054	74	0.878	176
340	0.926	177	0.74	27	0.053	74	0.897	177
350	0.926	177	0.71	24	0.054	77	0.879	179

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 4\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
360	0.927	177	0.68	26	0.056	75	0.888	177
370	0.929	177	0.64	24	0.058	73	0.893	175
380	0.931	176	0.62	23	0.062	72	0.885	174
390	0.934	176	0.60	25	0.064	74	0.903	174
400	0.934	176	0.57	22	0.065	78	0.898	177
410	0.936	175	0.56	21	0.068	77	0.931	175
420	0.938	175	0.53	20	0.070	74	0.906	173
430	0.938	174	0.51	21	0.072	73	0.885	173
440	0.939	174	0.49	21	0.075	75	0.895	172
450	0.941	174	0.48	19	0.080	78	0.923	172
460	0.941	173	0.47	19	0.082	75	0.940	171
470	0.942	173	0.45	18	0.080	75	0.904	172
480	0.940	173	0.44	18	0.083	74	0.910	171
490	0.940	172	0.43	18	0.088	72	0.906	169
500	0.940	172	0.42	17	0.092	72	0.927	168

DESIGN CONSIDERATIONS

The MRF173 is a RF MOSFET power N-channel enhancement mode field-effect transistor (FET) designed for VHF power amplifier applications. Motorola's RF MOSFETs feature a vertical structure with a planar design, thus avoiding the processing difficulties associated with V-groove power FETs.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power FETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal, thus facilitating manual gain control, ALC and modulation.

DC BIAS

The MRF173 is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. See Figure 9 for a typical plot of drain current versus gate voltage. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The

MRF173 was characterized at $I_{DQ} = 50\text{ mA}$, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of the MRF173 may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems. (see Figure 8.)

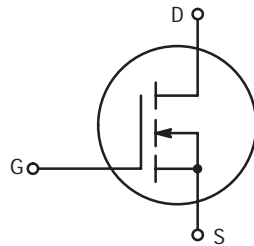
AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar VHF transistors are suitable for MRF173. See Motorola Application Note AN721, Impedance Matching Networks Applied to RF Power Transistors. The higher input impedance of RF MOSFETs helps ease the task of broadband network design. Both small-signal scattering parameters and large-signal impedances are provided. While the s-parameters will not produce an exact design solution for high power operation, they do yield a good first approximation. This is an additional advantage of RF MOS power FETs.

The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode

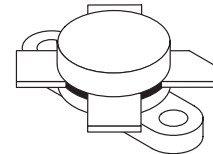
. . . designed primarily for wideband large-signal output and driver stages up to 200 MHz frequency range.

- Guaranteed Performance at 150 MHz, 28 Vdc
Output Power = 125 Watts
Minimum Gain = 9.0 dB
Efficiency = 50% (Min)
- Excellent Thermal Stability, Ideally Suited For Class A Operation
- Facilitates Manual Gain Control, ALC and Modulation Techniques
- 100% Tested For Load Mismatch At All Phase Angles With 30:1 VSWR
- Low Noise Figure — 3.0 dB Typ at 2.0 A, 150 MHz



MRF174

**125 W, to 200 MHz
N-CHANNEL MOS
BROADBAND RF POWER
FET**



CASE 211-11, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1.0 \text{ M}\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	13	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	270 1.54	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.65	$^\circ\text{C/W}$

Handling and Packaging — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 50 \text{ mA}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	10	mAdc
Gate–Source Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS

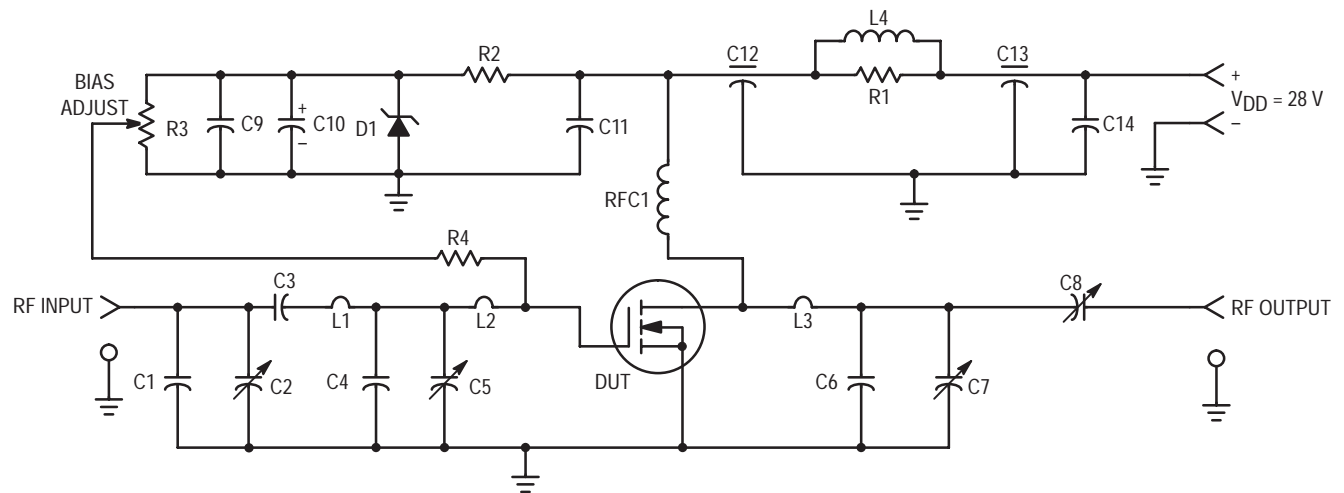
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 100 \text{ mA}$)	$V_{GS(th)}$	1.0	3.0	6.0	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 3.0 \text{ A}$)	g_{fs}	1.75	2.5	—	mhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{iss}	—	175	—	pF
Output Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{oss}	—	190	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{rss}	—	40	—	pF

FUNCTIONAL CHARACTERISTICS (Figure 1)

Noise Figure ($V_{DD} = 28 \text{ Vdc}, I_D = 2.0 \text{ A}, f = 150 \text{ MHz}$)	NF	—	3.0	—	dB
Common Source Power Gain ($V_{DD} = 28 \text{ Vdc}, P_{out} = 125 \text{ W}, f = 150 \text{ MHz}, I_{DQ} = 100 \text{ mA}$)	G_{ps}	9.0	11.8	—	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}, P_{out} = 125 \text{ W}, f = 150 \text{ MHz}, I_{DQ} = 100 \text{ mA}$)	η	50	60	—	%
Electrical Ruggedness ($V_{DD} = 28 \text{ Vdc}, P_{out} = 125 \text{ W}, f = 150 \text{ MHz}, I_{DQ} = 100 \text{ mA},$ $V_{SWR} 30:1$ at all Phase Angles)	ψ	No Degradation in Output Power			



- C1 — 15 pF Unelco
- C2 — Arco 462, 5.0–80 pF
- C3 — 100 pF Unelco
- C4 — 25 pF Unelco
- C6 — 40 pF Unelco
- C7 — Arco 461, 2.7–30 pF
- C5, C8 — Arco 463, 9.0–180 pF
- C9, C11, C14 — 0.1 μF Erie Redcap
- C10 — 50 μF , 50 V
- C12, C13 — 680 pF Feedthru
- D1 — 1N5925A Motorola Zener

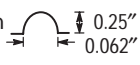
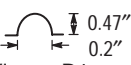
- L1 — #16 AWG, 1–1/4 Turns, 0.213" ID
- L2 — #16 AWG, Hairpin 
- L3 — #14 AWG, Hairpin 
- L4 — 10 Turns #16 AWG Enameled Wire on R1
- RFC1 — 18 Turns #16 AWG Enameled Wire, 0.3" ID
- R1 — 10 Ω , 2.0 W
- R2 — 1.8 k Ω , 1/2 W
- R3 — 10 k Ω , 10 Turn Bourns
- R4 — 10 k Ω , 1/4 W

Figure 1. 150 MHz Test Circuit

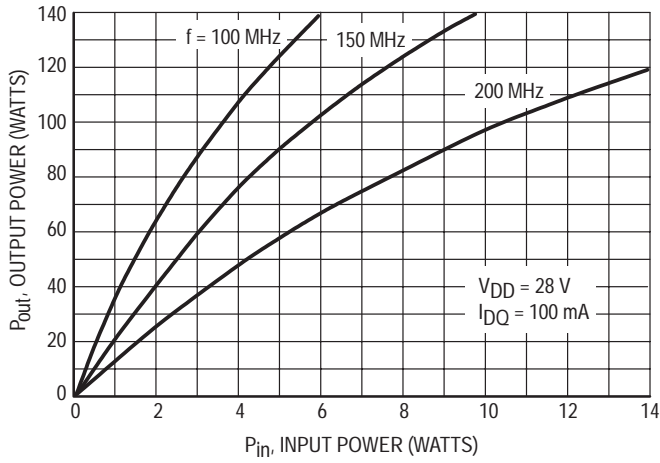


Figure 2. Output Power versus Input Power

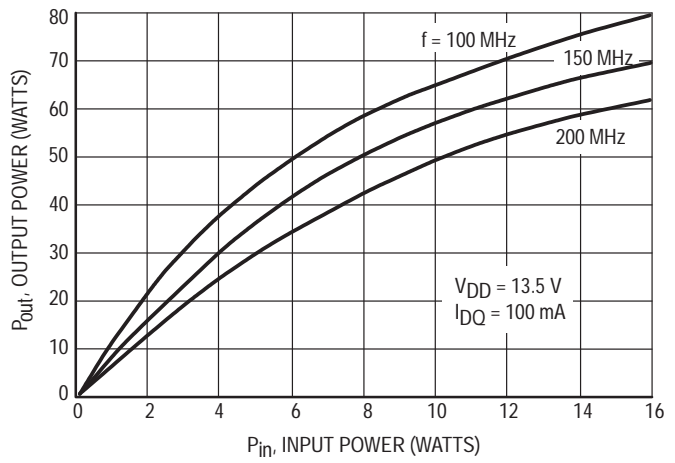


Figure 3. Output Power versus Input Power

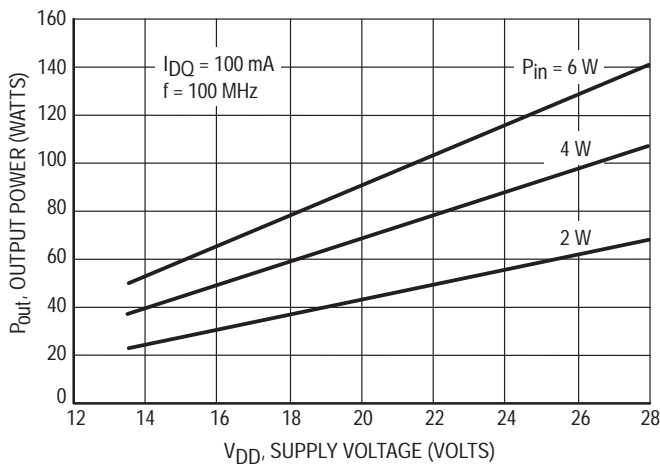


Figure 4. Output Power versus Supply Voltage

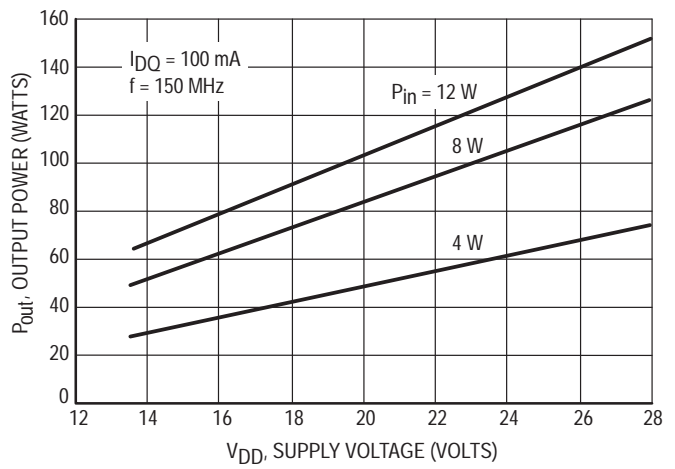


Figure 5. Output Power versus Supply Voltage

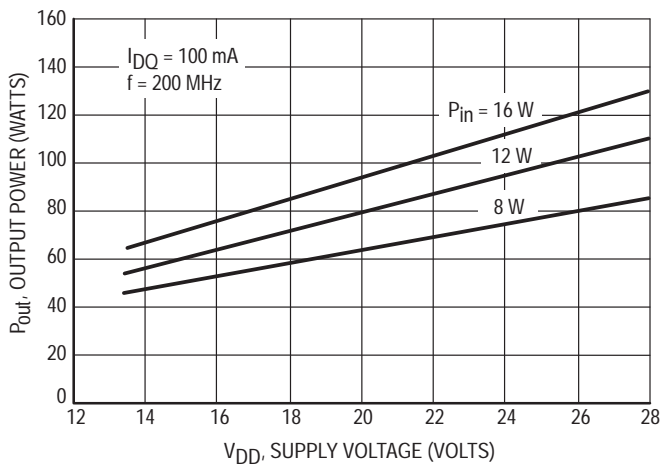


Figure 6. Output Power versus Supply Voltage

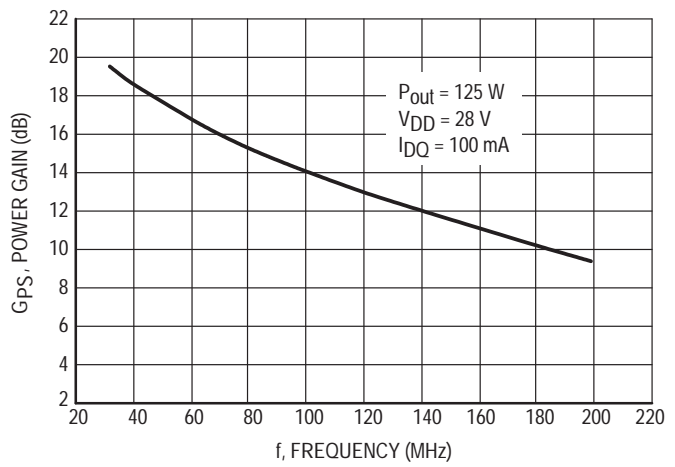


Figure 7. Power Gain versus Frequency

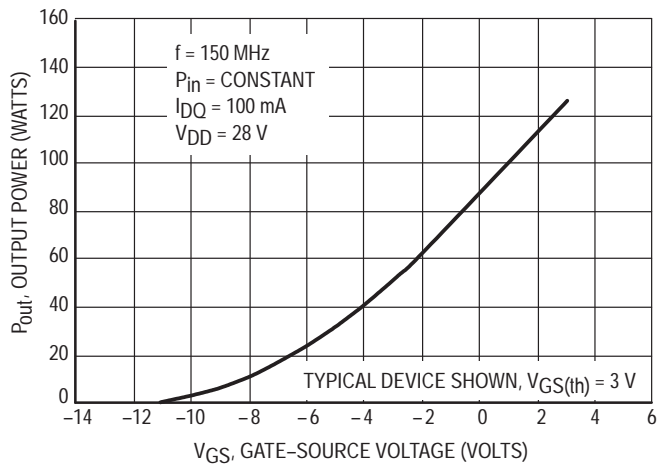


Figure 8. Output Power versus Gate Voltage

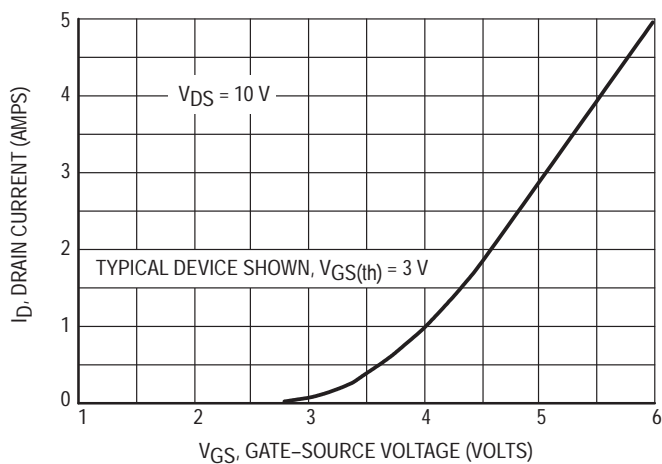


Figure 9. Drain Current versus Gate Voltage (Transfer Characteristics)

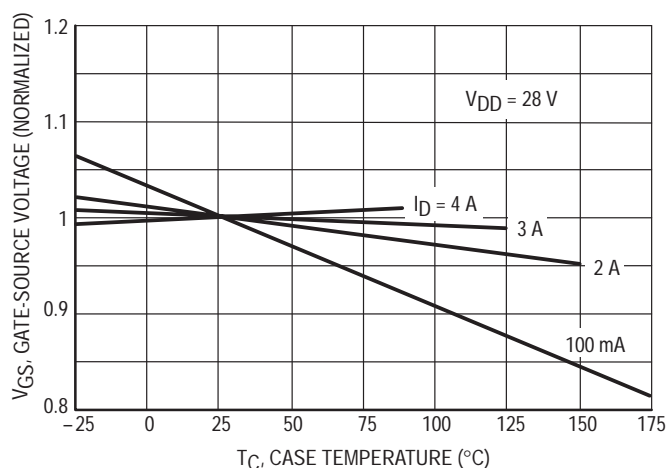


Figure 10. Gate-Source Voltage versus Case Temperature

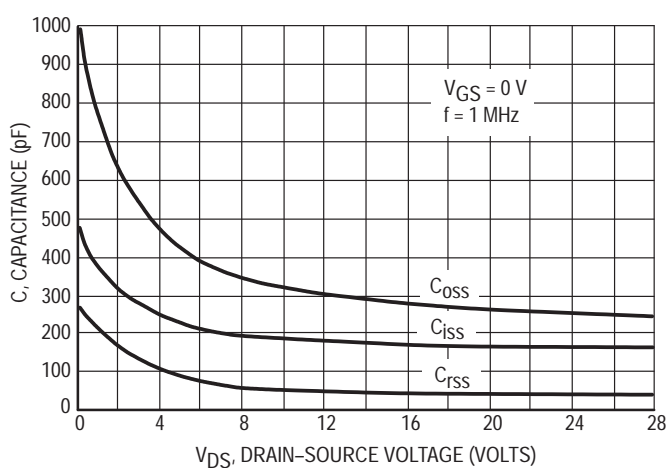


Figure 11. Capacitance versus Drain Voltage

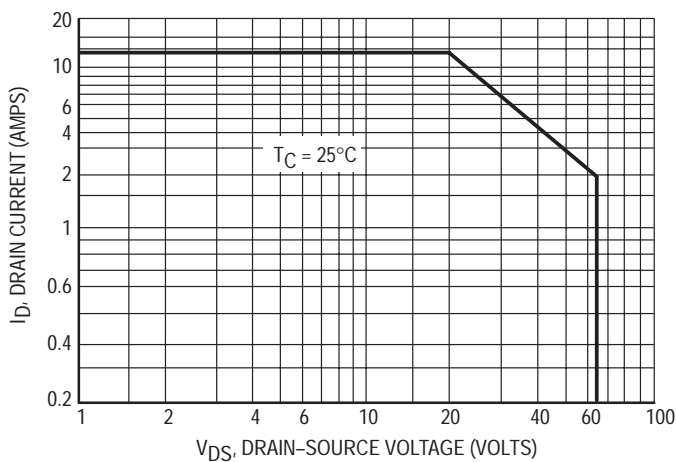


Figure 12. DC Safe Operating Area

f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
2.0	0.932	-133	74.0	112	0.011	23	0.835	-151
5.0	0.923	-160	31.6	98	0.011	12	0.886	-168
10	0.921	-170	16.0	93	0.011	10	0.896	-174
20	0.921	-175	8.00	88	0.011	12	0.899	-177
30	0.921	-177	5.32	86	0.011	16	0.900	-178
40	0.921	-177	3.98	83	0.012	21	0.901	-178
50	0.922	-178	3.17	81	0.012	26	0.902	-178
60	0.923	-178	2.63	79	0.012	30	0.903	-178
70	0.924	-178	2.24	77	0.013	34	0.904	-178
80	0.925	-178	1.95	75	0.013	39	0.906	-178
90	0.927	-178	1.72	73	0.014	43	0.907	-178
100	0.930	-178	1.50	71	0.016	45	0.910	-178
110	0.930	-178	1.31	70	0.018	46	0.912	-178
120	0.931	-178	1.19	68	0.019	47	0.914	-178
130	0.942	-178	1.10	67	0.019	49	0.919	-178
140	0.936	-178	1.01	66	0.021	50	0.921	-178
150	0.938	-178	0.936	65	0.021	53	0.922	-178
160	0.938	-178	0.879	64	0.022	53	0.923	-178
170	0.940	-178	0.830	63	0.023	54	0.923	-177
180	0.942	-178	0.780	61	0.024	56	0.924	-177
190	0.942	-178	0.737	60	0.026	59	0.928	-177
200	0.952	-178	0.705	59	0.027	58	0.929	-177
210	0.950	-178	0.668	57	0.029	61	0.934	-177
220	0.942	-178	0.626	56	0.030	61	0.933	-177
230	0.943	-178	0.592	56	0.032	62	0.939	-177
240	0.946	-177	0.566	55	0.033	64	0.941	-177
250	0.952	-177	0.545	54	0.035	64	0.943	-177
260	0.958	-177	0.523	53	0.036	65	0.946	-177
270	0.956	-177	0.500	52	0.038	67	0.943	-177
280	0.960	-177	0.481	52	0.039	68	0.946	-177
290	0.956	-178	0.460	51	0.042	68	0.944	-177
300	0.955	-178	0.443	50	0.043	68	0.947	-177

Table 1. Common Source Scattering Parameters
V_{DS} = 28 V, I_D = 3.0 A

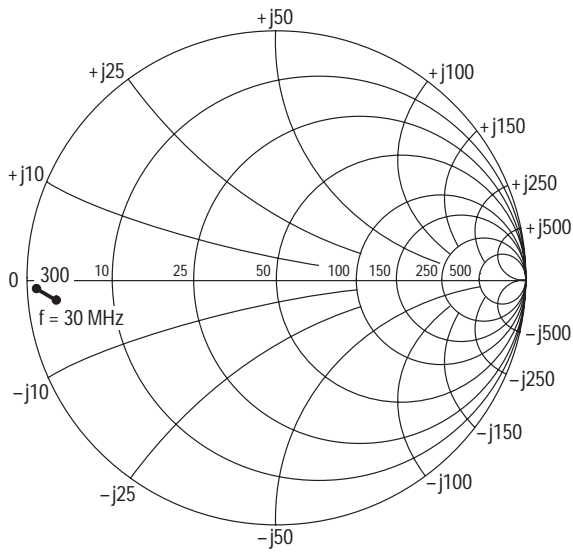


Figure 13. S_{11} , Input Reflection Coefficient versus Frequency
 $V_{DS} = 28 \text{ V}$, $I_D = 3.0 \text{ A}$

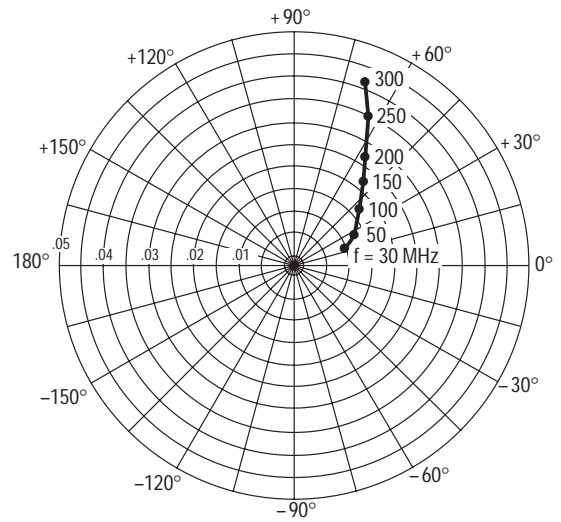


Figure 14. S_{12} , Reverse Transmission Coefficient versus Frequency
 $V_{DS} = 28 \text{ V}$, $I_D = 3.0 \text{ A}$

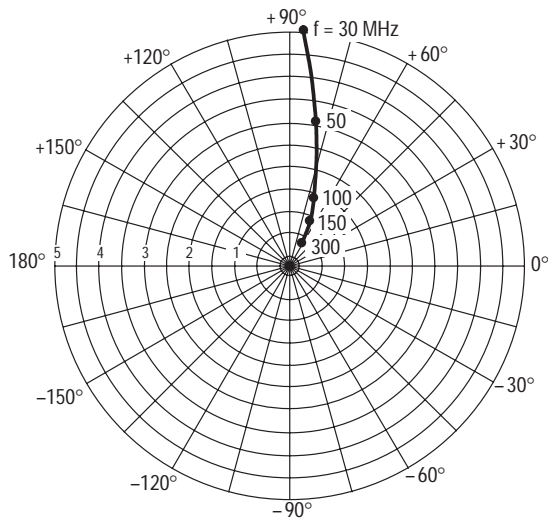


Figure 15. S_{21} , Forward Transmission Coefficient versus Frequency
 $V_{DS} = 28 \text{ V}$, $I_D = 3.0 \text{ A}$

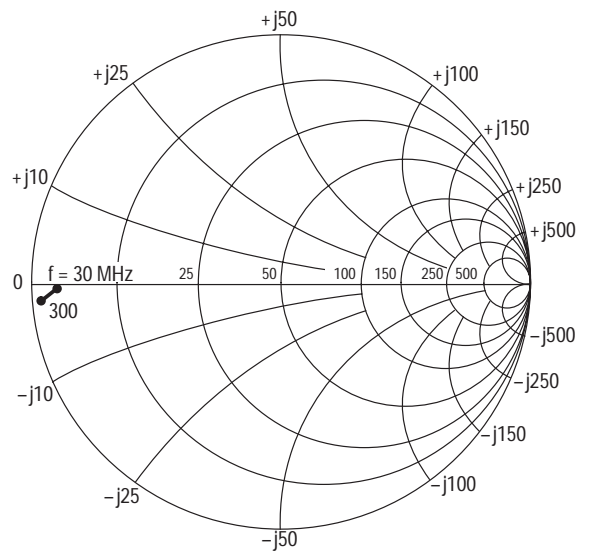


Figure 16. S_{22} , Output Reflection Coefficient versus Frequency
 $V_{DS} = 28 \text{ V}$, $I_D = 3.0 \text{ A}$

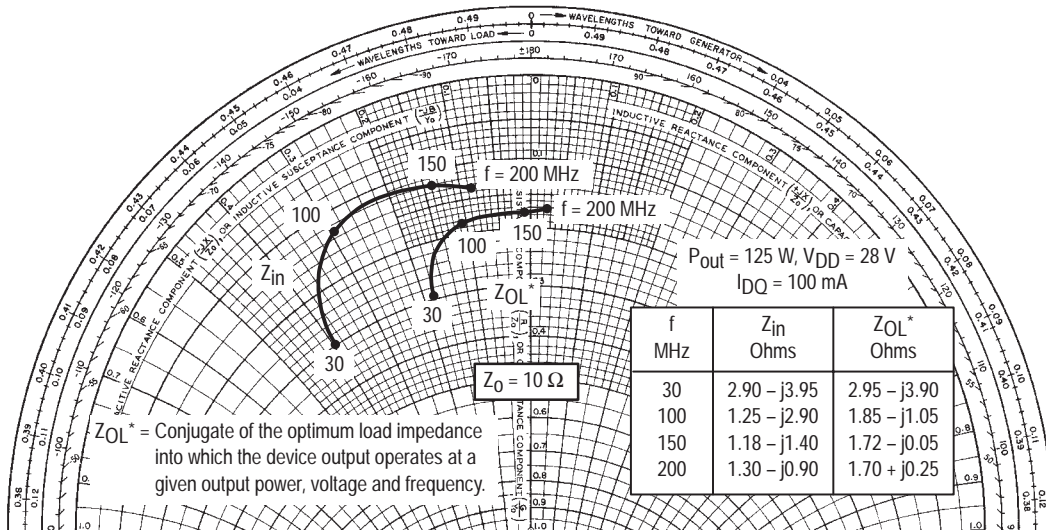


Figure 17. Series Equivalent Input/Output Impedance, Z_{in} , Z_{OL}^*

DESIGN CONSIDERATIONS

The MRF174 is a RF power N-Channel enhancement mode field-effect transistor (FET) designed especially for UHF power amplifier and oscillator applications. Motorola RF MOSFETs feature a vertical structure with a planar design, thus avoiding the processing difficulties associated with V-groove vertical power FETs.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power FETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal, thus facilitating manual gain control, ALC and modulation.

DC BIAS

The MRF174 is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. See Figure 9 for a typical plot of drain current versus gate voltage. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF174 was charac-

terized at $I_{DQ} = 100$ mA, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of the MRF174 may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems. (See Figure 8.)

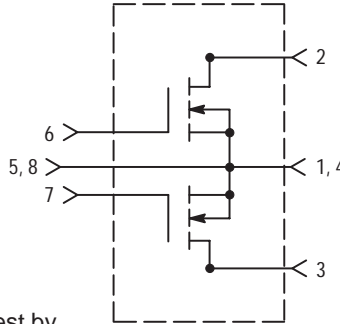
AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar UHF transistors are suitable for MRF174. See Motorola Application Note AN721, Impedance Matching Networks Applied to RF Power Transistors. The higher input impedance of RF MOSFETs helps ease the task of broadband network design. Both small signal scattering parameters and large signal impedances are provided. While the s-parameters will not produce an exact design solution for high power operation, they do yield a good first approximation. This is an additional advantage of RF MOS power FETs.

The RF MOSFET Line
RF Power
Field Effect Transistors
N-Channel Enhancement Mode MOSFET

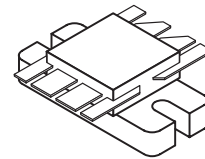
Designed for broadband commercial and military applications up to 400 MHz frequency range. Primarily used as a driver or output amplifier in push-pull configurations. Can be used in manual gain control, ALC and modulation circuits.

- Typical Performance at 400 MHz, 28 V:
Output Power — 100 W
Gain — 12 dB
Efficiency — 60%
- Low Thermal Resistance
- Low C_{RSS} — 10 pF Typ @ $V_{DS} = 28$ Volts
- Ruggedness Tested at Rated Output Power
- Nitride Passivated Die for Enhanced Reliability
- Excellent Thermal Stability; Suited for Class A Operation
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.
- S-Parameters Available for Download into Frequency Domain Simulators. See <http://motorola.com/sps/rf/designrtds/>



MRF177

100 W, 28 V, 400 MHz
N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 744A-01, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1.0 \text{ M}\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 40	Vdc
Drain Current — Continuous	I_D	16	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1) Derate above 25°C	P_D	270 1.54	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Temperature Range	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction-to-Case	$R_{\theta JC}$	0.65	$^\circ\text{C}/\text{W}$

(1) Total device dissipation rating applies only when the device is operated as an RF push-pull amplifier.

NOTE — CAUTION — MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic (1)	Symbol	Min	Typ	Max	Unit
--------------------	--------	-----	-----	-----	------

OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 50 \text{ mA}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ V}, V_{GS} = 0$)	I_{DSS}	—	—	2.0	mAdc
Gate–Source Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

ON CHARACTERISTICS (1)

Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 50 \text{ mA}$)	$V_{GS(th)}$	1.0	3.0	6.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 3.0 \text{ A}$)	$V_{DS(on)}$	—	—	1.4	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 2.0 \text{ A}$)	g_{fs}	1.8	2.2	—	mhos

DYNAMIC CHARACTERISTICS (1)

Input Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{iss}	—	100	—	pF
Output Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{oss}	—	105	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1.0 \text{ MHz}$)	C_{rss}	—	10	—	pF

FUNCTIONAL CHARACTERISTICS (Figure 8) (2)

Common Source Power Gain ($V_{DD} = 28 \text{ Vdc}, P_{out} = 100 \text{ W}, f = 400 \text{ MHz}, I_{DQ} = 200 \text{ mA}$)	G_{PS}	10	12	—	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}, P_{out} = 100 \text{ W}, f = 400 \text{ MHz}, I_{DQ} = 200 \text{ mA}$)	η	55	60	—	%
Electrical Ruggedness ($V_{DD} = 28 \text{ Vdc}, P_{out} = 100 \text{ W}, f = 400 \text{ MHz}, I_{DQ} = 200 \text{ mA}$, Load VSWR = 30:1, All Phase Angles At Frequency of Test)	ψ	No Degradation in Output Power Before & After Test			

(1) Note each transistor chip measured separately

(2) Both transistor chips operating in push–pull amplifier

TYPICAL CHARACTERISTICS

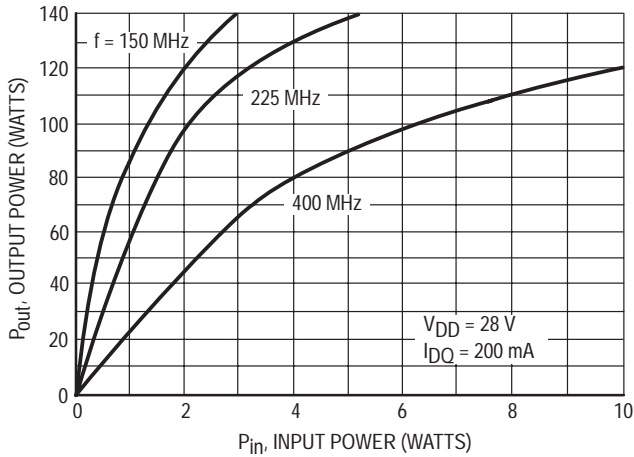


Figure 1. Output Power versus Input Power

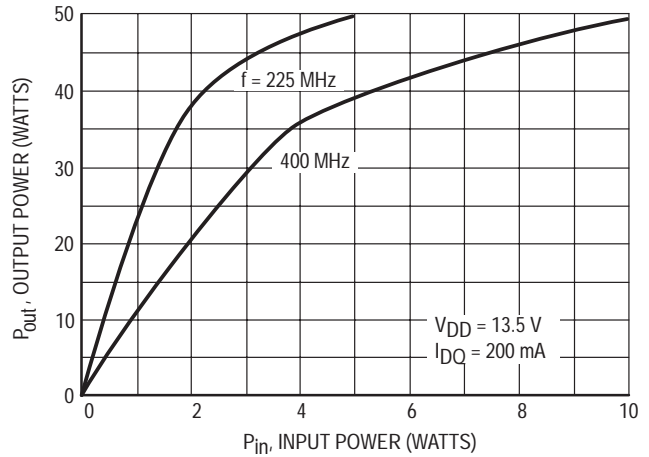


Figure 2. Output Power versus Input Power

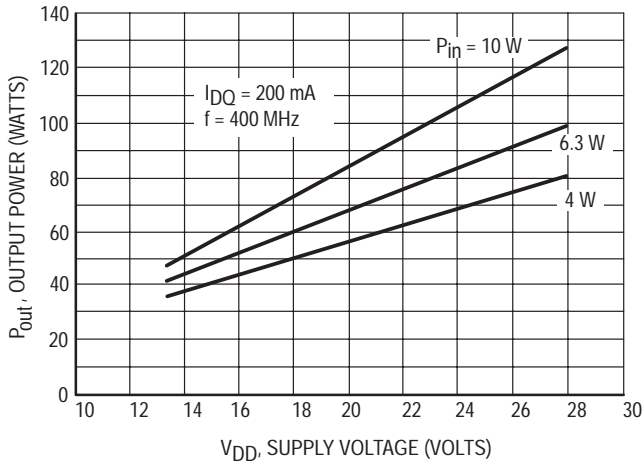


Figure 3. Output Power versus Supply Voltage

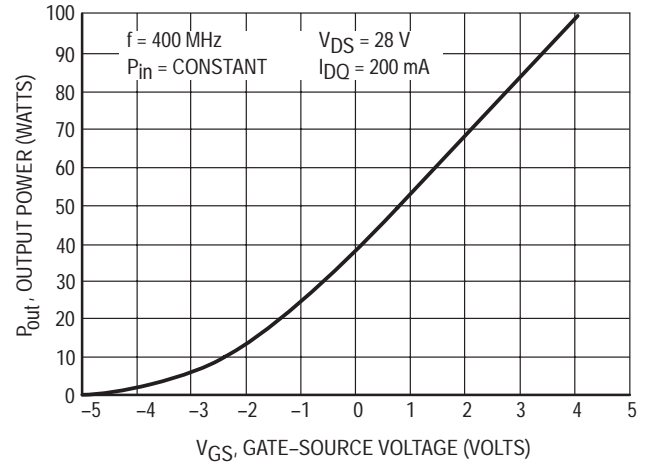


Figure 4. Output Power versus Gate Voltage

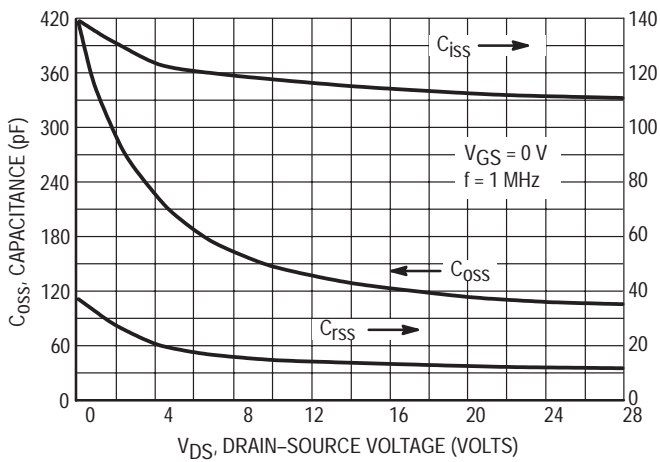


Figure 5. Capacitance versus Drain Voltage

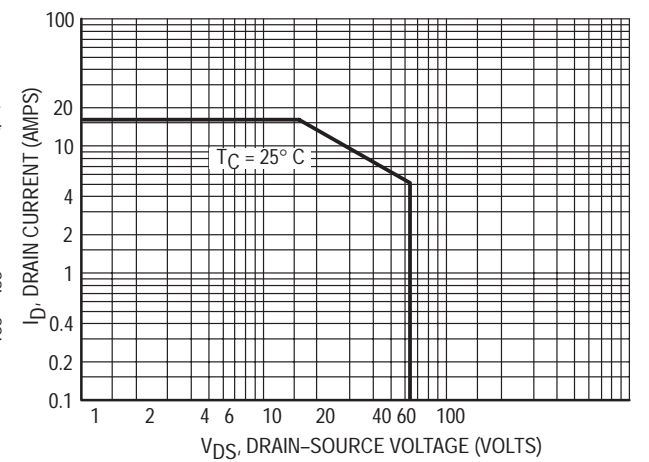
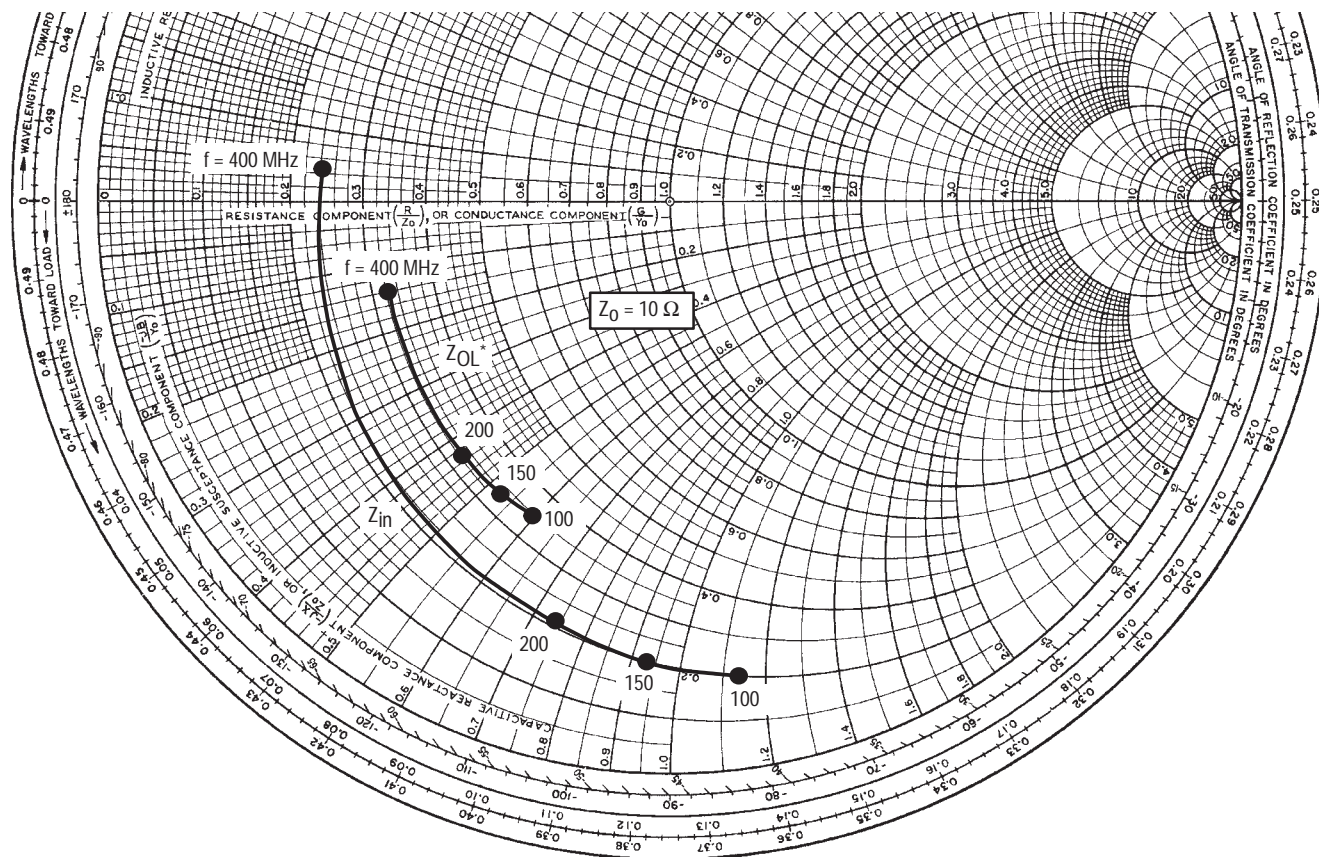


Figure 6. DC Safe Operating Area

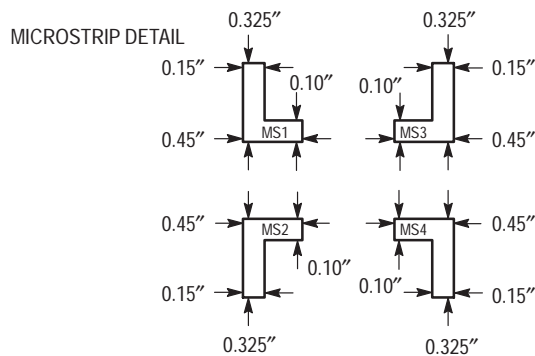
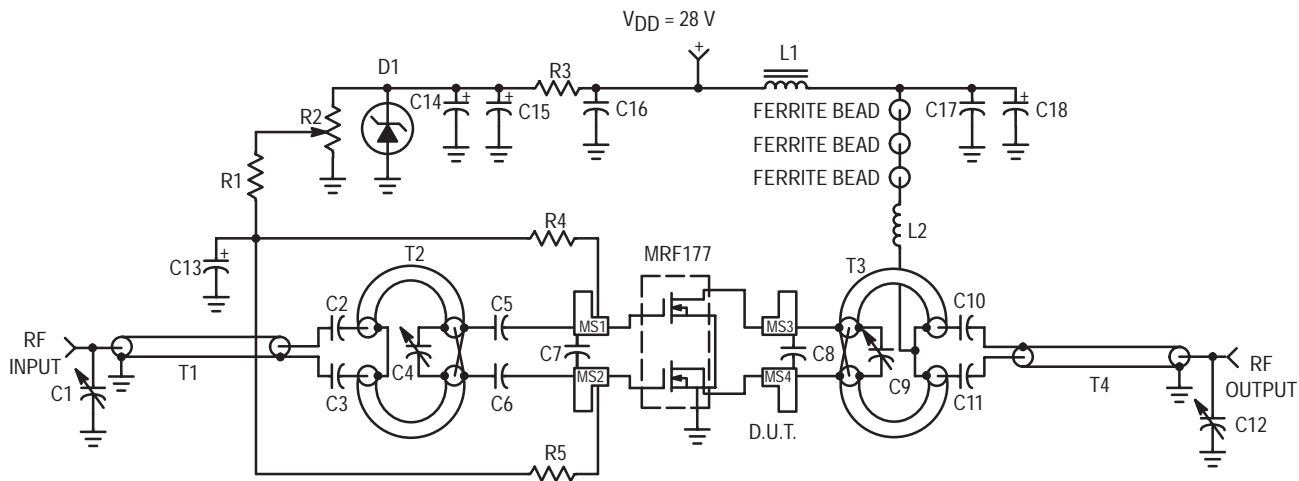


NOTE: Input and Output Impedance values given are measured gate-to-gate and drain-to-drain respectively.

V _{DD} = 28 V I _{DQ} = 200 mA P _{out} = 100 W		
f (MHz)	Z _{in} Ohms	Z _{OL} * Ohms
100	2.0 - j11.5	3.5 - j6
150	2.05 - j9.45	3.35 - j5.34
200	2.1 - j7.5	3.3 - j4.4
400	2.35 + j0.4	3.2 - j1.38

Z_{OL}*: Conjugate of optimum load impedance into which the device operates at a given output power, voltage, current and frequency.

Figure 7. Impedance or Admittance Coordinates



C1, C12	1-10 pF JOHANSON OR EQUIVALENT	D1	1N5347B, 20 Vdc
C2, C3, C5, C6, C10, C11	270 pF ATC 100 MIL CHIP CAP	L1	1-TURN NO. 18, 0.25", 2-HOLE FERRITE BEAD
C4, C9	1-20 pF	L2	8-1/2 TURNS NO. 18, CLOSE WOUND .375" DIA.
C7	36 pF CHIP CAP	R1, R4, R5	10 kΩ @ 1/2 W RESISTOR
C8	10 pF CHIP CAP	R2	10 kΩ, 10 TURN RESISTOR
C13, C14	0.1 μFD @ 50 Vdc	R3	2.0 kΩ @ 1/2 W RESISTOR
C15, C18	10 μFD @ 50 Vdc	T1	1-1/2 T, 50 Ω COAX, .034" DIA. ON DUAL 0.5" FERRITE CORE
C16	500 pF BUTTON	T2	2.0" 25 Ω COAX, .075" DIA.
C17	1000 pF UNCASED MICA	T3	2.1" 10 Ω COAX, .075" DIA.
		T4	4.0" 50 Ω COAX, .0865" DIA.
		BOARD	Dielectric Thickness = 0.060" 2oz Copper, Cu-Clad, Teflon Fiberglass, ε _r = 2.55

Figure 8. Test Circuit Electrical Schematic

NOTE: S-Parameter data represents measurements taken from one chip only.

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 0.4\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.797	-154	12.40	88	0.029	2	0.756	-159
40	0.739	-161	9.06	89	0.027	8	0.702	-165
50	0.749	-164	6.84	85	0.026	7	0.707	-168
60	0.770	-163	6.06	80	0.027	3	0.754	-168
70	0.790	-164	5.40	73	0.027	-1	0.776	-168
80	0.800	-166	4.60	70	0.026	-1	0.777	-168
90	0.808	-167	3.94	67	0.025	-1	0.795	-168
100	0.816	-168	3.47	64	0.024	-1	0.809	-169
110	0.816	-169	3.14	62	0.023	1	0.809	-169
120	0.815	-170	2.76	61	0.022	6	0.794	-169
130	0.821	-171	2.45	59	0.021	12	0.799	-170
140	0.828	-171	2.27	56	0.022	18	0.806	-169
150	0.836	-171	2.10	53	0.028	25	0.805	-169
160	0.861	-172	1.96	51	0.032	-6	0.823	-168
170	0.863	-173	1.77	49	0.020	-4	0.836	-166
180	0.869	-173	1.63	46	0.018	5	0.881	-169
190	0.872	-174	1.52	44	0.017	14	0.894	-169
200	0.873	-175	1.41	43	0.017	25	0.888	-171
210	0.877	-176	1.28	42	0.018	36	0.877	-171
220	0.880	-176	1.18	41	0.019	46	0.868	-171
230	0.881	-177	1.15	38	0.024	51	0.926	-173
240	0.877	-178	1.09	35	0.031	56	0.893	-174
250	0.857	-180	1.04	33	0.049	55	0.903	-173
260	0.758	-178	0.95	31	0.090	24	0.903	-172
270	0.862	-171	0.87	31	0.056	-33	0.933	-173
280	0.902	-174	0.85	32	0.027	-39	0.949	-174
290	0.913	-176	0.77	30	0.017	-28	0.891	-175
300	0.919	-177	0.72	30	0.012	-8	0.894	-175
310	0.922	-178	0.71	28	0.012	11	0.913	-175
320	0.925	-178	0.67	26	0.012	28	0.896	-175
330	0.927	-179	0.64	24	0.012	40	0.929	-176
340	0.929	-179	0.62	24	0.013	46	0.925	-179
350	0.931	-180	0.58	24	0.015	52	0.942	-174
360	0.934	180	0.55	24	0.017	55	0.944	-176
370	0.937	179	0.52	23	0.019	61	0.944	-176
380	0.940	179	0.49	21	0.020	68	0.919	-175
390	0.941	178	0.45	22	0.020	69	0.938	-177
400	0.942	178	0.46	18	0.021	73	0.920	-173
410	0.941	177	0.45	19	0.023	67	0.961	-178
420	0.943	177	0.44	18	0.026	67	0.945	-178
430	0.945	176	0.41	16	0.029	70	0.959	-179

Table 1. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 0.4\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
440	0.947	176	0.38	16	0.029	75	0.962	-179
450	0.949	176	0.38	19	0.030	78	0.984	-178
460	0.952	175	0.36	17	0.029	72	0.987	178
470	0.953	175	0.34	18	0.030	70	0.976	179
480	0.952	174	0.34	14	0.035	69	0.968	179
490	0.952	174	0.34	14	0.039	72	0.987	178
500	0.952	174	0.32	13	0.040	76	1.002	179
600	0.938	170	0.22	9	0.047	117	1.013	172
700	0.962	166	0.19	13	0.060	73	0.993	171
800	0.953	162	0.17	18	0.097	68	0.981	171
900	0.953	159	0.14	21	0.097	65	0.949	166
1000	0.952	156	0.14	27	0.110	68	0.982	163

Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.435\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.803	-153	13.50	89	0.028	3	0.746	-157
40	0.742	-160	9.90	90	0.026	9	0.686	-164
50	0.752	-163	7.48	85	0.025	8	0.692	-168
60	0.773	-163	6.62	80	0.026	4	0.739	-167
70	0.794	-164	5.91	74	0.026	1	0.761	-167
80	0.803	-166	5.04	70	0.025	1	0.763	-167
90	0.812	-167	4.32	68	0.024	1	0.783	-167
100	0.819	-168	3.81	64	0.022	1	0.798	-168
110	0.818	-169	3.44	62	0.022	3	0.797	-168
120	0.817	-170	3.03	61	0.021	9	0.779	-168
130	0.823	-171	2.68	59	0.020	15	0.784	-170
140	0.830	-171	2.49	57	0.021	21	0.793	-169
150	0.838	-171	2.30	53	0.027	27	0.792	-169
160	0.864	-172	2.16	52	0.030	-5	0.816	-167
170	0.865	-173	1.95	49	0.019	-2	0.827	-166
180	0.870	-173	1.79	46	0.017	8	0.869	-168
190	0.873	-174	1.67	44	0.016	18	0.882	-168
200	0.874	-175	1.55	43	0.017	27	0.878	-171
210	0.878	-176	1.40	42	0.017	37	0.866	-171
220	0.881	-176	1.29	41	0.019	47	0.858	-171
230	0.881	-177	1.25	38	0.025	53	0.918	-172
240	0.877	-178	1.20	35	0.031	59	0.882	-173
250	0.856	-180	1.13	33	0.048	57	0.893	-173
260	0.760	-178	1.03	31	0.088	24	0.899	-172
270	0.864	-171	0.96	31	0.056	-33	0.931	-172
280	0.903	-174	0.93	32	0.027	-38	0.946	-173
290	0.914	-176	0.85	30	0.015	-25	0.885	-174

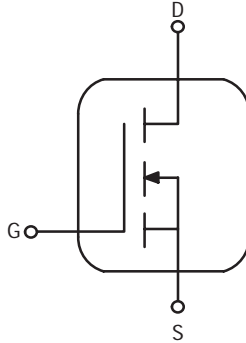
Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.435\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
300	0.919	-177	0.79	30	0.010	-7	0.881	-175
310	0.922	-178	0.78	28	0.009	6	0.903	-175
320	0.925	-178	0.75	26	0.010	18	0.900	-175
330	0.927	-179	0.70	24	0.012	31	0.925	-176
340	0.929	-180	0.68	24	0.014	45	0.920	-178
350	0.931	180	0.63	25	0.015	63	0.932	-173
360	0.934	179	0.61	23	0.014	70	0.931	-176
370	0.936	179	0.57	23	0.013	68	0.929	-176
380	0.939	178	0.53	21	0.015	61	0.909	-176
390	0.941	178	0.50	22	0.018	61	0.940	-178
400	0.941	178	0.50	18	0.022	74	0.917	-173
410	0.940	177	0.49	19	0.024	80	0.955	-178
420	0.941	177	0.48	18	0.022	83	0.942	-178
430	0.943	176	0.46	16	0.020	77	0.957	-179
440	0.946	176	0.42	16	0.022	69	0.960	-178
450	0.948	175	0.41	18	0.029	71	0.982	-177
460	0.951	175	0.39	17	0.032	76	0.983	178
470	0.951	175	0.37	17	0.031	88	0.968	179
480	0.950	174	0.37	13	0.027	93	0.965	179
490	0.950	174	0.37	13	0.025	81	0.994	179
500	0.950	173	0.36	12	0.031	69	1.012	180
600	0.936	170	0.24	7	0.063	127	1.005	171
700	0.960	166	0.20	11	0.064	72	0.989	171
800	0.953	162	0.17	15	0.092	66	1.017	169
900	0.954	159	0.15	19	0.092	65	0.952	167
1000	0.952	156	0.15	24	0.082	56	0.988	162

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MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current — Continuous	I_D	2.0	Adc
Total Device Dissipation @ $T_C = 70^\circ\text{C}$ Derate above 70°C	P_D	36 0.278	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	5.42	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 50 \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS1}	—	—	1.0	μA
Zero Gate Voltage Drain Current ($V_{DS} = 65 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS2}	—	—	1.0	μA
Gate–Source Leakage Current ($V_{GS} = 20 \text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1.0	μA

ON CHARACTERISTICS

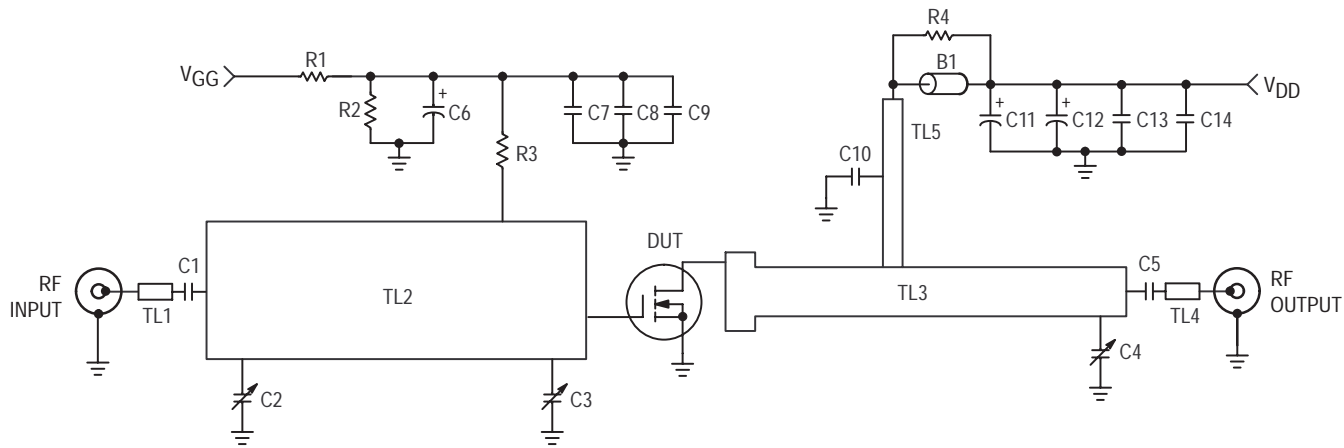
Gate Threshold Voltage ($V_{DS} = 10 \text{ Vdc}$, $I_D = 55 \mu\text{A}$)	$V_{GS(th)}$	2.0	3.6	4.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ Vdc}$, $I_D = 0.5 \text{ A}$)	$V_{DS(on)}$	0.3	0.66	0.8	Vdc
Gate Quiescent Voltage ($V_{DS} = 28 \text{ Vdc}$, $I_D = 170 \text{ mA}$)	$V_{GS(q)}$	3.5	—	5.5	Vdc

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$, $f = 1.0 \text{ MHz}$)	C_{iss}	—	13	—	pF
Output Capacitance ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$, $f = 1.0 \text{ MHz}$)	C_{oss}	—	6.6	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$, $f = 1.0 \text{ MHz}$)	C_{rss}	—	0.69	—	pF

FUNCTIONAL TESTS (In Motorola Test Circuit. See Figure 1.)

Common–Source Power Gain ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 7.5 \text{ W PEP}$, $I_{DQ} = 170 \text{ mA}$, $f_1 = 945 \text{ MHz}$, $f_2 = 945.1 \text{ MHz}$, Min 15.5 dB)	G_{ps}	15.5	17	—	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 7.5 \text{ W PEP}$, $I_{DQ} = 170 \text{ mA}$, $f_1 = 945 \text{ MHz}$, $f_2 = 945.1 \text{ MHz}$)	η	30	32.5	—	%
Input Return Loss ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 7.5 \text{ W PEP}$, $I_{DQ} = 170 \text{ mA}$, $f_1 = 945 \text{ MHz}$, $f_2 = 945.1 \text{ MHz}$)	IRL	—	–12.7	–9	dB
Intermodulation Distortion ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 7.5 \text{ W PEP}$, $I_{DQ} = 170 \text{ mA}$, $f_1 = 945 \text{ MHz}$, $f_2 = 945.1 \text{ MHz}$)	IMD	—	–30	–28.5	dBc
Output Mismatch Stress ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 7.5 \text{ W CW}$, $I_{DQ} = 170 \text{ mA}$, $f_1 = 945 \text{ MHz}$, Load VSWR = 5:1, All Phase Angles)	Ψ	No Degradation In Output Power			



B1	Short RF Bead, Fair Rite-2743019447	C10	30 pF Chip Capacitor, ATC 100B390CCA500X
C1	18 pF Chip Capacitor, ATC 100B180CCA500X	C11	250 μ F, 50 Vdc Electrolytic Capacitor, Mallory TC50025
C2, C3	0.8–8.0 pF Variable Capacitor, Johansen Gigatrim	N1, N2	Type N Connector
C4	0.4–2.5 pF Variable Capacitor, Johansen Gigatrim	R1	1.2 k Ω , 1/4 W Resistor
C5	100 pF Chip Capacitor, ATC 100A101CCA150X	R2	47 k Ω , 1/4 W Resistor
C6, C12	10 μ F, 50 Vdc Electrolytic Capacitor, Panasonic ECEV1HV100R	R3	10 k Ω , 1/4 W Chip Resistor
C7	43 pF Chip Capacitor, ATC 100B430CCA500X	R4	4.0 x 39 Ω , 1/8 W Chip Resistor
C8, C13	1000 pF Chip Capacitor, ATC 100B102CCA500X	TL1-TL5	Microstrip Line
C9, C14	0.1 μ F 50 Vdc Ceramic, Kemet CDR33BX104AKWS	Ckt Board	1/32" Glass Teflon [®] , $\epsilon_r = 2.55$, Arlon-GX-0300-55-22

Figure 1. MRF181 Test Circuit Schematic

TYPICAL CHARACTERISTICS

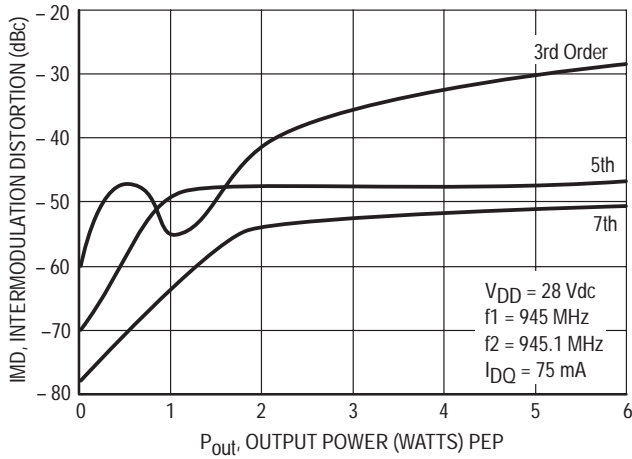


Figure 2. Intermodulation Distortion Products versus Output Power

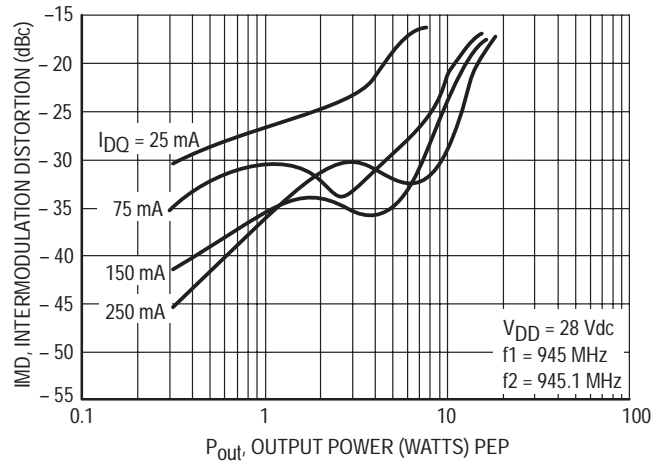


Figure 3. Intermodulation Distortion versus Output Power

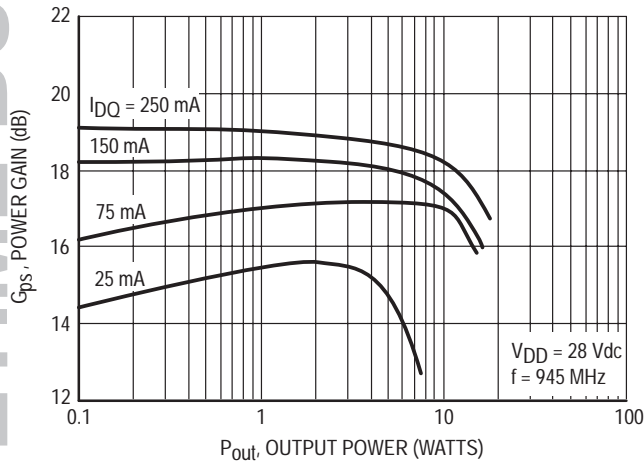


Figure 4. Power Gain versus Output Power

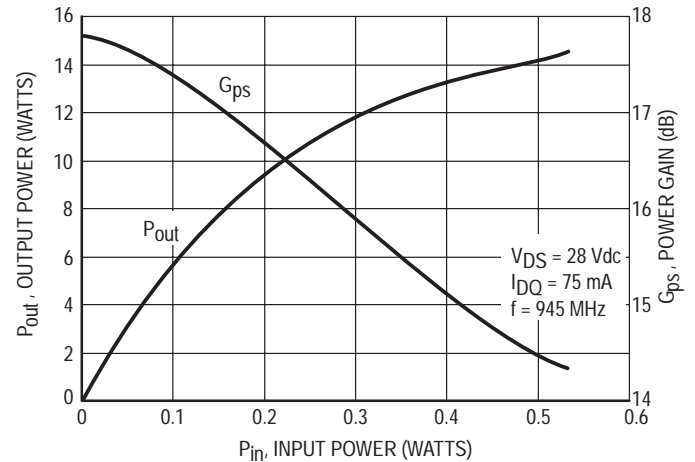


Figure 5. Output Power versus Input Power

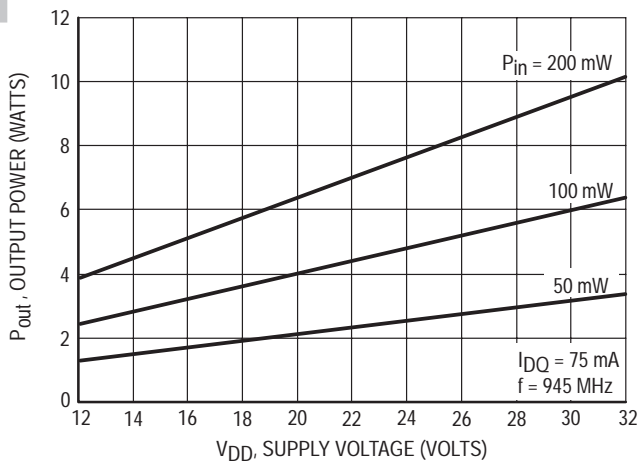


Figure 6. Output Power versus Supply Voltage

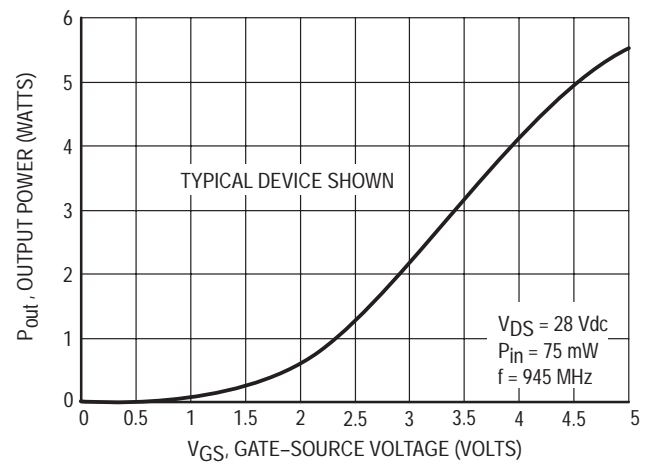


Figure 7. Output Power versus Gate Voltage

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TYPICAL CHARACTERISTICS

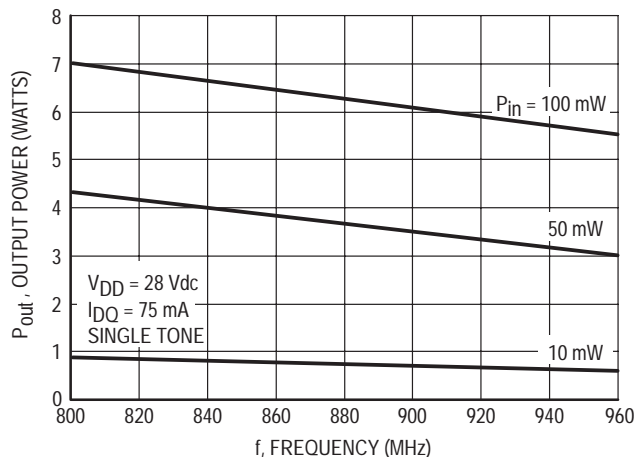


Figure 8. Output Power versus Frequency

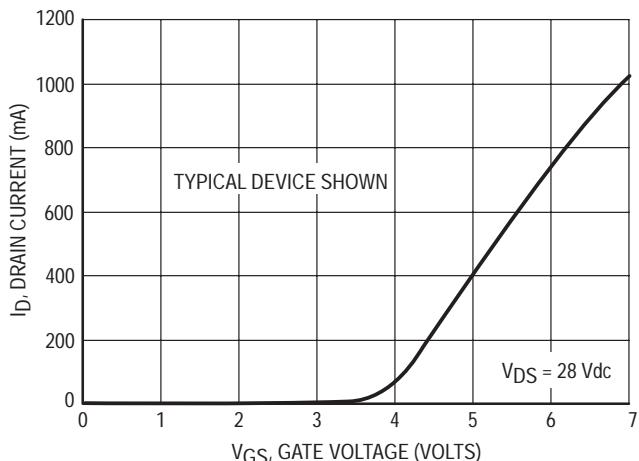


Figure 9. Drain Current versus Gate Voltage

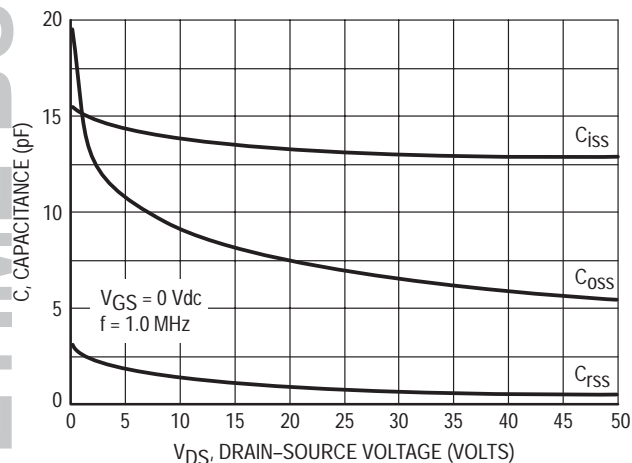


Figure 10. Capacitance versus Voltage

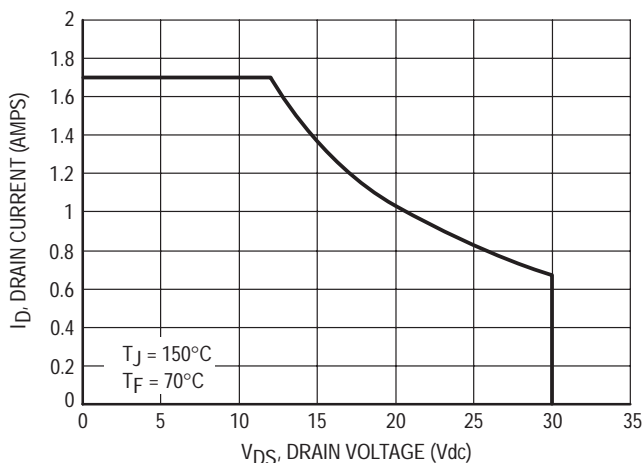


Figure 11. DC Safe Operating Area

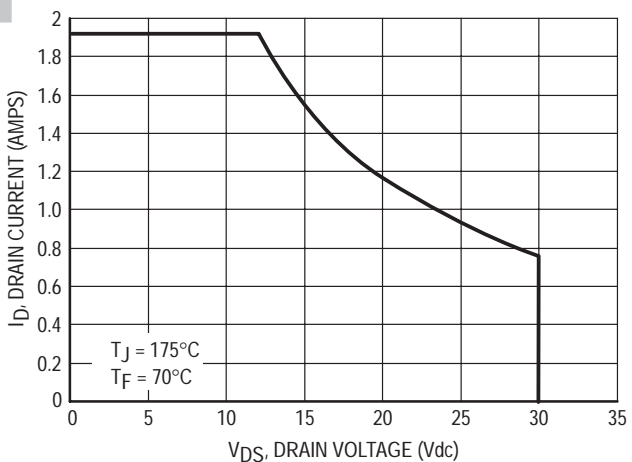


Figure 12. DC Safe Operating Area

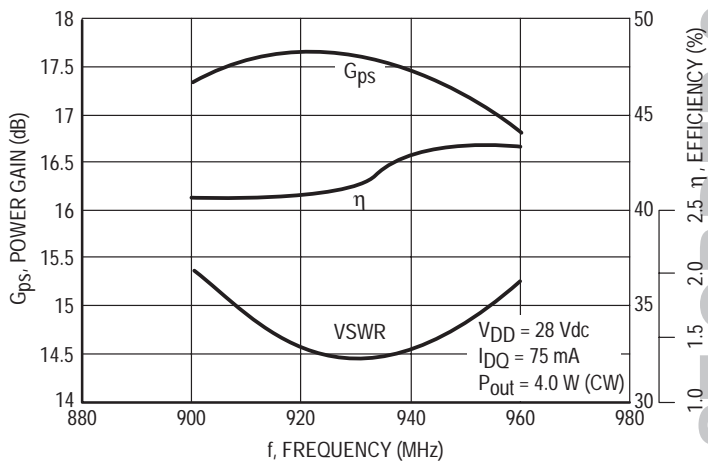


Figure 13. Performance in Broadband Circuit

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TYPICAL CHARACTERISTICS

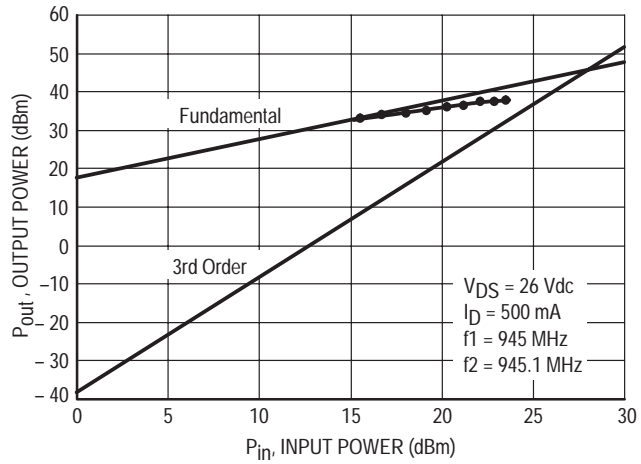


Figure 14. Class A Third Order Intercept Point

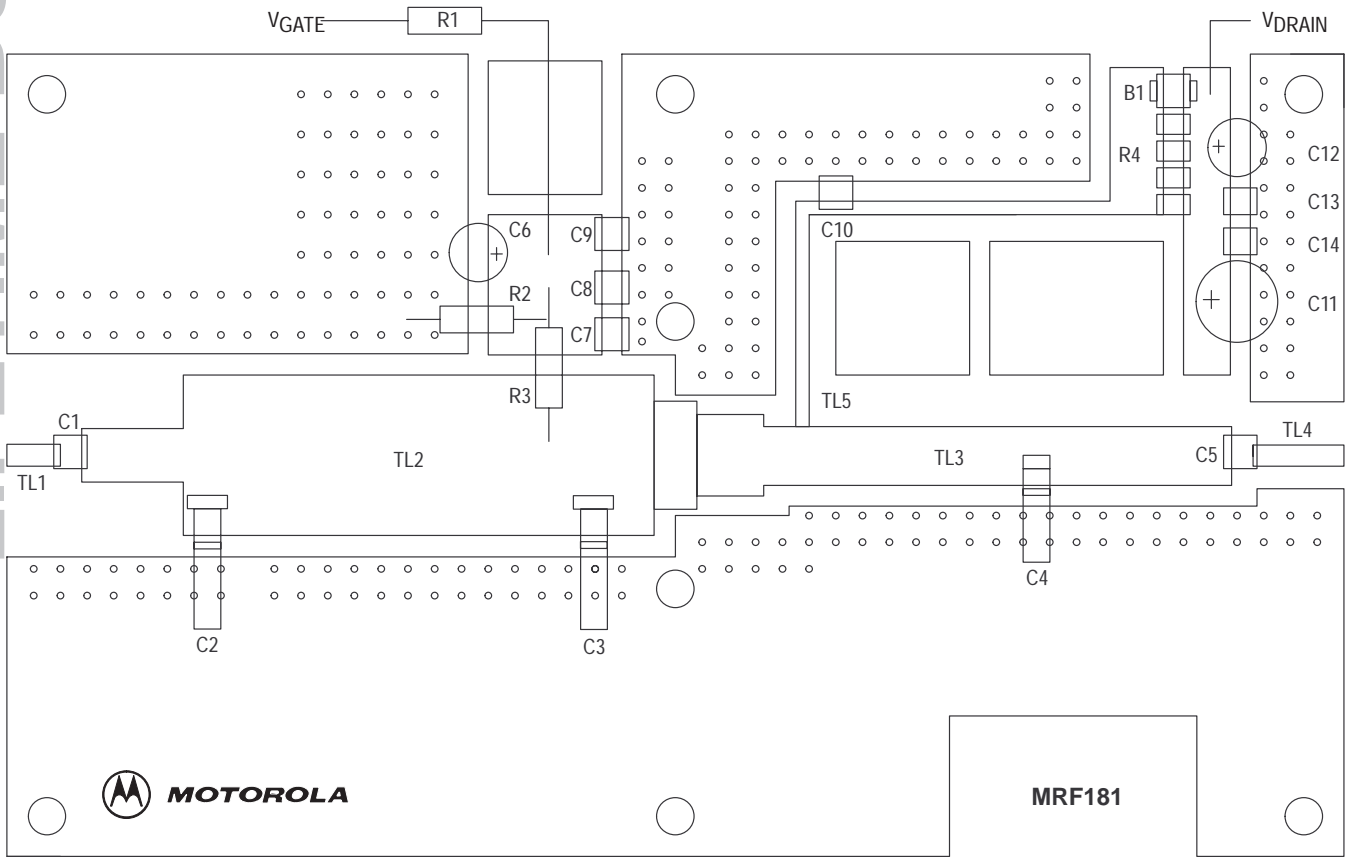
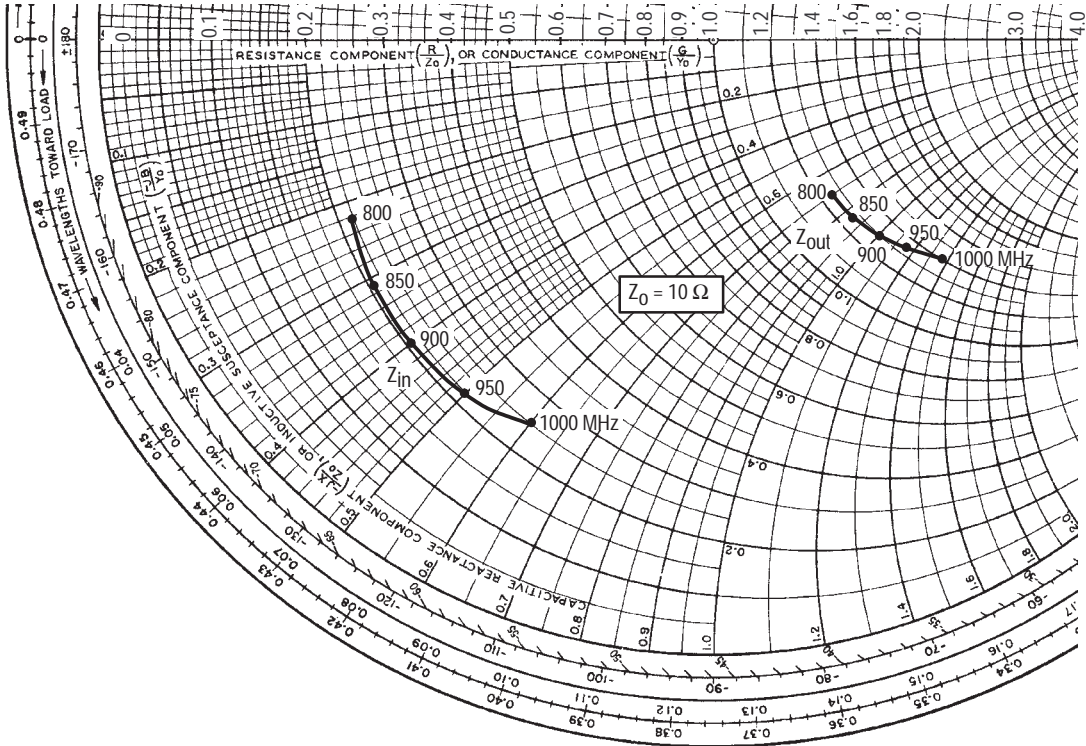


Figure 15. Component Parts Layout

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$V_{DD} = 28 \text{ Vdc}$, $I_{DQ} = 170 \text{ mA}$, $P_{out} = 7.5 \text{ W (PEP)}$

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
800	$2.15 - j2.2$	$12.45 - j7.0$
850	$2.11 - j3.5$	$12.65 - j8.5$
900	$2.14 - j4.0$	$12.95 - j10.0$
950	$2.20 - j5.0$	$13.52 - j11.5$
1000	$2.35 - j5.8$	$14.11 - j13.7$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency and efficiency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

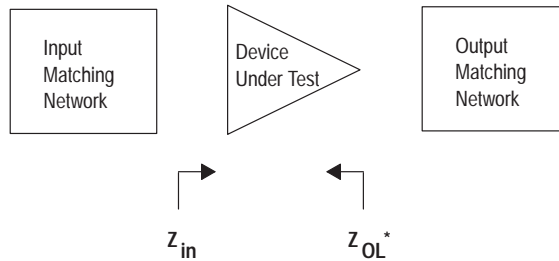


Figure 16. Series Equivalent Input and Output Impedance

Table 1. Common Emitter S-Parameters ($V_{DS} = 26$ Vdc)

$I_D = 500$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	∠φ	S ₂₁	∠φ	S ₁₂	∠φ	S ₂₂	∠φ
10	0.944	-10	31.66	174	0.004	84	0.772	-7
20	0.940	-20	31.23	168	0.008	78	0.765	-14
30	0.934	-30	30.54	162	0.011	73	0.752	-21
40	0.927	-39	29.66	156	0.015	67	0.736	-28
50	0.918	-48	28.62	151	0.018	62	0.718	-34
100	0.873	-83	22.81	129	0.028	41	0.620	-60
150	0.843	-106	17.94	114	0.033	28	0.549	-78
200	0.827	-121	14.44	103	0.035	18	0.509	-90
250	0.820	-131	11.94	95	0.036	11	0.490	-99
300	0.817	-139	10.09	88	0.036	6	0.484	-105
350	0.817	-145	8.69	82	0.036	1	0.487	-111
400	0.820	-149	7.59	77	0.035	-3	0.496	-115
450	0.823	-153	6.71	72	0.034	-7	0.508	-118
500	0.828	-156	5.99	68	0.033	-10	0.523	-122
550	0.833	-159	5.39	64	0.032	-12	0.538	-125
600	0.839	-161	4.88	60	0.031	-15	0.555	-127
650	0.845	-163	4.44	56	0.029	-17	0.572	-130
700	0.851	-165	4.06	52	0.028	-19	0.589	-132
750	0.857	-167	3.73	49	0.026	-20	0.606	-134
800	0.864	-169	3.44	45	0.025	-22	0.622	-137
850	0.870	-171	3.18	42	0.023	-23	0.638	-139
900	0.876	-172	2.95	39	0.022	-23	0.654	-141
950	0.882	-174	2.74	36	0.020	-24	0.669	-143
1000	0.888	-175	2.55	33	0.018	-24	0.683	-144
1050	0.893	-176	2.38	30	0.017	-23	0.697	-146
1100	0.899	-178	2.23	28	0.015	-22	0.710	-148
1150	0.904	-179	2.09	25	0.014	-20	0.722	-150
1200	0.909	180	1.96	22	0.012	-16	0.734	-151
1250	0.914	179	1.85	20	0.011	-12	0.745	-153
1300	0.918	177	1.74	17	0.010	-6	0.756	-155
1350	0.922	176	1.64	15	0.009	1	0.766	-156
1400	0.927	175	1.55	13	0.009	10	0.775	-158
1450	0.931	174	1.47	10	0.008	20	0.784	-159
1500	0.934	173	1.39	8	0.008	30	0.793	-161

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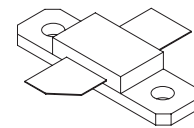
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The RF MOSFET Line
RF Power
Field Effect Transistors
N-Channel Enhancement-Mode Lateral
MOSFETs

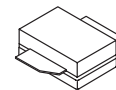
- High Gain, Rugged Device
- Broadband Performance from HF to 1 GHz
- Bottom Side Source Eliminates DC Isolators, Reducing Common Mode Inductances
- MRF182S Available in Tape and Reel by Adding R1 Suffix to Part Number. MRF182SR1 = 500 Units per 24 mm, 13 inch Reel.

MRF182
MRF182S, R1

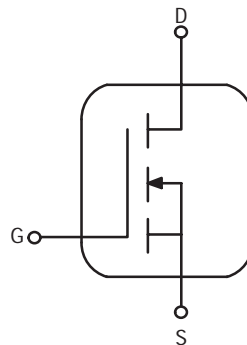
30 W, 1.0 GHz
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 360B-03, STYLE 1
(MRF182)



CASE 360C-03, STYLE 1
(MRF182S)



MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Total Device Dissipation @ $T_C = 70^\circ\text{C}$ Derate above 70°C	P_D	74 0.57	W W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	- 65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.75	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0, I_D = 1.0 \mu\text{A dc}$)	$V_{(BR)DSS}$	65	-	-	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ V}, V_{GS} = 0$)	I_{DSS}	-	-	1	$\mu\text{A dc}$
Gate-Source Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	-	-	1	$\mu\text{A dc}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

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ELECTRICAL CHARACTERISTICS – continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 100\ \mu\text{A}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ V}$, $I_D = 50\text{ mA}$)	$V_{GS(Q)}$	3	4	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 3\text{ A}$)	$V_{DS(on)}$	–	0.9	1.2	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 3\text{ A}$)	g_{fs}	1.6	1.8	–	S

DYNAMIC CHARACTERISTICS

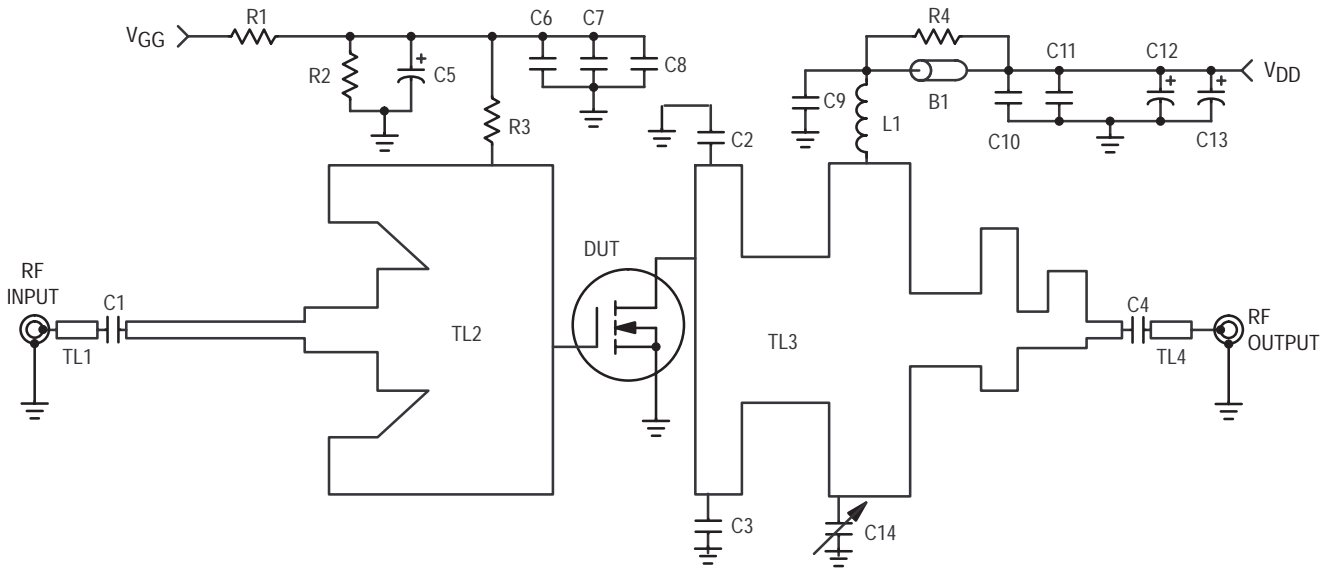
Input Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	–	56	–	pF
Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	–	28	–	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	–	2.5	–	pF

FUNCTIONAL CHARACTERISTICS

Common Source Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W}$, $I_{DQ} = 50\text{ mA}$, $f = 945\text{ MHz}$)	G_{ps}	11	14	–	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W}$, $I_{DQ} = 50\text{ mA}$, $f = 945\text{ MHz}$)	η	50	58	–	%
Load Mismatch ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W}$, $I_{DQ} = 50\text{ mA}$, $f = 945\text{ MHz}$, Load VSWR 5:1 at All Phase Angles)	Ψ	No Degradation in Output Power			
Series Equivalent Input Impedance ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W}$, $I_{DQ} = 50\text{ mA}$, $f = 960\text{ MHz}$)	Z_{in}	–	$0.81 + j1.6$	–	ohms
Series Equivalent Output Impedance ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W}$, $I_{DQ} = 50\text{ mA}$, $f = 960\text{ MHz}$)	Z_{out}	–	$2.15 - j1.7$	–	ohms

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B1	Short RF Bead Fair Rite-274301944	L1	5 Turns, 20 AWG, IDIA 0.126
C1	18 pF Chip Capacitor	R1	10 kΩ, 1/4 W Resistor
C2, C3, C6, C9	43 pF Chip Capacitor	R2	13 kΩ, 1/4 W Resistor
C4	100 pF Chip Capacitor	R3	1.0 kΩ, 1/4 W Chip Resistor
C5, C12	10 μF, 50 Vdc Electrolytic Capacitor	R4	4 x 39 Ω, 1/8 W Chip Resistor
C7, C10	1000 pF Chip Capacitor	TL1-TL4	Microstrip Line See Photomaster
C8, C11	0.1 μF, 50 Vdc Chip Capacitor	Ckt Board	1/32" Glass Teflon, ε _r = 2.55
C13	250 μF, 50 Vdc Electrolytic Capacitor		ARLON-GX-0300-55-22
C14	0.6-4.5 pF Variable Capacitor		

Figure 1. MRF182 Schematic

TYPICAL CHARACTERISTICS

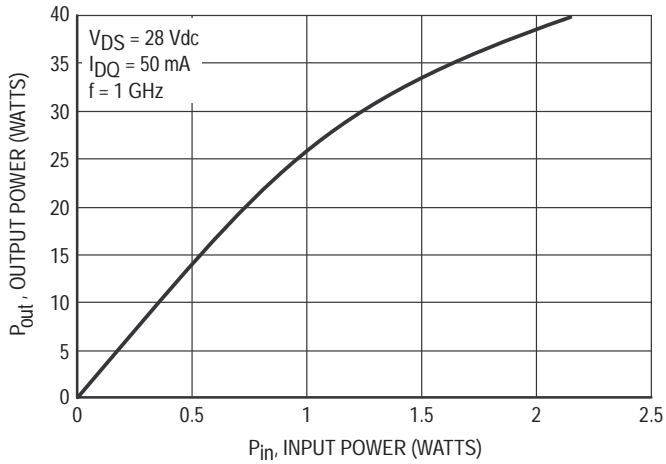


Figure 2. Output Power versus Input Power at 1 GHz

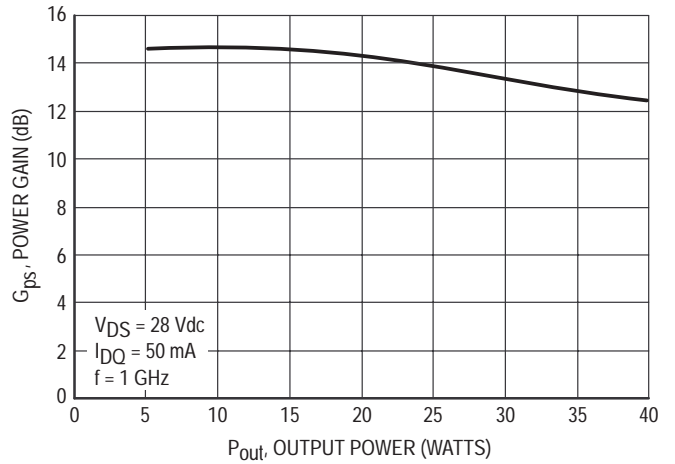


Figure 3. Power Gain versus Output Power at 1 GHz

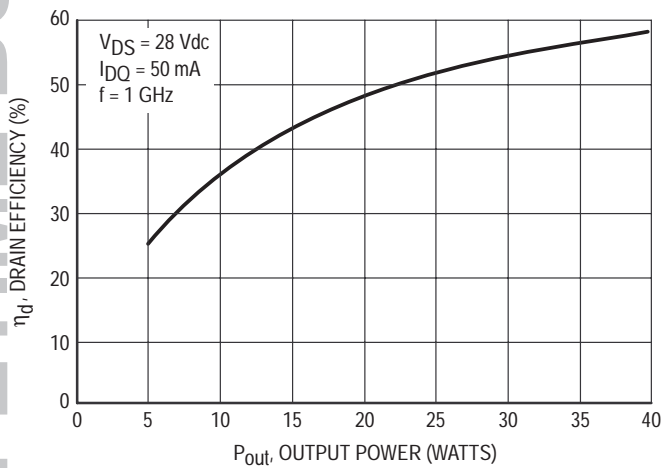


Figure 4. Drain Efficiency versus Output Power at 1 GHz

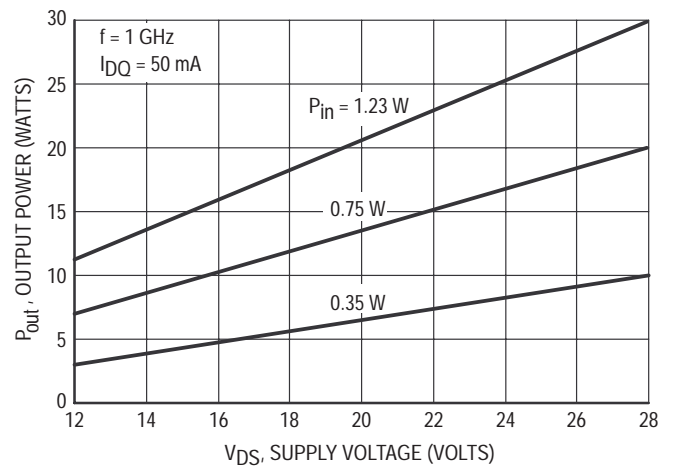


Figure 5. Output Power versus Supply Voltage

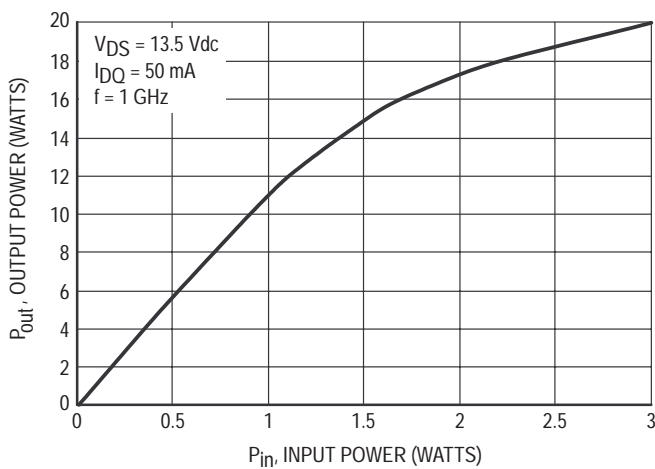


Figure 6. Output Power versus Input Power

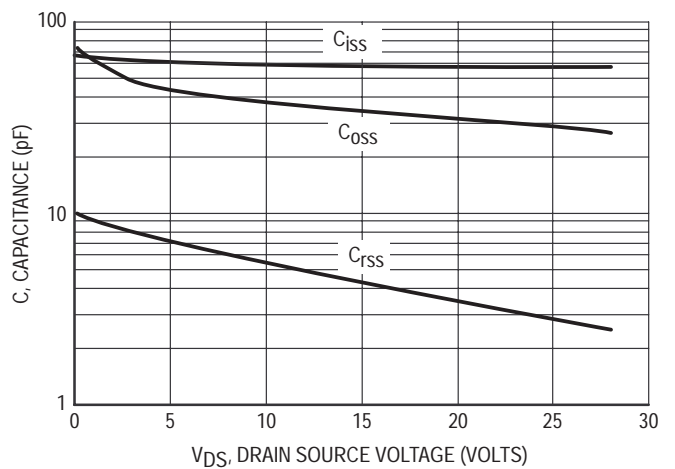


Figure 7. Capacitance versus Drain Source Voltage

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Table 1. Typical Common Source S-Parameters ($V_{DS} = 13.5\text{ V}$)

$I_D = 1.0\text{ A}$

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	∠	S ₂₁	∠	S ₁₂	∠	S ₂₂	∠
20	0.933	-131	40.81	112	0.021	22	0.664	-138
30	0.922	-148	29.31	104	0.022	15	0.700	-151
40	0.892	-156	22.19	99	0.022	10	0.718	-158
50	0.877	-161	17.91	95	0.023	7	0.725	-162
60	0.870	-164	14.67	92	0.023	4	0.732	-164
70	0.863	-166	12.57	90	0.022	2	0.735	-166
80	0.860	-168	11.00	89	0.022	1	0.738	-168
90	0.860	-169	9.79	87	0.022	0	0.740	-169
100	0.859	-170	8.79	86	0.022	-1	0.741	-169
150	0.859	-173	5.78	80	0.022	-7	0.750	-172
200	0.862	-175	4.29	74	0.022	-11	0.759	-172
250	0.868	-176	3.38	69	0.021	-14	0.770	-173
300	0.880	-177	2.77	65	0.020	-17	0.780	-173
350	0.877	-177	2.32	61	0.020	-19	0.793	-173
400	0.882	-178	1.98	56	0.019	-22	0.808	-173
450	0.892	-179	1.72	52	0.018	-24	0.816	-173
500	0.899	-180	1.51	49	0.017	-26	0.828	-174
550	0.898	180	1.33	45	0.017	-27	0.838	-174
600	0.907	179	1.19	42	0.016	-28	0.849	-175
650	0.914	179	1.07	38	0.015	-28	0.859	-175
700	0.916	177	0.95	35	0.014	-25	0.867	-176
750	0.920	177	0.88	34	0.015	-26	0.874	-176
800	0.924	176	0.80	30	0.015	-27	0.884	-177
850	0.929	175	0.74	27	0.015	-33	0.891	-178
900	0.929	174	0.68	25	0.013	-38	0.897	-178
950	0.933	173	0.63	22	0.011	-39	0.905	-179
1000	0.934	173	0.58	20	0.010	-37	0.912	-180
1050	0.930	172	0.54	17	0.009	-33	0.918	180
1100	0.938	171	0.52	15	0.009	-29	0.924	179
1150	0.933	170	0.48	13	0.008	-28	0.929	178
1200	0.930	169	0.45	10	0.008	-25	0.930	177
1250	0.939	168	0.42	8	0.007	-23	0.935	177
1300	0.936	168	0.40	6	0.007	-21	0.934	176
1350	0.933	167	0.38	4	0.006	-19	0.936	175
1400	0.937	166	0.35	2	0.005	-14	0.939	174
1450	0.937	165	0.33	0	0.005	-5	0.934	174
1500	0.927	164	0.32	-2	0.004	0	0.930	173

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Table 2. Typical Common Emitter S-Parameters ($V_{DS} = 28\text{ V}$)

$I_D = 1.0\text{ A}$

f MHz	S11		S21		S12		S22	
	S11	ϕ	S21	ϕ	S12	ϕ	S22	ϕ
20	0.964	-99	54.39	129	0.014	39	0.429	-108
30	0.949	-121	43.46	118	0.017	28	0.478	-125
40	0.909	-134	34.35	109	0.018	20	0.520	-137
50	0.884	-142	28.27	103	0.018	15	0.540	-144
60	0.875	-148	23.38	98	0.019	11	0.553	-149
70	0.862	-152	20.10	95	0.019	8	0.562	-152
80	0.861	-156	17.64	92	0.019	5	0.569	-154
90	0.858	-158	15.72	90	0.019	3	0.575	-156
100	0.858	-160	14.11	88	0.019	1	0.580	-157
150	0.856	-166	9.26	79	0.018	-7	0.606	-160
200	0.862	-169	6.80	71	0.018	-12	0.633	-161
250	0.871	-171	5.29	65	0.017	-16	0.661	-161
300	0.882	-173	4.27	59	0.016	-21	0.690	-162
350	0.883	-174	3.52	54	0.015	-23	0.718	-162
400	0.895	-175	2.97	49	0.014	-26	0.747	-163
450	0.904	-176	2.54	45	0.013	-28	0.767	-164
500	0.911	-177	2.20	41	0.012	-30	0.789	-165
550	0.911	-178	1.90	37	0.011	-30	0.807	-166
600	0.923	-179	1.69	33	0.010	-30	0.825	-167
650	0.929	-180	1.50	30	0.009	-29	0.841	-168
700	0.929	179	1.32	26	0.009	-22	0.855	-169
750	0.933	178	1.21	24	0.010	-22	0.865	-170
800	0.938	177	1.09	21	0.009	-20	0.877	-171
850	0.942	176	1.00	18	0.010	-31	0.886	-172
900	0.942	175	0.92	16	0.008	-37	0.894	-173
950	0.947	174	0.84	13	0.006	-38	0.904	-174
1000	0.946	173	0.77	11	0.005	-28	0.912	-175
1050	0.943	172	0.72	8	0.005	-18	0.919	-176
1100	0.948	171	0.67	6	0.004	-9	0.926	-177
1150	0.945	171	0.62	4	0.005	0	0.932	-178
1200	0.939	170	0.59	1	0.004	3	0.934	-179
1250	0.949	169	0.54	0	0.005	12	0.940	-180
1300	0.947	168	0.51	-3	0.005	18	0.939	180
1350	0.944	167	0.48	-4	0.005	22	0.941	179
1400	0.945	166	0.44	-7	0.004	34	0.943	178
1450	0.944	165	0.42	-9	0.005	45	0.940	177
1500	0.933	164	0.40	-10	0.005	55	0.936	176

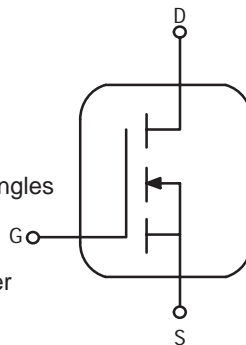
LIFETIME BUY

LAST ORDER 31JUL04 LAST SHIP 31JAN05

The RF MOSFET Line
RF Power
Field Effect Transistors
N-Channel Enhancement-Mode Lateral
MOSFETs

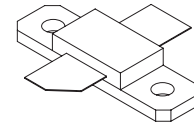
Designed for broadband commercial and industrial applications at frequencies to 1.0 GHz. The high gain and broadband performance of these devices makes them ideal for large-signal, common source amplifier applications in 28 volt base station equipment.

- Guaranteed Performance at 945 MHz, 28 Volts
Output Power — 45 Watts PEP
Power Gain — 11.5 dB
Efficiency — 33%
IMD — -28 dBc
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- S-Parameter Characterization at High Bias Levels
- Excellent Thermal Stability
- 100% Tested for Load Mismatch Stress at all Phase Angles with 5:1 VSWR @ 28 Vdc, 945 MHz, 45 Watts CW
- MRF183S Available in Tape and Reel by Adding R1 Suffix to Part Number. MRF183SR1 = 500 Units per 24 mm, 13 inch Reel.

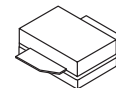


MRF183
MRF183S
MRF183SR1

1.0 GHz, 45 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 360B-03, STYLE 1
(MRF183)



CASE 360C-03, STYLE 1
(MRF183S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage (RGS = 1 Meg Ohm)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current - Continuous	I_D	5	Adc
Total Device Dissipation @ $T_C = 70^\circ\text{C}$ Derate above 70°C	P_D	86 0.67	W W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.5	$^\circ\text{C/W}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 50 \mu\text{Adc}$)	BV_{DSS}	65	–	–	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ V}, V_{GS} = 0$)	I_{DSS}	–	–	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	–	–	1	μAdc

ON CHARACTERISTICS

Gate Quiescent Voltage ($V_{DS} = 28 \text{ Vdc}, I_D = 250 \text{ mAdc}$)	$V_{GS(Q)}$	3	–	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 3 \text{ A}$)	$V_{DS(on)}$	–	0.7	–	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ Vdc}, I_D = 5 \text{ Adc}$)	g_{fs}	–	2	–	S

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1 \text{ MHz}$)	C_{iss}	–	82	–	pF
Output Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1 \text{ MHz}$)	C_{oss}	–	38	–	pF
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1 \text{ MHz}$)	C_{rss}	–	4.5	–	pF

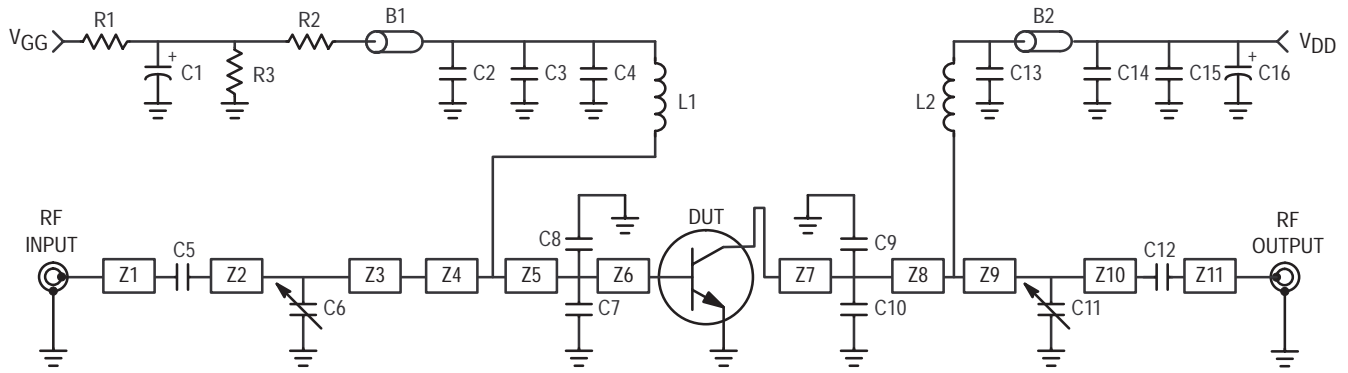
FUNCTIONAL TESTS (In Motorola Test Fixture)

($V_{DD} = 28 \text{ Vdc}, P_{out} = 45 \text{ Watts PEP}, f_1 = 945.0, f_2 = 945.1 \text{ MHz}, I_{DQ} = 250 \text{ mA}$)

Two–Tone Common Source Amplifier Power Gain	G_{ps}	11.5	13.5	–	dB
Two–Tone Drain Efficiency	η	33	38	–	%
3rd Order Intermodulation Distortion	IMD	–	–32	–28	dBc
Input Return Loss	IRL	9	14	–	dB

($V_{DD} = 28 \text{ Vdc}, P_{out} = 45 \text{ Watts PEP}, f_1 = 930.0, f_2 = 930.1 \text{ MHz}, \text{ and } f_1 = 960.0, f_2 = 960.1 \text{ MHz}, I_{DQ} = 250 \text{ mA}$)

Two–Tone Common Source Amplifier Power Gain	G_{ps}	–	13	–	dB
Two–Tone Drain Efficiency	η	–	35	–	%
3rd Order Intermodulation Distortion	IMD	–	–32	–	dBc
Input Return Loss	IRL	–	12	–	dB
Output Mismatch Stress ($V_{DD} = 28 \text{ Vdc}, P_{out} = 45 \text{ Watts CW}, I_{DQ} = 250 \text{ mA}, f = 945 \text{ MHz}, \text{ VSWR } 5:1 \text{ at All Phase Angles}$)	Ψ	No Degradation in Output Power Before and After Test			



B1	Short Ferrite Bead	R3	4.7 M Ω , 1/4 W Carbon
B2	Long Ferrite Bead	Z1	T-Line, 0.200" x 0.080"
C1	10 μ F, 50 V Electrolytic Capacitor	Z2	T-Line, 0.570" x 0.120"
C2, C14	0.1 μ F Chip Capacitor	Z3	T-Line, 0.610" x 0.320"
C3	1000 pF Chip Capacitor	Z4	T-Line, 0.160" x 0.320" x 0.620"
C4, C13	47 pF Chip Capacitor	Z5	Tapered Line
C5, C12	47 pF Chip Capacitor	Z6	T-Line, 0.650" x 0.620"
C6, C11	0.8–8.0 pF Trim Capacitor	Z7	T-Line, 0.020" x 0.620"
C7, C8	10 pF Chip Capacitor	Z8	T-Line, 0.270" x 0.320"
C9, C10	10 pF Chip Capacitor	Z9	T-Line, 0.130" x 0.320"
C15	100 pF Chip Capacitor	Z10	T-Line, 0.370" x 0.080"
C16	250 μ F, 50 V Electrolytic Capacitor	Z11	T-Line, 1.050" x 0.080"
L1, L2	5 Turns, 24 AWG, ID 0.059"	Board	T-Line, 0.290" x 0.080"
R1	120 Ω , 1/4 W Carbon		0.030" Glass Teflon, $\epsilon_r = 2.55$
R2	18 k Ω , 1/4 W Carbon		ARLON-GX-0300-55-22

Figure 1. MRF183S Two Tone Test Circuit Schematic

TYPICAL CHARACTERISTICS

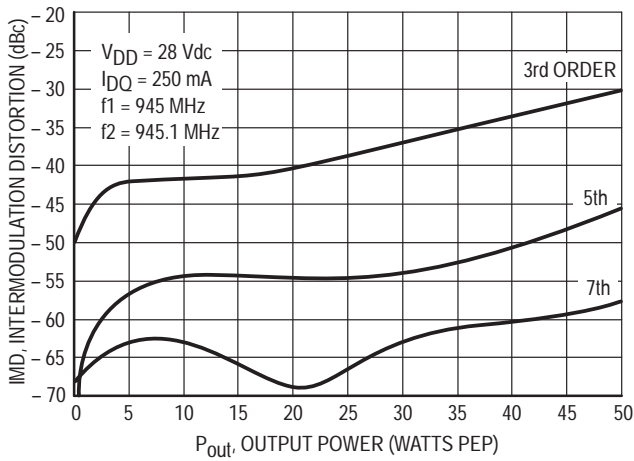


Figure 2. Intermodulation Distortion Products versus Output Power

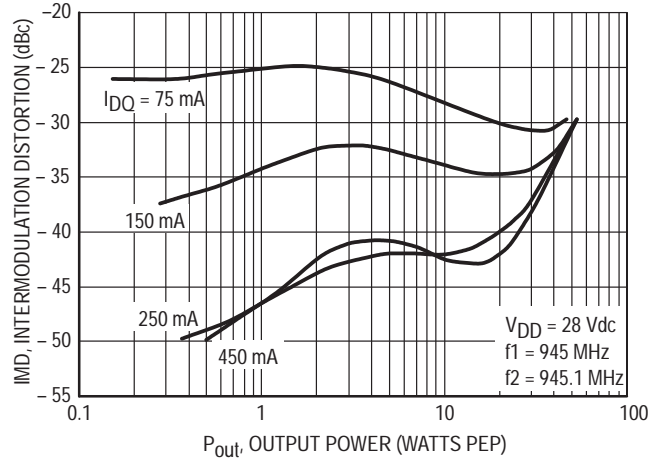


Figure 3. Intermodulation Distortion versus Output Power

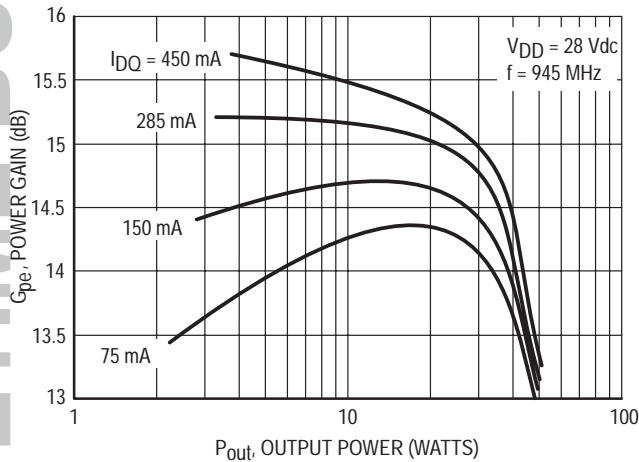


Figure 4. Power Gain versus Output Power

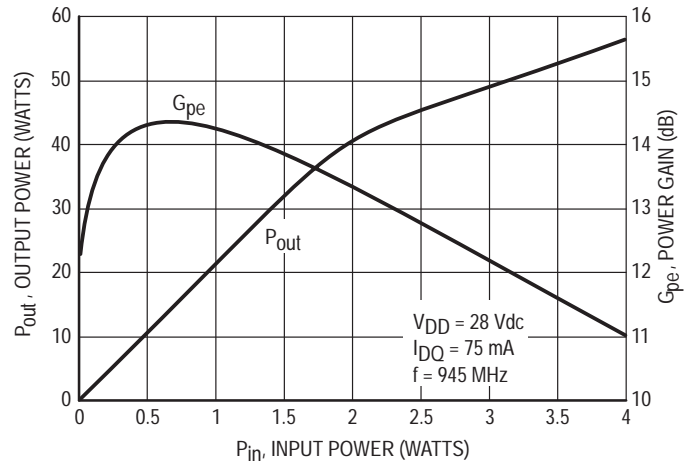


Figure 5. Output Power versus Input Power

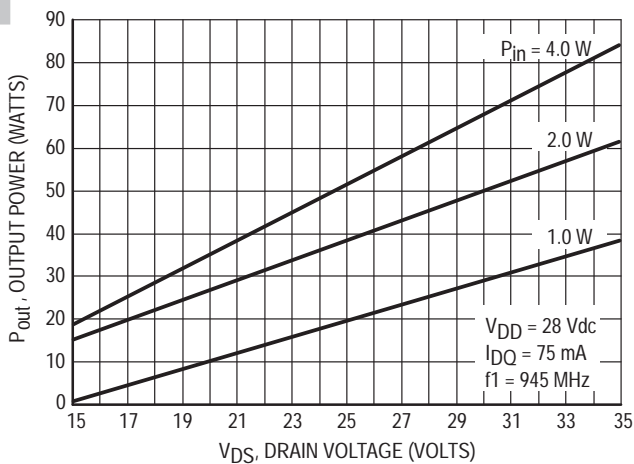


Figure 6. Output Power versus Drain Bias Supply Voltage

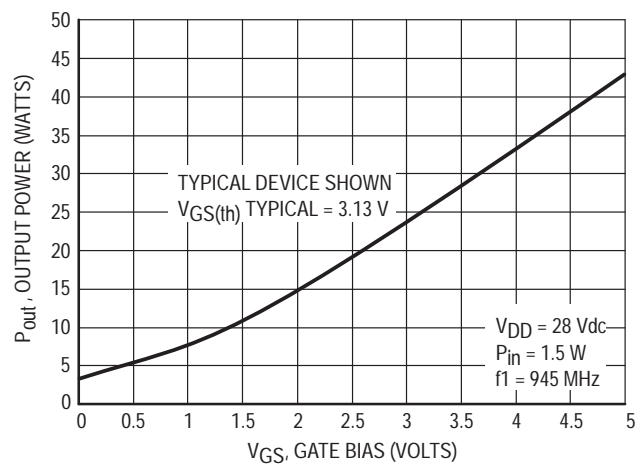


Figure 7. Output Power versus Gate Bias Supply Voltage

LIFETIME BUY

LAST ORDER 31JUL04 LAST SHIP 31JAN05

TYPICAL CHARACTERISTICS

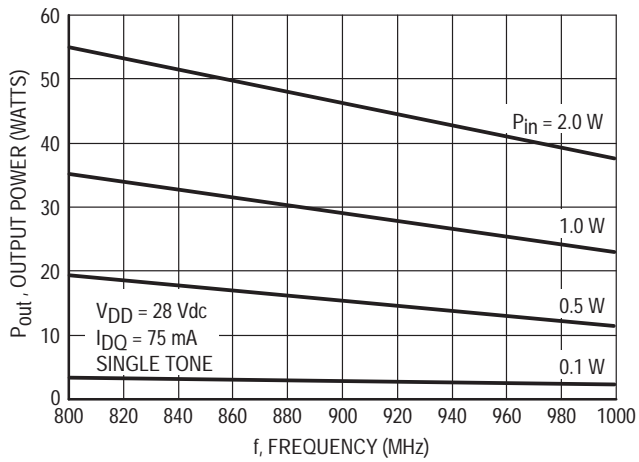


Figure 8. Output Power versus Frequency

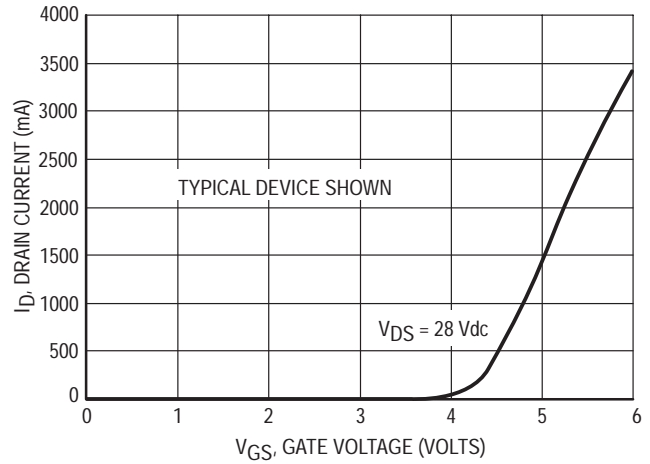


Figure 9. Drain Current versus Gate Voltage

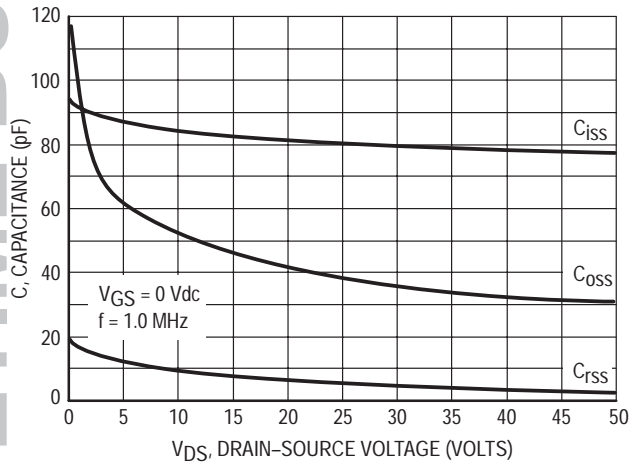


Figure 10. Capacitance versus Voltage

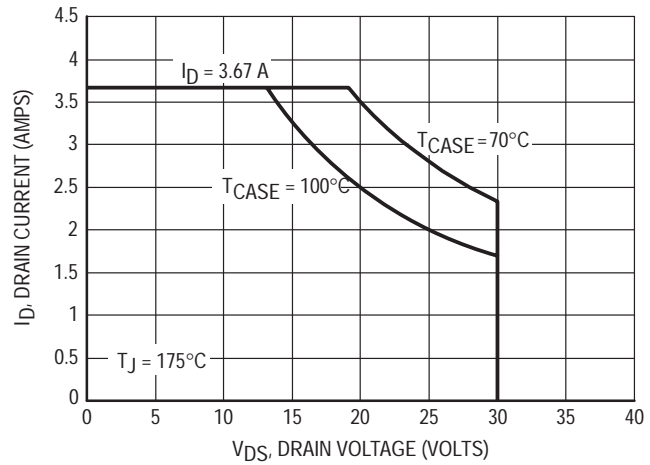


Figure 11. Class A Safe Operating Region

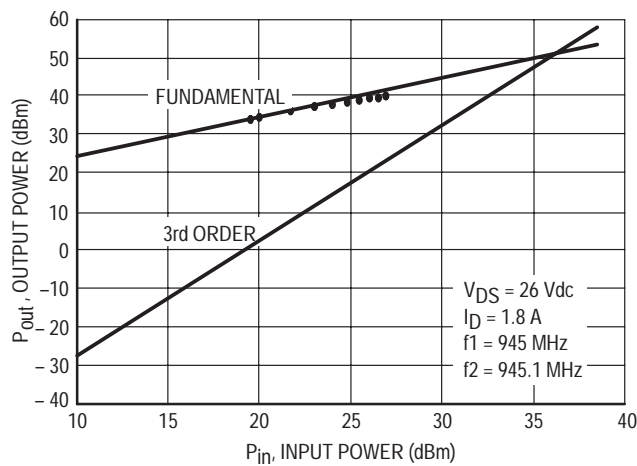


Figure 12. Class A Third Order Intercept Point

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

LIFETIME BUY

LAST ORDER 31JUL04 LAST SHIP 31JAN05

TYPICAL CHARACTERISTICS

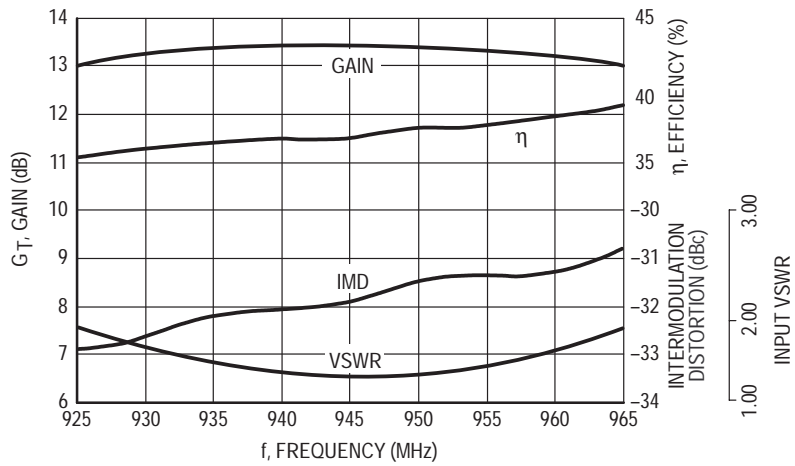


Figure 13. Broadband Power Performance of MRF183S

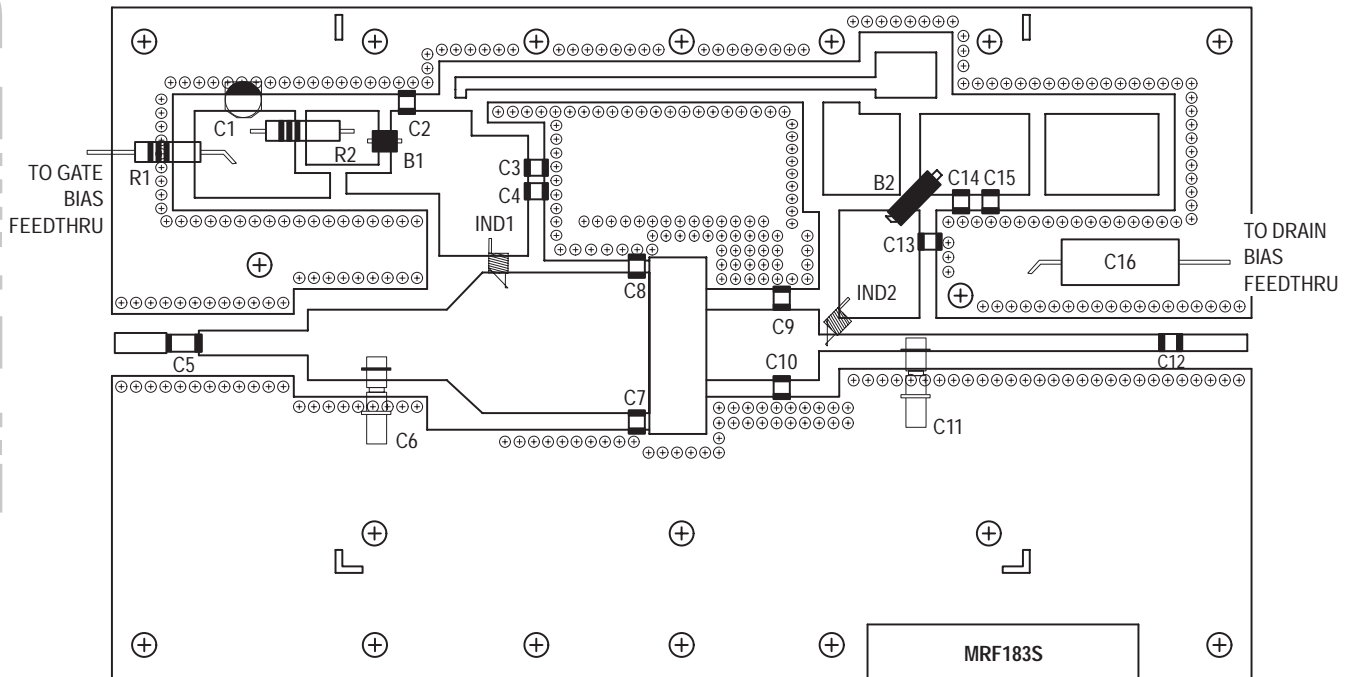
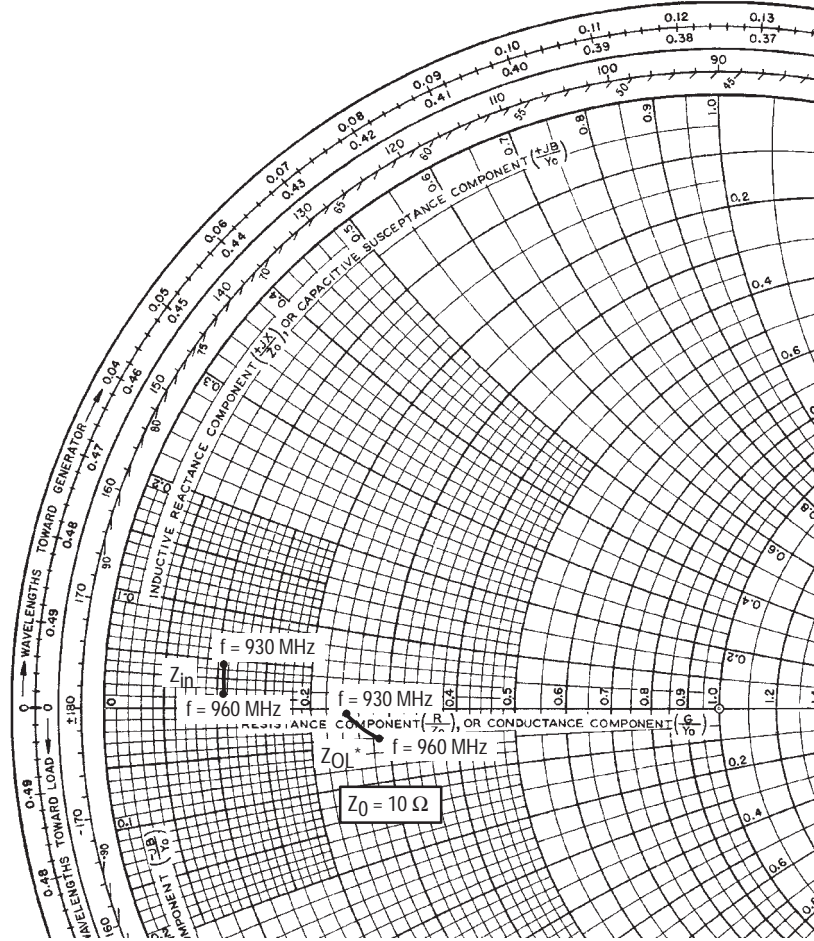


Figure 14. MRF183S Two Tone Test Circuit Component Parts Layout



$V_{DD} = 28\text{ V}$, $I_{DQ} = 250\text{ mA}$, $P_{out} = 45\text{ W (PEP)}$

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
930	$1.10 + j0.93$	$2.60 - j0.13$
945	$1.10 + j0.78$	$2.70 - j0.28$
960	$1.10 + j0.60$	$2.80 - j0.42$

Z_{in} = Conjugate of source impedance.

Z_{OL}^* = Conjugate of the load impedance at a given output power, voltage, and current conditions.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

Figure 15. Series Equivalent Input and Output Impedance

Table 1. Typical Common Source S-Parameters ($V_{DS} = 13.5\text{ V}$)

$I_D = 1.5\text{ A}$

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
20	0.954	-157	29.58	100	0.017	11	0.778	-161
30	0.941	-164	19.73	96	0.017	8	0.796	-168
40	0.922	-168	14.84	93	0.017	4	0.804	-170
50	0.907	-171	11.94	91	0.017	3	0.808	-172
60	0.903	-172	9.75	89	0.017	2	0.812	-173
70	0.899	-173	8.34	88	0.017	0	0.814	-174
80	0.898	-174	7.29	86	0.017	-1	0.816	-175
90	0.896	-175	6.49	85	0.017	-2	0.816	-175
100	0.897	-175	5.83	84	0.017	-2	0.817	-175
150	0.895	-177	3.82	79	0.017	-6	0.822	-176
200	0.898	-178	2.84	74	0.016	-9	0.828	-176
250	0.902	-178	2.24	70	0.016	-11	0.835	-176
300	0.908	-179	1.84	66	0.015	-14	0.842	-176
350	0.905	-179	1.55	62	0.015	-16	0.850	-176
400	0.913	-180	1.32	58	0.014	-18	0.861	-176
450	0.920	180	1.15	54	0.014	-18	0.865	-176
500	0.924	179	1.01	51	0.013	-20	0.874	-177
550	0.922	179	0.89	47	0.013	-21	0.881	-177
600	0.931	178	0.80	44	0.012	-21	0.889	-177
650	0.935	178	0.72	41	0.011	-20	0.895	-177
700	0.935	177	0.64	38	0.011	-17	0.901	-178
750	0.937	177	0.59	37	0.012	-18	0.905	-178
800	0.940	176	0.54	33	0.012	-20	0.913	-178
850	0.943	176	0.50	30	0.012	-29	0.919	-179
900	0.945	175	0.46	28	0.010	-33	0.924	-179
950	0.947	174	0.43	26	0.009	-34	0.930	-180
1000	0.947	174	0.40	24	0.008	-29	0.935	180
1050	0.947	173	0.37	21	0.007	-24	0.939	179
1100	0.952	172	0.35	19	0.007	-19	0.944	179
1150	0.949	172	0.32	17	0.007	-17	0.948	178
1200	0.946	171	0.30	14	0.006	-16	0.948	177
1250	0.954	170	0.28	12	0.006	-13	0.953	177
1300	0.952	170	0.27	9	0.006	-12	0.950	176
1350	0.949	169	0.26	9	0.006	-10	0.951	176
1400	0.948	168	0.23	8	0.005	-7	0.953	175
1450	0.948	168	0.22	6	0.004	4	0.948	174
1500	0.940	167	0.21	4	0.004	19	0.944	174

LIFETIME BUY

LAST ORDER 31JUL04 LAST SHIP 31JAN05

Table 2. Typical Common Source S-Parameters ($V_{DS} = 28\text{ V}$)

$I_D = 1.5\text{ A}$

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
20	0.968	-132	45.79	113	0.014	24	0.579	-145
30	0.953	-145	31.75	106	0.015	17	0.623	-157
40	0.921	-154	24.33	99	0.015	12	0.648	-161
50	0.904	-159	19.68	95	0.015	7	0.661	-164
60	0.898	-163	16.11	92	0.015	5	0.670	-166
70	0.890	-165	13.79	90	0.015	2	0.677	-167
80	0.886	-167	12.06	87	0.015	1	0.681	-168
90	0.886	-168	10.71	86	0.015	-1	0.684	-169
100	0.887	-169	9.61	84	0.015	-3	0.688	-169
150	0.886	-172	6.26	76	0.015	-9	0.706	-170
200	0.890	-174	4.59	69	0.014	-13	0.724	-170
250	0.898	-175	3.57	64	0.014	-17	0.744	-169
300	0.906	-176	2.88	59	0.013	-19	0.764	-169
350	0.908	-177	2.37	54	0.012	-23	0.785	-169
400	0.915	-178	2.00	49	0.011	-24	0.807	-170
450	0.924	-178	1.71	45	0.010	-25	0.821	-170
500	0.930	-179	1.48	41	0.010	-26	0.838	-171
550	0.928	-180	1.28	37	0.009	-26	0.851	-171
600	0.937	180	1.13	33	0.008	-25	0.865	-172
650	0.944	179	1.00	30	0.007	-22	0.878	-172
700	0.943	178	0.88	27	0.008	-14	0.888	-173
750	0.946	178	0.81	25	0.008	-15	0.895	-173
800	0.949	177	0.73	22	0.009	-17	0.906	-174
850	0.954	177	0.67	20	0.009	-28	0.912	-175
900	0.953	175	0.61	18	0.007	-34	0.919	-175
950	0.957	175	0.56	15	0.005	-32	0.927	-176
1000	0.957	174	0.51	13	0.004	-22	0.934	-177
1050	0.957	174	0.48	10	0.004	-11	0.939	-178
1100	0.962	173	0.45	8	0.004	-2	0.945	-178
1150	0.959	172	0.41	7	0.004	3	0.950	-179
1200	0.955	171	0.39	4	0.004	9	0.950	-180
1250	0.962	170	0.36	2	0.004	13	0.955	180
1300	0.959	170	0.33	0	0.004	17	0.953	179
1350	0.956	169	0.31	-1	0.004	25	0.954	178
1400	0.954	168	0.29	-4	0.004	32	0.957	177
1450	0.955	168	0.28	-6	0.004	46	0.952	177
1500	0.948	167	0.26	-7	0.004	56	0.948	176

LIFETIME BUY

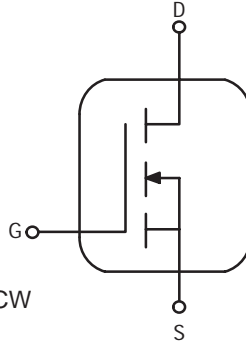
LAST SHIP 31JAN05
LAST ORDER 31JUL04

The RF MOSFET Line
RF POWER Field-Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

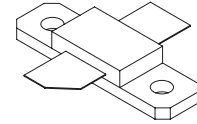
MRF184
MRF184S, R1

Designed for broadband commercial and industrial applications at frequencies to 1.0 GHz. The high gain and broadband performance of these devices makes them ideal for large-signal, common source amplifier applications in 28 volt base station equipment.

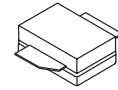
- Guaranteed Performance @ 945 MHz, 28 Volts
Output Power = 60 Watts
Power Gain = 11.5 dB
Efficiency = 53%
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- S-Parameter Characterization at High Bias Levels
- Excellent Thermal Stability
- 100% Tested for Load Mismatch Stress at all Phase Angles with 5:1 VSWR @ 28 Vdc, 945 MHz, 60 Watts CW
- MRF184S Available in Tape and Reel by Adding R1 Suffix to Part Number. MRF184SR1 = 500 Units per 24 mm, 13 inch Reel.



60 W, 1.0 GHz
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 360B-03, STYLE 1
(MRF184)



CASE 360C-03, STYLE 1
(MRF184S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current — Continuous	I_D	7	Adc
Total Device Dissipation @ $T_C = 70^\circ\text{C}$ Derate above 70°C	P_D	118 0.9	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	- 65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.1	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0\text{ V}$, $I_D = 1\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	-	-	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	-	-	1	μAdc
Gate-Source Leakage Current ($V_{GS} = 20\text{ V}$, $V_{DS} = 0\text{ V}$)	I_{GSS}	-	-	1	μAdc

NOTE - CAUTION - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS – continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

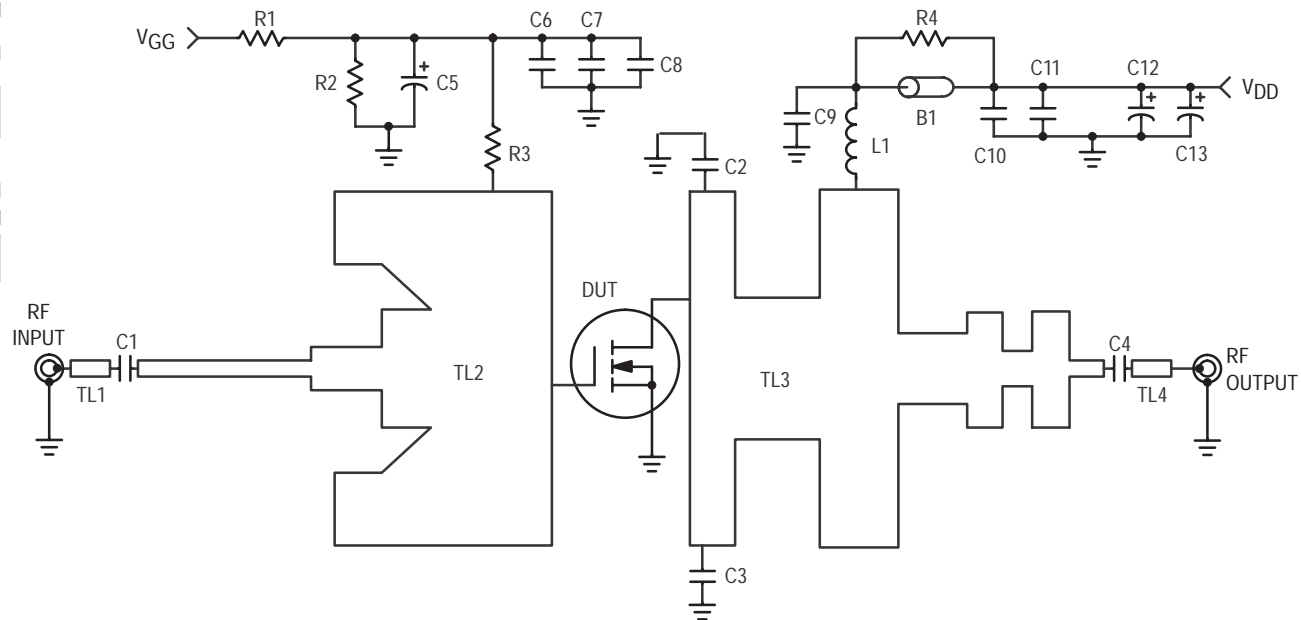
Characteristic	Symbol	Min	Typ	Max	Unit
Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 200\ \mu\text{A}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$)	$V_{GS(Q)}$	3	4	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 3\text{ A}$)	$V_{DS(on)}$	–	0.65	0.8	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 3\text{ A}$)	g_{fs}	2.2	2.6	–	s

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{iss}	–	83	–	pF
Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{oss}	–	44	–	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{rss}	–	4.3	–	pF

FUNCTIONAL CHARACTERISTICS

Common Source Power Gain ($V_{DD} = 28\text{ V}$, $P_{out} = 60\text{ W}$, $f = 945\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	G_{ps}	11.5	13.5	–	dB
Drain Efficiency ($V_{DD} = 28\text{ V}$, $P_{out} = 60\text{ W}$, $f = 945\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	η	53	60	–	%
Load Mismatch ($V_{DD} = 28\text{ V}$, $P_{out} = 60\text{ W}$, $I_{DQ} = 100\text{ mA}$, $f = 945\text{ MHz}$, Load VSWR 5:1 at all Phase Angles)	ψ	No Degradation in Output Power			



- | | | | |
|----------------|---|-----------|---|
| B1 | Short RF Bead Fair Rite–2743019447 | L1 | 5 Turns, 20 AWG, IDIA 0.126" |
| C1 | 18 pF Chip Capacitor | R1 | 10 k Ω , 1/4 W Resistor |
| C2, C3, C6, C9 | 43 pF Chip Capacitor | R2 | 13 k Ω , 1/4 W Resistor |
| C4 | 100 pF Chip Capacitor | R3 | 1.0 k Ω , 1/4 W Chip Resistor |
| C5, C12 | 10 μF , 50 Vdc Electrolytic Capacitor | R4 | 4 x 39 Ω , 1/8 W Chip Resistor |
| C7, C10 | 1000 pF Chip Capacitor | TL1–TL4 | Microstrip Line See Photomaster |
| C8, C11 | 0.1 μF , 50 Vdc Chip Capacitor | Ckt Board | 1/32" Glass Teflon, $\epsilon_r = 2.55$ |
| C13 | 250 μF , 50 Vdc Electrolytic Capacitor | | ARLON–GX–0300–55–22 |

Figure 1. MRF184 Test Circuit Schematic

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LAST SHIP 31JAN05
LAST ORDER 31JUL04

TYPICAL CHARACTERISTICS

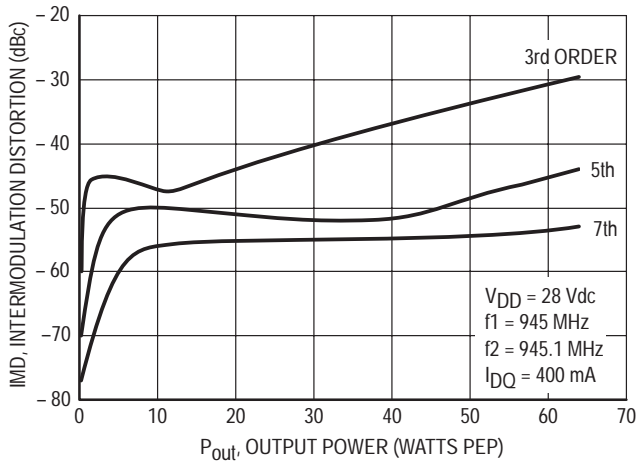


Figure 2. Intermodulation Distortion Products versus Output Power

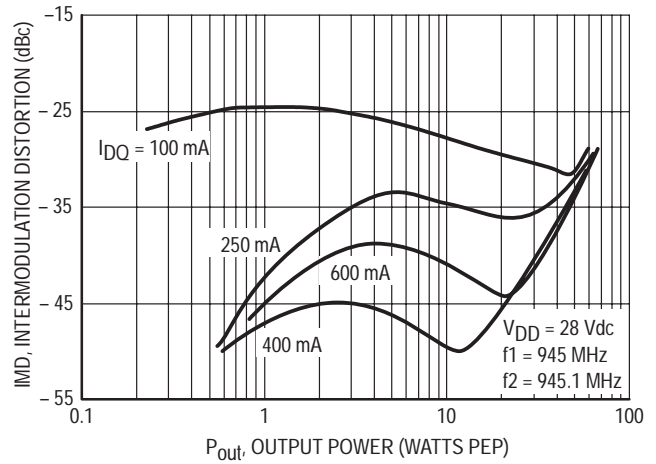


Figure 3. Intermodulation Distortion versus Output Power

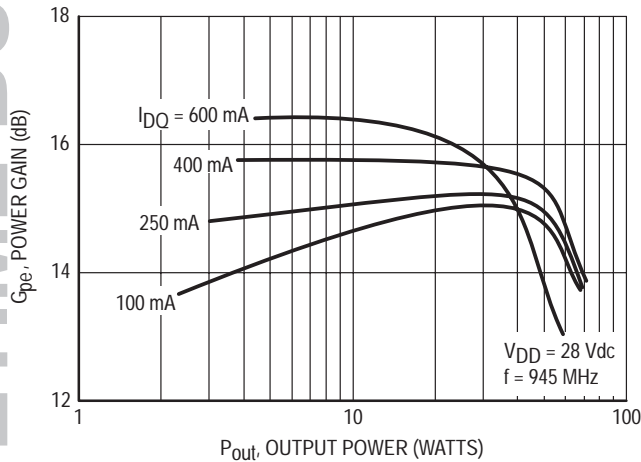


Figure 4. Power Gain versus Output Power

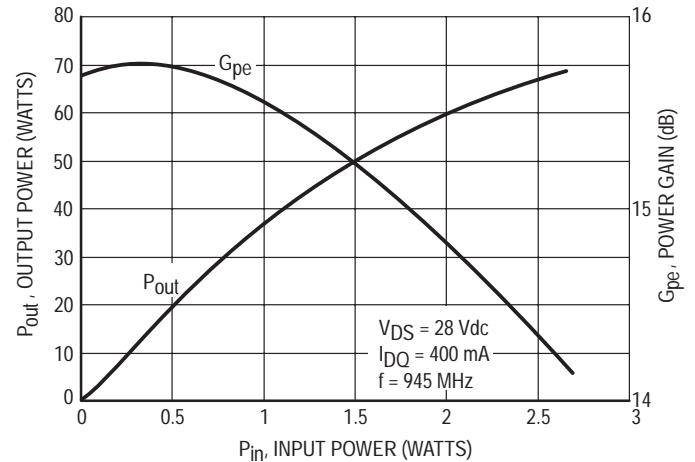


Figure 5. Output Power versus Input Power

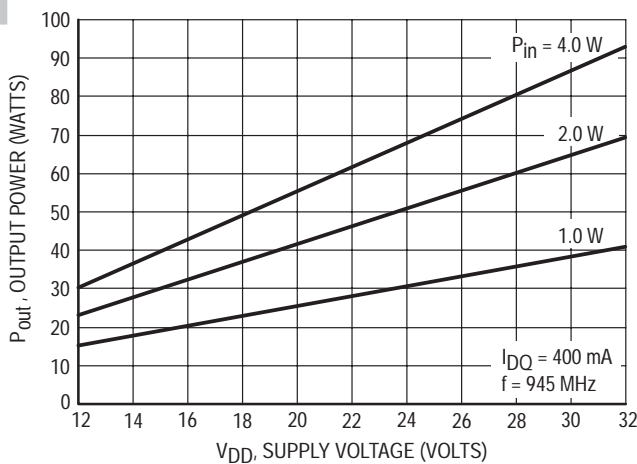


Figure 6. Output Power versus Supply Voltage

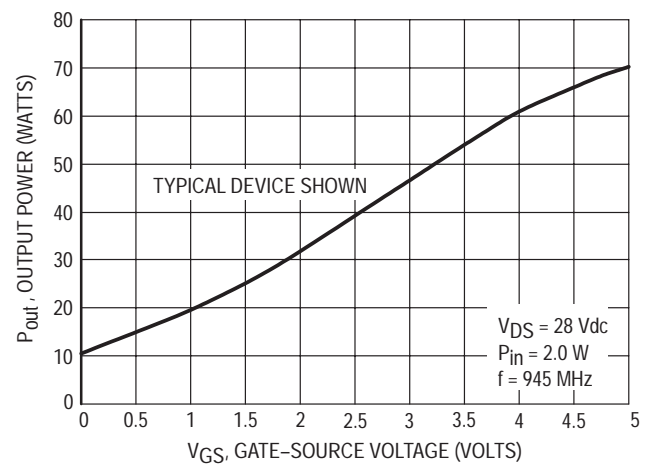


Figure 7. Output Power versus Gate Voltage

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LAST ORDER 31JUL04 LAST SHIP 31JAN05

TYPICAL CHARACTERISTICS

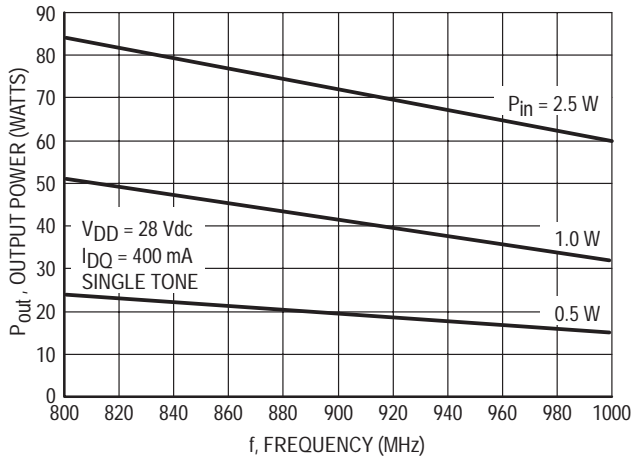


Figure 8. Output Power versus Frequency

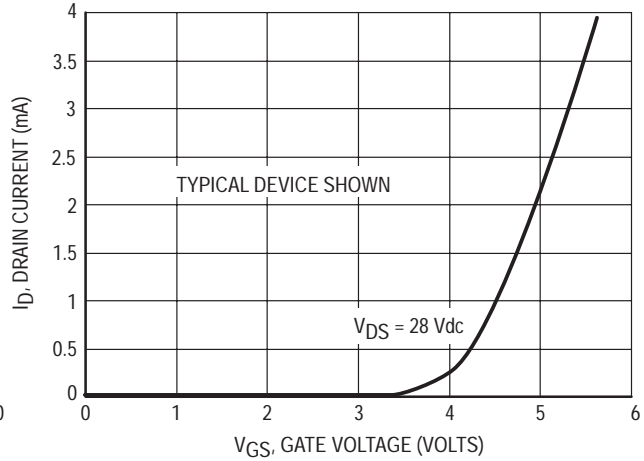


Figure 9. Drain Current versus Gate Voltage

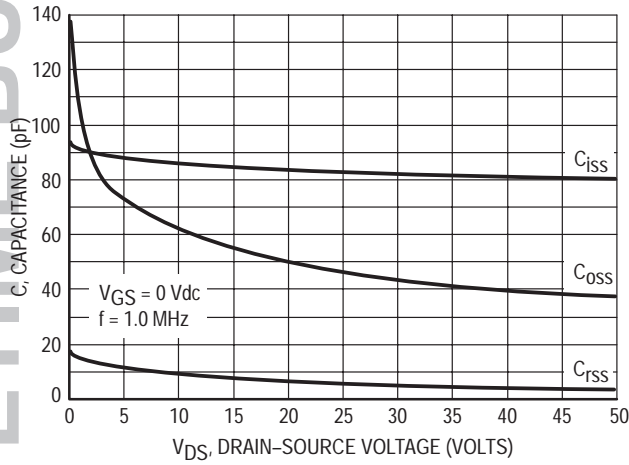


Figure 10. Capacitance versus Voltage

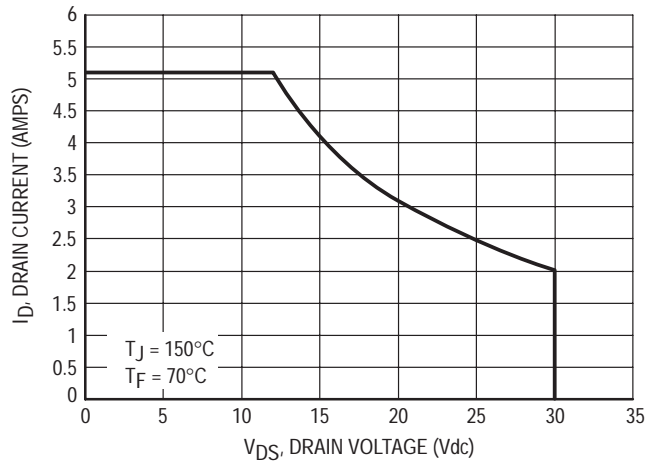


Figure 11. DC Safe Operating Area

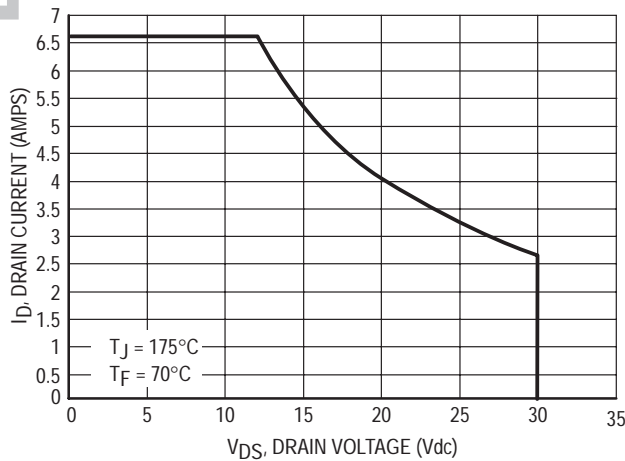


Figure 12. DC Safe Operating Area

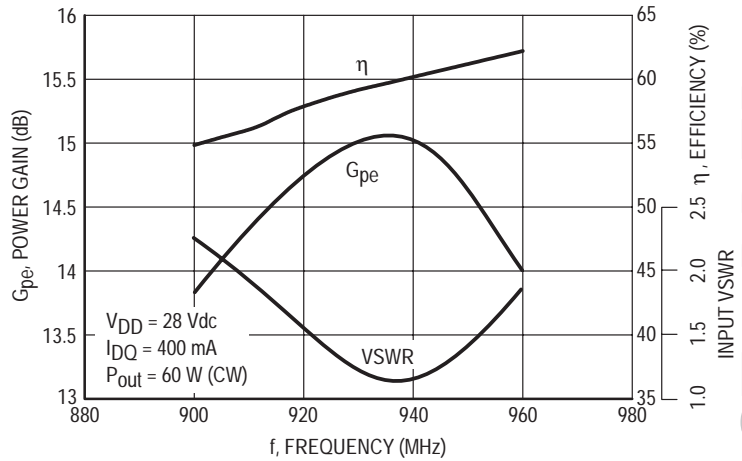


Figure 13. Performance in Broadband Circuit

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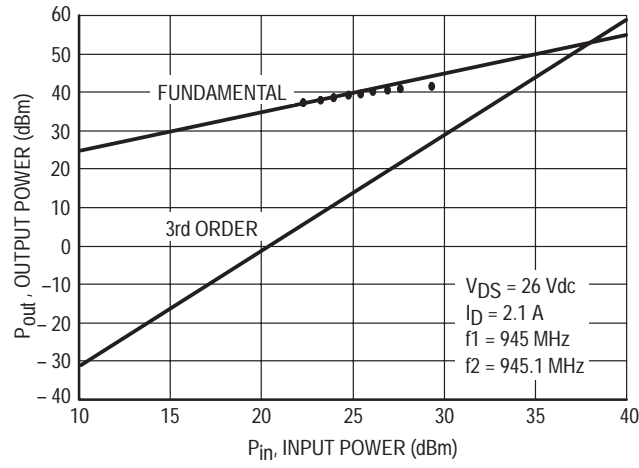


Figure 14. Class A Third Order Intercept Point

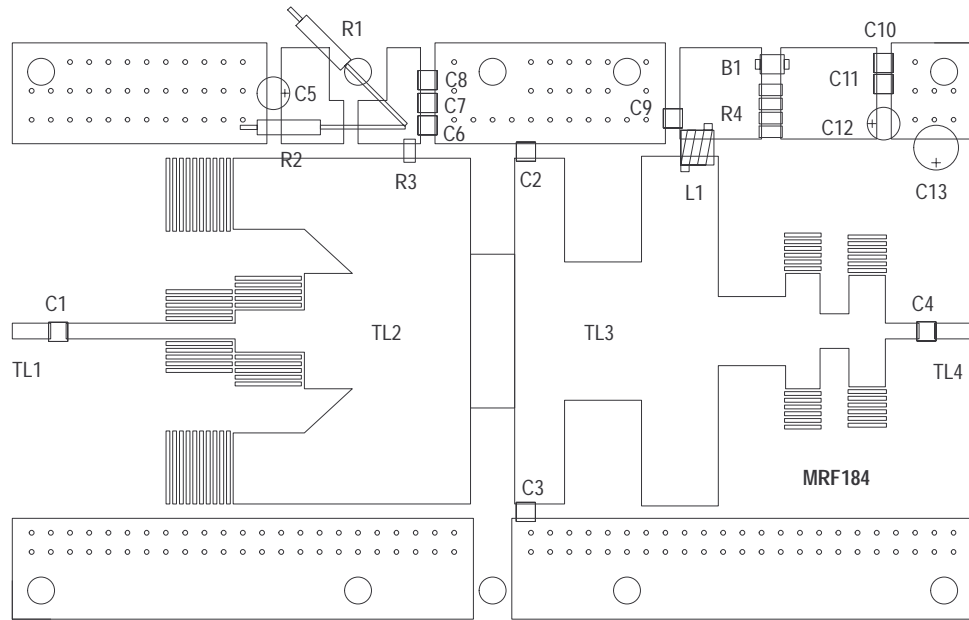
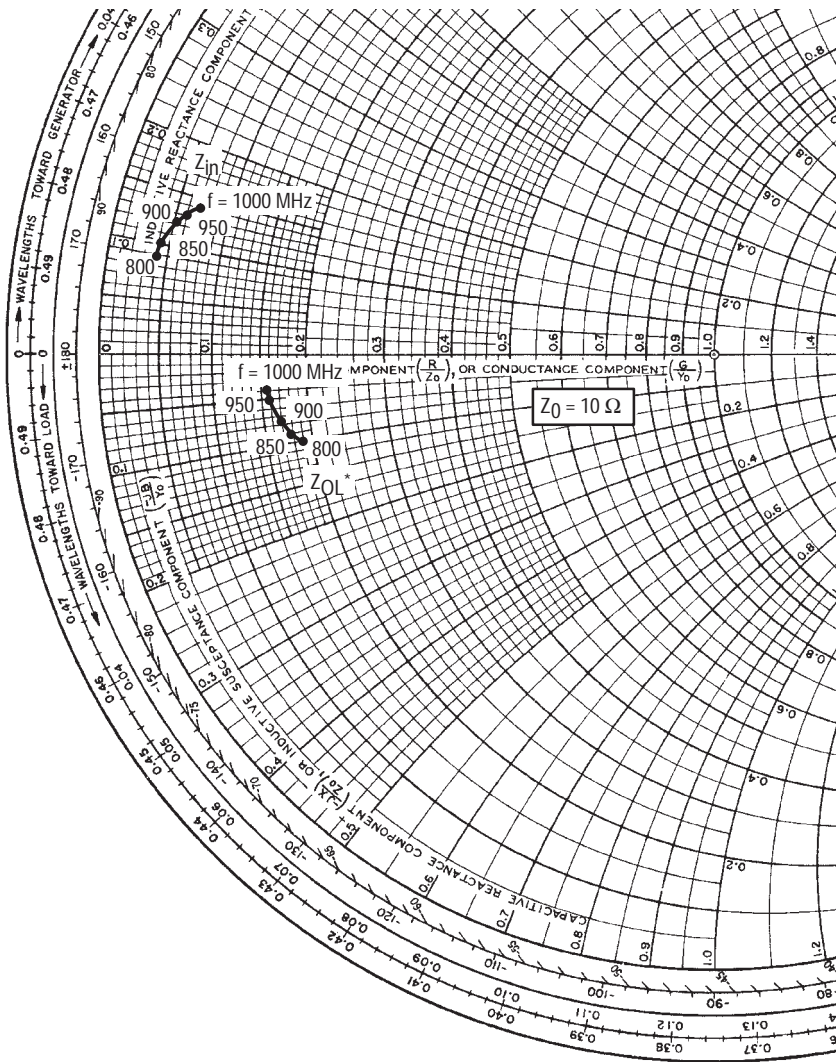


Figure 15. Component Parts Layout



$V_{DD} = 28 \text{ Vdc}$, $I_{DQ} = 100 \text{ mA}$, $P_{out} = 60 \text{ W}$

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
800	$0.40 + j0.90$	$1.85 - j1.00$
850	$0.45 + j1.10$	$1.75 - j0.90$
900	$0.52 + j1.20$	$1.70 - j0.75$
950	$0.60 + j1.30$	$1.60 - j0.50$
1000	$0.70 + j1.38$	$1.57 - j0.40$

Z_{in} = Conjugate of source impedance.

Z_{out} = Conjugate of the load impedance at a given output power, voltage, frequency and efficiency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency and device stability.

Figure 16. Series Equivalent Input and Output Impedance

Table 1. Common Source S-Parameters ($V_{DS} = 13.5\text{ V}$)

$I_D = 2.0\text{ A}$

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
20	0.916	179	10.88	80	0.014	-22	0.843	175
30	0.917	178	9.26	79	0.014	-25	0.847	174
40	0.918	177	8.10	78	0.015	-29	0.852	174
50	0.919	176	7.16	77	0.015	-33	0.853	174
100	0.919	175	4.57	75	0.015	-35	0.855	173
150	0.920	174	3.34	67	0.015	-38	0.865	173
200	0.921	173	2.60	62	0.014	-41	0.867	173
250	0.922	173	2.11	59	0.014	-45	0.877	173
300	0.928	172	1.77	55	0.014	-49	0.881	173
350	0.938	172	1.50	50	0.013	-55	0.887	173
400	0.941	171	1.28	47	0.013	-59	0.895	173
450	0.942	171	1.12	44	0.012	-62	0.896	173
500	0.943	171	1.00	41	0.012	-68	0.898	172
550	0.945	171	0.91	38	0.010	-75	0.899	172
600	0.947	171	0.80	35	0.010	-79	0.903	172
650	0.948	171	0.71	33	0.009	-85	0.905	172
700	0.955	170	0.65	30	0.008	-88	0.909	172
750	0.959	170	0.60	28	0.008	-95	0.919	172
800	0.962	169	0.55	25	0.007	-102	0.922	172
850	0.963	169	0.50	23	0.007	-111	0.923	171
900	0.964	169	0.45	21	0.007	-118	0.926	171
950	0.968	169	0.43	19	0.006	-125	0.929	171
1000	0.970	169	0.39	18	0.006	-129	0.933	171
1050	0.971	168	0.36	17	0.005	-134	0.935	171
1100	0.972	168	0.34	14	0.005	-142	0.936	170
1150	0.973	168	0.32	13	0.005	-149	0.938	170
1200	0.974	167	0.29	12	0.006	-156	0.940	169
1250	0.976	167	0.28	10	0.007	-162	0.943	169
1300	0.975	167	0.26	9	0.008	-173	0.945	168
1350	0.972	166	0.25	8	0.009	-178	0.946	167
1400	0.969	166	0.24	7	0.011	175	0.947	167
1450	0.965	165	0.22	6	0.012	172	0.948	167
1500	0.959	164	0.21	5	0.013	169	0.950	167

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Table 2. Common Source S-Parameters ($V_{DS} = 28\text{ V}$)

$I_D = 2.0\text{ A}$

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
20	0.912	-170	16.01	84	0.016	-12	0.746	178
30	0.917	-173	13.73	82	0.015	-15	0.755	177
40	0.918	-174	12.02	80	0.014	-17	0.759	177
50	0.919	-176	10.62	78	0.013	-20	0.766	176
100	0.922	-178	6.76	71	0.012	-22	0.775	176
150	0.930	177	4.92	65	0.011	-25	0.791	176
200	0.931	176	3.82	60	0.010	-27	0.791	176
250	0.933	175	3.07	55	0.009	-29	0.793	176
300	0.941	174	2.53	51	0.009	-31	0.826	176
350	0.943	173	2.14	45	0.008	-35	0.834	176
400	0.945	172	1.83	41	0.008	-45	0.853	176
450	0.948	172	1.58	38	0.007	-52	0.858	176
500	0.950	172	1.39	35	0.007	-57	0.865	176
550	0.955	172	1.24	32	0.007	-61	0.876	176
600	0.960	172	1.10	29	0.006	-64	0.882	176
650	0.965	171	0.96	26	0.006	-68	0.888	175
700	0.967	171	0.89	24	0.006	-71	0.894	175
750	0.970	171	0.80	20	0.005	-73	0.904	175
800	0.973	170	0.73	18	0.005	-78	0.906	175
850	0.974	169	0.66	17	0.004	-83	0.908	174
900	0.975	169	0.61	13	0.004	-91	0.909	173
950	0.976	169	0.57	12	0.004	-94	0.915	173
1000	0.978	168	0.52	11	0.004	-96	0.916	173
1050	0.979	168	0.47	9	0.005	-102	0.919	172
1100	0.980	168	0.43	7	0.005	-115	0.924	172
1150	0.980	167	0.41	6	0.006	-119	0.931	171
1200	0.979	167	0.38	5	0.006	-125	0.934	170
1250	0.978	167	0.36	2	0.006	-139	0.935	170
1300	0.974	167	0.34	1	0.007	-148	0.936	170
1350	0.971	166	0.32	0	0.007	-156	0.937	169
1400	0.970	165	0.31	-1	0.007	-165	0.938	169
1450	0.969	165	0.30	-2	0.008	-171	0.939	169
1500	0.965	164	0.27	-3	0.008	-178	0.946	169

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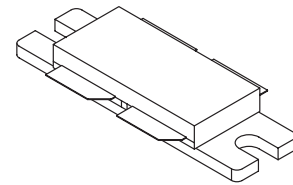
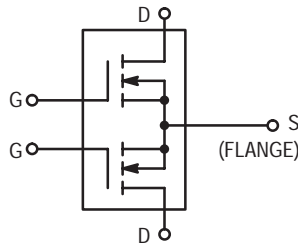
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The RF MOSFET Line
RF POWER
Field-Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

- High Gain, Rugged Device
- Broadband Performance from HF to 1 GHz
- Bottom Side Source Eliminates DC Isolators, Reducing Common Mode Inductances

MRF185

85 WATTS, 1.0 GHz
28 VOLTS
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 375B-02, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Storage Temperature Range	T_{stg}	-65 to +150	$^{\circ}C$
Operating Junction Temperature	T_J	200	$^{\circ}C$
Total Device Dissipation @ $T_C = 25^{\circ}C$ Derate above $25^{\circ}C$	P_D	250 1.45	Watts W/ $^{\circ}C$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.7	$^{\circ}C/W$

ELECTRICAL CHARACTERISTICS ($T_C = 25^{\circ}C$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0 V, I_D = 1 \mu A_{dc}$)	$V_{(BR)DSS}$	65	-	-	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 V, V_{GS} = 0 V$)	I_{DSS}	-	-	1	μA_{dc}
Gate-Source Leakage Current ($V_{GS} = 20 V, V_{DS} = 0 V$)	I_{GSS}	-	-	1	μA_{dc}

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS – continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

ON CHARACTERISTICS

Gate Quiescent Voltage ($V_{DS} = 26\text{ V}$, $I_D = 300\text{ mA}$ per side)	$V_{GS(Q)}$	3	4	5	Vdc
Delta Quiescent Voltage between sides ($V_{DS} = 26\text{ V}$, $I_D = 300\text{ mA}$ per side)	$\Delta V_{GS(Q)}$	–	0.15	0.3	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 3\text{ A}$ per side)	$V_{DS(on)}$	–	0.75	1	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 3\text{ A}$ per side)	g_{fs}	1.6	2	–	s

DYNAMIC CHARACTERISTICS

Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{oss}	–	38	–	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{rss}	–	4.6	6	pF

FUNCTIONAL CHARACTERISTICS

Common Source Power Gain ($V_{DD} = 28\text{ V}$, $P_{out} = 85\text{ W}$, $f = 960\text{ MHz}$, $I_{DQ} = 600\text{ mA}$)	G_{ps}	11	14	–	dB
Drain Efficiency ($V_{DD} = 28\text{ V}$, $P_{out} = 85\text{ W}$, $f = 960\text{ MHz}$, $I_{DQ} = 600\text{ mA}$)	η	45	53	–	%
Load Mismatch ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 85\text{ W}$, $f = 960\text{ MHz}$, $I_{DQ} = 600\text{ mA}$, Load VSWR 5:1 at All Phase Angles)	Ψ	No Degradation in Output Power			

LIFETIME BUY

LAST SHIP 31JAN05
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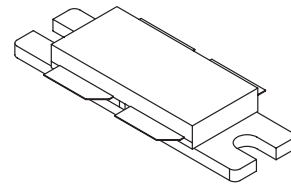
The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

Designed for broadband commercial and industrial applications at frequencies from 800 MHz to 1.0 GHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 28 volt base station equipment.

- Guaranteed Performance @ 960 MHz, 28 Volts
Output Power — 120 Watts (PEP)
Power Gain — 11 dB
Efficiency — 30%
Intermodulation Distortion — -28 dBc
- Excellent Thermal Stability
- 100% Tested for Load Mismatch Stress at all Phase Angles with 5:1 VSWR @ 28 Vdc, 960 MHz, 120 Watts CW

MRF186

120 W, 1.0 GHz, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 375B-02, STYLE 2

MAXIMUM RATINGS (2)

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1 \text{ M}\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current — Continuous	I_D	14	Adc
Total Device Dissipation @ $T_C = 70^\circ\text{C}$ Derate above 70°C	P_D	162.5 1.25	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS (2)

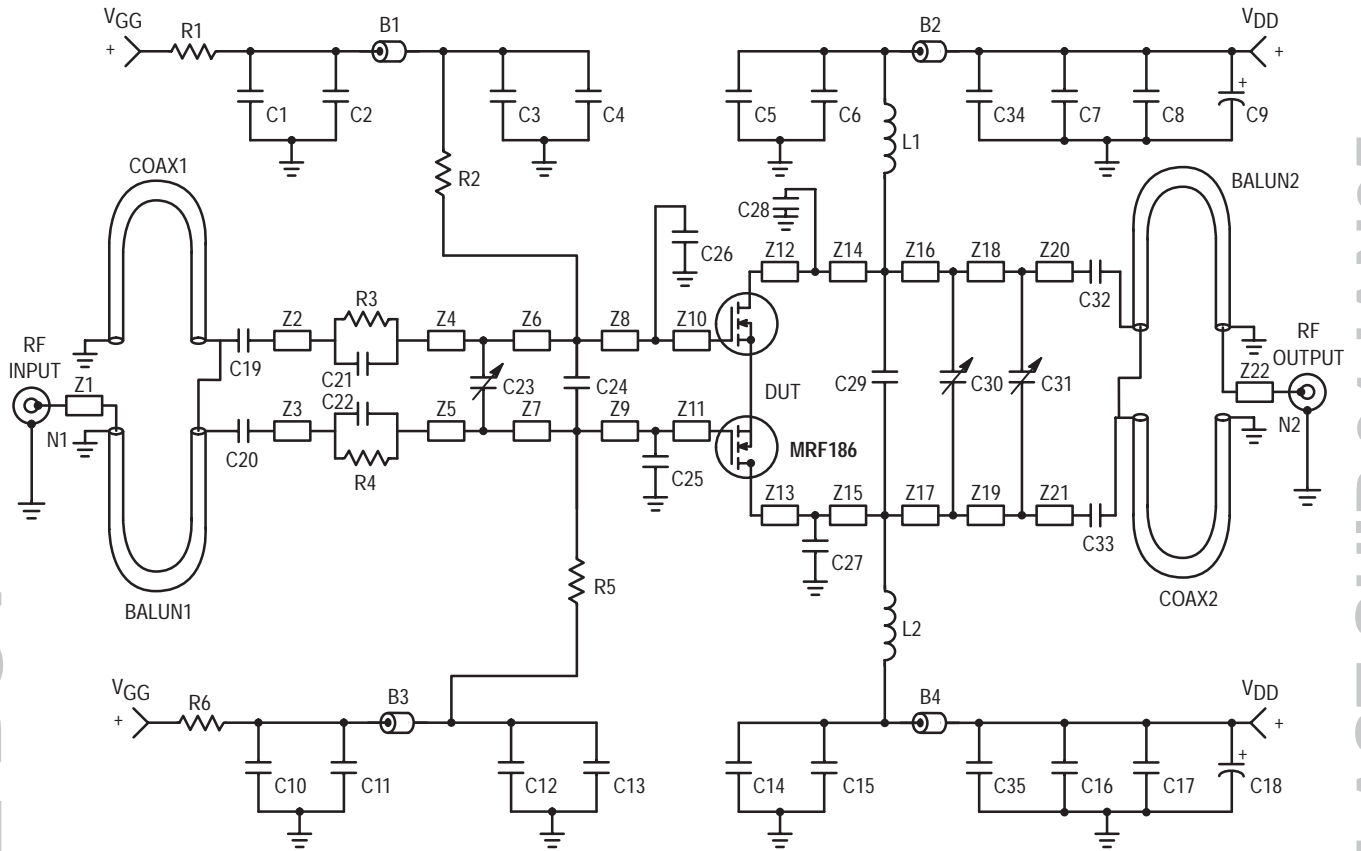
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.8	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 50\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 20\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS (1)					
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$ Per Side)	$V_{GS(th)}$	2.5	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 300\text{ mAdc}$ Per Side)	$V_{GS(Q)}$	3.3	4.2	5	Vdc
Delta Gate Threshold Voltage (Side to Side) ($V_{DS} = 28\text{ V}$, $I_D = 300\text{ mA}$ Per Side)	$\Delta V_{GS(Q)}$	—	—	0.3	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$ Per Side)	$V_{DS(on)}$	—	0.58	0.7	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$ Per Side)	g_{fs}	2.4	2.8	—	S
DYNAMIC CHARACTERISTICS (1)					
Input Capacitance (Per Side) ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	177	—	pF
Output Capacitance (Per Side) ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	45	—	pF
Reverse Transfer Capacitance (Per Side) ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	3.4	—	pF
FUNCTIONAL CHARACTERISTICS (In Motorola Test Fixture) (2)					
Two–Tone Common Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	G_{ps}	11	12.2	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	η	30	35	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	IMD	—	–32	–28	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	IRL	9	16	—	dB
Two–Tone Common Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	G_{ps}	—	12	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	η	—	33	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	IMD	—	–32	—	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	IRL	—	16	—	dB
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W CW}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f = 960\text{ MHz}$, $V_{SWR} = 5:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

- (1) Each side of device measured separately.
 (2) Device measured in push–pull configuration.



- B1 – B4 Fair Rite Products Short Ferrite Bead, 2743021446
- C1, C7, C8, C10, C16, C17 10 μ F, 50 V, Tantalum
- C2, C11, C34, C35 0.1 μ F, Chip Capacitor
- C3, C6, C12, C15 330 pF, Chip Capacitor
- C4, C5, C13, C14, C19, C20, C32, C33 47 pF, Chip Capacitor
- C9, C18 250 μ F, 50 V, Electrolytic Capacitor
- C21, C22 12 pF, Chip Capacitor
- C23, C30 0.6 – 4.5 pF, Variable Capacitor, Johanson Gigatrim
- C24, C25, C26 5.1 pF, Chip Capacitor
- C27, C28 3.9 pF, Chip Capacitor

- C31 0.8 – 8.0 pF, Variable Capacitor, Johanson Gigatrim
- L1, L2 3 Turns, #20 AWG, IDIA 0.126", 24.7 nH
- N1, N2 Type N Connectors
- R1, R6 1 k Ω , 1/4 W, Carbon Resistor
- R2, R5 1.2 k Ω , 0.1 W, Chip Resistor
- R3, R4 75 Ω , 0.1 W, Chip Resistor
- Z1 – Z22 Microstrip (See Component Placement)
- Balun1, Balun2, Coax1, Coax2 2.20" 50 Ω , 0.086" OD Semi-Rigid Coax Board
- 1/32" Glass Teflon[®], $\epsilon_r = 2.55$

Figure 1. 930 – 960 MHz Test Circuit Schematic

TYPICAL CHARACTERISTICS

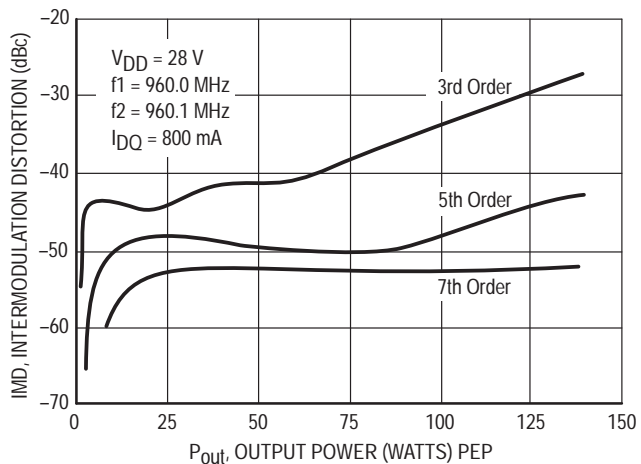


Figure 2. Intermodulation Distortion Products versus Output Power

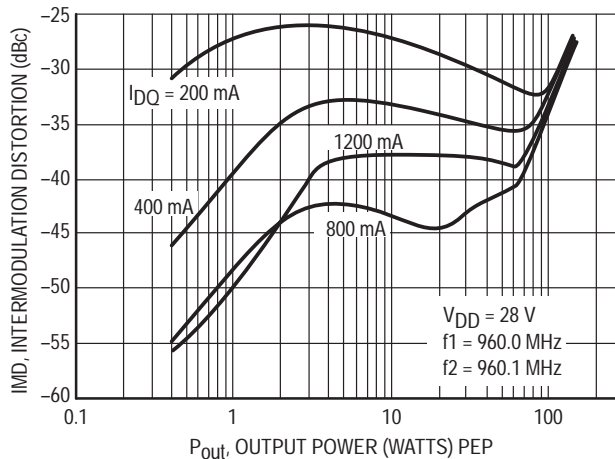


Figure 3. Intermodulation Distortion versus Output Power

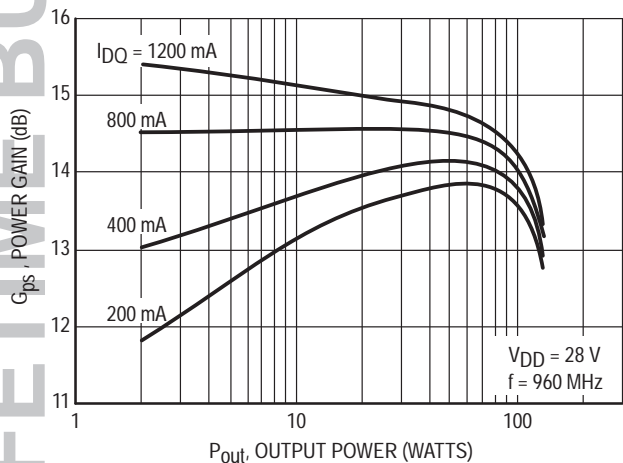


Figure 4. Power Gain versus Output Power

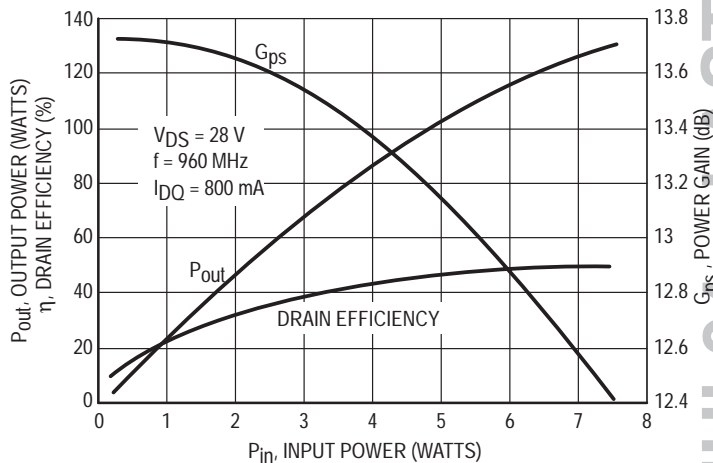


Figure 5. Output Power versus Input Power

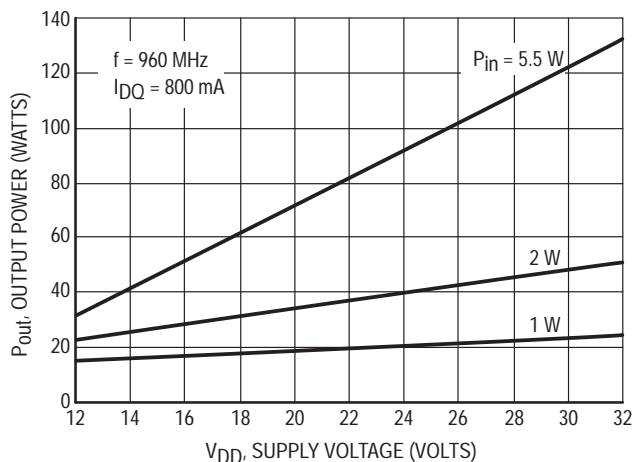


Figure 6. Output Power versus Supply Voltage

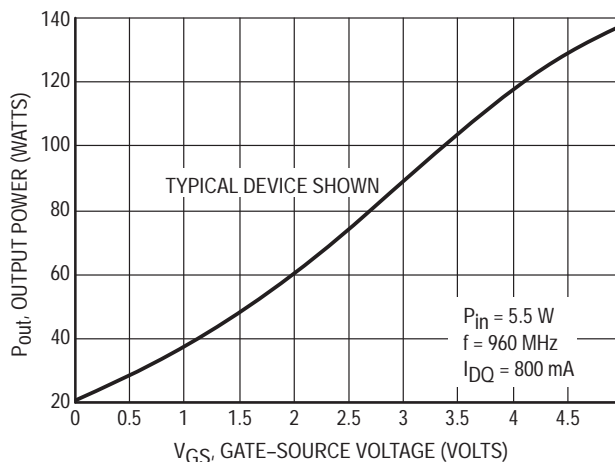


Figure 7. Output Power versus Gate Voltage

LIFETIME BUY

LAST SHIP 31 JAN 05
LAST ORDER 31 JUL 04

TYPICAL CHARACTERISTICS

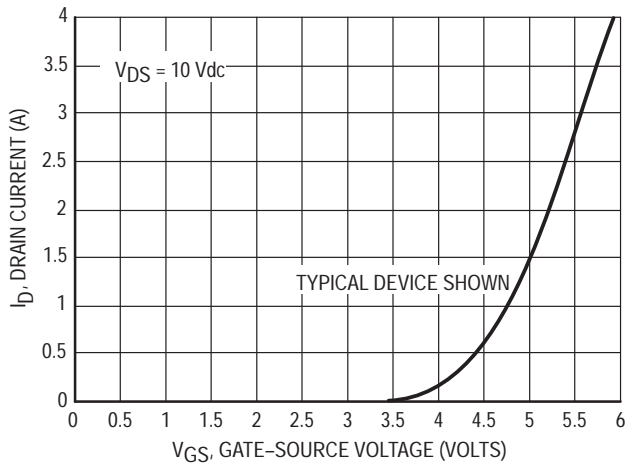


Figure 8. Drain Current versus Gate Voltage

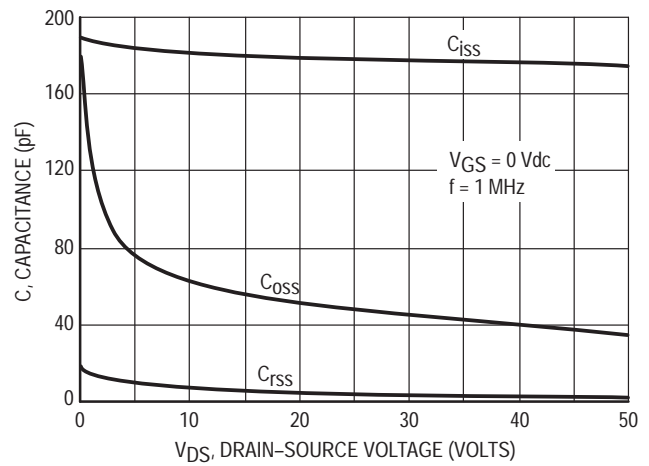


Figure 9. Capacitance versus Voltage

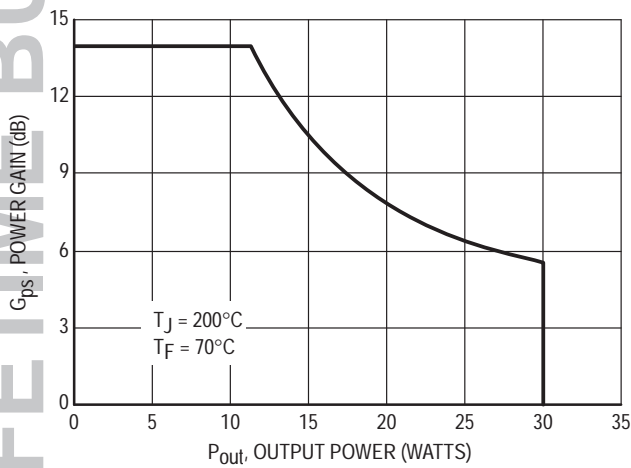


Figure 10. DC Safe Operating Area

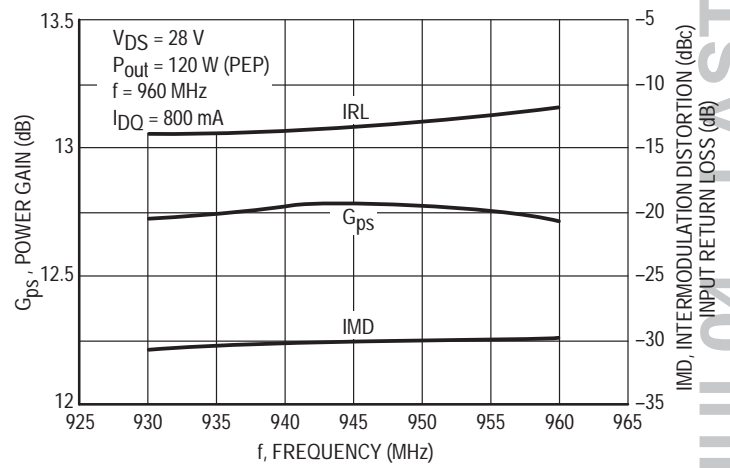
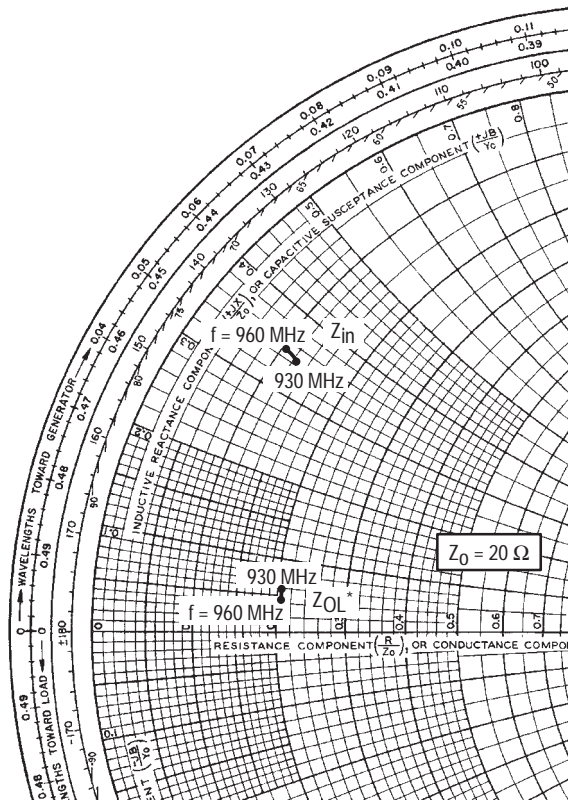


Figure 11. Broadband Circuit Performance

LIFETIME BUY

LAST ORDER 31 JUL 04 LAST SHIP 31 JAN 05



$V_{CC} = 28\text{ V}$, $I_{DQ} = 2 \times 400\text{ mA}$, $P_{out} = 120\text{ Watts (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
930	$2.5 + j6.9$	$4.3 + j1.2$
945	$2.5 + j7.0$	$4.3 + j1.0$
960	$2.2 + j7.1$	$4.3 + j0.9$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current, efficiency and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation performance. Impedances shown represent a single channel (1/2 of MRF186) impedance measurement.

Figure 12. Series Equivalent Input and Output Impedance

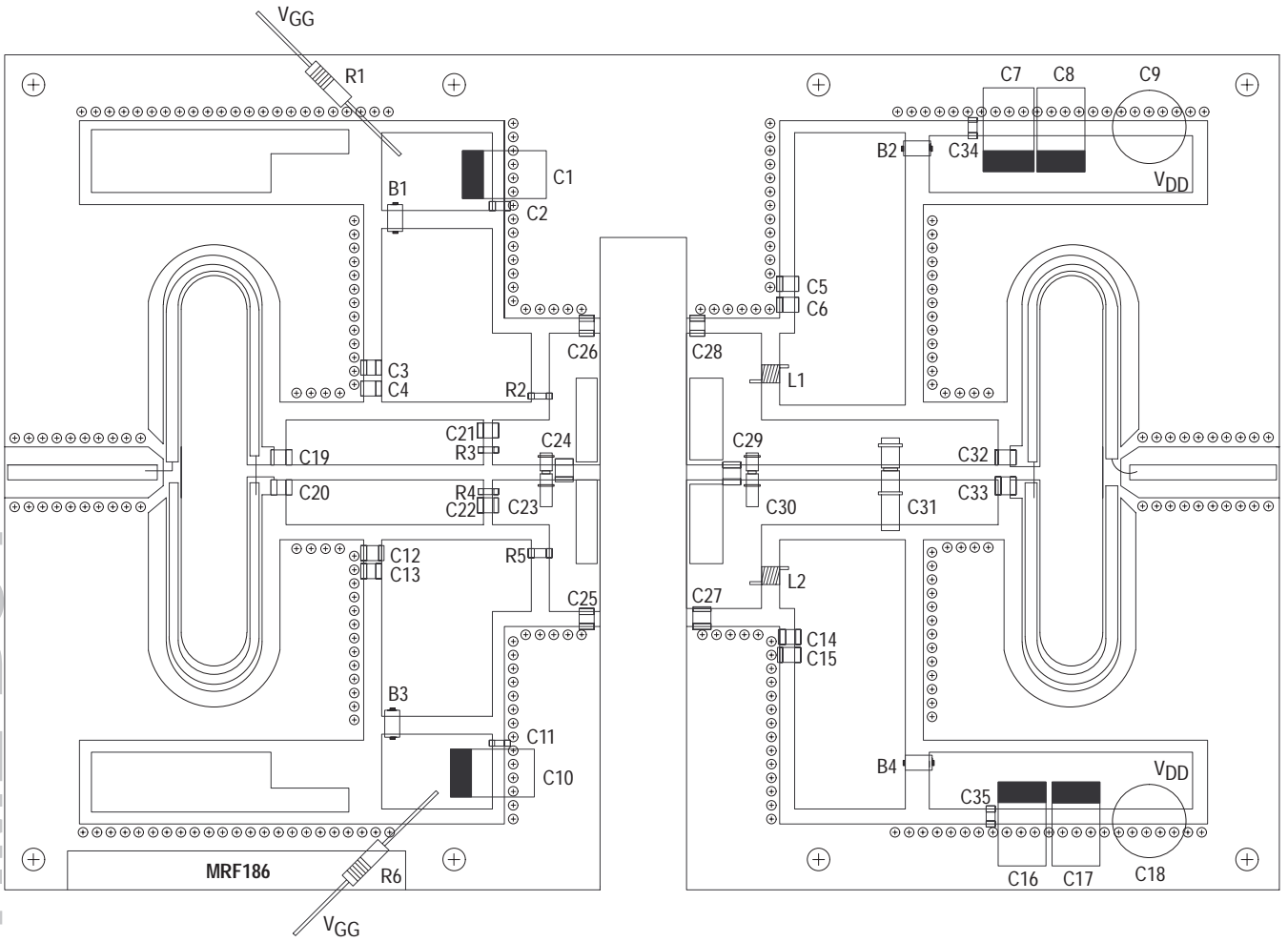


Figure 13. Component Placement Diagram of 930 – 960 MHz Broadband Test Fixture

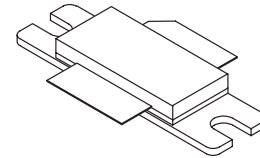
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for broadband commercial and industrial applications at frequencies up to 1.0 GHz. The high gain and broadband performance of these devices makes them ideal for large-signal, common source amplifier applications in 26 volt base station equipment.

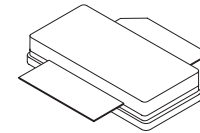
- Guaranteed Performance @ 880 MHz, 26 Volts
 - Output Power — 85 Watts (PEP)
 - Power Gain — 12 dB
 - Efficiency — 30%
 - Intermodulation Distortion — -28 dBc
- 100% Tested for Load Mismatch Stress at all Phase Angles with 5:1 VSWR @ 26 Vdc, 880 MHz, 85 Watts CW
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF187
MRF187S

85 W, 1.0 GHz, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465-04, STYLE 1
(MRF187)



CASE 465A-04, STYLE 1
(MRF187S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Drain-Gate Voltage ($R_{GS} = 1 M\Omega$)	V_{DGR}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current — Continuous	I_D	15	Adc
Total Device Dissipation @ $T_C \geq 25^\circ C$ Derate above 25°C	P_D	250 1.43	Watts W/°C
Storage Temperature Range	T_{stg}	-65 to +200	°C
Operating Junction Temperature	T_J	200	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.70	°C/W

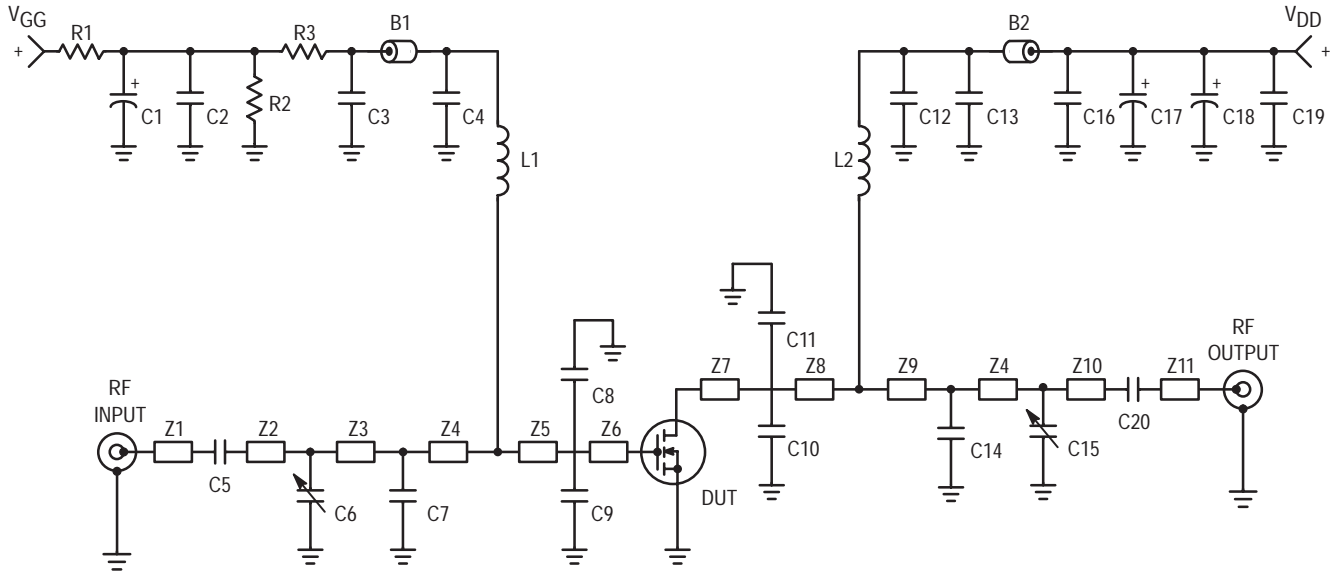
NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 50\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 20\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 550\text{ mA}$)	$V_{GS(Q)}$	3	—	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$)	$V_{DS(on)}$	—	0.40	0.55	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 5\text{ Adc}$)	g_{fs}	—	2	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance (Includes Internal Input MOScap) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	295	—	pF
Output Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	85	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	10	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	G_{ps}	12	13	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	η_D	30	33	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	IMD	—	–31	–28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	IRL	9	15	—	dB
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$ and $f_1 = 895.0\text{ MHz}$, $f_2 = 895.1\text{ MHz}$)	G_{ps}	—	13	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$ and $f_1 = 895.0\text{ MHz}$, $f_2 = 895.1\text{ MHz}$)	η_D	—	33	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$ and $f_1 = 895.0\text{ MHz}$, $f_2 = 895.1\text{ MHz}$)	IMD	—	–31	—	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W PEP}$, $I_{DQ} = 550\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$ and $f_1 = 895.0\text{ MHz}$, $f_2 = 895.1\text{ MHz}$)	IRL	—	12	—	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 85\text{ W CW}$, $I_{DQ} = 550\text{ mA}$, $f = 880\text{ MHz}$, $V_{SWR} = 5:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			



B1 – B2	Ferrite Bead, Fair Rite, 2743019447	L1, L2	5 Turns, #24 AWG, 0.059" OD
C1	10 μ F, 50 V, Electrolytic Capacitor, ECEV1HV100R Panasonic	R1	12 Ω , 1/4 Watt Carbon
C2, C16	0.10 μ F, B Case Chip Capacitors, CDR33BX104AKWS, Kemet	R2	4.7 M Ω , 1/4 Watt Carbon
C3	20000 pF, B Case Chip Capacitor, 200B203MCA50X, ATC	R3	16 k Ω , 1/4 Watt Carbon
C4, C13	100 pF, B Case Chip Capacitors, 100B101JCA500X, ATC	Z1, Z11	0.150" x 0.220" Microstrip
C5, C20	47 pF, B Case Chip Capacitors, 100B470JCA500X, ATC	Z2, Z10	0.410" x 0.220" Microstrip
C6, C15	0.8 – 8.0 pF, Variable Capacitors, Johanson Gigatrim	Z3	0.160" x 0.630" Microstrip
C7	4.7 pF, B Case Chip Capacitor, 100B4R7JCA500X, ATC	Z4	0.160" x 0.630" Microstrip
C8, C9	10 pF, B Case Chip Capacitors, 100B100JCA500X, ATC	Z5	0.098" x 0.630" Microstrip
C10, C11	16 pF, B Case Chip Capacitors, 100B160JCA500X, ATC	Z6	0.098" x 0.630" Microstrip
C12	43 pF, B Case Chip Capacitor, 100B430JCA500X, ATC	Z7	0.210" x 0.220" Microstrip
C14	7.5 pF, B Case Chip Capacitor, 100B7R5JCA500X, ATC	Z8	0.050" x 0.220" Microstrip
C17, C18, C19	10 μ F, 35 V, Electrolytic Capacitors, SMT, Kemet		

Figure 1. MRF187 Schematic

TYPICAL CHARACTERISTICS

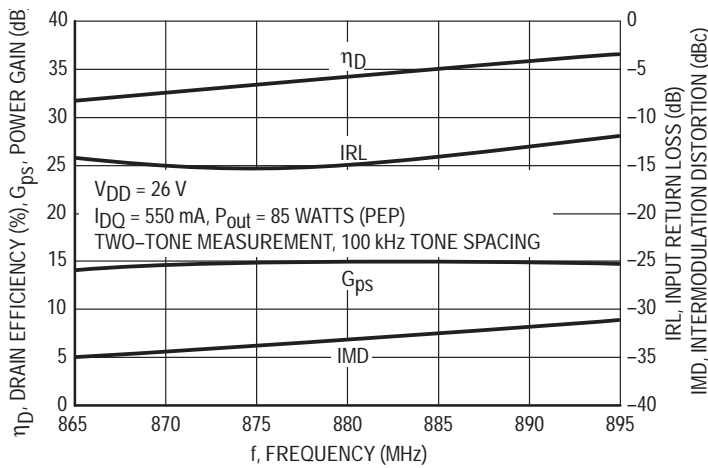


Figure 2. Class AB Broadband Circuit Performance

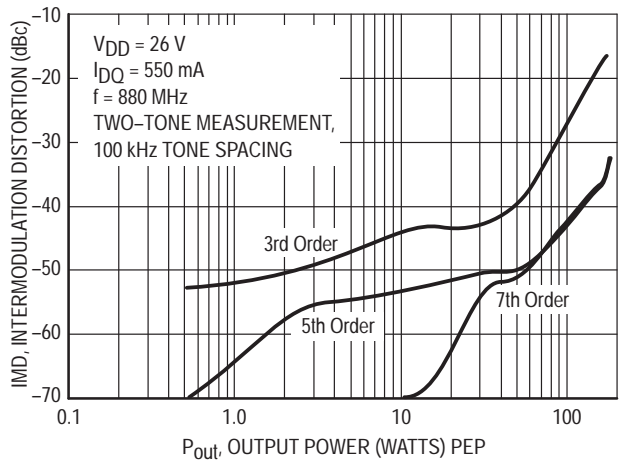


Figure 3. Intermodulation Distortion Products versus Output Power

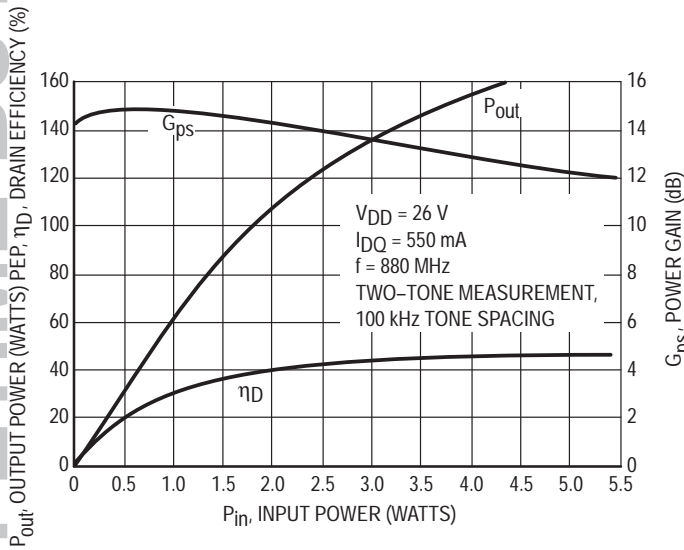


Figure 4. Class AB Parameters versus Input Power

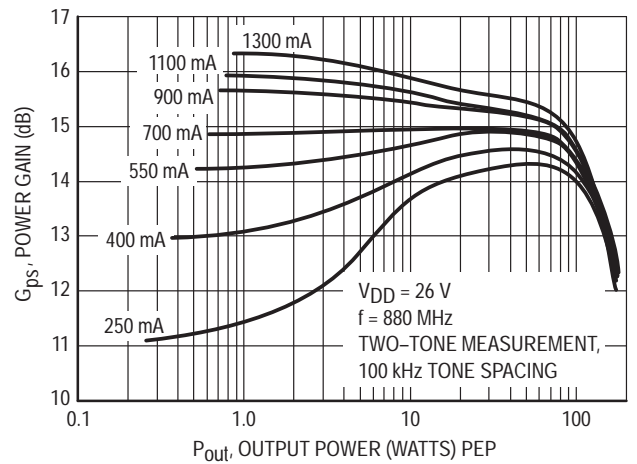


Figure 5. Power Gain versus Output Power

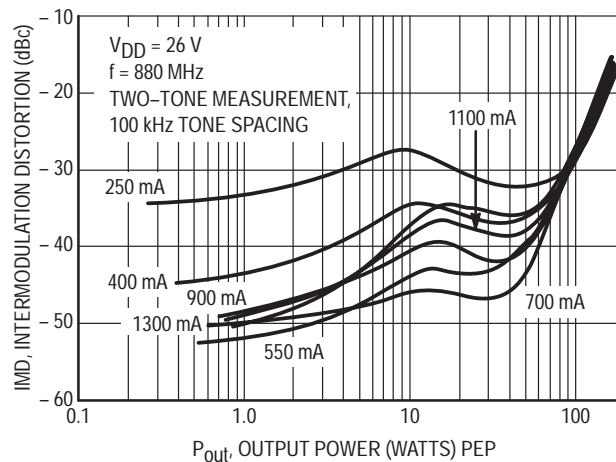
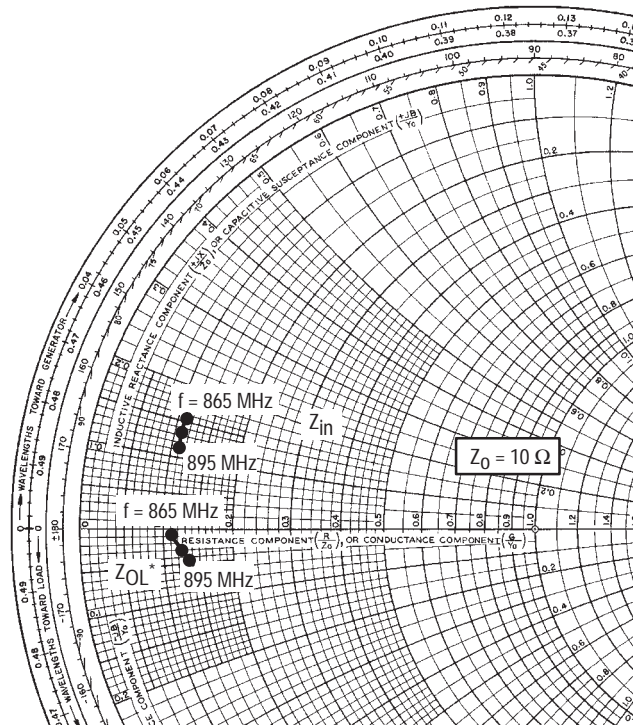


Figure 6. Intermodulation Distortion versus Output Power

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04



$V_{CC} = 26\text{ V}$, $I_{DQ} = 550\text{ mA}$, $P_{Out} = 85\text{ Watts (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
865	$1.04 + j1.51$	$1.13 - j0.091$
880	$1.03 + j1.39$	$1.20 - j0.176$
895	$1.03 + j1.29$	$1.28 - j0.242$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

Figure 7. Series Equivalent Input and Output Impedance

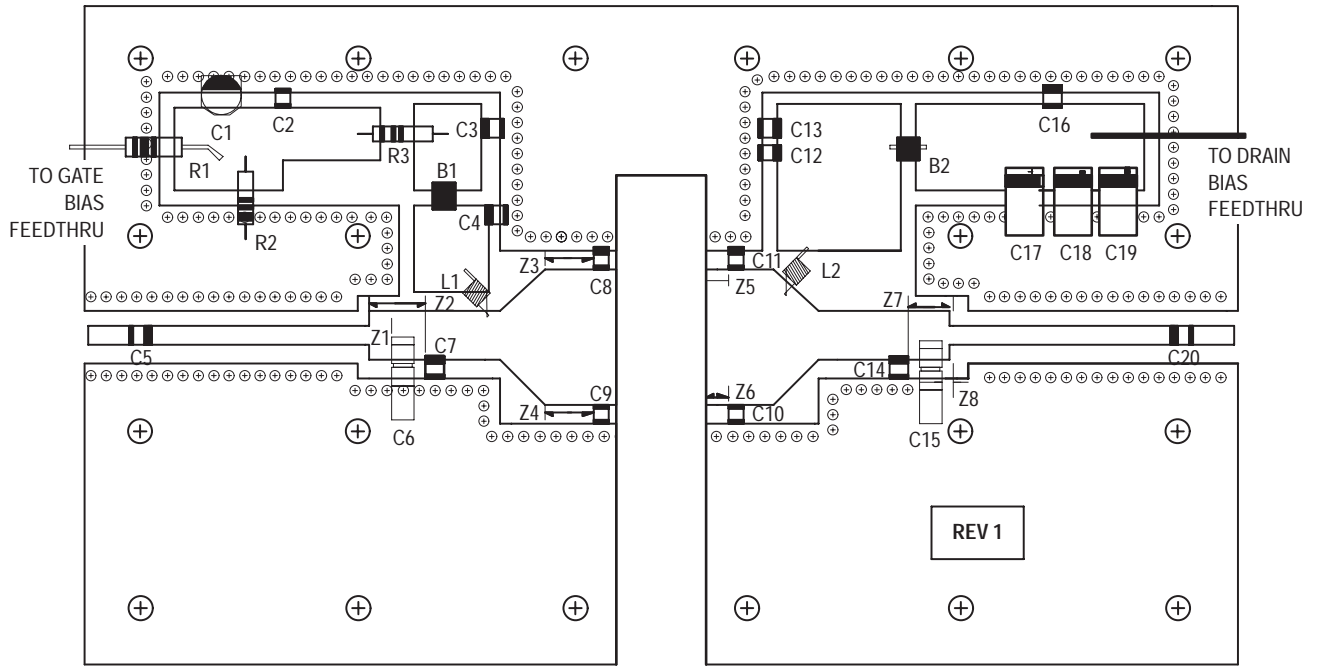


Figure 8. MRF187 Populated PC Board Layout Diagram

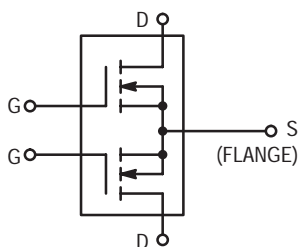
The RF MOSFET Line
Power Field-Effect Transistor
N-Channel Enhancement-Mode

Designed primarily for wideband large-signal output and driver stages from 100 – 500 MHz.

- Guaranteed Performance @ 500 MHz, 28 Vdc
Output Power — 150 Watts
Power Gain — 10 dB (Min)
Efficiency — 50% (Min)
100% Tested for Load Mismatch at all Phase Angles with VSWR 30:1
- Overall Lower Capacitance @ 28 V
C_{iSS} — 135 pF
C_{oss} — 140 pF
C_{rSS} — 17 pF
- Simplified AVC, ALC and Modulation

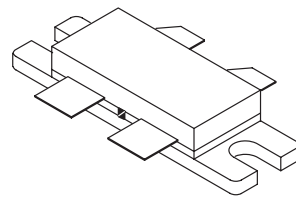
Typical data for power amplifiers in industrial and commercial applications:

- Typical Performance @ 400 MHz, 28 Vdc
Output Power — 150 Watts
Power Gain — 12.5 dB
Efficiency — 60%
- Typical Performance @ 225 MHz, 28 Vdc
Output Power — 200 Watts
Power Gain — 15 dB
Efficiency — 65%
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://motorola.com/sps/rf/designtds/>



MRF275G

150 W, 28 V, 500 MHz
N-CHANNEL MOS
BROADBAND
100 – 500 MHz
RF POWER FET



CASE 375-04, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	65	Vdc
Drain-Gate Voltage (R _{GS} = 1.0 MΩ)	V _{DGR}	65	Vdc
Gate-Source Voltage	V _{GS}	±40	Adc
Drain Current — Continuous	I _D	26	Adc
Total Device Dissipation @ T _C = 25°C Derate above 25°C	P _D	400 2.27	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	200	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	0.44	°C/W

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

OFF CHARACTERISTICS (1)

Drain–Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 50$ mA)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28$ V, $V_{GS} = 0$)	I_{DSS}	—	—	1	mA
Gate–Source Leakage Current ($V_{GS} = 20$ V, $V_{DS} = 0$)	I_{GSS}	—	—	1	μA

ON CHARACTERISTICS (1)

Gate Threshold Voltage ($V_{DS} = 10$ V, $I_D = 100$ mA)	$V_{GS(th)}$	1.5	2.5	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10$ V, $I_D = 5$ A)	$V_{DS(on)}$	0.5	0.9	1.5	Vdc
Forward Transconductance ($V_{DS} = 10$ V, $I_D = 2.5$ A)	g_{fs}	3	3.75	—	mhos

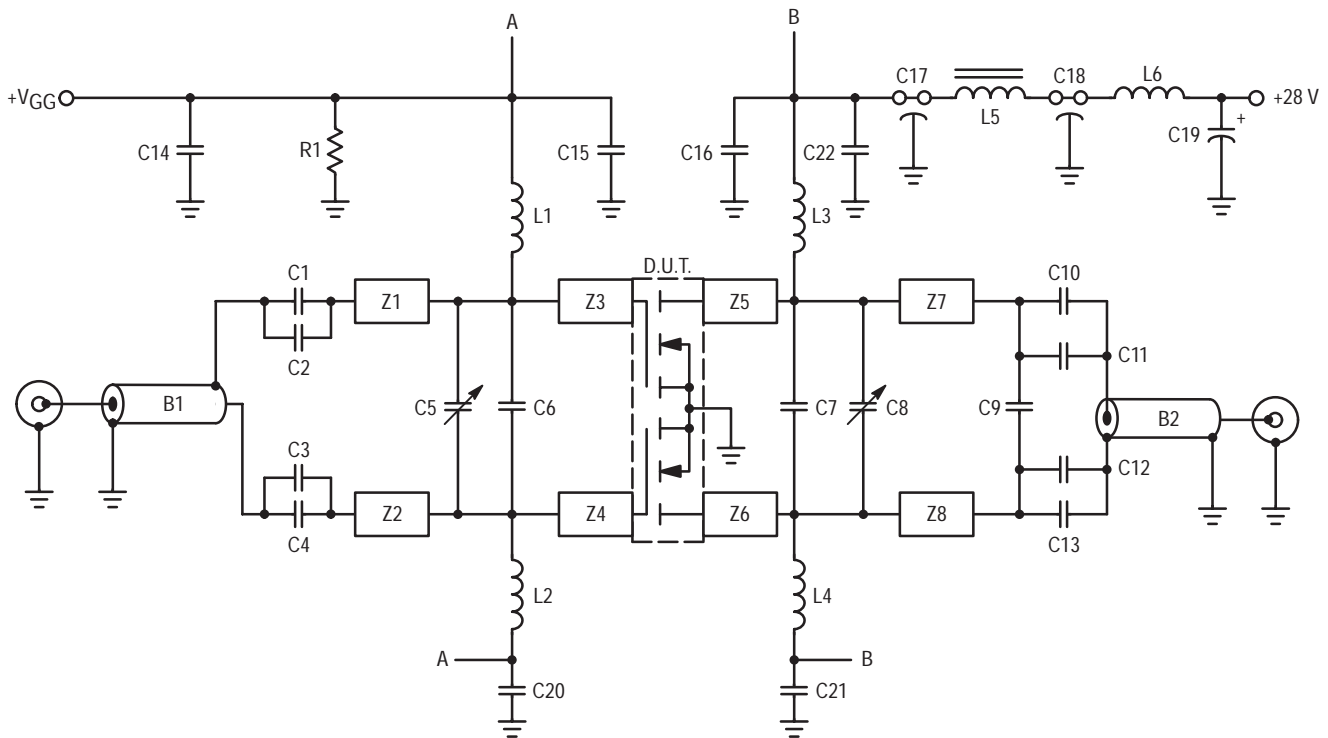
DYNAMIC CHARACTERISTICS (1)

Input Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1$ MHz)	C_{iss}	—	135	—	pF
Output Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1$ MHz)	C_{oss}	—	140	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28$ V, $V_{GS} = 0$, $f = 1$ MHz)	C_{rss}	—	17	—	pF

FUNCTIONAL CHARACTERISTICS (2) (Figure 1)

Common Source Power Gain ($V_{DD} = 28$ V, $P_{Out} = 150$ W, $f = 500$ MHz, $I_{DQ} = 2 \times 100$ mA)	G_{ps}	10	11.2	—	dB
Drain Efficiency ($V_{DD} = 28$ V, $P_{Out} = 150$ W, $f = 500$ MHz, $I_{DQ} = 2 \times 100$ mA)	η	50	55	—	%
Electrical Ruggedness ($V_{DD} = 28$ V, $P_{Out} = 150$ W, $f = 500$ MHz, $I_{DQ} = 2 \times 100$ mA, VSWR 30:1 at all Phase Angles)	ψ	No Degradation in Output Power			

1. Each side of device measured separately.
2. Measured in push–pull configuration.



B1	Balun, 50 Ω , 0.086" O.D. 2" Long, Semi Rigid Coax	L5	Ferroxcube VK200 20/4B
B2	Balun, 50 Ω , Coax 0.141" O.D. 2" Long, Semi Rigid	L6	4 Turns #16, 0.340" I.D., Enameled Wire
C1, C2, C3, C4,	270 pF, ATC Chip Capacitor	R1	1.0 k Ω , 1/4 W Resistor
C10, C11, C12, C13	1.0–20 pF, Trimmer Capacitor, Johanson	W1 – W4	20 x 200 x 250 mils, Wear Pads, Beryllium–Copper, (See Component Location Diagram)
C5, C8	22 pF, Mini–Unelco Capacitor	Z1, Z2	1.10" x 0.245", Microstrip Line
C6	15 pF, Unelco Capacitor	Z3, Z4, Z5, Z6	0.300" x 0.245", Microstrip Line
C7	2.1 pF, ATC Chip Capacitor	Z7, Z8	1.00" x 0.245", Microstrip Line
C14, C15, C16,	0.1 μ F, Ceramic Capacitor	Board material	0.060" Teflon–fiberglass, $\epsilon_r = 2.55$, copper clad both sides, 2 oz. copper.
C20, C21, C22	680 pF, Feedthru Capacitor	Points A are connected together on PCB.	
C17, C18	10 μ F, 50 V, Electrolytic Capacitor, Tantalum	Points B are connected together on PCB.	
C19	10 Turns AWG #24, 0.145" O.D., 106 nH		
L1, L2	Taylor–Spring Inductor		
L3, L4	10 Turns AWG #18, 0.340" I.D., Enameled Wire		

Figure 1. 500 MHz Test Circuit

TYPICAL CHARACTERISTICS

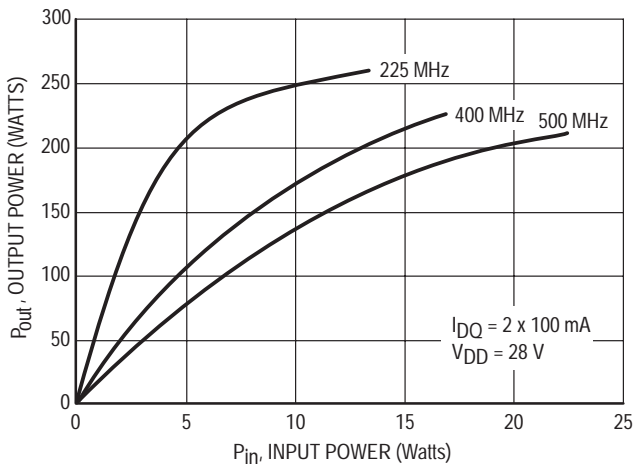


Figure 2. Output Power versus Input Power

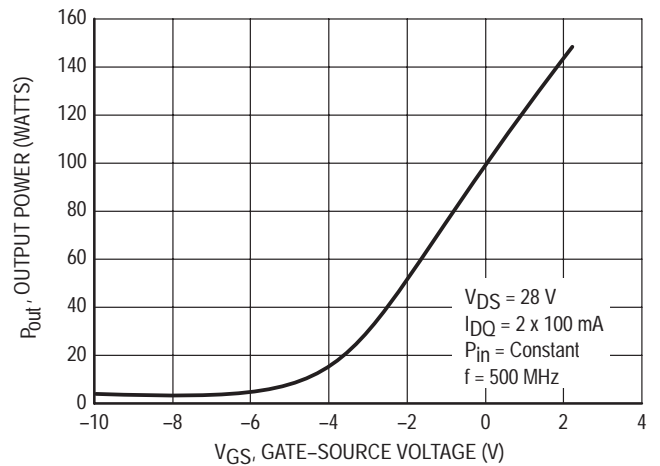


Figure 3. Output Power versus Gate Voltage

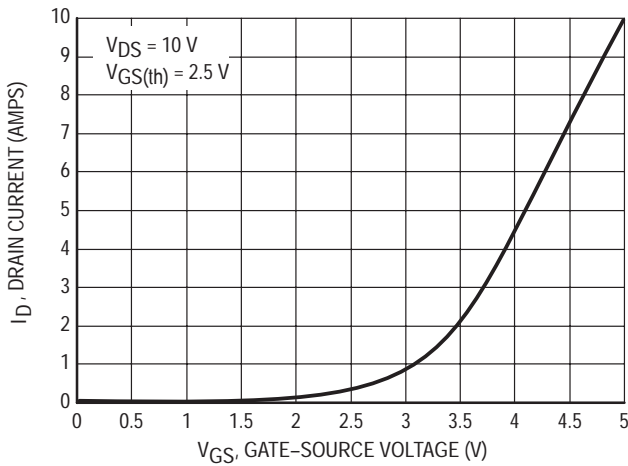


Figure 4. Drain Current versus Gate Voltage (Transfer Characteristics)

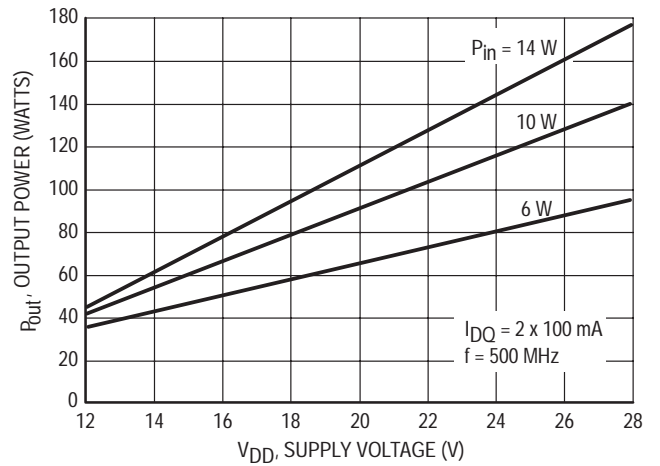


Figure 5. Output Power versus Supply Voltage

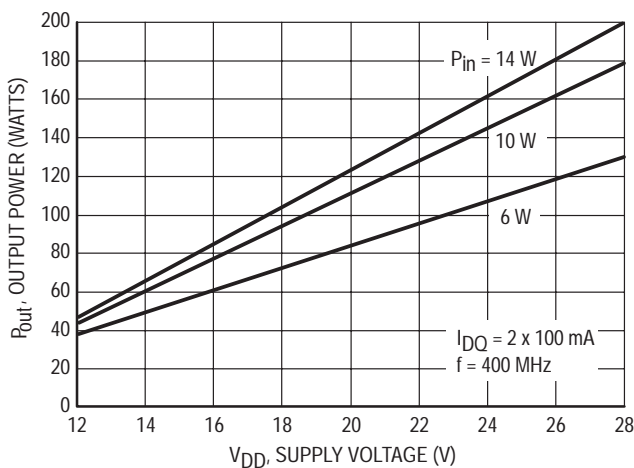


Figure 6. Output Power versus Supply Voltage

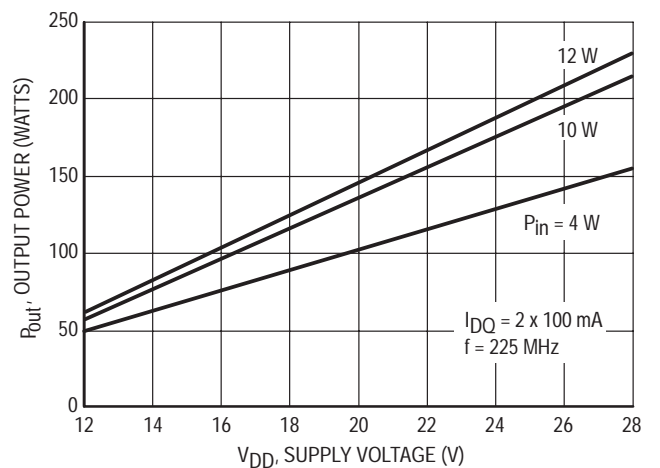


Figure 7. Output Power versus Supply Voltage

TYPICAL CHARACTERISTICS

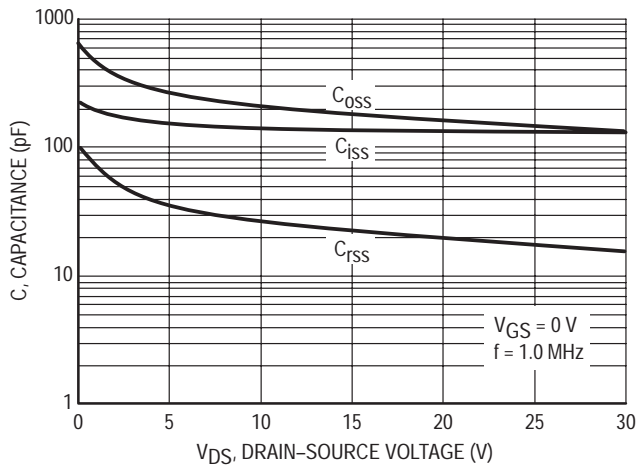


Figure 8. Capacitance versus Drain-Source Voltage*
 *Data shown applies only to one half of device, MRF275G

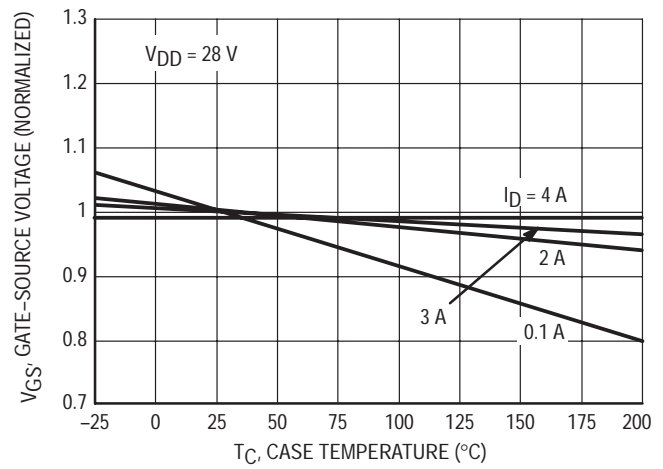


Figure 9. Gate-Source Voltage versus Case Temperature

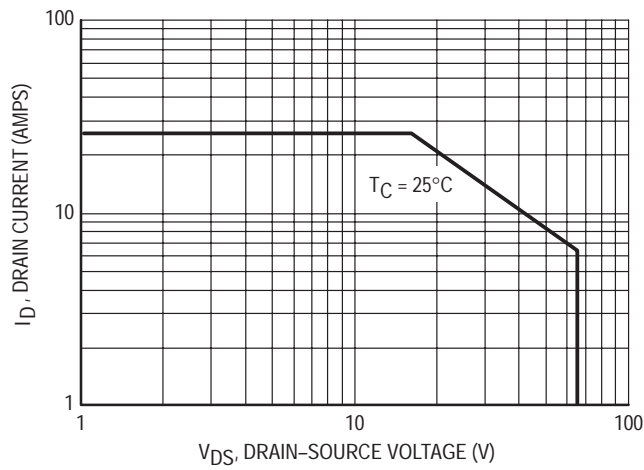
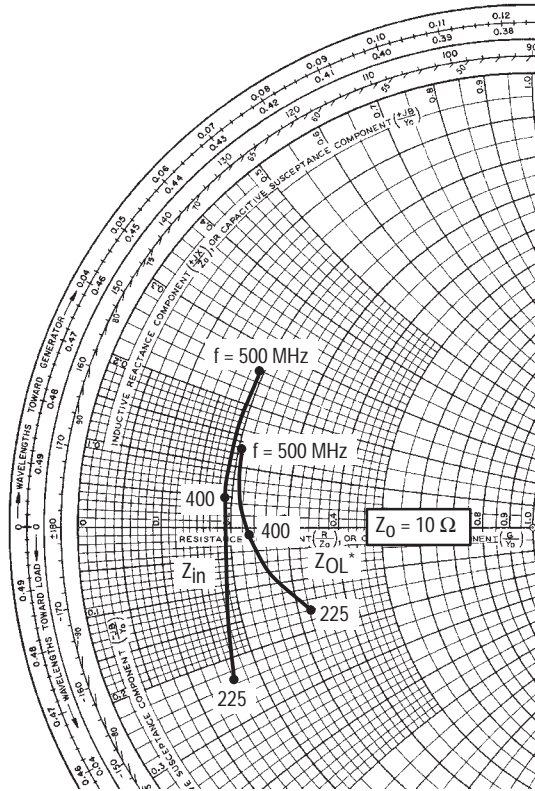


Figure 10. DC Safe Operating Area



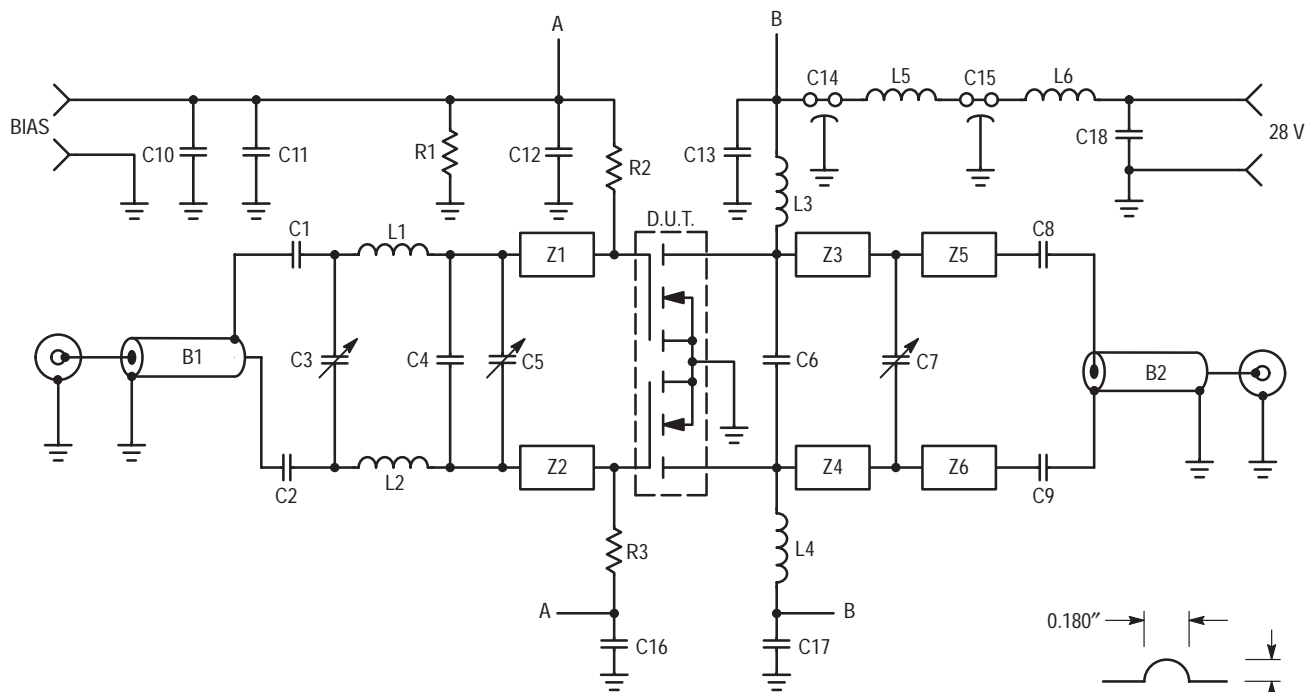
$V_{DD} = 28\text{ V}$, $I_{DQ} = 2 \times 100\text{ mA}$, $P_{out} = 150\text{ W}$

f (MHz)	Z_{in} Ohms	Z_{OL}^* Ohms
225	$1.6 - j2.30$	$3.2 - j1.50$
400	$1.9 + j0.48$	$2.3 - j0.19$
500	$1.9 + j2.60$	$2.0 + j1.30$

Z_{OL}^* = Conjugate of the optimum load impedance into which the device operates at a given output power, voltage and frequency.

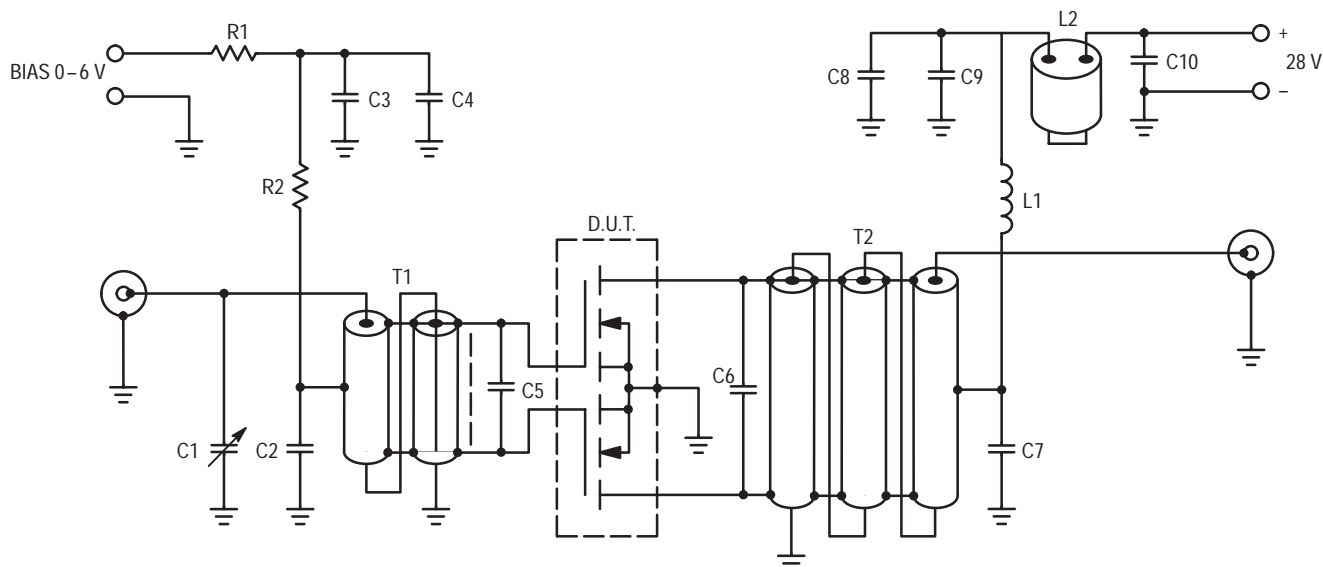
Note: Input and output impedance values given are measured from gate to gate and drain to drain respectively.

Figure 11. Series Equivalent Input/Output Impedance



B1	Balun, 50 Ω , 0.086" O.D. 2" Long, Semi Rigid Coax	L1, L2	#18 Wire, Hairpin Inductor
B2	Balun, 50 Ω , 0.141" O.D. 2" Long, Semi Rigid Coax	L3, L4	12 Turns #18, 0.340" I.D., Enameled Wire
C1, C2, C8, C9	270 pF, ATC Chip Capacitor	L5	Ferroxcube VK200 20/4B
C3, C5, C7	1.0–20 pF, Trimmer Capacitor	L6	3 Turns #16, 0.340" I.D., Enameled Wire
C4	15 pF, ATC Chip Capacitor	R1	1.0 k Ω , 1/4 W Resistor
C6	33 pF, ATC Chip Capacitor	R2, R3	10 k Ω , 1/4 W Resistor
C10, C12, C13,	0.01 μ F, Ceramic Capacitor	Z1, Z2	0.400" x 0.250", Microstrip Line
C16, C17		Z3, Z4	0.870" x 0.250", Microstrip Line
C11	1.0 μ F, 50 V, Tantalum	Z5, Z6	0.500" x 0.250", Microstrip Line
C14, C15	680 pF, Feedthru Capacitor	Board material	0.060" Teflon–fiberglass, $\epsilon_r = 2.55$, copper clad both sides, 2 oz. copper.
C18	20 μ F, 50 V, Tantalum		

Figure 12. 400 MHz Test Circuit



C1	8.0–60 pF, Arco 404
C2, C3, C7, C8	1000 pF, Chip Capacitor
C4, C9	0.1 μF, Chip Capacitor
C5	180 pF, Chip Capacitor
C6	100 pF and 130 pF, Chips in Parallel
C10	0.47 μF, Chip Capacitor, 1215 or Equivalent, Kemet
L1	10 Turns AWG #16, 1/4" I.D., Enamel Wire, Close Wound
L2	Ferrite Beads of Suitable Material for 1.5–2.0 μH Total Inductance

R1	100 Ω, 1/2 W
R2	1.0 k Ω, 1/2 W
T1	4:1 Impedance Ratio, RF Transformer Can Be Made of 25 Ω, Semi Rigid Coax, 47–52 Mils O.D.
T2	1:9 Impedance Ratio, RF Transformer. Can Be Made of 15–18 Ω, Semi Rigid Coax, 62–90 Mils O.D.

NOTE: For stability, the input transformer T1 should be loaded with ferrite toroids or beads to increase the common mode inductance. For operation below 100 MHz. The same is required for the output transformer.

Board material 062" fiberglass (G10),
 $\epsilon_r \cong 5$, Two sided, 1 oz. Copper.
 Unless otherwise noted, all chip capacitors
 are ATC Type 100 or Equivalent.

Figure 13. 225 MHz Test Circuit

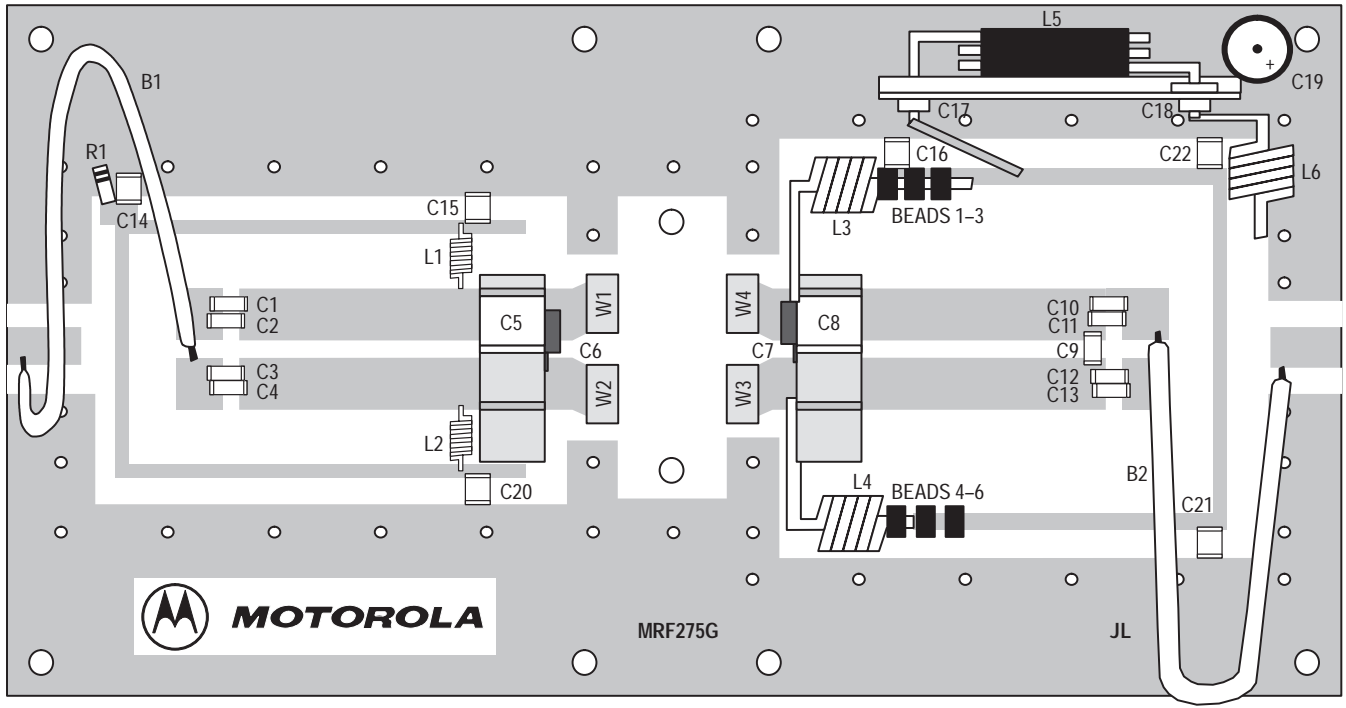


Figure 14. MRF275G Component Location (500 MHz)

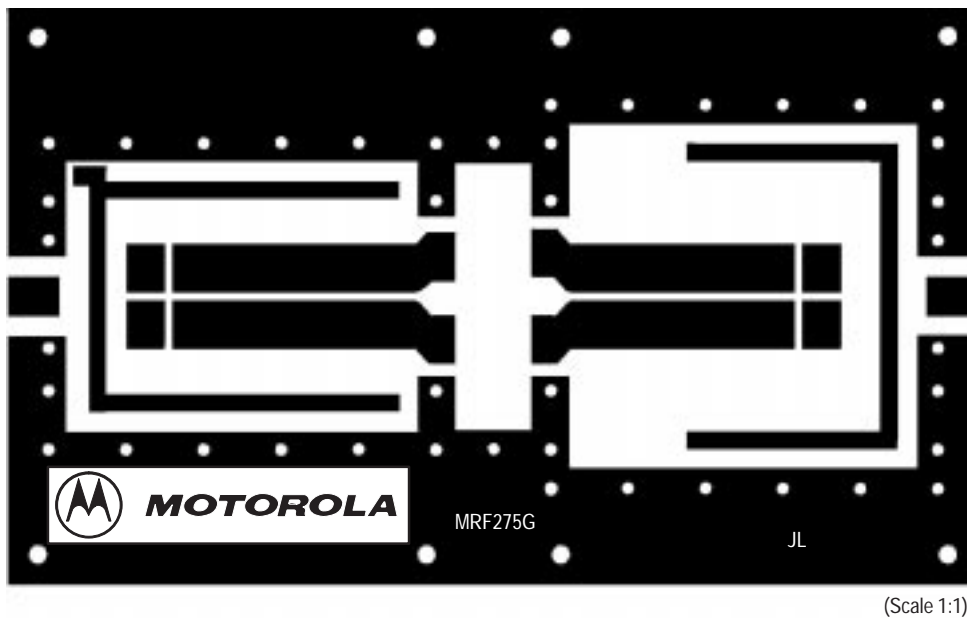


Figure 15. MRF275G Circuit Board Photo Master (500 MHz)
(Reduced 18% in printed data book, DL110/D)

NOTE: S-Parameter data represents measurements taken from one chip only.

Table 1. Common Source S-Parameters ($V_{DS} = 12\text{ V}$, $I_D = 4.5\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.822	-172	6.34	91	0.027	3	0.946	-173
40	0.846	-173	4.32	81	0.027	-6	0.859	-172
50	0.842	-174	3.62	79	0.027	-8	0.863	-175
60	0.838	-175	3.03	79	0.027	-5	0.923	-177
70	0.836	-175	2.76	80	0.028	-3	1.010	-178
80	0.841	-176	2.43	78	0.029	-4	1.080	-178
90	0.849	-176	2.19	74	0.029	-7	1.150	-176
100	0.857	-176	1.89	68	0.028	-13	1.110	-176
110	0.864	-176	1.66	63	0.026	-19	1.050	-177
120	0.868	-176	1.43	60	0.024	-19	0.958	-175
130	0.871	-176	1.25	59	0.023	-19	0.905	-176
140	0.874	-176	1.15	59	0.023	-17	0.914	-177
150	0.876	-176	1.11	59	0.023	-16	0.969	-178
160	0.880	-176	1.06	59	0.023	-17	1.060	-178
170	0.885	-177	1.01	55	0.023	-18	1.130	-177
180	0.891	-177	0.96	51	0.023	-23	1.190	-178
190	0.896	-177	0.87	45	0.022	-26	1.140	-179
200	0.900	-177	0.77	43	0.020	-26	1.050	-177
210	0.904	-177	0.69	42	0.018	-25	0.958	-176
220	0.907	-177	0.63	43	0.017	-23	0.924	-175
230	0.909	-177	0.60	43	0.018	-23	0.981	-178
240	0.912	-178	0.58	44	0.017	-22	0.981	-180
250	0.915	-178	0.58	42	0.017	-20	1.040	-179
260	0.918	-178	0.56	40	0.016	-20	1.150	-180
270	0.922	-178	0.54	34	0.015	-24	1.170	179
280	0.925	-179	0.49	32	0.014	-27	1.130	-180
290	0.927	-179	0.43	28	0.013	-27	1.010	-178
300	0.930	-179	0.41	30	0.013	-23	0.964	-178
310	0.932	-179	0.40	32	0.013	-14	0.936	-178
320	0.934	-180	0.39	31	0.012	-9	0.948	180
330	0.936	-180	0.35	32	0.011	-9	1.000	180
340	0.938	180	0.38	31	0.011	-12	1.070	178
350	0.941	180	0.35	28	0.011	-12	1.100	180
360	0.943	179	0.33	23	0.011	-10	1.120	-180
370	0.944	179	0.30	21	0.011	-4	1.080	180
380	0.945	179	0.29	21	0.009	1	1.020	180
390	0.947	179	0.28	22	0.008	3	0.966	-180
400	0.948	179	0.26	25	0.008	4	0.936	-179
410	0.949	178	0.26	24	0.010	5	1.010	179
420	0.951	178	0.25	25	0.010	11	1.040	178

Table 1. Common Source S-Parameters ($V_{DS} = 12\text{ V}$, $I_D = 4.5\text{ A}$) continued

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
430	0.952	178	0.25	22	0.010	19	1.080	177
440	0.953	177	0.24	19	0.009	22	1.100	178
450	0.955	177	0.24	16	0.008	21	1.100	179
460	0.956	177	0.21	15	0.008	11	1.080	177
470	0.956	177	0.20	16	0.009	16	0.992	178
480	0.957	176	0.19	18	0.010	27	0.975	179
490	0.958	176	0.19	18	0.010	40	0.974	178
500	0.960	176	0.19	19	0.010	46	1.010	177
600	0.956	175	0.18	12	0.007	49	0.940	175
700	0.958	172	0.11	14	0.018	61	0.989	173
800	0.962	170	0.10	12	0.029	51	0.967	172
900	0.965	168	0.08	16	0.021	72	0.973	170
1000	0.964	165	0.07	12	0.021	57	1.010	168

Table 2. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 0.35\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.829	-170	9.20	92	0.023	4	0.915	-171
40	0.858	-172	6.30	83	0.022	-4	0.834	-170
50	0.852	-173	5.28	80	0.023	-6	0.836	-174
60	0.846	-174	4.42	80	0.023	-3	0.892	-175
70	0.843	-175	4.01	81	0.024	-1	0.978	-177
80	0.847	-175	3.53	80	0.024	-2	1.050	-177
90	0.855	-175	3.18	76	0.024	-5	1.110	-176
100	0.865	-176	2.75	70	0.023	-10	1.080	-175
110	0.872	-176	2.43	65	0.022	-16	1.020	-176
120	0.874	-176	2.10	62	0.020	-16	0.932	-174
130	0.876	-176	1.84	61	0.019	-15	0.882	-175
140	0.878	-176	1.70	61	0.019	-14	0.889	-176
150	0.880	-176	1.63	61	0.019	-13	0.943	-177
160	0.883	-176	1.56	61	0.019	-13	1.030	-177
170	0.888	-177	1.49	58	0.019	-14	1.100	-176
180	0.894	-177	1.42	53	0.019	-18	1.160	-176
190	0.899	-177	1.29	47	0.018	-22	1.120	-177
200	0.902	-177	1.14	45	0.017	-24	1.030	-176
210	0.905	-177	1.02	44	0.015	-23	0.941	-175
220	0.907	-177	0.94	46	0.015	-19	0.903	-174
230	0.909	-178	0.89	45	0.015	-16	0.957	-177
240	0.912	-178	0.87	46	0.014	-15	0.961	-179
250	0.915	-178	0.86	44	0.014	-15	1.020	-178
260	0.918	-178	0.83	42	0.014	-17	1.120	-178
270	0.922	-178	0.80	36	0.013	-19	1.140	-180

Table 2. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 0.35\text{ mA}$) continued

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
280	0.925	-179	0.73	34	0.013	-20	1.110	-179
290	0.927	-179	0.65	32	0.011	-18	0.994	-177
300	0.929	-179	0.62	32	0.011	-15	0.948	-177
310	0.931	-179	0.60	34	0.010	-9	0.916	-177
320	0.932	-180	0.57	33	0.010	-6	0.934	-180
330	0.934	-180	0.53	34	0.010	-4	0.985	-180
340	0.937	180	0.56	33	0.010	-2	1.050	179
350	0.939	180	0.53	30	0.010	0	1.090	-179
360	0.941	179	0.50	25	0.010	0	1.110	-178
370	0.943	179	0.46	23	0.009	0	1.080	-179
380	0.944	179	0.44	22	0.009	2	1.010	-179
390	0.945	179	0.41	24	0.008	8	0.956	-179
400	0.946	178	0.40	27	0.008	16	0.926	-178
410	0.947	178	0.38	26	0.009	20	1.000	-180
420	0.949	178	0.38	26	0.009	22	1.040	179
430	0.950	178	0.37	23	0.009	25	1.070	179
440	0.952	177	0.36	21	0.009	26	1.090	180
450	0.953	177	0.36	18	0.009	28	1.090	-180
460	0.954	177	0.31	17	0.009	24	1.070	178
470	0.955	177	0.30	17	0.009	29	0.990	179
480	0.956	176	0.29	19	0.009	36	0.963	-179
490	0.957	176	0.29	20	0.010	45	0.959	180
500	0.958	176	0.28	20	0.010	50	0.996	178
600	0.956	175	0.24	12	0.006	90	0.924	176
700	0.959	172	0.16	13	0.019	63	0.986	174
800	0.963	170	0.14	10	0.023	63	0.963	173
900	0.968	168	0.12	11	0.026	84	0.967	171
1000	0.969	165	0.09	7	0.025	70	1.000	169

Table 3. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.39\text{ mA}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.834	-169	10.08	93	0.021	4	0.807	-171
40	0.863	-172	6.91	83	0.021	-4	0.828	-170
50	0.857	-173	5.79	81	0.021	-5	0.830	-173
60	0.851	-174	4.86	81	0.022	-3	0.883	-175
70	0.848	-175	4.41	82	0.022	-1	0.970	-177
80	0.852	-175	3.87	80	0.022	-1	1.040	-177
90	0.860	-175	3.49	77	0.023	-5	1.100	-176
100	0.869	-176	3.03	71	0.022	-9	1.070	-175
110	0.876	-176	2.68	66	0.021	-14	1.010	-176
120	0.878	-176	2.31	63	0.019	-14	0.923	-174
130	0.879	-176	2.03	62	0.018	-15	0.876	-175

Table 3. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 0.39\text{ mA}$) continued

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
140	0.881	-176	1.87	62	0.018	-13	0.884	-176
150	0.883	-176	1.79	62	0.018	-11	0.934	-177
160	0.886	-177	1.72	62	0.018	-11	1.020	-177
170	0.890	-177	1.64	58	0.018	-12	1.090	-176
180	0.896	-177	1.56	54	0.018	-16	1.150	-176
190	0.901	-177	1.42	48	0.018	-21	1.110	-177
200	0.904	-177	1.26	46	0.017	-19	1.030	-176
210	0.907	-177	1.13	45	0.015	-14	0.938	-175
220	0.908	-177	1.03	47	0.013	-13	0.897	-174
230	0.910	-178	0.99	46	0.014	-15	0.948	-176
240	0.912	-178	0.96	47	0.014	-13	0.956	-179
250	0.916	-178	0.95	45	0.014	-10	1.020	-178
260	0.919	-178	0.93	42	0.013	-12	1.120	-178
270	0.922	-179	0.89	37	0.012	-15	1.140	-179
280	0.925	-179	0.81	35	0.012	-16	1.110	-178
290	0.927	-179	0.72	33	0.011	-16	0.988	-176
300	0.929	-179	0.69	33	0.011	-10	0.944	-177
310	0.931	-179	0.66	35	0.012	5	0.920	-177
320	0.933	-180	0.63	34	0.011	16	0.936	-180
330	0.934	-180	0.59	35	0.009	14	0.989	-180
340	0.937	180	0.62	34	0.009	3	1.050	180
350	0.939	180	0.59	31	0.010	4	1.080	-179
360	0.941	179	0.55	26	0.010	8	1.110	-178
370	0.943	179	0.51	24	0.009	11	1.070	-179
380	0.944	179	0.49	23	0.008	17	1.010	-178
390	0.945	179	0.46	25	0.008	24	0.949	-178
400	0.946	178	0.44	27	0.007	20	0.922	-178
410	0.947	178	0.43	26	0.010	19	0.995	-180
420	0.949	178	0.42	27	0.012	29	1.030	179
430	0.950	178	0.41	24	0.010	41	1.060	179
440	0.951	177	0.40	21	0.008	40	1.090	180
450	0.953	177	0.39	19	0.008	34	1.090	-180
460	0.953	177	0.35	17	0.009	26	1.070	178
470	0.954	177	0.33	18	0.010	30	0.983	179
480	0.955	176	0.32	19	0.012	43	0.964	-180
490	0.956	176	0.32	20	0.012	60	0.956	179
500	0.957	176	0.31	21	0.010	65	0.993	178
600	0.955	174	0.26	13	0.012	67	0.926	176
700	0.958	172	0.18	12	0.018	64	0.984	174
800	0.963	170	0.15	9	0.020	89	0.961	173
900	0.966	168	0.13	9	0.028	81	0.967	171
1000	0.968	165	0.10	6	0.033	73	0.997	169

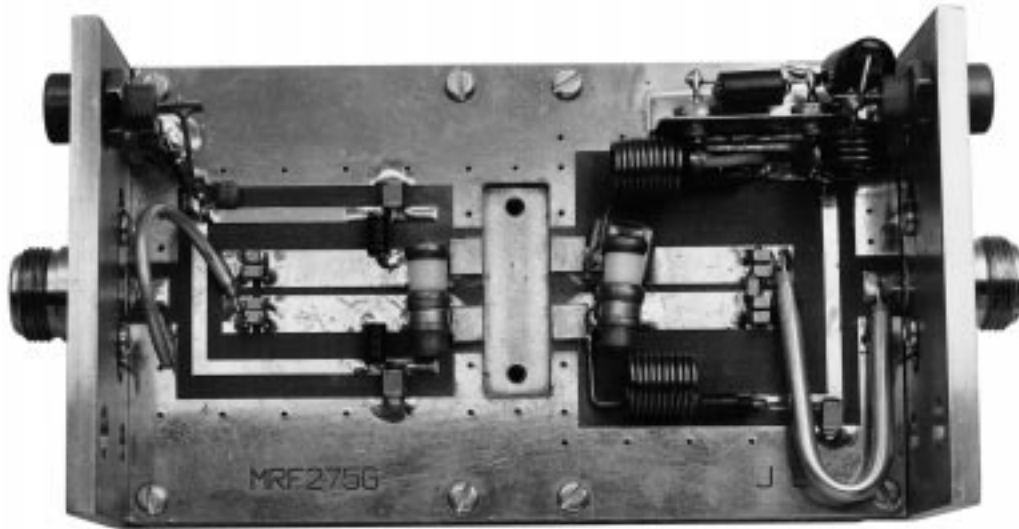


Figure 16. MRF275G Test Fixture

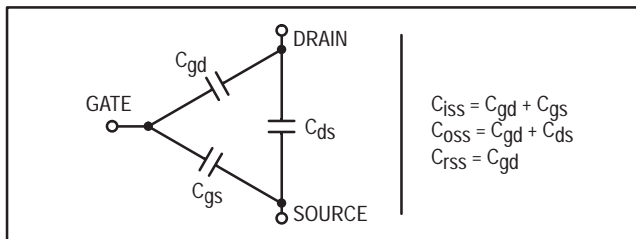
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the MOSFET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iSS}), output (C_{oSS}) and reverse transfer (C_{rSS}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iSS} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



The C_{iSS} given in the electrical characteristics table was measured using method 2 above. It should be noted that C_{iSS} , C_{oSS} , C_{rSS} are measured at zero drain current and are provided for general information about the device. They are not RF design parameters and no attempt should be made to use them as such.

DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating (or any of the maximum ratings on the front page). Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of this device are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

Using a resistor to keep the gate-to-source impedance low also helps damp transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate

may be large enough to exceed the gate–threshold voltage and turn the device on.

HANDLING CONSIDERATIONS

When shipping, the devices should be transported only in antistatic bags or conductive foam. Upon removal from the packaging, careful handling procedures should be adhered to. Those handling the devices should wear grounding straps and devices not in the antistatic packaging should be kept in metal tote bins. MOSFETs should be handled by the case and not by the leads, and when testing the device, all leads should make good electrical contact before voltage is applied. As a final note, when placing the FET into the system it is designed for, soldering should be done with grounded equipment.

DESIGN CONSIDERATIONS

The MRF275G is a RF power N–channel enhancement mode field–effect transistor (FETs) designed for HF, VHF and UHF power amplifier applications. Motorola RF MOSFETs feature a vertical structure with a planar design.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power FETs include high gain, low noise, simple bias systems, relative immunity from

thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal.

DC BIAS

The MRF275G is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF275G was characterized at $I_{DQ} = 100$ mA, each side, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may be just a simple resistive divider network. Some applications may require a more elaborate bias system.

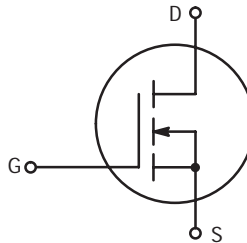
GAIN CONTROL

Power output of the MRF275G may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems.

The RF MOSFET Line
RF Power
Field-Effect Transistor
N-Channel Enhancement-Mode

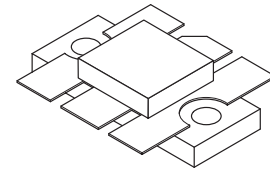
Designed for broadband commercial and military applications using single ended circuits at frequencies to 500 MHz. The high power, high gain and broadband performance of this device makes possible solid state transmitters for FM broadcast or TV channel frequency bands.

- Guaranteed Performance @ 500 MHz, 28 Vdc
Output Power — 100 Watts
Power Gain — 8.8 dB Typ
Efficiency — 55% Typ
- 100% Ruggedness Tested At Rated Output Power
- Low Thermal Resistance
- Low C_{RSS} — 17 pF Typ @ $V_{DS} = 28$ Volts
- S-Parameters Available for Download into Frequency Domain Simulators.
See <http://mot-sps.com/rf/designtds/>



MRF275L

100 W, 28 V, 500 MHz
N-CHANNEL
BROADBAND
RF POWER FET



CASE 333-04, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current — Continuous	I_D	13	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	270 1.54	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.65	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 50$ mA)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28$ V, $V_{GS} = 0$)	I_{DSS}	—	—	2.5	mAdc
Gate-Body Leakage Current ($V_{GS} = 20$ V, $V_{DS} = 0$)	I_{GSS}	—	—	1.0	μAdc

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

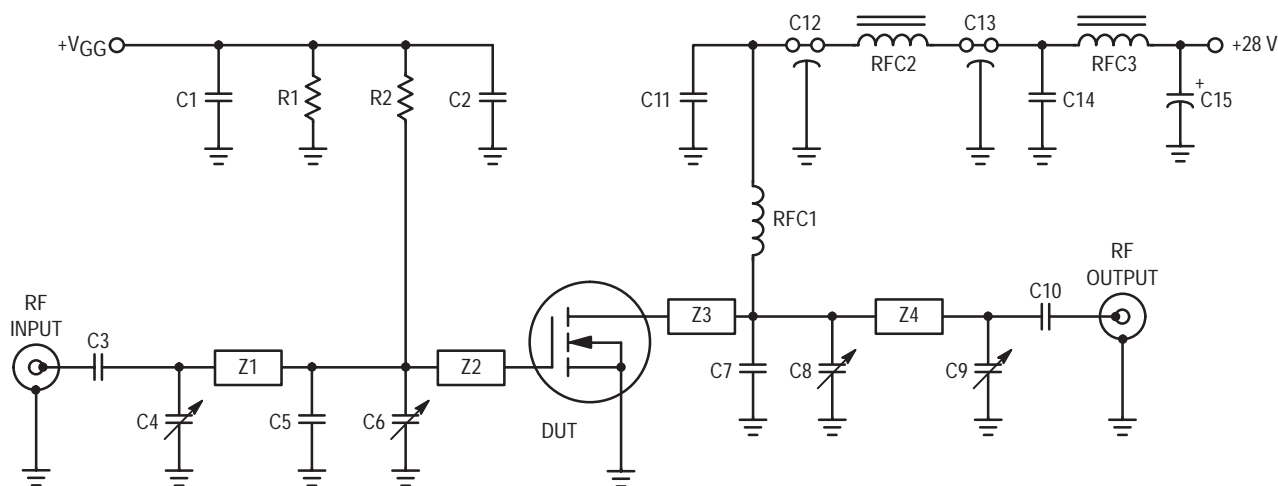
Characteristic	Symbol	Min	Typ	Max	Unit
Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 100\text{ mA}$)	$V_{GS(th)}$	1.5	2.5	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 5.0\text{ A}$)	$V_{DS(on)}$	0.5	0.9	1.5	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 2.5\text{ A}$)	g_{fs}	3.0	3.75	—	mhos

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{iss}	—	135	—	pF
Output Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{oss}	—	140	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{rss}	—	17	—	pF

FUNCTIONAL CHARACTERISTICS

Common Source Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	G_{ps}	7.5	8.8	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$)	η	50	55	—	%
Electrical Ruggedness ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W}$, $f = 500\text{ MHz}$, $I_{DQ} = 100\text{ mA}$, VSWR 10:1 at all Phase Angles)	ψ	No Degradation in Output Power			



- | | | | |
|----------------|---|----------------|---------------------------------------|
| C1, C11, C14 | 0.1 μF , Ceramic Capacitor | RFC1 | 8 Turns AWG #18, 0.25" I.D., Enameled |
| C2 | 240 pF, ATC Type Chip Capacitor | RFC2, RFC3 | Ferroxcube VK200 19/4B |
| C3, C10 | 270 pF, ATC Type Chip Capacitor | Z1, | 0.250" x 0.800", Microstrip Line |
| C4, C6, C8, C9 | 1–20 pF, Trimmer Capacitor, Johansen | Z2, Z3 | 0.250" x 0.400", Microstrip Line |
| C5 | 24 pF, Mini–Unelco Type Capacitor | Z4 | 0.250" x 1.25", Microstrip Line |
| C7 | 24 pF, Mini–Unelco Type Capacitor | Board Material | 0.062" Glass Teflon [®] , |
| C12, C13 | 680 pF, Feedthru Capacitors | | 2 oz. Copper, Double Clad Copper |
| C15 | 10 μF , 50 V, Electrolytic Capacitor | | Board, $\epsilon_r = 2.55$ |

Figure 1. 500 MHz Test Circuit

TYPICAL CHARACTERISTICS

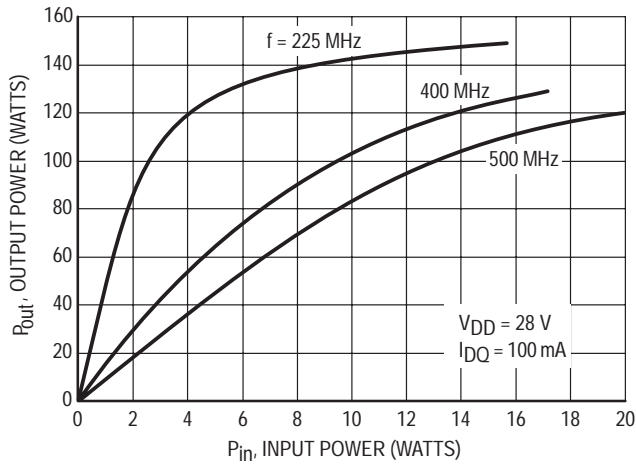


Figure 2. Output Power versus Input Power

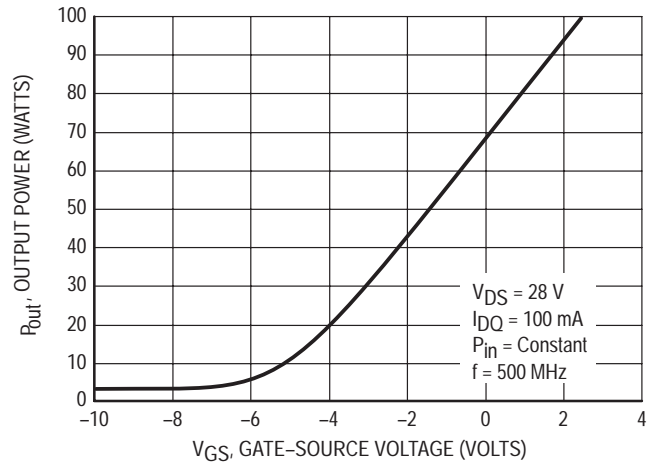


Figure 3. Output Power versus Gate Voltage

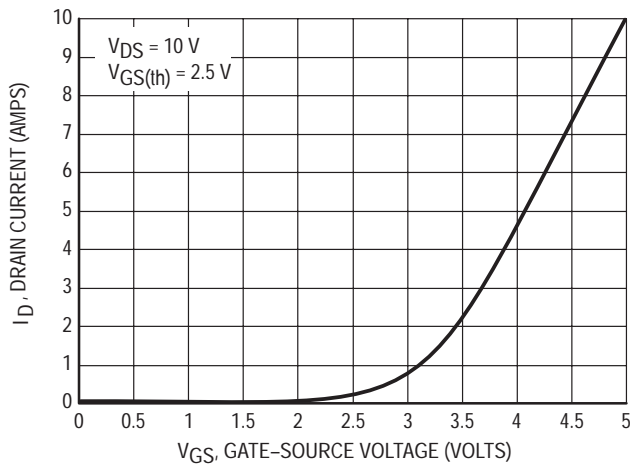


Figure 4. Drain Current versus Gate Voltage (Transfer Characteristics)

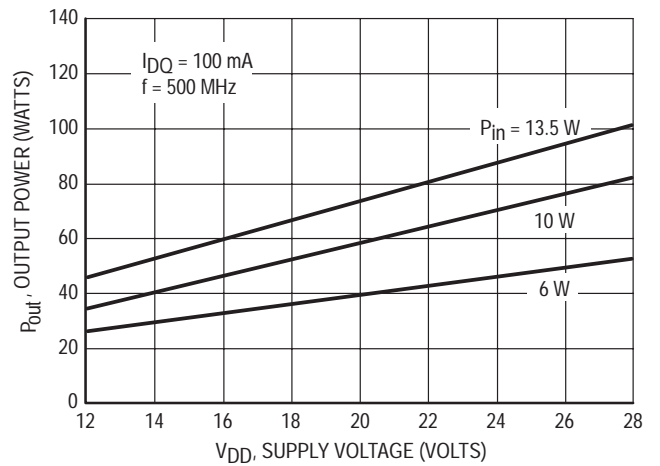


Figure 5. Output Power versus Supply Voltage

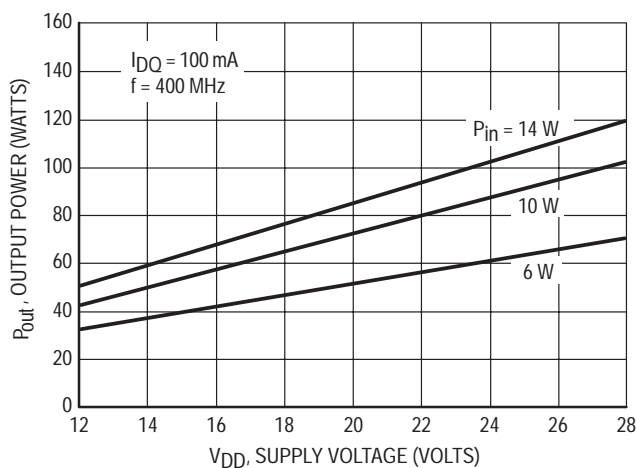


Figure 6. Output Power versus Supply Voltage

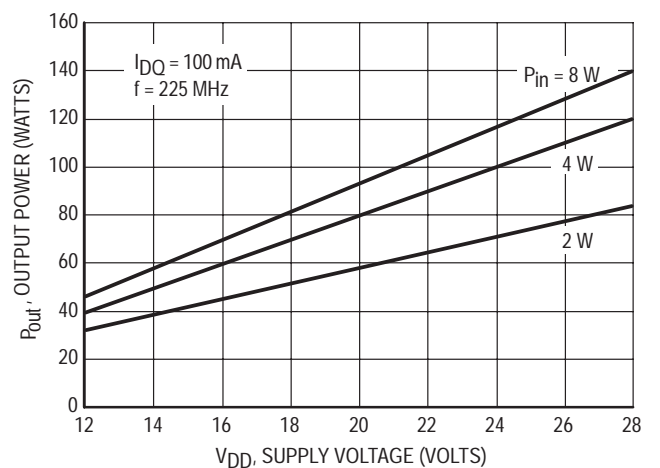


Figure 7. Output Power versus Supply Voltage

TYPICAL CHARACTERISTICS

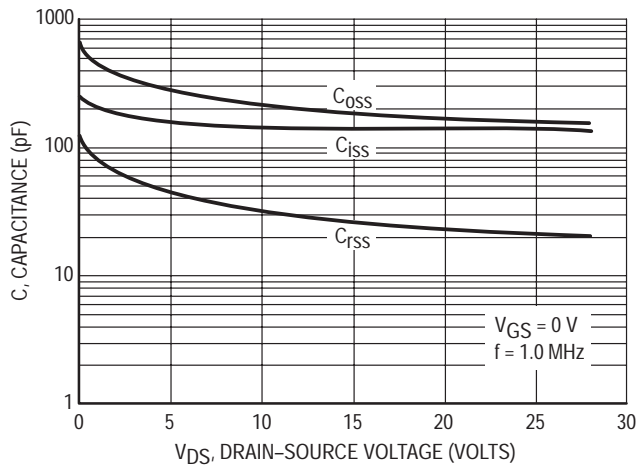


Figure 8. Capacitance versus Drain-Source Voltage

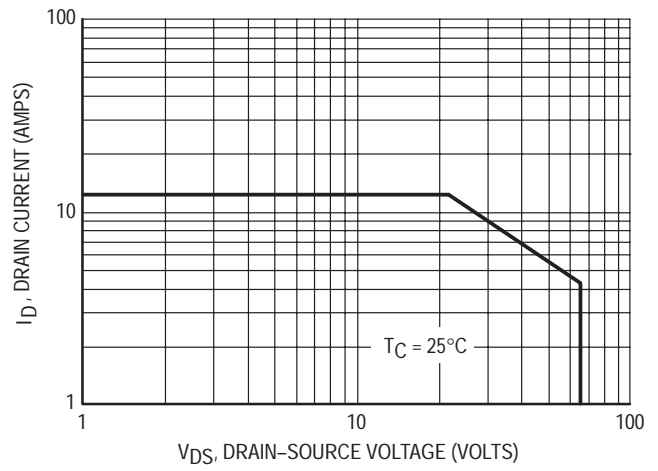
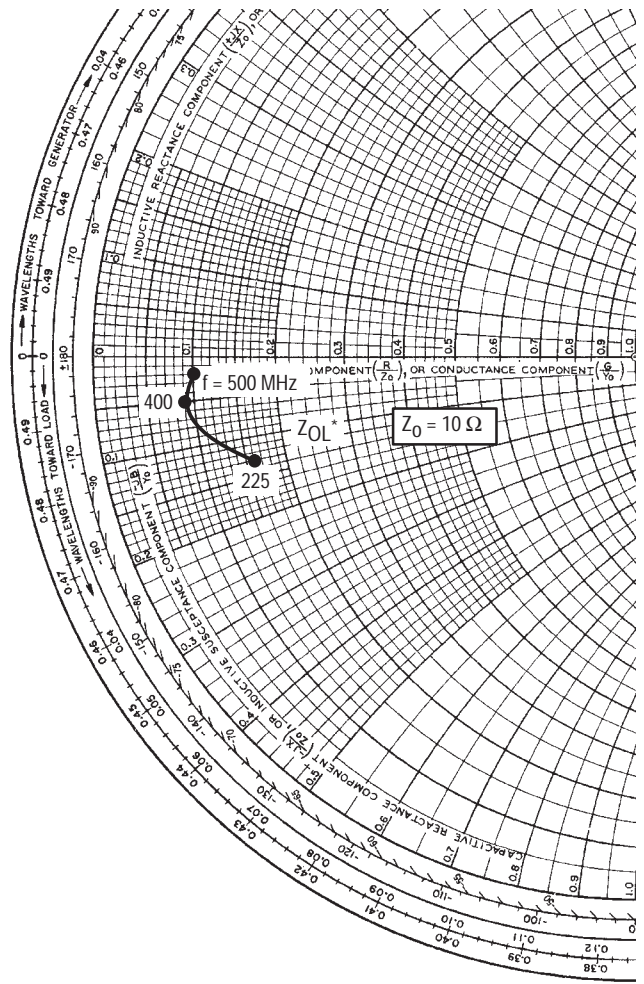
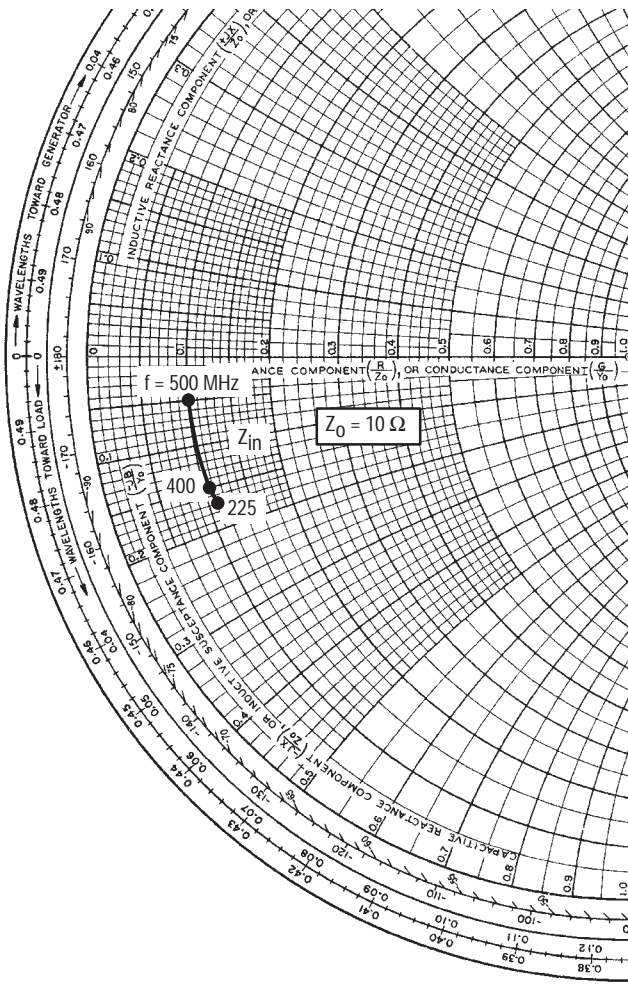


Figure 9. DC Safe Operating Area



$V_{DD} = 28\text{ V}$, $I_{DQ} = 100\text{ mA}$, $P_{out} = 100\text{ W}$

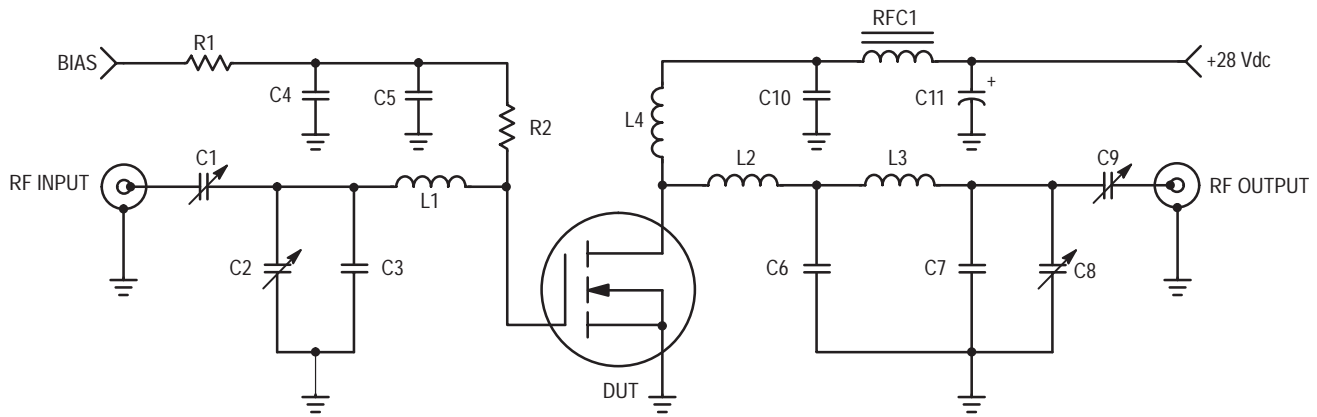
f (MHz)	Z_{in} Ohms
225	$1.1 - j1.7$
400	$1.08 - j1.5$
500	$1.0 - j0.5$

$V_{DD} = 28\text{ V}$, $I_{DQ} = 100\text{ mA}$, $P_{out} = 100\text{ W}$

f (MHz)	Z_{OL}^* Ohms
225	$1.6 - j1.3$
400	$0.9 - j0.5$
500	$1.0 - j0.2$

Z_{OL}^* = Conjugate of the optimum load impedance into which the device operates at a given output power, voltage and frequency.

Figure 10. Series Equivalent Input/Output Impedance



C1, C2, C8	Arco 463 or Equivalent	L1	Hairpin Inductor #18 Wire	L3	Hairpin Inductor #16 Wire
C3, C7	25 pF, Unelco Capacitor				
C4	1000 pF, Chip Capacitor				
C5	0.01 μ F, Chip Capacitor				
C6	250 pF, Unelco Capacitor				
C9	Arco 462 or Equivalent				
C10	1000 pF, ATC Chip Capacitor				
C11	10 μ F, 100 V, Electrolytic Capacitor	L2	Stripline Inductor 0.200" x 0.500"	L4	2 Turns #16 Wire, 5/16" ID
				RFC1	VK200-4B
				R1	1.0 k, 1/4 W Resistor
				R2	100 Ω Resistor

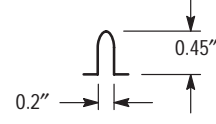
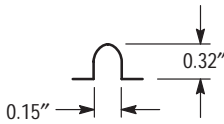
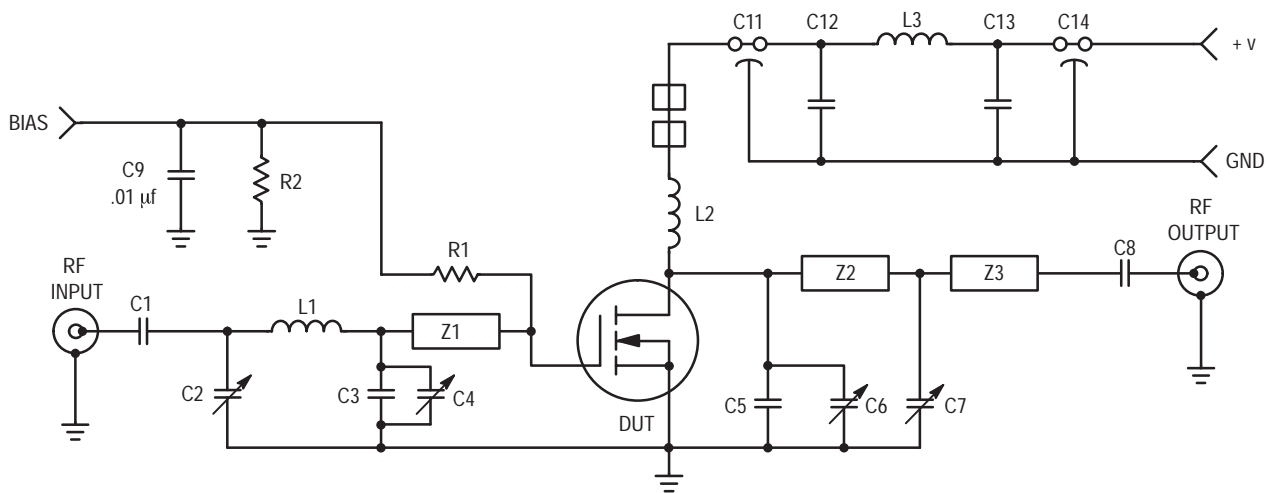


Figure 11. 225 MHz Test Circuit



C1, C8	270 pF, ATC Chip Capacitor	L1	Hairpin Inductor #18 Wire	R1	10 k, 1/4 W Resistor
C2, C4, C6, C7	1.0–20 pF, Trimmer Capacitor			R2	1 k, 1/4 W Resistor
C3	15 pF, Mini Unelco Capacitor			R3	1.5 k, 1/4 W Resistor
C5	47 pF, Mini Unelco Capacitor			Z1	0.950" x 0.250", Microstrip Line
C9, C12	0.1 μ F, Ceramic Capacitor			Z2	1.25" x 0.250", Microstrip Line
C11, C14	680 pF, Feed Thru Capacitor			Z3	0.300" x 0.250", Microstrip Line
C13	50 μ F, Tantalum Capacitor	L2	12 Turns #18 Wire, 0.450" ID	Board Material	0.062" Teflon [®] , Fiberglass, 1 oz. Copper, Clad Both Sides, $\epsilon_r = 2.56$
		L3	Ferroxcube VK200 20/4B		

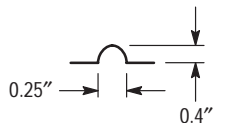
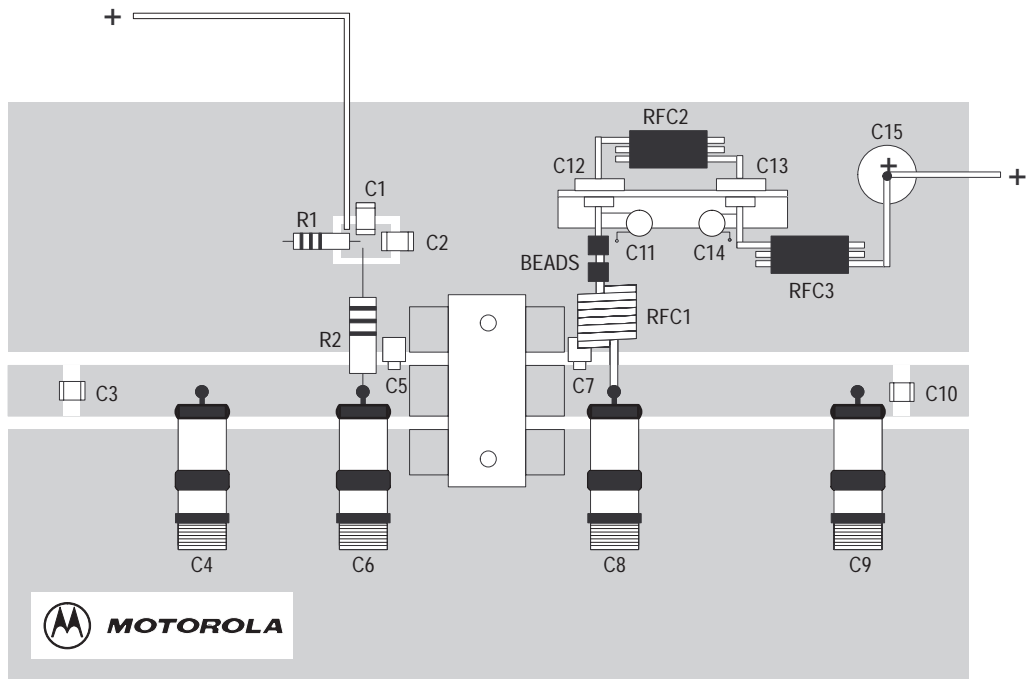
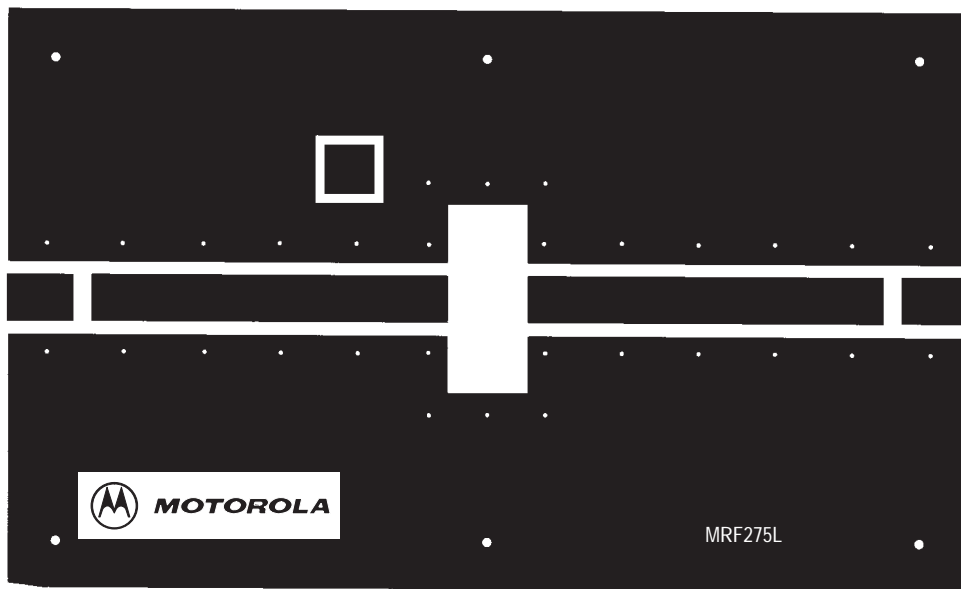


Figure 12. 400 MHz Test Circuit



(Not to Scale)

Figure 13. MRF275L Component Location (500 MHz)



(Scale 1:1)

Figure 14. MRF275L Test Circuit Photomaster
(Reduced 18% in printed data book, DL110/D)

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 4.5\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.936	-176	6.22	87	0.010	21	0.944	-179
40	0.938	-178	4.28	87	0.010	24	0.930	-177
50	0.937	-178	3.65	83	0.010	29	0.922	179
60	0.937	-179	2.99	83	0.011	34	0.920	179
70	0.938	-179	2.54	81	0.011	39	0.917	179
80	0.938	-179	2.18	80	0.012	42	0.913	179
90	0.939	-180	1.94	78	0.012	44	0.909	180
100	0.939	-180	1.77	77	0.013	47	0.913	-180
110	0.939	180	1.57	77	0.015	50	0.916	-179
120	0.940	180	1.45	74	0.015	54	0.914	179
130	0.940	179	1.34	75	0.016	57	0.935	180
140	0.940	179	1.26	72	0.016	58	0.943	180
150	0.940	179	1.19	71	0.017	57	0.951	178
160	0.941	179	1.09	70	0.019	58	0.943	179
170	0.941	179	1.01	69	0.019	62	0.940	180
180	0.941	179	0.956	68	0.021	64	0.948	179
190	0.941	178	0.912	67	0.022	65	0.957	180
200	0.942	178	0.860	65	0.022	65	0.941	178
210	0.942	178	0.816	64	0.023	65	0.931	178
220	0.943	178	0.779	63	0.025	66	0.922	178
230	0.943	177	0.717	60	0.027	67	0.965	177
240	0.943	177	0.709	61	0.026	68	0.927	176
250	0.944	177	0.674	60	0.026	70	0.924	178
260	0.944	177	0.645	58	0.028	69	0.930	179
270	0.944	177	0.627	57	0.030	70	0.933	178
280	0.945	176	0.608	58	0.032	70	0.940	177
290	0.946	176	0.580	54	0.031	71	0.941	175
300	0.946	176	0.569	56	0.033	71	0.945	176
310	0.946	176	0.539	55	0.033	72	0.953	178
320	0.947	175	0.512	54	0.035	71	0.952	177
330	0.948	175	0.483	51	0.037	72	0.927	176
340	0.947	175	0.477	52	0.038	72	0.921	176
350	0.947	175	0.466	51	0.039	75	0.929	178
360	0.947	175	0.459	51	0.040	73	0.963	177
370	0.948	174	0.441	50	0.043	71	0.968	175
380	0.949	174	0.428	49	0.044	72	0.937	175
390	0.949	174	0.417	49	0.045	74	0.907	176
400	0.949	174	0.409	47	0.044	77	0.912	177
410	0.950	173	0.390	46	0.046	74	0.962	175
420	0.950	173	0.377	45	0.047	71	0.971	174
430	0.950	173	0.369	45	0.050	72	0.948	176
440	0.951	173	0.368	47	0.052	74	0.953	176

Table 1. Common Source S-Parameters ($V_{DS} = 12.5\text{ V}$, $I_D = 4.5\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
450	0.951	172	0.371	42	0.053	76	0.943	175
460	0.952	172	0.347	44	0.053	72	0.965	172
470	0.952	172	0.331	43	0.053	71	0.933	173
480	0.953	172	0.323	43	0.056	71	0.936	173
490	0.953	171	0.317	41	0.059	72	0.965	173
500	0.954	171	0.306	41	0.061	74	0.963	173
600	0.957	168	0.267	35	0.069	77	0.941	171
700	0.965	165	0.224	35	0.090	70	0.958	169
800	0.967	160	0.219	32	0.099	67	0.937	164
900	0.980	156	0.214	33	0.114	69	0.943	164
1000	0.986	151	0.218	34	0.146	67	0.955	162

Table 2. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 4.5\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.914	-174	9.08	87	0.011	19	0.882	-178
40	0.918	-176	6.29	86	0.011	22	0.876	-176
50	0.918	-177	5.31	82	0.011	26	0.871	180
60	0.917	-177	4.35	82	0.012	29	0.871	-179
70	0.919	-178	3.70	79	0.012	32	0.865	-179
80	0.919	-178	3.16	77	0.013	37	0.857	-179
90	0.920	-179	2.81	75	0.013	42	0.851	-180
100	0.921	-179	2.55	74	0.014	46	0.863	-179
110	0.922	-179	2.27	73	0.014	47	0.876	-178
120	0.923	-179	2.08	70	0.015	49	0.867	-179
130	0.923	-180	1.92	70	0.016	51	0.880	-178
140	0.924	-180	1.78	67	0.017	55	0.880	-179
150	0.925	-180	1.68	65	0.018	58	0.904	179
160	0.926	180	1.53	64	0.018	60	0.901	-180
170	0.927	180	1.42	62	0.018	61	0.900	-179
180	0.928	180	1.34	62	0.020	61	0.901	-179
190	0.929	179	1.28	60	0.021	63	0.906	-179
200	0.930	179	1.19	58	0.022	65	0.892	179
210	0.931	179	1.12	56	0.022	67	0.902	178
220	0.932	179	1.06	55	0.023	68	0.903	179
230	0.933	179	0.988	53	0.024	67	0.931	179
240	0.934	178	0.960	53	0.025	69	0.889	179
250	0.934	178	0.910	52	0.026	73	0.877	180
260	0.935	178	0.866	50	0.026	74	0.895	180
270	0.936	178	0.838	49	0.027	74	0.908	180
280	0.937	177	0.803	49	0.029	71	0.923	179
290	0.939	177	0.766	46	0.030	72	0.915	177

Table 2. Common Source S-Parameters ($V_{DS} = 24\text{ V}$, $I_D = 4.5\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
300	0.939	177	0.744	46	0.032	76	0.907	178
310	0.939	177	0.702	46	0.032	81	0.908	180
320	0.940	176	0.660	45	0.031	81	0.913	178
330	0.941	176	0.623	41	0.031	75	0.909	177
340	0.942	176	0.613	42	0.035	71	0.910	178
350	0.943	176	0.599	41	0.039	78	0.905	-180
360	0.943	175	0.585	41	0.040	83	0.913	179
370	0.943	175	0.556	39	0.037	85	0.924	176
380	0.944	175	0.534	38	0.035	80	0.922	175
390	0.944	175	0.512	38	0.037	73	0.907	176
400	0.946	174	0.503	37	0.043	76	0.906	179
410	0.948	174	0.482	36	0.049	81	0.944	177
420	0.948	174	0.464	35	0.047	87	0.940	176
430	0.947	174	0.450	36	0.040	88	0.912	176
440	0.947	173	0.440	36	0.039	79	0.947	176
450	0.948	173	0.445	32	0.047	73	0.944	177
460	0.951	173	0.414	32	0.057	75	0.959	174
470	0.952	173	0.397	32	0.057	86	0.913	176
480	0.951	172	0.387	33	0.050	95	0.908	175
490	0.950	172	0.376	31	0.042	90	0.941	174
500	0.950	172	0.361	31	0.044	74	0.963	175
600	0.957	168	0.287	24	0.073	75	0.932	172
700	0.965	164	0.231	24	0.091	70	0.952	169
800	0.966	160	0.216	23	0.091	67	0.928	163
900	0.979	156	0.205	27	0.112	69	0.930	164
1000	0.981	150	0.206	29	0.146	58	0.947	162

Table 3. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 4.5\text{ A}$)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.910	-173	9.76	87	0.011	17	0.872	-177
40	0.913	-175	6.73	86	0.011	17	0.860	-174
50	0.913	-176	5.69	81	0.011	21	0.849	-179
60	0.913	-177	4.66	81	0.012	26	0.846	-178
70	0.915	-177	3.97	78	0.012	31	0.853	-179
80	0.916	-178	3.39	76	0.012	33	0.858	-178
90	0.916	-178	3.01	74	0.012	34	0.853	-178
100	0.917	-178	2.73	73	0.013	36	0.851	-177
110	0.918	-179	2.42	72	0.014	41	0.849	-177
120	0.919	-179	2.22	68	0.014	48	0.853	-178
130	0.920	-179	2.05	68	0.014	52	0.879	-178
140	0.921	-179	1.90	66	0.014	52	0.894	-178
150	0.922	-180	1.79	64	0.015	51	0.898	-178

Table 3. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 4.5\text{ A}$) (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
160	0.923	-180	1.63	63	0.016	53	0.880	-177
170	0.924	-180	1.50	61	0.017	58	0.890	-178
180	0.925	180	1.42	60	0.019	62	0.904	-178
190	0.926	180	1.35	58	0.019	64	0.922	-179
200	0.928	179	1.26	56	0.019	63	0.914	-179
210	0.929	179	1.19	54	0.020	62	0.897	-179
220	0.930	179	1.12	53	0.022	64	0.881	-179
230	0.932	179	1.04	51	0.024	67	0.907	180
240	0.932	179	1.01	51	0.024	69	0.892	179
250	0.933	178	0.955	49	0.024	70	0.910	-180
260	0.934	178	0.912	47	0.025	70	0.912	-178
270	0.936	178	0.882	46	0.027	71	0.904	-178
280	0.936	178	0.842	46	0.029	72	0.901	-180
290	0.938	177	0.798	43	0.028	71	0.920	177
300	0.939	177	0.770	44	0.030	71	0.930	178
310	0.939	177	0.731	43	0.032	72	0.934	-179
320	0.941	177	0.690	42	0.035	74	0.939	-180
330	0.942	176	0.655	39	0.036	76	0.895	180
340	0.942	176	0.639	40	0.035	75	0.892	179
350	0.942	176	0.613	39	0.036	75	0.906	-180
360	0.943	175	0.601	38	0.040	71	0.945	179
370	0.945	175	0.577	36	0.045	71	0.960	178
380	0.946	175	0.555	35	0.047	74	0.928	178
390	0.947	175	0.531	35	0.045	79	0.893	178
400	0.946	174	0.518	34	0.042	80	0.892	179
410	0.947	174	0.492	33	0.044	72	0.948	176
420	0.948	174	0.472	32	0.049	67	0.960	176
430	0.950	173	0.462	32	0.056	71	0.936	179
440	0.951	173	0.455	32	0.058	78	0.945	179
450	0.951	173	0.460	30	0.054	82	0.920	177
460	0.950	173	0.424	30	0.050	73	0.951	173
470	0.950	172	0.400	29	0.053	65	0.937	174
480	0.952	172	0.389	29	0.063	65	0.941	175
490	0.954	172	0.382	27	0.071	72	0.960	175
500	0.955	172	0.367	27	0.069	80	0.954	176
600	0.958	168	0.284	22	0.071	80	0.935	172
700	0.967	164	0.226	22	0.088	71	0.950	169
800	0.967	160	0.211	22	0.096	67	0.929	164
900	0.979	156	0.197	26	0.116	69	0.929	165
1000	0.978	150	0.200	29	0.139	67	0.944	163

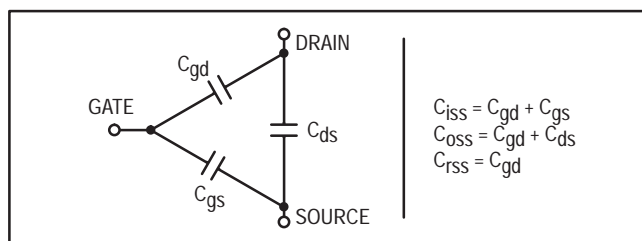
RF POWER MOSFET CONSIDERATIONS

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between the terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during the fabrication of the FET results in a junction capacitance from drain-to-source (C_{ds}).

These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate. In the latter case the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $V_{DS(on)}$, occurs in the linear region of the output characteristic and is specified under specific test conditions for gate-source voltage and drain current. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient and constitutes an important design consideration at high temperatures, because it contributes to the power dissipation within the device.

GATE CHARACTERISTICS

The gate of the FET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The input resistance is very high — on the order of 10^9 ohms — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage slightly in excess of the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended.

Using a resistor to keep the gate-to-source impedance low also helps damp transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

HANDLING CONSIDERATIONS

When shipping, the devices should be transported only in antistatic bags or conductive foam. Upon removal from the packaging, careful handling procedures should be adhered to. Those handling the devices should wear grounding straps and devices not in the antistatic packaging should be kept in metal tote bins. MOSFETs should be handled by the case and not by the leads, and when testing the device, all leads should make good electrical contact before voltage is applied. As a final note, when placing the FET into the system it is designed for, soldering should be done with a grounded iron.

DESIGN CONSIDERATIONS

The MRF275L is a RF power N-channel enhancement mode field-effect transistor (FETs) designed for HF, VHF and UHF power amplifier applications. Motorola FETs feature a vertical structure with a planar design.

Motorola Application Note AN211A, FETs in Theory and Practice, is suggested reading for those not familiar with the construction and characteristics of FETs.

The major advantages of RF power FETs include high gain, low noise, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage. Power output can be varied over a wide range with a low power dc control signal.

DC BIAS

The MRF275L is an enhancement mode FET and, therefore, does not conduct when drain voltage is applied. Drain current flows when a positive voltage is applied to the gate. RF power FETs require forward bias for optimum performance. The value of quiescent drain current (I_{DQ}) is not critical for many applications. The MRF275L was characterized at $I_{DQ} = 100$ mA, each side, which is the suggested minimum value of I_{DQ} . For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may be just a simple resistive divider network. Some applications may require a more elaborate bias system.

GAIN CONTROL

Power output of the MRF275L may be controlled from its rated value down to zero (negative gain) by varying the dc gate voltage. This feature facilitates the design of manual gain control, AGC/ALC and modulation systems.

The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

MRF281SR1
MRF281ZR1

Designed for digital and analog cellular PCN and PCS base station applications at frequencies from 1000 to 2500 MHz. Characterized for operation Class A and Class AB at 26 volts in commercial and industrial applications.

- Specified Two-Tone Performance @ 1930 and 2000 MHz, 26 Volts
Output Power = 4 Watts PEP
Power Gain = 11 dB
Efficiency = 30%
Intermodulation Distortion = -29 dBc
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 2000 MHz, 4 Watts CW Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- S-Parameter Characterization at High Bias Levels
- Available in Tape and Reel. R1 Suffix = 500 Units per 12 mm, 7 inch Reel.
- LDMOS Models Available at <http://www.motorola.com/semiconductors/rf/models/>

2000 MHz, 4 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 458B-02, STYLE 1
(MRF281SR1)



CASE 458C-02, STYLE 1
(MRF281ZR1)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	20 0.115	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	5.74	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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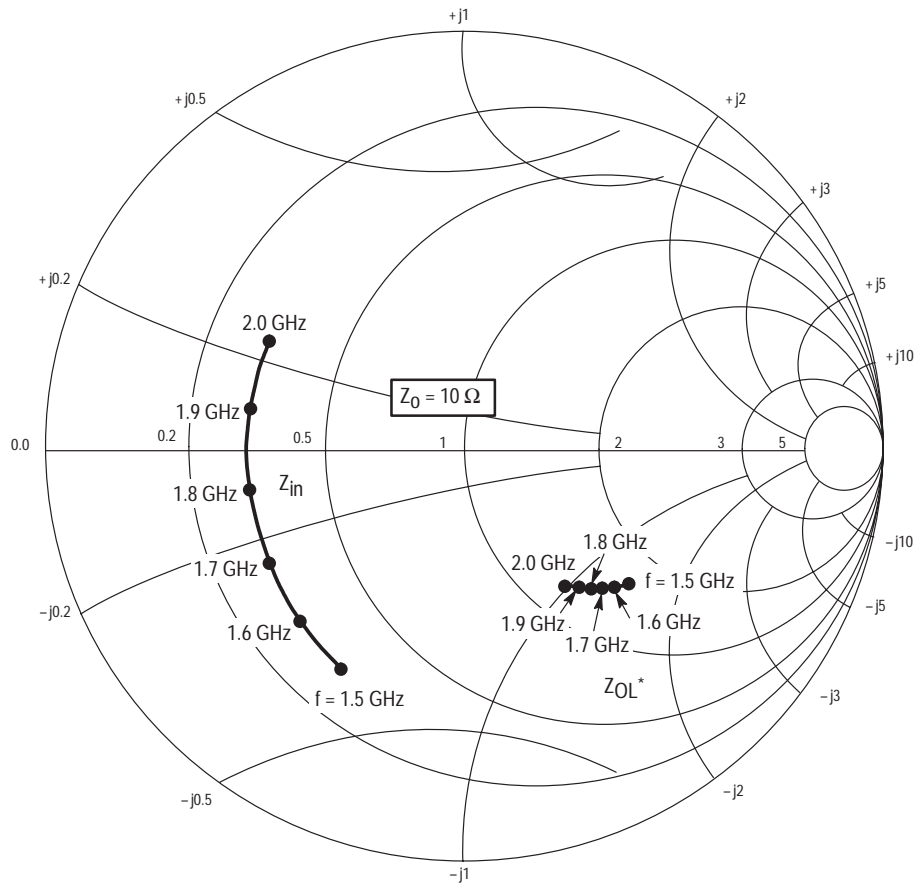
OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0, I_D = 10 \mu\text{A}_{dc}$)	$V_{(BR)DSS}$	65	74	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ Vdc}, V_{GS} = 0$)	I_{DSS}	—	—	10	μA_{dc}
Gate-Source Leakage Current ($V_{GS} = 20 \text{ Vdc}, V_{DS} = 0$)	I_{GSS}	—	—	1	μA_{dc}

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 20\ \mu\text{Adc}$)	$V_{GS(th)}$	2.4	3.2	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 25\text{ mAdc}$)	$V_{GS(q)}$	3	4.1	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 0.1\text{ A}$)	$V_{DS(on)}$	0.18	0.24	0.30	Vdc
DYNAMIC CHARACTERISTICS					
Input Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{iss}	—	5.5	—	pF
Output Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{oss}	—	3.3	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{rss}	—	0.17	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W PEP}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	G_{ps}	11	12.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W PEP}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	η	30	33	—	%
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W PEP}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IRL	10	16	—	dB
Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W PEP}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IMD	—	–31	–29	dBc
Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W PEP}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	G_{ps}	11	12.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	η	30	—	—	%
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W PEP}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	IRL	10	16	—	dB
Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W PEP}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	IMD	—	–31	—	dBc
Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W CW}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 2000.0\text{ MHz}$)	G_{ps}	10.5	12	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W CW}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 2000.0\text{ MHz}$)	η	40	44	—	%
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 4\text{ W CW}$, $I_{DQ} = 25\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $V_{SWR} = 10:1$, All Phase Angles at Frequency of Test)	Ψ	No Degradation In Output Power			



$V_{DD} = 26 \text{ V}$, $I_{DQ} = 25 \text{ mA}$, $P_{out} = 4 \text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1500	$3.15 - j5.3$	$15.5 - j13.6$
1600	$3.1 - j3.8$	$14.7 - j12.5$
1700	$3.1 - j2.3$	$14.0 - j11.7$
1800	$3.1 - j0.7$	$13.4 - j11.0$
1900	$3.1 + j0.9$	$12.8 - j10.1$
2000	$3.1 + j2.4$	$12.2 - j9.2$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at given output power, voltage, IMD, bias current and frequency.

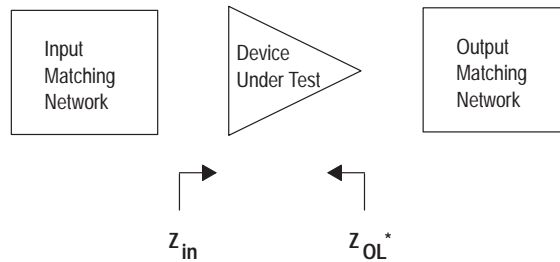


Figure 1. Series Equivalent Input and Output Impedance

Table 1. Common Source S-Parameters at $V_{DS} = 26$ Vdc, $I_D = 250$ mAdc

f GHz	S11		S21		S12		S22	
	S11	ϕ	dB	ϕ	S12	ϕ	S22	ϕ
0.1	.982	-28	18.9	160	.008	73	.851	-13
0.2	.947	-52	17.0	143	.015	58	.811	-25
0.3	.912	-73	15.0	129	.019	45	.770	-33
0.4	.886	-90	12.9	117	.022	36	.741	-42
0.5	.859	-103	11.1	108	.022	28	.719	-47
0.6	.854	-114	9.69	100	.023	23	.718	-51
0.7	.841	-123	8.54	93	.022	18	.709	-56
0.8	.837	-131	7.57	87	.021	15	.714	-59
0.9	.838	-138	6.69	81	.019	12	.719	-62
1.0	.841	-143	6.01	76	.018	11	.728	-64
1.1	.840	-149	5.41	72	.015	12	.742	-66
1.2	.849	-153	4.91	68	.013	13	.745	-68
1.3	.848	-158	4.51	64	.012	18	.758	-69
1.4	.856	-162	4.12	60	.010	26	.769	-70
1.5	.858	-167	3.78	57	.009	36	.786	-70
1.6	.871	-170	3.50	54	.008	54	.797	-72
1.7	.868	-173	3.22	51	.009	69	.808	-71
1.8	.870	-176	3.00	49	.009	82	.823	-72
1.9	.872	-180	2.80	46	.011	95	.828	-72
2.0	.877	178	2.63	44	.013	104	.845	-72
2.1	.876	174	2.47	41	.015	109	.843	-72
2.2	.880	171	2.36	39	.018	111	.859	-71
2.3	.882	168	2.21	36	.021	114	.858	-72
2.4	.886	165	2.12	34	.024	114	.872	-70
2.5	.896	162	1.97	32	.027	115	.863	-70
2.6	.897	158	1.89	29	.029	117	.873	-69

The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

MRF282SR1
MRF282ZR1

Designed for class A and class AB PCN and PCS base station applications at frequencies up to 2600 MHz. Suitable for FM, TDMA, CDMA, and multicarrier amplifier applications.

- Specified Two-Tone Performance @ 2000 MHz, 26 Volts
Output Power = 10 Watts PEP
Power Gain = 10.5 dB
Efficiency = 28%
Intermodulation Distortion = -31 dBc
- Specified Single-Tone Performance @ 2000 MHz, 26 Volts
Output Power = 10 Watts CW
Power Gain = 9.5 dB
Efficiency = 35%
- Capable of Handling 10:1 VSWR, @ 26 Vdc,
2000 MHz, 10 Watts CW Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal
Impedance Parameters
- Available in Tape and Reel. R1 Suffix = 500 Units per 12 mm, 7 inch Reel.
- LD MOS Models Available at
<http://www.motorola.com/semiconductors/rf/models/>

2000 MHz, 10 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 458B-02, STYLE 1
(MRF282SR1)



CASE 458C-02, STYLE 1
(MRF282ZR1)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	60 0.34	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	4.2	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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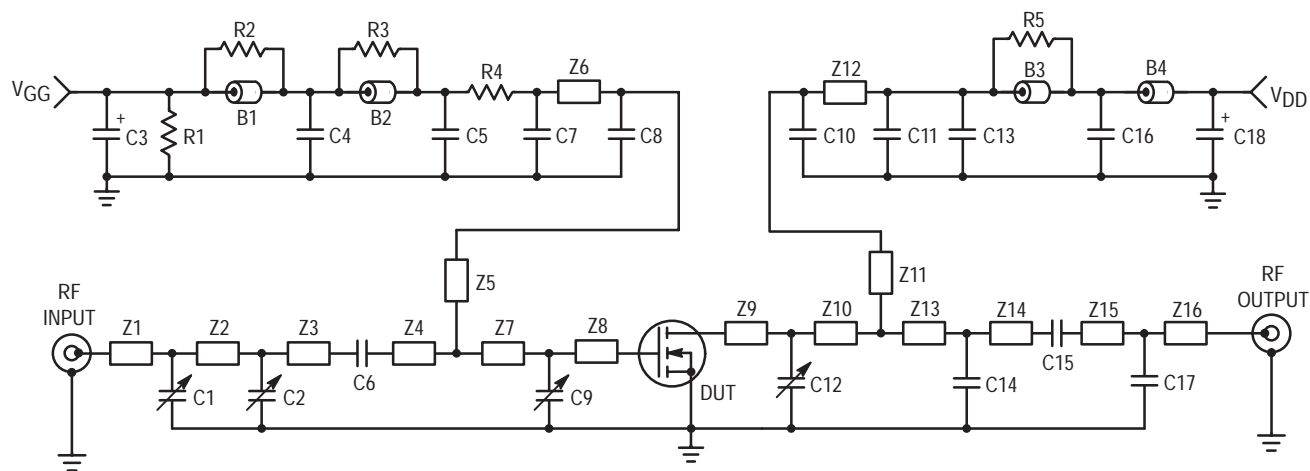
OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 10 \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1.0	μA
Gate-Source Leakage Current ($V_{GS} = 20 \text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1.0	μA

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 50\ \mu\text{Adc}$)	$V_{GS(th)}$	2.0	3.0	4.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 0.5\text{ Adc}$)	$V_{DS(on)}$	—	0.4	0.6	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 75\text{ mAdc}$)	$V_{GS(q)}$	3.0	4.0	5.0	Vdc
DYNAMIC CHARACTERISTICS					
Input Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{iss}	—	15	—	pF
Output Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{oss}	—	8.0	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{rss}	—	0.45	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Source Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	G_{ps}	10.5	11.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	η	28	—	—	%
Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IMD	—	–31	–28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IRL	9	14	—	dB
Common–Source Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	G_{ps}	10.5	11.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	η	28	—	—	%
Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	IMD	—	–31	–28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	IRL	9	14	—	dB
Common–Source Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 75\text{ mA}$, $f = 2000.0\text{ MHz}$)	G_{ps}	9.5	11.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 75\text{ mA}$, $f = 2000.0\text{ MHz}$)	η	35	40	—	%
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 75\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$, Load VSWR = 10:1, All Phase Angles at Frequency of Test)	Ψ	No Degradation In Output Power			



Z1	0.491" x 0.080" Microstrip	Z11	0.636" x 0.055" Microstrip
Z2	0.253" x 0.080" Microstrip	Z12	0.303" x 0.055" Microstrip
Z3	0.632" x 0.080" Microstrip	Z13	0.463" x 0.080" Microstrip
Z4	0.567" x 0.080" Microstrip	Z14	0.105" x 0.080" Microstrip
Z5	1.139" x 0.055" Microstrip	Z15	0.452" ± 0.085" x 0.080" Microstrip
Z6	0.236" x 0.055" Microstrip	Z16	0.910" ± 0.085" x 0.080" Microstrip
Z7	0.180" x 0.325" Microstrip	Raw Board	0.030" Glass Teflon®, 2 oz Copper,
Z8	0.301" x 0.325" Microstrip	Material	3" x 5" Dimensions,
Z9	0.439" x 0.325" Microstrip		Arlon GX0300-55-22, ε _r = 2.55
Z10	0.055" x 0.325" Microstrip		

Figure 1. 1.93 – 2.0 GHz Broadband Test Circuit Schematic

Table 1. 1.93 – 2.0 GHz Broadband Component Designations and Values

Designators	Description
B1, B4	0.120" x 0.333" x 0.100", Surface Mount Ferrite Beads, Fair Rite # 2743019446
B2, B3	0.120" x 0.170" x 0.100", Surface Mount Ferrite Beads, Fair Rite # 2743029446
C1, C2, C9	0.8–8.0 pF Gigatrim Variable Capacitors, Johanson # 27291SL
C3	10 μF, 35 V Tantalum Surface Mount Chip Capacitor, Kemet # T495X106K035AS4394
C4, C5, C13, C16	0.1 μF Chip Capacitor, Kemet # CDR33BX104AKWS
C6	200 pF, B Case RF Chip Capacitors, ATC # 100B201JCA500X
C7	18 pF, B Case RF Chip Capacitors, ATC # 100B180KP500X
C8	39 pF, B Case RF Chip Capacitors, ATC # 100B390JCA500X
C10	27 pF, B Case RF Chip Capacitors, ATC # 100B270JCA500X
C11	1.2 pF, B Case RF Chip Capacitors, ATC # 100B1R2CCA500X
C12	0.6–4.5 pF, Gigatrim Variable Capacitor, Johanson # 27271SL
C14	0.5 pF, B Case RF Chip Capacitors, ATC # 100B0R5BCA500X
C15	15 pF, B Case RF Chip Capacitors, ATC # 100B150JCA500X
C17	0.1 pF, B Case RF Chip Capacitors, ATC # 100B0R1BCA500X
C18	22 μF, 35 V Tantalum Surface Mount Chip Capacitor, Kemet # T491X226K035AS4394
R1	560 kΩ, 1/4 W Chip Resistor 0.08" x 0.13"
R2, R5	12 Ω, 1/4 W Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B120JT
R3, R4	91 Ω, 1/4 W Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B910JT
WS1, WS2	Beryllium Copper Wear Blocks 0.010" x 0.235" x 0.135" NOM
	Brass Banana Jack and Nut
	Red Banana Jack and Nut
	Green Banana Jack and Nut
	Type "N" Jack Connectors, Omni-Spectra # 3052-1648-10
	4-40 Ph Head Screws, 0.125" Long
	4-40 Ph Head Screws, 0.188" Long
	4-40 Ph Head Screws, 0.312" Long
	4-40 Ph Rec. Hd. Screws, 0.438" Long
RF Circuit Board	3" x 5" Copper Clad PCB, Glass Teflon®

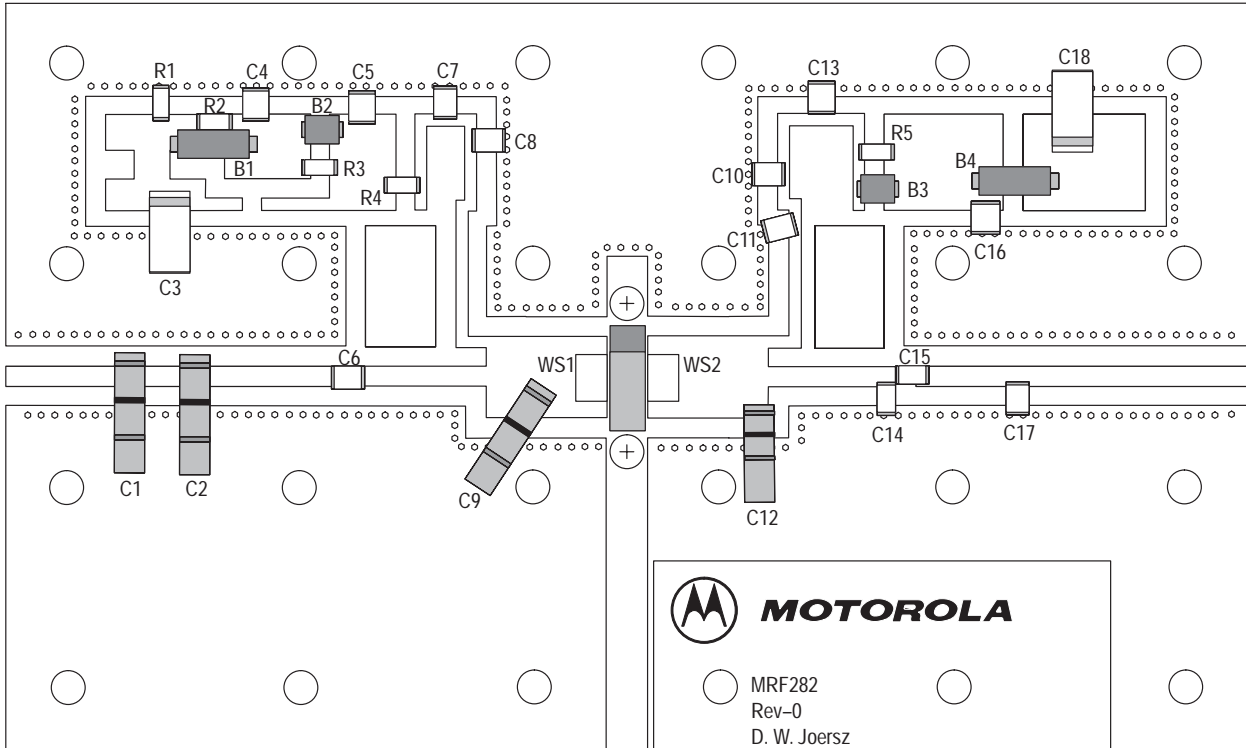


Figure 2. 1.93–2.0 GHz Broadband Test Circuit Component Layout

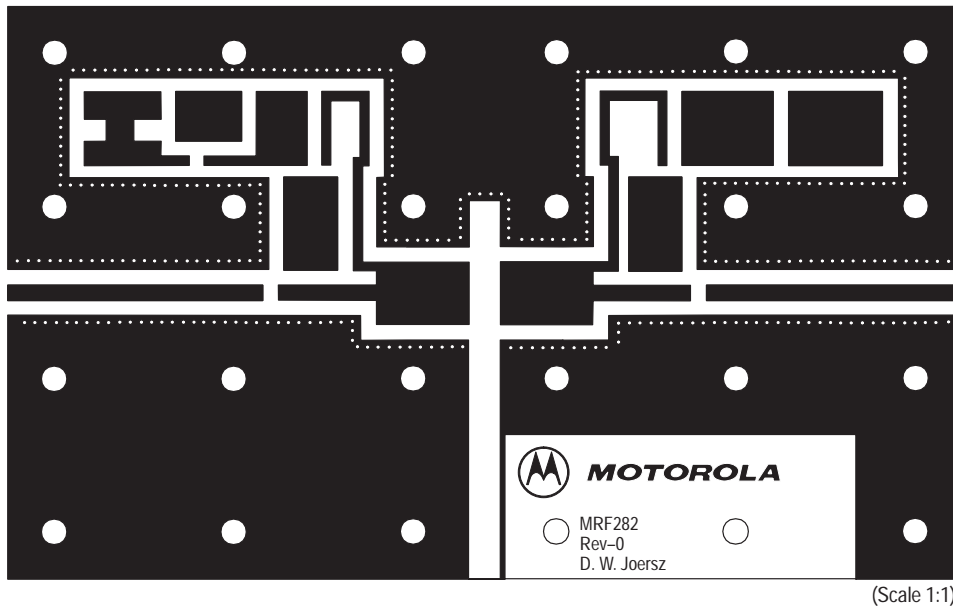
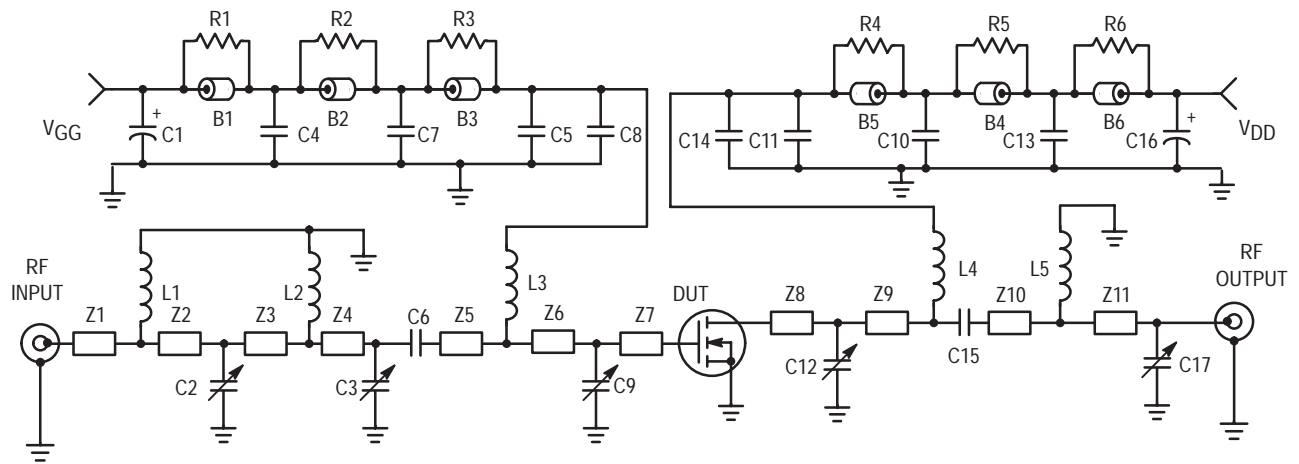


Figure 3. MRF282 Test Circuit Photomaster
(Reduced 18% in printed data book, DL110/D)



Z1	0.122" x 0.08" Microstrip	Z8	0.414" x 0.330" Microstrip
Z2	0.650" x 0.08" Microstrip	Z9	0.392" x 0.08" Microstrip
Z3	0.160" x 0.08" Microstrip	Z10	0.070" x 0.08" Microstrip
Z4	0.030" x 0.08" Microstrip	Z11	1.110" x 0.08" Microstrip
Z5	0.045" x 0.08" Microstrip	Raw Board	0.030" Glass Teflon [®] , 2 oz Copper,
Z6	0.291" x 0.08" Microstrip	Material	3" x 5" Dimensions,
Z7	0.483" x 0.330" Microstrip		Arlon GX0300–55–22, $\epsilon_r = 2.55$

Figure 4. 1.81 – 1.88 GHz Broadband Test Circuit Schematic

Table 2. 1.81 – 1.88 GHz Broadband Component Designations and Values

Designators	Description
B1, B2, B3, B4, B5, B6	0.120" x 0.170" x 0.100", Surface Mount Ferrite Beads, Fair Rite # 2743029446
C1, C16	470 μ F, 63 V, Electrolytic Capacitor, Mallory # SME63UB471M12X25L
C2, C9, C12, C17	0.6–4.5 pF, Variable Capacitor, Johanson Gigatrim # 27271SL
C3	0.8–8.0 pF, Variable Capacitor, Johanson Gigatrim # 27291SL
C4, C13	0.1 μ F, Chip Capacitor, Kemet # CDR33BX104AKWS
C5, C14	100 pF, B Case Chip Capacitor, ATC # 100B101JCA500X
C6, C8, C11, C15	12 pF, B Case Chip Capacitor, ATC # 100B120JCA500X
C7, C10	1000 pF, B Case Chip Capacitor, ATC # 100B102JCA50X
L1	3 Turns, 27 AWG, 0.087" OD, 0.050" ID, 0.053" Long, 6.0 nH
L2	5 Turns, 27 AWG, 0.087" OD, 0.050" ID, 0.091" Long, 15 nH
L3, L4	9 Turns, 26 AWG, 0.080" OD, 0.046" ID, 0.170" Long, 30.8 nH
L5	4 Turns, 27 AWG, 0.087" OD, 0.050" ID, 0.078" Long, 10 nH
R1, R2, R3	12 Ω , 1/8 W Fixed Film Chip Resistor. Garrett Instruments # RM73B2B120JT
R4, R5, R6	0.08" x 0.13". Garrett Instruments # RM73B2B120JT
W1, W2	Beryllium Copper 0.010" x 0.110" x 0.210"

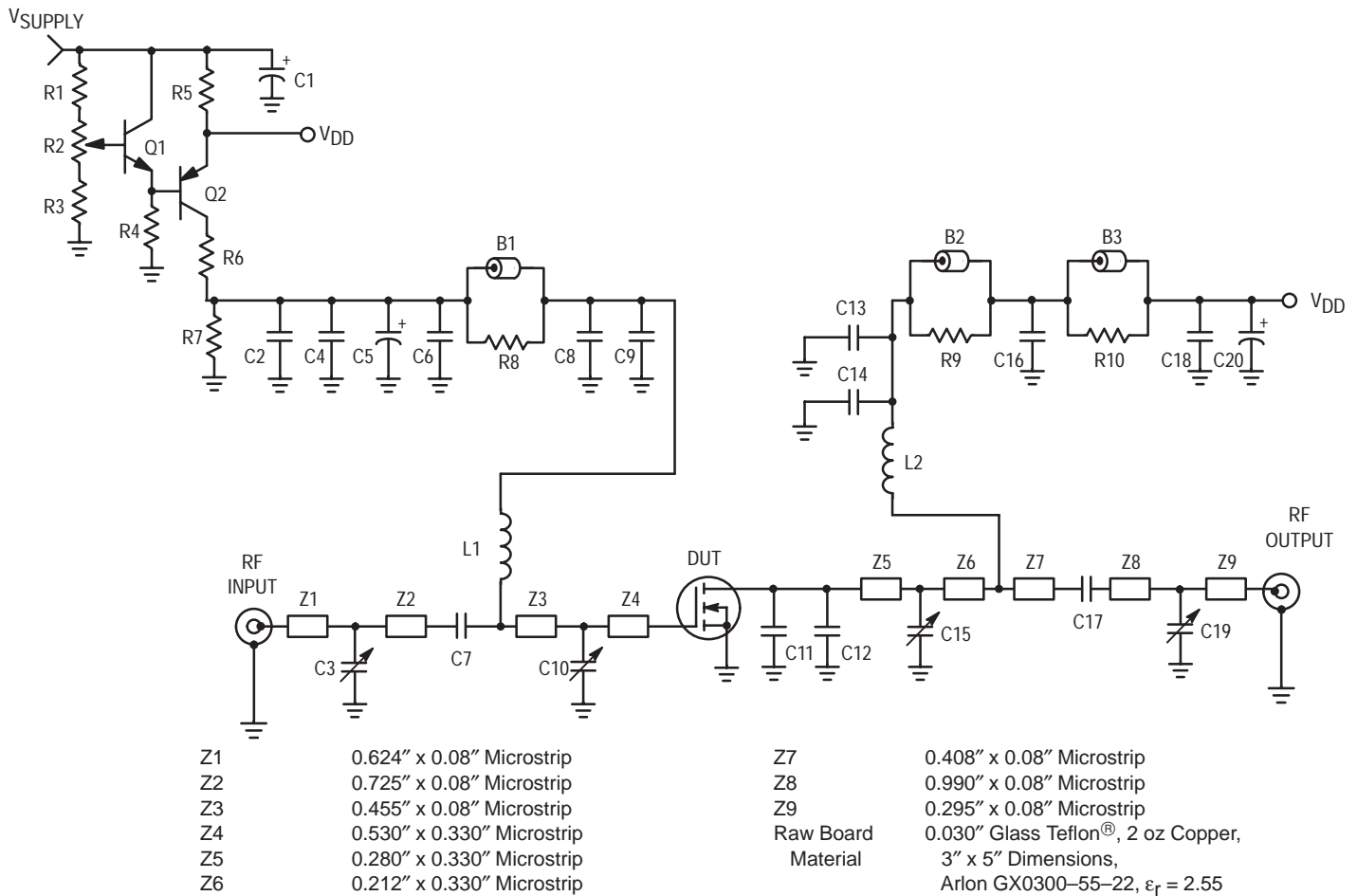
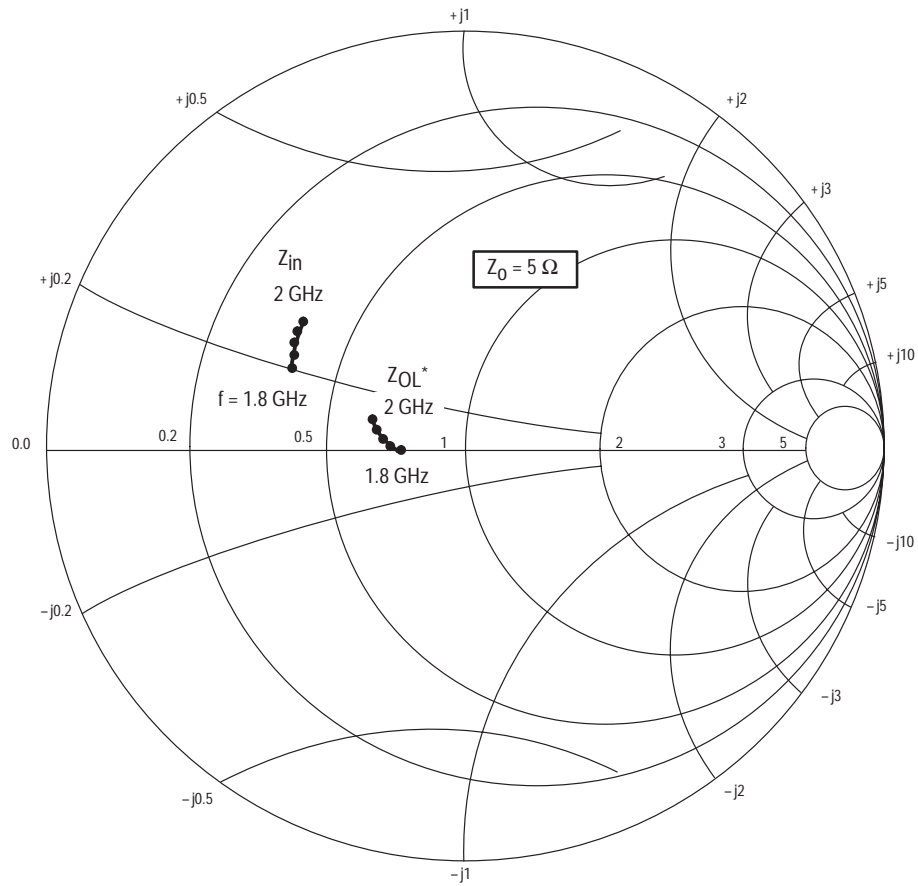


Figure 5. Class A Test Circuit Schematic

Table 3. Class A Broadband Component Designations and Values

Designators	Description
B1, B2, B3	Ferrite Bead, Ferroxcube, 56-590-65-3B
C1, C20	470 μ F, 63 V, Electrolytic Capacitor, Mallory # SME63V471M12X25L
C2	0.01 μ F, B Case Chip Capacitor, ATC # 100B103JCA50X
C3, C10, C15	0.6-4.5 pF, Variable Capacitor, Johanson # 27271SL
C4, C16	0.02 μ F, B Case Chip Capacitor, ATC # 100B203JCA50X
C5	100 μ F, 50 V, Electrolytic Capacitor, Mallory # SME50VB101M12X256
C6, C7, C9, C14, C17	12 pF, B Case Chip Capacitor, ATC # 100B120JCA500X
C8, C13	51 pF, B Case Chip Capacitor, ATC # 100B510JCA500X
C11, C12	0.3 pF, B Case Chip Capacitor, ATC # 100B0R3CCA500X
C18	0.1 μ F, Chip Capacitor, Kemet # CDR33BX104AKWS
C19	0.4-2.5 pF, Variable Capacitor, Johanson # 27285
L1	8 Turns, 0.042" ID, 24 AWG, Enamel
L2	9 Turns, 0.046" ID, 26 AWG, Enamel
Q1	NPN, 15 W, Bipolar Transistor, MJD310
Q2	PNP, 15 W, Bipolar Transistor, MJD320
R1	200 Ω , Axial, 1/4 W Resistor
R2	1.0 k Ω , 1/2 W Potentiometer, Bourns
R3	13 k Ω , Axial, 1/4 W Resistor
R4, R6, R7	390 Ω , 1/8 W Chip Resistor, Garrett Instruments # RM73B2B391JT
R5	1.0 Ω , 10 W 1% Resistor, DALE # RE65G1R00
R8, R9, R10	12 Ω , 1/8 W Chip Resistor, Garrett Instruments # RM73B2B120JT
Input/Output	Type N Flange Mount RF55-22, Connectors, Omni-Spectra



$V_{DD} = 26 \text{ V}$, $I_{DQ} = 75 \text{ mA}$, $P_{out} = 10 \text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1800	$2.1 + j1.0$	$3.8 - j0.15$
1860	$2.05 + j1.15$	$3.77 - j0.13$
1900	$2.0 + j1.2$	$3.75 - j0.1$
1960	$1.9 + j1.4$	$3.65 + j0.1$
2000	$1.85 + j1.6$	$3.55 + j0.2$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at given output power, voltage, IMD, bias current and frequency.

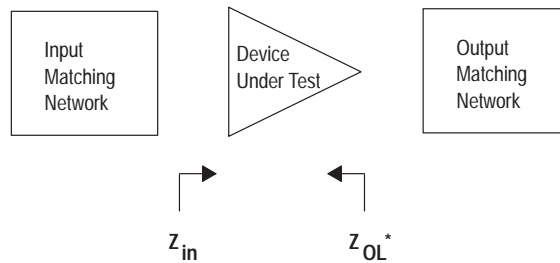


Figure 6. Series Equivalent Input and Output Impedance

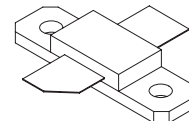
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for PCN and PCS base station applications at frequencies from 1000 to 2600 MHz. Suitable for FM, TDMA, CDMA, and multicarrier amplifier applications. To be used in class A and class AB for PCN-PCS/cellular radio and wireless local loop.

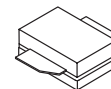
- Specified Two-Tone Performance @ 2000 MHz, 26 Volts
Output Power = 30 Watts (PEP)
Power Gain = 9 dB
Efficiency = 30%
Intermodulation Distortion = -29 dBc
- Typical Single-Tone Performance at 2000 MHz, 26 Volts
Output Power = 30 Watts (CW)
Power Gain = 9.5 dB
Efficiency = 45%
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- Excellent Thermal Stability
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 2000 MHz, 30 Watts (CW) Output Power
- MRF284SR1 Is Available in Tape and Reel. R1 Suffix = 500 Units per 12 mm, 7 inch Reel.
- LD MOS Models, Test Fixture, Reference Design and Circuit Board Artwork Available at: <http://motorola.com/sps/rf/design/tds/>

MRF284
MRF284SR1

30 W, 2000 MHz, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 360B-03, STYLE 1
(MRF284)



CASE 360C-03, STYLE 1
(MRF284SR1)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	87.5 0.5	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	2.0	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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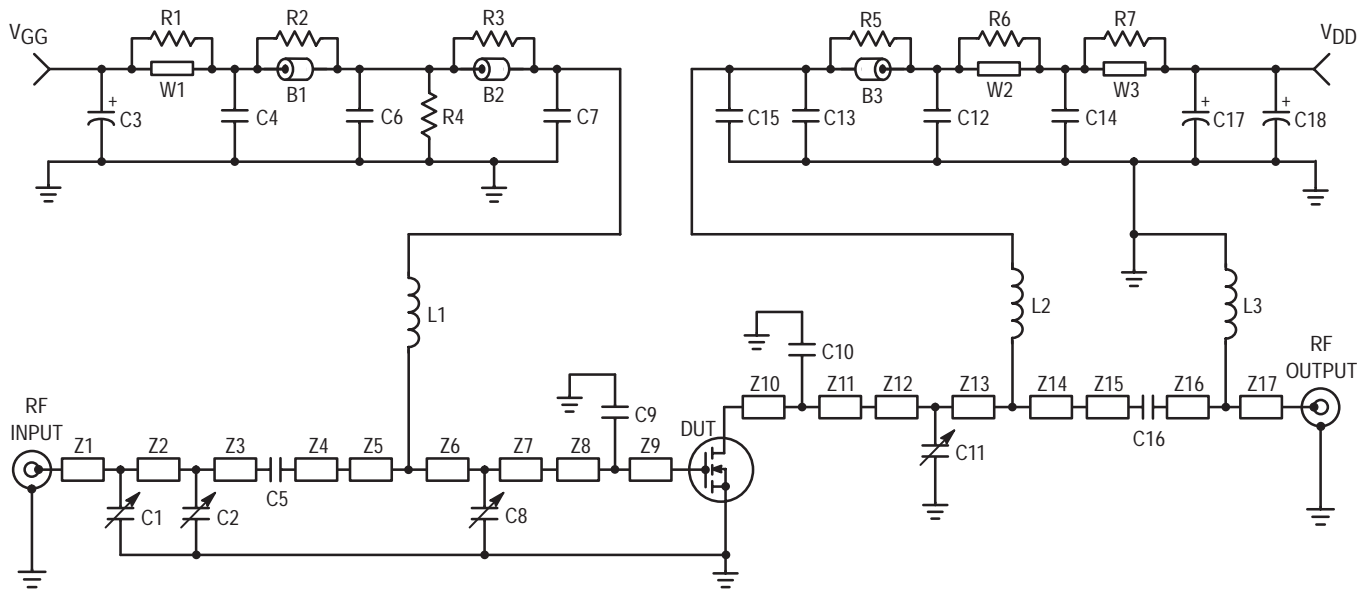
OFF CHARACTERISTICS

Drain-Source Breakdown Voltage ($V_{GS} = 0, I_D = 10 \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 20 \text{ Vdc}, V_{GS} = 0$)	I_{DSS}	—	—	1.0	μA
Gate-Source Leakage Current ($V_{GS} = 20 \text{ Vdc}, V_{DS} = 0$)	I_{GSS}	—	—	10	μA

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 150\ \mu\text{Adc}$)	$V_{GS(th)}$	2.0	3.0	4.0	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 200\ \text{mAdc}$)	$V_{GS(q)}$	3.0	4.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1.0\ \text{Adc}$)	$V_{DS(on)}$	—	0.3	0.6	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 1.0\ \text{Adc}$)	g_{fs}	—	1.5	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\ \text{MHz}$)	C_{iss}	—	43	—	pF
Output Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\ \text{MHz}$)	C_{oss}	—	23	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\ \text{MHz}$)	C_{rss}	—	1.4	—	pF
FUNCTIONAL TESTS (in Motorola Test Fixture)					
Common–Source Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 2000.0\ \text{MHz}$, $f_2 = 2000.1\ \text{MHz}$)	G_{ps}	9	10.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 2000.0\ \text{MHz}$, $f_2 = 2000.1\ \text{MHz}$)	η	30	35	—	%
Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 2000.0\ \text{MHz}$, $f_2 = 2000.1\ \text{MHz}$)	IMD	—	–32	–29	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 2000.0\ \text{MHz}$, $f_2 = 2000.1\ \text{MHz}$)	IRL	9	15	—	dB
Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W PEP}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 1930.0\ \text{MHz}$, $f_2 = 1930.1\ \text{MHz}$)	G_{ps}	9	10.4	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W PEP}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 1930.0\ \text{MHz}$, $f_2 = 1930.1\ \text{MHz}$)	η	—	35	—	%
Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W PEP}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 1930.0\ \text{MHz}$, $f_2 = 1930.1\ \text{MHz}$)	IMD	—	–34	—	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W PEP}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 1930.0\ \text{MHz}$, $f_2 = 1930.1\ \text{MHz}$)	IRL	9	15	—	dB
Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W CW}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 2000.0\ \text{MHz}$)	G_{ps}	8.5	9.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W CW}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 2000.0\ \text{MHz}$)	η	35	45	—	%
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\ \text{W CW}$, $I_{DQ} = 200\ \text{mA}$, $f_1 = 2000.0\ \text{MHz}$, $V_{SWR} = 10:1$, at All Phase Angles)	Ψ	No Degradation In Output Power			



Z1	0.530" x 0.080" Microstrip
Z2	0.255" x 0.080" Microstrip
Z3	0.600" x 0.080" Microstrip
Z4	0.525" x 0.080" Microstrip
Z5	0.015" x 0.325" Microstrip
Z6	0.085" x 0.325" Microstrip
Z7	0.165" x 0.325" Microstrip
Z8	0.110" x 0.515" Microstrip
Z9	0.095" x 0.515" Microstrip
Z10	0.050" x 0.515" Microstrip

Z11	0.155" x 0.515" Microstrip
Z12	0.120" x 0.325" Microstrip
Z13	0.150" x 0.325" Microstrip
Z14	0.010" x 0.325" Microstrip
Z15	0.505" x 0.080" Microstrip
Z16	0.865" x 0.080" Microstrip
Z17	0.525" x 0.080" Microstrip
Raw Board	0.030" Glass Teflon®, 2 oz Copper,
Material	3" x 5" Dimensions,
	Arlon GX0300-55-22, $\epsilon_r = 2.55$

Figure 1. 1.93–2.0 GHz Broadband Test Circuit Schematic

Table 1. 1.93 – 2.0 GHz Broadband Component Designations and Values

Designators	Description
B1 – B3	Ferrite Bead, Round, Ferroxcube # 56–590–65–3B
C1, C2, C8	0.8–8.0 pF Gigatrim Variable Capacitors, Johanson # 27291SL
C3, C17	22 μ F, 35 V Tantalum Surface Mount Chip Capacitor, Kemet # T491X226K035AS4394
C4, C14	0.1 μ F Chip Capacitor, Kemet # CDR33BX104AKWS
C5	220 pF B Case RF Chip Capacitor, ATC # 100B221KP500X
C6, C12	1000 pF B Case RF Chip Capacitor, ATC # 100B102JCA50X
C7, C13	5.1 pF B Case RF Chip Capacitor, ATC # 100B5R1CCA500X
C9	1.2 pF B Case RF Chip Capacitor, ATC # 100B1R2CCA500X
C10	2.7 pF B Case RF Chip Capacitor, ATC # 100B2R7CCA500X
C11	0.6–4.5 pF Gigatrim Variable Capacitors, Johanson # 27271SL
C15, C16	200 pF B Case RF Chip Capacitor, ATC # 100B201KP500X
C18	10 μ F, 35 V Tantalum Surface Mount Chip Capacitor, Kemet # T495X106K035AS4394
L1, L2	4 Turns, #24 AWG, 0.120" OD, 0.140" Long, (12.5 nH), Coilcraft # A04T–5
L3	2 Turns, #24 AWG, 0.120" OD, 0.140" Long, (5.0 nH), Coilcraft # A02T–5
R1, R2, R3, R5, R6, R7	12 Ω , 1/4 W Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B120JT
R4	560 k Ω , 1/4 W Chip Resistor 0.08" x 0.13"
W1, W2, W3	Solid Copper Buss Wire, 16 AWG
WS1, WS2	Beryllium Copper Wear Blocks 0.005" x 0.250" x 0.250"
	Brass Banana Jack and Nut
	Red Banana Jack and Nut
	Green Banana Jack and Nut
	Type "N" Jack Connectors, Omni–Spectra # 3052–1648–10
	4–40 Ph Head Screws, 0.125" Long
	4–40 Ph Head Screws, 0.188" Long
	4–40 Ph Head Screws, 0.312" Long
	4–40 Ph Rec. Hd. Screws, 0.438" Long
RF Circuit Board	3" x 5" Copper Clad PCB, Glass Teflon [®]

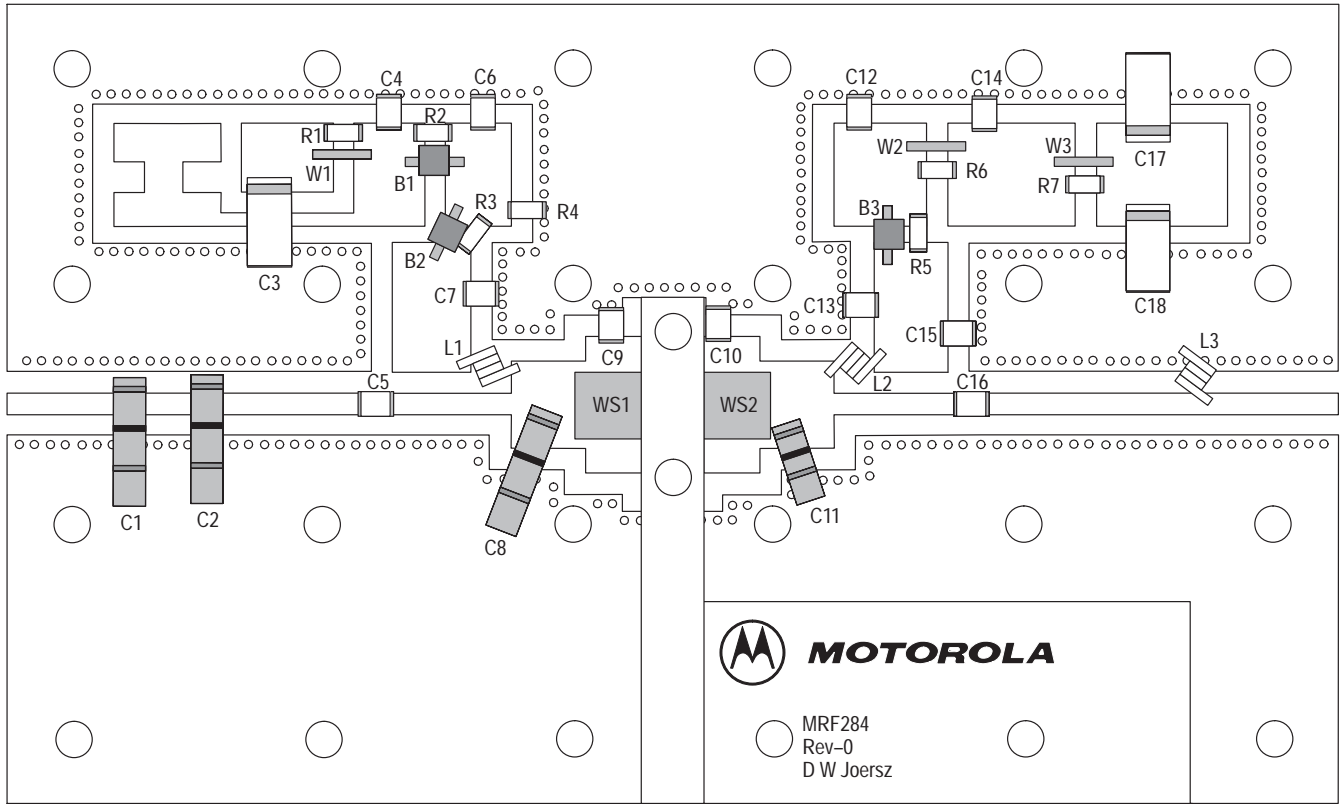


Figure 2. 1.93–2.0 GHz Broadband Test Circuit Component Layout

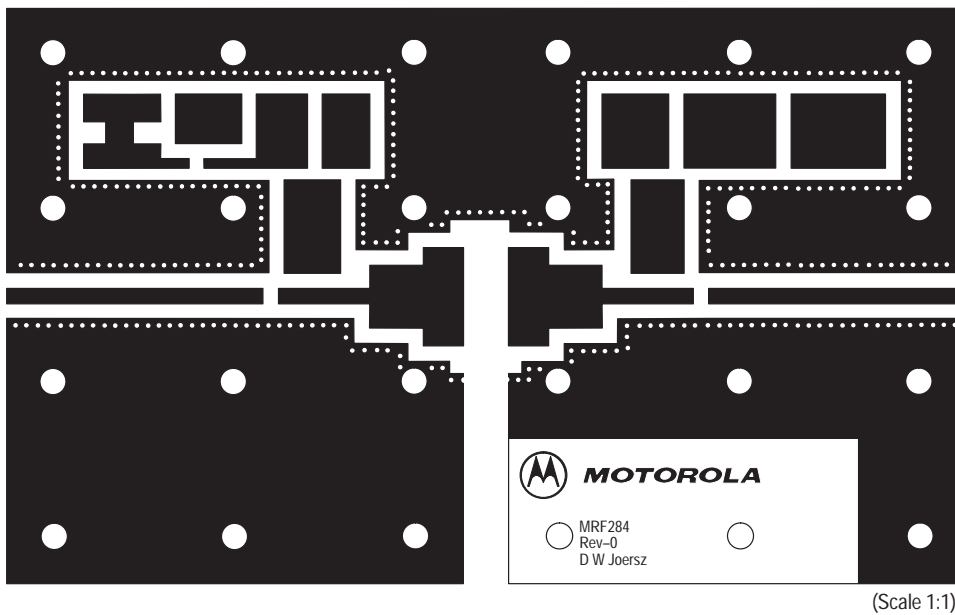
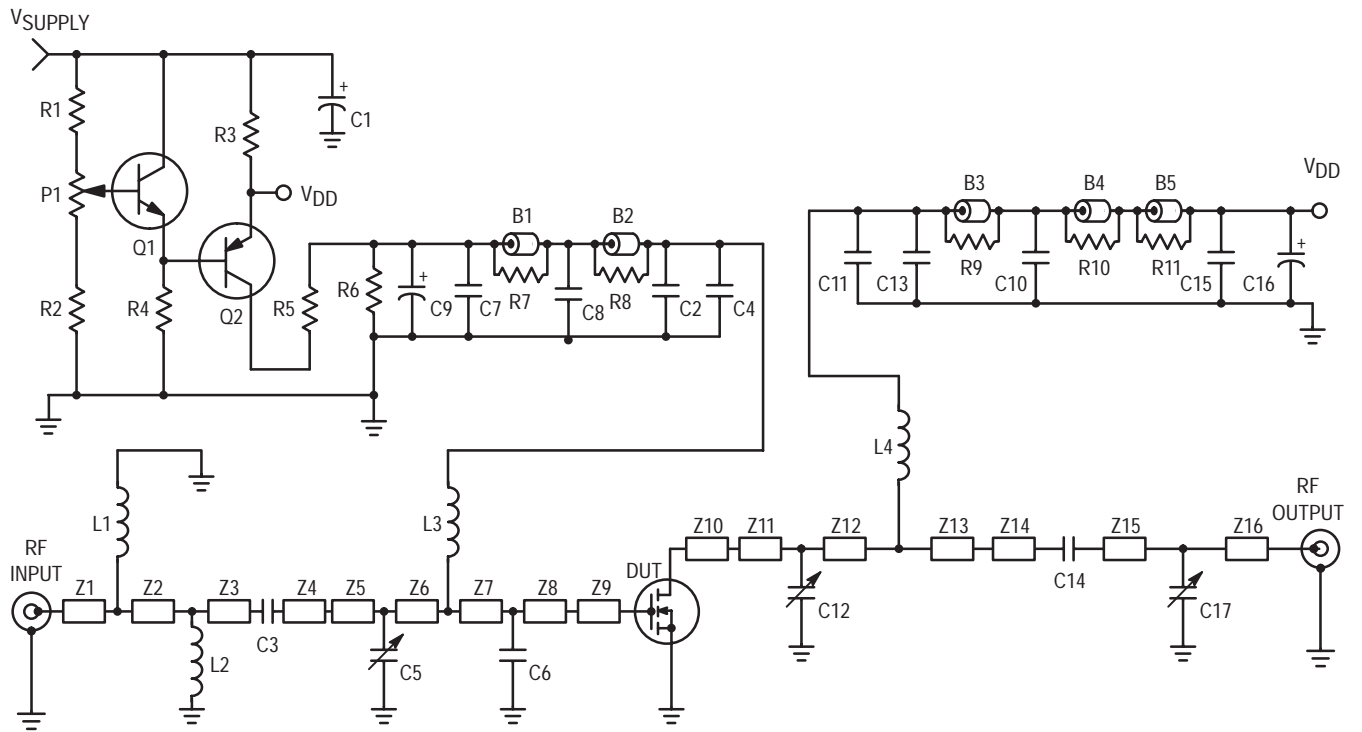


Figure 3. MRF284 Test Circuit Photomaster
(Reduced 18% in printed data book, DL110/D)



Z1	0.363" x 0.080" Microstrip	Z11	0.235" x 0.325" Microstrip
Z2	0.080" x 0.080" Microstrip	Z12	0.02" x 0.325" Microstrip
Z3	0.916" x 0.080" Microstrip	Z13	0.02" x 0.325" Microstrip
Z4	0.517" x 0.080" Microstrip	Z14	0.510" x 0.080" Microstrip
Z5	0.050" x 0.325" Microstrip	Z15	0.990" x 0.080" Microstrip
Z6	0.050" x 0.325" Microstrip	Z16	0.390" x 0.080" Microstrip
Z7	0.071" x 0.325" Microstrip	Raw Board	0.030" Glass Teflon®, 2 oz Copper,
Z8	0.125" x 0.325" Microstrip	Material	3" x 5" Dimensions,
Z9	0.210" x 0.515" Microstrip		Arlon GX0300-55-22, $\epsilon_r = 2.55$
Z10	0.210" x 0.515" Microstrip		

Figure 4. 2.0 GHz Class A Test Circuit Schematic

Table 2. 2.0 GHz Class A Component Designations and Values

Designators	Description
B1 – B5	Ferrite Bead, Round, Ferroxcube # 56–590–65–3B
C1, C9, C16	100 μ F, 50 V, Electrolytic Capacitor, Mallory # SME50VB101M12X25L
C2, C13	51 pF, ATC RF Chip Capacitors, Case "B" # 100B510JCA500x
C3, C14	10 pF, ATC RF Chip Capacitors, Case "B" # 100B100JCA500X
C4, C11	12 pF, ATC RF Chip Capacitors, Case "B" # 100B120JCA500X
C5	0.8 – 8.0 pF Variable Capacitor, Johansen Gigatrim # 27291SL
C6	4.7 pF, ATC RF Chip Capacitor, Case "B" # 100B4R7CCA500X
C7, C15	91 pF, ATC RF Chip Capacitors, Case "B" # 100B910KP500X
C8	1000 pF, ATC RF Chip Capacitor, Case "B" # 100B102JCA50X
C10	0.1 μ F, Chip Capacitor, Kemet # CDR33BX104AKWS
C12, C17	0.6 – 4.5 pF, Variable Capacitors, Johansen Gigatrim # 27271SL
L1	4 Turns, #27 AWG, 0.087" OD, 0.050" ID, 0.069" Long, 10 nH
L2	5 Turns, #24 AWG, 0.083" OD, 0.040" ID, 0.128" Long, 12.5 nH
L3, L4	9 Turns, #26 AWG, 0.080" OD, 0.046" ID, 0.170" Long, 30.8 nH
P1	1000 Ω Potentiometer, 1/2 W, 10 Turns, Bourns
Q1	Transistor, NPN, Motorola P/N: MJD31, Case 369A–10
Q2	Transistor, PNP, Motorola P/N: MJD32, Case 369A–10
R1	360 Ω , Fixed Film Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B361JT
R2	2 x 12 k Ω , Fixed Film Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B122JT
R3	1 Ω , Wirewound, 5 W, 3% Resistor, Dale # RE60G1R00
R4	4 x 6.8 k Ω , Fixed Film Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B682JT
R5	2 x 1500 Ω , Fixed Film Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B152JT
R6	270 Ω , Fixed Film Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B271JT
R7 – R11	12 Ω , Fixed Film Chip Resistor 0.08" x 0.13", Garrett Instruments # RM73B2B120JT

TYPICAL CHARACTERISTICS

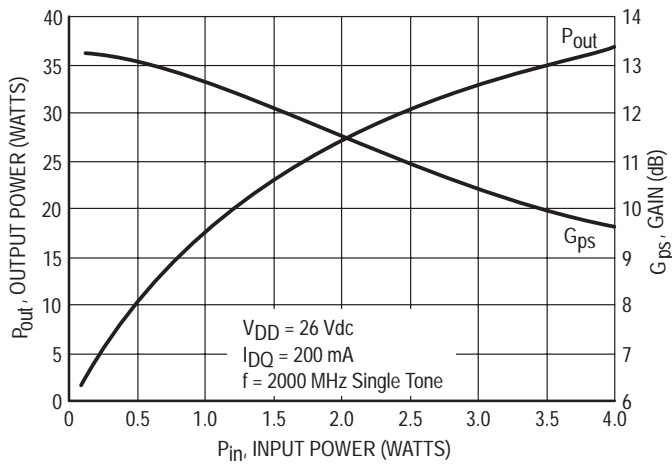


Figure 5. Output Power & Power Gain versus Input Power

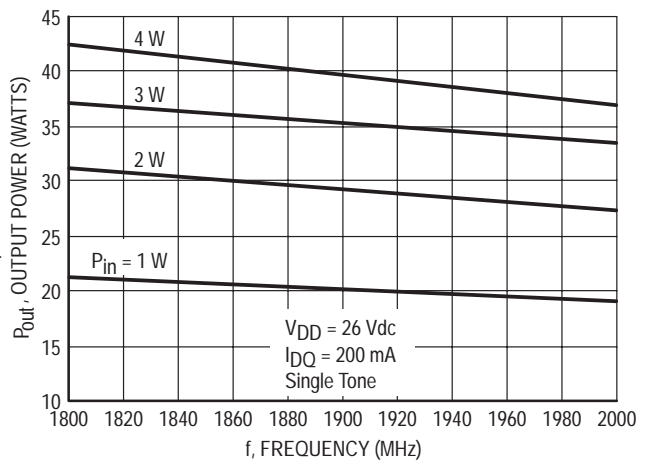


Figure 6. Output Power versus Frequency

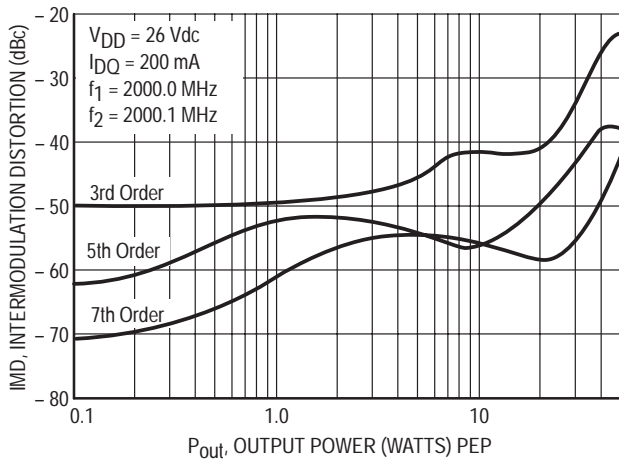


Figure 7. Intermodulation Distortion Products versus Output Power

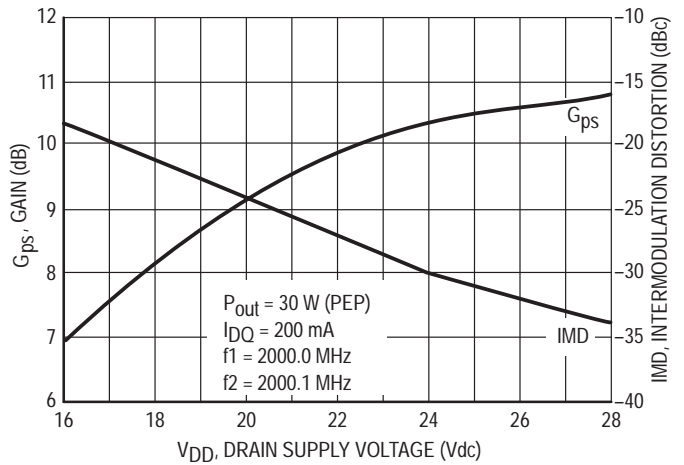


Figure 8. Power Gain and Intermodulation Distortion versus Supply Voltage

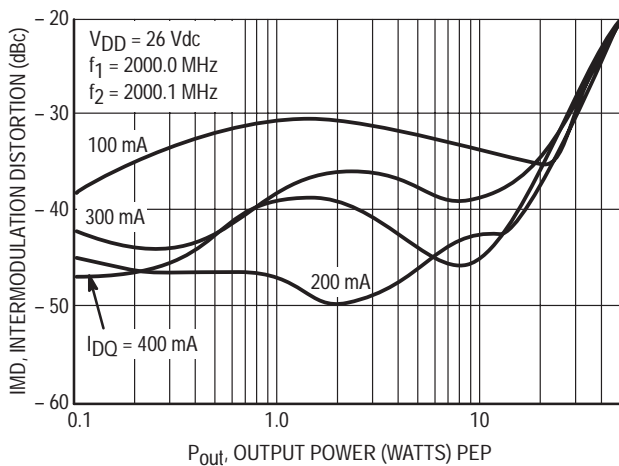


Figure 9. Intermodulation Distortion versus Output Power

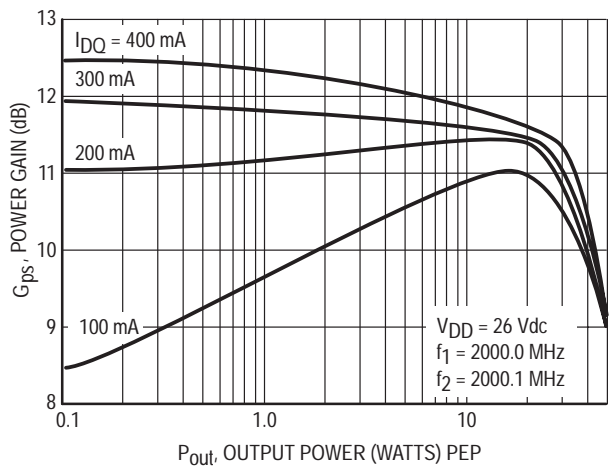


Figure 10. Power Gain versus Output Power

TYPICAL CHARACTERISTICS

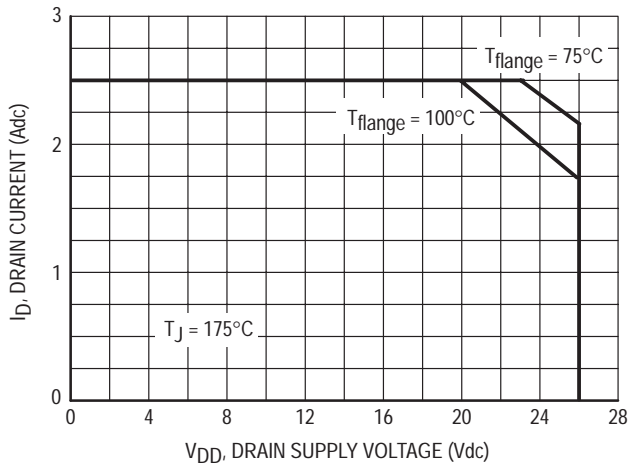


Figure 11. DC Safe Operating Area

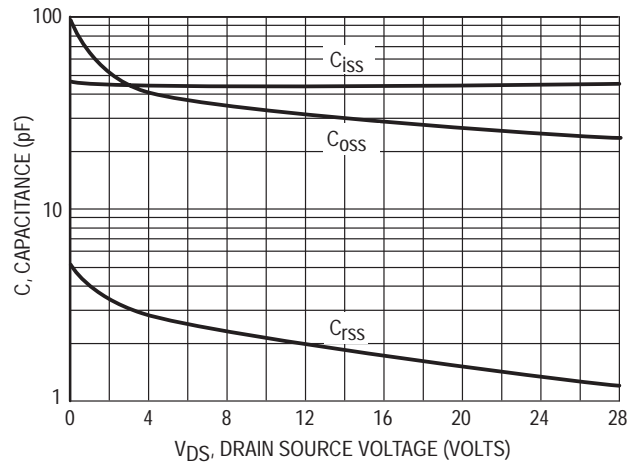


Figure 12. Capacitance versus Drain Source Voltage

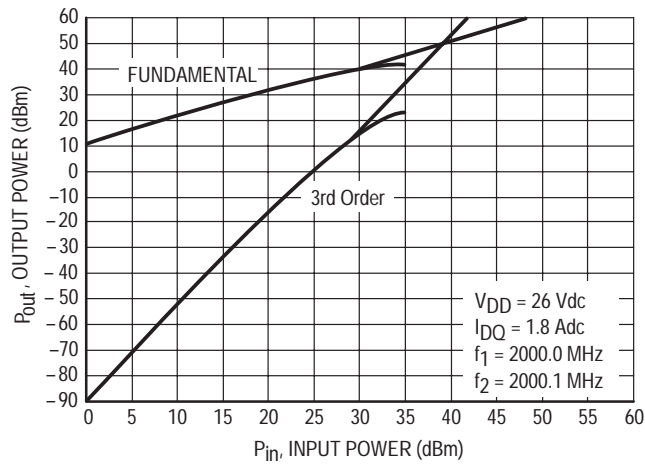


Figure 13. Class A Third Order Intercept Point

TYPICAL CHARACTERISTICS

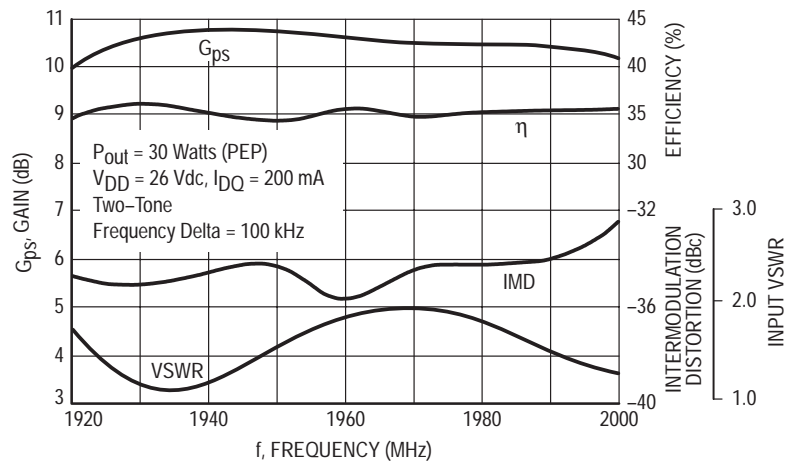
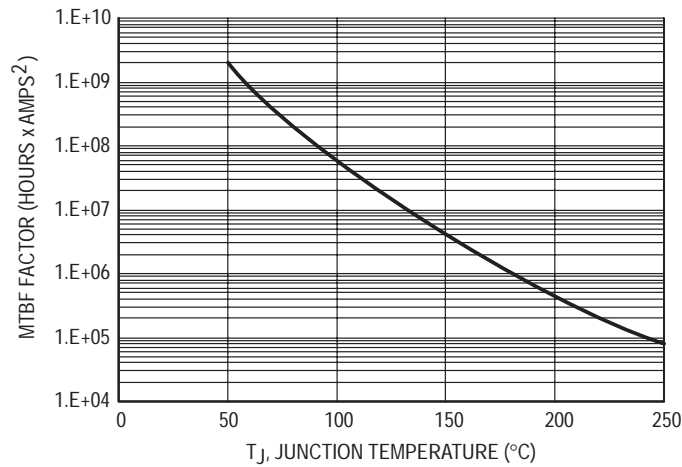
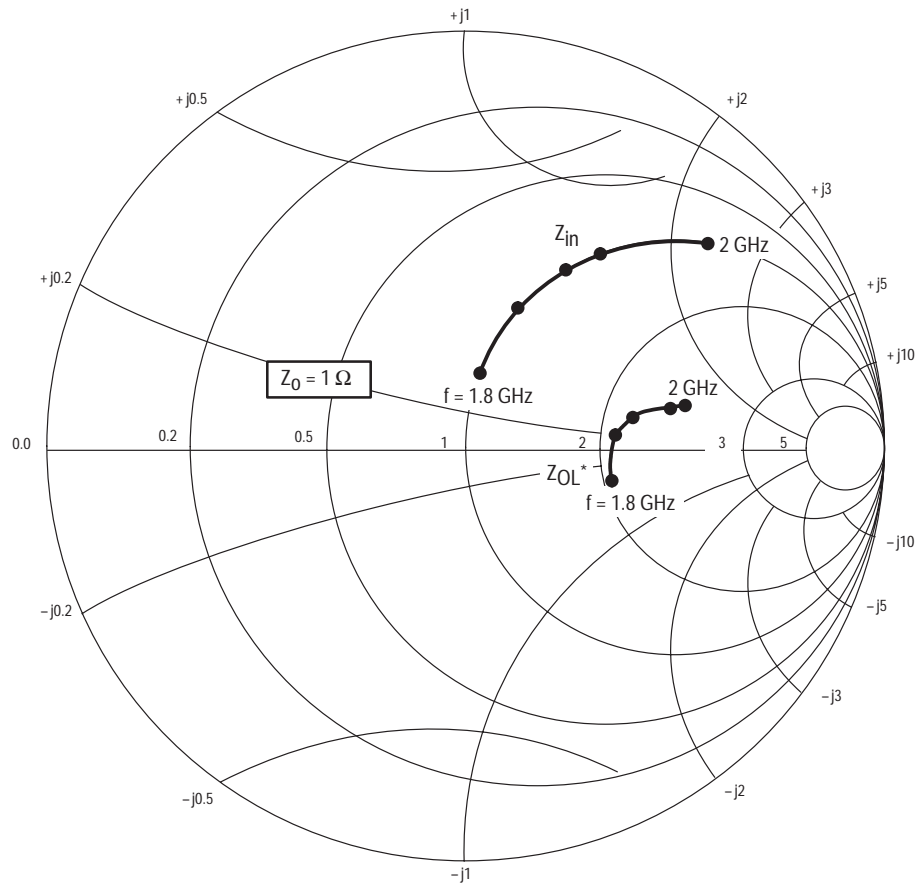


Figure 14. 1.92–2.0 GHz Broadband Circuit Performance



This graph displays calculated MTBF in hours \times ampere² drain current. Life tests at elevated temperature have correlated to better than $\pm 10\%$ of the theoretical prediction for metal failure. Divide MTBF factor by I_D^2 for MTBF in a particular application.

Figure 15. MTBF Factor versus Junction Temperature



$V_{CC} = 26 \text{ V}$, $I_{CQ} = 200 \text{ mA}$, $P_{out} = 15 \text{ W}_{avg}$

f MHz	$Z_{in}(1)$ Ohms	Z_{OL}^* Ohms
1800	$1.0 + j0.4$	$2.1 - j0.4$
1860	$1.0 + j0.8$	$2.2 + j0.2$
1900	$1.0 + j1.1$	$2.3 + j0.5$
1960	$1.0 + j1.4$	$2.5 + j0.9$
2000	$1.0 + j2.3$	$2.6 + j0.92$

$Z_{in}(1)$ = Complex conjugate of source impedance.

Z_{OL}^* = Conjugate of the optimum load impedance at given output power, voltage, bias current and frequency.

Figure 16. Series Equivalent Input and Output Impedance

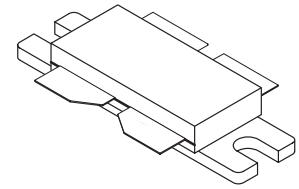
The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

Designed for broadband commercial and industrial applications at frequencies from 470 – 860 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 32 volt transmitter equipment.

- Typical Narrowband Two-Tone Performance @ f1 = 857 MHz, f2 = 863 MHz, 32 Volts
Output Power – 180 Watts PEP
Power Gain – 17 dB
Efficiency – 36%
IMD – –35 dBc
- Typical Broadband Two-Tone Performance @ f1 = 857 MHz, f2 = 863 MHz, 32 Volts
Output Power – 180 Watts PEP
Power Gain – 14.5 dB
Efficiency – 37%
IMD – –31 dBc
- Internally Matched
- Integrated ESD Protection
- 100% Tested for Load Mismatch Stress at All Phase Angles with 3:1 VSWR @ 32 Vdc, f1 = 857 MHz, f2 = 863 MHz, 180 Watts PEP
- Excellent Thermal Stability

MRF372

470 – 860 MHz, 180 W, 32 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 375G-03, STYLE 2

MAXIMUM RATINGS (1)

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	68	Vdc
Gate-Source Voltage	V _{GS}	+15, – 0.5	Vdc
Drain Current – Continuous	I _D	17	Adc
Total Device Dissipation @ T _C = 25°C Derate above 25°C	P _D	350 2.0	W W/°C
Storage Temperature Range	T _{stg}	– 65 to +150	°C
Operating Junction Temperature	T _J	200	°C

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	0.5	°C/W

(1) Each side of device measured separately.

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

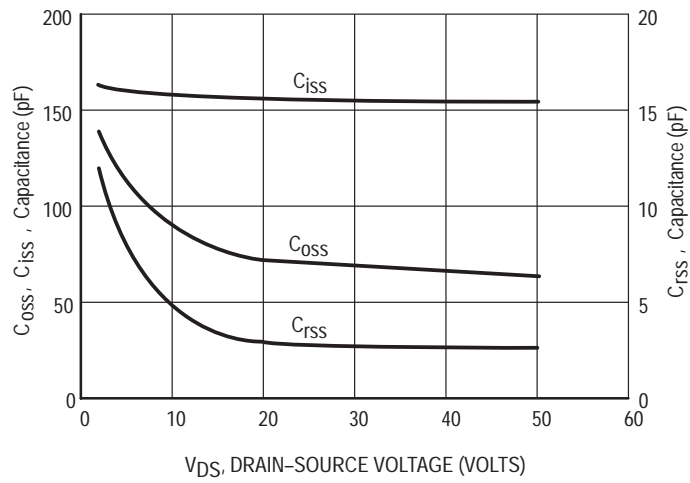
ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ V}$, $I_D = 10\ \mu\text{A}$)	$V_{(BR)DSS}$	68	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 32\text{ V}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	—	—	10	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ V}$, $V_{DS} = 0\text{ V}$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS (1)					
Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 200\ \mu\text{A}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 32\text{ V}$, $I_D = 100\text{ mA}$)	$V_{GS(Q)}$	2.5	3.5	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 3\text{ A}$)	$V_{DS(on)}$	—	0.28	0.45	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 3\text{ A}$)	g_{fs}	—	2.6	—	S
DYNAMIC CHARACTERISTICS (1)					
Input Capacitance (Includes Input Matching Capacitance) ($V_{DS} = 32\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{iss}	—	260	—	pF
Output Capacitance ($V_{DS} = 32\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{oss}	—	69	—	pF
Reverse Transfer Capacitance ($V_{DS} = 32\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{rss}	—	2.5	—	pF
FUNCTIONAL CHARACTERISTICS, TWO–TONE TESTING, NARROWBAND FIXTURE (2)					
Common Source Power Gain ($V_{DD} = 32\text{ V}$, $P_{out} = 180\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	G_{ps}	16	17	—	dB
Drain Efficiency ($V_{DD} = 32\text{ V}$, $P_{out} = 180\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	η	33	36	—	%
Intermodulation Distortion ($V_{DD} = 32\text{ Vdc}$, $P_{out} = 180\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	IMD	—	–35	–31	dBc
Output Mismatch Stress ($V_{DD} = 32\text{ Vdc}$, $P_{out} = 180\text{ W PEP}$, $I_{DQ} = 2 \times 400\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$, $V_{SWR} = 3:1$ at all phase angles of test)	ψ	No Degradation in Output Power			
TYPICAL CHARACTERISTICS, TWO–TONE OPERATION, BROADBAND FIXTURE (2)					
Common Source Power Gain ($V_{DD} = 32\text{ Vdc}$, $P_{out} = 180\text{ W PEP}$, $I_{DQ} = 2 \times 500\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	G_{ps}	—	14.5	—	dB
Drain Efficiency ($V_{DD} = 32\text{ Vdc}$, $P_{out} = 180\text{ W PEP}$, $I_{DQ} = 2 \times 500\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	η	—	37	—	%
Intermodulation Distortion ($V_{DD} = 32\text{ Vdc}$, $P_{out} = 180\text{ W PEP}$, $I_{DQ} = 2 \times 500\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	IMD	—	–31	—	dBc

(1) Each side of device measured separately.

(2) Measured in push–pull configuration.

TYPICAL CHARACTERISTICS



Note: C_{iss} does not include input matching capacitance.

Figure 1. Capacitance versus Voltage

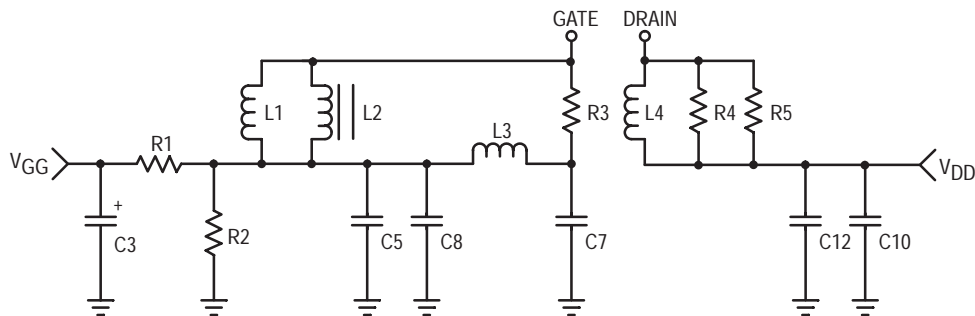
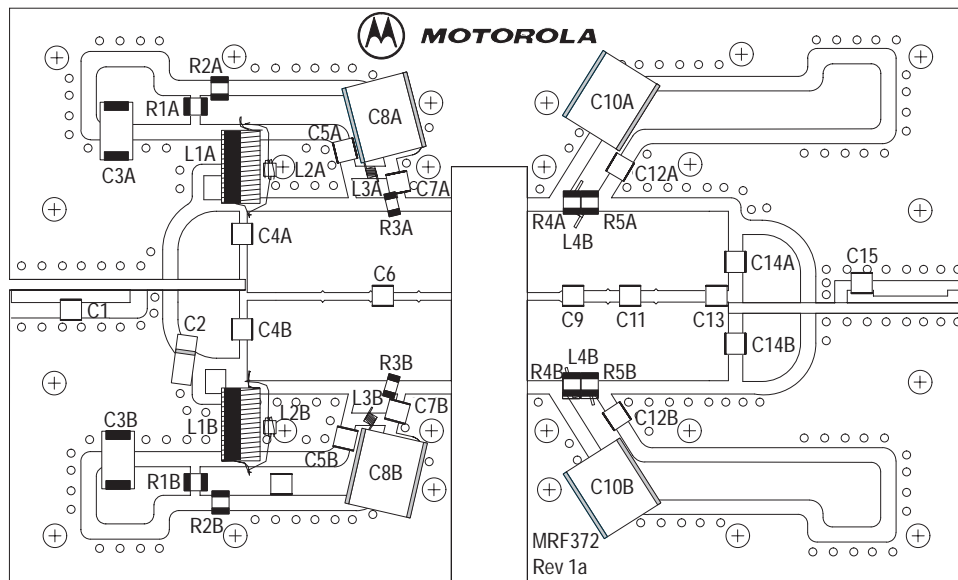


Figure 2. 860 MHz Narrowband DC Bias Networks

Table 1. 860 MHz Narrowband DC Bias Networks Component Designations and Values

Designation	Description
C1	2.2 pF, Chip Capacitor, B Case, ATC
C2	0.5 — 5.0 pF, Variable Capacitor, B Case, Johansen Gigatrim
C3A, B	22 μ F, 22 V, Tantalum Chip Capacitors, Kemet #T491D226K22AS
C4A, B, C14A, B	47.0 pF, Chip Capacitors, B Case, ATC
C5A, B	100 pF, Chip Capacitors, B Case, ATC
C6	10.0 pF, Chip Capacitor, B Case, ATC
C7A, B	2.7 pF, Chip Capacitors, A Case, ATC
C8A, B	1.0 μ F, 100 V, Chip Capacitors, Vitramon #VJ3640Y105KXBAT
C9	10.0 pF, Chip Capacitor, B Case, ATC
C10A, B	2.2 μ F, 100 V, Chip Capacitors, Vitramon #VJ3640Y225KXBAT
C11	5.1 pF, Chip Capacitor, B Case, ATC
C12A, B	0.01 μ F, 100 V, Chip Capacitors, Kemet #VJ1210Y103KXBAT
C15	1.2 pF, Chip Capacitor, B Case, ATC
L1A, B	130 nH, Coilcraft #132-11SM
L2A, B	#24 AWG, 3 Turns Loose, Fair Rite #2643706001
L3A, B	3.85 nH, Coilcraft #0906-4
L4A, B	5.0 nH, Coilcraft #A02T
R1A, B, R2A, B R4A, B, R5A, B	180 Ω , 1/4 W, Chip Resistors, Vishay Dale (1210)
R3A, B	12 Ω , 1/8 W Chip Resistors, Vishay Dale (1206)
PCB	MRF372 Printed Circuit Board Rev 1a, Rogers RO4350, Height 30 mils, $\epsilon_r = 3.48$
Balun A, B	Vertical 860 MHz Broadband Balun, Printed Circuit Board Rev 01, Rogers RO3010, Height 50 mils, $\epsilon_r = 10.2$



Vertical Balun Mounting Detail

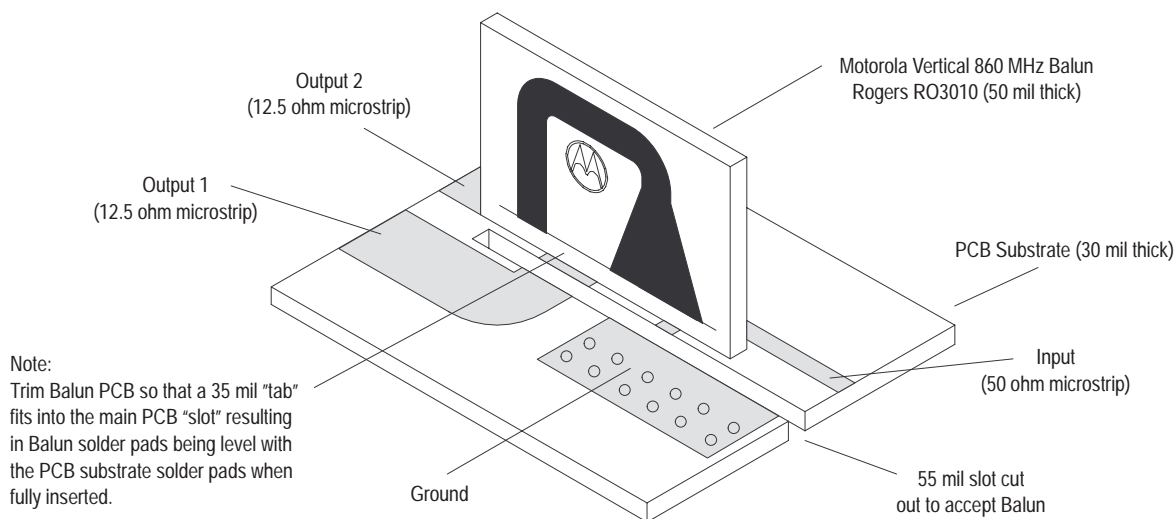
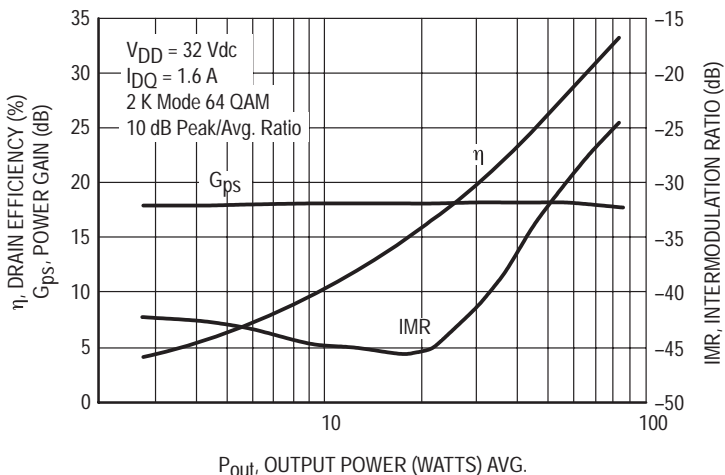


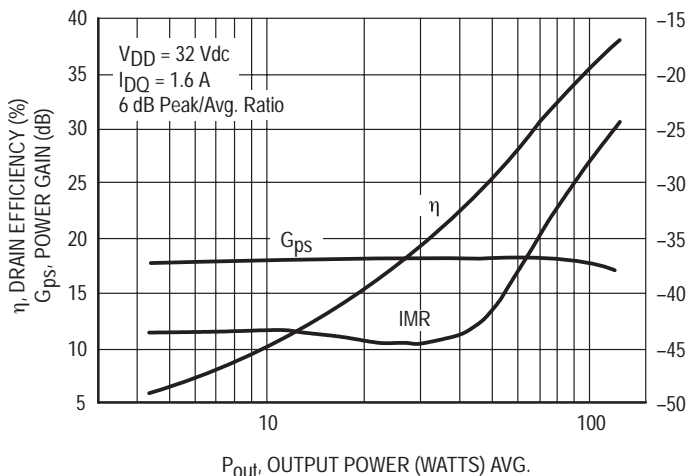
Figure 3. 860 MHz Narrowband Component Layout

TYPICAL TWO-TONE NARROWBAND CHARACTERISTICS



Note: IMR measured using Delta Marker Method.

Figure 4. COFDM Performance (860 MHz)



Note: IMR measured using Delta Marker Method.

Figure 5. 8-VSB Performance (860 MHz)

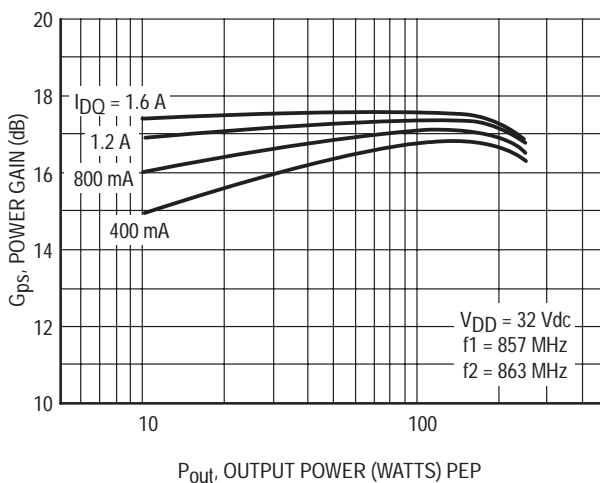


Figure 6. Power Gain versus Output Power

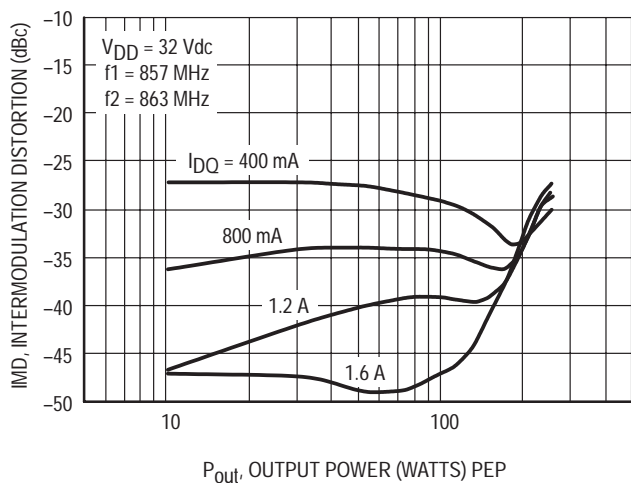


Figure 7. Intermodulation Distortion versus Output Power

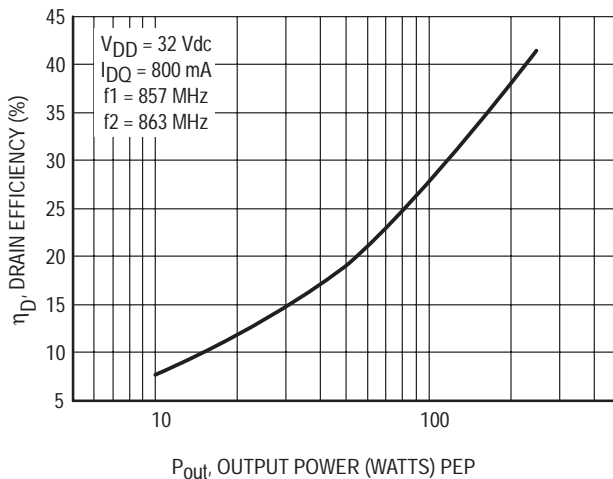
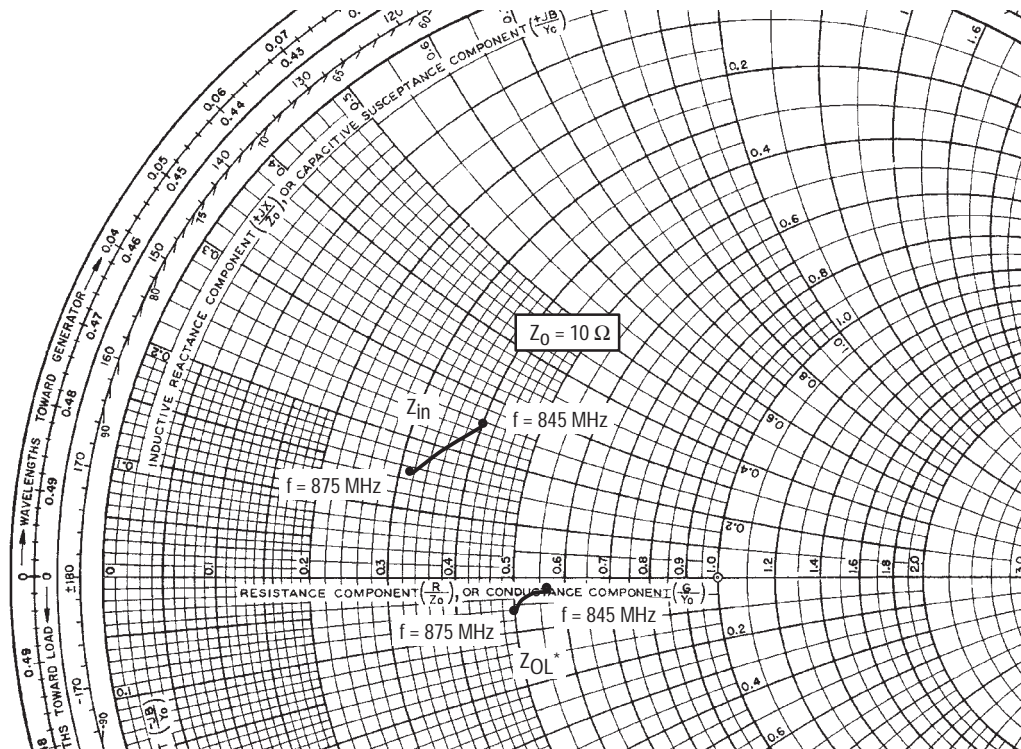


Figure 8. Drain Efficiency versus Output Power



$V_{DD} = 32\text{ V}$, $I_{DQ} = 800\text{ mA}$, $P_{out} = 180\text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
845	$3.99 + j2.50$	$5.63 - j0.38$
860	$3.56 + j1.98$	$5.28 - j0.43$
875	$3.18 + j1.46$	$4.94 - j0.56$
Harmonics		
f GHz	Z_{in} Ω	Z_{OL}^* Ω
1.69	$2.85 - j14.30$	$1.23 - j9.37$
1.72	$3.27 - j14.32$	$1.54 - j9.60$
1.75	$3.35 - j14.36$	$1.73 - j9.62$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{in} and Z_{OL}^* were chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

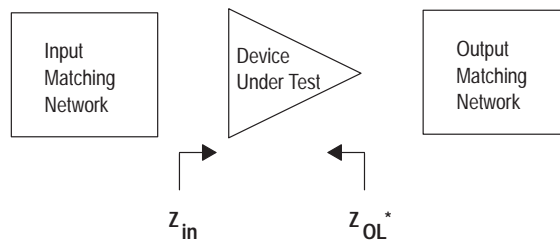


Figure 9. Narrowband Series Equivalent Input and Output Impedance

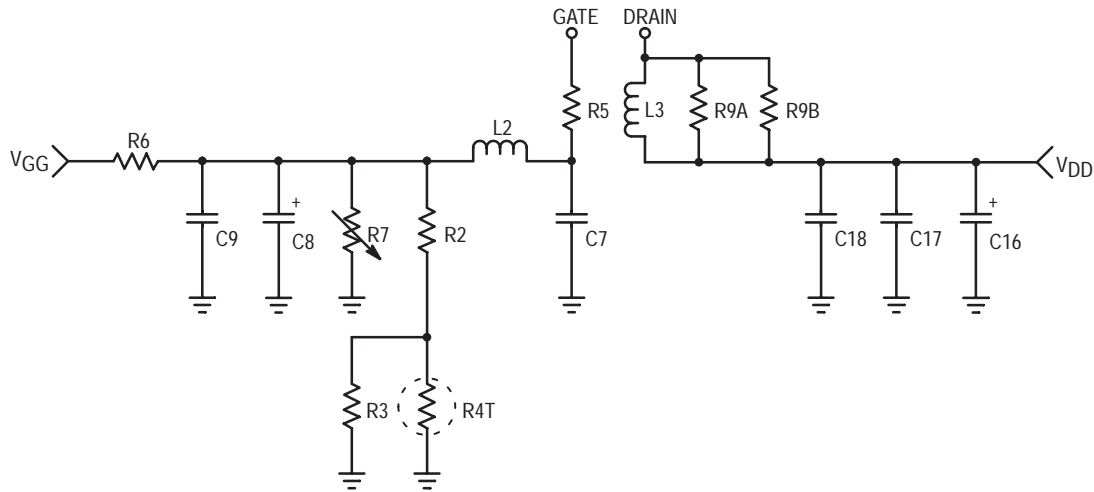
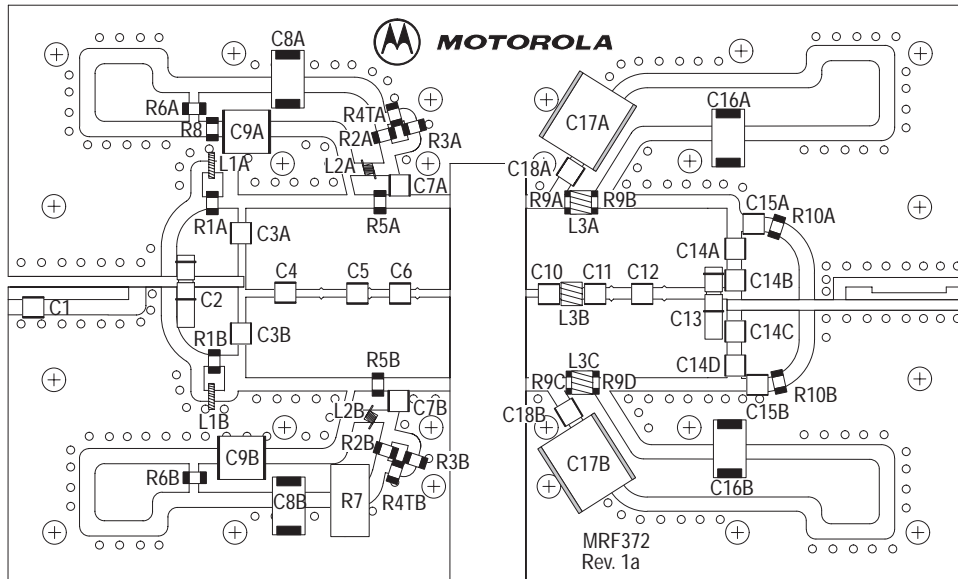


Figure 10. 470–860 MHz Broadband DC Bias Networks

Table 2. 470–860 MHz Broadband DC Bias Networks Component Designations and Values

Designation	Description
C1	0.7 pF, Chip Capacitor, B Case, ATC
C2, C13	0.8 — 8.0 pF, Variable Capacitors, Johansen Gigatrim
C3A, B, C14A, B, C, D	100 pF, Chip Capacitors, B Case, ATC
C4	4.7 pF, Chip Capacitor, B Case, ATC
C5	7.5 pF, Chip Capacitor, B Case, ATC
C6	10.0 pF, Chip Capacitor, B Case, ATC
C7A, B	6.2 pF, Chip Capacitors, A Case, ATC
C8A, B	22 μ F, 22 V, Tantalum Chip Capacitors, Kemet #T491D226K22AS
C9A, B	0.1 μ F, 100 V, Chip Capacitors, Vitramon #VJ3640Y104KXBAT
C10	13 pF, Chip Capacitor, B Case, ATC
C11	6.8 pF, Chip Capacitor, B Case, ATC
C12	3.9 pF, Chip Capacitor, B Case, ATC
C15A, B	3.3 pF, Chip Capacitors, B Case, ATC
C16A, B	10 μ F, 35 V, Tantalum Chip Capacitors, Kemet #T491D106K35AS
C17A, B	3.3 μ F, 100 V, Chip Capacitors, Vitramon #VJ3640Y335KXBAT
C18A, B	0.01 μ F, Chip Capacitors, B Case, ATC
L1A, B	12.55 nH, Coilcraft #1606–10
L2A, B	5.45 nH, Coilcraft #0906–5
L3A, B, C	12.5 nH, Coilcraft #A04T
R1A, B	10 Ω , 1/4 W, Chip Resistors, Vishay Dale (1210)
R2A, B	2.2 k Ω , 1/4 W, Chip Resistors, Vishay Dale (1210)
R3A, B, R10A, B	390 Ω , 1/8 W Chip Resistors, Vishay Dale (1206)
R4TA, B	520 Ω , Thermistor, Vishay #NTHS—1206J14520R5%
R5A, B	6.2 Ω , 1/4 W, Chip Resistors, Vishay Dale (1210)
R6A, B	6.8 k Ω , 1/4 W, Chip Resistors, Vishay Dale (1210)
R7	100 k Ω , Potentiometer, Bourns
R8	47.3 k Ω , 1/8 W Chip Resistor, Vishay Dale (1206)
R9A, B, C, D	180 Ω , 1/4 W, Chip Resistors, Vishay Dale (1210)
PCB	MRF372 Printed Circuit Board Rev 1a, Rogers RO4350, Height 30 mils, $\epsilon_r = 3.48$
Balun A, B	Vertical 660 MHz Broadband Balun, Printed Circuit Board Rev 01, Rogers RO3010, Height 50 mils, $\epsilon_r = 10.2$



Vertical Balun Mounting Detail

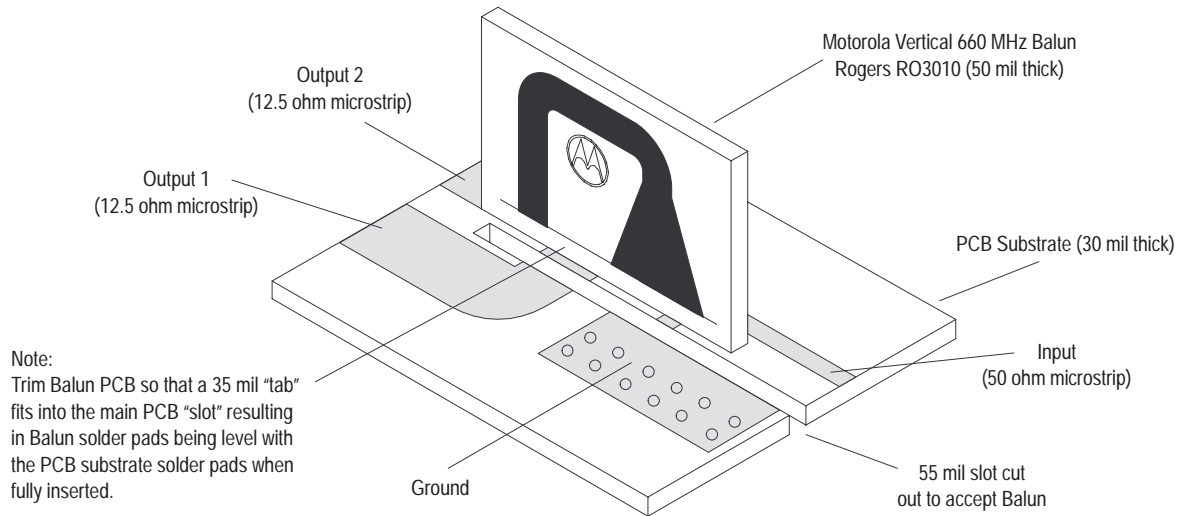


Figure 11. 470–860 MHz Broadband Component Layout

TYPICAL TWO-TONE BROADBAND CHARACTERISTICS

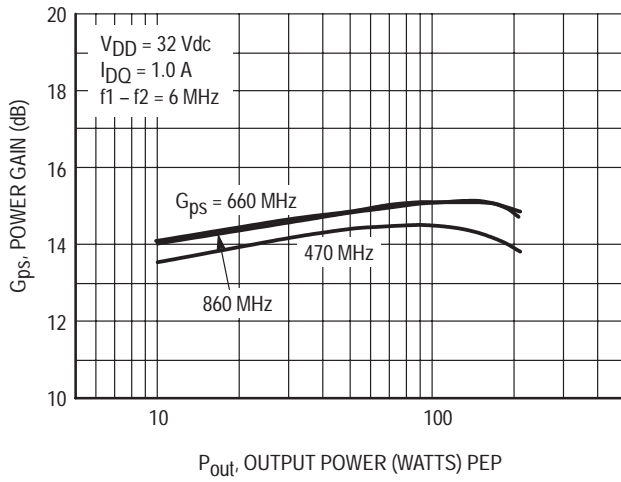


Figure 12. Power Gain versus Output Power

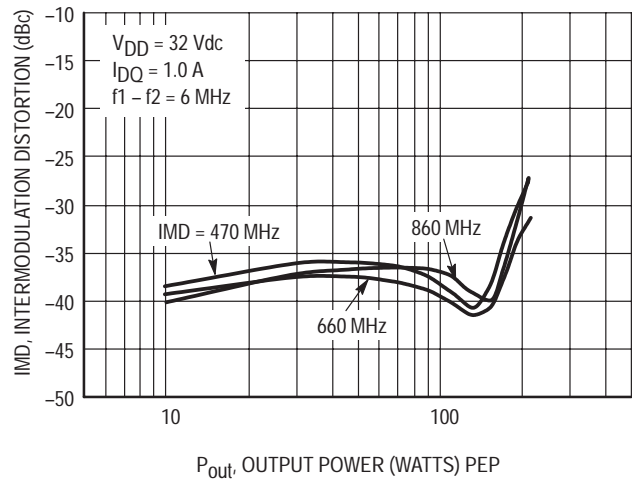


Figure 13. Intermodulation Distortion versus Output Power

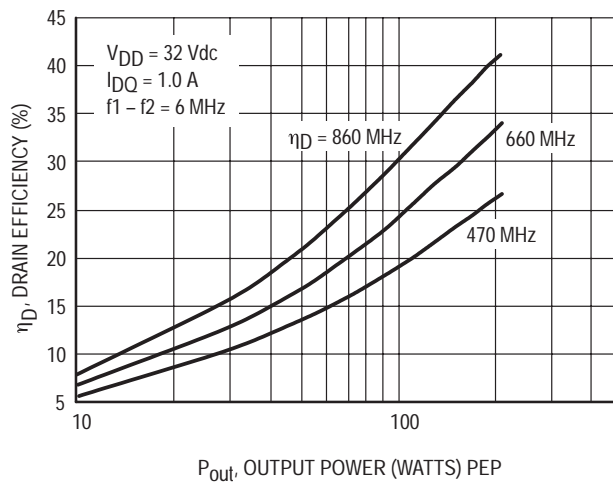
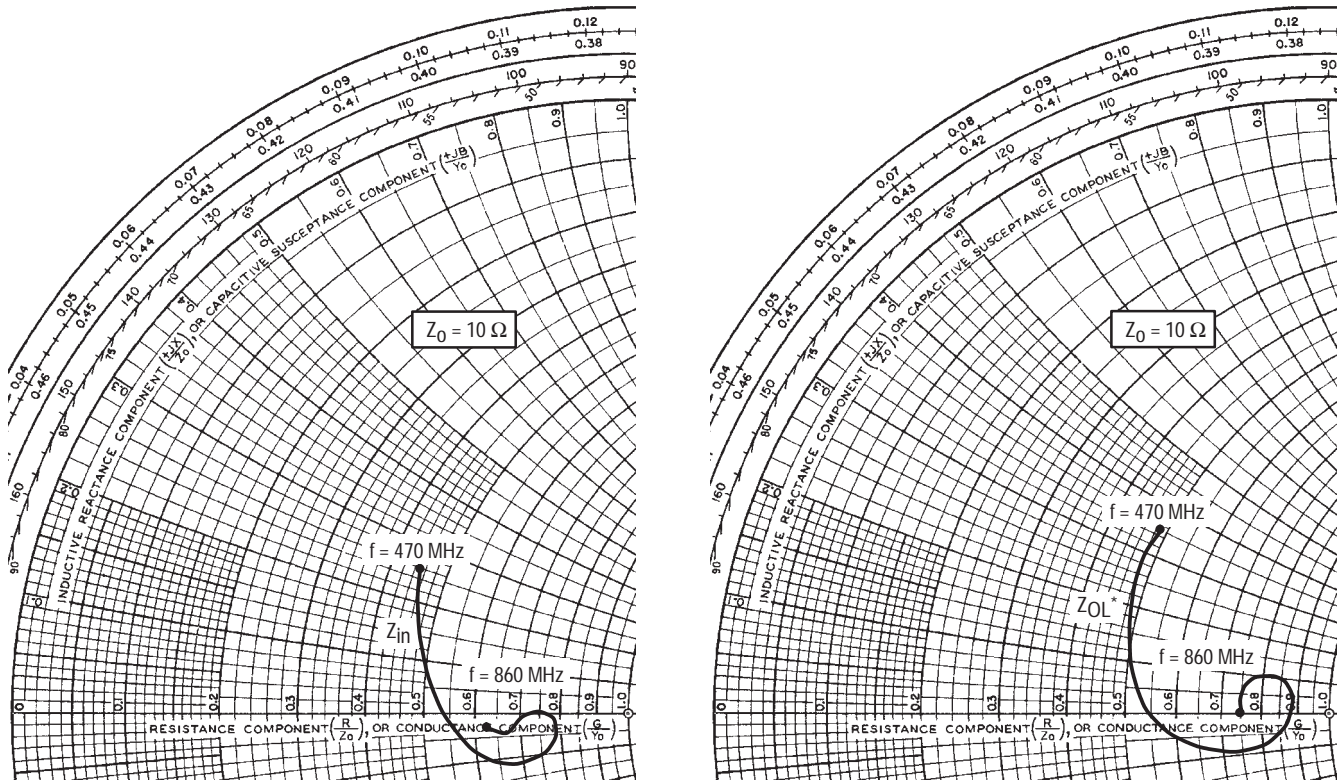


Figure 14. Drain Efficiency versus Output Power



$V_{DD} = 32\text{ V}$, $I_{DQ} = 1.0\text{ mA}$, $P_{out} = 180\text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
470	$4.46 + j2.57$	$4.88 + j3.50$
560	$6.40 - j1.06$	$5.45 + j0.07$
660	$7.84 - j0.14$	$8.13 - j0.73$
760	$6.67 - j0.46$	$8.27 + j1.00$
860	$6.25 - j0.31$	$7.52 - j0.02$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{in} and Z_{OL}^* were chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

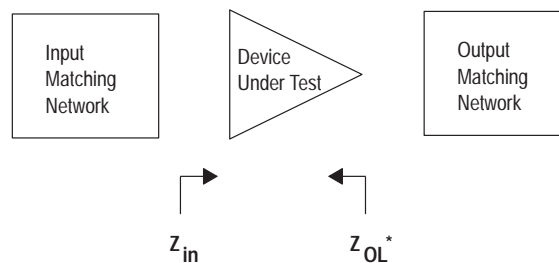
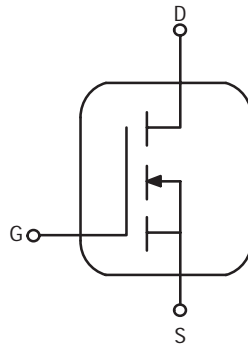


Figure 15. Broadband Series Equivalent Input and Output Impedance

The RF MOSFET Line
RF Power
Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

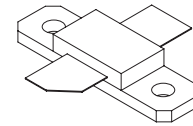
Designed for broadband commercial and industrial applications at frequencies from 470 – 860 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 28 volt transmitter equipment.

- Guaranteed CW Performance at 860 MHz, 28 Volts, Narrowband Fixture
Output Power – 60 Watts
Power Gain – 13 dB
Efficiency – 50%
- Typical Performance at 860 MHz, 28 Volts, Broadband Push-Pull Fixture
Output Power – 100 Watts (PEP)
Power Gain – 11.2 dB
Efficiency – 40%
IMD – -30 dBc
- Excellent Thermal Stability
- 100% Tested for Load Mismatch Stress at All Phase Angles with 5:1 VSWR @ 28 Vdc, 860 MHz, 60 Watts CW

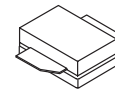


MRF373
MRF373S

60 W, 470 – 860 MHz, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETS



CASE 360B-03, STYLE 1
(MRF373)



CASE 360C-03, STYLE 1
(MRF373S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current – Continuous	I_D	7	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	MRF373S P_D	173 1.33	W W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	- 65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	MRF373S $R_{\theta JC}$	0.75	$^\circ\text{C/W}$
Thermal Resistance, Junction to Case	MRF373 $R_{\theta JC}$	1	$^\circ\text{C/W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 1 \mu\text{A}$)	$V_{(BR)DSS}$	65	–	–	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28 \text{ V}, V_{GS} = 0$)	I_{DSS}	–	–	1	μA dc
Gate–Source Leakage Current ($V_{GS} = 20 \text{ V}, V_{DS} = 0$)	I_{GSS}	–	–	1	μA dc

ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 200 \mu\text{A}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28 \text{ V}, I_D = 100 \text{ mA}$)	$V_{GS(Q)}$	3	4	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 3 \text{ A}$)	$V_{DS(on)}$	–	0.6	0.8	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ V}, I_D = 3 \text{ A}$)	g_{fs}	2.2	2.9	–	S

DYNAMIC CHARACTERISTICS

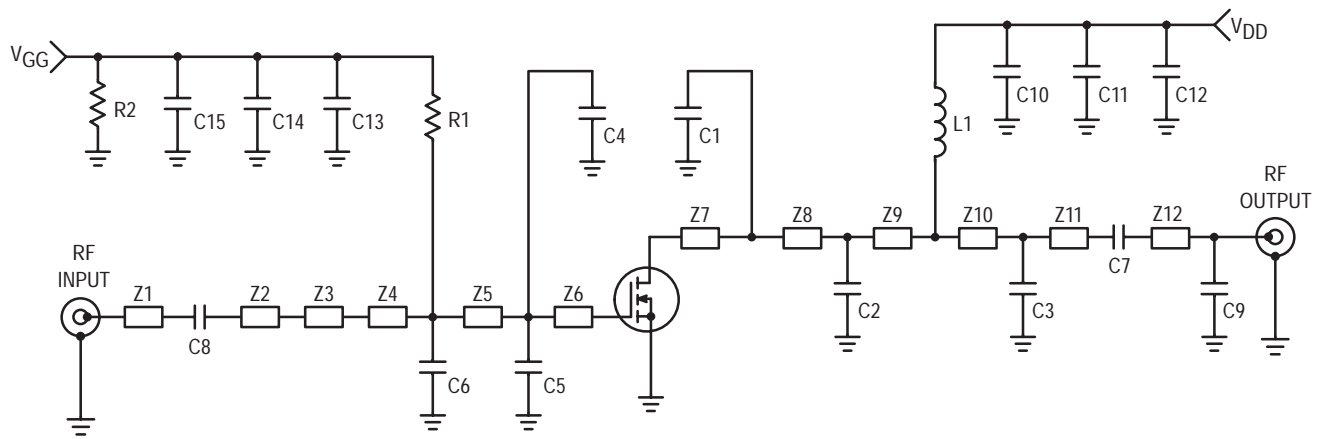
Input Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1 \text{ MHz}$)	C_{iss}	–	79	–	pF
Output Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1 \text{ MHz}$)	C_{oss}	–	46	–	pF
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ V}, V_{GS} = 0, f = 1 \text{ MHz}$)	C_{rss}	–	4	–	pF

FUNCTIONAL CHARACTERISTICS, CW Operation

Common Source Power Gain ($V_{DD} = 28 \text{ V}, P_{out} = 60 \text{ W}, I_{DQ} = 200 \text{ mA}, f = 860 \text{ MHz}$)	G_{ps}	13	14.7	–	dB
Drain Efficiency ($V_{DD} = 28 \text{ V}, P_{out} = 60 \text{ W}, I_{DQ} = 200 \text{ mA}, f = 860 \text{ MHz}$)	η	50	54	–	%
Load Mismatch ($V_{DD} = 28 \text{ V}, P_{out} = 60 \text{ W}, I_{DQ} = 200 \text{ mA}, f = 860 \text{ MHz}$, Load VSWR at 5:1 at All Phase Angles)	ψ	No Degradation in Output Power			

TYPICAL CHARACTERISTICS, 2 Tone Operation, Push Pull Configuration (MRF373S), Broadband Fixture

Common Source Power Gain ($V_{DD} = 28 \text{ Vdc}, P_{out} = 100 \text{ W PEP}, I_{DQ} = 400 \text{ mA}$, $f_1 = 860.0 \text{ MHz}, f_2 = 866 \text{ MHz}$)	G_{ps}	–	11.2	–	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}, P_{out} = 100 \text{ W PEP}, I_{DQ} = 400 \text{ mA}$, $f_1 = 860.0 \text{ MHz}, f_2 = 866 \text{ MHz}$)	η	–	40	–	%
Third Order Intermodulation Distortion ($V_{DD} = 28 \text{ Vdc}, P_{out} = 100 \text{ W PEP}, I_{DQ} = 400 \text{ mA}$, $f_1 = 860.0 \text{ MHz}, f_2 = 866 \text{ MHz}$)	IMD	–	–30	–	dBc



- | | | | |
|------------|---|---------------------|---|
| C1 | 4.7 pF, B Case Chip Capacitor, ATC | Connectors | N-Type (female), M/A Com P/N 3052-1648-10 |
| C2 | 15 pF, B Case Chip Capacitor, ATC | PCB | MRF373 Printed Circuit Board Rev 01, CuClad 250 (GX-0300-55), height 30 mils, $\epsilon_r = 2.55$ |
| C3 | 6.8 pF, B Case Chip Capacitor, ATC | Heatsink | Motorola P/N 95-11LDMOSKPS-1 |
| C4, C5, C6 | 10 pF, B Case Chip Capacitor, ATC | | LDMOS $\mu 250$ 3" x 5" Bedstead |
| C7, C8 | 47 pF, B Case Chip Capacitor, ATC | Insert | Motorola P/N 95-11LDMOSKPS-2 |
| C9 | 0.2 pF, B Case Chip Capacitor, ATC | | Insert for LDMOS $\mu 250$ 3" x 5" Bedstead |
| C10, C13 | 300 pF, B Case Chip Capacitor, ATC, Side Mounted | End Plates | 2) Motorola P/N 93-3MB-9, End Plate for Type-N Connector |
| C11 | 2) 2.2 μ F, 50 V, Kemet P/N C1825C225 | Banana Jack and Nut | 2) Johnson P/N 108-0904-001 |
| C12 | 22 μ F, 50 V, Kemet P/N T491D226K50AS | Brass Banana Jack | 2) H.H. Smith P/N SM-101 |
| C14 | 2) 1.0 μ F, 50 V, Kemet P/N C1825C105 | | |
| C15 | 10 μ F, 35 V, Kemet P/N T491D106K35AS | | |
| L1 | 22 nH, Coilcraft P/N B07T | | |
| R1 | 1.2 k Ω , Vishay Dale Chip Resistor (1206) | | |
| R2 | 12 k Ω , Vishay Dale Chip Resistor (1206) | | |

Figure 1. Single-Ended Narrowband Test Circuit Schematic (MRF373)

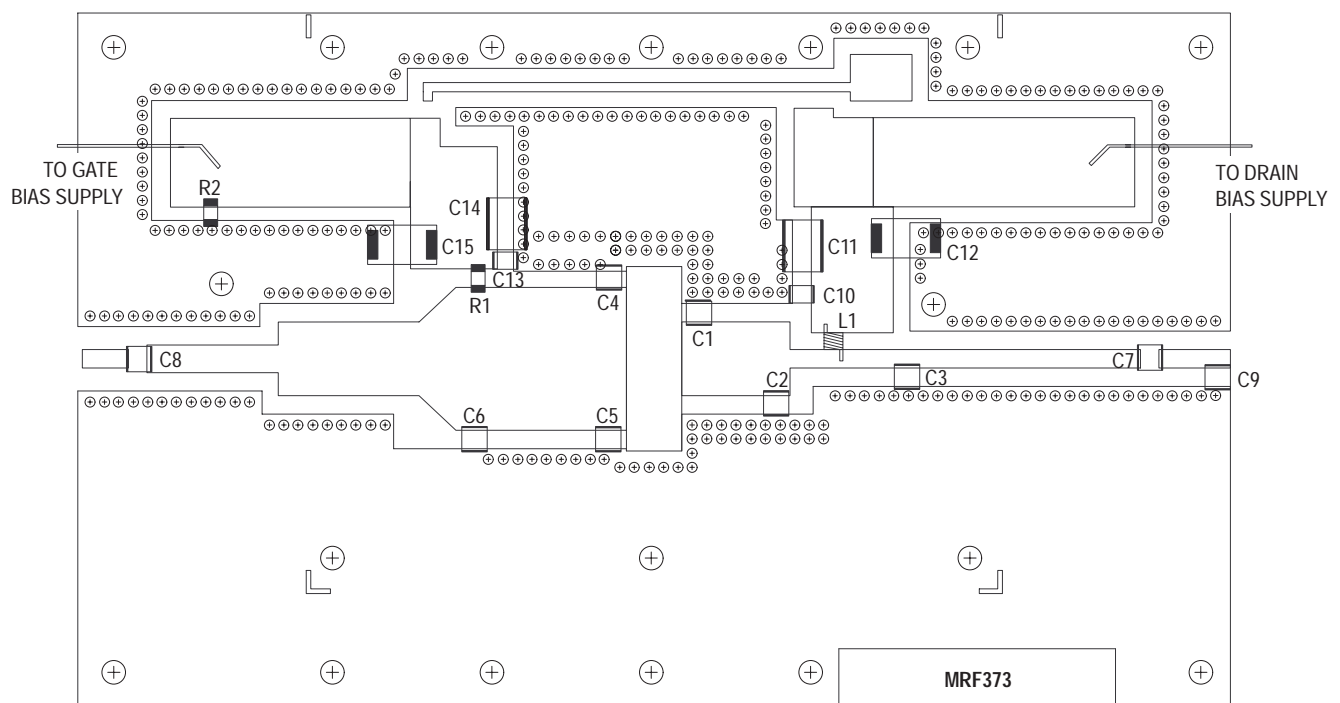


Figure 2. Single-Ended Narrowband Test Circuit Layout (Suitable for Use with MRF373)

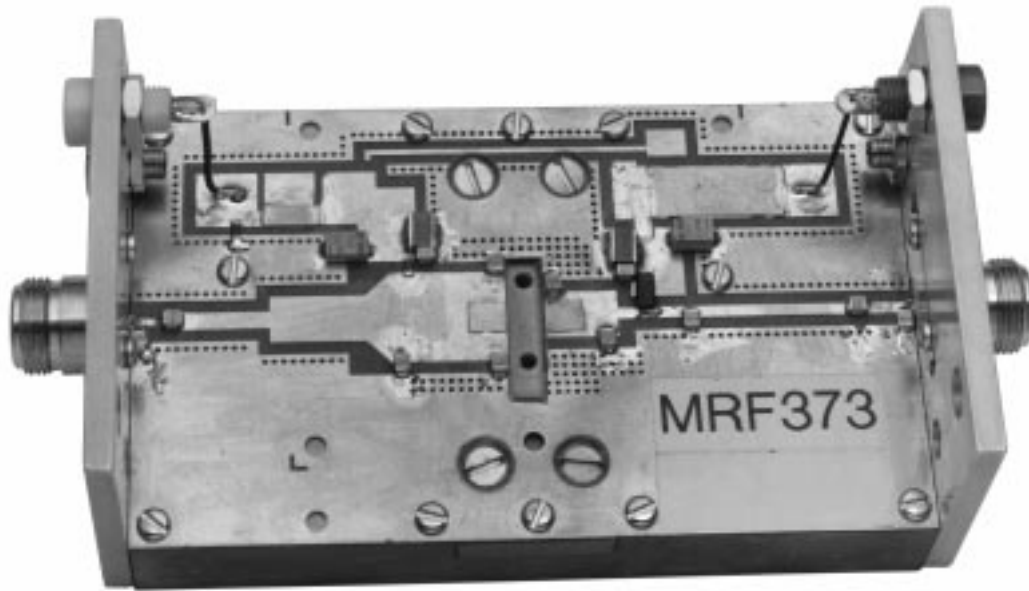
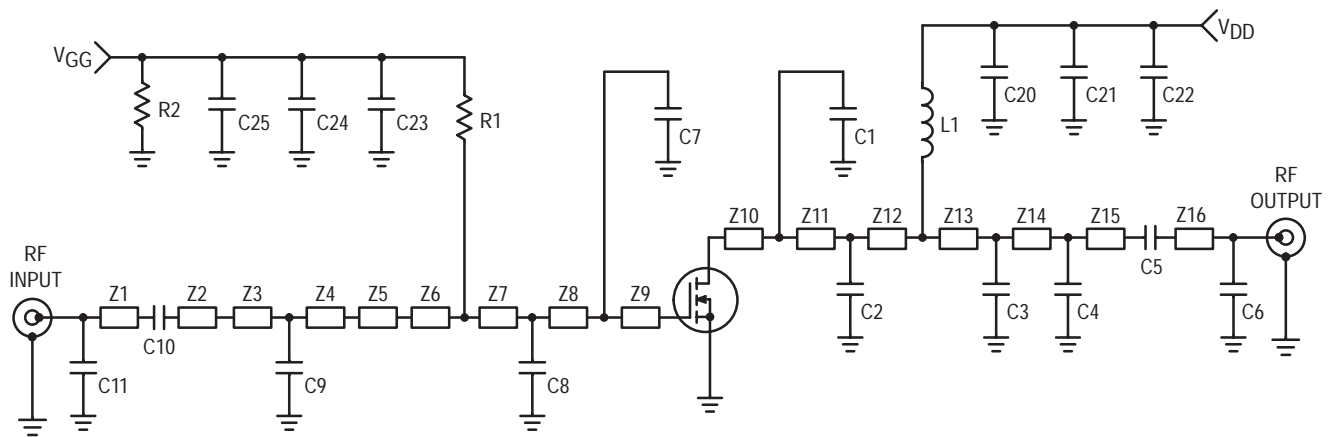


Figure 3. MRF373 Narrowband Test Fixture Photo



C1, C2	18 pF, B Case Chip Capacitor, ATC
C3	12 pF, B Case Chip Capacitor, ATC
C4, C11	0.8 pF, B Case Chip Capacitor, ATC
C5, C10	68 pF, B Case Chip Capacitor, ATC
C6	0.3 pF, B Case Chip Capacitor, ATC
C7	15 pF, B Case Chip Capacitor, ATC
C8	10 pF, B Case Chip Capacitor, ATC
C9	1.8 pF, B Case Chip Capacitor, ATC
C20, C23	300 pF, B Case Chip Capacitor, ATC, Side Mounted
C21	2) 2.2 μ F, 100 V, Vishay P/N VJ3640Y225KXBAT
C24	2) 1.0 μ F, 50 V, Kemet P/N C1825C105
C22	22 μ F, 35 V, Kemet P/N T491D226K35AS
C25	10 μ F, 35 V, Kemet P/N T491D106K35AS
L1	22 nH, Coilcraft P/N B07T
R1	1.2 k Ω , Vishay Dale Chip Resistor (1206)
R2	12 k Ω , Vishay Dale Chip Resistor (1206)

Connectors	N-Type (female), M/A Com P/N 3052-1648-10
PCB	MRF373 Printed Circuit Board Rev 01, CuClad 250 (GX-0300-55), height 30 mils, $\epsilon_r = 2.55$ (new PCB's available from CMR)
Heatsink	Motorola P/N 95-11LDMOSKPS-1 LDMOS μ 250 3" x 5" Bedstead
Insert	Motorola P/N 95-11LDMOSKPS-2S Insert for LDMOS μ 250S 3" x 5" Bedstead
End Plates	2) Motorola P/N 93-3MB-9, End Plate for Type-N Connector
Banana Jack and Nut	2) Johnson P/N 108-0904-001
Brass Banana Jack	2) H.H. Smith P/N SM-101

Figure 4. Single-Ended Narrowband Test Circuit Schematic (MRF373S)

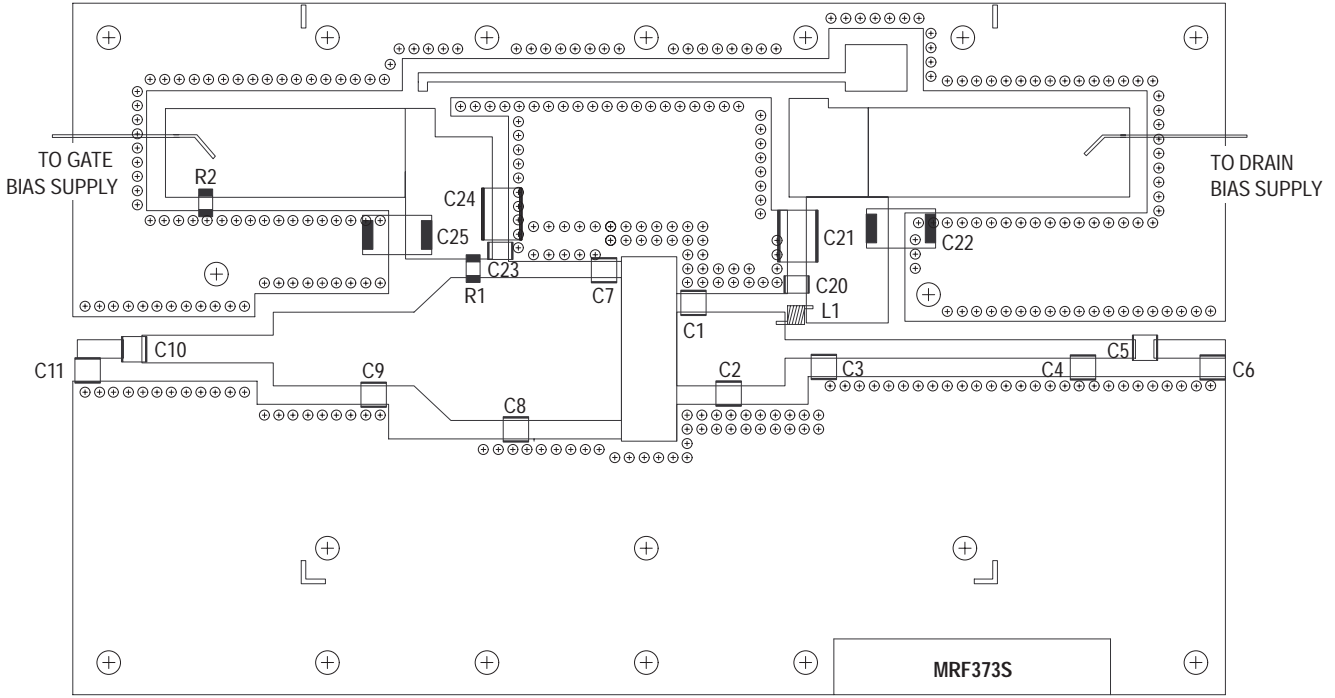


Figure 5. Single-Ended Narrowband Test Circuit Layout (Suitable for Use with MRF373S)

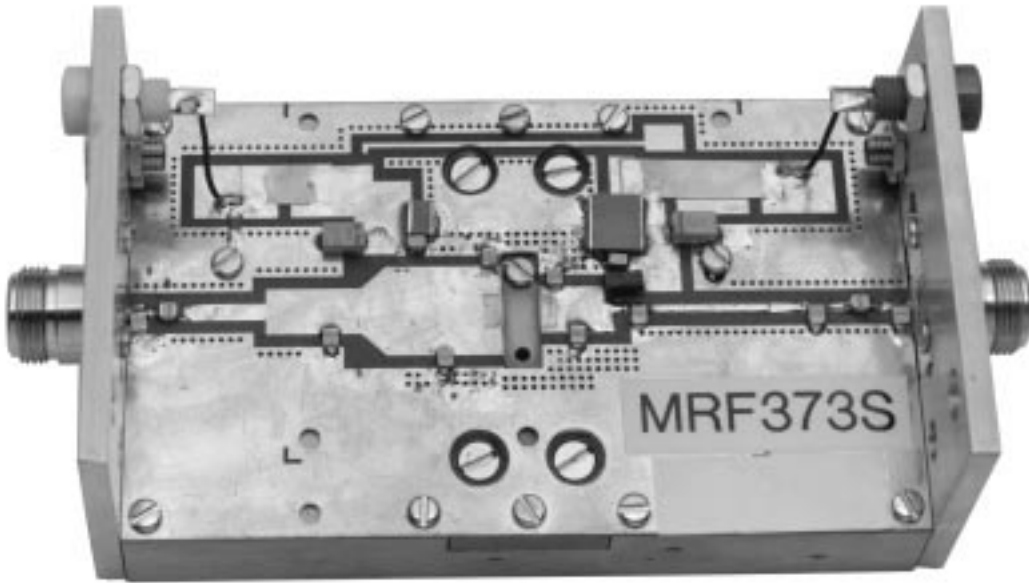


Figure 6. MRF373S Narrowband Test Circuit Photo

TYPICAL CHARACTERISTICS FOR MRF373 IN SINGLE-ENDED FIXTURE

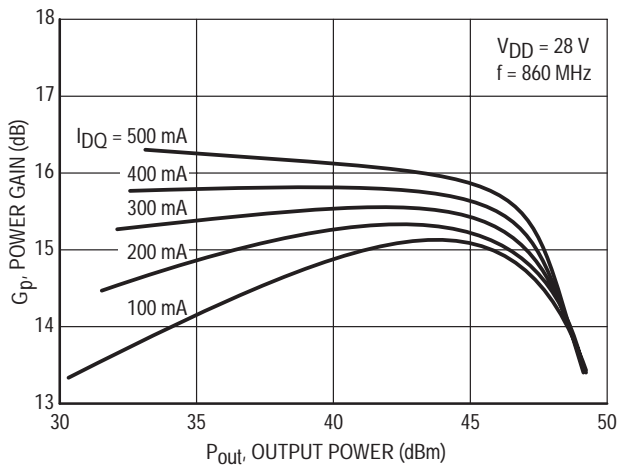


Figure 7. Power Gain versus Output Power

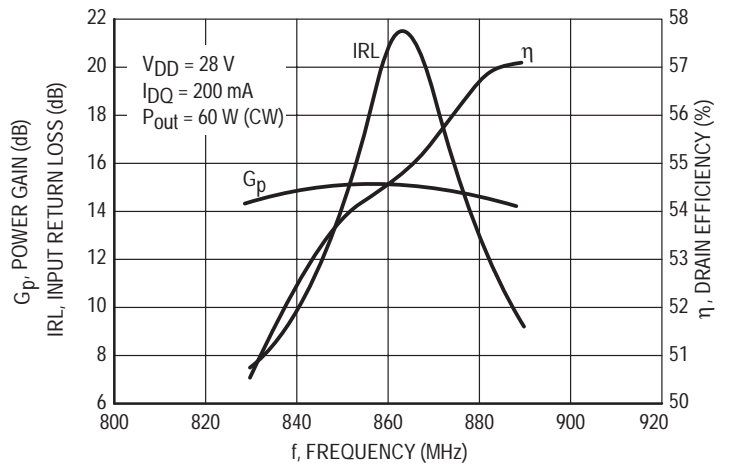


Figure 8. Performance in Narrowband Circuit

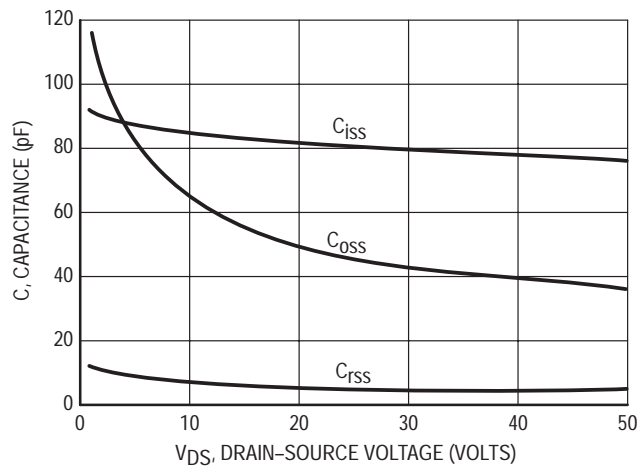


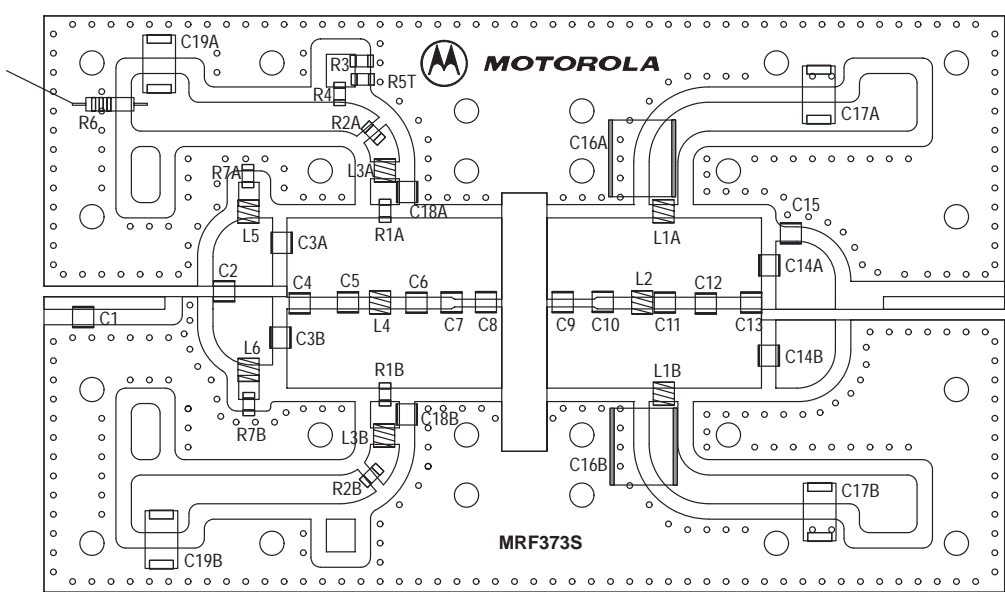
Figure 9. Capacitance versus Voltage

Table 1. Common Source S-Parameters ($V_{DS} = 28\text{ V}$, $I_D = 2.0\text{ A}$)

f MHz	S11		S21		S12		S22	
	S11	ϕ	S21	ϕ	S12	ϕ	S22	ϕ
400	0.921	182	2.23	52	0.009	39	0.824	184
450	0.922	181	1.95	49	0.009	53	0.832	184
500	0.924	180	1.70	46	0.010	64	0.841	184
550	0.926	179	1.49	42	0.011	72	0.851	183
600	0.929	178	1.31	38	0.013	78	0.860	183
650	0.932	177	1.16	35	0.015	81	0.870	182
700	0.936	176	1.03	31	0.017	82	0.881	182
750	0.940	176	0.93	28	0.019	82	0.892	181
800	0.945	175	0.84	26	0.021	82	0.904	180
850	0.951	174	0.78	24	0.023	80	0.917	180
900	0.957	173	0.72	24	0.025	78	0.929	179

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04



Vertical Balun Mounting Detail

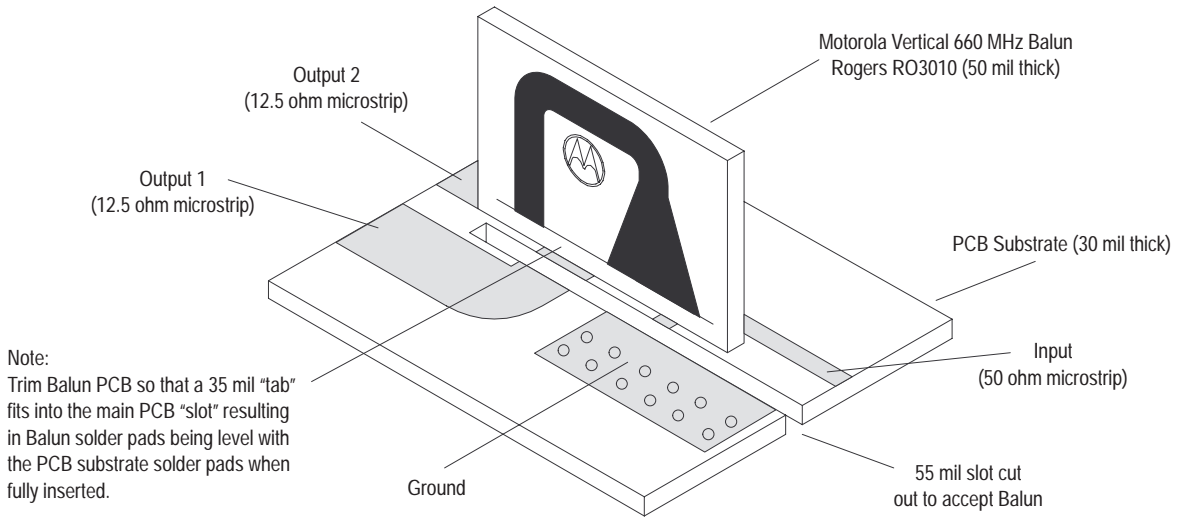


Figure 10. MRF373S Broadband Push-Pull Component Layout

LIFETIME BUY

Table 2. MRF373S Broadband Push–Pull Application Parts List

Designation	Description
C1	1.0 pF, AVX, P12101J1R0BBT
C2, C4, C10	10 pF, AVX, P12101J100GBT
C3A, B	120 pF, 300 V, AVX, AQ149M121JAJBE
C5, C6, C9	12 pF, AVX, P12101J120GBT
C7, C8	18 pF, AVX, P12101J180GBT
C11	6.8 pF, AVX, P12101J6R8BBT
C12	4.7 pF, AVX, P12101J4R7BBT
C13, C18A, B	3.3 pF, AVX, P12101J3R3BBT
C14A, B	100 pF, 500 V, AVX, AQ147M101JAJBE
C15	2.7 pF, AVX, P12101J2R7BBT
C16A, B	3.3 μ F, 100 V, Vitramon P/N VJ3640Y335KXBAT
C17A, B, C19A, B	22 μ F, 35 V, Kemet P/N T491D226K35AS
L1A, B, L3A, B, L4, L5	8.0 nH, Coilcraft P/N A03T
L2, L6	12.5 nH, Coilcraft P/N A04T
R1A, B	22 Ω , Vishay Dale Chip Resistor, 1/4 W (1206)
R2A, B	10 Ω , Vishay Dale Chip Resistor, 1/4 W (1206)
R3	390 Ω , Vishay Dale Chip Resistor (1206)
R4	2.4 k Ω , Vishay Dale Chip Resistor (1206)
R5T	470 Ω Thermistor, KOA SPEER MOT P/N 0680149M01
PCB	MRF373 PP Printed Circuit Board Rev 2C, Rogers RO4350, Height 30 mils, $\epsilon_r = 3.48$
Balun A, B	Vertical 660 MHz Broadband Balun, Printed Circuit Board Rev 01, Rogers RO3010, Height 50 mils, $\epsilon_r = 10.2$

LAST ORDER 31JUL04 LAST SHIP 31JAN05

TYPICAL TWO-TONE BROADBAND CHARACTERISTICS

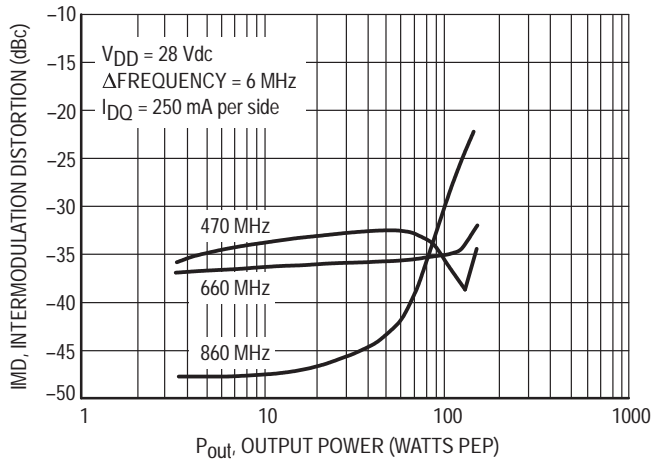


Figure 11. Intermodulation Distortion versus Output Power (MRF373S Broadband Push-Pull Fixture)

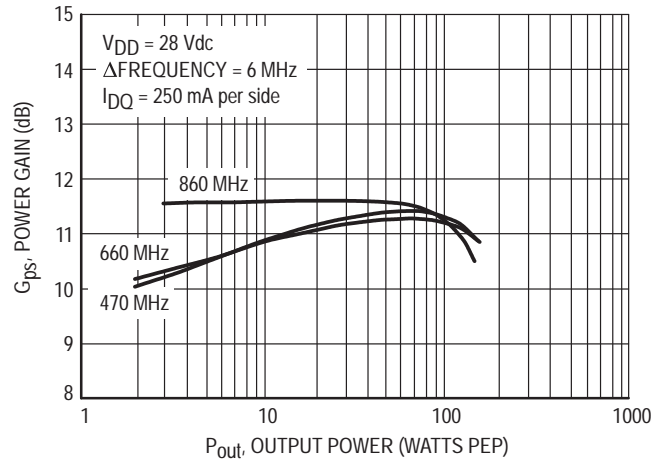


Figure 12. Broadband Power Gain versus Output Power (MRF373S Broadband Push-Pull Fixture)

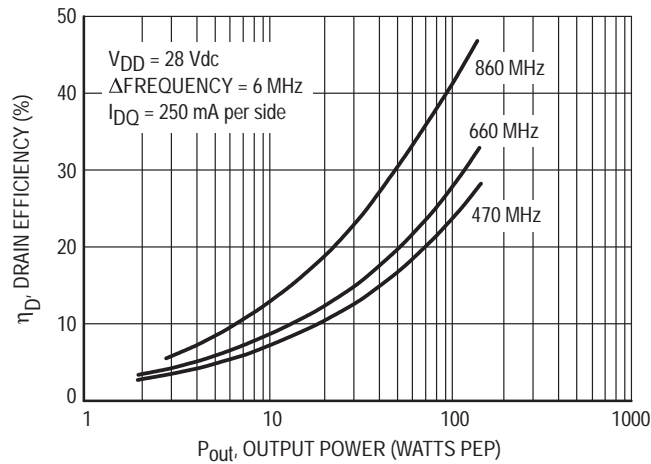


Figure 13. Efficiency versus Output Power (MRF373S Broadband Push-Pull Fixture)

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

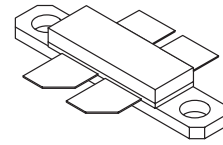
The RF MOSFET Line
RF Power Field-Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

Designed for broadband commercial and industrial applications at frequencies from 470 – 860 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 28 volt transmitter equipment.

- Typical Two-Tone Performance @ 860 MHz, 28 Volts, Narrowband Fixture
Output Power – 100 Watts PEP
Power Gain – 13.5 dB
Efficiency – 36%
IMD – –31 dBc
- Typical Performance at 860 MHz, 28 Volts, Broadband Fixture
Output Power – 100 Watts PEP
Power Gain – 12 dB
Efficiency – 36%
IMD – –34 dBc
- 100% Tested for Load Mismatch Stress at All Phase Angles with 5:1 VSWR @ 28 Vdc, 860 MHz, 100 Watts CW
- Excellent Thermal Stability
- Characterized with Differential Large-Signal Impedance Parameters

MRF374

470 – 860 MHz, 100 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 375F-02, STYLE 2

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	±20	Vdc
Drain Current – Continuous (per Side)	I_D	7	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	270 1.25	W W/°C
Storage Temperature Range	T_{stg}	– 65 to +150	°C
Operating Junction Temperature	T_J	200	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.65	°C/W

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage (per Side) ($V_{GS} = 0\text{ V}$, $I_D = 1\ \mu\text{A}$ per Side)	$V_{(BR)DSS}$	65	–	–	Vdc
Zero Gate Voltage Drain Current (per Side) ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	–	–	1	μAdc
Gate–Source Leakage Current (per Side) ($V_{GS} = 20\text{ V}$, $V_{DS} = 0\text{ V}$)	I_{GSS}	–	–	1	μAdc

ON CHARACTERISTICS

Gate Threshold Voltage (per Side) ($V_{DS} = 10\text{ V}$, $I_D = 200\ \mu\text{A}$ per Side)	$V_{GS(th)}$	2	3.5	4	Vdc
Gate Quiescent Voltage (per Side) ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$ per Side)	$V_{GS(Q)}$	3	4.2	5	Vdc
Drain–Source On–Voltage (per Side) ($V_{GS} = 10\text{ V}$, $I_D = 3\text{ A}$ per Side)	$V_{DS(on)}$	–	0.56	0.8	Vdc
Forward Transconductance (per Side) ($V_{DS} = 10\text{ V}$, $I_D = 3\text{ A}$ per Side)	g_{fs}	2.2	2.8	–	S

DYNAMIC CHARACTERISTICS (1)

Input Capacitance (per Side) ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{iss}	–	80	–	pF
Output Capacitance (per Side) ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{oss}	–	45	–	pF
Reverse Transfer Capacitance (per Side) ($V_{DS} = 28\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{rss}	–	3.5	–	pF

FUNCTIONAL CHARACTERISTICS, TWO–TONE TESTING (2)

Common Source Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W PEP}$, $I_{DQ} = 400\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	G_{ps}	12.5	13.5	–	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W PEP}$, $I_{DQ} = 400\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	η	30	36	–	%
Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W PEP}$, $I_{DQ} = 400\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	IMD	–28	–31	–	dB
Load Mismatch ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W CW}$, $I_{DQ} = 400\text{ mA}$, $f = 860\text{ MHz}$, VSWR 5:1 at All Phase Angles of Test)		No Degradation in Output Power			

TYPICAL TWO–TONE BROADBAND

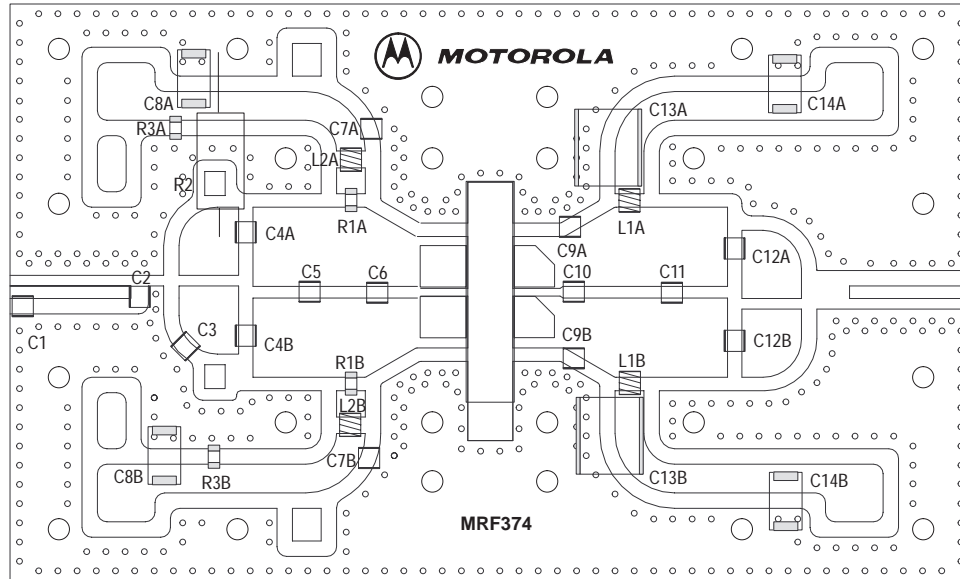
Common Source Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	G_{ps}	–	12	–	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	η	–	36	–	%
Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 100\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 857\text{ MHz}$, $f_2 = 863\text{ MHz}$)	IMD	–	–34	–	dB

(1) Each side of device measured separately.

(2) Measured in push–pull configuration.

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04



Vertical Balun Mounting Detail

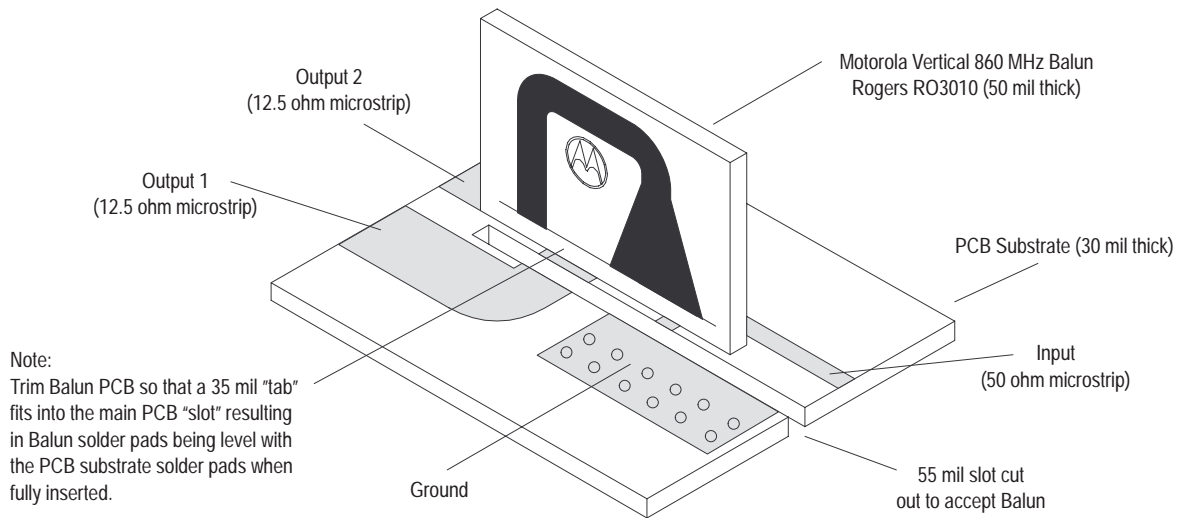


Figure 1. Narrowband Component Layout

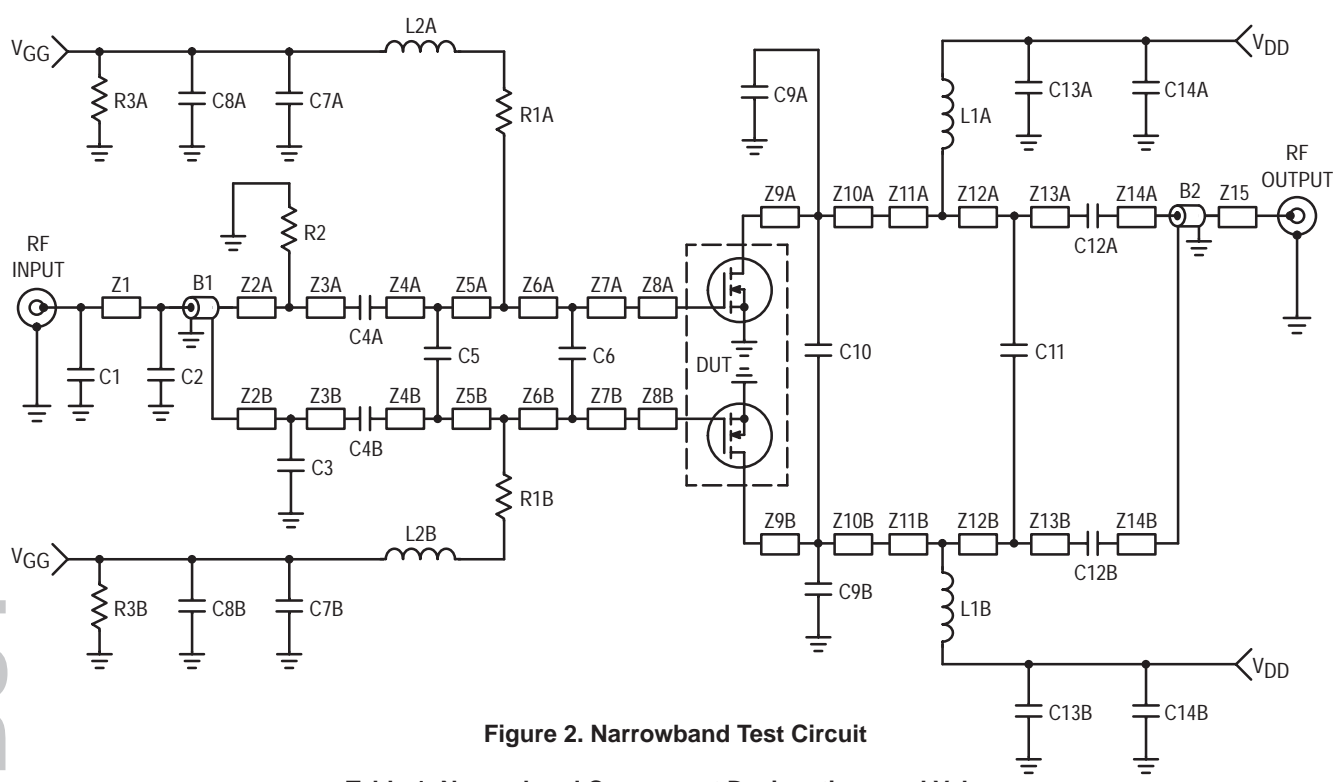


Figure 2. Narrowband Test Circuit

Table 1. Narrowband Component Designations and Values

Designation	Description
C1	0.3 pF, ATC, Case B
C2	3.0 pF, ATC, Case B
C3, C5	1.8 pF, ATC, Case B
C4A, B, C12A, B	47 pF, ATC, Case B
C6	10 pF, ATC, Case B
C7A, B	68 pF, ATC, Case B
C8A, B	10 μ F, 35 V Kemet P/N T491D106K35AS
C9A, B	15 pF, ATC, Case B
C10	5.6 pF, ATC, Case B
C11	5.1 pF, ATC, Case B
C12	3.0 pF, ATC, Case B
C13A, B	2.2 μ F, 100 V, Vishay P/N VJ3640Y225KXBAT
C14A, B	22 μ F, 35 V Kemet P/N T491D226K35AS
L1A, B	5.0 nH, Coilcraft P/N A02T
L2A, B	8.0 nH, Coilcraft P/N A03T
R1A, B	180 Ω , Vishay Dale Chip Resistor, 1/4 W (1210)
R2	10 Ω , Dale Axial Carbon Resistor, 1 W
R3A, B	3.3 k Ω , Vishay Dale Chip Resistor (1206)
PCB	MRF374 Printed Circuit Board Rev 03, Rogers RO4350, Height 30 mils, $\epsilon_r = 3.48$
Balun B1A, B	860 MHz Vertical Balun, 4:1 Impedance Translation (i.e., 12.5 Ω : 50 Ω), Printed Circuit Board Rev 01, Rogers RO3010, Height 50 mils, $\epsilon_r = 10.2$
Connectors	N-Type (female), M/A-Com P/N 3052-1648-10
Heatsink	Motorola P/N 99-1RH-2C 3" X 5" Bedstead
Insert	Motorola P/N 99-7RI-1D Insert for LDMOS μ 650 in 3" X 5" Bedstead
Protective Cover	Motorola P/N 99-2PC-2B
End Plates	2) Motorola P/N 94-7GB-1EPL, End Plate for Type-N Connector
Banana Jack and Nut	2) Johnson P/N 108-0904-001
Brass Banana Jack	2) H.H. Smith P/N SM-101

TYPICAL TWO-TONE NARROWBAND CHARACTERISTICS

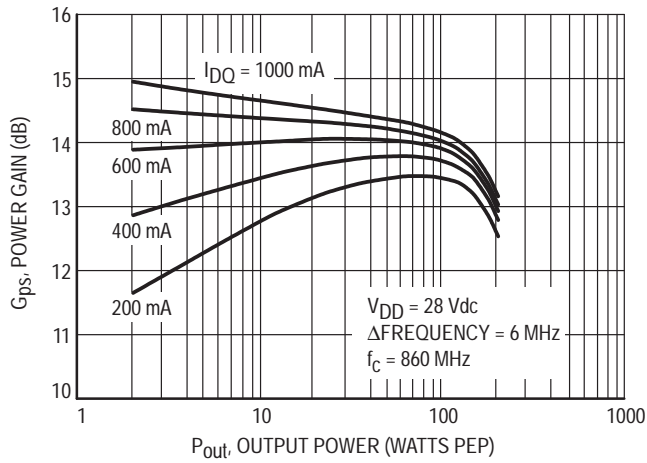


Figure 3. Power Gain versus Peak Output Power

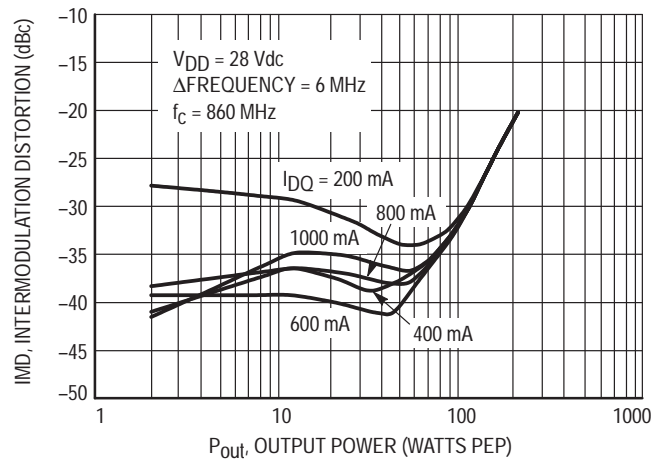


Figure 4. Intermodulation Distortion versus Peak Output Power

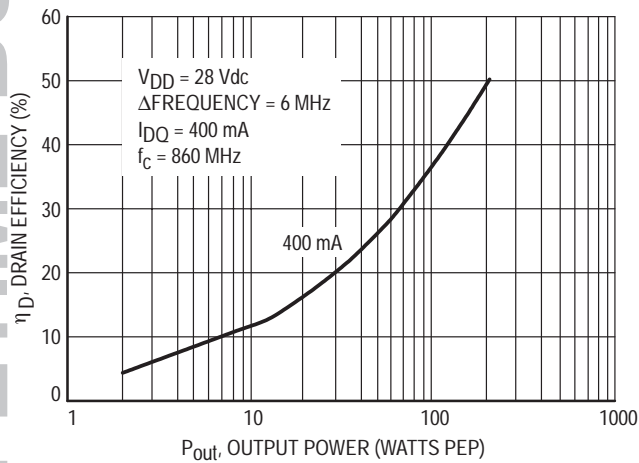


Figure 5. Drain Efficiency versus Peak Output Power

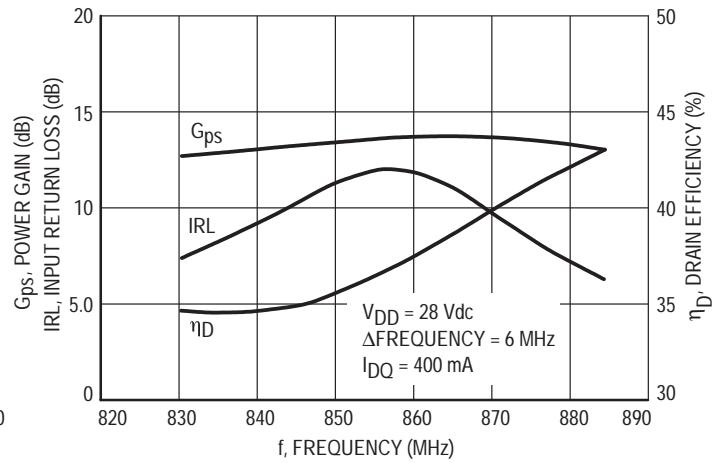


Figure 6. Performance in Narrowband Test Circuit

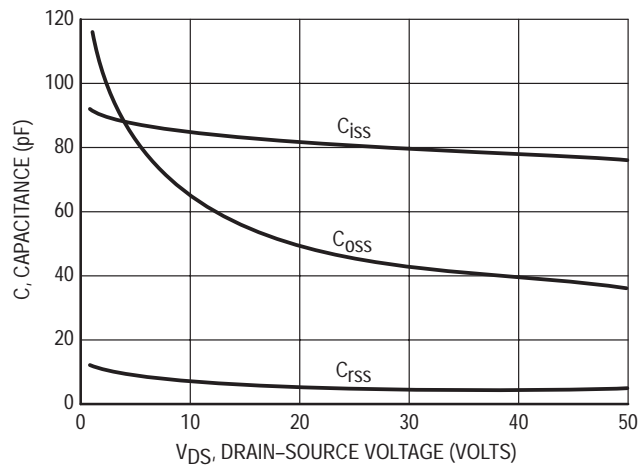
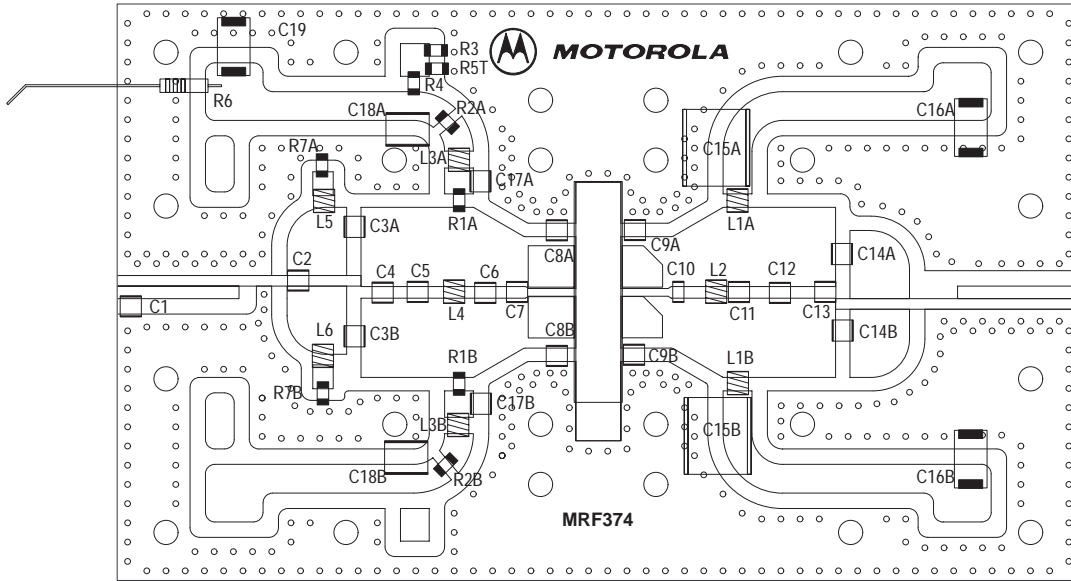


Figure 7. Capacitance versus Voltage

LIFETIME BUY

LAST ORDER 31JUL04 LAST SHIP 31JAN05



Vertical Balun Mounting Detail

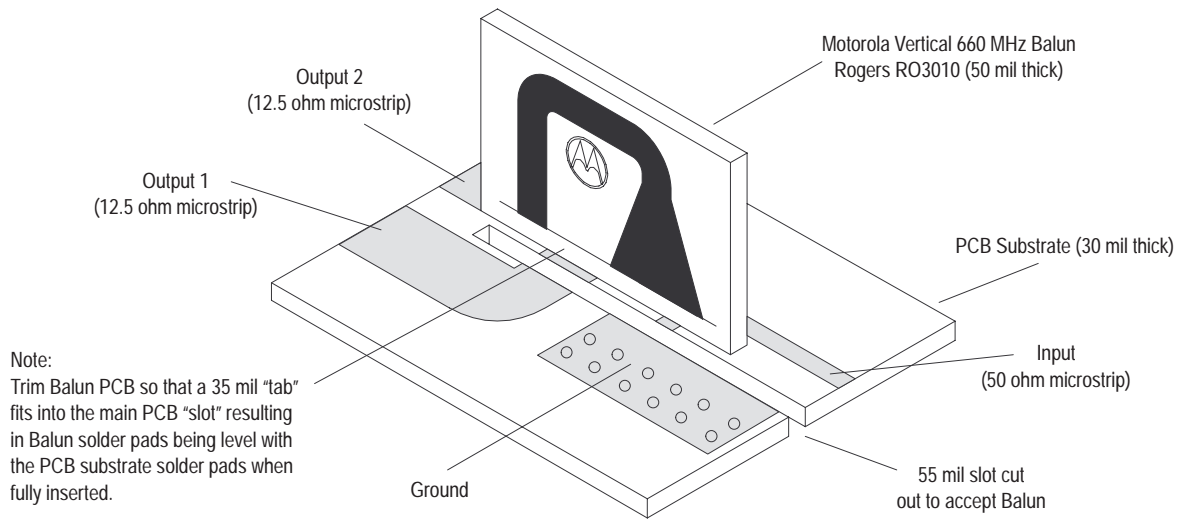


Figure 8. Broadband Component Layout

Table 2. Broadband Component Designations and Values

Designation	Description
C1	0.8 pF, ATC, Case B
C2	8.2 pF, ATC, Case B
C3A, B, C14A, B	100 pF, ATC, Case B
C4	7.5 pF, ATC, Case B
C5	3.0 pF, ATC, Case B
C6	9.1 pF, ATC, Case B
C7	15 pF, ATC, Case B
C8A, B	12 pF, ATC, Case B
C9A, B	4.7 pF, ATC, Case B
C10	10 pF, ATC, Case B
C11	3.6 pF, ATC, Case B
C12	3.0 pF, ATC, Case B
C13	2.7 pF, ATC, Case B
C15A, B	3.3 μ F, 100 V, Vitramon P/N VJ3640Y335KXBAT
C16A, B	22 μ F, 35 V, Kemet P/N T491D226K035AS
C17A, B	3.9 pF, ATC, Case B
C18A, B	2.2 μ F, 50 V, Vitramon P/N VJ2225Y225KXAAT
C19	10 μ F, 35 V, Kemet P/N T491D106K035AS
L1A, B, L3A, B, L4, L5	8.0 nH, Coilcraft P/N A03T
L2, L6	12.5 nH, Coilcraft P/N A04T
R1A, B	22 Ω , Vishay Dale Chip Resistor, 1/4 W (1206)
R2A, B, R7A, B	10 Ω , Vishay Dale Chip Resistor, 1/4 W (1206)
R3	390 Ω , Vishay Dale Chip Resistor (1206)
R4	2.4 k Ω , Vishay Dale Chip Resistor (1206)
R5T	470 Ω Thermistor, KOA SPEER MOT P/N 0680149M01
R6	6.8 k Ω , Vishay Dale Resistor, 1/2 W (Axial Lead)
PCB	MRF374 Printed Circuit Board Rev 03, Rogers RO4350, Height 30 mils, $\epsilon_r = 3.48$
Balun B1, B2	Vertical 660 MHz Broadband Balun, Printed Circuit Board Rev 01, Rogers RO3010, Height 50 mils, $\epsilon_r = 10.2$

f MHz	Z _{in} Ω	Z _{OL} * Ω
470	5.79 - j0.97	4.54 + j2.82
660	4.52 + j0.50	4.21 + j3.04
860	3.16 + j3.73	3.86 + j3.44

Z_{in} = Input impedance from the transistor.

Z_{OL}* = Complex conjugate of the optimum load at a given voltage, P1dB, gain, efficiency, bias current and frequency.

Note: Z_{in} and Z_{OL} are measured impedances taken from gate-to-gate and drain-to-drain, respectively.

Table 3. Broadband Push-Pull Balanced Fixture Impedances

TYPICAL TWO-TONE BROADBAND CHARACTERISTICS

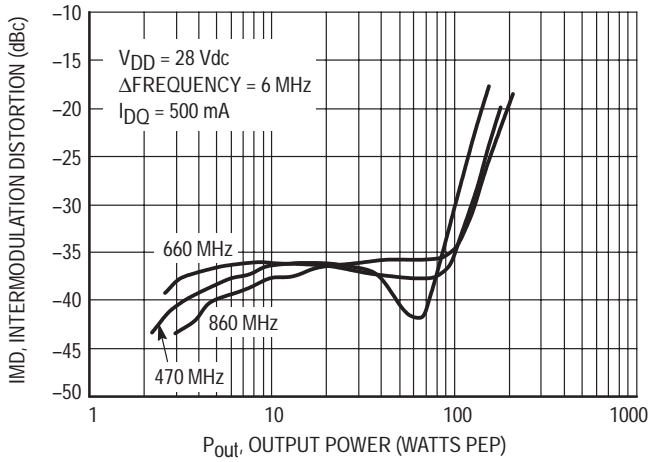


Figure 9. Broadband Intermodulation Distortion versus Output Power

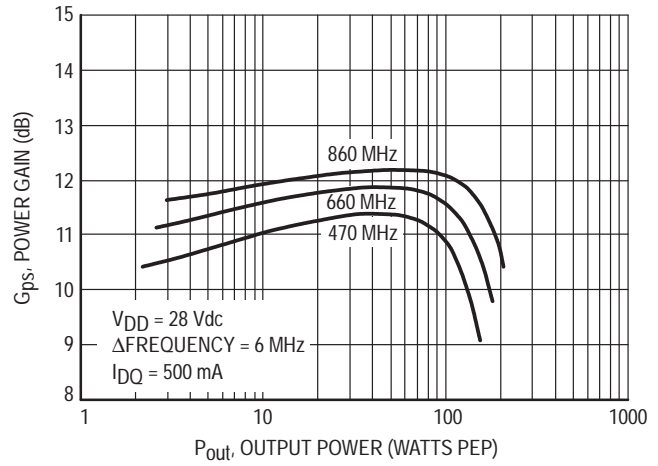


Figure 10. Broadband Power Gain versus Output Power

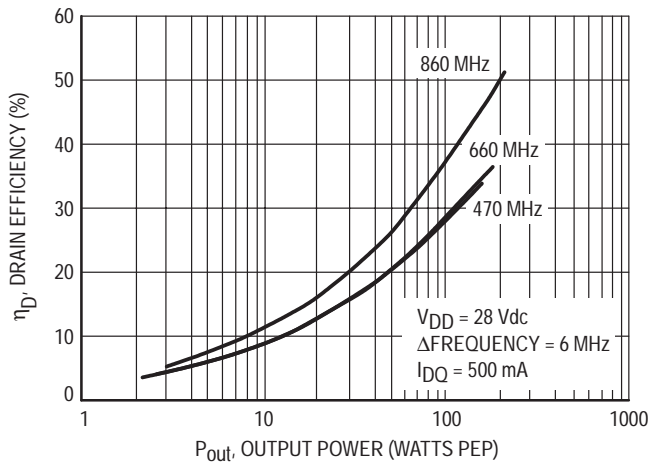


Figure 11. Broadband Efficiency versus Output Power

LIFETIME BUY

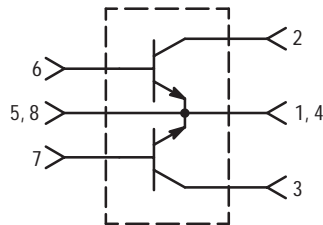
LAST SHIP 31JAN05
LAST ORDER 31JUL04

The RF Line

NPN Silicon Push-Pull RF Power Transistor

Designed primarily for wideband large-signal output and driver amplifier stages in the 30 to 500 MHz frequency range.

- Specified 28 Volt, 400 MHz Characteristics —
Output Power = 125 W
Typical Gain = 10 dB
Efficiency = 55% (Typ)
- Built-In Input Impedance Matching Networks for Broadband Operation
- Push-Pull Configuration Reduces Even Numbered Harmonics
- Gold Metallization System for High Reliability
- 100% Tested for Load Mismatch
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.



The MRF392 is two transistors in a single package with separate base and collector leads and emitters common. This arrangement provides the designer with a space saving device capable of operation in a push-pull configuration.

PUSH-PULL TRANSISTORS

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CEO}	30	Vdc
Collector-Base Voltage	V_{CBO}	60	Vdc
Emitter-Base Voltage	V_{EBO}	4.0	Vdc
Collector Current — Continuous	I_C	16	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1) Derate above 25°C	P_D	270 1.54	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

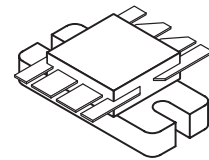
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.65	$^\circ\text{C}/\text{W}$

NOTE:

1. This device is designed for RF operation. The total device dissipation rating applies only when the device is operated as an RF push-pull amplifier.

MRF392

125 W, 30 to 500 MHz
CONTROLLED "Q"
BROADBAND PUSH-PULL
RF POWER TRANSISTOR
NPN SILICON



CASE 744A-01, STYLE 1

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)					
Collector–Emitter Breakdown Voltage ($I_C = 50\text{ mA dc}$, $I_B = 0$)	$V_{(BR)CEO}$	30	—	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 50\text{ mA dc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	60	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 5.0\text{ mA dc}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 30\text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	5.0	mAdc

ON CHARACTERISTICS (1)

DC Current Gain ($I_C = 1.0\text{ A dc}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	40	60	100	—
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DYNAMIC CHARACTERISTICS (1)

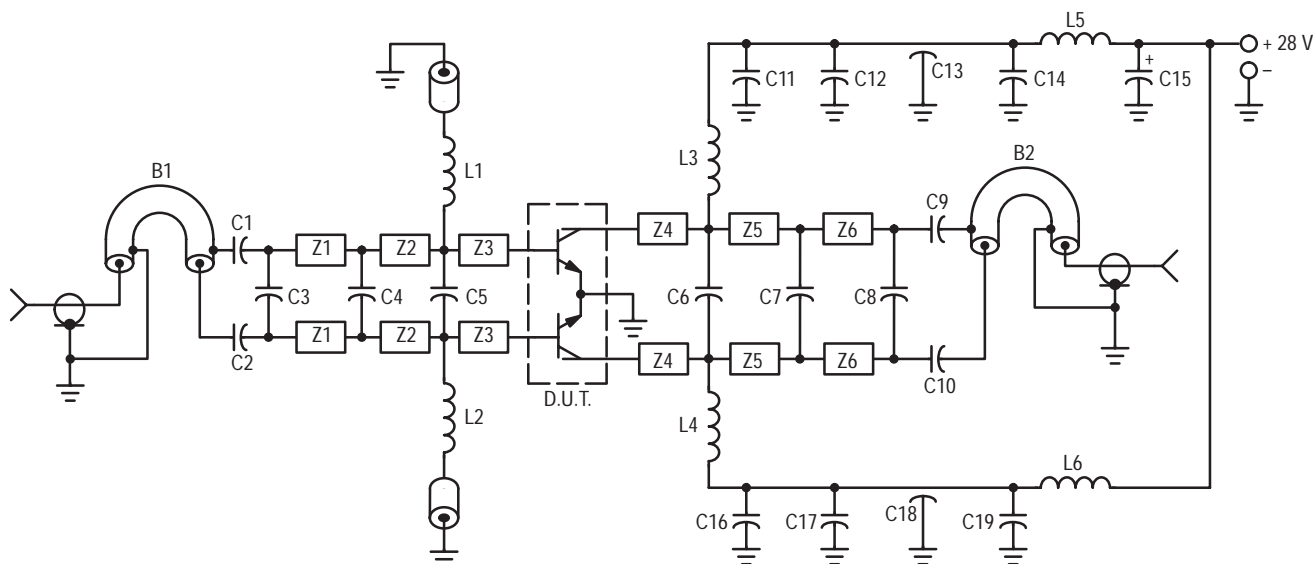
Output Capacitance ($V_{CB} = 28\text{ Vdc}$, $I_E = 0$, $f = 1.0\text{ MHz}$)	C_{ob}	—	75	95	pF
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FUNCTIONAL TESTS (2) — See Figure 1

Common–Emitter Amplifier Power Gain ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 125\text{ W}$, $f = 400\text{ MHz}$)	G_{pe}	8.0	10	—	dB
Collector Efficiency ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 125\text{ W}$, $f = 400\text{ MHz}$)	η	50	55	—	%
Load Mismatch ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 125\text{ W}$, $f = 400\text{ MHz}$, VSWR = 30:1, all phase angles)	ψ	No Degradation in Output Power			

NOTES:

- Each transistor chip measured separately.
- Both transistor chips operating in push–pull amplifier.



- C1, C2 — 240 pF, 100 Mil Chip Cap (ATC) or Equivalent
 C3 — 3.6 pF, 100 Mil Chip Cap (ATC) or Equivalent
 C4, C8 — 8.2 pF, 100 Mil Chip Cap (ATC) or Equivalent
 C5, C6 — 20 pF, 100 Mil Chip Cap (ATC) or Equivalent
 C7 — 18 pF, Mini Unelco or Equivalent
 C9, C10 — 270 pF, 100 Mil Chip Cap (ATC) or Equivalent
 C11, C12, C16, C17 — 470 pF 100 Mil Chip Cap (ATC) or Equivalent
 C13, C18 — 680 pF Feedthru
 C14, C19 — 0.1 μF Erie Redcap or Equivalent
 C15 — 20 μF , 50 V

- L1, L2 — 0.15 μH Molded Choke With Ferrite Bead
 L3, L4 — 2–1/2 Turns #20 AWG, 0.200 ID
 L5, L6 — 3–1/2 Turns #18 AWG, 0.200 ID

- B1 — Balun, 50 Ω Semi–Rigid Coaxial Cable 86 Mil OD, 2" L
 B2 — Balun, 50 Ω Semi–Rigid Coaxial Cable 86 Mil OD, 2" L
 Z1 — Microstrip Line 270 Mil L x 125 Mil W
 Z2 — Microstrip Line 375 Mil L x 125 Mil W
 Z3 — Microstrip Line 280 Mil L x 125 Mil W
 Z4 — Microstrip Line 300 Mil L x 125 Mil W
 Z5 — Microstrip Line 350 Mil L x 125 Mil W
 Z6 — Microstrip Line 365 Mil L x 125 Mil W

Board Material — 0.0625" Teflon Fiberglass $\epsilon_r = 2.5 \pm 0.05$ 1 oz. Cu.
 CLAD, Double Sided

Figure 1. 400 MHz Test Fixture

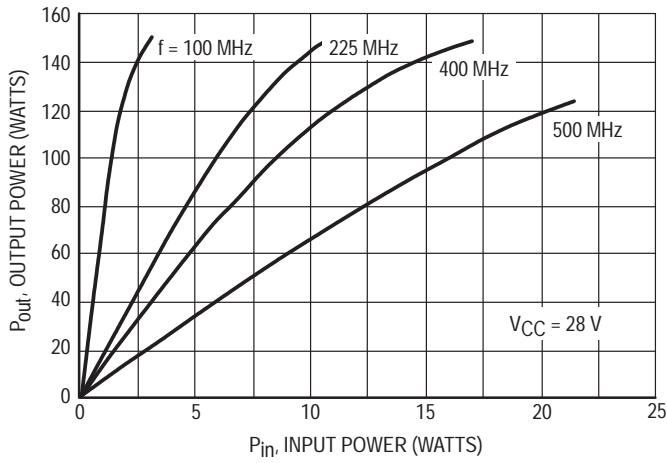


Figure 2. Output Power versus Input Power

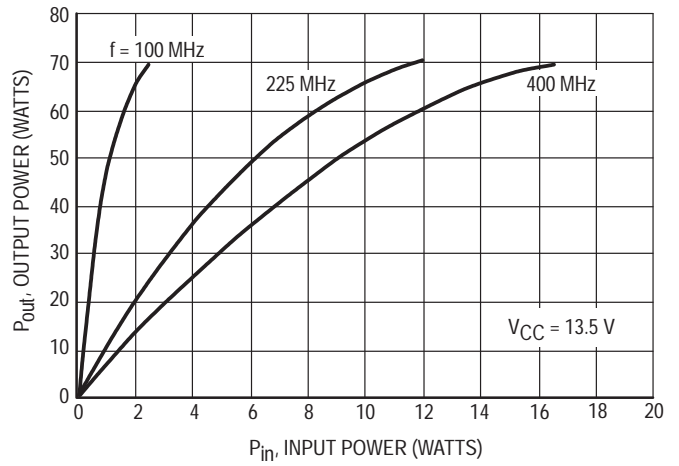


Figure 3. Output Power versus Input Power

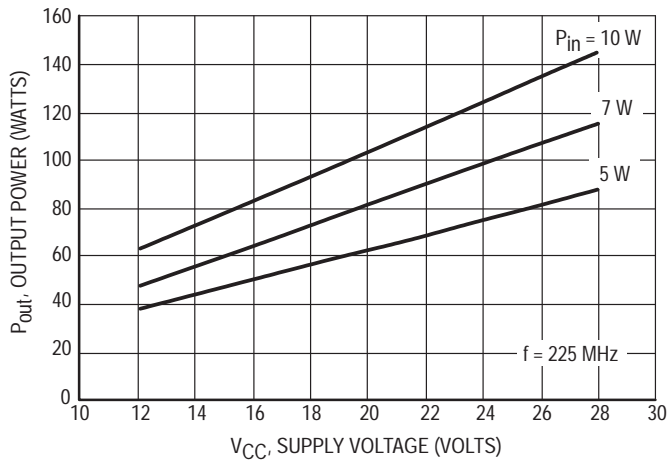


Figure 4. Output Power versus Supply Voltage

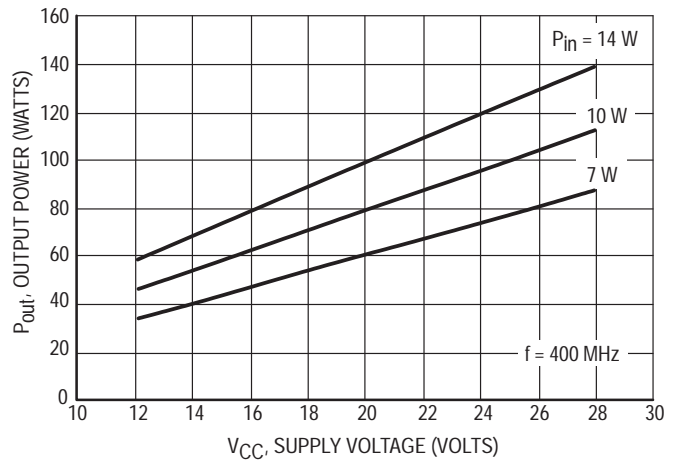


Figure 5. Output Power versus Supply Voltage

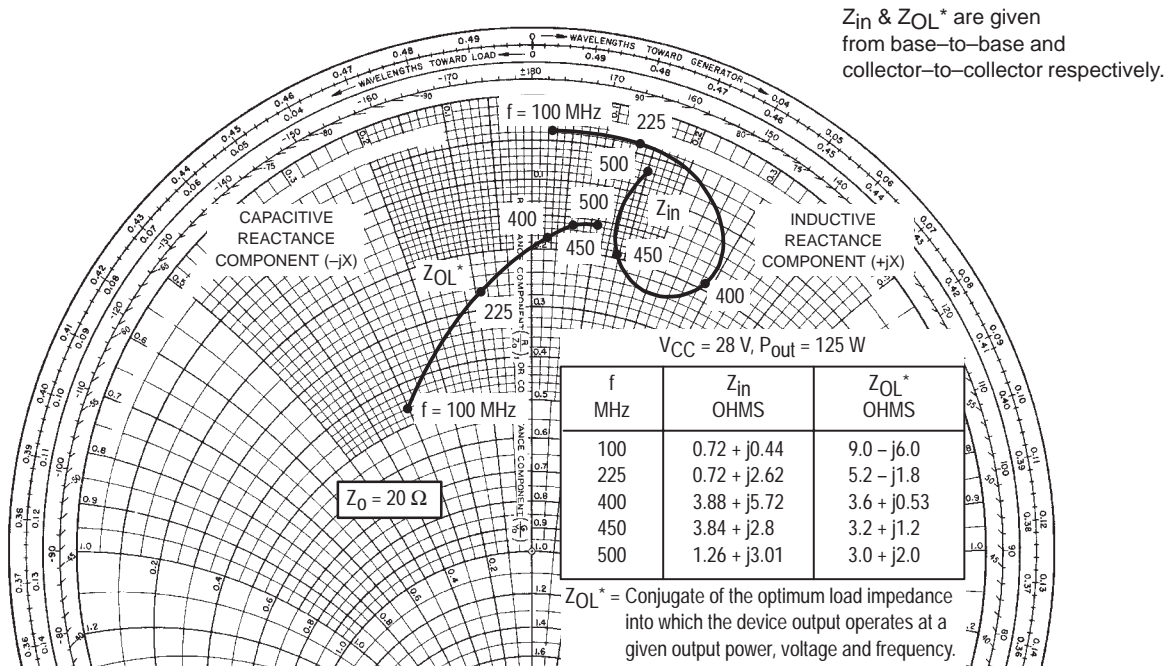
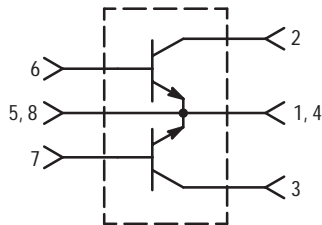


Figure 6. Series Equivalent Input/Output Impedance

The RF Line
**NPN Silicon Push-Pull
RF Power Transistor**

... designed primarily for wideband large-signal output and driver amplifier stages in the 30 to 500 MHz frequency range.

- Specified 28 Volt, 500 MHz Characteristics —
Output Power = 100 W
Typical Gain = 9.5 dB (Class AB); 8.5 dB (Class C)
Efficiency = 55% (Typ)
- Built-In Input Impedance Matching Networks for Broadband Operation
- Push-Pull Configuration Reduces Even Numbered Harmonics
- Gold Metallization System for High Reliability
- 100% Tested for Load Mismatch
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

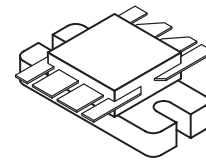


The MRF393 is two transistors in a single package with separate base and collector leads and emitters common. This arrangement provides the designer with a space saving device capable of operation in a push-pull configuration.

PUSH-PULL TRANSISTORS

MRF393

**100 W, 30 to 500 MHz
CONTROLLED "Q"
BROADBAND PUSH-PULL
RF POWER TRANSISTOR
NPN SILICON**



CASE 744A-01, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CEO}	30	Vdc
Collector-Base Voltage	V_{CBO}	60	Vdc
Emitter-Base Voltage	V_{EBO}	4.0	Vdc
Collector Current — Continuous	I_C	16	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1) Derate above 25°C	P_D	270 1.54	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.65	$^\circ\text{C}/\text{W}$

NOTE:

- This device is designed for RF operation. The total device dissipation rating applies only when the device is operated as an RF push-pull amplifier.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)					
Collector–Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $I_B = 0$)	$V_{(BR)CEO}$	30	—	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	60	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 5.0 \text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 30 \text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	5.0	mAdc

ON CHARACTERISTICS (1)

DC Current Gain ($I_C = 1.0 \text{ Adc}$, $V_{CE} = 5.0 \text{ Vdc}$)	h_{FE}	20	—	100	—
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DYNAMIC CHARACTERISTICS (1)

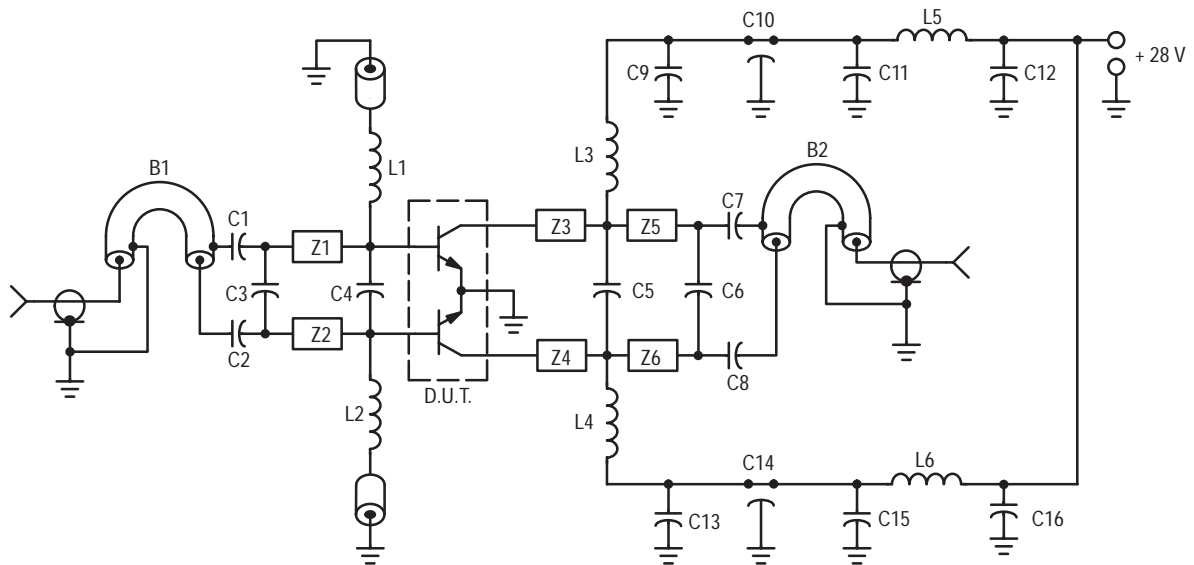
Output Capacitance ($V_{CB} = 28 \text{ Vdc}$, $I_E = 0$, $f = 1.0 \text{ MHz}$)	C_{ob}	40	75	95	pF
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FUNCTIONAL TESTS (2) — See Figure 1

Common–Emitter Amplifier Power Gain ($V_{CC} = 28 \text{ Vdc}$, $P_{out} = 100 \text{ W}$, $f = 500 \text{ MHz}$)	G_{pe}	7.5	8.5	—	dB
Collector Efficiency ($V_{CC} = 28 \text{ Vdc}$, $P_{out} = 100 \text{ W}$, $f = 500 \text{ MHz}$)	η	50	55	—	%
Load Mismatch ($V_{CC} = 28 \text{ Vdc}$, $P_{out} = 100 \text{ W}$, $f = 500 \text{ MHz}$, $VSWR = 30:1$, all phase angles)	ψ	No Degradation in Output Power			

NOTES:

- Each transistor chip measured separately.
- Both transistor chips operating in push–pull amplifier.



C1, C2, C7, C8 — 240 pF 100 mil Chip Cap
 C3 — 15 pF 100 mil Chip Cap
 C4 — 24 pF 100 mil Chip Cap
 C5 — 33 pF 100 mil Chip Cap
 C6 — 12 pF 100 mil Chip Cap
 C9, C13 — 1000 pF 100 mil Chip Cap
 C10, C14 — 680 pF Feedthru Cap
 C11, C15 — 0.1 μF Ceramic Disc Cap
 C12, C16 — 50 μF 50 V

L1, L2 — 0.15 μH Molded Choke with Ferrite Bead
 L3, L4 — 2–1/2 Turns #20 AWG 0.200" ID
 L5, L6 — 3–1/2 Turns #18 AWG 0.200" ID
 B1, B2 — Balun 50 Ω Semi Rigid Coax, 86 mil OD, 4" Long
 Z1, Z2 — 850 mil Long x 125 mil W. Microstrip
 Z3, Z4 — 200 mil Long x 125 mil W. Microstrip
 Z5, Z6 — 800 mil Long x 125 mil W. Microstrip
 Board Material — 0.0325" Teflon–Fiberglass, $\epsilon_r = 2.56$,
 1 oz. Copper Clad both sides.

Figure 1. 500 MHz Test Fixture

CLASS C

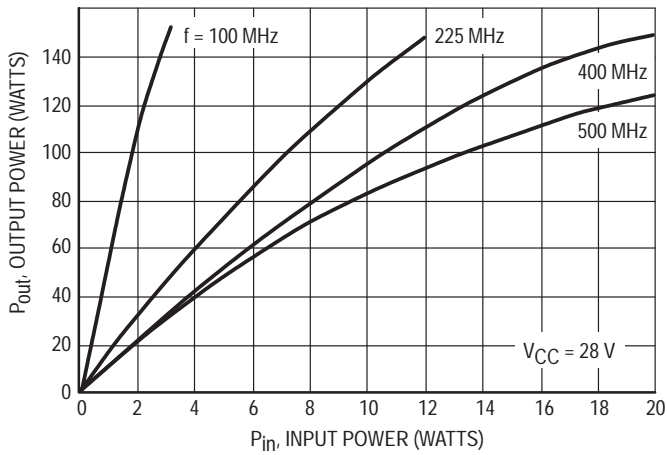


Figure 2. Output Power versus Input Power

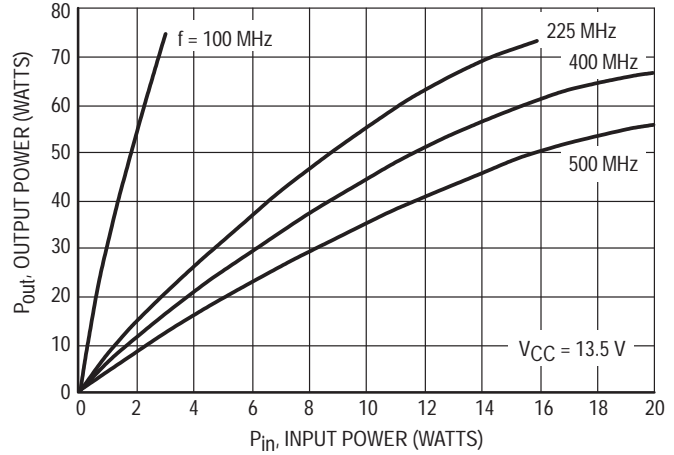


Figure 3. Output Power versus Input Power

CLASS C

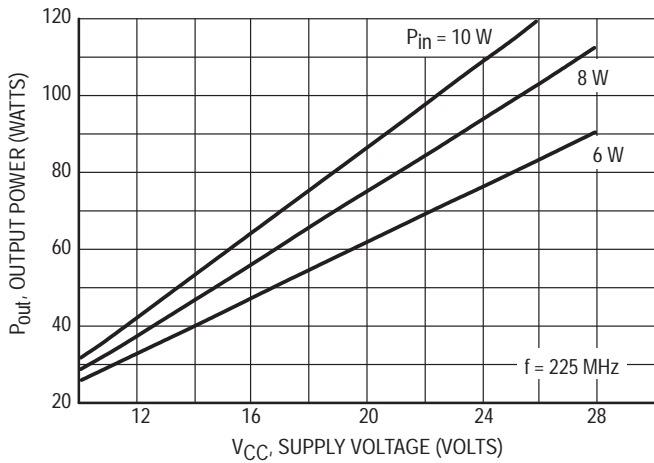


Figure 4. Output Power versus Supply Voltage

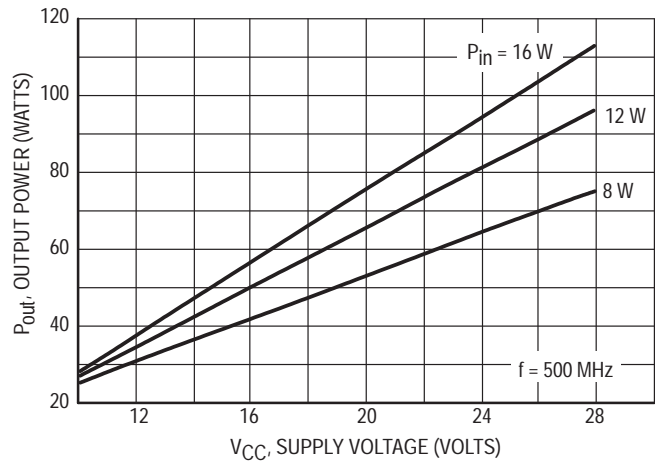
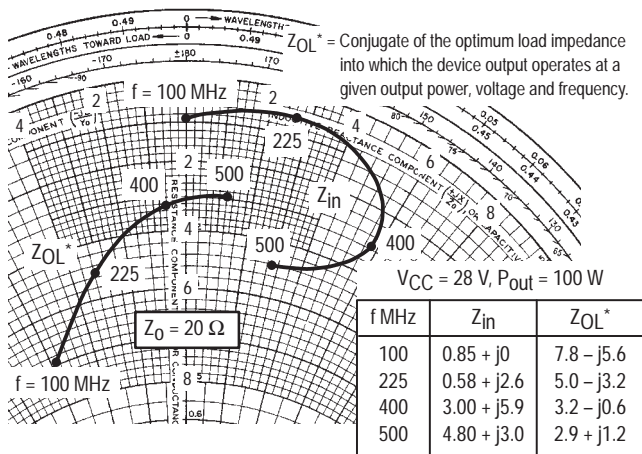


Figure 5. Output Power versus Supply Voltage



NOTE: Z_{in} & Z_{OL}* are given from base-to-base and collector-to-collector respectively.

Figure 6. Series Equivalent Input/Output Impedance

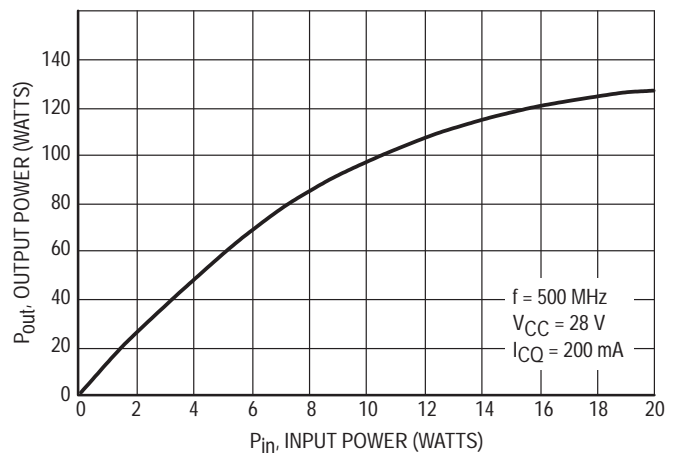
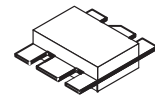


Figure 7. Class AB Output Power versus Input Power

The RF Line
NPN Silicon
RF Power Transistor

MRF858S

CLASS A
800–960 MHz
3.6 W (CW), 24 V
NPN SILICON
RF POWER TRANSISTOR



CASE 319A-02, STYLE 2

Designed for 24 Volt UHF large-signal, common emitter, class A linear amplifier applications in industrial and commercial equipment operating in the range of 800–960 MHz.

- Specified for $V_{CE} = 24$ Vdc, $I_C = 0.5$ Adc Characteristics
Output Power = 3.6 Watts CW
Minimum Power Gain = 11 dB
Minimum ITO = +44.5 dBm
Typical Noise Figure = 6 dB
- Characterized with Small-Signal S-Parameters and Series Equivalent Large-Signal Parameters from 800–960 MHz
- Silicon Nitride Passivated
- 100% Tested for Load Mismatch Stress at All Phase Angles with 30:1 VSWR @ 24 Vdc, $I_C = 0.5$ Adc and Rated Output Power
- Will Withstand RF Input Overdrive of 0.85 W CW
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CEO}	30	Vdc
Collector–Base Voltage	V_{CBO}	55	Vdc
Emitter–Base Voltage	V_{EBO}	4	Vdc
Total Device Dissipation @ $T_C = 50^\circ\text{C}$ Derate above 50°C	P_D	20 0.138	Watts W/ $^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance ($T_J = 150^\circ\text{C}$, $T_C = 50^\circ\text{C}$)	$R_{\theta JC}$	6.9	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector–Emitter Breakdown Voltage ($I_C = 20$ mA, $I_B = 0$)	$V_{(BR)CEO}$	28	35	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 20$ mA, $V_{BE} = 0$)	$V_{(BR)CES}$	55	85	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 20$ mA, $I_E = 0$)	$V_{(BR)CBO}$	55	85	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 1$ mA, $I_C = 0$)	$V_{(BR)EBO}$	4	5	—	Vdc
Collector Cutoff Current ($V_{CB} = 24$ V, $I_E = 0$)	I_{CES}	—	—	1	mA

ELECTRICAL CHARACTERISTICS — continued

Characteristic	Symbol	Min	Typ	Max	Unit
ON CHARACTERISTICS					
DC Current Gain ($I_C = 0.1\text{ A}$, $V_{CE} = 5\text{ V}$)	h_{FE}	30	60	120	—
DYNAMIC CHARACTERISTICS					
Output Capacitance ($V_{CB} = 24\text{ V}$, $f = 1\text{ MHz}$)	C_{ob}	—	6.5	8	pF
FUNCTIONAL CHARACTERISTICS					
Common-Emitter Power Gain ($V_{CE} = 24\text{ V}$, $I_C = 0.5\text{ A}$, $f = 840\text{--}900\text{ MHz}$, Power Output = 3.6 W)	P_g	11	12	—	dB
Load Mismatch ($P_O = 3.6\text{ W}$) ($V_{CE} = 24\text{ V}$, $I_C = 0.5\text{ A}$, $f = 840\text{ MHz}$, Load VSWR = 30:1, All Phase Angles)	ψ	No Degradation in Output Power			
RF Input Overdrive ($V_{CE} = 24\text{ V}$, $I_C = 0.5\text{ A}$, $f = 840\text{ MHz}$) No degradation	$P_{in(over)}$	—	—	0.85	W
Third Order Intercept Point ($V_{CE} = 24\text{ V}$, $I_C = 0.5\text{ A}$) ($f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$, Meas. @ IMD 3rd Order = -40 dBc)	ITO	+44.5	+45.5	—	dBm
Noise Figure ($V_{CE} = 24\text{ V}$, $I_C = 0.5\text{ A}$, $f = 900\text{ MHz}$)	NF	—	6	—	dB
Input Return Loss ($V_{CE} = 24\text{ V}$, $I_C = 0.5\text{ A}$, $f = 840\text{--}900\text{ MHz}$, Power Output = 3.6 W)	IRL	—	-12	-9	dB

Table 1. Common Emitter S-Parameters

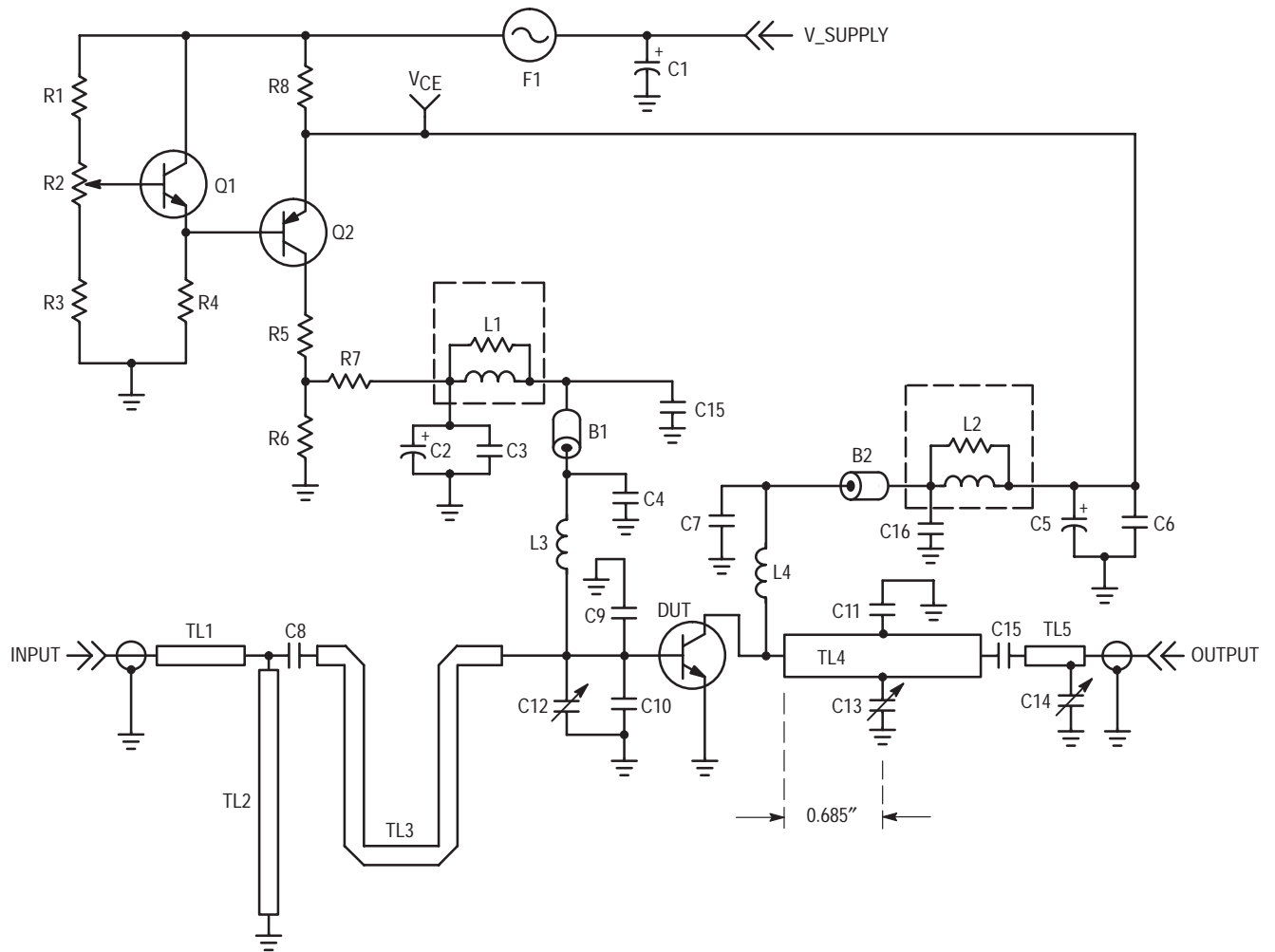
V_{CE} (V)	I_C (A)	f (MHz)	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
			S ₁₁	ϕ	S ₂₁	ϕ	S ₁₂	ϕ	S ₂₂	ϕ
24	0.5	800	0.942	167	1.493	50	0.027	58	0.538	-165
		820	0.942	166	1.453	50	0.027	58	0.541	-164
		840	0.941	166	1.415	49	0.028	59	0.545	-165
		860	0.940	166	1.379	48	0.028	59	0.550	-165
		880	0.941	165	1.351	47	0.029	59	0.553	-165
		900	0.940	165	1.320	46	0.030	59	0.557	-165
		920	0.940	165	1.289	45	0.030	59	0.562	-165
		940	0.940	164	1.252	44	0.031	59	0.566	-165
		960	0.940	164	1.222	43	0.031	59	0.570	-165

Table 2. Z_{in} and Z_{OL}* versus Frequency

f (MHz)	Z _{in} (Ohms)		Z _{OL} * (Ohms)	
840	1.1	2.9	9.9	-14.4
870	1.1	3.5	9.5	-14.6
900	1.2	3.5	9	-14.5

$V_{CE} = 24\text{ V}$, $I_C = 0.5\text{ A}$, $P_O = 3.6\text{ W}$

Z_{OL}* = Conjugate of optimum load impedance into which the device operates at a given output power, voltage and frequency.



B1, B2	Short Ferrite Bead, Fair Rite (2743021447)	R1	390 Ω, 1/4 W
C1	250 μF, 50 Vdc Electrolytic Capacitor	R2	500 Ω Potentiometer, 1/4 W
C2, C5	10 μF, 50 Vdc Electrolytic Capacitor	R3	7.5K Ω, 1/4 W
C3, C6	0.1 μF, Chip Capacitor	R4	2 x 4.7K Ω, 1/4 W
C4, C7	100 pF, Chip Capacitor	R5	56 Ω, 2 W
C8, C15	43 pF, 100 Mil Chip Capacitor	R6	75 Ω, 1/4 W
C9, C10	10 pF, Mini-Unelco	R7	4.7 Ω, 1/4 W
C11	5 pF, Mini-Unelco	R8	4 Ω, 10 W
C12, C13, C14	0.8–8.0 pF, Johanson Gigatrim	TL1, TL5	50 Ω, Microstrip Transmission Line
C15, C16	1000 pF, Chip Capacitor	TL2	Microstrip Transmission Line
F1	1 A Micro-Fuse	TL3	Microstrip Transmission Line
L1, L2	10 Turns, 20 AWG, 0.150" ID (10 Ω 1/2 W Resistor)	TL4	Microstrip Transmission Line
L3	4 Turns, 16 AWG, 0.101" ID	V_Supply	+26 Vdc ±0.5 Vdc Due to Resistor Tolerance
L4	0.5" 18 AWG Wire	VCE	+24 Vdc @ 0.5 A
Q1	MMBT2222ALT1, NPN Transistor	Board	0.030" Glass-Teflon® 2 oz. Cu, ε _r = 2.55
Q2	BD136, PNP Transistor		

Figure 1. MRF858S Class A RF Test Fixture Schematic

TYPICAL CHARACTERISTICS

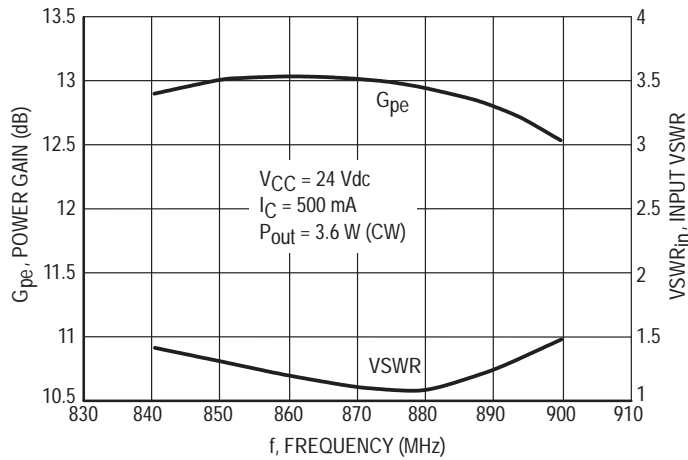


Figure 2. Performance in Broadband Circuit

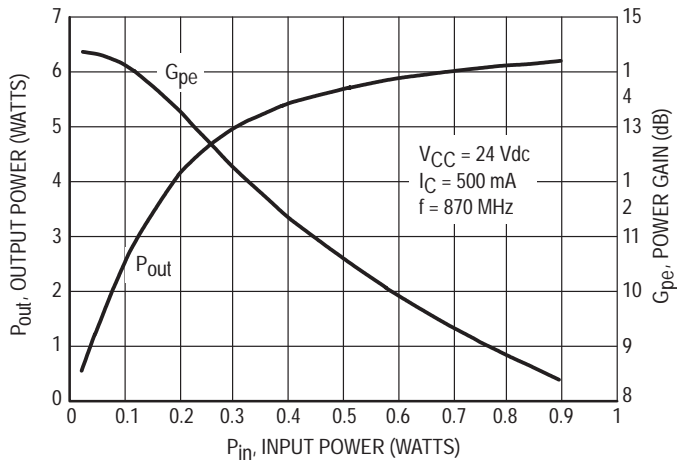


Figure 3. Output Power & Power Gain versus Input Power

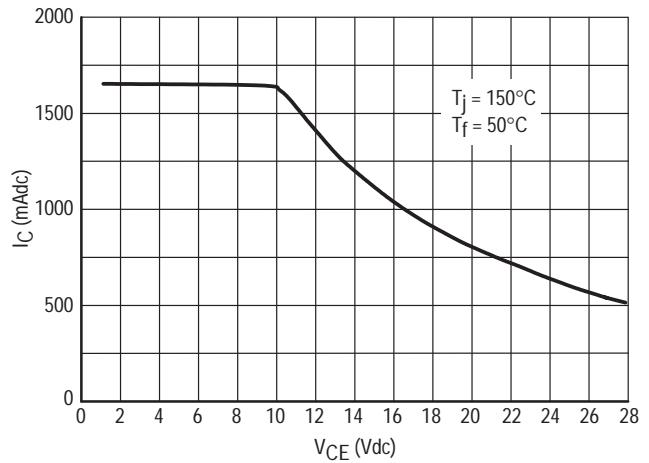


Figure 4. DC SOA

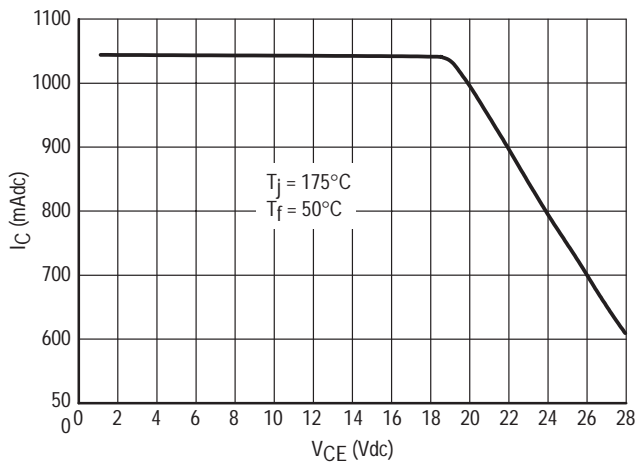


Figure 5. DC SOA
(This device is MTBF limited for $V_{CE} < 20$ Vdc.)

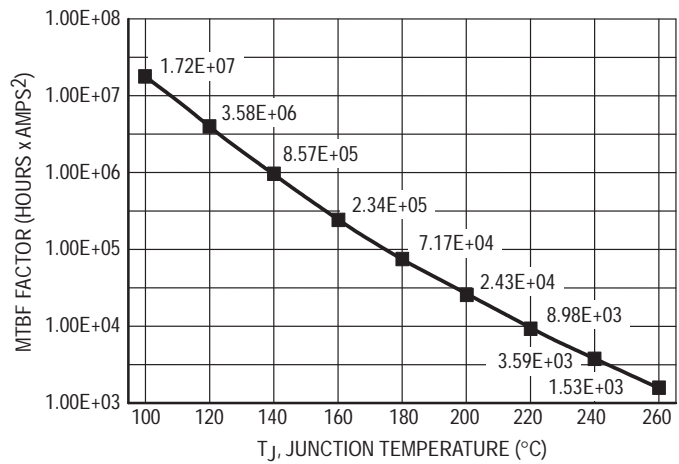


Figure 6. MTBF Factor versus Junction Temperature

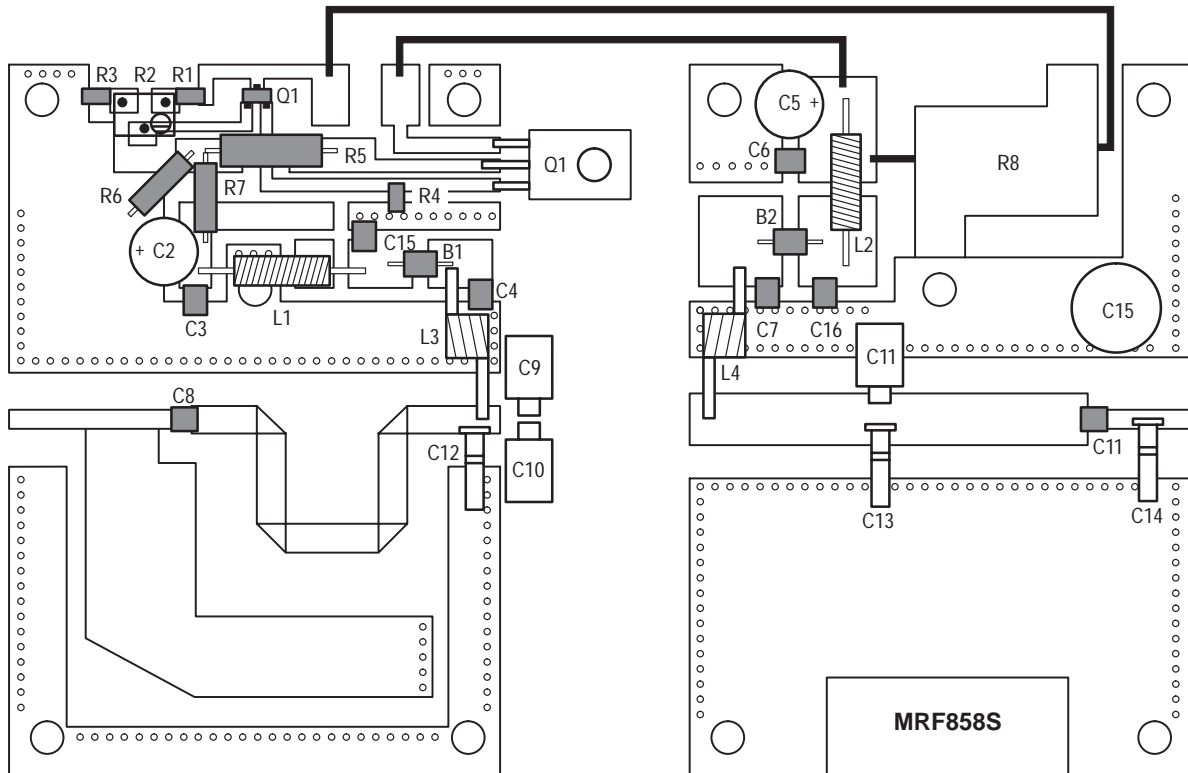


Figure 7. MRF858S Test Fixture Component Layout

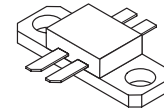
The RF Line
NPN Silicon
RF Power Transistor

Designed for 24 Volt UHF large-signal, common emitter, class-AB linear amplifier applications in industrial and commercial FM/AM equipment operating in the range 800–970 MHz.

- Specified 24 Volt, 900 MHz Characteristics
Output Power = 30 Watts
Minimum Gain = 10 dB @ 900 MHz, class-AB
Minimum Efficiency = 30% @ 900 MHz, 30 Watts (PEP)
Maximum Intermodulation Distortion –30 dBc @ 30 Watts (PEP)
- Characterized with Series Equivalent Large-Signal Parameters from 800 to 960 MHz
- Silicon Nitride Passivated
- 100% Tested for Load Mismatch Stress at all Phase Angles with 5:1 VSWR @ 26 Vdc, and Rated Output Power
- Gold Metalized, Emitter Ballasted for Long Life and Resistance to Metal-Migration
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MRF897

30 W, 900 MHz
RF POWER
TRANSISTOR
NPN SILICON



CASE 395B-01, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CEO}	30	Vdc
Collector-Emitter Voltage	V_{CES}	60	Vdc
Emitter-Base Voltage	V_{EBO}	4.0	Vdc
Collector-Current — Continuous	I_C	4.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	105 0.60	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.67	$^\circ\text{C/W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector-Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $I_B = 0$)	$V_{(BR)CEO}$	30	33	—	Vdc
Collector-Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	60	80	—	Vdc
Emitter-Base Breakdown Voltage ($I_E = 5 \text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	4.7	—	Vdc
Collector Cutoff Current ($V_{CE} = 30 \text{ Vdc}$, $V_{BE} = 0$)	I_{CES}	—	—	10.0	mAdc

ON CHARACTERISTICS

DC Current Gain ($I_{CE} = 1.0 \text{ Adc}$, $V_{CE} = 5 \text{ Vdc}$)	h_{FE}	30	80	120	—
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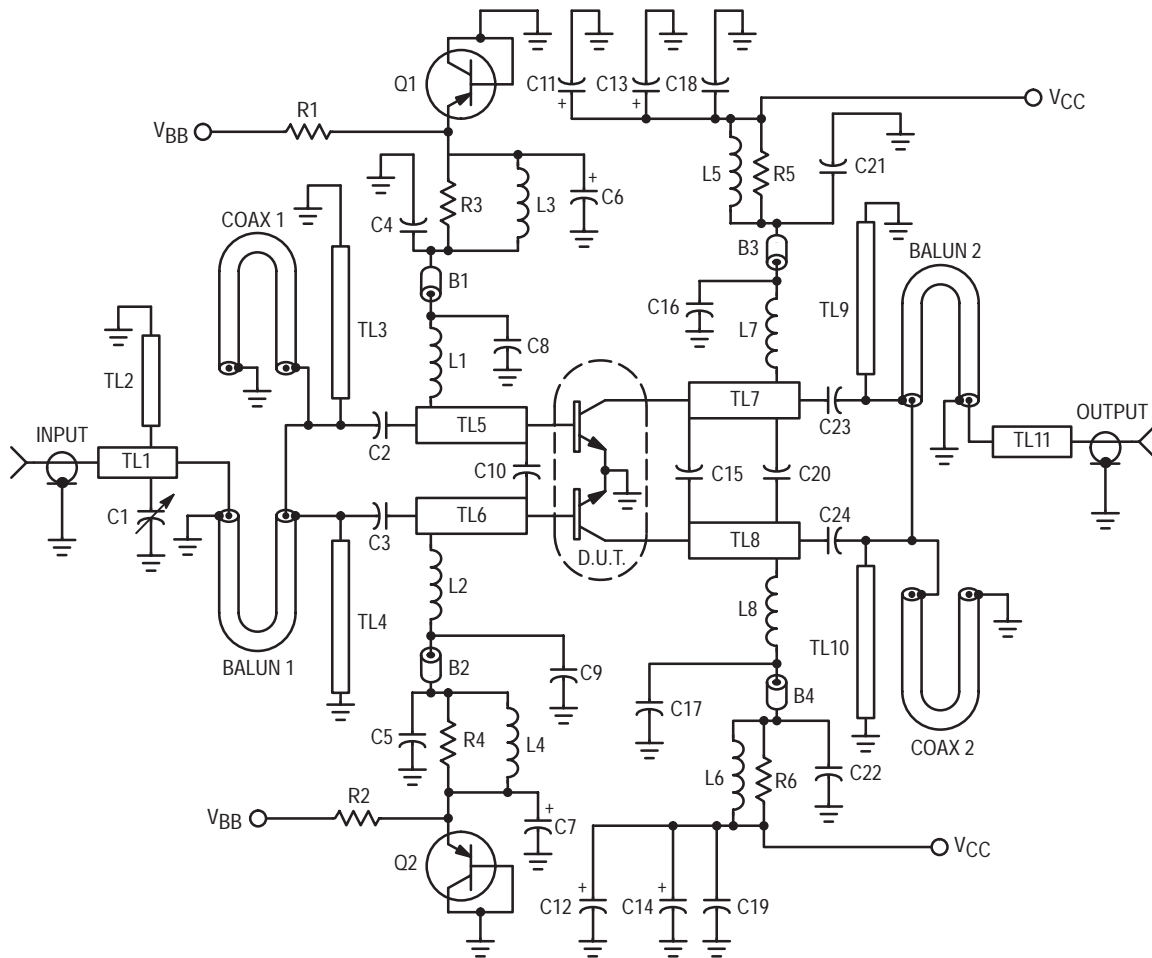
DYNAMIC CHARACTERISTICS

Output Capacitance ($V_{CB} = 24 \text{ Vdc}$, $I_E = 0$, $f = 1.0 \text{ MHz}$)	C_{ob}	14	21	28	pF
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(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL CHARACTERISTICS					
Common-Emitter Amplifier Power Gain ($V_{CC} = 24\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$)	G_{pe}	10.0	12.0	—	dB
Collector Efficiency ($V_{CC} = 24\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$)	η	35	38	—	%
Intermodulation Distortion ($V_{CC} = 24\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$)	IMD	—	-37	-30	dBc
Output Mismatch Stress ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$, Load VSWR = 5:1 (all phase angles))	ψ	No Degradation in Output Power Before and After Test			



- | | |
|---|--|
| B1, B2, B3, B4 — Ferrite Bead, Fair Rite #2743019447 | N1, N2 — Type N Flange Mount, Omni Spectra 3052-1648-10 |
| C1 — 0.8–8.0 pF Trimmer Capacitor, Johanson | Q1 — Bias Transistor BD136 PNP |
| C2, C3, C23, C24 — 43 pF, 100 mil, ATC Chip Capacitor | R1, R12 — 39 Ohm, 2.0 W |
| C4, C5, C18, C19, C21, C22 — 820 pF, 100 mil, Chip Capacitor, Kemet | R3, R4, R5, R6 — 4.0 x 39 Ohm, 1/8 W, Chips in Parallel, Rohm 390-J |
| C6, C7, C11, C12 — 10 μF , Lytic Capacitor, Panasonic | TL1–TL11 — See Photomaster |
| C8, C9, C16, C17 — 100 pF, 100 mil, Chip Capacitor, Murata Erie | Balun1, Balun2, Coax 1, Coax 2 — 2.20" 50 Ohm, 0.088" o.d. semi-rigid coax, Micro Coax UT-85-M17 |
| C10 — 13 pF, 50 mil, ATC Chip Capacitor | Board — 1/32" Glass Teflon, Arlon GX-0300-55-22, $\epsilon_r = 2.55$ |
| C13, C14 — 250 μF Lytic Capacitor, Mallory | |
| C15 — 1.1 pF, 50 mil, ATC Chip Capacitor | |
| C20 — 6.8 pF, 100 mil, ATC Chip Capacitor | |
| L1, L2, L3, L4, L5, L6 — 5 Turns 20 AWG, IDIA 0.126" choke | |

Figure 1. MRF897 Broadband Test Circuit

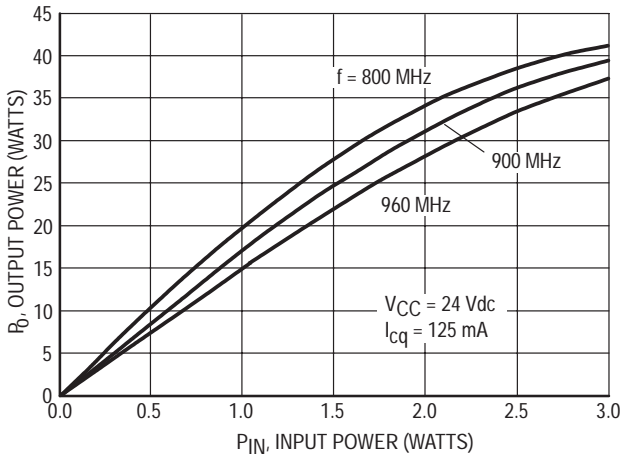


Figure 2. Output Power versus Input Power

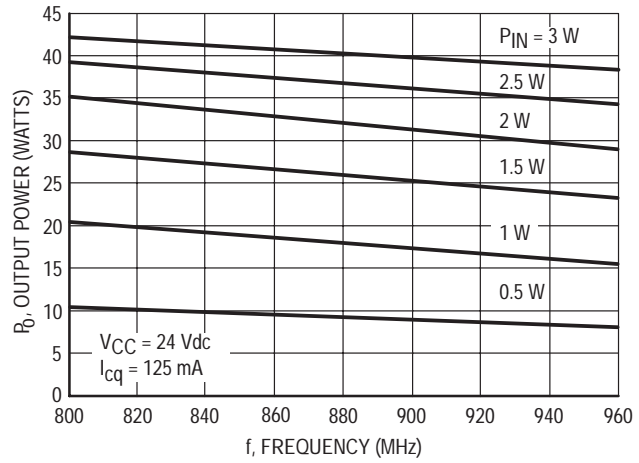


Figure 3. Output Power versus Frequency

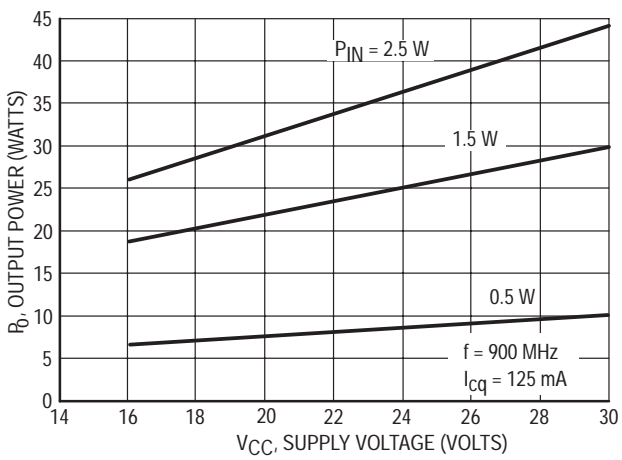


Figure 4. Output Power versus Supply Voltage

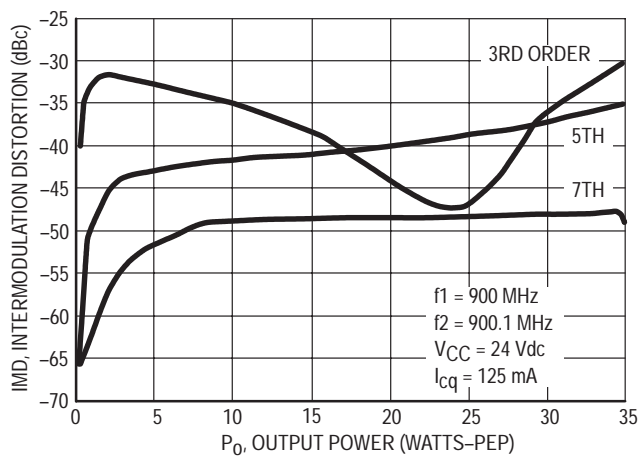


Figure 5. Intermodulation versus Output Power

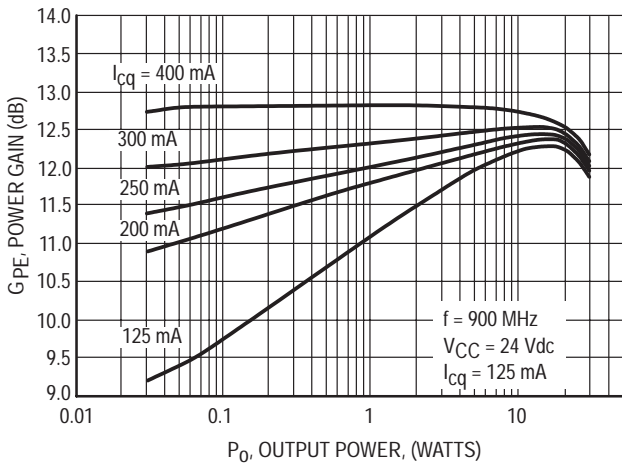


Figure 6. Power Gain versus Output Power

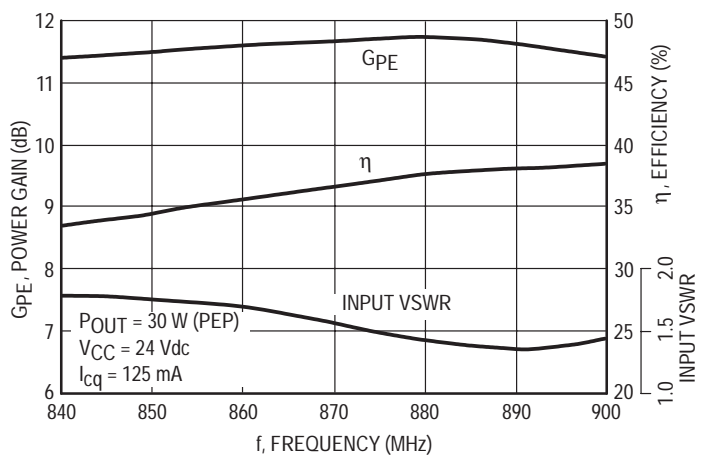
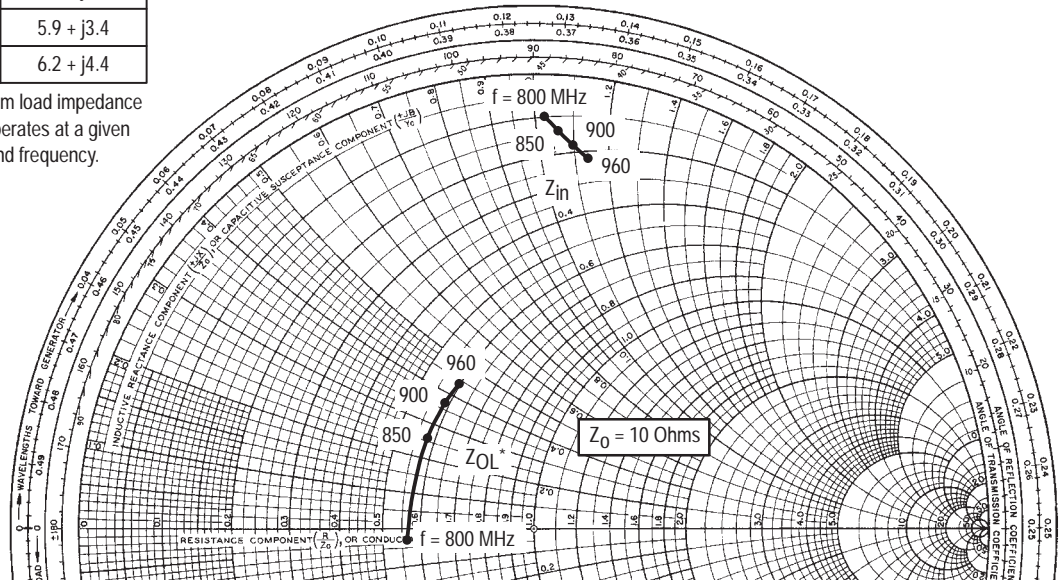


Figure 7. Broadband Test Fixture Performance

f MHz	Z _{in} Ohms	Z _{OL} [*] Ohms
800	1.0 + j10.3	5.9 - j0.4
850	1.5 + j10.5	5.7 + j2.6
900	1.8 + j11.0	5.9 + j3.4
960	2.2 + j11.4	6.2 + j4.4

Z_{OL}^{*} = Conjugate of the optimum load impedance into which the device operates at a given output power, voltage and frequency.



NOTE: Z_{in} & Z_{OL}^{*} are given from base-to-base and collector-to-collector respectively.

P₀ = 300 W (PEP), V_{CC} = 24 V

Figure 8. Series Equivalent Input/Output Impedances

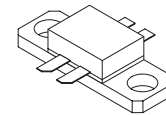
The RF Line
NPN Silicon
RF Power Transistor

Designed for 24 Volt UHF large-signal, common emitter, class-AB linear amplifier applications in industrial and commercial FM/AM equipment operating in the range 800–970 MHz.

- Specified 24 Volt, 900 MHz Characteristics
Output Power = 30 Watts
Minimum Gain = 10.5 dB @ 900 MHz, class-AB
Minimum Efficiency = 30% @ 900 MHz, 30 Watts (PEP)
Maximum Intermodulation Distortion –30 dBc @ 30 Watts (PEP)
- Characterized with Series Equivalent Large-Signal Parameters from 800 to 960 MHz
- Silicon Nitride Passivated
- 100% Tested for Load Mismatch Stress at all Phase Angles with 5:1 VSWR @ 26 Vdc, and Rated Output Power
- Gold Metalized, Emitter Ballasted for Long Life and Resistance to Metal-Migration

MRF897R

30 W, 900 MHz
RF POWER
TRANSISTOR
NPN SILICON



CASE 395E-01, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CEO}	30	Vdc
Collector-Emitter Voltage	V_{CES}	60	Vdc
Emitter-Base Voltage	V_{EBO}	4.0	Vdc
Collector-Current — Continuous	I_C	4.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	105 0.60	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.67	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector-Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $I_B = 0$)	$V_{(BR)CEO}$	30	33	—	Vdc
Collector-Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	60	80	—	Vdc
Emitter-Base Breakdown Voltage ($I_E = 5 \text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	4.7	—	Vdc
Collector Cutoff Current ($V_{CE} = 30 \text{ Vdc}$, $V_{BE} = 0$, $T_C = 25^\circ\text{C}$)	I_{CES}	—	—	10.0	mAdc

ON CHARACTERISTICS

DC Current Gain ($I_{CE} = 1.0 \text{ Adc}$, $V_{CE} = 5 \text{ Vdc}$)	h_{FE}	30	80	120	—
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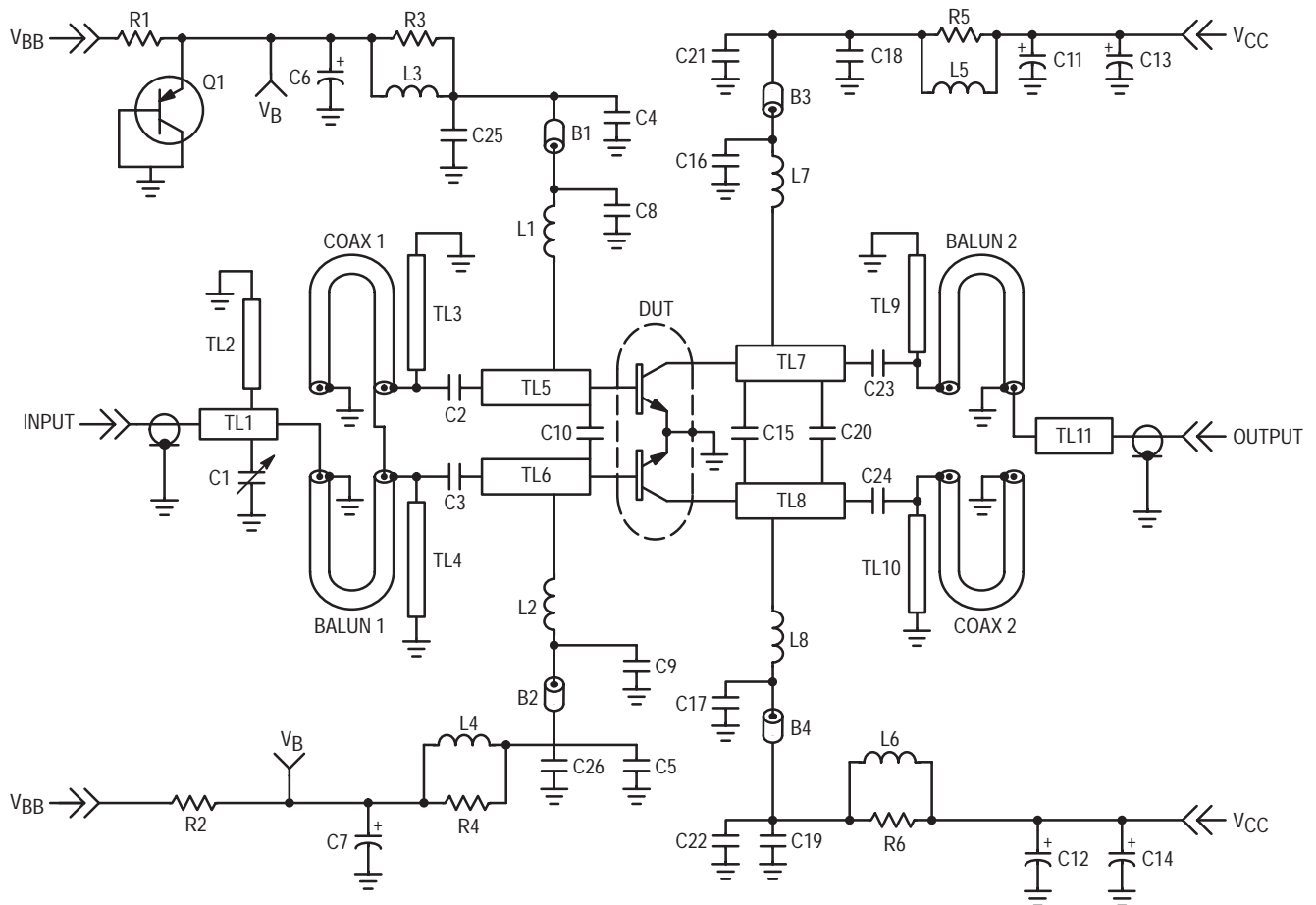
DYNAMIC CHARACTERISTICS

Output Capacitance ($V_{CB} = 24 \text{ Vdc}$, $I_E = 0$, $f = 1.0 \text{ MHz}$)	C_{ob}	14	21	28	pF
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(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL CHARACTERISTICS					
Common-Emitter Amplifier Power Gain ($V_{CC} = 24\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$)	G_{pe}	10.5	12.0	—	dB
Collector Efficiency ($V_{CC} = 24\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$)	η	30	38	—	%
Intermodulation Distortion ($V_{CC} = 24\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$)	IMD	—	-37	-30	dBc
Output Mismatch Stress ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 900\text{ MHz}$, $f_2 = 900.1\text{ MHz}$, Load VSWR = 5:1 (all phase angles))	ψ	No Degradation in Output Power			



B1, B2, B3, B4 — Short Ferrite Bead, Fair Rite #2743019447
 C1 — 0.8–8.0 pF Var Capacitor, Johansen Gigatrim
 C2, C3, C23, C24 — 43 pF, 100 mil, ATC Chip Capacitor
 C4, C5, C21, C22 — 1000 pF, 100 mil, ATC Chip Capacitor
 C6, C7, C11, C12 — 10 μF , Electrolytic Capacitor, Panasonic
 C8, C9, C16, C17 — 100 pF, 100 mil, ATC Chip Capacitor
 C10 — 9.1 pF, 50 mil, ATC Chip Capacitor
 C13 — 250 μF Electrolytic Capacitor, Mallory
 C14, C18, C19, C25 — 0.1 μF , Chip Capacitor, Kemet
 C15 — 1.1 pF, 50 mil, ATC Chip Capacitor
 C20 — 6.8 pF, 100 mil, ATC Chip Capacitor
 L1, L2, L3, L4, L5, L6, L7, L8 — 5 Turns 20 AWG,
 IDIA 0.126" Choke, Taylor Spring 46 nH

N1, N2 — Type N Flange Mount, Omni Spectra 3052–1648–10
 Q1 — Bias Transistor BD136 PNP
 R1, R12 — 27 Ohm, 2.0 W
 R3, R4, R5, R6 — 4.0 x 39 Ohm, 1/8 W, Chips Resistors in
 Parallel, Rohm 390–J
 SB1 — 0.15" x 0.3" x 0.03" Cu
 TL1–TL11 — Microstrip Line, See Photomaster
 Balun1, Balun2, Coax 1, Coax 2 — 2.20" 50 Ohm, 0.086" o.d.
 semi-rigid coax, Micro Coax
 UT–85–M17
 Circuit Board — 1/32" Glass Teflon, Arlon GX–0300–55–22,
 $\epsilon_r = 2.55$

Figure 1. 840–900 MHz Test Circuit Schematic

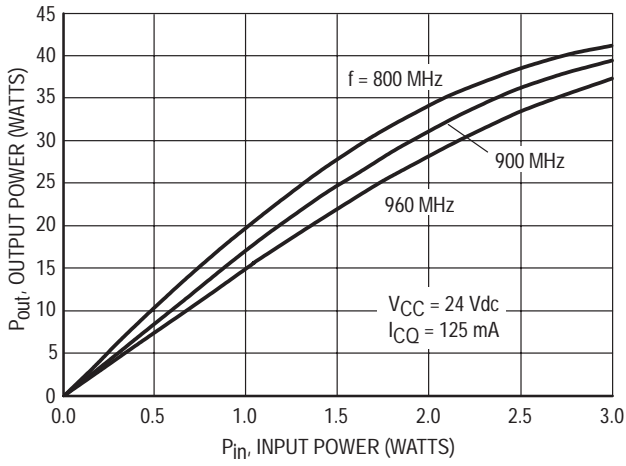


Figure 2. Output Power versus Input Power

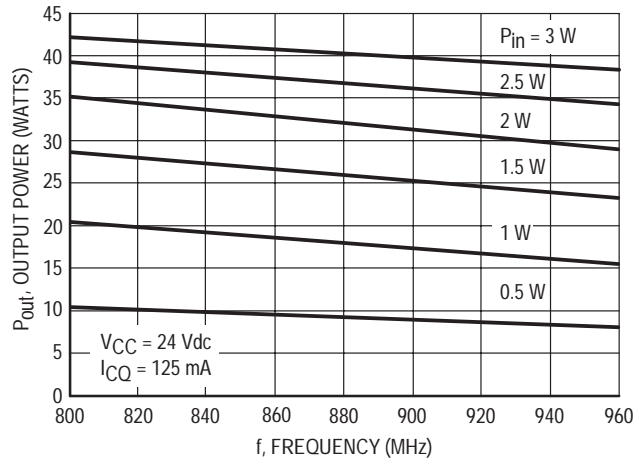


Figure 3. Output Power versus Frequency

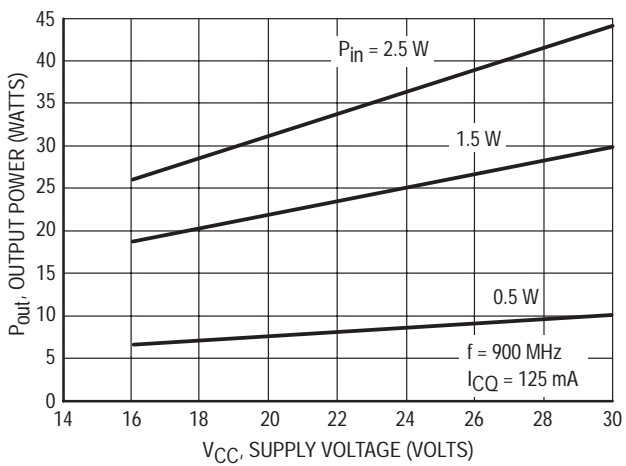


Figure 4. Output Power versus Supply Voltage

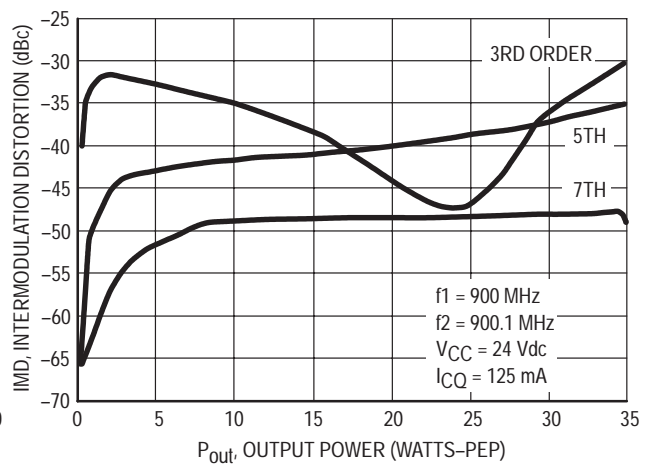


Figure 5. Intermodulation versus Output Power

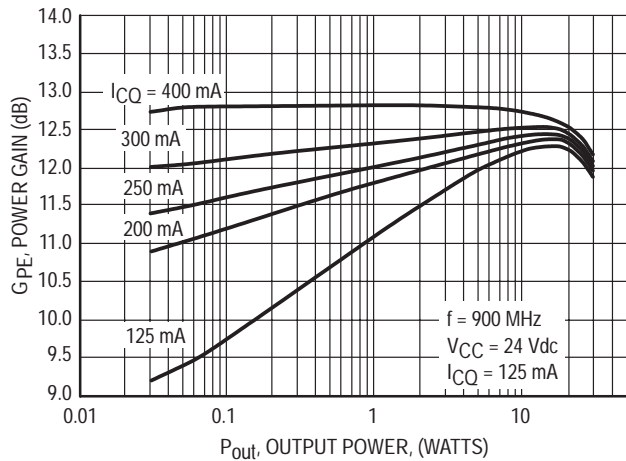


Figure 6. Power Gain versus Output Power

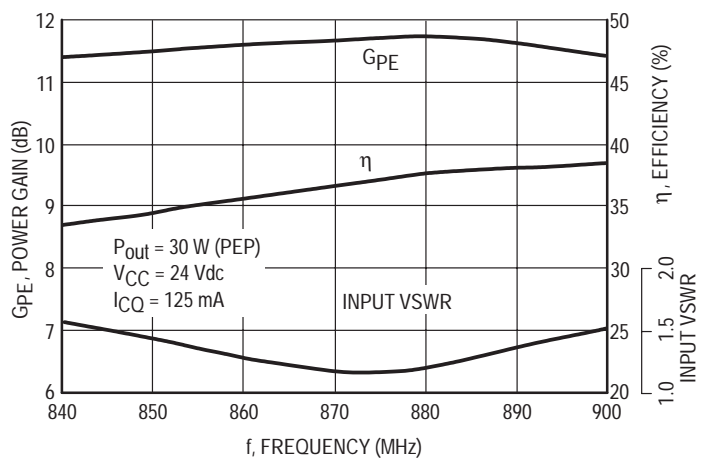
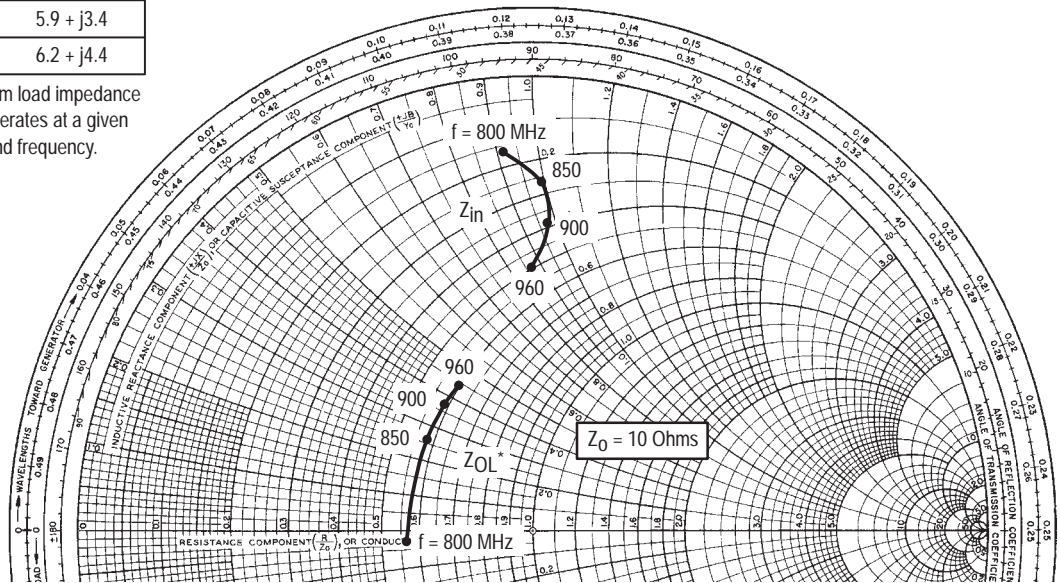


Figure 7. Broadband Test Fixture Performance

$P_{out} = 30 \text{ W (PEP)}, V_{CC} = 24 \text{ V}$

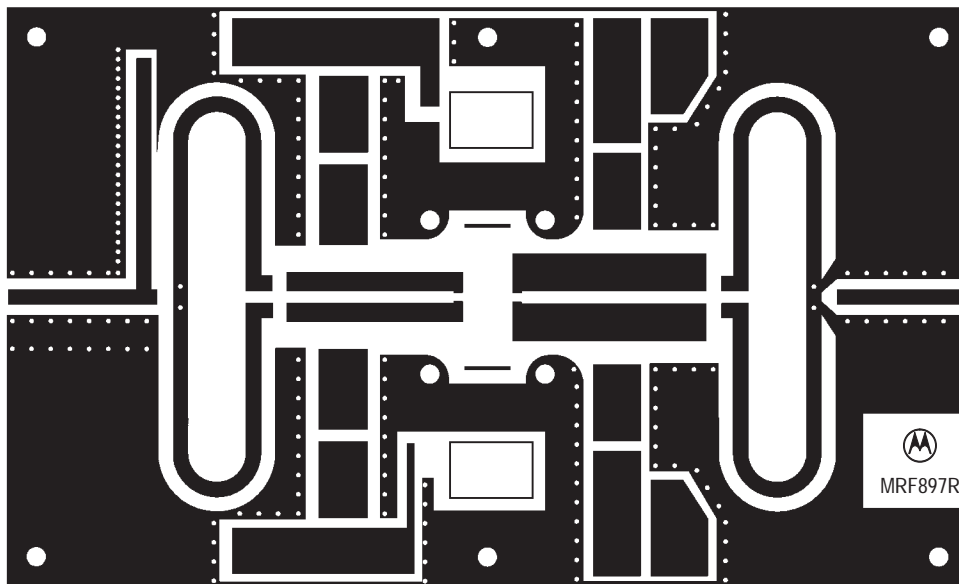
f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
800	$1.7 + j9.2$	$5.9 - j0.4$
850	$2.6 + j10$	$5.7 + j2.6$
900	$4 + j9.9$	$5.9 + j3.4$
950	$5 + j8.8$	$6.2 + j4.4$

Z_{OL}^* = Conjugate of the optimum load impedance into which the device operates at a given output power, voltage and frequency.



NOTE: Z_{in} & Z_{OL}^* are given from base-to-base and collector-to-collector respectively.

Figure 8. Series Equivalent Input/Output Impedances



(SCALE: 1:1)

Figure 9. MRF897R Photomaster
(Reduced 18% in printed data book, DL110/D)

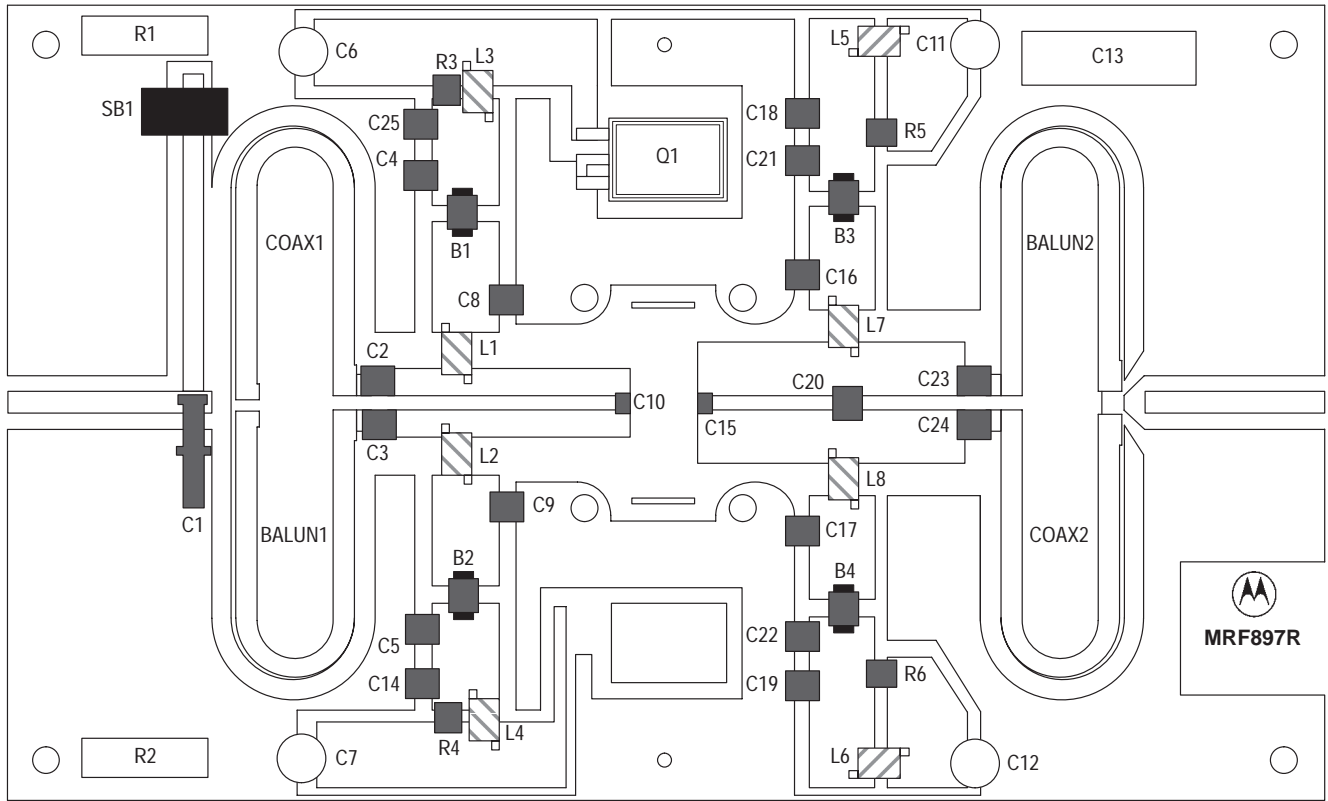


Figure 10. 840–900 MHz Test Circuit Component Layout

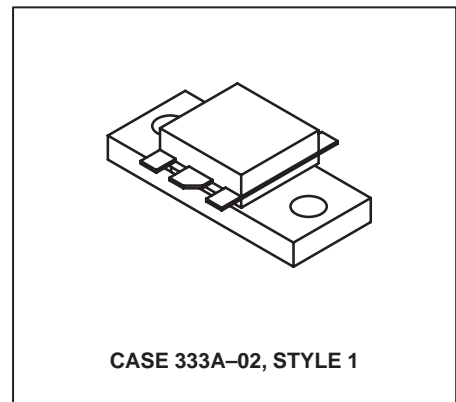
The RF Line
NPN Silicon
RF Power Transistor

... designed for 24 Volt UHF large-signal, common base amplifier applications in industrial and commercial FM equipment operating in the range of 850–960 MHz.

- Motorola Advanced Amplifier Concept Package
- Specified 24 Volt, 900 MHz Characteristics
Output Power = 60 Watts
Power Gain = 7.0 dB Min
Efficiency = 60% Min
- Double Input/Output Matched for Wideband Performance and Simplified External Matching
- Series Equivalent Large-Signal Characterization
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Silicon Nitride Passivated
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MRF898

60 W, 850–960 MHz
RF POWER
TRANSISTOR
NPN SILICON



MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CEO}	30	Vdc
Collector–Base Voltage	V_{CBO}	55	Vdc
Emitter–Base Voltage	V_{EBO}	4.0	Vdc
Collector Current — Continuous	I_C	10	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	175 1.0	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.0	$^\circ\text{C/W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
Collector–Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $I_B = 0$)	$V_{(BR)CEO}$	30	—	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 50 \text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	55	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 5.0 \text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	—	—	Vdc
Collector Cutoff Current ($V_{CE} = 30 \text{ Vdc}$, $V_{BE} = 0$, $T_C = 25^\circ\text{C}$)	I_{CES}	—	—	10	mAdc

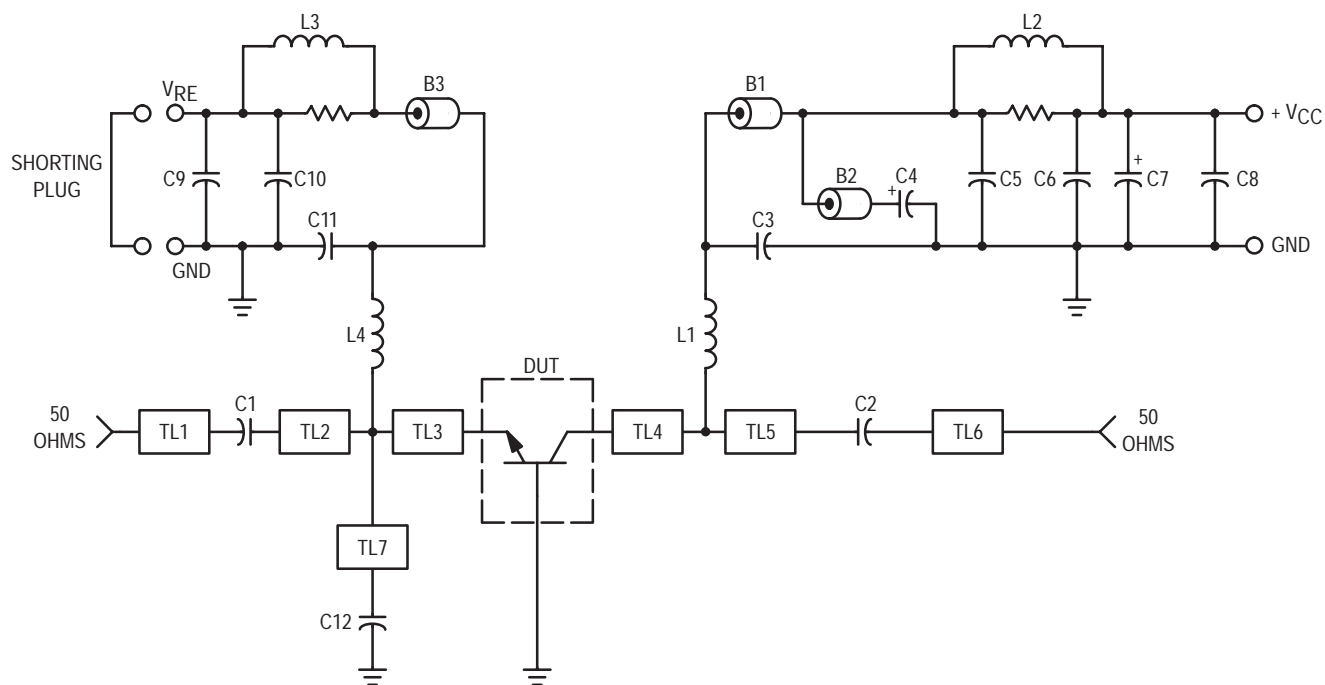
(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
ON CHARACTERISTICS					
DC Current Gain ($I_C = 2.0 \text{ Adc}$, $V_{CE} = 5.0 \text{ Vdc}$)	h_{FE}	20	50	150	—
DYNAMIC CHARACTERISTICS					
Output Capacitance (1) ($V_{CB} = 24 \text{ Vdc}$, $I_E = 0$, $f = 1.0 \text{ MHz}$)	C_{ob}	—	60	—	pF
FUNCTIONAL TESTS					
Common-Base Amplifier Power Gain ($V_{CC} = 24 \text{ Vdc}$, $P_{out} = 60 \text{ W}$, $f = 900 \text{ MHz}$)	G_{pb}	7.0	7.9	—	dB
Collector Efficiency ($V_{CC} = 24 \text{ Vdc}$, $P_{out} = 60 \text{ W}$, $f = 900 \text{ MHz}$)	η	60	65	—	%
Output Mismatch Stress ($V_{CC} = 24 \text{ Vdc}$, $P_{out} = 60 \text{ W}$, $f = 900 \text{ MHz}$, $VSWR = 5:1$, all phase angles)	ψ	No Degradation in Output Power			

NOTE:

1. Value of " C_{ob} " is that of die only. It is not measurable in MRF898 because of internal matching network.



B1, B2, B3 — Bead, Ferroxcube 56-390-65/3B
 C1, C2, C12 — 39 pF, 100 Mil Chip Capacitor
 C3, C11 — 91 pF, Mini Underwood or Equivalent
 C4, C7, C9 — 10 μF , 35 V Electrolytic
 C5 — 4000 pF, 1.0 kV Ceramic
 C6, C10 — 1000 pF, 350 V Unelco or Equivalent
 C8 — 47 pF, 100 Mil Chip Capacitor
 L1, L4 — 4 Turns #18 AWG Choke
 L2 — 11 Turns #20 AWG Choke on 10 Ohm, 1.0 Watt Resistor
 L3 — 3 Turns #18 AWG Choke on 10 Ohm, 1.0 Watt Resistor

TL1, TL6 — 50 Ohm Microstrip
 TL2 — 400 x 950 Mils
 TL3, TL4 — 140 x 200 Mils
 TL5 — 320 x 690 Mils
 TL7 — 260 x 230 Mils
 Board — 3M Epsilam-10, 50 Mil
 Bias Boards — 1/32" G10 or Equivalent

Figure 1. 850-960 MHz Broadband Test Circuit

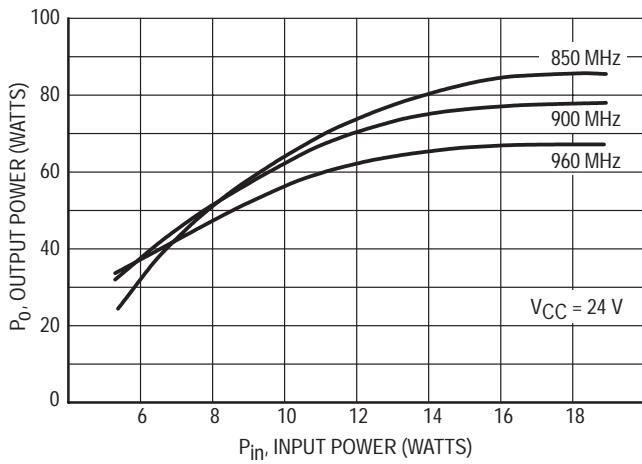


Figure 2. Output Power versus Input Power

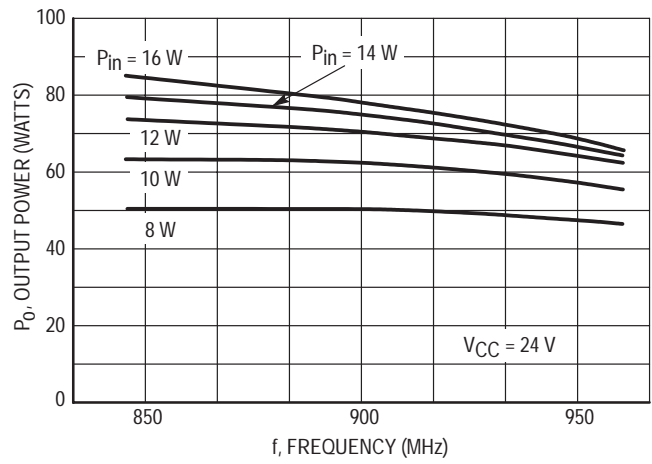


Figure 3. Output Power versus Frequency

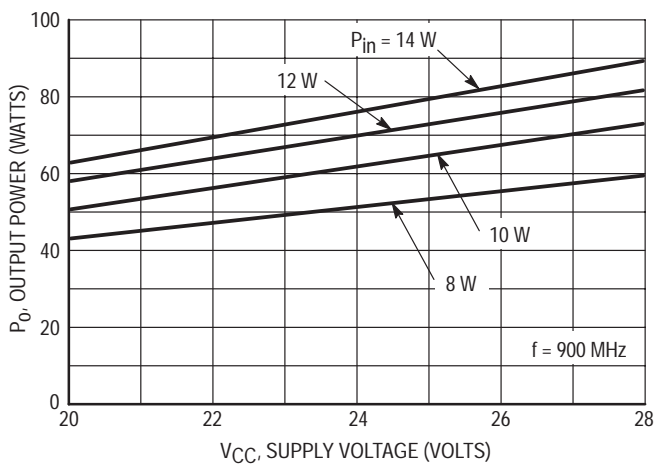


Figure 4. Output Power versus Supply Voltage

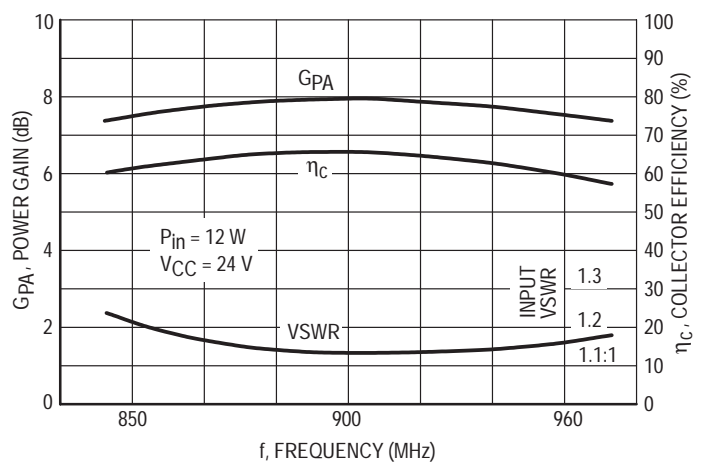


Figure 5. Typical Broadband Circuit Performance

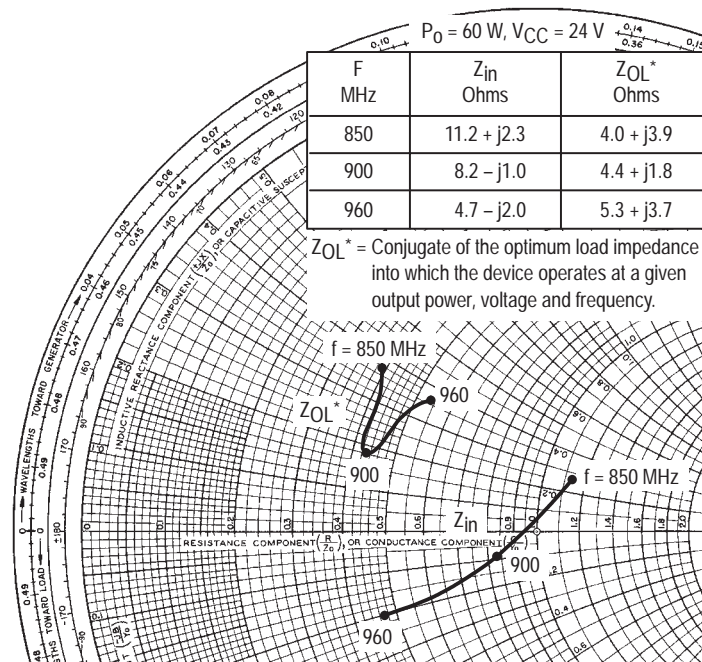


Figure 6. Input/Output Impedance versus Frequency

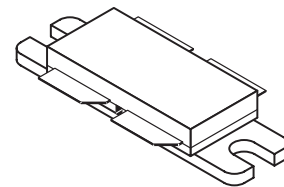
The RF Line
NPN Silicon
RF Power Transistor

Designed for 26 Volt UHF large-signal, common emitter, Class AB linear amplifier applications in industrial and commercial FM/AM equipment operating in the range 800–960 MHz.

- Specified 26 Volt, 900 MHz Characteristics
Output Power = 150 Watts (PEP)
Minimum Gain = 8.0 dB @ 900 MHz, Class AB
Minimum Efficiency = 35% @ 900 MHz, 150 Watts (PEP)
Maximum Intermodulation Distortion –28 dBc @ 150 Watts (PEP)
- Characterized with Series Equivalent Large-Signal Parameters from 800 to 960 MHz
- Silicon Nitride Passivated
- 100% Tested for Load Mismatch Stress at all Phase Angles with 5:1 VSWR @ 26 Vdc, and Rated Output Power
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MRF899

150 W, 900 MHz
RF POWER
TRANSISTOR
NPN SILICON



CASE 375A-01, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CEO}	28	Vdc
Collector–Emitter Voltage	V_{CES}	60	Vdc
Emitter–Base Voltage	V_{EBO}	4.0	Vdc
Collector–Current — Continuous	I_C	25	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	230 1.33	Watts W/°C
Storage Temperature Range	T_{stg}	–65 to +150	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.75	°C/W

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector–Emitter Breakdown Voltage ($I_C = 100\text{ mA}$, $I_B = 0$)	$V_{(BR)CEO}$	28	37	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 50\text{ mA}$, $V_{BE} = 0$)	$V_{(BR)CES}$	60	85	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 10\text{ mA}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	4.9	—	Vdc
Collector Cutoff Current ($V_{CE} = 30\text{ Vdc}$, $V_{BE} = 0$)	I_{CES}	—	—	10	mAdc

ON CHARACTERISTICS

DC Current Gain ($I_{CE} = 1.0\text{ Adc}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	30	75	120	—
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DYNAMIC CHARACTERISTICS

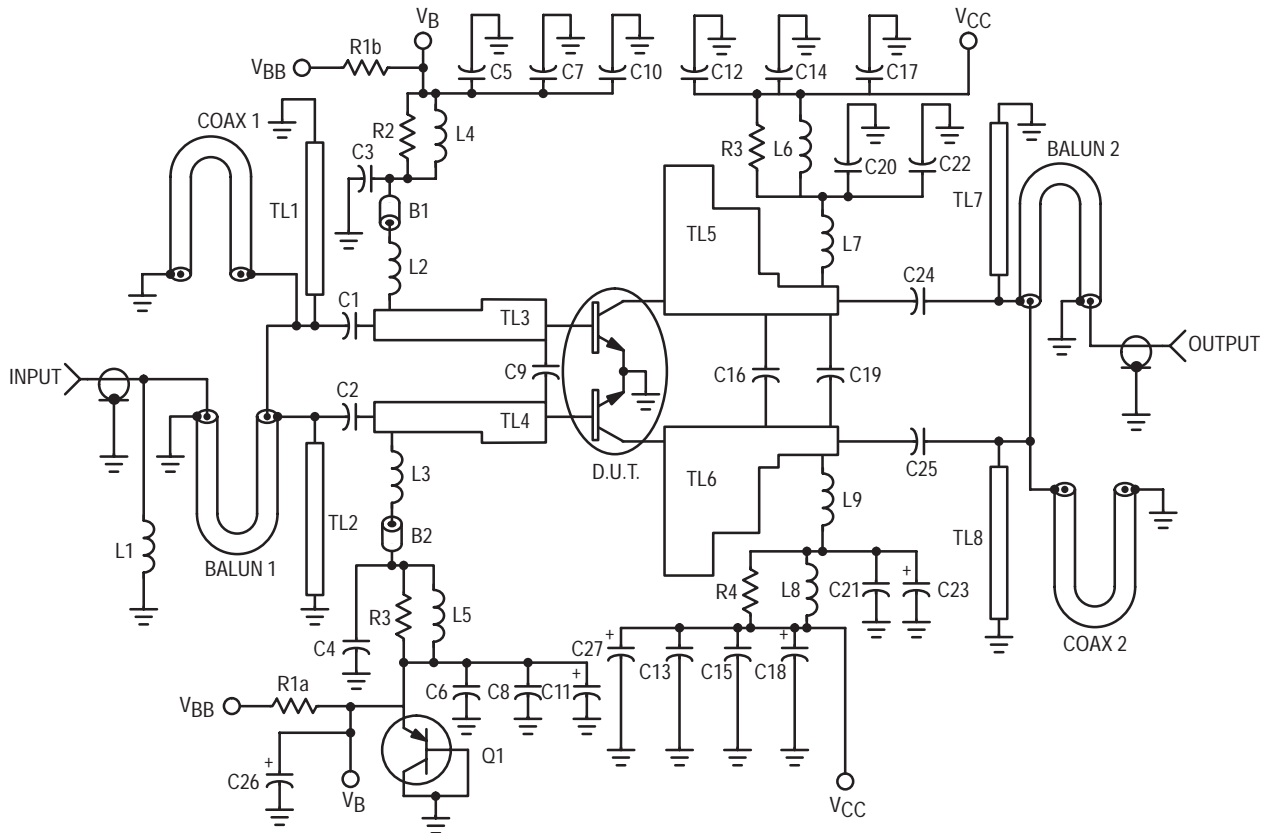
Output Capacitance ($V_{CB} = 26\text{ Vdc}$, $I_E = 0$, $f = 1.0\text{ MHz}$) (1)	C_{ob}	—	75	—	pF
--	----------	---	----	---	----

(1) For information only. This part is collector matched.

(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL CHARACTERISTICS					
Common-Emitter Amplifier Power Gain $V_{CC} = 26 \text{ Vdc}$, $P_{\text{out}} = 150 \text{ Watts (PEP)}$, $I_{CQ} = 300 \text{ mA}$, $f_1 = 900 \text{ MHz}$, $f_2 = 900.1 \text{ MHz}$	G_{pe}	8.0	9.0	—	dB
Collector Efficiency $V_{CC} = 26 \text{ Vdc}$, $P_{\text{out}} = 150 \text{ Watts (PEP)}$, $I_{CQ} = 300 \text{ mA}$, $f_1 = 900 \text{ MHz}$, $f_2 = 900.1 \text{ MHz}$	η	30	40	—	%
3rd Order Intermodulation Distortion $V_{CC} = 26 \text{ Vdc}$, $P_{\text{out}} = 150 \text{ Watts (PEP)}$, $I_{CQ} = 300 \text{ mA}$, $f_1 = 900 \text{ MHz}$, $f_2 = 900.1 \text{ MHz}$	IMD	—	-32	-28	dBc
Output Mismatch Stress $V_{CC} = 26 \text{ Vdc}$, $P_{\text{out}} = 150 \text{ Watts (PEP)}$, $I_{CQ} = 300 \text{ mA}$, $f_1 = 900 \text{ MHz}$, $f_2 = 900.1 \text{ MHz}$, VSWR = 5:1 (all phase angles)	ψ	No Degradation in Output Power Before and After Test			



- B1, B2 — Ferrite Bead, Ferroxcube #56-590-65-3B
- C1, C2, C24, C25 — 43 pF, B Case, ATC Chip Capacitor
- C3, C4, C20, C21 — 100 pF, B Case, ATC Chip Capacitor
- C5, C6, C12, C13 — 1000 pF, B Case, ATC Chip Capacitor
- C7, C8, C14, C15 — 1800 pF, AVX Chip Capacitor
- C9 — 9.1 pF, A Case, ATC Chip Capacitor
- C10, C11, C17, C18, C22, C23 — 10 μF , Electrolytic Capacitor
Panasonic
- C16 — 3.9 pF, B Case, ATC Chip Capacitor
- C19 — 0.8 pF, B Case, ATC Chip Capacitor
- C26 — 200 μF , Electrolytic Capacitor Mallory Sprague
- C27 — 500 μF Electrolytic Capacitor

- L1 — 5 Turns 24 AWG IDIA 0.059" Choke, 19.8 nH
- L2, L3, L7, L9 — 4 Turns 20 AWG IDIA 0.163" Choke
- L4, L5, L6, L8 — 12 Turns 22 AWG IDIA 0.140" Choke
- N1, N2 — Type N Flange Mount, Omni Spectra
- Q1 — Bias Transistor BD136 PNP
- R2, R3, R4, R5 — 4.0 x 39 Ohm 1/8 W Chips in Parallel
- R1a, R1b — 56 Ohm 1.0 W
- TL1 — TL8 — See Photomaster
- Balun1, Balun2, Coax 1, Coax 2 — 2.20" 50 Ohm 0.088" o.d.
Semi-rigid Coax, Micro Coax
- Board — 1/32" Glass Teflon, $\epsilon_r = 2.55$ " Arlon (GX-0300-55-22)

Figure 1. 900 MHz Power Gain Test Circuit

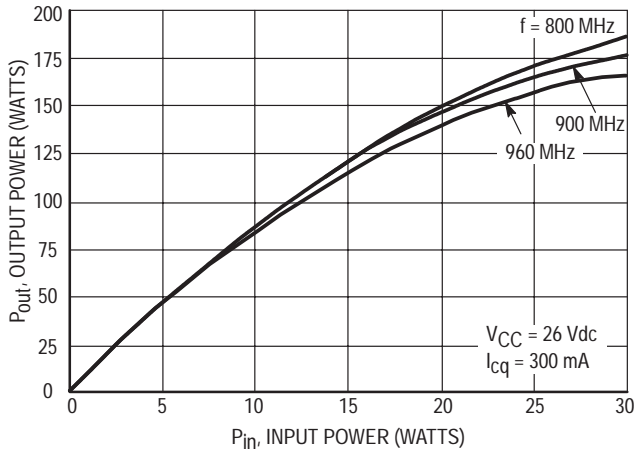


Figure 2. Output Power versus Input Power

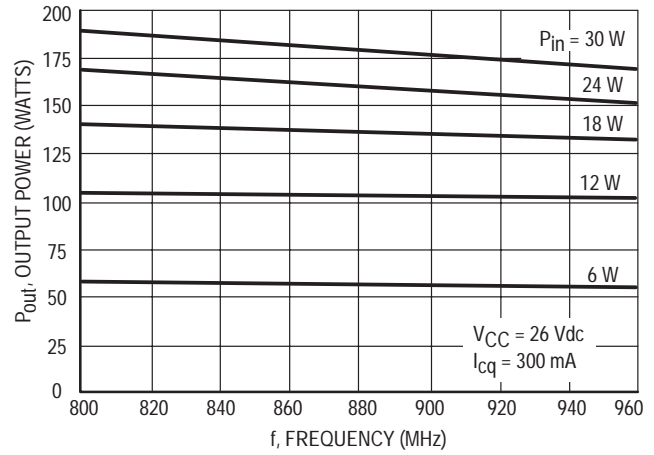


Figure 3. Output Power versus Frequency

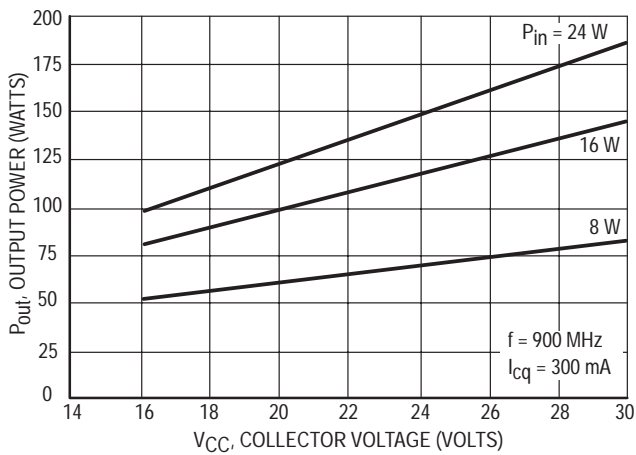


Figure 4. Output Power versus Supply Voltage

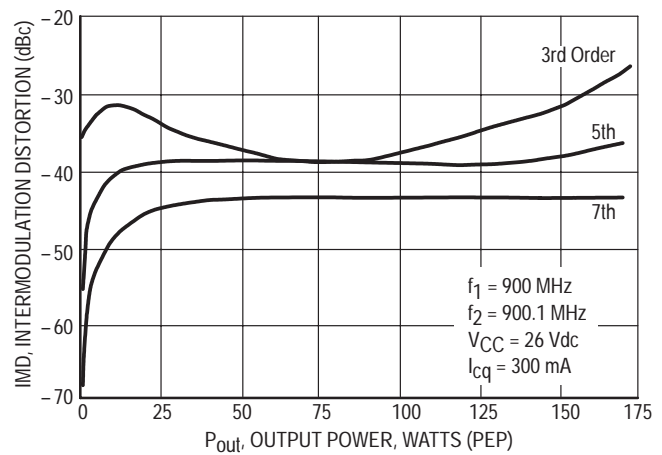


Figure 5. Intermodulation versus Output Power

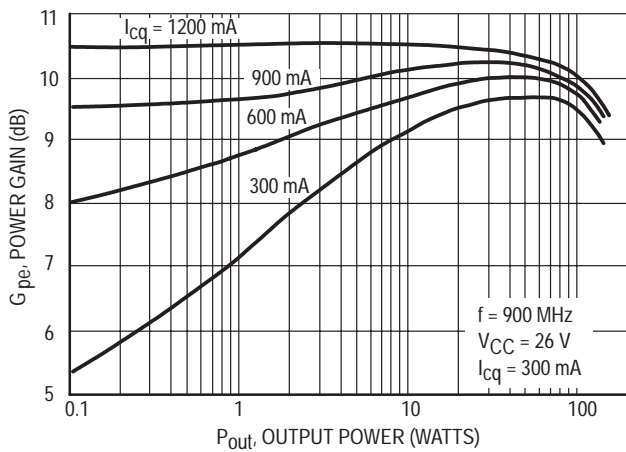


Figure 6. Power Gain versus Output Power

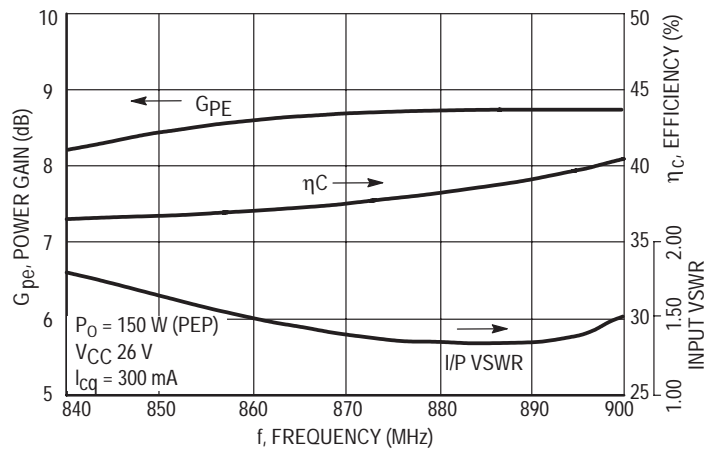
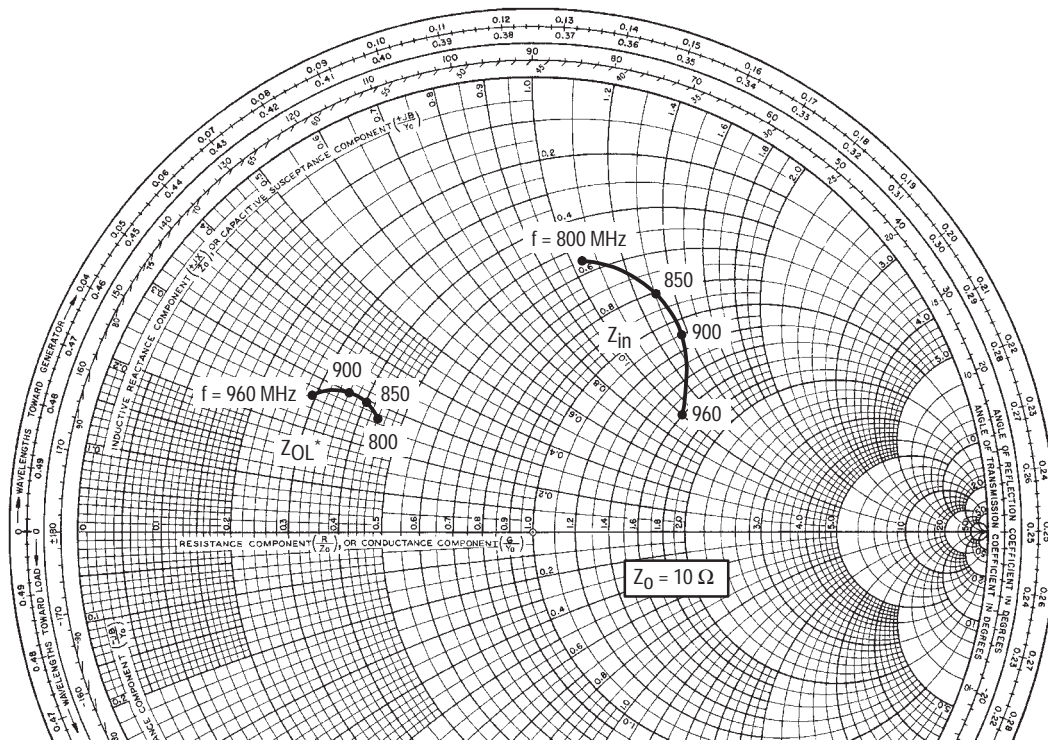


Figure 7. Broadband Test Fixture Performance



f MHz	Z _{in} Ohms	Z _{OL*} Ohms
800	5.51 + j10.6	4.52 + j2.64
850	8.17 + j13.2	4.21 + j2.98
900	11.2 + j13.8	3.68 + j2.97
960	16.8 + j10.1	2.98 + j2.71

NOTE: Z_{in} & Z_{OL*} are given from base-to-base and collector-to-collector respectively

Z_{OL*} = Conjugate of optimum load impedance into which the device operates at a given output power, voltage and frequency.

Figure 8. Input and Output Impedances with Circuit Tuned for Maximum Gain @ P_O = 150 W (PEP), V_{CC} = 26 V

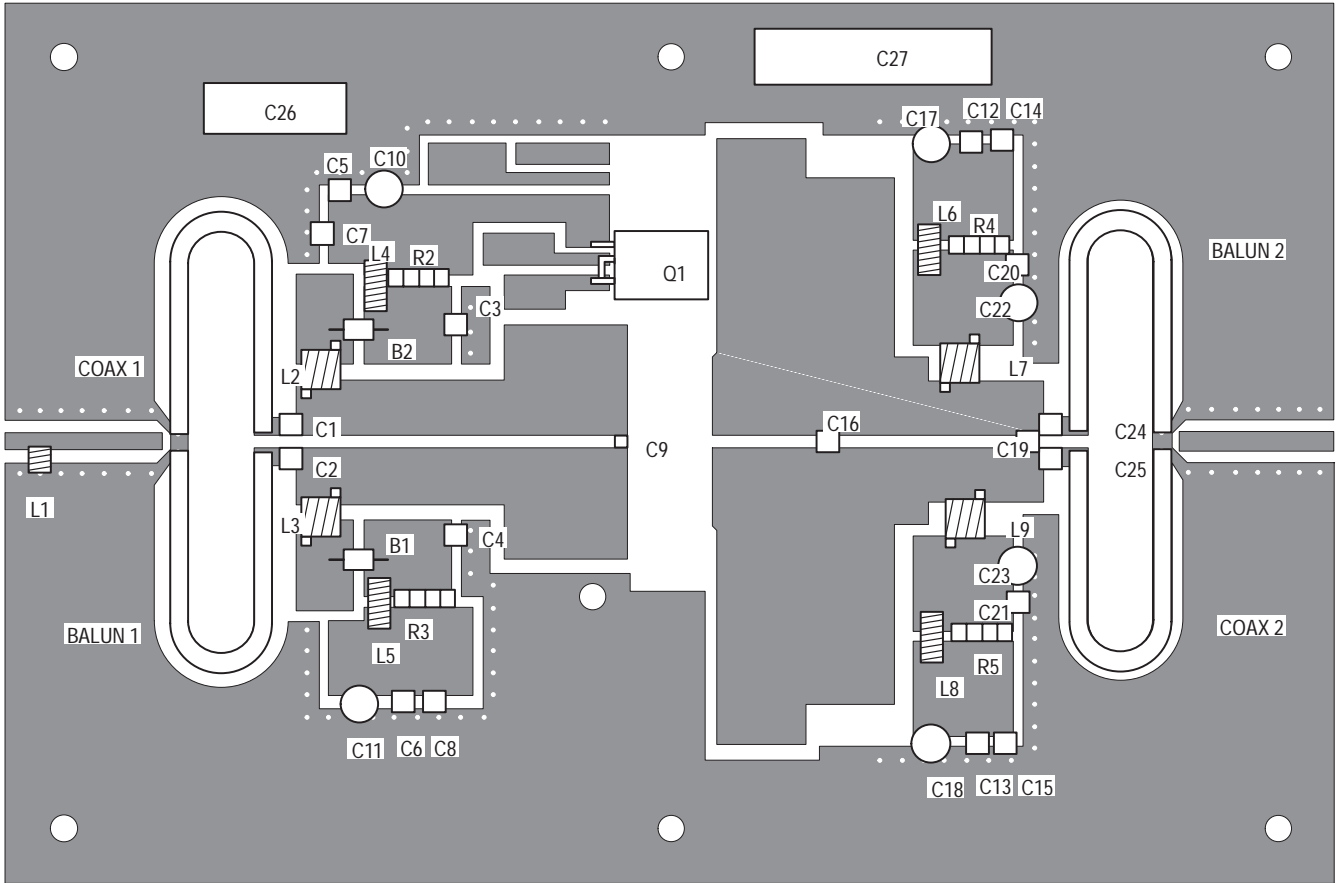


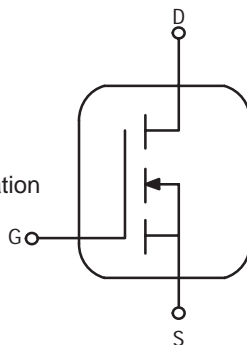
Figure 9. MRF899 Test Fixture Component Layout

The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

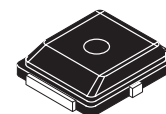
MRF1511T1

The MRF1511T1 is designed for broadband commercial and industrial applications at frequencies to 175 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 7.5 volt portable FM equipment.

- Specified Performance @ 175 MHz, 7.5 Volts
Output Power — 8 Watts
Power Gain — 11.5 dB
Efficiency — 55%
- Capable of Handling 20:1 VSWR, @ 9.5 Vdc,
175 MHz, 2 dB Overdrive
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal
Impedance Parameters
- Broadband UHF/VHF Demonstration Amplifier Information
Available Upon Request
- RF Power Plastic Surface Mount Package
- Available in Tape and Reel.
T1 Suffix = 1,000 Units per 12 mm, 7 Inch Reel.



175 MHz, 8 W, 7.5 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 466-02, STYLE 1
(PLD-1.5)

PLASTIC

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	40	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	4	Adc
Total Device Dissipation @ T _C = 25°C (1) Derate above 25°C	P _D	62.5 0.5	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	150	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	2	°C/W

(1) Calculated based on the formula $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Zero Gate Voltage Drain Current ($V_{DS} = 35\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 10\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc

ON CHARACTERISTICS

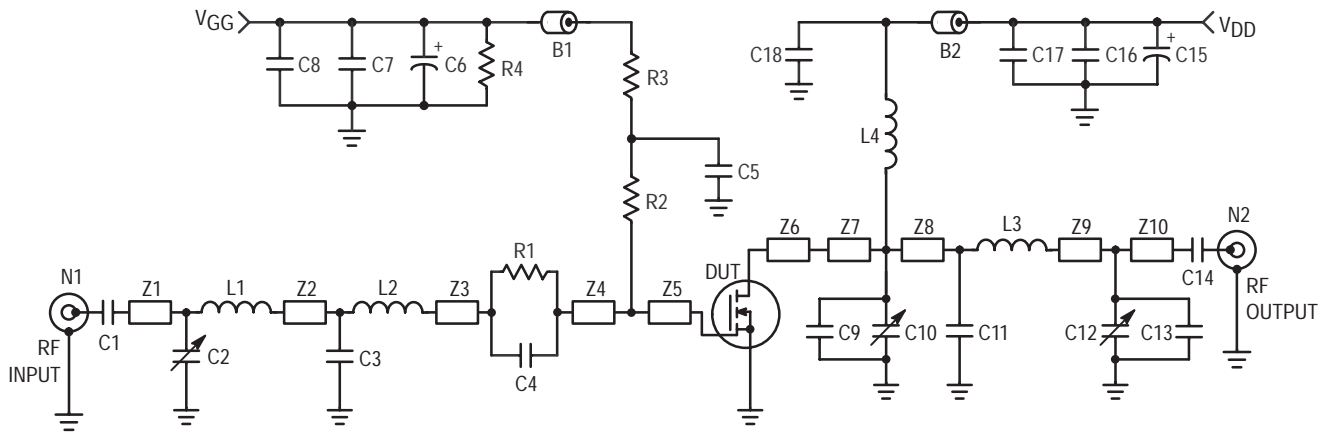
Gate Threshold Voltage ($V_{DS} = 7.5\text{ Vdc}$, $I_D = 170\ \mu\text{A}$)	$V_{GS(th)}$	1.0	1.6	2.1	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.4	—	Vdc

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 7.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	100	—	pF
Output Capacitance ($V_{DS} = 7.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	53	—	pF
Reverse Transfer Capacitance ($V_{DS} = 7.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	8	—	pF

FUNCTIONAL TESTS (In Motorola Test Fixture)

Common–Source Amplifier Power Gain ($V_{DD} = 7.5\text{ Vdc}$, $P_{out} = 8\text{ Watts}$, $I_{DQ} = 150\text{ mA}$, $f = 175\text{ MHz}$)	G_{ps}	10	11.5	—	dB
Drain Efficiency ($V_{DD} = 7.5\text{ Vdc}$, $P_{out} = 8\text{ Watts}$, $I_{DQ} = 150\text{ mA}$, $f = 175\text{ MHz}$)	η	50	55	—	%



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R1	15 Ω , 0805 Chip Resistor
C1, C5, C18	120 pF, 100 mil Chip Capacitor	R2	1.0 k Ω , 1/8 W Resistor
C2, C10, C12	0 to 20 pF, Trimmer Capacitor	R3	1.0 k Ω , 0805 Chip Resistor
C3	33 pF, 100 mil Chip Capacitor	R4	33 k Ω , 1/8 W Resistor
C4	68 pF, 100 mil Chip Capacitor	Z1	0.200" x 0.080" Microstrip
C6, C15	10 μ F, 50 V Electrolytic Capacitor	Z2	0.755" x 0.080" Microstrip
C7, C16	1,200 pF, 100 mil Chip Capacitor	Z3	0.300" x 0.080" Microstrip
C8, C17	0.1 μ F, 100 mil Chip Capacitor	Z4	0.065" x 0.080" Microstrip
C9	150 pF, 100 mil Chip Capacitor	Z5, Z6	0.260" x 0.223" Microstrip
C11	43 pF, 100 mil Chip Capacitor	Z7	0.095" x 0.080" Microstrip
C13	24 pF, 100 mil Chip Capacitor	Z8	0.418" x 0.080" Microstrip
C14	300 pF, 100 mil Chip Capacitor	Z9	1.057" x 0.080" Microstrip
L1, L3	12.5 nH, A04T, Coilcraft	Z10	0.120" x 0.080" Microstrip
L2	26 nH, 4 Turn, Coilcraft	Board	Glass Teflon [®] , 31 mils, 2 oz. Copper
L4	55.5 nH, 5 Turn, Coilcraft		
N1, N2	Type N Flange Mount		

Figure 1. 135 – 175 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 135 – 175 MHz

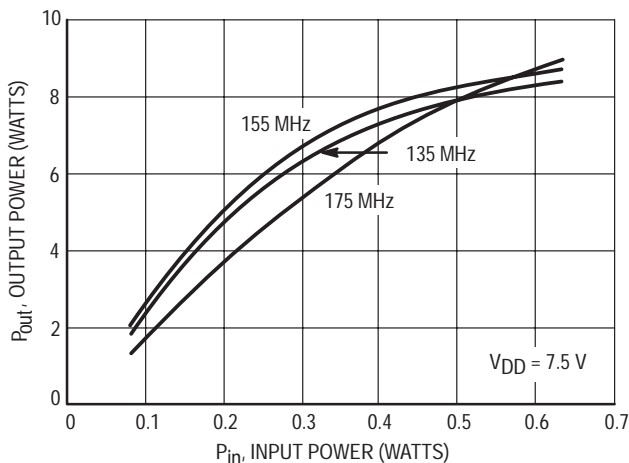


Figure 2. Output Power versus Input Power

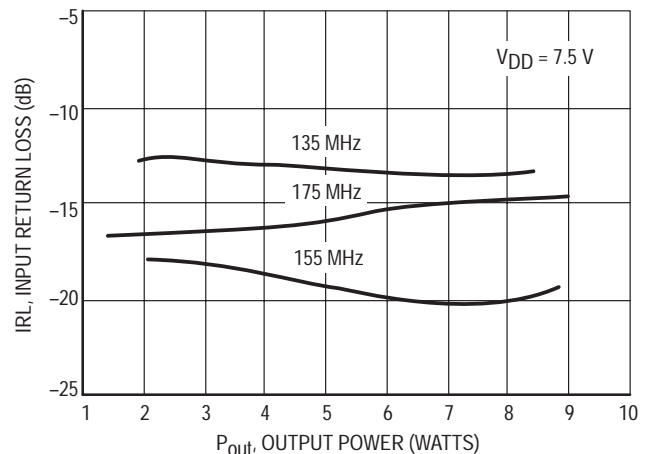


Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 135 – 175 MHz

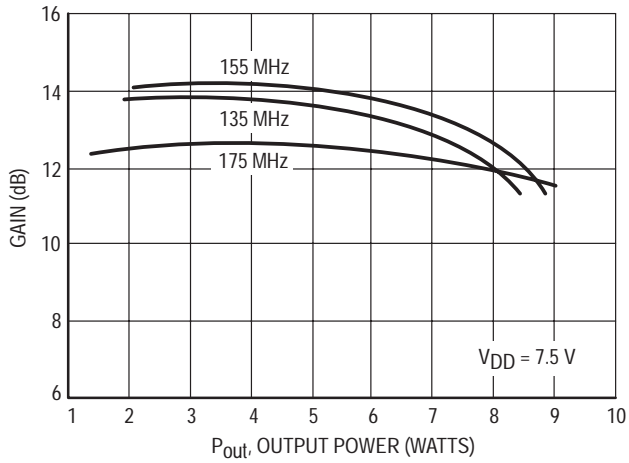


Figure 4. Gain versus Output Power

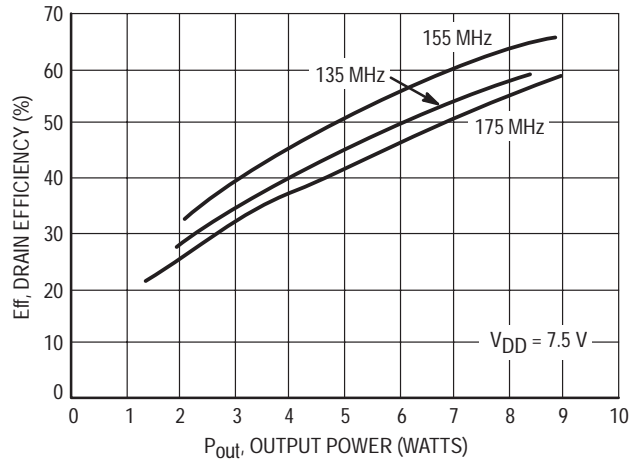


Figure 5. Drain Efficiency versus Output Power

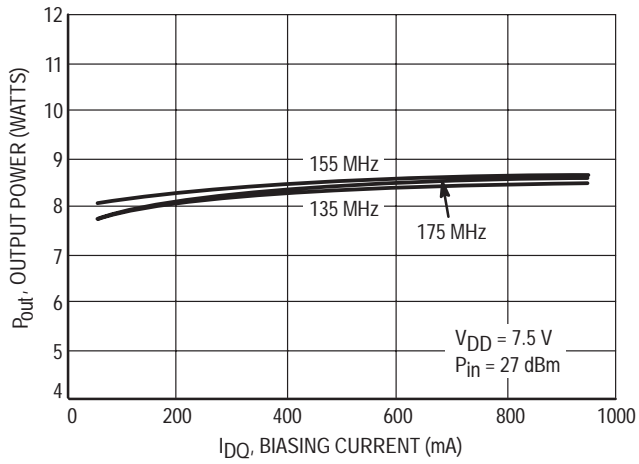


Figure 6. Output Power versus Biasing Current

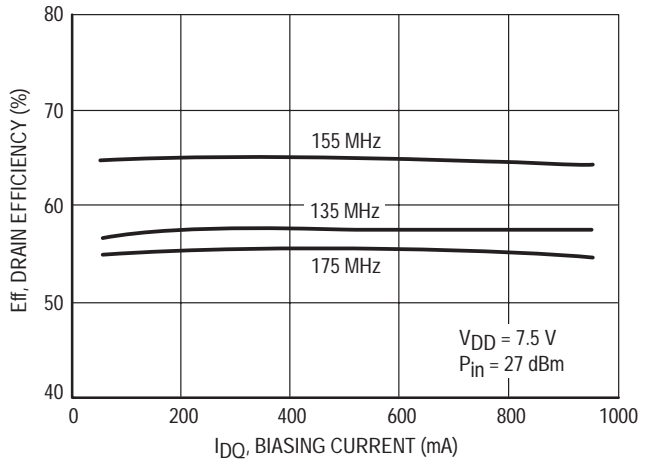


Figure 7. Drain Efficiency versus Biasing Current

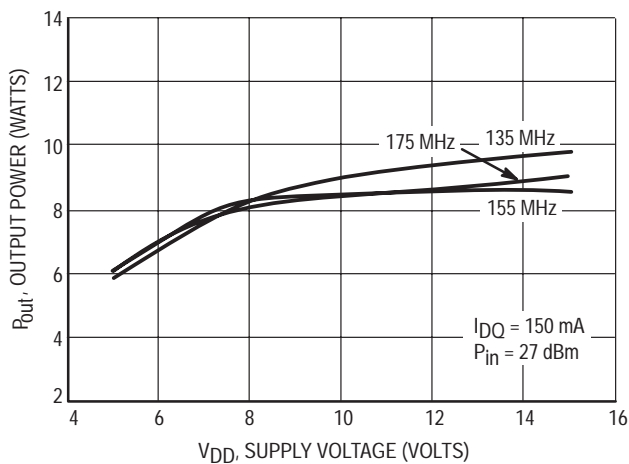


Figure 8. Output Power versus Supply Voltage

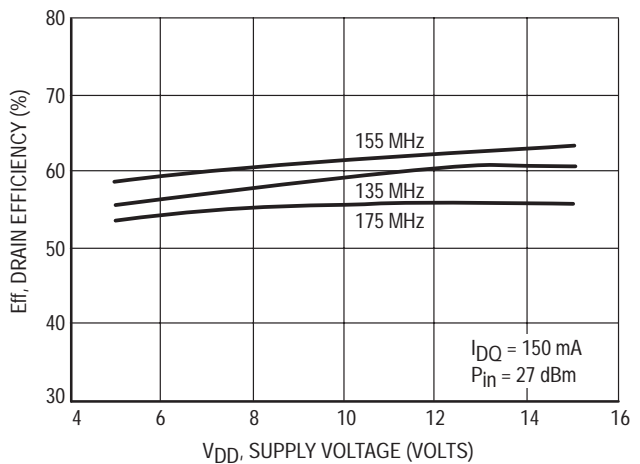
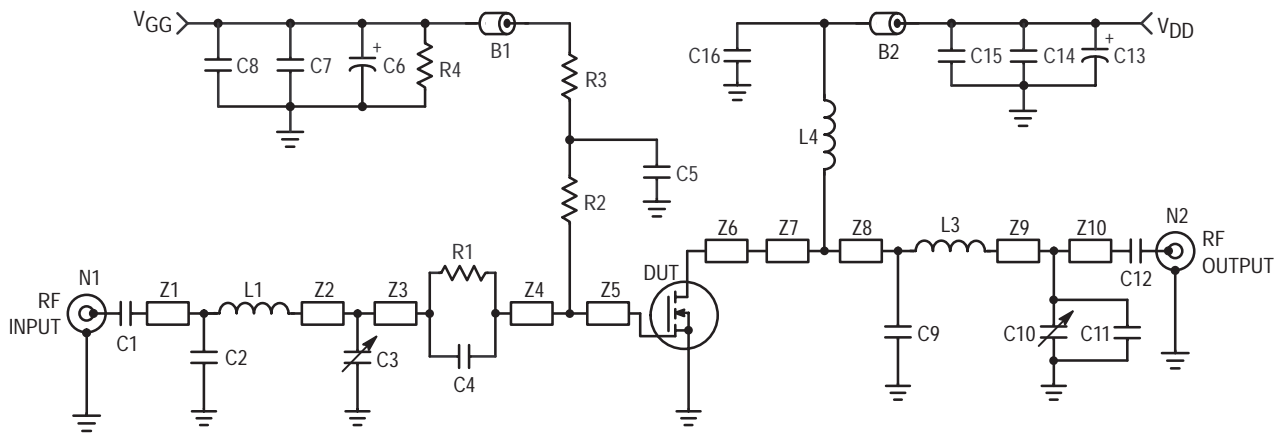


Figure 9. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	N1, N2	Type N Flange Mount
C1, C12	330 pF, 100 mil Chip Capacitor	R1	15 Ω , 0805 Chip Resistor
C2	43 pF, 100 mil Chip Capacitor	R2	51 Ω , 1/2 W Resistor
C3, C10	0 to 20 pF, Trimmer Capacitor	R3	100 Ω , 0805 Chip Resistor
C4	24 pF, 100 mil Chip Capacitor	R4	33 k Ω , 1/8 W Resistor
C5, C16	120 pF, 100 mil Chip Capacitor	Z1	0.136" x 0.080" Microstrip
C6, C13	10 μ F, 50 V Electrolytic Capacitor	Z2	0.242" x 0.080" Microstrip
C7, C14	1,200 pF, 100 mil Chip Capacitor	Z3	1.032" x 0.080" Microstrip
C8, C15	0.1 μ F, 100 mil Chip Capacitor	Z4	0.145" x 0.080" Microstrip
C9	380 pF, 100 mil Chip Capacitor	Z5, Z6	0.260" x 0.223" Microstrip
C11	75 pF, 100 mil Chip Capacitor	Z7	0.134" x 0.080" Microstrip
L1	82 nH, Coilcraft	Z8	0.490" x 0.080" Microstrip
L2	55.5 nH, 5 Turn, Coilcraft	Z9	0.872" x 0.080" Microstrip
L3	39 nH, 6 Turn, Coilcraft	Z10	0.206" x 0.080" Microstrip
		Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 10. 66 – 88 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 66 – 88 MHz

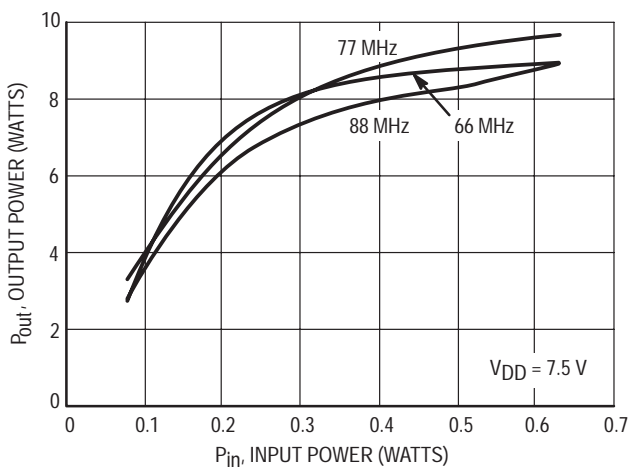


Figure 11. Output Power versus Input Power

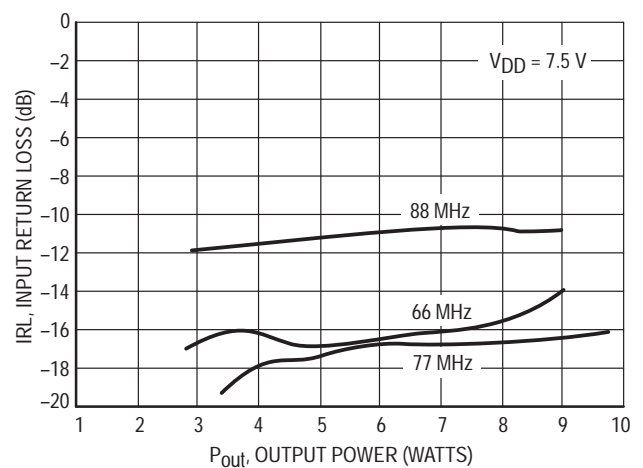


Figure 12. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 66 – 88 MHz

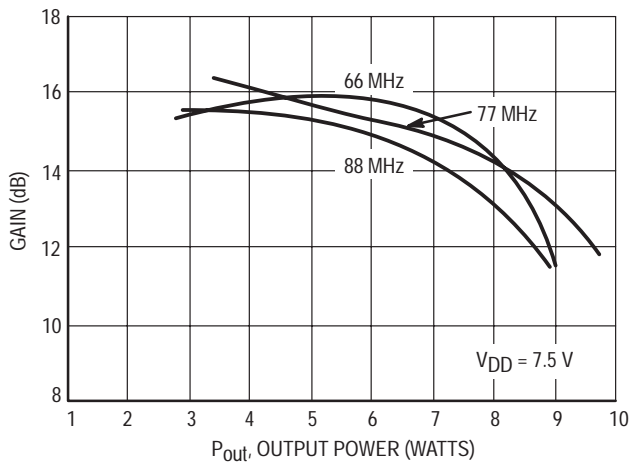


Figure 13. Gain versus Output Power

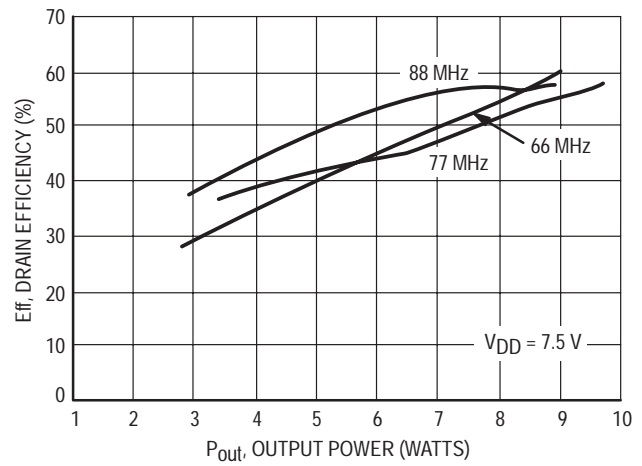


Figure 14. Drain Efficiency versus Output Power

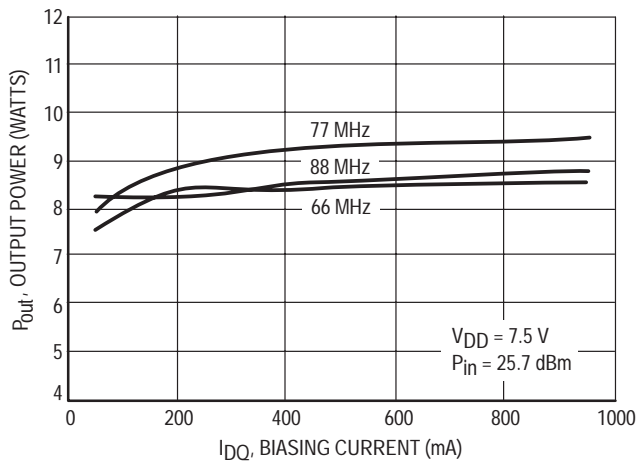


Figure 15. Output Power versus Biasing Current

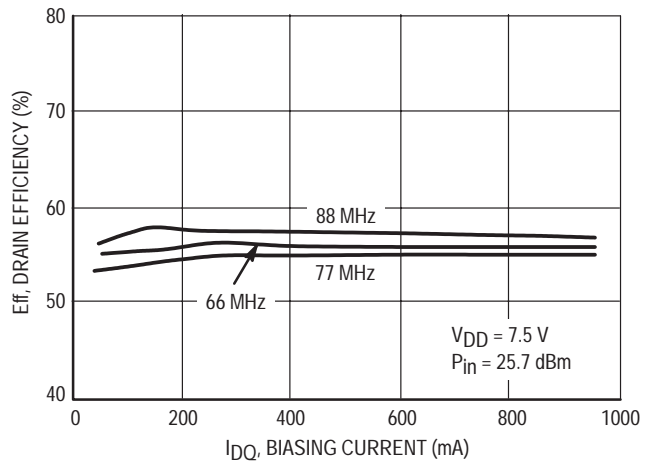


Figure 16. Drain Efficiency versus Biasing Current

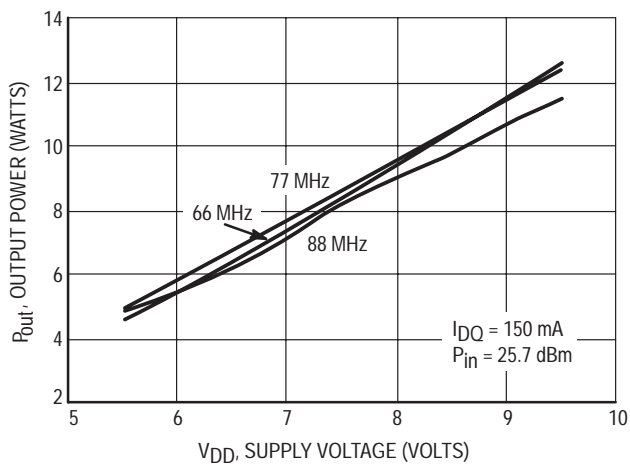


Figure 17. Output Power versus Supply Voltage

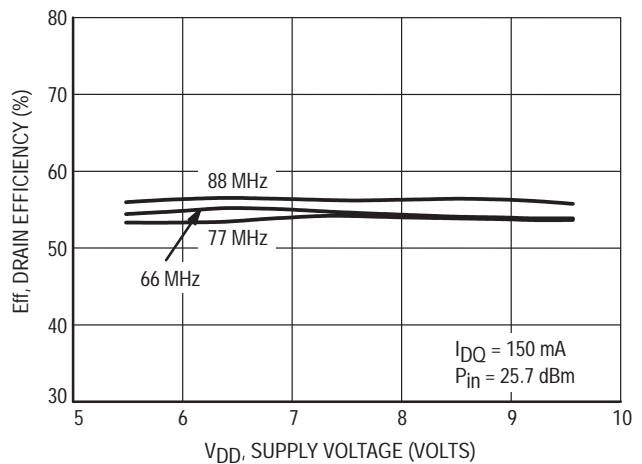
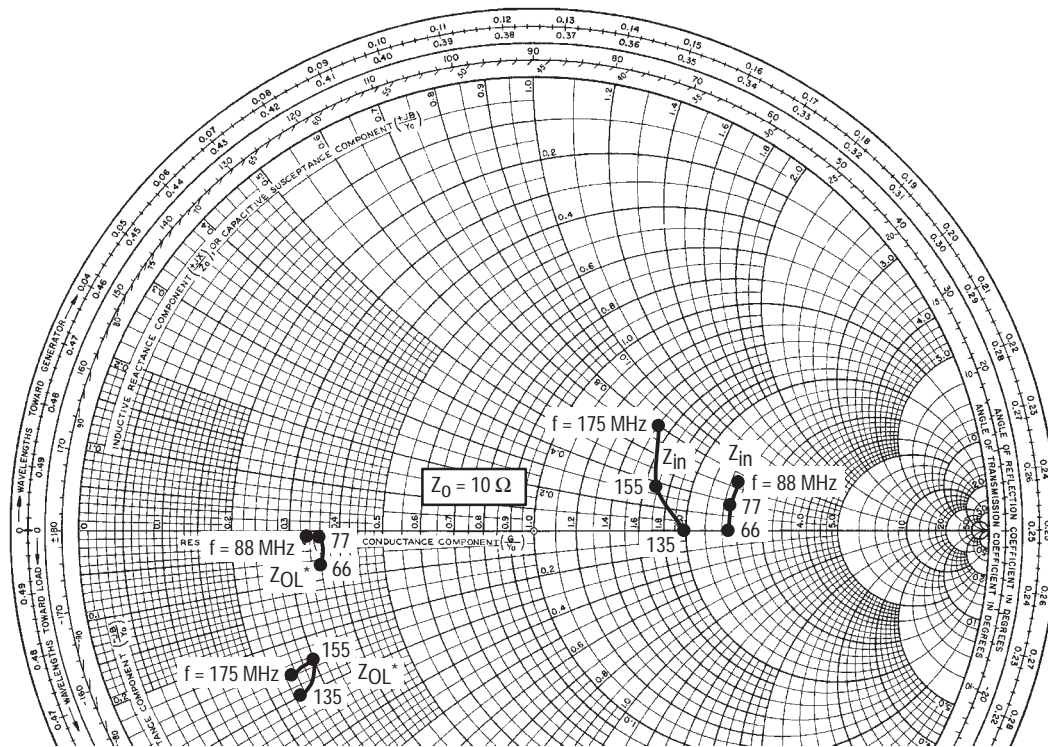


Figure 18. Drain Efficiency versus Supply Voltage



$V_{DD} = 7.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
135	$20.1 - j0.5$	$2.53 - j2.61$
155	$17.0 + j3.6$	$3.01 - j2.48$
175	$15.2 + j7.9$	$2.52 - j3.02$

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 68 pF capacitor in series with gate. (See Figure 1).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

$V_{DD} = 7.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
66	$25.3 - j0.31$	$3.62 - j0.751$
77	$25.6 + j3.62$	$3.59 - j0.129$
88	$26.7 + j6.79$	$3.37 - j0.173$

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 24 pF capacitor in series with gate. (See Figure 10).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

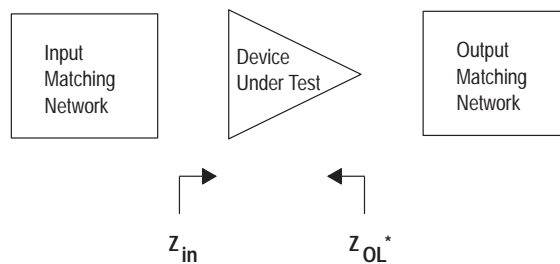


Figure 19. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ($V_{DD} = 7.5$ Vdc)

$I_{DQ} = 150$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.88	-165	18.92	95	0.015	8	0.84	-169
50	0.88	-171	11.47	91	0.016	-5	0.84	-173
100	0.87	-175	5.66	85	0.016	-7	0.84	-176
150	0.87	-176	3.75	82	0.015	-5	0.85	-176
200	0.87	-177	2.78	78	0.014	-6	0.84	-176
250	0.87	-177	2.16	75	0.014	-10	0.85	-176
300	0.88	-177	1.77	72	0.012	-17	0.86	-176
350	0.88	-177	1.49	69	0.013	-11	0.86	-176
400	0.88	-177	1.26	66	0.013	-17	0.87	-175
450	0.88	-177	1.08	64	0.011	-20	0.87	-175
500	0.89	-176	0.96	63	0.012	-20	0.88	-175

$I_{DQ} = 800$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.89	-166	18.89	95	0.014	10	0.85	-170
50	0.88	-172	11.44	91	0.015	8	0.84	-174
100	0.87	-175	5.65	86	0.016	-2	0.85	-176
150	0.87	-177	3.74	82	0.014	-8	0.84	-177
200	0.87	-177	2.78	78	0.013	-18	0.85	-177
250	0.88	-177	2.16	75	0.012	-11	0.85	-176
300	0.88	-177	1.77	73	0.015	-15	0.86	-176
350	0.88	-177	1.50	70	0.009	-7	0.87	-176
400	0.88	-177	1.26	67	0.012	-3	0.87	-176
450	0.88	-177	1.09	65	0.012	-18	0.87	-175
500	0.89	-177	0.97	64	0.009	-10	0.88	-175

$I_{DQ} = 1.5$ A

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
30	0.90	-168	17.89	95	0.013	2	0.86	-172
50	0.89	-173	10.76	91	0.013	3	0.86	-175
100	0.88	-176	5.32	86	0.014	-19	0.86	-177
150	0.88	-177	3.53	83	0.013	-6	0.86	-177
200	0.88	-177	2.63	80	0.011	-4	0.86	-177
250	0.88	-178	2.05	77	0.012	-14	0.86	-177
300	0.88	-177	1.69	75	0.013	-2	0.87	-177
350	0.89	-177	1.43	72	0.010	-9	0.87	-176
400	0.89	-177	1.22	70	0.014	-3	0.88	-176
450	0.89	-177	1.06	68	0.011	-8	0.88	-176
500	0.89	-177	0.94	67	0.011	-15	0.88	-176

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

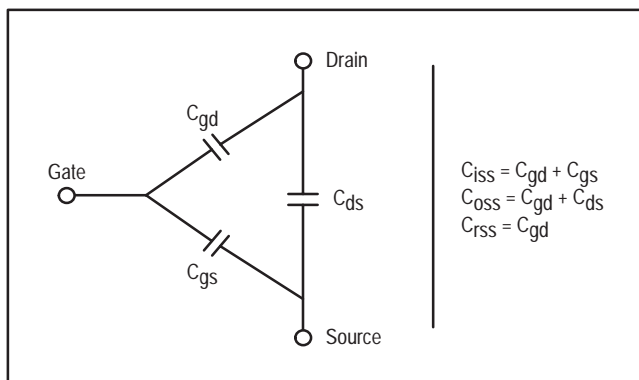
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

BV_{DSS} values for this device are higher than normally required for typical applications. Measurement of BV_{DSS} is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of $10^9 \Omega$ – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 150 \text{ mA}$, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 2°C/W assumes a majority of the 0.065" x 0.180" source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

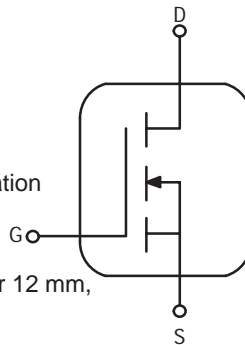
Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

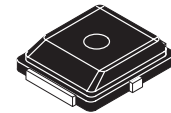
The MRF1513T1 is designed for broadband commercial and industrial applications at frequencies to 520 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 7.5 volt portable and 12.5 volt mobile FM equipment.

- Specified Performance @ 520 MHz, 12.5 Volts
Output Power — 3 Watts
Power Gain — 11 dB
Efficiency — 55%
- Capable of Handling 20:1 VSWR, @ 15.5 Vdc, 520 MHz, 2 dB Overdrive
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- Broadband UHF/VHF Demonstration Amplifier Information Available Upon Request
- RF Power Plastic Surface Mount Package
- Available in Tape and Reel. T1 Suffix = 1,000 Units per 12 mm, 7 Inch Reel.



MRF1513T1

520 MHz, 3 W, 12.5 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 466-02, STYLE 1
(PLD-1.5)
PLASTIC

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	40	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	2	Adc
Total Device Dissipation @ T _C = 25°C (1) Derate above 25°C	P _D	31.25 0.25	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	150	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	4	°C/W

(1) Calculated based on the formula $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Zero Gate Voltage Drain Current ($V_{DS} = 40\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 10\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc

ON CHARACTERISTICS

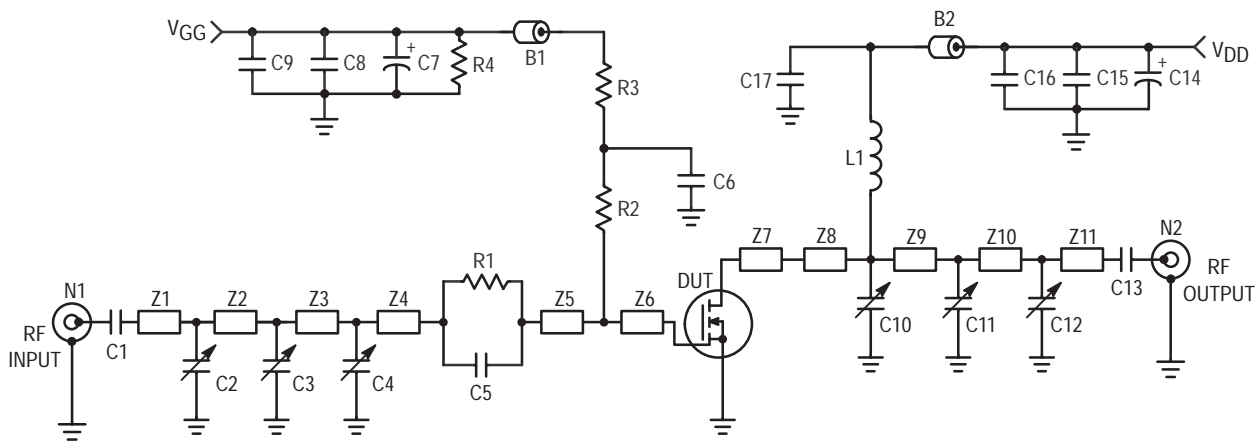
Gate Threshold Voltage ($V_{DS} = 12.5\text{ Vdc}$, $I_D = 60\ \mu\text{A}$)	$V_{GS(th)}$	1.0	1.7	2.1	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 500\text{ mAdc}$)	$V_{DS(on)}$	—	0.65	—	Vdc

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	33	—	pF
Output Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	16.5	—	pF
Reverse Transfer Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	2.2	—	pF

FUNCTIONAL TESTS (In Motorola Test Fixture)

Common–Source Amplifier Power Gain ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 3\text{ Watts}$, $I_{DQ} = 50\text{ mA}$, $f = 520\text{ MHz}$)	G_{ps}	10	11	—	dB
Drain Efficiency ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 3\text{ Watts}$, $I_{DQ} = 50\text{ mA}$, $f = 520\text{ MHz}$)	η	50	55	—	%



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R4	33 k Ω , 1/8 W Resistor
C1, C13	240 pF, 100 mil Chip Capacitor	Z1	0.236" x 0.080" Microstrip
C2, C3, C4, C10,		Z2	0.981" x 0.080" Microstrip
C11, C12	0 to 20 pF, Trimmer Capacitor	Z3	0.240" x 0.080" Microstrip
C5, C6, C17	120 pF, 100 mil Chip Capacitor	Z4	0.098" x 0.080" Microstrip
C7, C14	10 μ F, 50 V Electrolytic Capacitor	Z5	0.192" x 0.223" Microstrip
C8, C15	1,200 pF, 100 mil Chip Capacitor	Z6, Z7	0.260" x 0.223" Microstrip
C9, C16	0.1 μ F, 100 mil Chip Capacitor	Z8	0.705" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z9	0.342" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Z10	0.347" x 0.080" Microstrip
R1, R3	15 Ω , 0805 Chip Resistor	Z11	0.846" x 0.080" Microstrip
R2	1 k Ω , 1/8 W Resistor	Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 1. 450 – 520 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 450 – 520 MHz

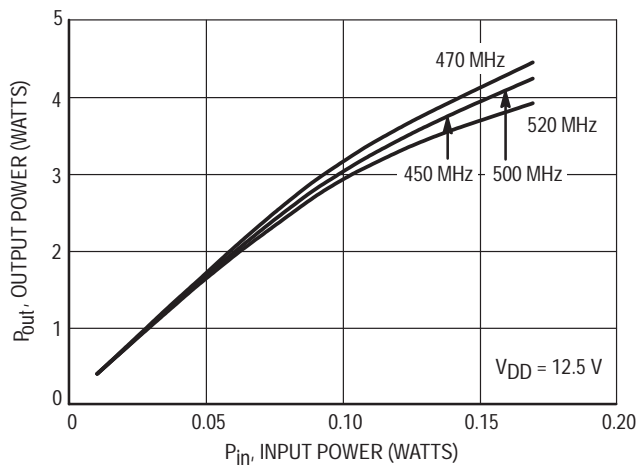


Figure 2. Output Power versus Input Power

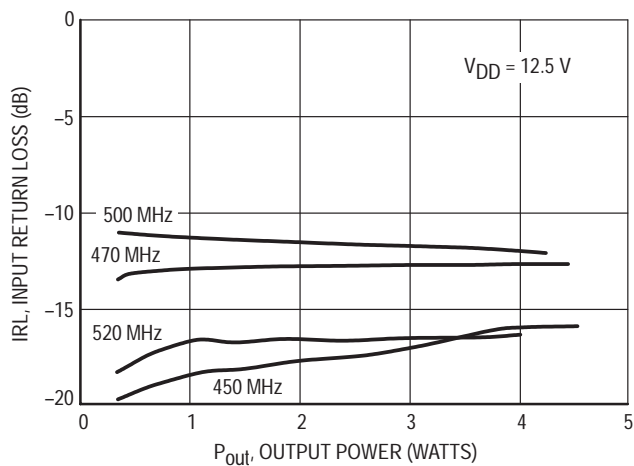


Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 450 – 520 MHz

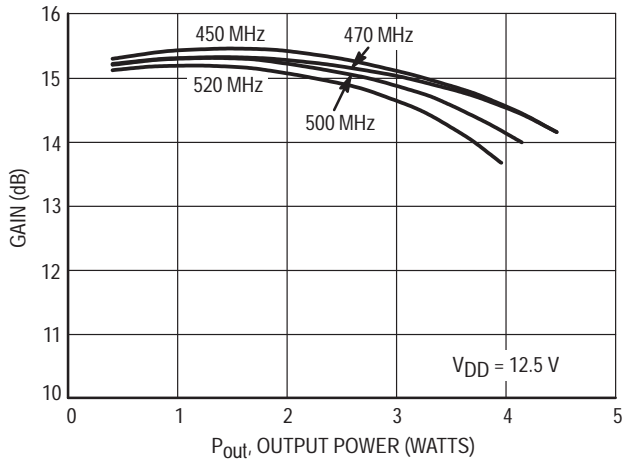


Figure 4. Gain versus Output Power

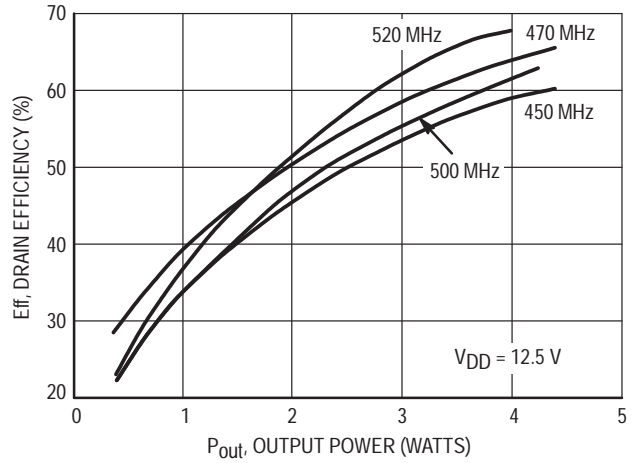


Figure 5. Drain Efficiency versus Output Power

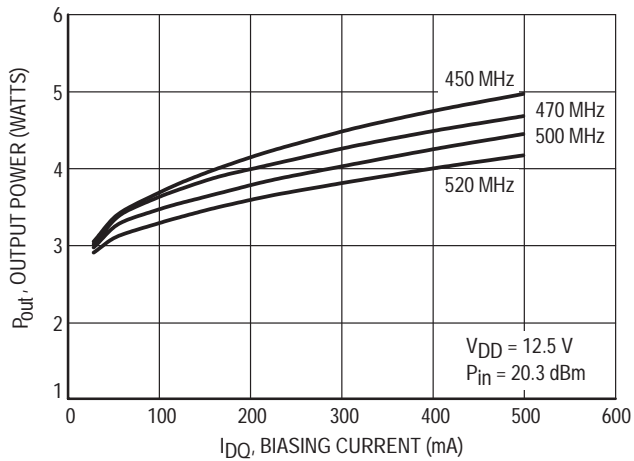


Figure 6. Output Power versus Biasing Current

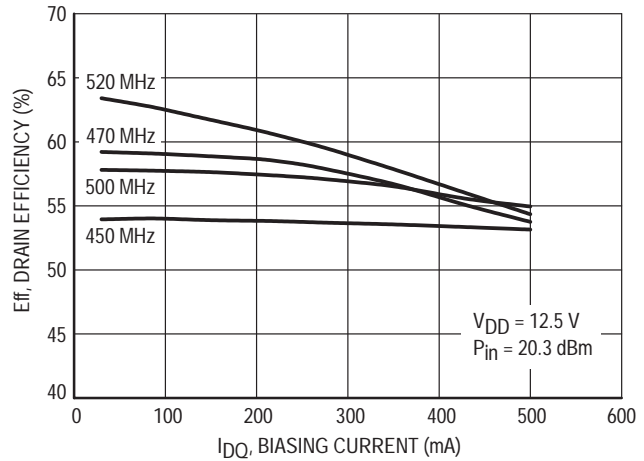


Figure 7. Drain Efficiency versus Biasing Current

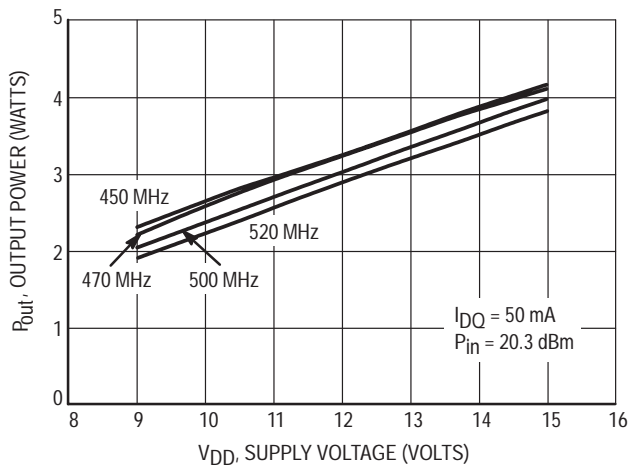


Figure 8. Output Power versus Supply Voltage

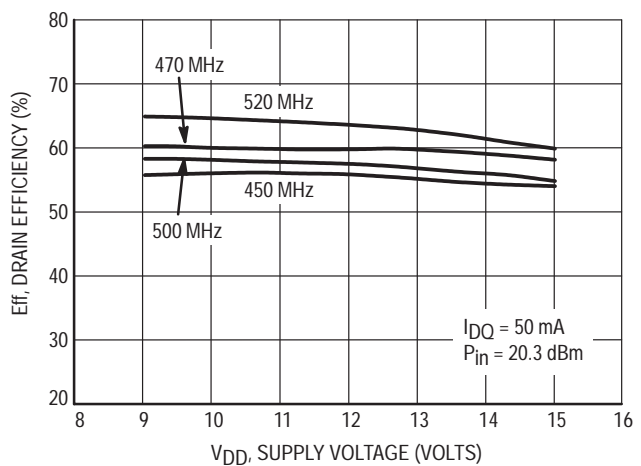
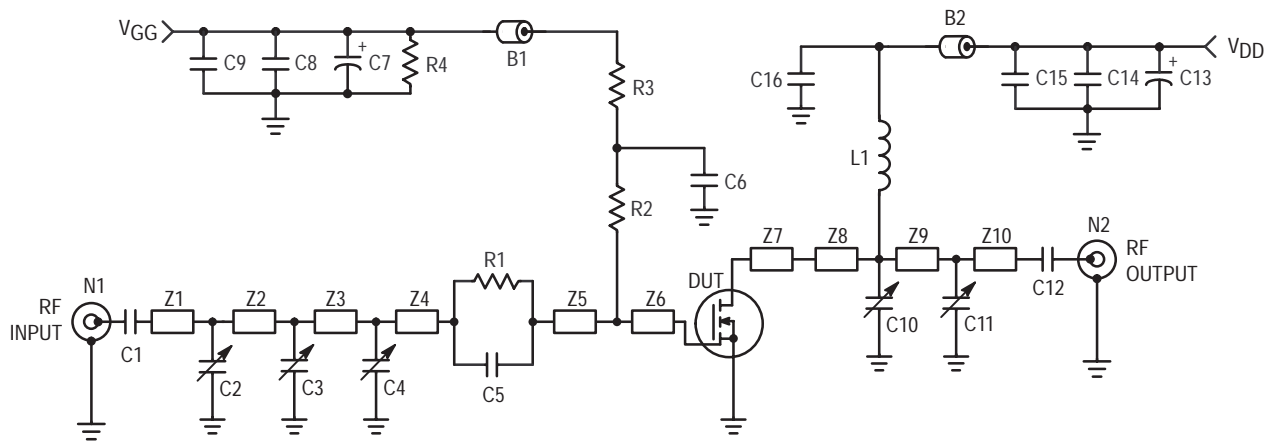


Figure 9. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R3	15 Ω , 0805 Chip Resistor
C1, C12	330 pF, 100 mil Chip Capacitor	R4	33 k Ω , 1/8 W Resistor
C2, C3, C4,		Z1	0.253" x 0.080" Microstrip
C10, C11	1 to 20 pF, Trimmer Capacitor	Z2	0.958" x 0.080" Microstrip
C5, C6, C16	120 pF, 100 mil Chip Capacitor	Z3	0.247" x 0.080" Microstrip
C7, C13	10 μ F, 50 V Electrolytic Capacitor	Z4	0.193" x 0.080" Microstrip
C8, C14	1,200 pF, 100 mil Chip Capacitor	Z5	0.132" x 0.223" Microstrip
C9, C15	0.1 μ F, 100 mil Chip Capacitor	Z6, Z7	0.260" x 0.223" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z8	0.494" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Z9	0.941" x 0.080" Microstrip
R1	15 Ω , 0805 Chip Resistor	Z10	0.452" x 0.080" Microstrip
R2	1 k Ω , 1/8 W Resistor	Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 10. 400 – 470 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 400 – 470 MHz

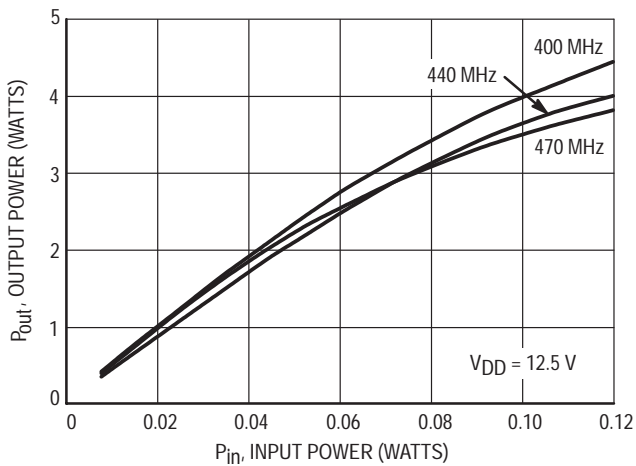


Figure 11. Output Power versus Input Power

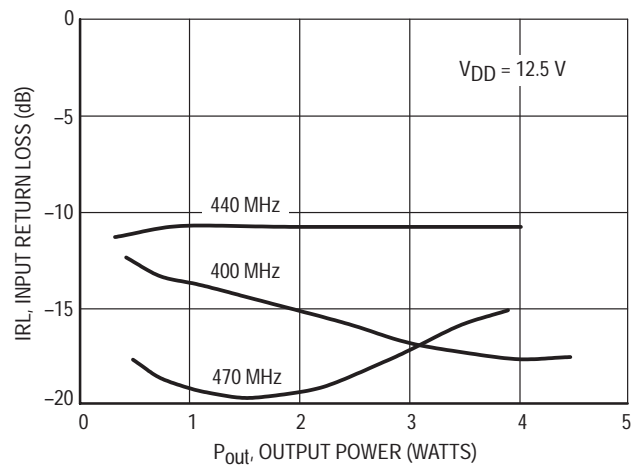


Figure 12. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 400 – 470 MHz

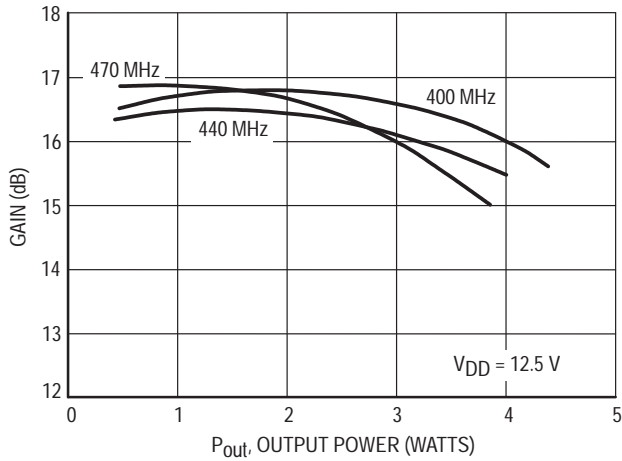


Figure 13. Gain versus Output Power

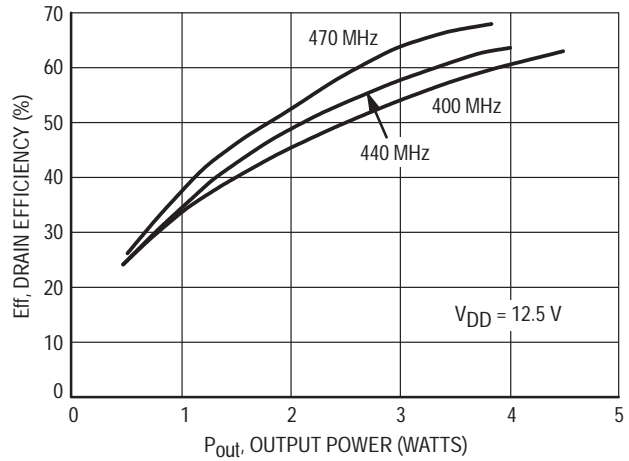


Figure 14. Drain Efficiency versus Output Power

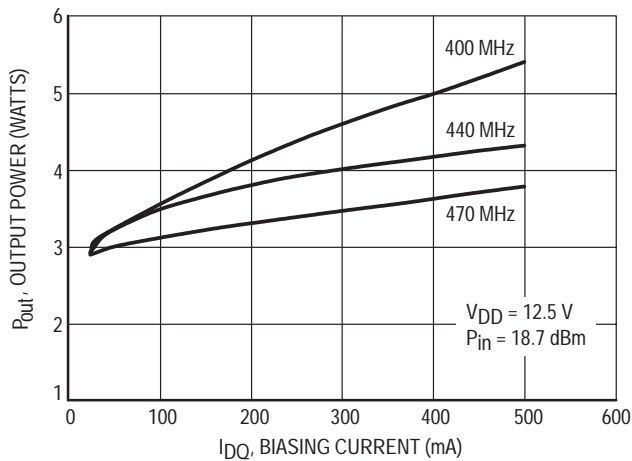


Figure 15. Output Power versus Biasing Current

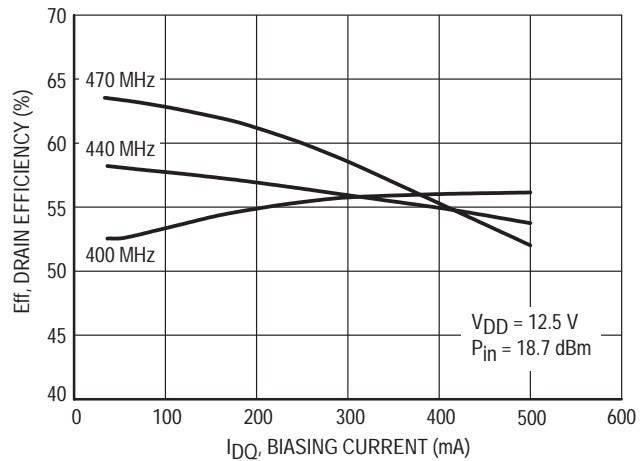


Figure 16. Drain Efficiency versus Biasing Current

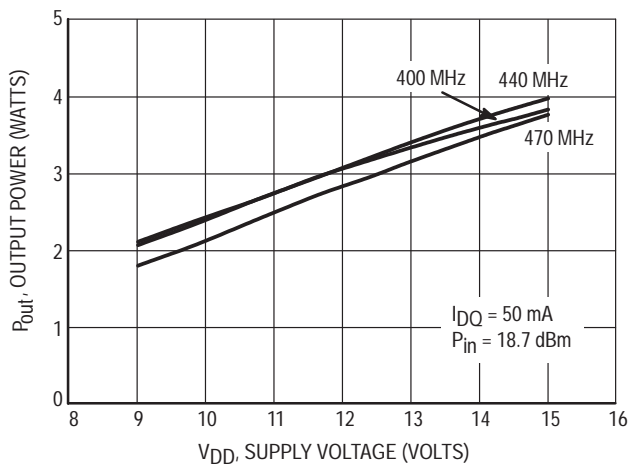


Figure 17. Output Power versus Supply Voltage

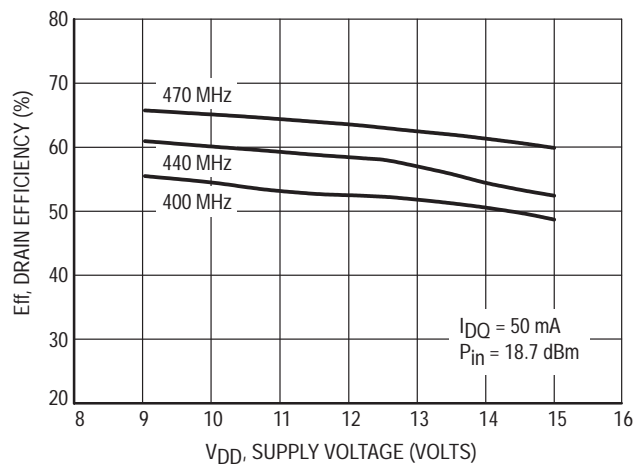
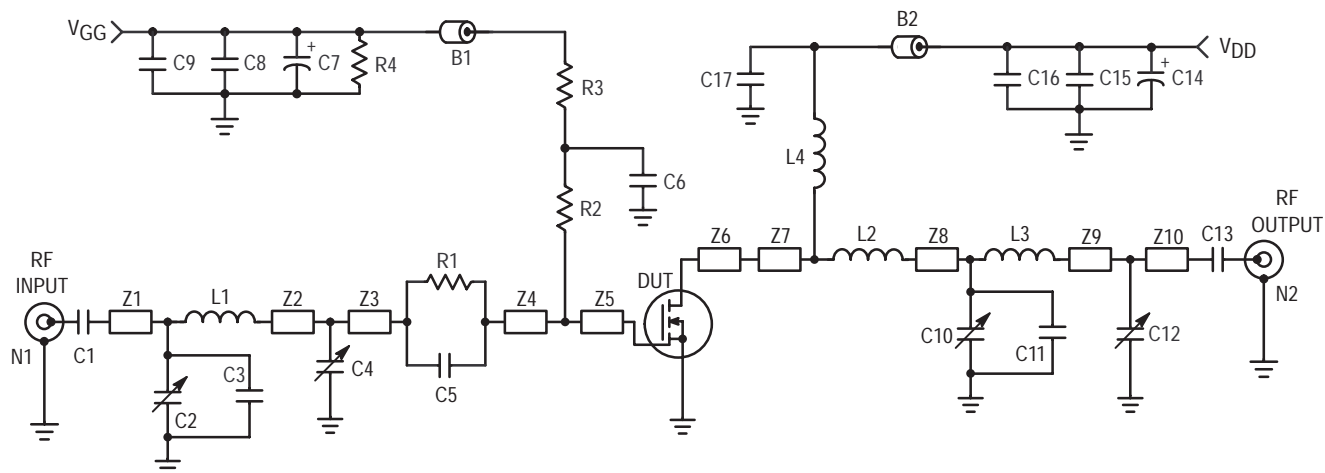


Figure 18. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	L4	33 nH, 5 Turn, Coilcraft
C1, C13	330 pF, 100 mil Chip Capacitor	N1, N2	Type N Flange Mount
C2, C4, C10, C12	0 to 20 pF, Trimmer Capacitor	R1	15 Ω , 0805 Chip Resistor
C3	12 pF, 100 mil Chip Capacitor	R2	56 Ω , 1/8 W Chip Resistor
C5	130 pF, 100 mil Chip Capacitor	R3	10 Ω , 1/8 W Chip Resistor
C6, C17	120 pF, 100 mil Chip Capacitor	R4	33 k Ω , 1/8 W Chip Resistor
C7, C14	10 μ F, 50 V Electrolytic Capacitor	Z1	0.115" x 0.080" Microstrip
C8, C15	1,000 pF, 100 mil Chip Capacitor	Z2	0.230" x 0.080" Microstrip
C9, C16	0.1 μ F, 100 mil Chip Capacitor	Z3	1.034" x 0.080" Microstrip
C11	18 pF, 100 mil Chip Capacitor	Z4	0.202" x 0.080" Microstrip
L1	26 nH, 4 Turn, Coilcraft	Z5, Z6	0.260" x 0.223" Microstrip
L2	8 nH, 3 Turn, Coilcraft	Z7	1.088" x 0.080" Microstrip
L3	55.5 nH, 5 Turn, Coilcraft	Z8	0.149" x 0.080" Microstrip
		Z9	0.171" x 0.080" Microstrip
		Z10	0.095" x 0.080" Microstrip
		Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 19. 135 – 175 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 135 – 175 MHz

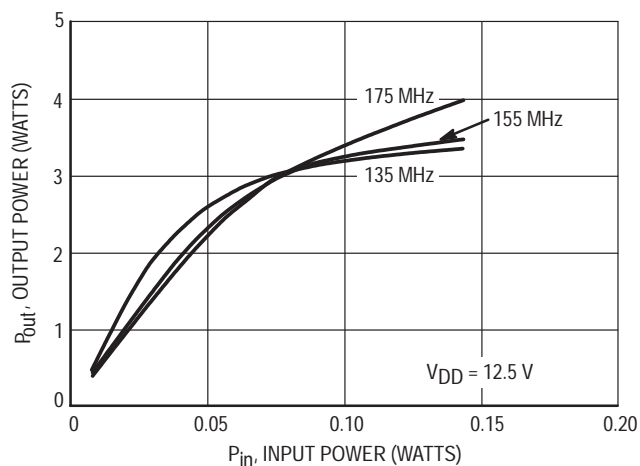


Figure 20. Output Power versus Input Power

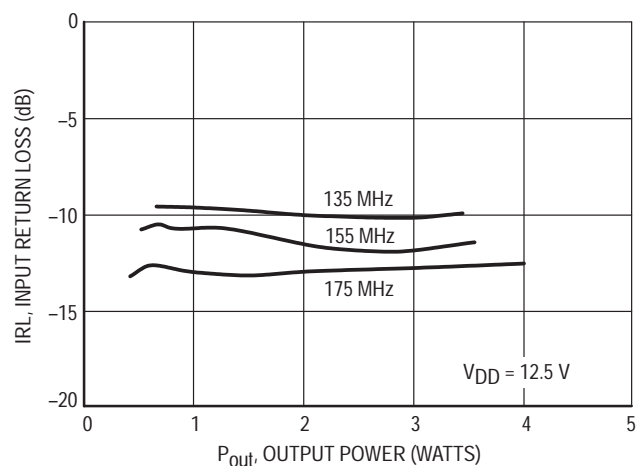


Figure 21. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 135 – 175 MHz

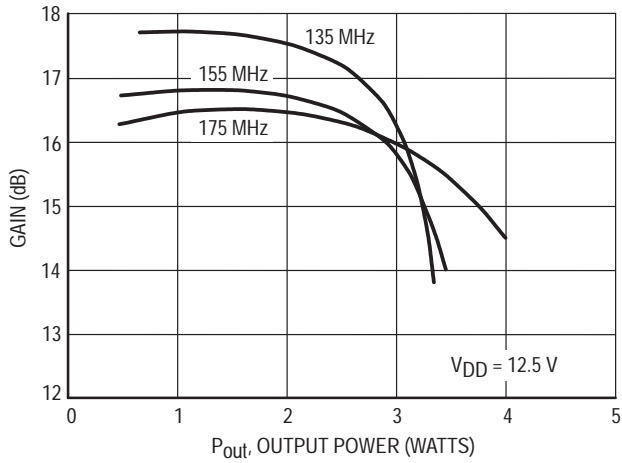


Figure 22. Gain versus Output Power

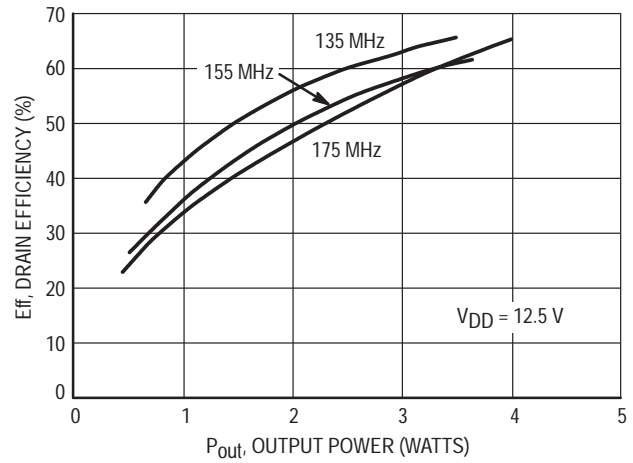


Figure 23. Drain Efficiency versus Output Power

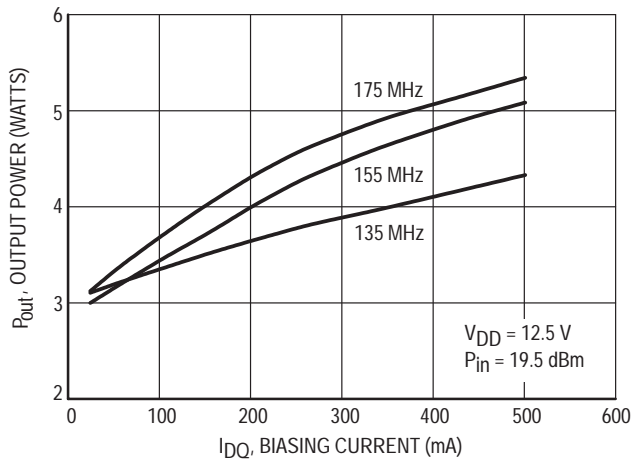


Figure 24. Output Power versus Biasing Current

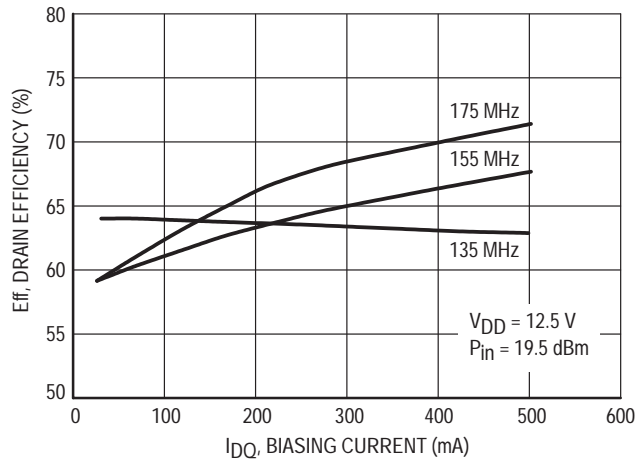


Figure 25. Drain Efficiency versus Biasing Current

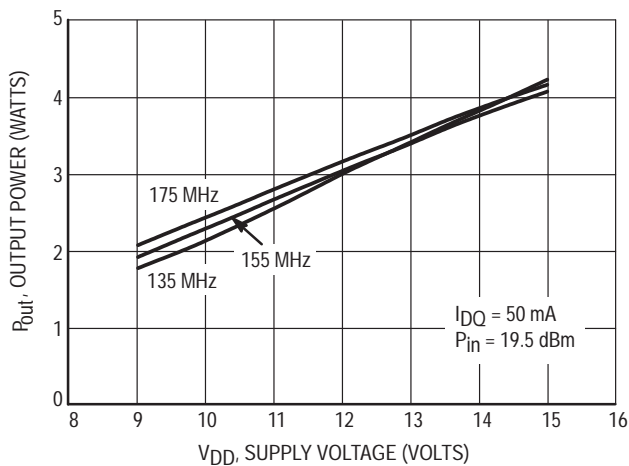


Figure 26. Output Power versus Supply Voltage

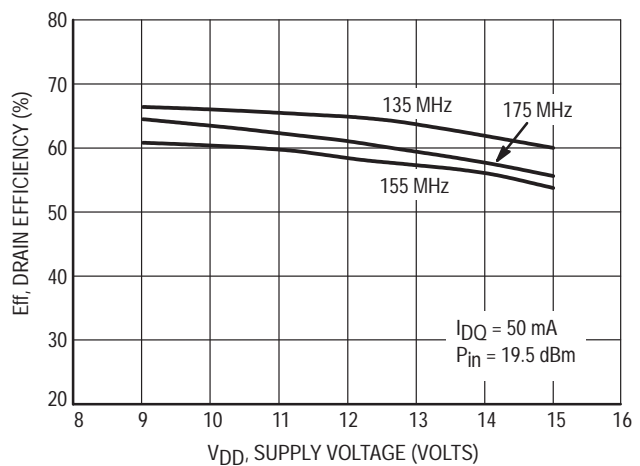
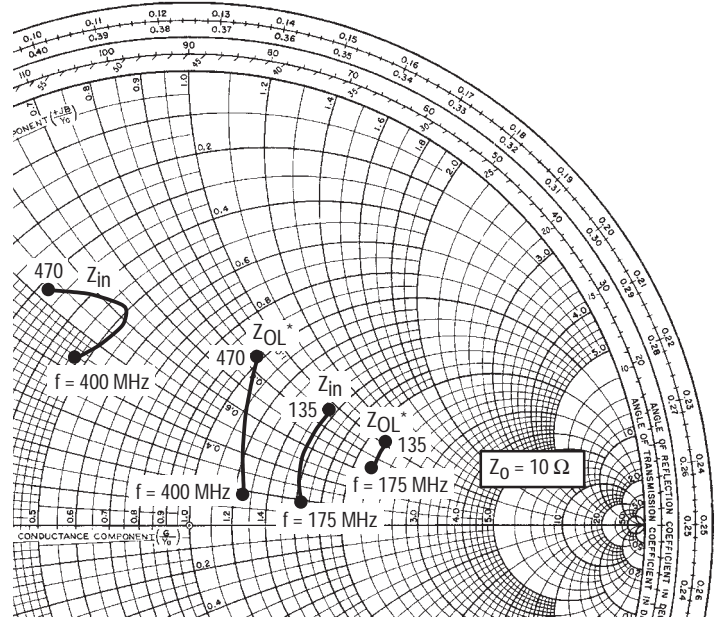
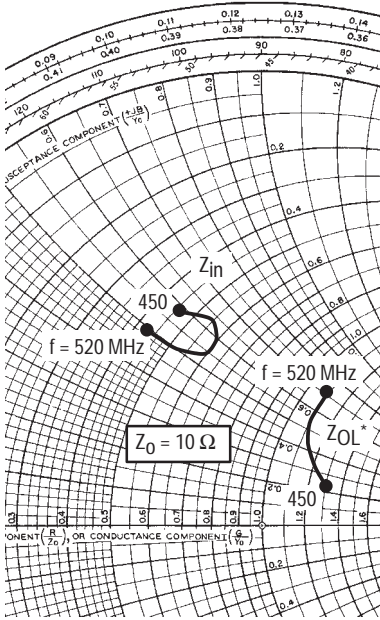


Figure 27. Drain Efficiency versus Supply Voltage



$V_{DD} = 12.5 \text{ V}$, $I_{DQ} = 50 \text{ mA}$, $P_{out} = 3 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
450	4.64 + j5.82	13.11 + j2.15
470	5.42 + j6.34	12.16 + j3.26
500	5.96 + j5.45	11.03 + j5.42
520	4.28 + j4.94	10.99 + j7.18

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 120 pF capacitor in series with gate. (See Figure 1).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

$V_{DD} = 12.5 \text{ V}$, $I_{DQ} = 50 \text{ mA}$, $P_{out} = 3 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
400	4.72 + j4.38	12.57 + j1.88
440	4.88 + j6.34	11.21 + j5.87
470	3.22 + j5.24	9.82 + j8.63

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 130 pF capacitor in series with gate. (See Figure 10).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

$V_{DD} = 12.5 \text{ V}$, $I_{DQ} = 50 \text{ mA}$, $P_{out} = 3 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
135	16.55 + j1.82	22.01 + j10.32
155	15.59 + j5.38	22.03 + j8.07
175	15.55 + j9.43	22.08 + j6.85

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 130 pF capacitor in series with gate. (See Figure 19).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

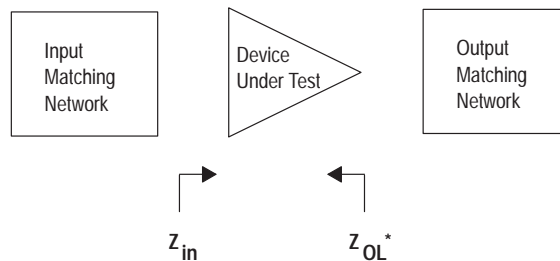


Figure 28. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ($V_{DD} = 12.5$ Vdc)

$I_{DQ} = 50$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.93	-94	22.09	125	0.044	33	0.77	-81
100	0.81	-131	12.78	101	0.052	6	0.61	-115
200	0.76	-153	6.31	81	0.047	-10	0.59	-135
300	0.76	-160	3.92	69	0.044	-19	0.64	-142
400	0.77	-164	2.74	60	0.040	-26	0.70	-147
500	0.79	-167	1.99	54	0.036	-31	0.75	-151
600	0.80	-169	1.55	48	0.034	-37	0.80	-155
700	0.81	-171	1.25	44	0.028	-40	0.82	-158
800	0.82	-172	1.02	38	0.027	-42	0.86	-161
900	0.83	-173	0.85	35	0.017	-42	0.88	-163
1000	0.84	-175	0.70	29	0.018	-49	0.91	-166

$I_{DQ} = 500$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.84	-127	32.57	112	0.025	17	0.64	-130
100	0.80	-152	17.23	97	0.025	13	0.64	-153
200	0.78	-166	8.62	85	0.025	-9	0.65	-163
300	0.78	-171	5.58	79	0.023	-9	0.67	-166
400	0.78	-173	4.08	72	0.022	-9	0.69	-166
500	0.78	-175	3.14	68	0.020	-10	0.71	-167
600	0.79	-176	2.55	63	0.022	-15	0.74	-168
700	0.79	-177	2.14	60	0.019	-20	0.76	-168
800	0.80	-178	1.80	54	0.018	-31	0.79	-170
900	0.81	-178	1.54	51	0.015	-25	0.80	-170
1000	0.82	-179	1.31	46	0.012	-36	0.81	-172

$I_{DQ} = 1$ A

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.84	-129	32.57	111	0.023	24	0.61	-137
100	0.80	-153	17.04	97	0.024	13	0.64	-156
200	0.78	-167	8.52	85	0.023	5	0.65	-165
300	0.77	-172	5.53	79	0.020	-7	0.67	-167
400	0.77	-174	4.06	73	0.020	-11	0.69	-167
500	0.78	-175	3.13	69	0.021	-9	0.72	-167
600	0.78	-177	2.54	64	0.017	-26	0.74	-168
700	0.78	-177	2.13	60	0.017	-14	0.75	-168
800	0.79	-178	1.81	55	0.015	-23	0.78	-170
900	0.80	-178	1.54	51	0.013	-31	0.79	-170
1000	0.80	-179	1.30	46	0.011	-17	0.80	-172

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

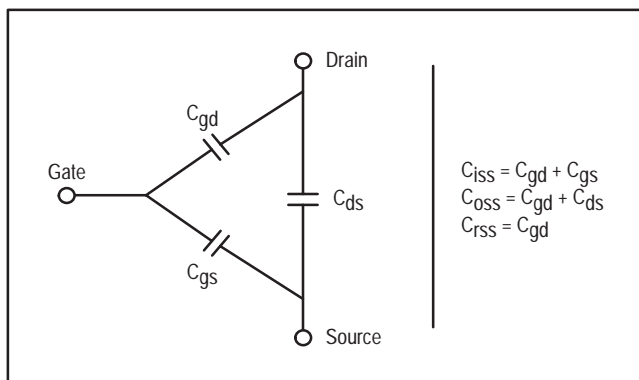
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

BV_{DSS} values for this device are higher than normally required for typical applications. Measurement of BV_{DSS} is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of $10^9 \Omega$ – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 150 \text{ mA}$, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 2°C/W assumes a majority of the 0.065" x 0.180" source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

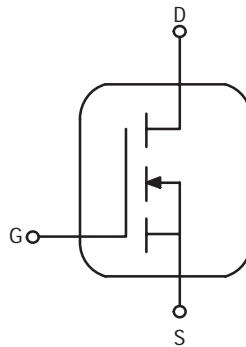
Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFETs

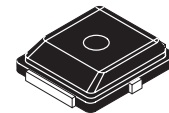
MRF1517T1

The MRF1517T1 is designed for broadband commercial and industrial applications at frequencies to 520 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 7.5 volt portable FM equipment.

- Specified Performance @ 520 MHz, 7.5 Volts
Output Power — 8 Watts
Power Gain — 11 dB
Efficiency — 55%
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- Excellent Thermal Stability
- Capable of Handling 20:1 VSWR, @ 9.5 Vdc, 520 MHz, 2 dB Overdrive
- Broadband UHF/VHF Demonstration Amplifier Information Available Upon Request
- RF Power Plastic Surface Mount Package
- Available in Tape and Reel.
T1 Suffix = 1,000 Units per 12 mm, 7 Inch Reel.



520 MHz, 8 W, 7.5 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 466-02, STYLE 1
(PLD-1.5)
PLASTIC

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage (1)	V _{DSS}	25	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	4	Adc
Total Device Dissipation @ T _C = 25°C (2) Derate above 25°C	P _D	62.5 0.50	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	150	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	2	°C/W

(1) Not designed for 12.5 volt applications.

(2) Calculated based on the formula $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Zero Gate Voltage Drain Current ($V_{DS} = 35\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 10\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc

ON CHARACTERISTICS

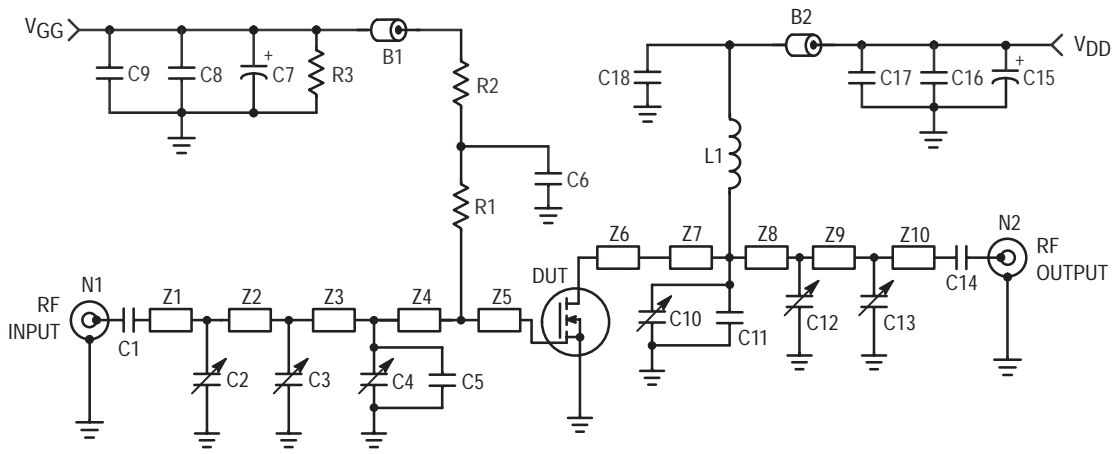
Gate Threshold Voltage ($V_{DS} = 7.5\text{ Vdc}$, $I_D = 120\ \mu\text{Adc}$)	$V_{GS(th)}$	1.0	1.7	2.1	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.5	—	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	g_{fs}	0.9	—	—	S

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 7.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	66	—	pF
Output Capacitance ($V_{DS} = 7.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	38	—	pF
Reverse Transfer Capacitance ($V_{DS} = 7.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	6	—	pF

FUNCTIONAL TESTS (In Motorola Test Fixture)

Common–Source Amplifier Power Gain ($V_{DD} = 7.5\text{ Vdc}$, $P_{out} = 8\text{ Watts}$, $I_{DQ} = 150\text{ mA}$, $f = 520\text{ MHz}$)	G_{ps}	10	11	—	dB
Drain Efficiency ($V_{DD} = 7.5\text{ Vdc}$, $P_{out} = 8\text{ Watts}$, $I_{DQ} = 150\text{ mA}$, $f = 520\text{ MHz}$)	η	50	55	—	%



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R1	15 Ω , 0805 Chip Resistor
C1	300 pF, 100 mil Chip Capacitor	R2	1.0 k Ω , 1/8 W Resistor
C2, C3, C4, C10,	0 to 20 pF, Trimmer Capacitor	R3	33 k Ω , 1/2 W Resistor
C12, C13	0 to 20 pF, Trimmer Capacitor	Z1	0.315" x 0.080" Microstrip
C5, C11	43 pF, 100 mil Chip Capacitor	Z2	1.415" x 0.080" Microstrip
C6, C18	120 pF, 100 mil Chip Capacitor	Z3	0.322" x 0.080" Microstrip
C7, C15	10 μ F, 50 V Electrolytic Capacitor	Z4	0.022" x 0.080" Microstrip
C8, C16	0.1 μ F, 100 mil Chip Capacitor	Z5, Z6	0.260" x 0.223" Microstrip
C9, C17	1,000 pF, 100 mil Chip Capacitor	Z7	0.050" x 0.080" Microstrip
C14	330 pF, 100 mil Chip Capacitor	Z8	0.625" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z9	0.800" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Z10	0.589" x 0.080" Microstrip
		Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 1. 480 – 520 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 480 – 520 MHz

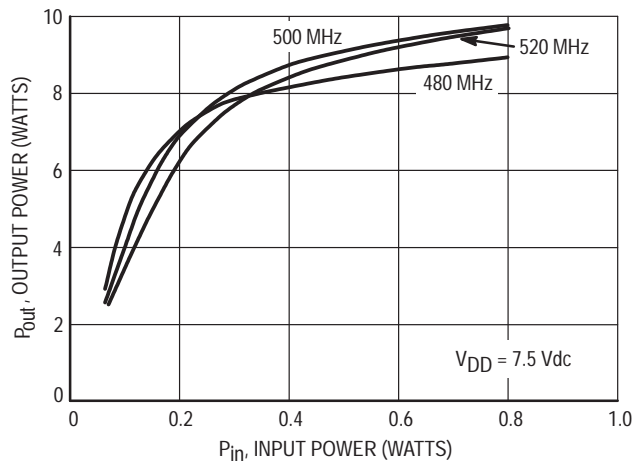


Figure 2. Output Power versus Input Power

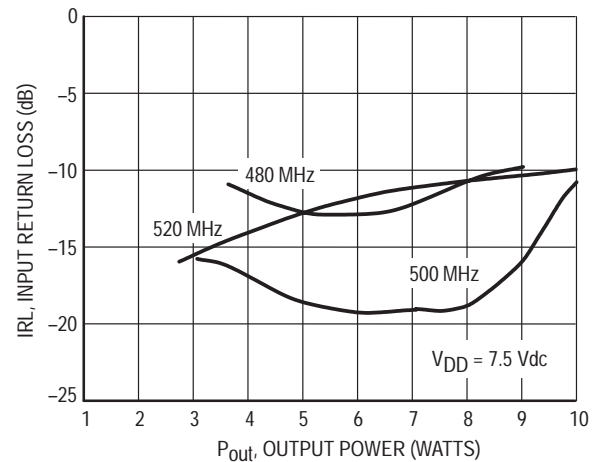


Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 480 – 520 MHz

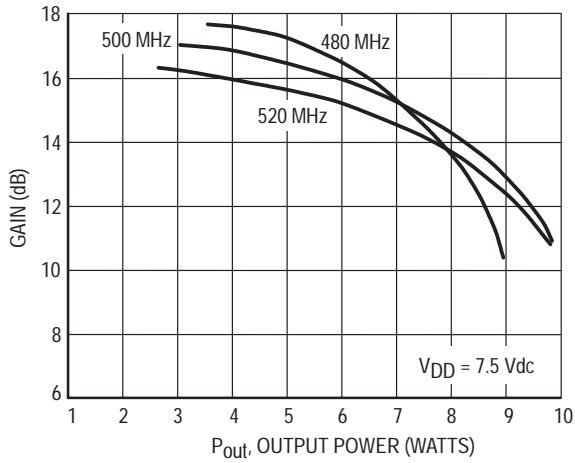


Figure 4. Gain versus Output Power

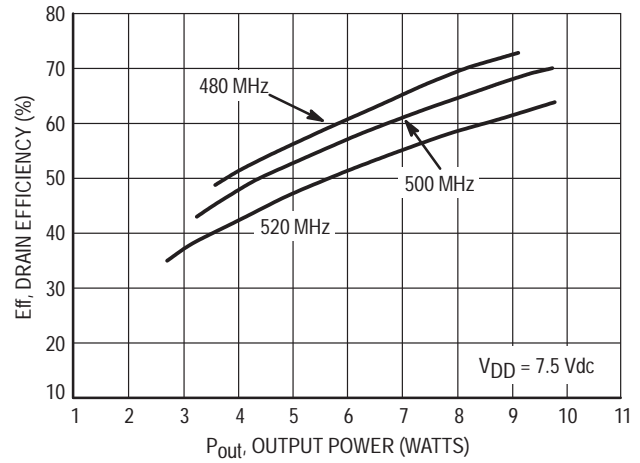


Figure 5. Drain Efficiency versus Output Power

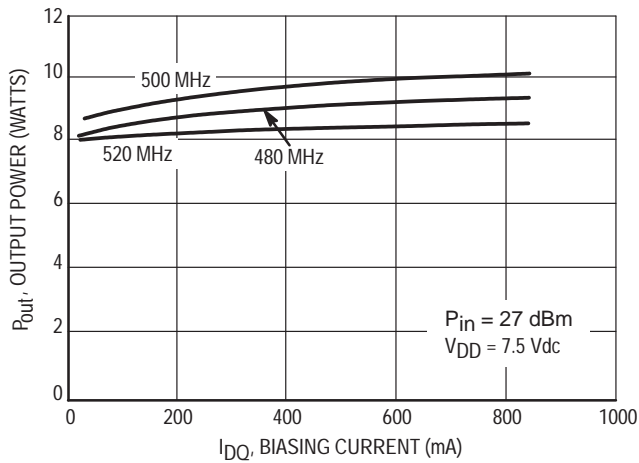


Figure 6. Output Power versus Biasing Current

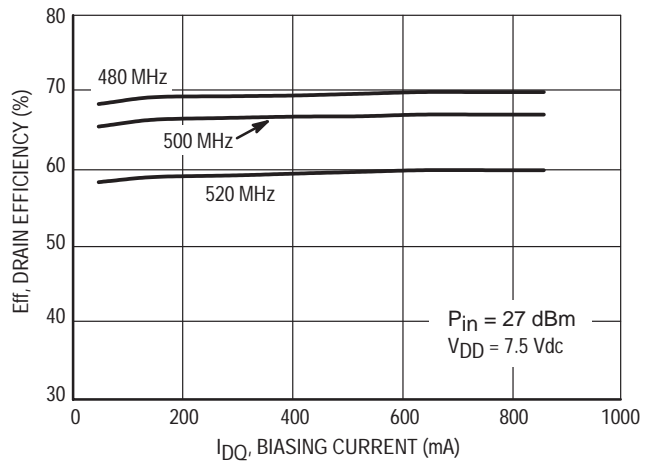


Figure 7. Drain Efficiency versus Biasing Current

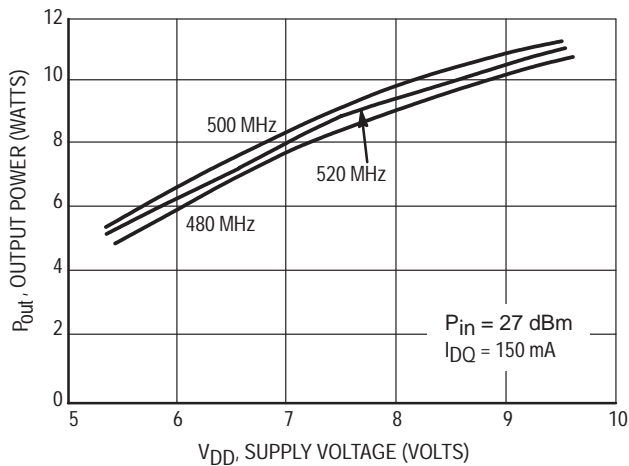


Figure 8. Output Power versus Supply Voltage

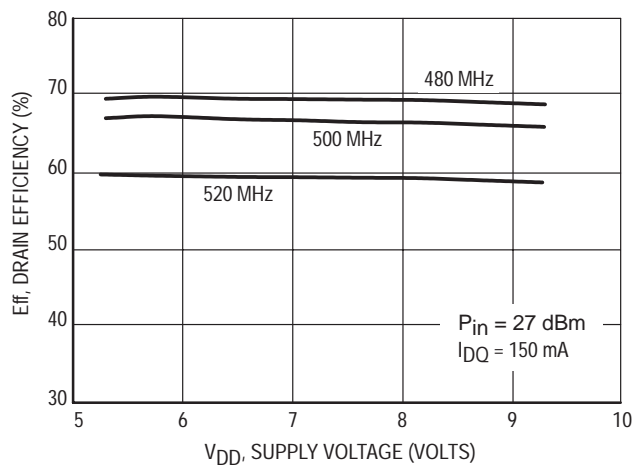
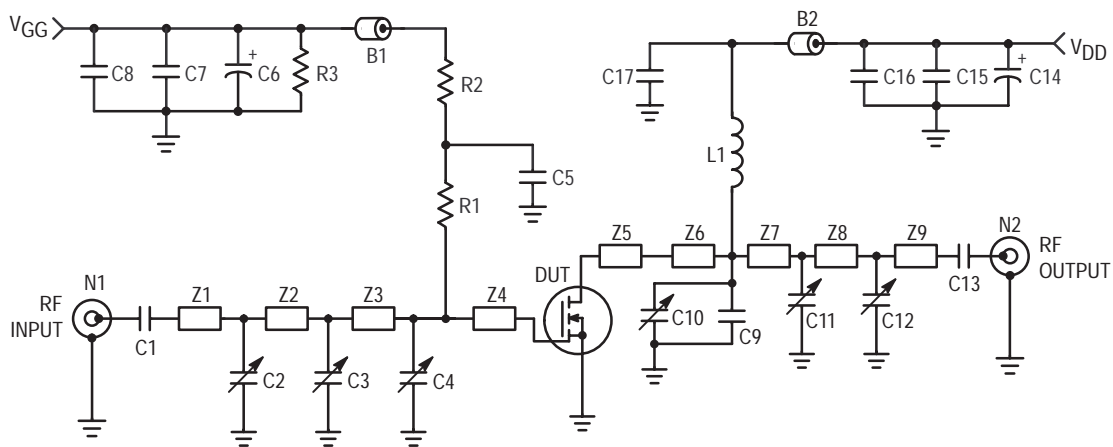


Figure 9. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R1	12 Ω , 0805 Chip Resistor
C1, C13	300 pF, 100 mil Chip Capacitor	R2	1.0 k Ω , 1/8 W Resistor
C2, C3, C4, C10,	0 to 20 pF, Trimmer Capacitor	R3	33 k Ω , 1/2 W Resistor
C11, C12	130 pF, 100 mil Chip Capacitor	Z1	0.617" x 0.080" Microstrip
C5, C17	10 μ F, 50 V Electrolytic Capacitor	Z2	0.723" x 0.080" Microstrip
C6, C14	0.1 μ F, 100 mil Chip Capacitor	Z3	0.513" x 0.080" Microstrip
C7, C15	1,000 pF, 100 mil Chip Capacitor	Z4, Z5	0.260" x 0.223" Microstrip
C8, C16	33 pF, 100 mil Chip Capacitor	Z6	0.048" x 0.080" Microstrip
C9	55.5 nH, 5 Turn, Coilcraft	Z7	0.577" x 0.080" Microstrip
L1	Type N Flange Mount	Z8	1.135" x 0.080" Microstrip
N1, N2		Z9	0.076" x 0.080" Microstrip
		Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 10. 400 – 440 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 400 – 440 MHz

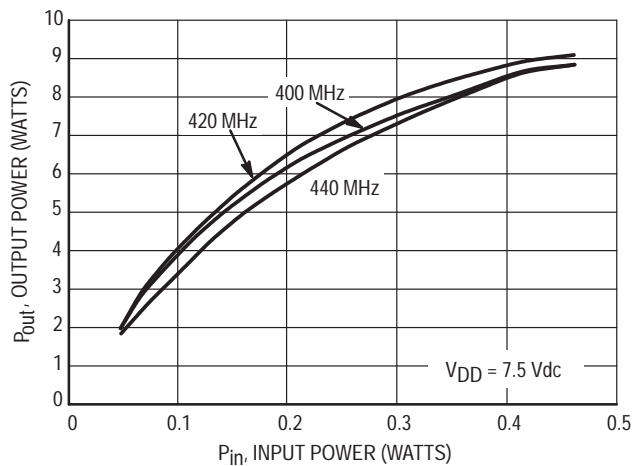


Figure 11. Output Power versus Input Power

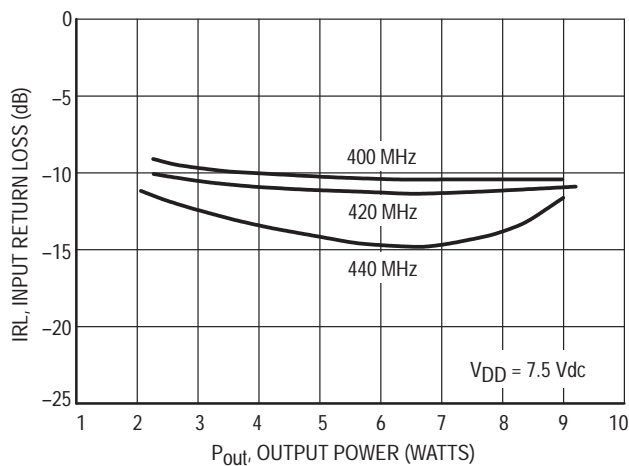


Figure 12. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 400 – 440 MHz

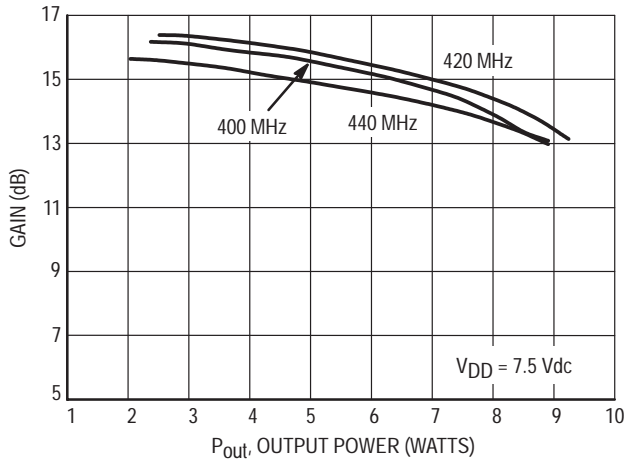


Figure 13. Gain versus Output Power

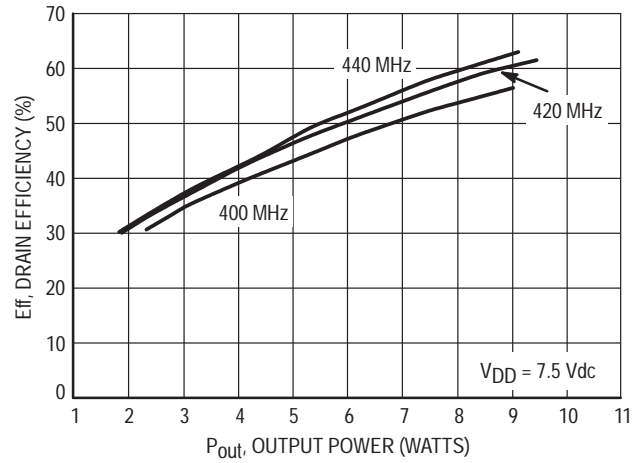


Figure 14. Drain Efficiency versus Output Power

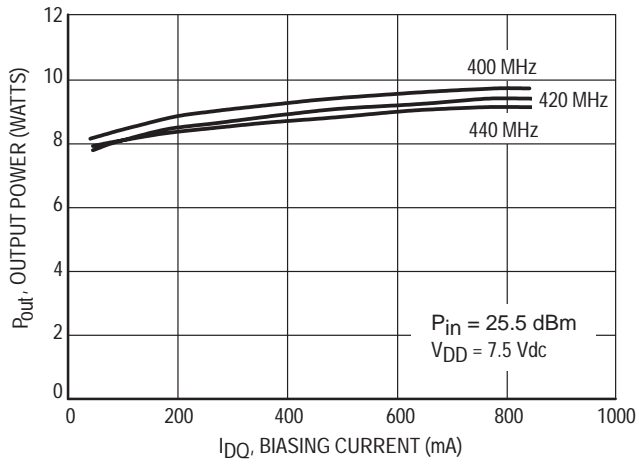


Figure 15. Output Power versus Biasing Current

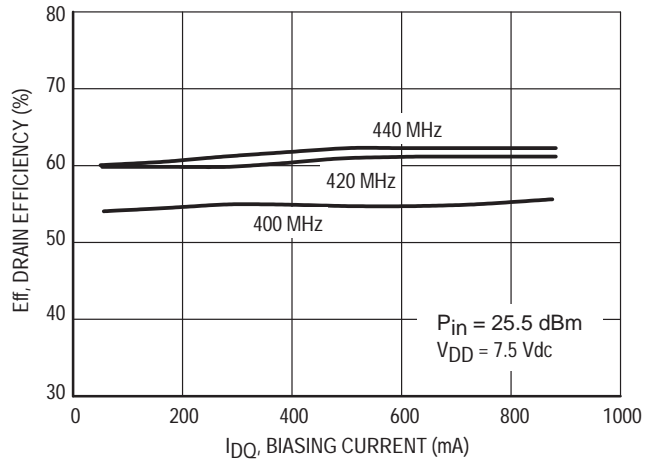


Figure 16. Drain Efficiency versus Biasing Current

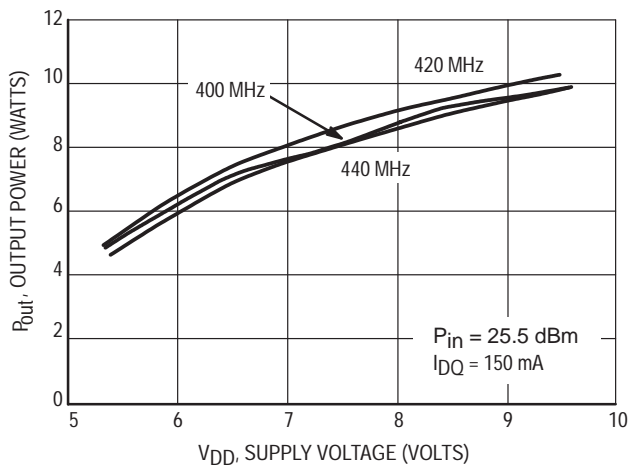


Figure 17. Output Power versus Supply Voltage

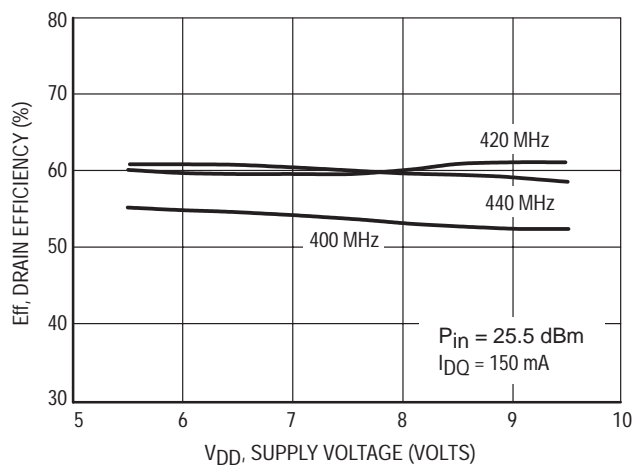
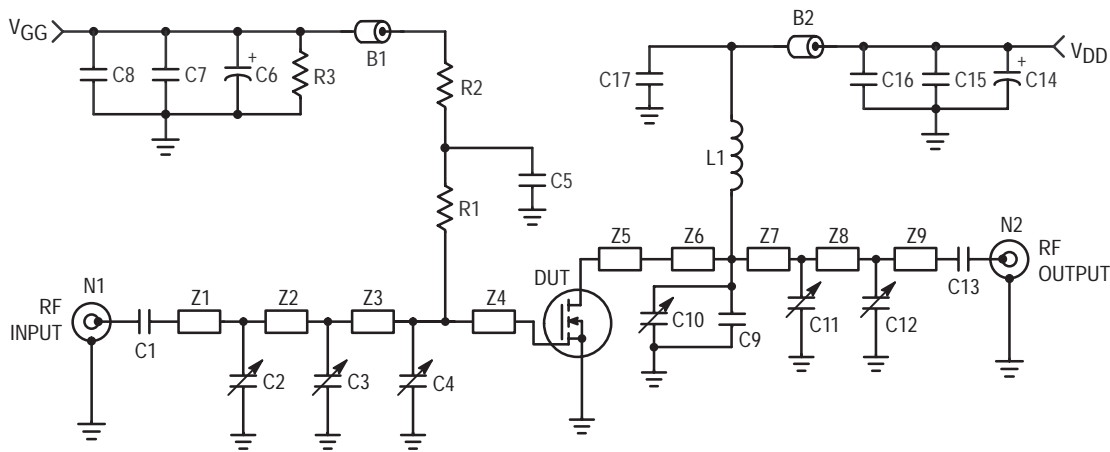


Figure 18. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R1	15 Ω , 0805 Chip Resistor
C1	240 pF, 100 mil Chip Capacitor	R2	1.0 k Ω , 1/8 W Resistor
C2, C3, C4, C10,	0 to 20 pF, Trimmer Capacitor	R3	33 k Ω , 1/2 W Resistor
C11, C12	0 to 20 pF, Trimmer Capacitor	Z1	0.471" x 0.080" Microstrip
C5, C17	130 pF, 100 mil Chip Capacitor	Z2	1.082" x 0.080" Microstrip
C6, C14	10 mF, 50 V Electrolytic Capacitor	Z3	0.372" x 0.080" Microstrip
C7, C15	0.1 mF, 100 mil Chip Capacitor	Z4, Z5	0.260" x 0.223" Microstrip
C8, C16	1,000 pF, 100 mil Chip Capacitor	Z6	0.050" x 0.080" Microstrip
C9	39 pF, 100 mil Chip Capacitor	Z7	0.551" x 0.080" Microstrip
C13	330 pF, 100 mil Chip Capacitor	Z8	0.825" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z9	0.489" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 19. 440 – 480 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 440 – 480 MHz

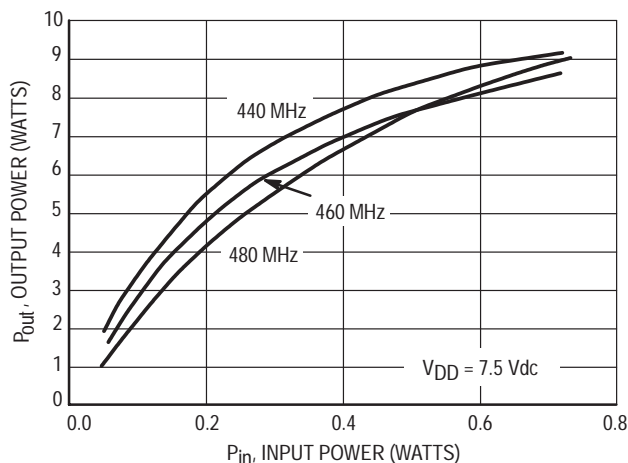


Figure 20. Output Power versus Input Power

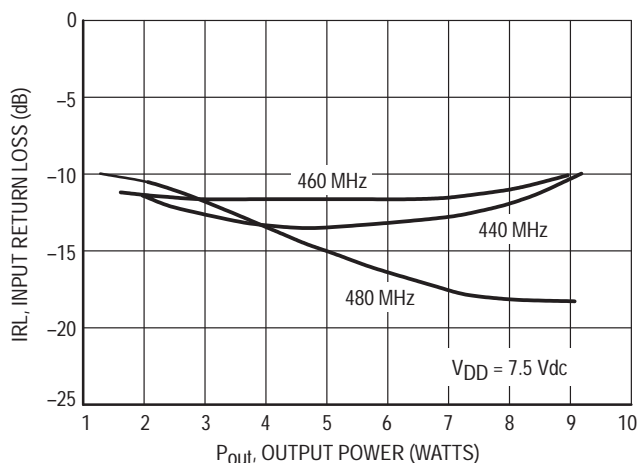


Figure 21. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 440 – 480 MHz

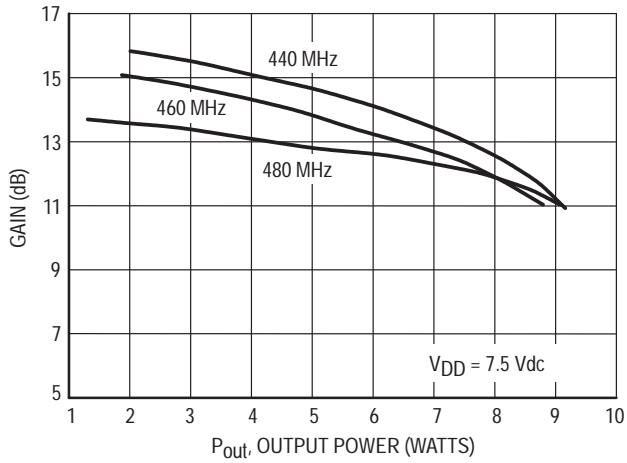


Figure 22. Gain versus Output Power

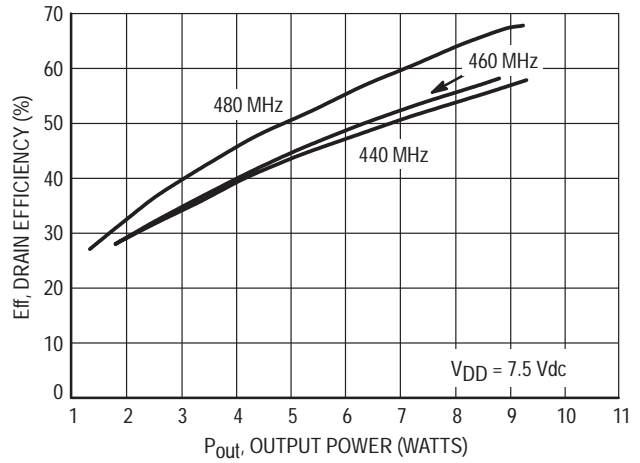


Figure 23. Drain Efficiency versus Output Power

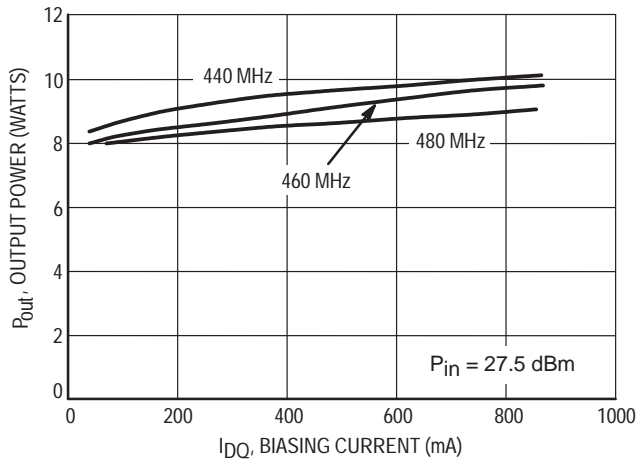


Figure 24. Output Power versus Biasing Current

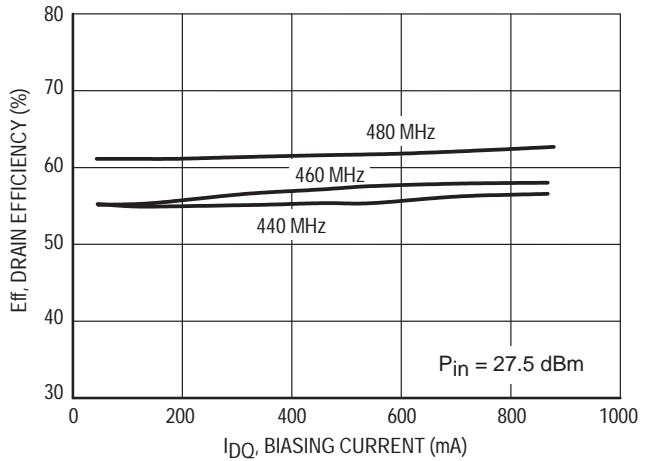


Figure 25. Drain Efficiency versus Biasing Current

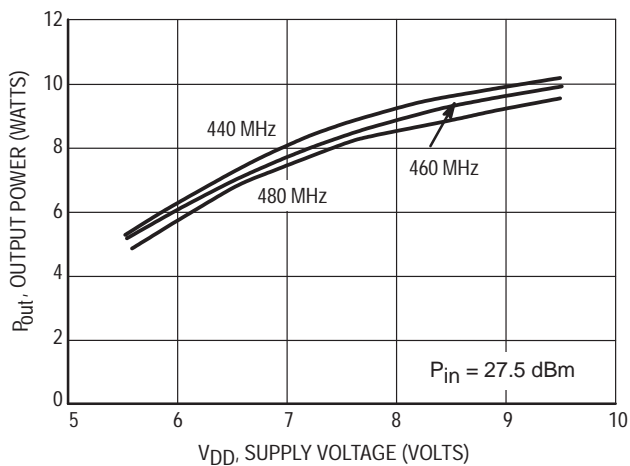


Figure 26. Output Power versus Supply Voltage

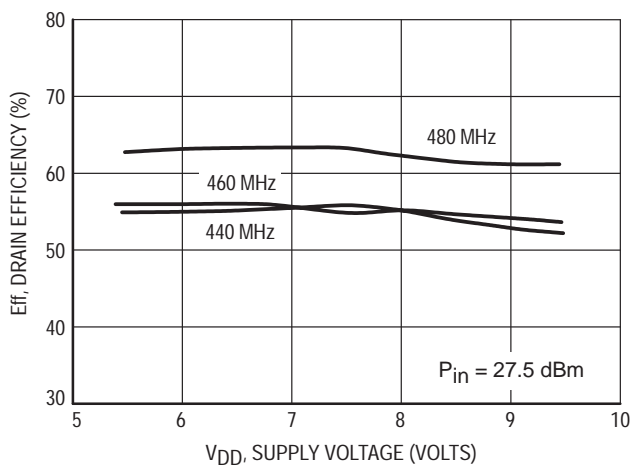
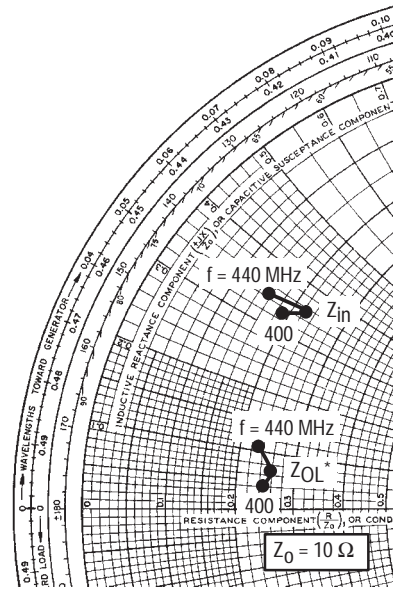
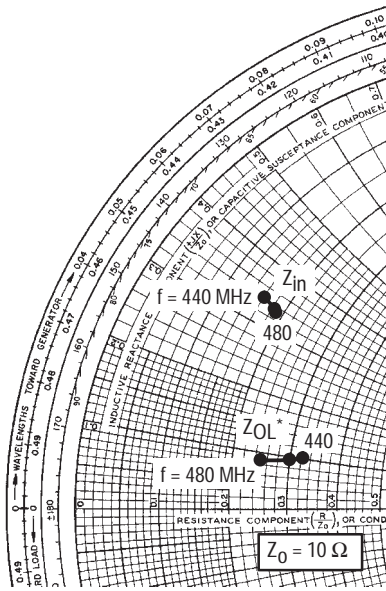
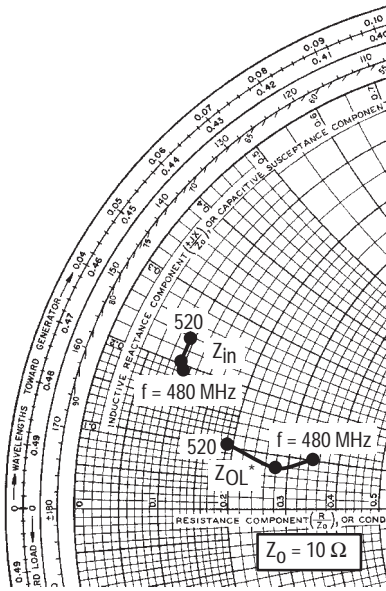


Figure 27. Drain Efficiency versus Supply Voltage



$V_{DD} = 7.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
480	$1.06 + j1.82$	$3.51 + j0.99$
500	$0.97 + j2.01$	$2.82 + j0.75$
520	$0.975 + j2.37$	$1.87 + j1.03$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50\%$.

$V_{DD} = 7.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
440	$1.62 + j3.41$	$3.25 + j0.98$
460	$1.85 + j3.35$	$3.05 + j0.93$
480	$1.91 + j3.31$	$2.54 + j0.84$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50\%$.

$V_{DD} = 7.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
400	$1.96 + j3.32$	$2.52 + j0.39$
420	$2.31 + j3.56$	$2.61 + j0.64$
440	$1.60 + j3.45$	$2.37 + j1.04$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50\%$.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

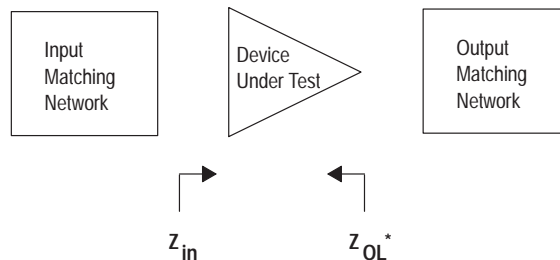


Figure 28. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ($V_{DD} = 7.5$ Vdc)

$I_{DQ} = 150$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.84	-152	17.66	97	0.016	0	0.77	-167
100	0.84	-164	8.86	85	0.016	5	0.78	-172
200	0.86	-170	4.17	72	0.015	-5	0.79	-173
300	0.88	-171	2.54	62	0.014	-8	0.80	-172
400	0.90	-172	1.72	55	0.013	-25	0.83	-172
500	0.92	-172	1.28	50	0.013	-10	0.84	-172
600	0.94	-173	0.98	46	0.014	-22	0.86	-171
700	0.95	-173	0.76	41	0.010	-30	0.86	-172
800	0.96	-174	0.61	38	0.011	-14	0.86	-171
900	0.96	-175	0.50	33	0.011	-31	0.85	-172
1000	0.97	-175	0.40	31	0.006	55	0.88	-171

$I_{DQ} = 800$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.90	-165	20.42	94	0.018	1	0.76	-164
100	0.89	-172	10.20	87	0.015	-7	0.77	-170
200	0.90	-175	4.96	79	0.015	-12	0.77	-172
300	0.90	-176	3.17	73	0.017	-2	0.80	-171
400	0.91	-176	2.26	67	0.013	1	0.82	-172
500	0.92	-176	1.75	63	0.011	-6	0.83	-171
600	0.93	-176	1.39	59	0.012	-31	0.85	-171
700	0.94	-176	1.14	55	0.015	-34	0.88	-171
800	0.94	-176	0.93	51	0.008	-22	0.87	-171
900	0.95	-177	0.78	45	0.007	2	0.87	-172
1000	0.96	-177	0.65	43	0.008	-40	0.90	-170

$I_{DQ} = 1.5$ A

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.92	-165	19.90	95	0.017	3	0.76	-164
100	0.90	-172	9.93	88	0.018	2	0.77	-170
200	0.91	-176	4.84	80	0.016	-4	0.77	-172
300	0.91	-176	3.10	74	0.014	-11	0.80	-172
400	0.92	-176	2.22	68	0.014	-14	0.81	-172
500	0.93	-176	1.73	64	0.016	-8	0.83	-171
600	0.94	-176	1.39	61	0.013	-24	0.85	-171
700	0.94	-176	1.12	56	0.013	-24	0.87	-171
800	0.95	-176	0.93	52	0.009	-12	0.87	-171
900	0.96	-177	0.78	46	0.008	10	0.87	-173
1000	0.97	-177	0.64	44	0.012	4	0.89	-169

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

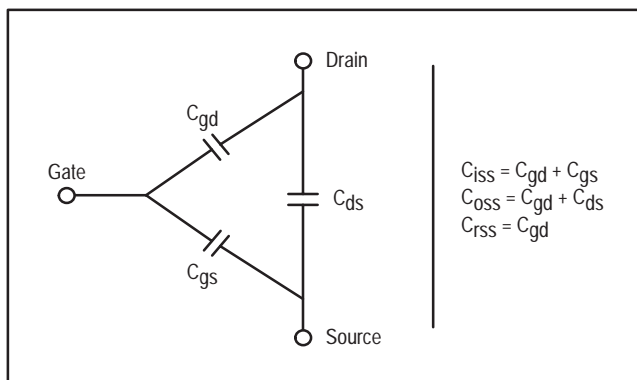
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

BV_{DSS} values for this device are higher than normally required for typical applications. Measurement of BV_{DSS} is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of $10^9 \Omega$ – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 150 \text{ mA}$, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 2°C/W assumes a majority of the 0.065" x 0.180" source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

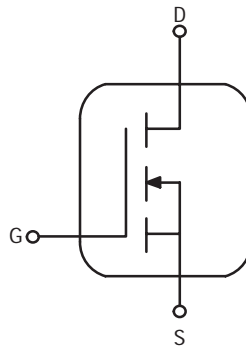
Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

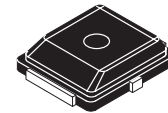
The MRF1518T1 is designed for broadband commercial and industrial applications at frequencies to 520 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 12.5 volt mobile FM equipment.

- Specified Performance @ 520 MHz, 12.5 Volts
Output Power — 8 Watts
Power Gain — 11 dB
Efficiency — 55%
- Capable of Handling 20:1 VSWR, @ 15.5 Vdc, 520 MHz, 2 dB Overdrive
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- RF Power Plastic Surface Mount Package
- Broadband UHF/VHF Demonstration Amplifier Information Available Upon Request
- Available in Tape and Reel. T1 Suffix = 1,000 Units per 12 mm, 7 Inch Reel.



MRF1518T1

**520 MHz, 8 W, 12.5 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET**



**CASE 466-02, STYLE 1
(PLD-1.5)**

PLASTIC

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	40	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	4	Adc
Total Device Dissipation @ T _C = 25°C (1) Derate above 25°C	P _D	62.5 0.50	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	150	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	2	°C/W

(1) Calculated based on the formula $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Zero Gate Voltage Drain Current ($V_{DS} = 40\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 10\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc

ON CHARACTERISTICS

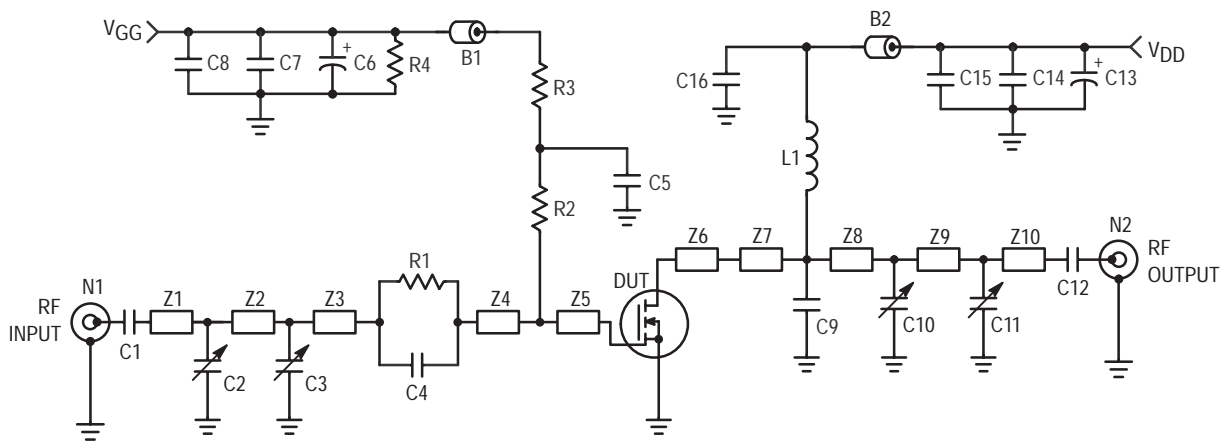
Gate Threshold Voltage ($V_{DS} = 12.5\text{ Vdc}$, $I_D = 100\ \mu\text{A}$)	$V_{GS(th)}$	1.0	1.6	2.1	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.4	—	Vdc

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	66	—	pF
Output Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	33	—	pF
Reverse Transfer Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	4.5	—	pF

FUNCTIONAL TESTS (In Motorola Test Fixture)

Common–Source Amplifier Power Gain ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 8\text{ Watts}$, $I_{DQ} = 150\text{ mA}$, $f = 520\text{ MHz}$)	G_{ps}	10	11	—	dB
Drain Efficiency ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 8\text{ Watts}$, $I_{DQ} = 150\text{ mA}$, $f = 520\text{ MHz}$)	η	50	55	—	%



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R4	33 k Ω , 1/8 W Resistor
C1, C14	240 pF, 100 mil Chip Capacitor	Z1	0.451" x 0.080" Microstrip
C2, C3, C10, C11	0 to 20 pF, Trimmer Capacitor	Z2	1.005" x 0.080" Microstrip
C4	82 pF, 100 mil Chip Capacitor	Z3	0.020" x 0.080" Microstrip
C5, C16	120 pF, 100 mil Chip Capacitor	Z4	0.155" x 0.080" Microstrip
C6, C13	10 μ F, 50 V Electrolytic Capacitor	Z5, Z6	0.260" x 0.223" Microstrip
C7, C14	1,200 pF, 100 mil Chip Capacitor	Z7	0.065" x 0.080" Microstrip
C8, C15	0.1 μ F, 100 mil Chip Capacitor	Z8	0.266" x 0.080" Microstrip
C9	30 pF, 100 mil Chip Capacitor	Z9	1.113" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z10	0.433" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Board	Glass Teflon [®] , 31 mils, 2 oz. Copper
R1	15 Ω , 0805 Chip Resistor		
R2	51 Ω , 1/2 W Resistor		
R3	10 Ω , 0805 Chip Resistor		

Figure 1. 450 – 520 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 450 – 520 MHz

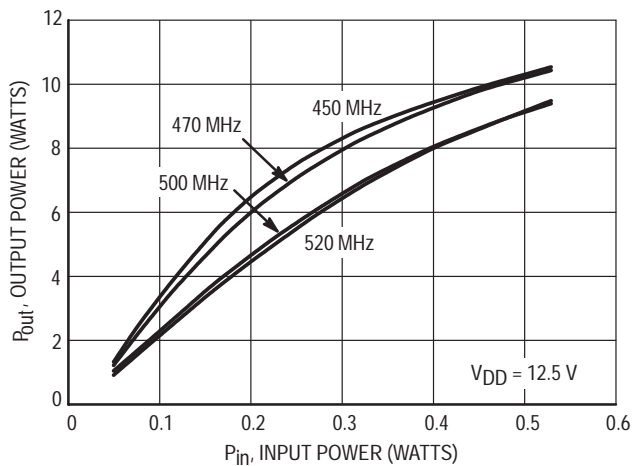


Figure 2. Output Power versus Input Power

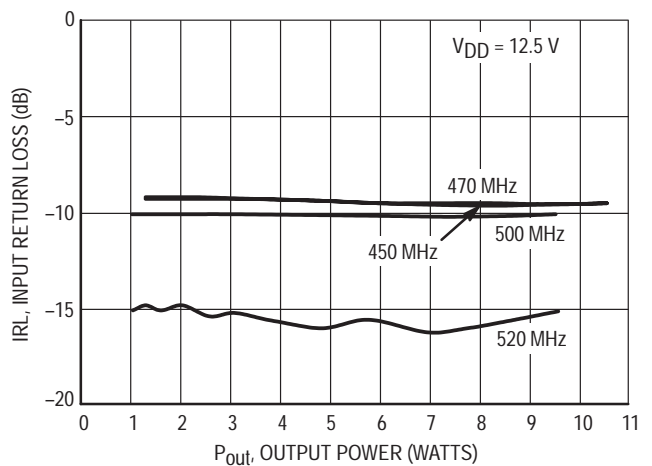


Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 450 – 520 MHz

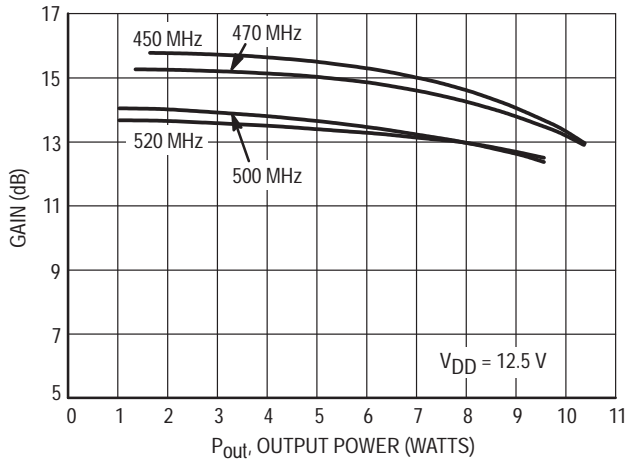


Figure 4. Gain versus Output Power

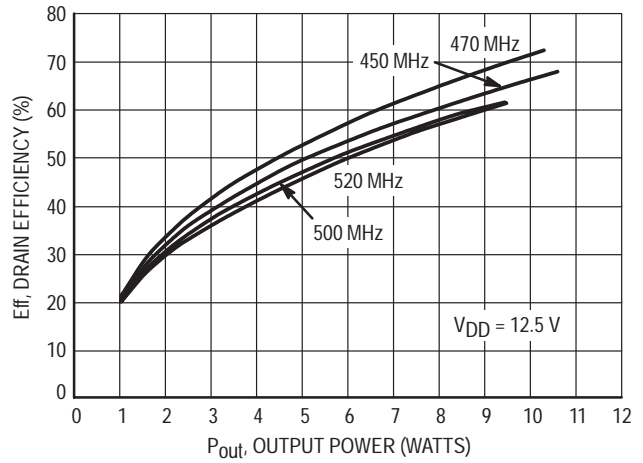


Figure 5. Drain Efficiency versus Output Power

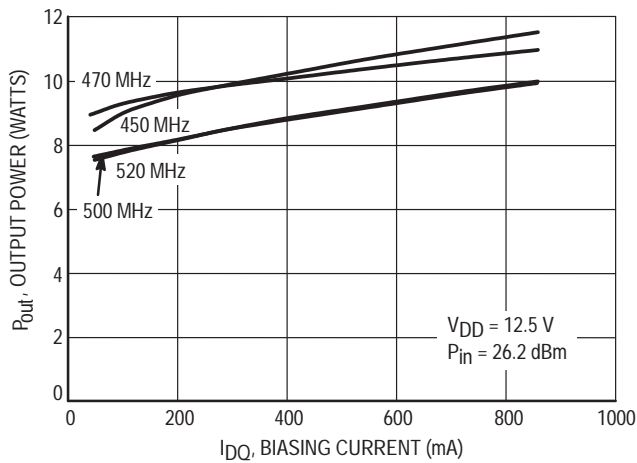


Figure 6. Output Power versus Biasing Current

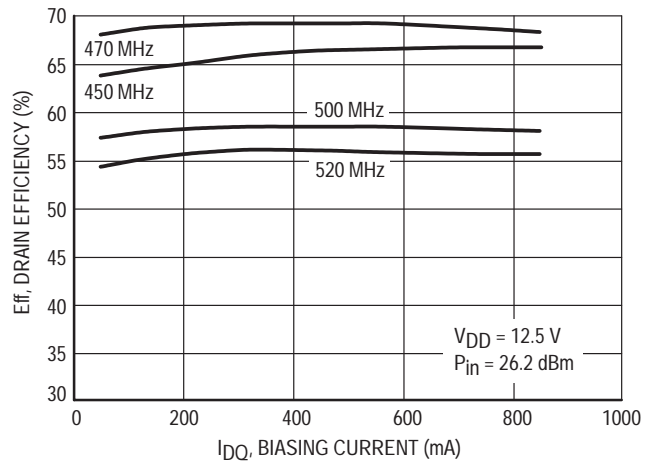


Figure 7. Drain Efficiency versus Biasing Current

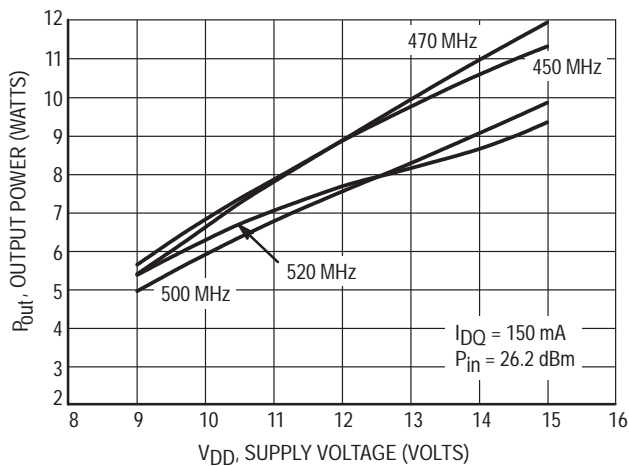


Figure 8. Output Power versus Supply Voltage

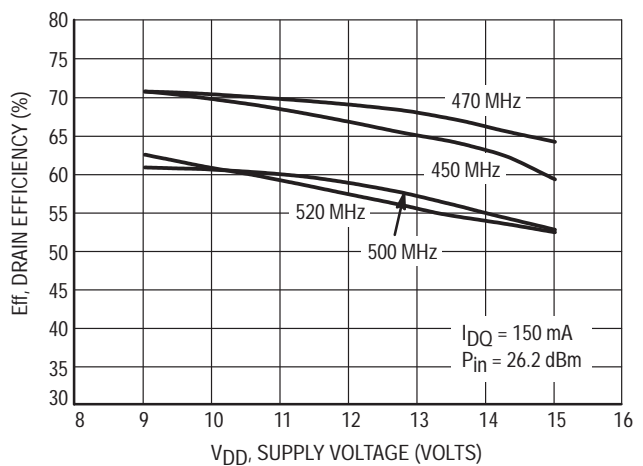
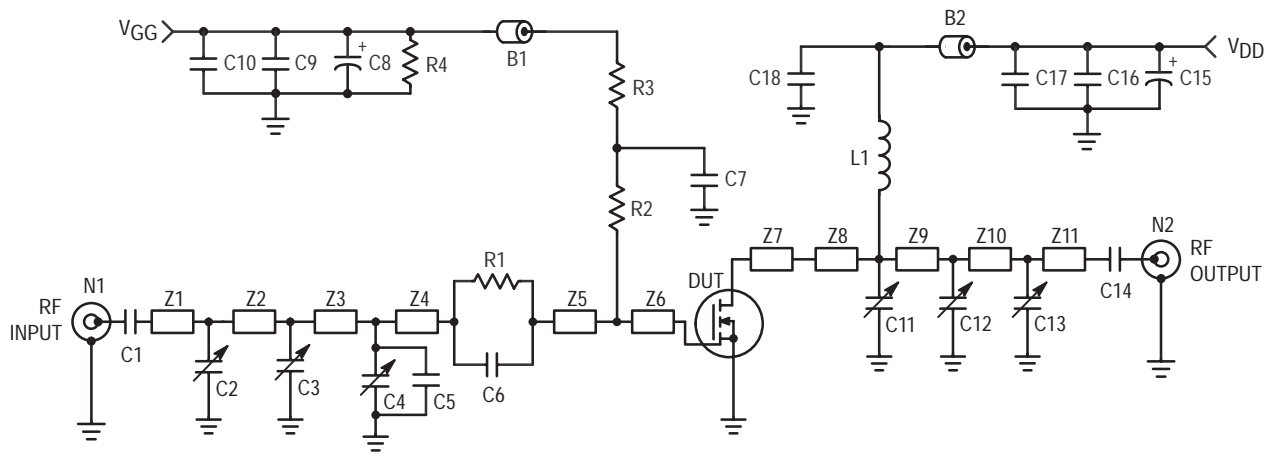


Figure 9. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R3	10 Ω , 0805 Chip Resistor
C1, C14	240 pF, 100 mil Chip Capacitor	R4	33 k Ω , 1/8 W Resistor
C2, C3, C4, C11,	0 to 20 pF, Trimmer Capacitor	Z1	0.476" x 0.080" Microstrip
C12, C13		Z2	0.724" x 0.080" Microstrip
C5	30 pF, 100 mil Chip Capacitor	Z3	0.348" x 0.080" Microstrip
C6	47 pF, 100 mil Chip Capacitor	Z4	0.048" x 0.080" Microstrip
C7, C18	120 pF, 100 mil Chip Capacitor	Z5	0.175" x 0.080" Microstrip
C8, C15	10 μ F, 50 V Electrolytic Capacitor	Z6, Z7	0.260" x 0.223" Microstrip
C9, C16	1,200 pF, 100 mil Chip Capacitor	Z8	0.239" x 0.080" Microstrip
C10, C17	0.1 μ F, 100 mil Chip Capacitor	Z9	0.286" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z10	0.806" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Z11	0.553" x 0.080" Microstrip
R1	15 Ω , 0805 Chip Resistor	Board	Glass Teflon [®] , 31 mils, 2 oz. Copper
R2	51 Ω , 1/2 W Resistor		

Figure 10. 400 – 470 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 400 – 470 MHz

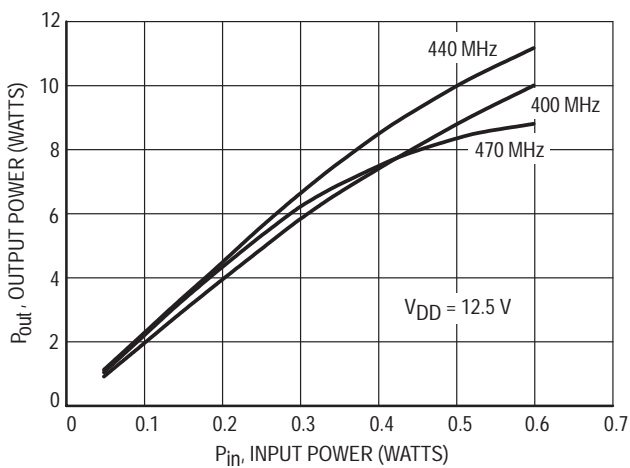


Figure 11. Output Power versus Input Power

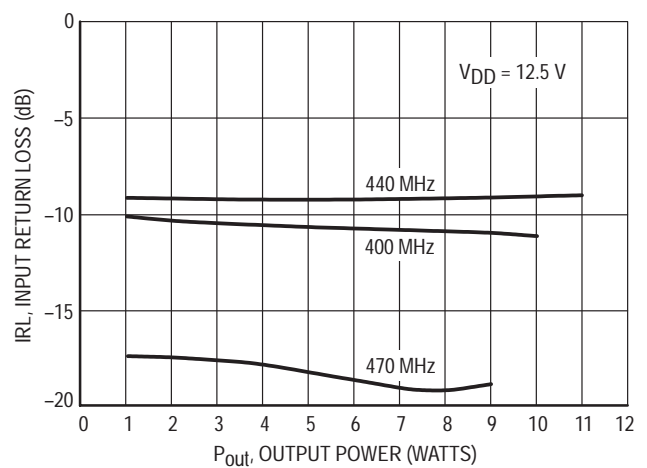


Figure 12. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 400 – 470 MHz

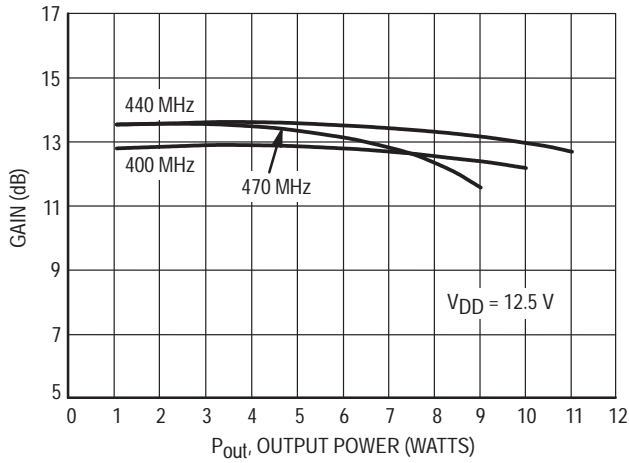


Figure 13. Gain versus Output Power

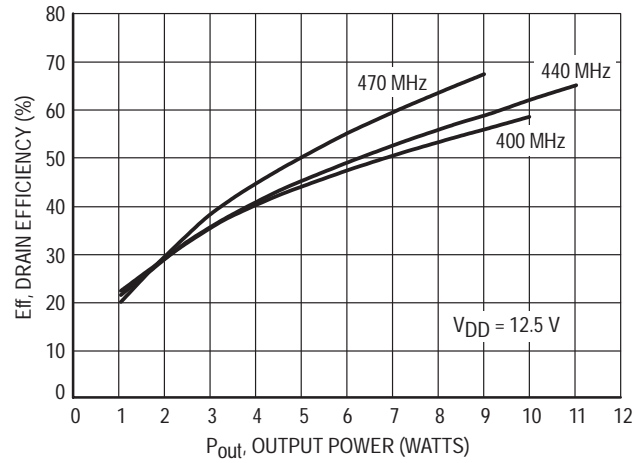


Figure 14. Drain Efficiency versus Output Power

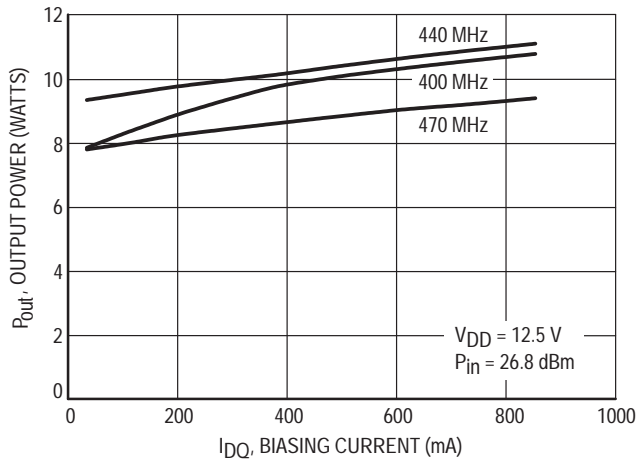


Figure 15. Output Power versus Biasing Current

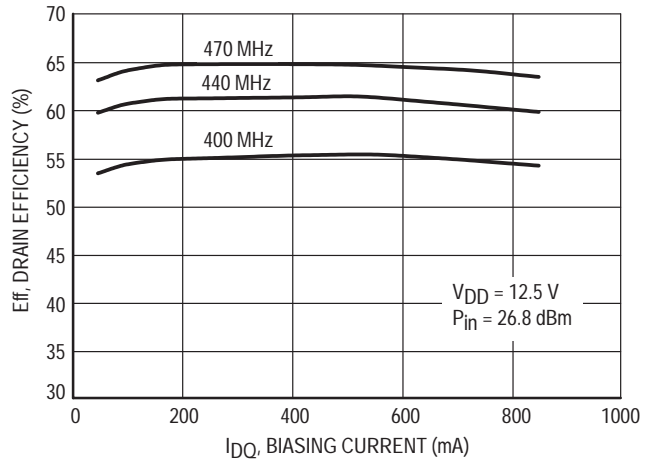


Figure 16. Drain Efficiency versus Biasing Current

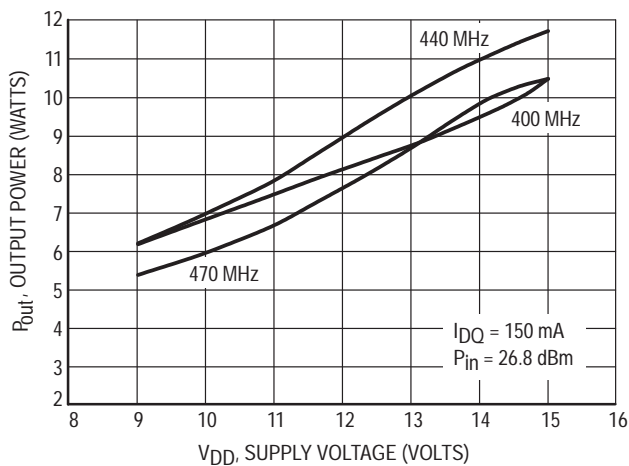


Figure 17. Output Power versus Supply Voltage

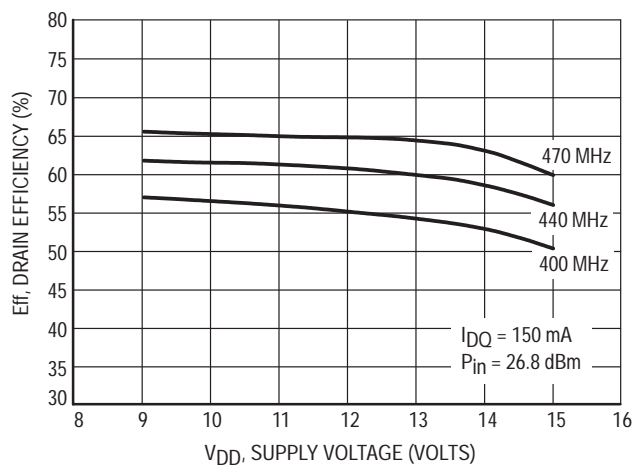
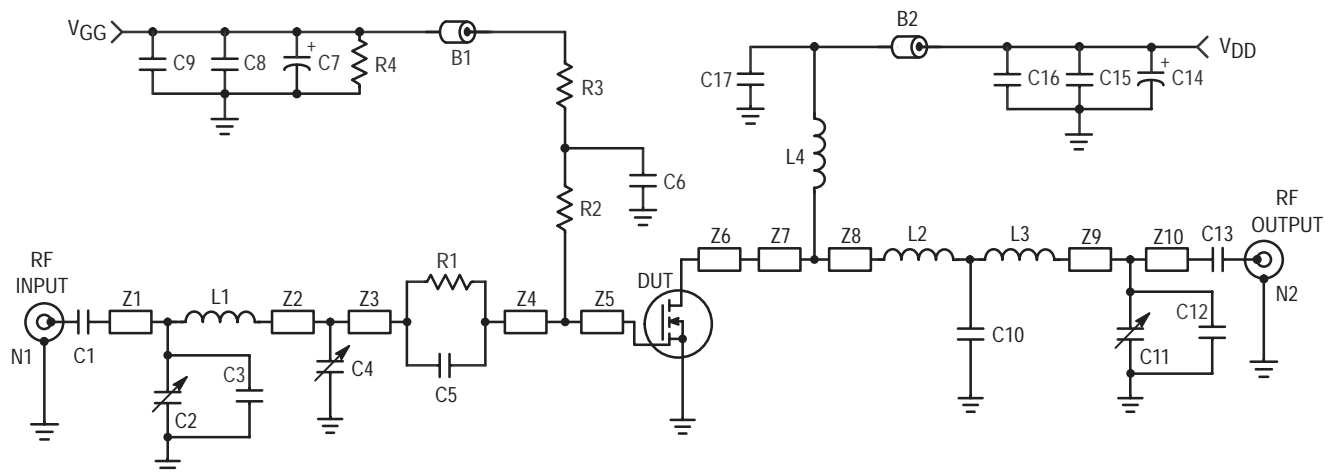


Figure 18. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	L4	55.5 nH, 5 Turn, Coilcraft
C1, C13	330 pF, 100 mil Chip Capacitor	N1, N2	Type N Flange Mount
C2, C4, C11	0 to 20 pF, Trimmer Capacitor	R1	15 Ω , 0805 Chip Resistor
C3	12 pF, 100 mil Chip Capacitor	R2	56 Ω , 1/4 W Carbon Resistor
C5	43 pF, 100 mil Chip Capacitor	R3	100 Ω , 0805 Chip Resistor
C6, C17	75 pF, 100 mil Chip Capacitor	R4	33 k Ω , 1/8 W Carbon Resistor
C7, C14	10 μ F, 50 V Electrolytic Capacitor	Z1	0.115" x 0.080" Microstrip
C8, C15	1,200 pF, 100 mil Chip Capacitor	Z2	0.255" x 0.080" Microstrip
C9, C16	0.1 μ F, 100 mil Chip Capacitor	Z3	1.037" x 0.080" Microstrip
C10	75 pF, 100 mil Chip Capacitor	Z4	0.192" x 0.080" Microstrip
C12	13 pF, 100 mil Chip Capacitor	Z5, Z6	0.260" x 0.223" Microstrip
L1	26 nH, 4 Turn, Coilcraft	Z7	0.125" x 0.080" Microstrip
L2	5 nH, 2 Turn, Coilcraft	Z8	0.962" x 0.080" Microstrip
L3	33 nH, 5 Turn, Coilcraft	Z9	0.305" x 0.080" Microstrip
		Z10	0.155" x 0.080" Microstrip
		Board	Glass Teflon [®] , 31 mils, 2 oz. Copper

Figure 19. 135 – 175 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 135 – 175 MHz

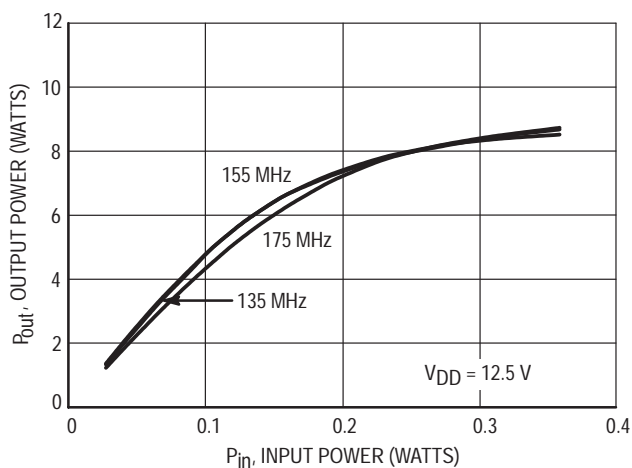


Figure 20. Output Power versus Input Power

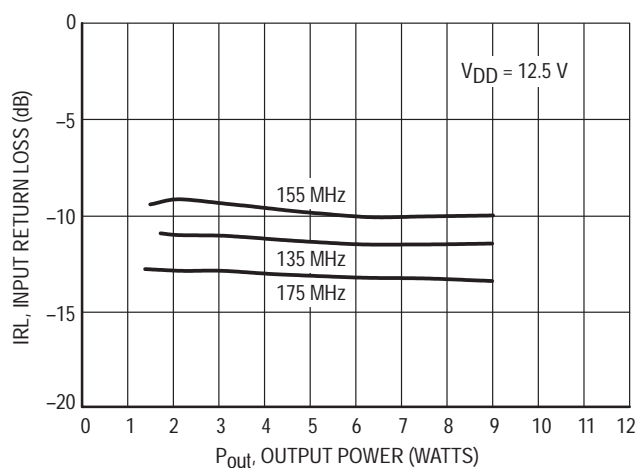


Figure 21. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 135 – 175 MHz

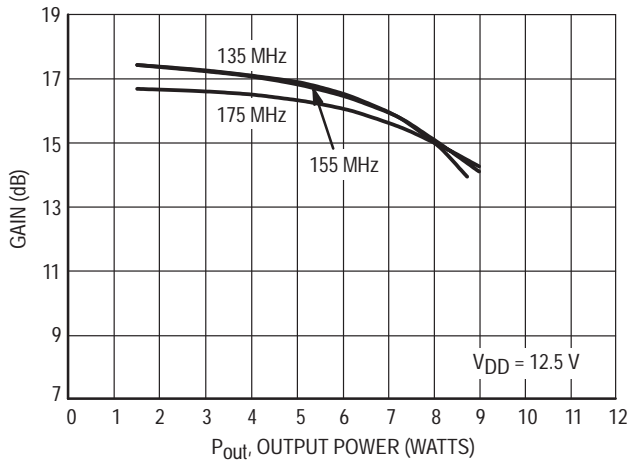


Figure 22. Gain versus Output Power

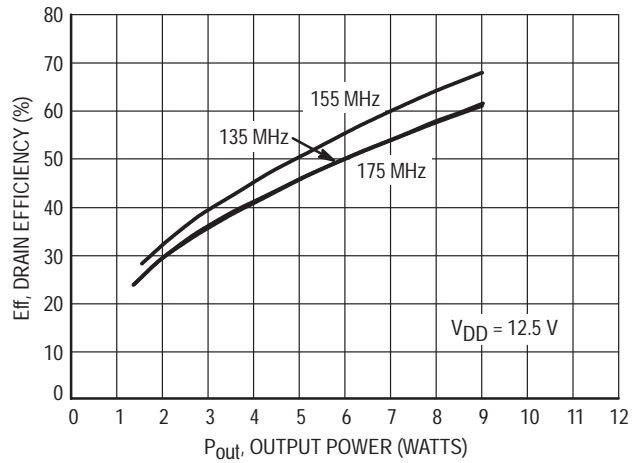


Figure 23. Drain Efficiency versus Output Power

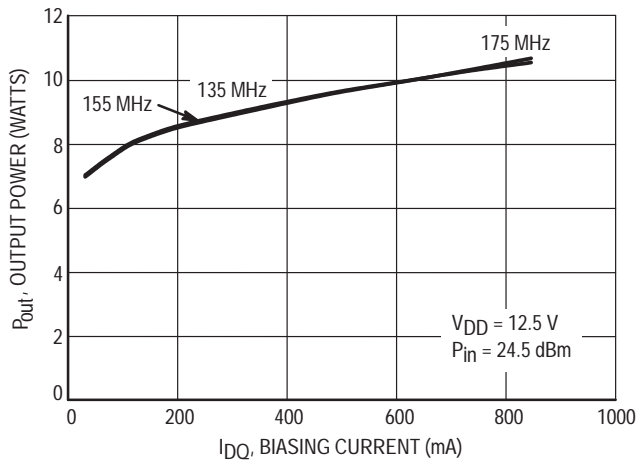


Figure 24. Output Power versus Biasing Current

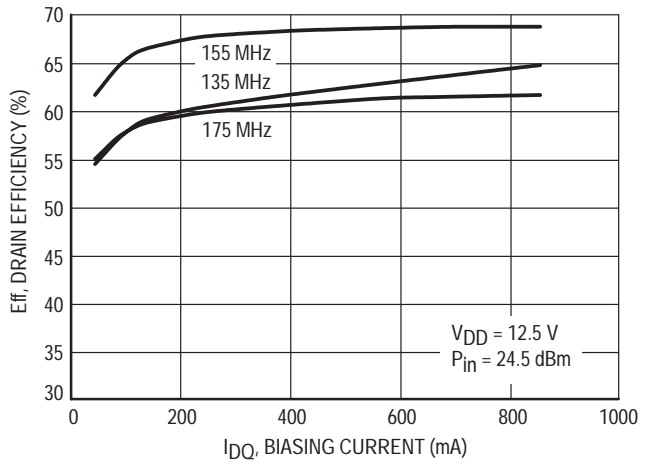


Figure 25. Drain Efficiency versus Biasing Current

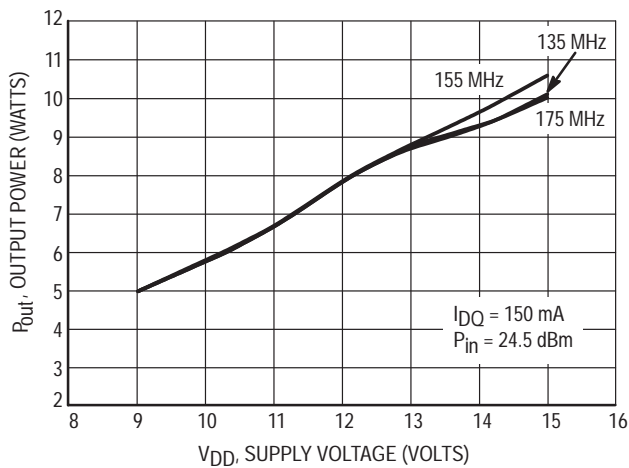


Figure 26. Output Power versus Supply Voltage

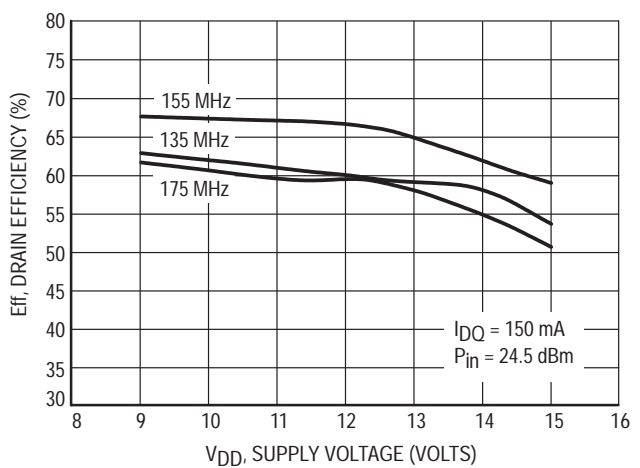
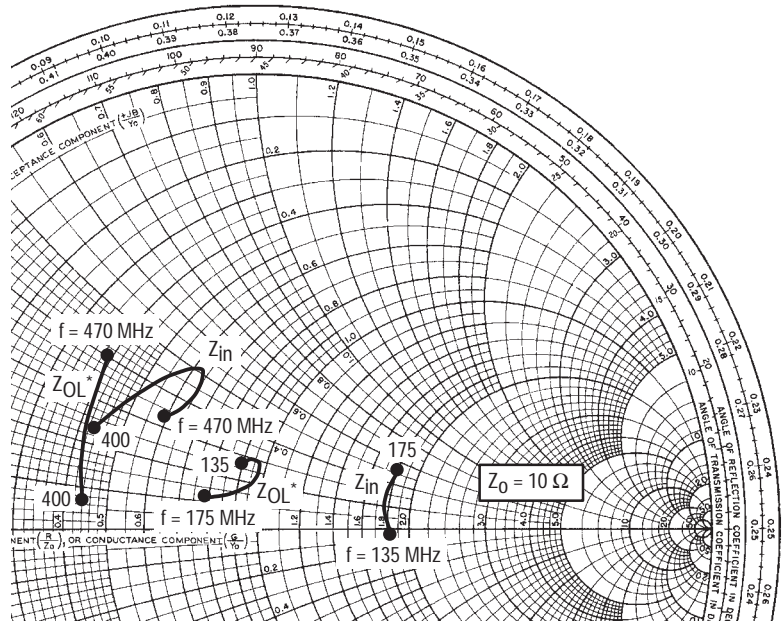
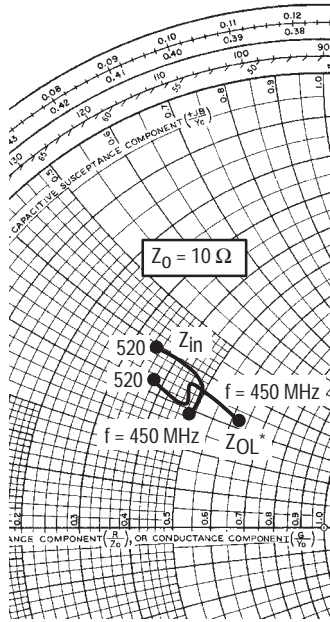


Figure 27. Drain Efficiency versus Supply Voltage



$V_{DD} = 12.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
450	$4.9 + j2.85$	$6.42 + j3.23$
470	$4.85 + j3.71$	$4.59 + j3.61$
500	$4.63 + j3.84$	$4.72 + j3.12$
520	$3.52 + j3.92$	$3.81 + j3.27$

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 82 pF capacitor in series with gate. (See Figure 1).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

$V_{DD} = 12.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
400	$4.28 + j2.36$	$4.41 + j0.67$
440	$6.45 + j5.13$	$4.14 + j2.53$
470	$5.91 + j3.34$	$3.92 + j4.02$

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 47 pF capacitor in series with gate. (See Figure 10).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

$V_{DD} = 12.5 \text{ V}$, $I_{DQ} = 150 \text{ mA}$, $P_{out} = 8 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
135	$18.31 - j0.76$	$8.97 + j2.62$
155	$17.72 + j1.85$	$9.69 + j2.81$
175	$18.06 + j5.23$	$7.94 + j1.14$

Z_{in} = Complex conjugate of source impedance with parallel 15Ω resistor and 43 pF capacitor in series with gate. (See Figure 19).

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

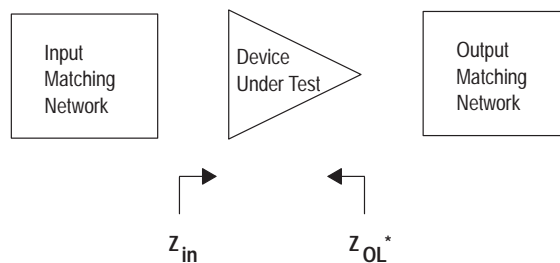


Figure 28. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ($V_{DD} = 12.5$ Vdc)

$I_{DQ} = 150$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.88	-148	18.91	99	0.033	11	0.67	-144
100	0.85	-163	9.40	86	0.033	-6	0.66	-158
200	0.85	-170	4.47	73	0.026	-17	0.69	-162
300	0.87	-171	2.72	64	0.025	-28	0.74	-163
400	0.88	-172	1.85	56	0.021	-21	0.79	-164
500	0.90	-173	1.35	52	0.019	-30	0.83	-165
600	0.92	-173	1.04	47	0.014	-26	0.85	-167
700	0.93	-174	0.83	44	0.015	-39	0.88	-168
800	0.94	-175	0.68	39	0.014	-31	0.90	-169
900	0.94	-175	0.55	36	0.010	-41	0.91	-170
1000	0.96	-176	0.46	30	0.011	-38	0.95	-170

$I_{DQ} = 800$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.90	-159	20.80	97	0.020	14	0.73	-162
100	0.88	-169	10.35	88	0.018	1	0.74	-169
200	0.88	-174	5.09	79	0.017	-9	0.75	-171
300	0.89	-175	3.23	73	0.015	-18	0.77	-171
400	0.89	-175	2.30	67	0.015	-17	0.80	-171
500	0.90	-176	1.74	63	0.014	-22	0.82	-170
600	0.91	-176	1.39	59	0.014	-19	0.83	-171
700	0.92	-176	1.16	55	0.009	-23	0.85	-171
800	0.93	-176	0.96	50	0.011	-14	0.87	-172
900	0.94	-177	0.80	46	0.007	4	0.88	-173
1000	0.94	-177	0.67	41	0.010	-15	0.89	-173

$I_{DQ} = 1.5$ A

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.91	-159	20.18	97	0.015	11	0.73	-165
100	0.89	-169	10.05	89	0.016	-5	0.74	-171
200	0.88	-174	4.93	80	0.015	-3	0.75	-172
300	0.89	-175	3.14	73	0.014	-14	0.78	-172
400	0.89	-176	2.24	67	0.014	-20	0.80	-171
500	0.90	-176	1.70	64	0.014	-22	0.82	-170
600	0.92	-176	1.36	59	0.010	-16	0.84	-171
700	0.92	-176	1.13	55	0.013	-10	0.85	-171
800	0.93	-177	0.94	50	0.008	-13	0.87	-172
900	0.94	-177	0.78	46	0.013	-26	0.87	-173
1000	0.94	-178	0.65	41	0.007	8	0.87	-172

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

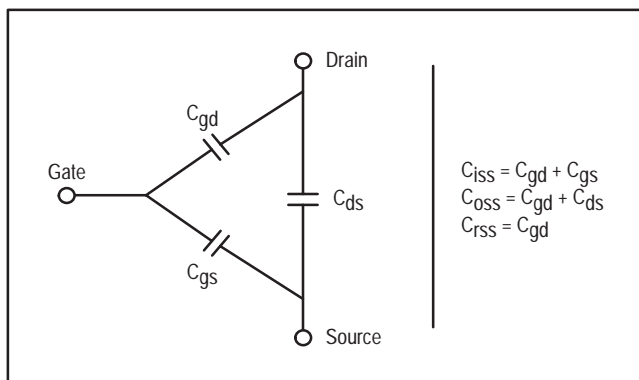
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

BV_{DSS} values for this device are higher than normally required for typical applications. Measurement of BV_{DSS} is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of $10^9 \Omega$ – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 150 \text{ mA}$, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 2°C/W assumes a majority of the 0.065" x 0.180" source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

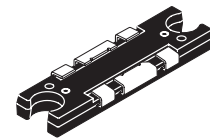
Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

MRF1535T1

520 MHz, 35 W, 12.5 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 1264-06, STYLE 1
(TO-272)

PLASTIC

The MRF1535T1 is designed for broadband commercial and industrial applications at frequencies to 520 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 12.5 volt mobile FM equipment.

- Specified Performance @ 520 MHz, 12.5 Volts
 - Output Power — 35 Watts
 - Power Gain — 10.0 dB
 - Efficiency — 50%
- Capable of Handling 20:1 VSWR, @ 15.6 Vdc, 520 MHz, 2 dB Overdrive
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- Broadband-Full Power Across the Band:
 - 135-175 MHz
 - 400-470 MHz
 - 450-520 MHz
- Broadband UHF/VHF Demonstration Amplifier Information Available Upon Request
- RF Power Plastic Surface Mount Package
- Available in Tape and Reel. T1 Suffix = 500 Units per 44 mm, 13 inch Reel.

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	40	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	6	Adc
Total Device Dissipation @ T _C = 25°C (1) Derate above 25°C	P _D	135 0.50	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	150	°C

THERMAL CHARACTERISTICS

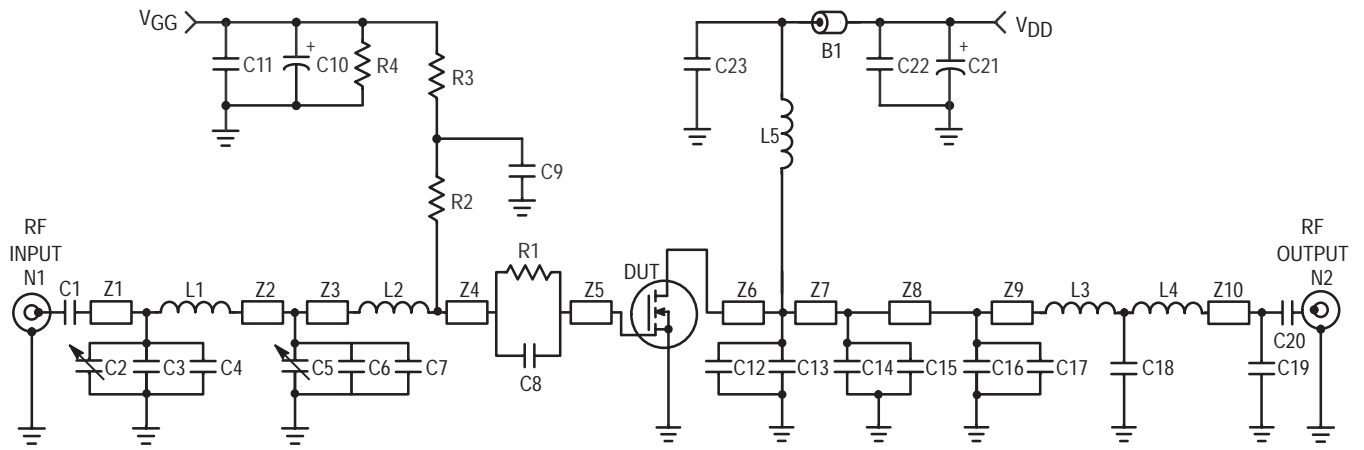
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	0.90	°C/W

(1) Calculated based on the formula $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{(BR)DSS}$	60	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 60\text{ Vdc}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 10\text{ Vdc}$, $V_{DS} = 0\text{ V}$)	I_{GSS}	—	—	0.3	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 12.5\text{ Vdc}$, $I_D = 400\ \mu\text{A}$)	$V_{GS(th)}$	1	—	2.6	Vdc
Drain–Source On–Voltage ($V_{GS} = 5\text{ Vdc}$, $I_D = 0.6\text{ A}$)	$R_{DS(on)}$	—	—	0.7	Ω
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2.0\text{ A}$)	$V_{DS(on)}$	—	—	1	Vdc
DYNAMIC CHARACTERISTICS					
Input Capacitance (Includes Input Matching Capacitance) ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{iss}	—	—	250	pF
Output Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{oss}	—	—	150	pF
Reverse Transfer Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{rss}	—	—	20	pF
RF CHARACTERISTICS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 35\text{ Watts}$, $I_{DQ} = 500\text{ mA}$) $f = 520\text{ MHz}$	G_{ps}	10	—	—	dB
Drain Efficiency ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 35\text{ Watts}$, $I_{DQ} = 500\text{ mA}$) $f = 520\text{ MHz}$	η	50	—	—	%
Load Mismatch ($V_{DD} = 15.6\text{ Vdc}$, $f = 520\text{ MHz}$, 2 dB Input Overdrive, VSWR 20:1 at All Phase Angles)	Ψ	No Degradation in Output Power Before and After Test			



B1	Ferroxcube #VK200	L4	1 Turn, #26 AWG, 0.240" ID
C1, C9, C20, C23	330 pF, 100 mil Chip Capacitors	L5	4 Turn, #24 AWG, 0.180" ID
C2, C5	0 to 20 pF, Trimmer Capacitors	N1, N2	Type N Flange Mounts
C3, C15	33 pF, 100 mil Chip Capacitors	R1	6.5 Ω, 1/4 W Chip Resistor
C4, C6, C19	18 pF, 100 mil Chip Capacitors	R2	39 Ω, Chip Resistor (0805)
C7	160 pF, 100 mil Chip Capacitor	R3	1.2 kΩ, 1/8 W Chip Resistor
C8	240 pF, 100 mil Chip Capacitor	R4	33 kΩ, 1/4 W Chip Resistor
C10, C21	10 μF, 50 V Electrolytic Capacitors	Z1	0.970" x 0.080" Microstrip
C11, C22	470 pF, 100 mil Chip Capacitors	Z2	0.380" x 0.080" Microstrip
C12, C13	150 pF, 100 mil Chip Capacitors	Z3	0.190" x 0.080" Microstrip
C14	110 pF, 100 mil Chip Capacitor	Z4	0.160" x 0.080" Microstrip
C16	68 pF, 100 mil Chip Capacitor	Z5, Z6	0.110" x 0.200" Microstrip
C17	120 pF, 100 mil Chip Capacitor	Z7	0.490" x 0.080" Microstrip
C18	51 pF, 100 mil Chip Capacitor	Z8	0.250" x 0.080" Microstrip
L1	17.5 nH, Coilcraft #A05T	Z9	0.320" x 0.080" Microstrip
L2	5 nH, Coilcraft #A02T	Z10	0.240" x 0.080" Microstrip
L3	1 Turn, #26 AWG, 0.250" ID	Board	Glass Teflon®, 31 mils

Figure 1. 135 – 175 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 135 – 175 MHz

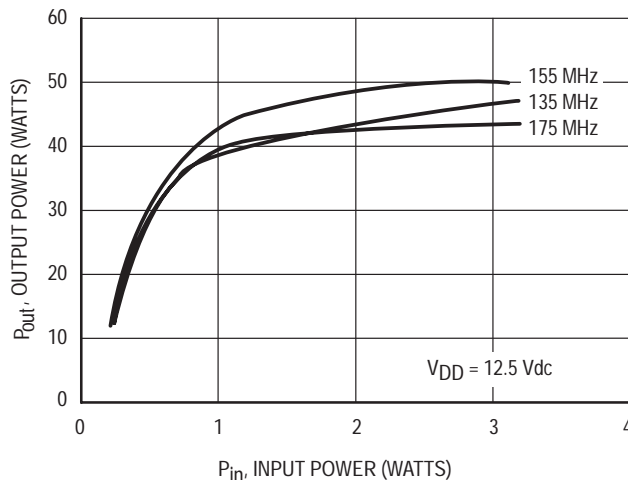


Figure 2. Output Power versus Input Power

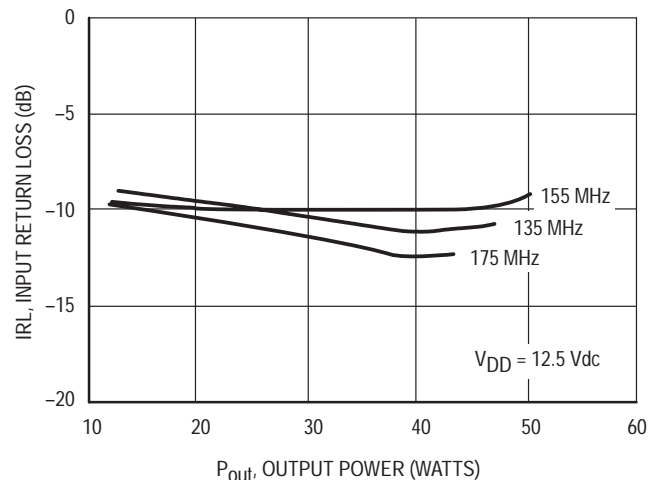


Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 135 – 175 MHz

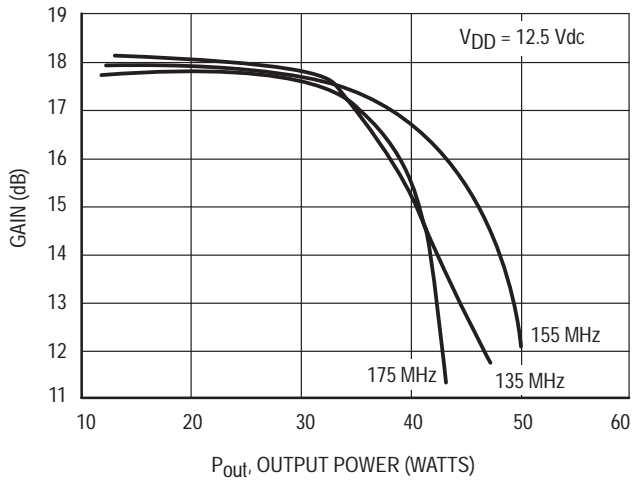


Figure 4. Gain versus Output Power

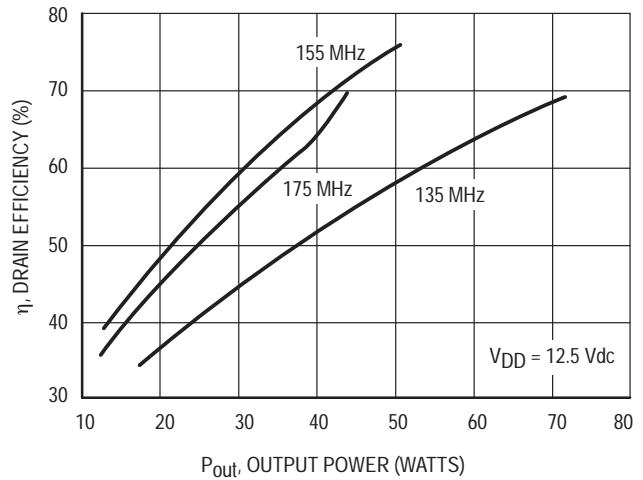


Figure 5. Drain Efficiency versus Output Power

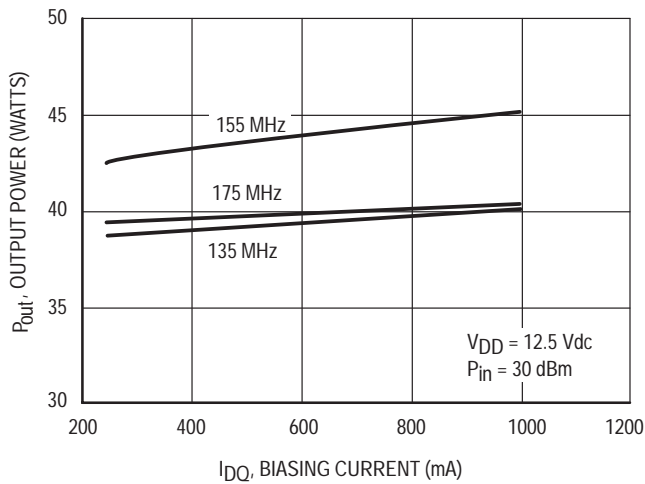


Figure 6. Output Power versus Biasing Current

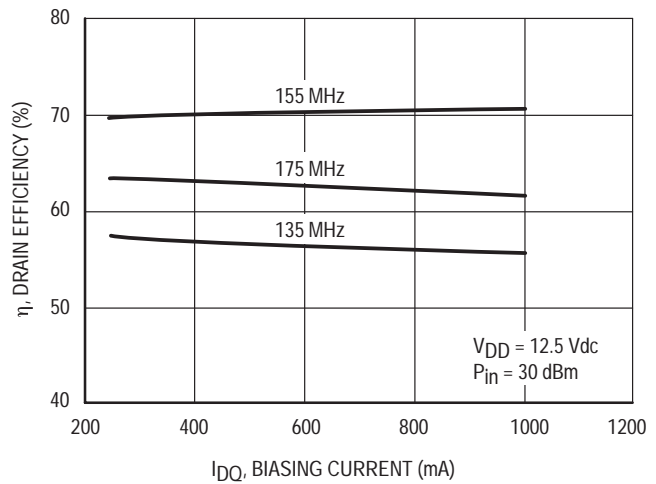


Figure 7. Drain Efficiency versus Biasing Current

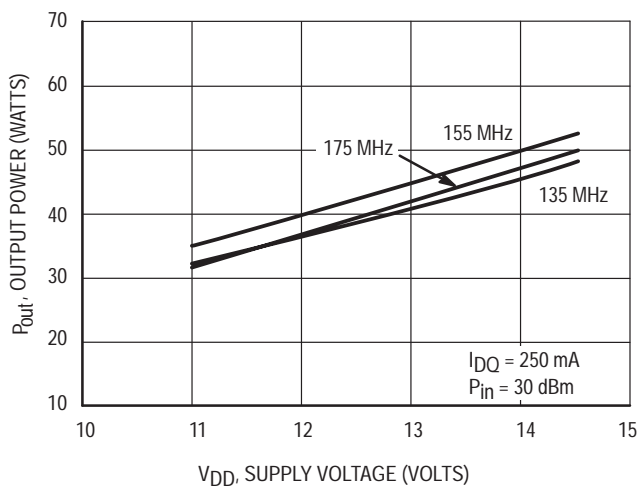


Figure 8. Output Power versus Supply Voltage

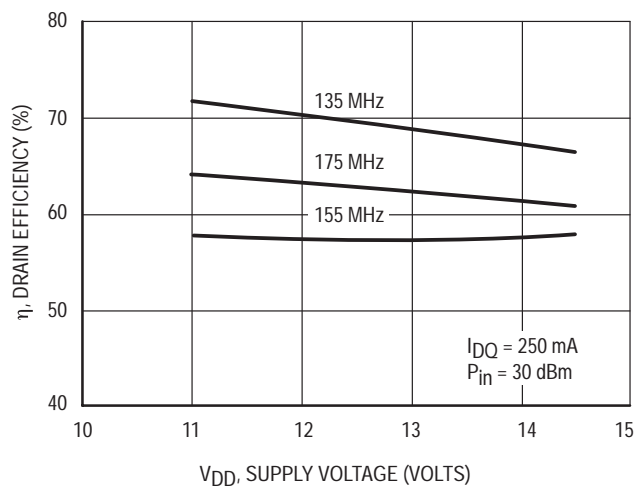
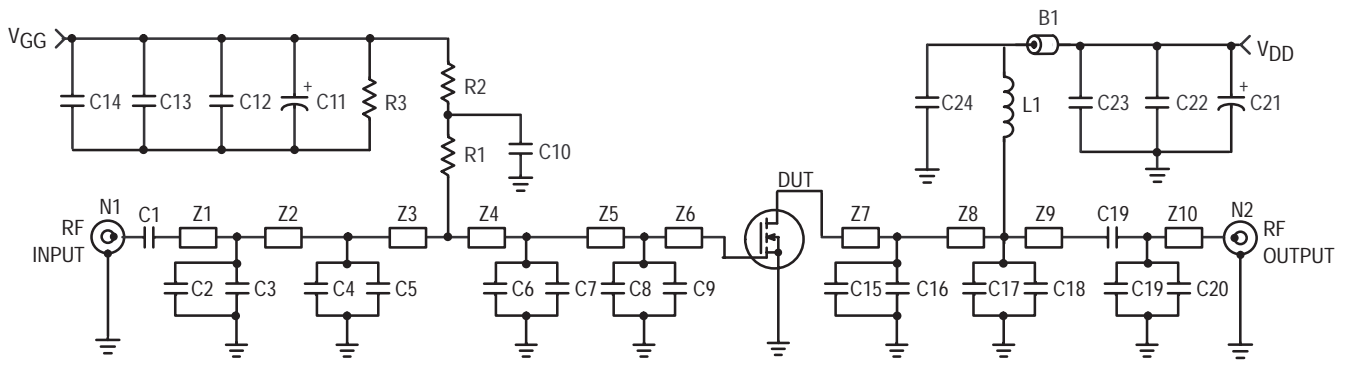


Figure 9. Drain Efficiency versus Supply Voltage



B1	Short Ferrite Bead, Fair Rite #2743021446	C21	4.8 pF, 100 mil Chip Capacitor
C1	160 pF, 100 mil Chip Capacitor	L1	47.5 nH, 5 Turn, Coilcraft
C2, C3	3.6 pF, 100 mil Chip Capacitors	N1, N2	Type N Flange Mount
C4	2.2 pF, 100 mil Chip Capacitor	R1	500 Ω , Chip Resistor (0805)
C5	10 pF, 100 mil Chip Capacitor	R2	1 k Ω , Chip Resistor (0805)
C6, C7	16 pF, 100 mil Chip Capacitors	R3	33 k Ω , 1/8 W Chip Resistor
C8, C15, C16	27 pF, 100 mil Chip Capacitors	Z1	0.480" x 0.080" Microstrip
C9	43 pF, 100 mil Chip Capacitor	Z2	1.070" x 0.080" Microstrip
C10, C14, C24	160 pF, 100 mil Chip Capacitors	Z3	0.290" x 0.080" Microstrip
C11, C21	10 μ F, 50 V Electrolytic Capacitors	Z4	0.160" x 0.080" Microstrip
C12, C22	1,200 pF, 100 mil Chip Capacitors	Z5, Z8	0.120" x 0.080" Microstrip
C13, C23	0.1 μ F, 100 mil Chip Capacitors	Z6, Z7	0.120" x 0.223" Microstrip
C17, C18	24 pF, 100 mil Chip Capacitors	Z9	1.380" x 0.080" Microstrip
C19	160 pF, 100 mil Chip Capacitor	Z10	0.625" x 0.080" Microstrip
C20	8.2 pF, 100 mil Chip Capacitor	Board	Glass Teflon [®] , 31 mils

Figure 10. 450 – 520 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 450 – 520 MHz

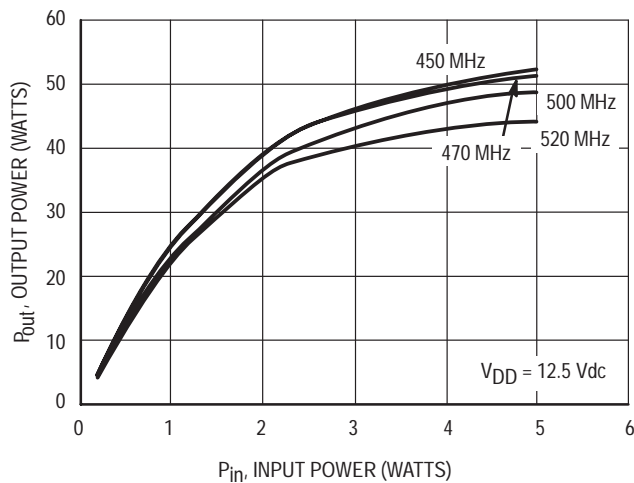


Figure 11. Output Power versus Input Power

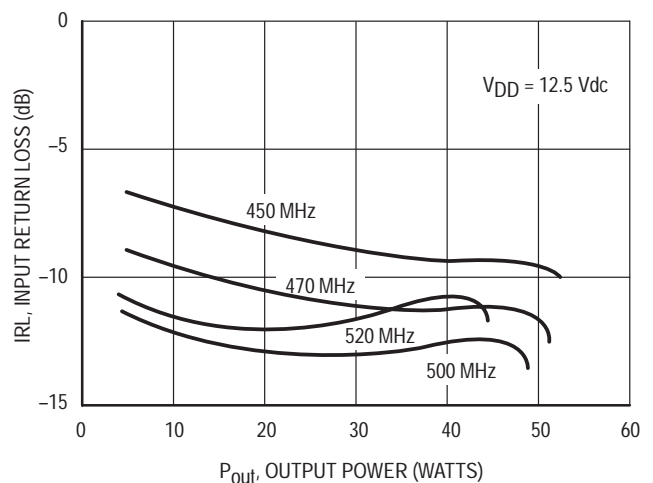


Figure 12. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 450 – 520 MHz

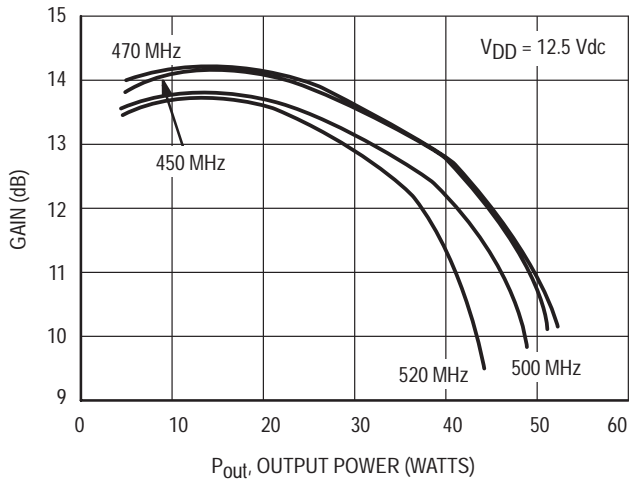


Figure 13. Gain versus Output Power

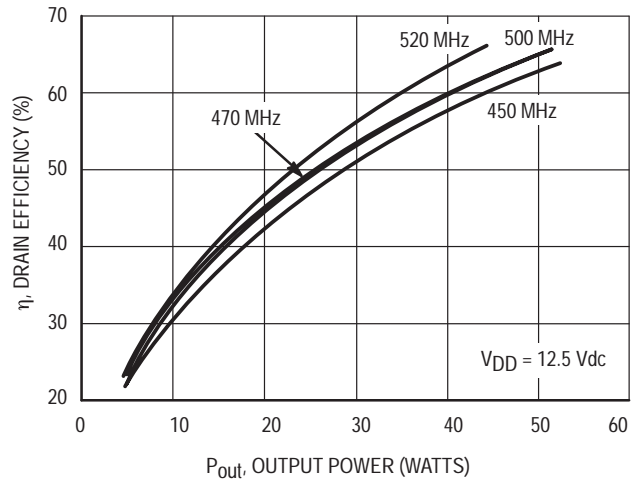


Figure 14. Drain Efficiency versus Output Power

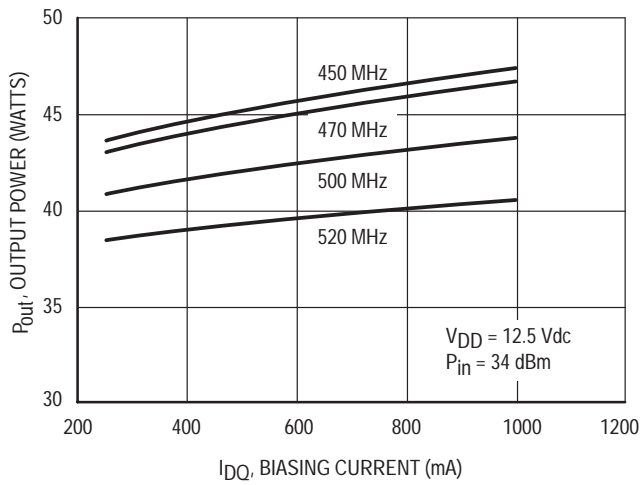


Figure 15. Output Power versus Biasing Current

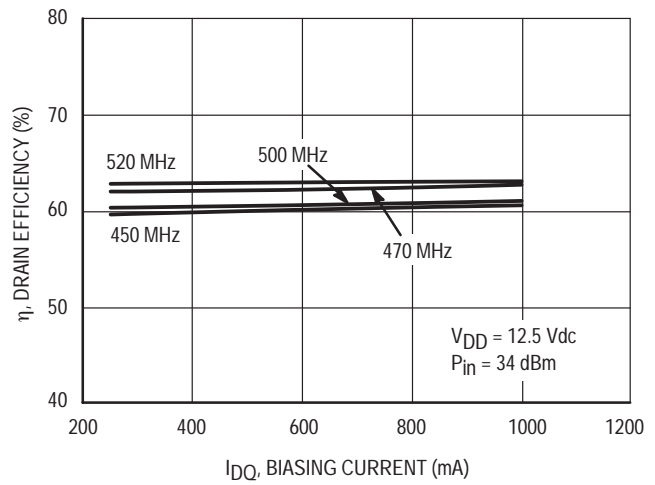


Figure 16. Drain Efficiency versus Biasing Current

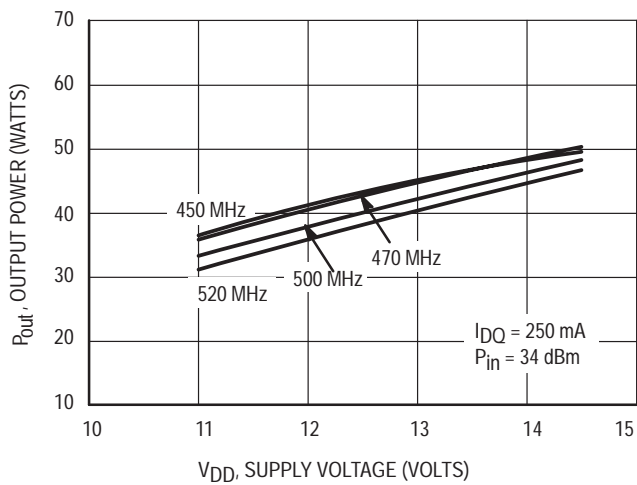


Figure 17. Output Power versus Supply Voltage

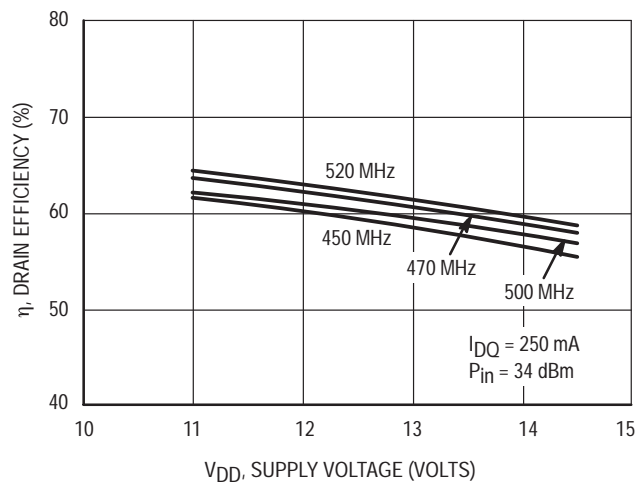
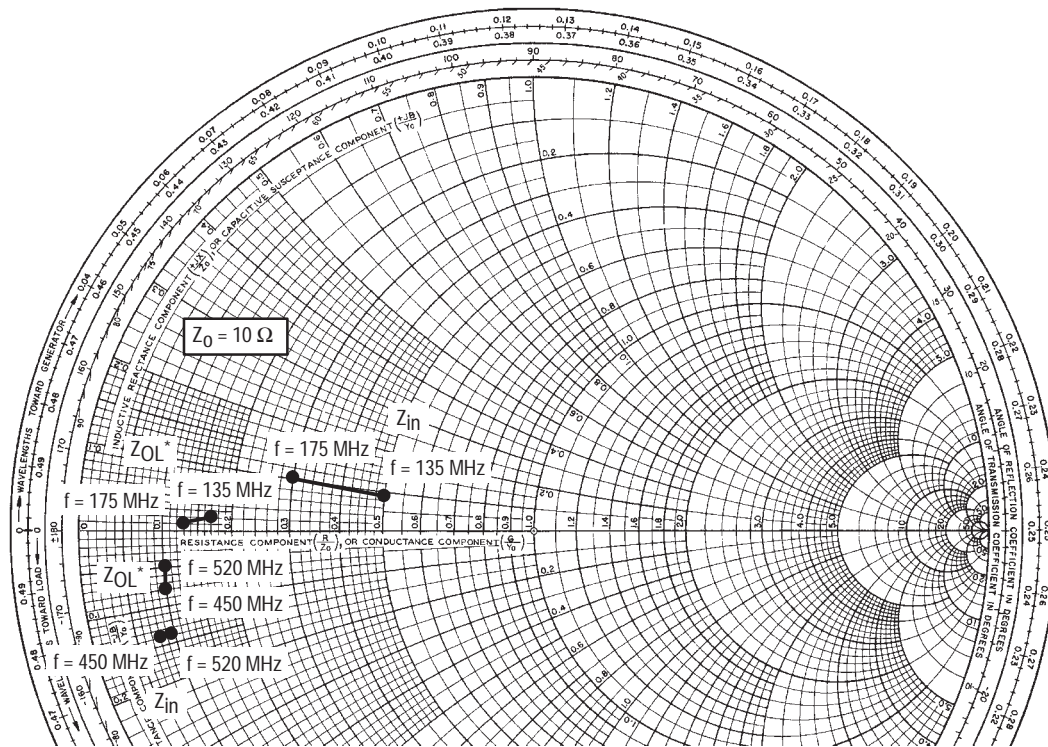


Figure 18. Drain Efficiency versus Supply Voltage



$V_{DD} = 12.5\text{ V}$, $I_{DQ} = 250\text{ mA}$, $P_{out} = 35\text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
135	$5.0 + j0.9$	$1.7 + j0.2$
155	$5.0 + j0.9$	$1.7 + j0.2$
175	$3.0 + j1.0$	$1.3 + j0.1$

Z_{in} = Complex conjugate of source impedance with parallel $6.5\ \Omega$ resistor and 240 pF capacitor in series with gate.

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50\%$.

$V_{DD} = 12.5\text{ V}$, $I_{DQ} = 500\text{ mA}$, $P_{out} = 35\text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
450	$0.8 - j1.4$	$1.0 - j0.8$
470	$0.9 - j1.4$	$1.1 - j0.6$
500	$1.0 - j1.4$	$1.1 - j0.6$
520	$0.9 - j1.4$	$1.1 - j0.5$

Z_{in} = Complex conjugate of source impedance with parallel $6.5\ \Omega$ resistor and 240 pF capacitor in series with gate.

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50\%$.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

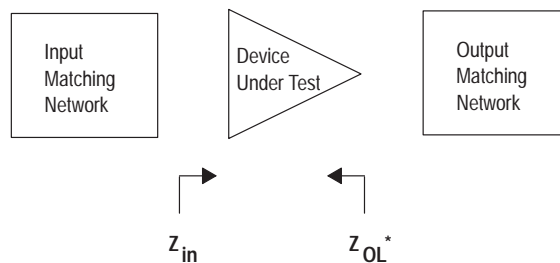


Figure 19. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ($V_{DD} = 12.5$ Vdc)

$I_{DQ} = 250$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.89	-173	8.496	83	0.014	-26	0.76	-170
100	0.90	-175	3.936	72	0.014	-14	0.79	-170
150	0.91	-175	2.429	63	0.011	-23	0.82	-170
200	0.92	-175	1.627	57	0.010	-44	0.86	-170
250	0.94	-176	1.186	53	0.007	-16	0.88	-170
300	0.95	-176	0.888	49	0.005	-44	0.91	-171
350	0.96	-176	0.686	48	0.005	36	0.92	-170
400	0.96	-176	0.568	44	0.005	-1	0.94	-171
450	0.97	-176	0.457	44	0.004	49	0.94	-172
500	0.97	-176	0.394	44	0.003	-51	0.95	-171
550	0.98	-176	0.332	42	0.001	31	0.95	-173
600	0.98	-177	0.286	41	0.013	99	0.94	-173

$I_{DQ} = 1.0$ A

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.90	-173	8.49	83	0.006	-39	0.86	-176
100	0.90	-175	3.92	72	0.009	-5	0.86	-176
150	0.91	-175	2.44	63	0.006	7	0.87	-176
200	0.92	-175	1.62	57	0.008	21	0.88	-175
250	0.94	-176	1.19	53	0.006	8	0.89	-174
300	0.95	-176	0.89	48	0.008	3	0.89	-174
350	0.96	-176	0.69	48	0.007	48	0.91	-174
400	0.96	-176	0.57	44	0.004	41	0.93	-173
450	0.97	-176	0.46	44	0.004	43	0.93	-173
500	0.97	-176	0.39	44	0.003	57	0.94	-173
550	0.98	-176	0.33	41	0.006	62	0.94	-174
600	0.98	-177	0.28	41	0.009	96	0.93	-173

$I_{DQ} = 2.0$ A

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.94	-176	9.42	88	0.005	-72	0.89	-177
100	0.94	-178	4.56	82	0.005	4	0.89	-177
150	0.94	-178	2.99	78	0.003	7	0.89	-177
200	0.94	-178	2.14	74	0.005	17	0.90	-176
250	0.95	-178	1.67	71	0.004	40	0.90	-175
300	0.95	-178	1.32	67	0.007	35	0.91	-175
350	0.95	-178	1.08	67	0.005	57	0.92	-174
400	0.96	-178	0.93	63	0.003	50	0.93	-173
450	0.96	-178	0.78	62	0.007	68	0.93	-173
500	0.96	-177	0.68	61	0.004	99	0.94	-173
550	0.97	-177	0.59	58	0.008	78	0.93	-175
600	0.97	-178	0.51	57	0.009	92	0.92	-174

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

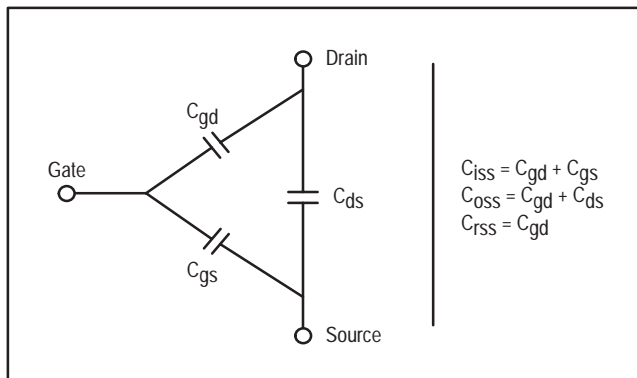
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

BV_{DSS} values for this device are higher than normally required for typical applications. Measurement of BV_{DSS} is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of $10^9 \Omega$ – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 150 \text{ mA}$, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 2°C/W assumes a majority of the 0.065" x 0.180" source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

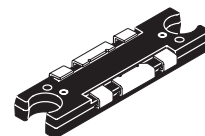
The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

MRF1550T1

The MRF1550T1 is designed for broadband commercial and industrial applications at frequencies to 175 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 12.5 volt mobile FM equipment.

175 MHz, 50 W, 12.5 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET

- Specified Performance @ 175 MHz, 12.5 Volts
Output Power — 50 Watts
Power Gain — 12 dB
Efficiency — 50%
- Capable of Handling 20:1 VSWR, @ 15.6 Vdc, 175 MHz, 2 dB Overdrive
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- RF Power Plastic Surface Mount Package
- Broadband-Full Power Across the Band: 135-175 MHz
- Broadband Demonstration Amplifier Information Available Upon Request
- Available in Tape and Reel. T1 Suffix = 500 Units per 44 mm, 13 inch Reel.



CASE 1264-06, STYLE 1
(TO-272)

PLASTIC

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	40	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Drain Current — Continuous	I_D	12	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1) Derate above 25°C	P_D	165 0.50	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.75	$^\circ\text{C}/\text{W}$

(1) Calculated based on the formula $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Zero Gate Voltage Drain Current ($V_{DS} = 60\text{ Vdc}$, $V_{GS} = 0\text{ V}$)	I_{DSS}	—	—	1	μA_{dc}
Gate–Source Leakage Current ($V_{GS} = 10\text{ Vdc}$, $V_{DS} = 0\text{ V}$)	I_{GSS}	—	—	0.5	μA_{dc}

ON CHARACTERISTICS

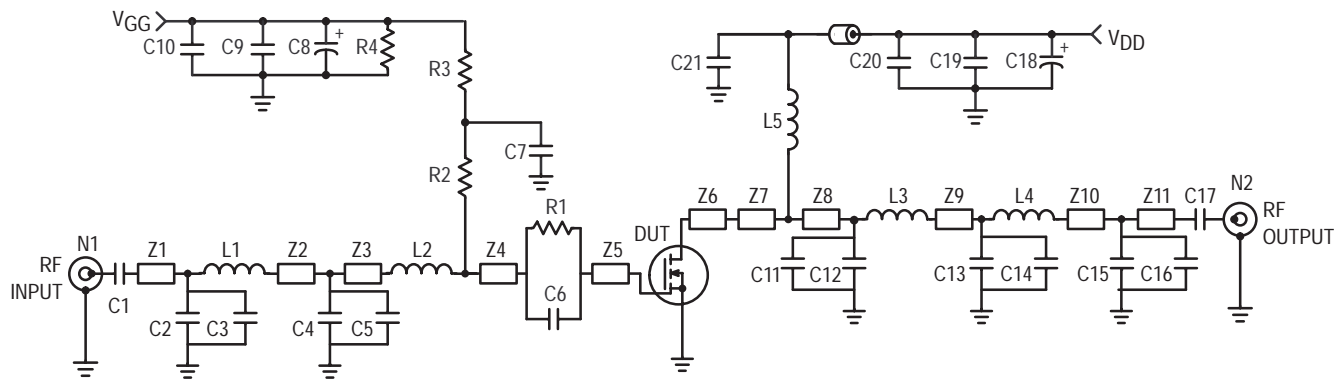
Gate Threshold Voltage ($V_{DS} = 12.5\text{ Vdc}$, $I_D = 800\ \mu\text{A}$)	$V_{GS(th)}$	1	—	3	Vdc
Drain–Source On–Voltage ($V_{GS} = 5\text{ Vdc}$, $I_D = 1.2\text{ A}$)	$R_{DS(on)}$	—	—	0.5	Ω
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 4.0\text{ A}_{dc}$)	$V_{DS(on)}$	—	—	1	Vdc

DYNAMIC CHARACTERISTICS

Input Capacitance (Includes Input Matching Capacitance) ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{iss}	—	—	500	pF
Output Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{oss}	—	—	250	pF
Reverse Transfer Capacitance ($V_{DS} = 12.5\text{ Vdc}$, $V_{GS} = 0\text{ V}$, $f = 1\text{ MHz}$)	C_{rss}	—	—	35	pF

RF CHARACTERISTICS (In Motorola Test Fixture)

Common–Source Amplifier Power Gain ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 50\text{ Watts}$, $I_{DQ} = 500\text{ mA}$) $f = 175\text{ MHz}$	G_{ps}	10	—	—	dB
Drain Efficiency ($V_{DD} = 12.5\text{ Vdc}$, $P_{out} = 50\text{ Watts}$, $I_{DQ} = 500\text{ mA}$) $f = 175\text{ MHz}$	η	50	—	—	%
Load Mismatch ($V_{DD} = 15.6\text{ Vdc}$, $f = 175\text{ MHz}$, 2 dB Input Overdrive, VSWR 20:1 at All Phase Angles)	Ψ	No Degradation in Output Power Before and After Test			



B1	Ferroxcube #VK200	L4	1 Turn, #26 AWG, 0.240" ID
C1	180 pF, 100 mil Chip Capacitor	L5	3 Turn, #24 AWG, 0.180" ID
C2	10 pF, 100 mil Chip Capacitor	N1, N2	Type N Flange Mount
C3	33 pF, 100 mil Chip Capacitor	R1	5.1 Ω , 1/4 W Chip Resistor
C4, C16	24 pF, 100 mil Chip Capacitors	R2	39 Ω , Chip Resistor (0805)
C5	160 pF, 100 mil Chip Capacitor	R3	1 k Ω , 1/8 W Chip Resistor
C6	240 pF, 100 mil Chip Capacitor	R4	33 k Ω , 1/4 W Chip Resistor
C7, C17	300 pF, 100 mil Chip Capacitors	Z1	1.000" x 0.080" Microstrip
C8, C18	10 μ F, 50 V Electrolytic Capacitors	Z2	0.400" x 0.080" Microstrip
C9, C19	0.1 μ F, 100 mil Chip Capacitors	Z3	0.200" x 0.080" Microstrip
C10	470 pF, 100 mil Chip Capacitor	Z4	0.200" x 0.080" Microstrip
C11, C12	200 pF, 100 mil Chip Capacitors	Z5, Z6	0.100" x 0.223" Microstrip
C13	22 pF, 100 mil Chip Capacitor	Z7	0.160" x 0.080" Microstrip
C14	30 pF, 100 mil Chip Capacitor	Z8	0.260" x 0.080" Microstrip
C15	6.8 pF, 100 mil Chip Capacitor	Z9	0.280" x 0.080" Microstrip
C20	1,000 pF, 100 mil Chip Capacitor	Z10	0.270" x 0.080" Microstrip
L1	18.5 nH, Coilcraft #A05T	Z11	0.730" x 0.080" Microstrip
L2	5 nH, Coilcraft #A02T	Board	Glass Teflon [®] , 31 mils
L3	1 Turn, #24 AWG, 0.250" ID		

Figure 1. 135 – 175 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS

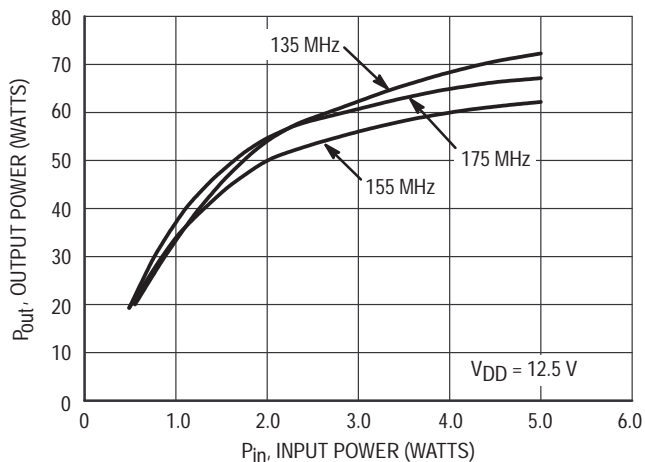


Figure 2. Output Power versus Input Power

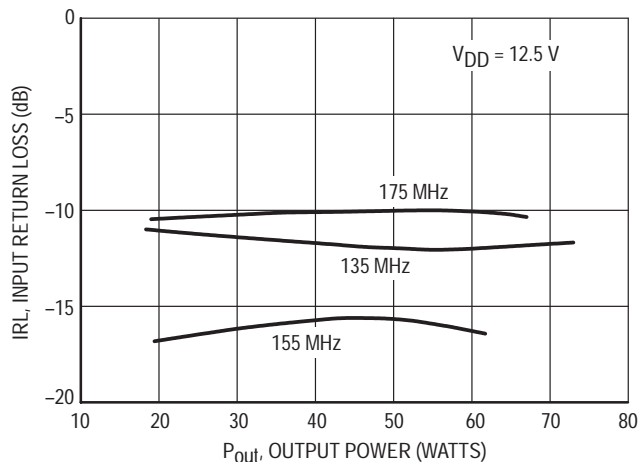


Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS

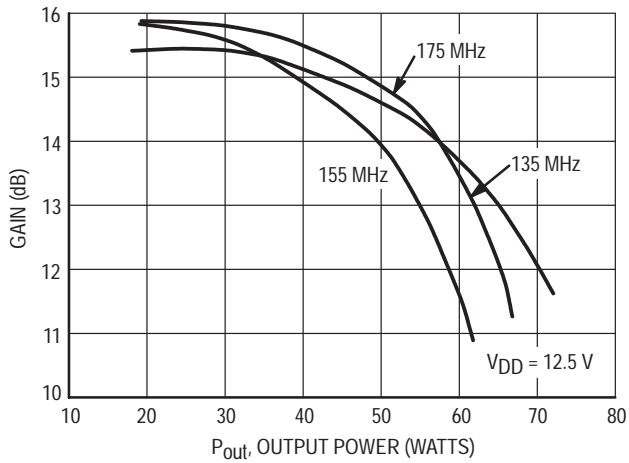


Figure 4. Gain versus Output Power

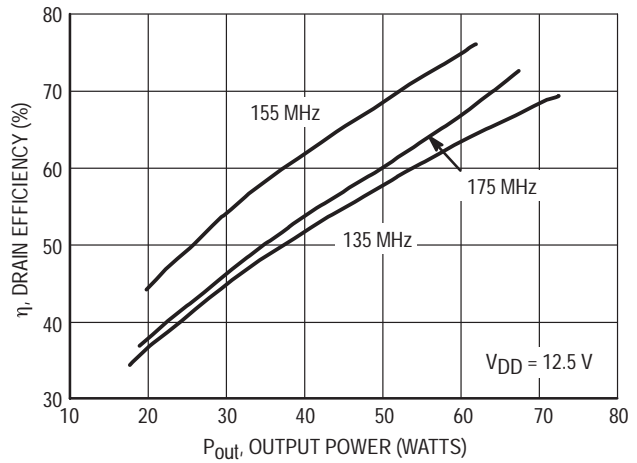


Figure 5. Drain Efficiency versus Output Power

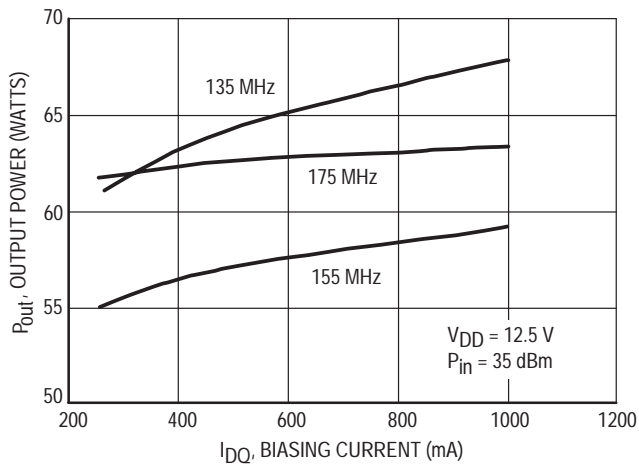


Figure 6. Output Power versus Biasing Current

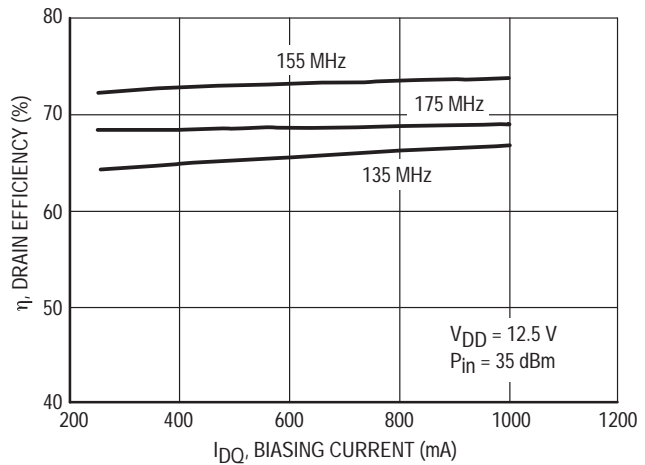


Figure 7. Drain Efficiency versus Biasing Current

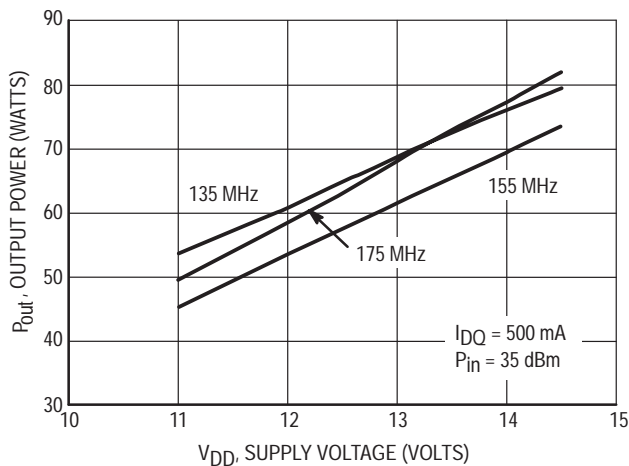


Figure 8. Output Power versus Supply Voltage

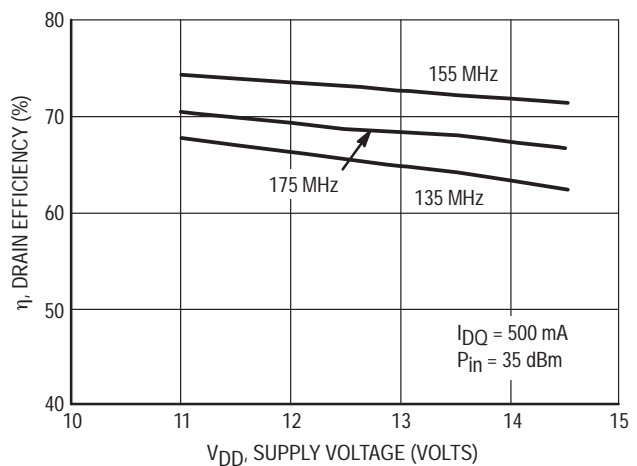
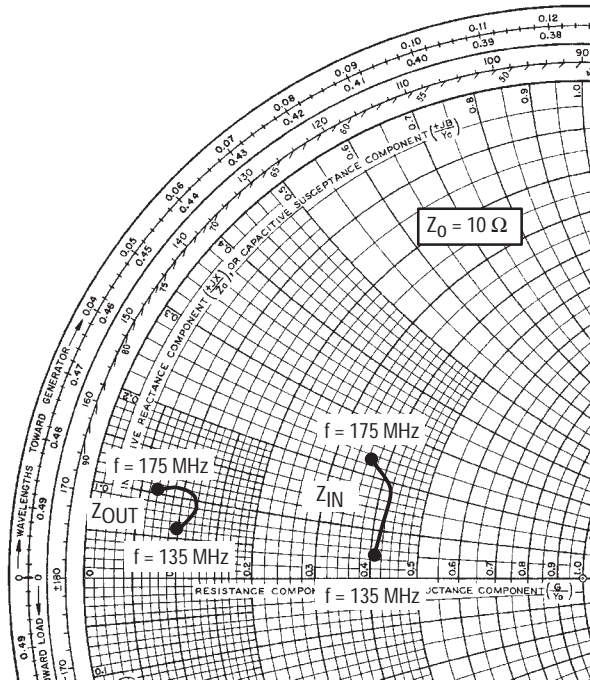


Figure 9. Drain Efficiency versus Supply Voltage



$V_{DD} = 12.5 \text{ V}$, $I_{DQ} = 500 \text{ mA}$, $P_{out} = 50 \text{ W}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
135	$4.1 + j0.5$	$1.0 + j0.6$
155	$4.2 + j1.7$	$1.2 + j.09$
175	$3.7 + j2.3$	$0.7 + j1.1$

Z_{in} = Complex conjugate of source impedance with parallel 5.1Ω resistor and 240 pF capacitor in series with gate.

Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50 \%$.

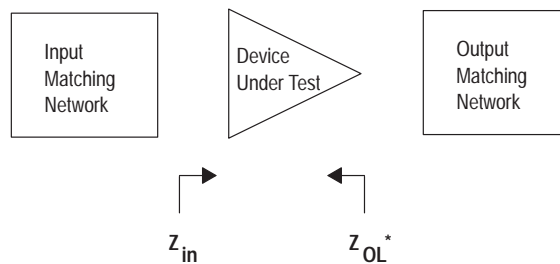


Figure 10. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ($V_{DD} = 12.5$ Vdc)

$I_{DQ} = 500$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.93	-178	4.817	80	0.009	-39	0.86	-176
100	0.94	-178	2.212	69	0.009	-3	0.88	-175
150	0.95	-178	1.349	61	0.008	-8	0.90	-174
200	0.95	-178	0.892	54	0.006	-13	0.92	-174
250	0.96	-178	0.648	51	0.005	-7	0.93	-174
300	0.97	-178	0.481	47	0.004	-8	0.95	-174
350	0.97	-178	0.370	46	0.005	4	0.95	-174
400	0.98	-178	0.304	43	0.001	15	0.97	-174
450	0.98	-178	0.245	43	0.005	81	0.97	-174
500	0.98	-178	0.209	43	0.003	84	0.97	-174
550	0.99	-177	0.178	41	0.007	70	0.98	-175
600	0.98	-178	0.149	41	0.010	106	0.96	-175

$I_{DQ} = 2.0$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.93	-177	4.81	80	0.003	-119	0.93	-178
100	0.94	-178	2.20	69	0.006	4	0.93	-178
150	0.95	-178	1.35	61	0.003	-1	0.93	-177
200	0.95	-178	0.89	54	0.004	18	0.93	-176
250	0.96	-178	0.65	51	0.001	28	0.94	-176
300	0.97	-178	0.48	47	0.004	77	0.94	-175
350	0.97	-178	0.37	46	0.006	85	0.95	-175
400	0.98	-178	0.30	43	0.007	53	0.96	-174
450	0.98	-178	0.25	43	0.006	74	0.97	-174
500	0.98	-177	0.21	44	0.006	84	0.97	-174
550	0.99	-177	0.18	41	0.002	106	0.97	-175
600	0.98	-178	0.15	41	0.004	116	0.96	-174

$I_{DQ} = 4.0$ mA

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
50	0.97	-179	5.04	87	0.002	-116	0.94	-179
100	0.96	-179	2.43	82	0.006	42	0.94	-178
150	0.96	-179	1.60	77	0.004	13	0.94	-177
200	0.96	-179	1.14	74	0.003	43	0.95	-176
250	0.97	-179	0.89	71	0.004	65	0.95	-175
300	0.97	-179	0.71	68	0.006	68	0.95	-175
350	0.97	-179	0.57	67	0.006	74	0.97	-174

Table 1. Common Source Scattering Parameters ($V_{DD} = 12.5$ Vdc) (continued)

$I_{DQ} = 4.0$ mA (continued)

f MHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
400	0.97	-179	0.49	63	0.005	58	0.97	-173
450	0.98	-178	0.41	63	0.005	73	0.98	-173
500	0.98	-178	0.36	62	0.003	128	0.98	-173
550	0.98	-178	0.32	58	0.004	57	0.99	-174
600	0.98	-178	0.27	58	0.009	83	0.98	-174

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

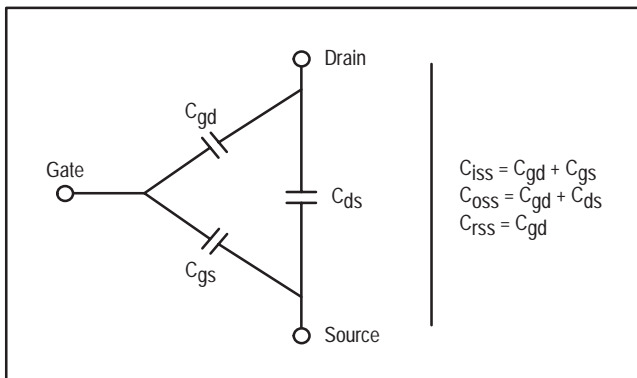
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

BV_{DSS} values for this device are higher than normally required for typical applications. Measurement of BV_{DSS} is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of $10^9 \Omega$ – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 150 \text{ mA}$, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 2°C/W assumes a majority of the 0.065" x 0.180" source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

AMPLIFIER DESIGN

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

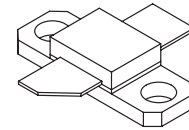
Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

The RF Line
NPN Silicon
RF Power Transistor

MRF6404

30 W, 1.88 GHz
RF POWER TRANSISTOR
NPN SILICON



CASE 395C-01, STYLE 1

The MRF6404 is designed for 26 volts microwave large signal, common emitter, class AB linear amplifier applications operating in the range 1.8 to 2.0 GHz.

- Specified 26 Volts, 1.88 GHz Characteristics
Output Power — 30 Watts
Gain — 7.5 dB Min @ 30 Watts
Efficiency — 38% Min @ 30 Watts
- Characterized with Series Equivalent Large-Signal Parameters from 1.8 to 2.0 GHz
- To be used in Class AB for DCS1800 and PCS1900/Cellular Radio
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CEO}	24	Vdc
Collector-Emitter Voltage	V_{CES}	60	Vdc
Emitter-Base Voltage	V_{EBO}	4	Vdc
Collector-Current — Continuous	I_C	10	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	125 0.71	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (1)	$R_{\theta JC}$	1.4	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector-Emitter Breakdown Voltage ($I_C = 50\text{ mA}$, $I_B = 0$)	$V_{(BR)CEO}$	24	29	—	Vdc
Emitter-Base Breakdown Voltage ($I_E = 10\text{ mAdc}$)	$V_{(BR)EBO}$	4	5	—	Vdc
Collector-Base Breakdown Voltage ($I_C = 50\text{ mAdc}$)	$V_{(BR)CES}$	60	68	—	Vdc
Collector-Base Breakdown Voltage ($I_C = 50\text{ mAdc}$, $R_{BE} = 75\ \Omega$)	$V_{(BR)CER}$	40	56	—	Vdc
Collector Cutoff Current ($V_{CE} = 30\text{ V}$, $V_{BE} = 0$)	I_{CES}	—	—	10	mA

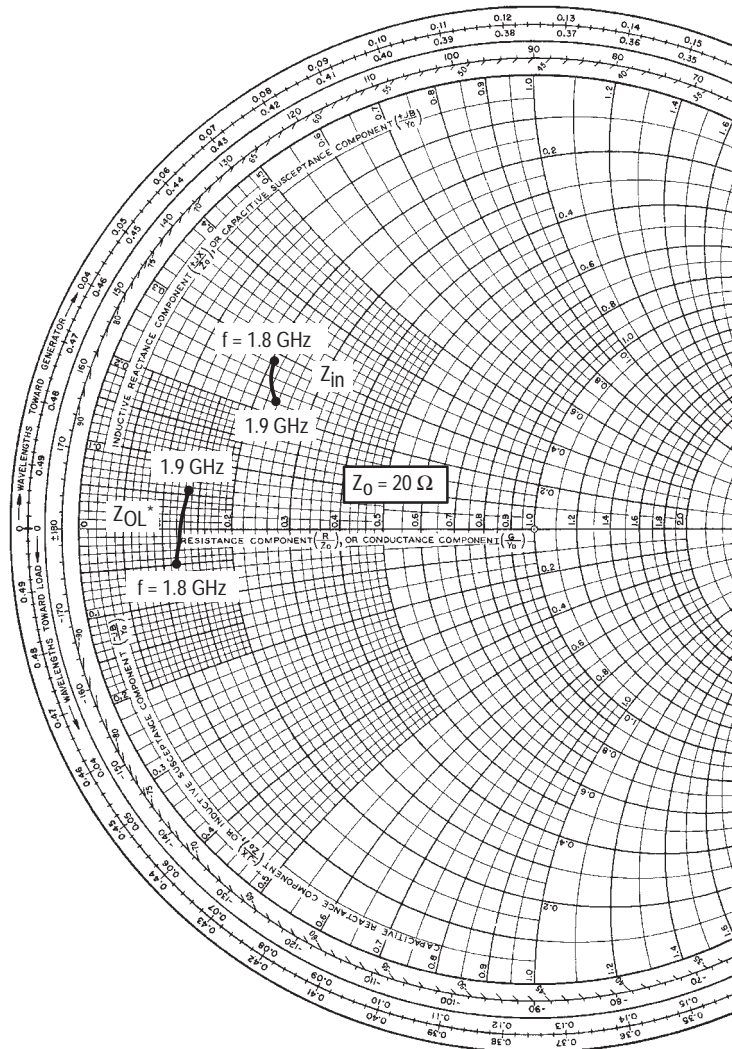
ON CHARACTERISTICS

DC Current Gain ($I_C = 1\text{ Adc}$, $V_{CE} = 5\text{ Vdc}$)	h_{FE}	20	50	120	—
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(1) Thermal resistance is determined under specified RF operating condition.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
DYNAMIC CHARACTERISTICS					
Output Capacitance ($V_{CB} = 26\text{ V}$, $I_E = 0$, $f = 1\text{ MHz}$) For information only. This part is collector matched.	C_{ob}	30	38	—	pF
FUNCTIONAL TESTS					
Common-Emitter Amplifier Power Gain ($V_{CC} = 26\text{ V}$, $P_{out} = 30\text{ W}$, $I_{CQ} = 150\text{ mA}$, $f = 1.88\text{ GHz}$)	G_{pe}	7.5	8.5	—	dB
Common-Emitter Amplifier Power Gain ($V_{CC} = 26\text{ V}$, $P_{out} = 28\text{ W}$, $I_{CQ} = 150\text{ mA}$) ($f = 1.99\text{ GHz}$)	G_{pe}	7	8	—	dB
Collector Efficiency ($V_{CC} = 26\text{ V}$, $P_{out} = 30\text{ W}$, $f = 1.88\text{ GHz}$) ($V_{CC} = 26\text{ V}$, $P_{out} = 28\text{ W}$, $f = 1.99\text{ GHz}$)	η	38 35	43 40	— —	%
Output Power at 1 dBc ($V_{CC} = 26\text{ V}$, $f = 1.88\text{ GHz}$) ($V_{CC} = 26\text{ V}$, $f = 1.99\text{ GHz}$)	P_{1dBc}	30 28	35 33	— —	Watts
Output Mismatch Stress: VSWR = 3:1 (all phase angles) ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 25\text{ W}$, $I_{CQ} = 150\text{ mA}$, $f = 1.88\text{ GHz}$)	Ψ	No Degradation in Output Power			



DCS EVALUATION

f (GHz)	Z_{in} (Ω)	Z_{OL}^* (Ω)
1.8	$4.3 + j6.1$	$2.7 - j1.0$
1.85	$4.6 + j5.3$	$2.9 + j0.3$
1.9	$4.8 + j5.0$	$3.0 + j1.2$

Z_{OL}^* : Conjugate of optimum load impedance into which the device operates at a given output power, voltage, current and frequency.

**Figure 1. Input and Output Impedances with Circuit Tuned for Maximum Gain
@ $V_{CC} = 26\text{ V}$, $I_{CQ} = 150\text{ mA}$, $P_{out} = 30\text{ W}$**

TYPICAL CHARACTERISTICS

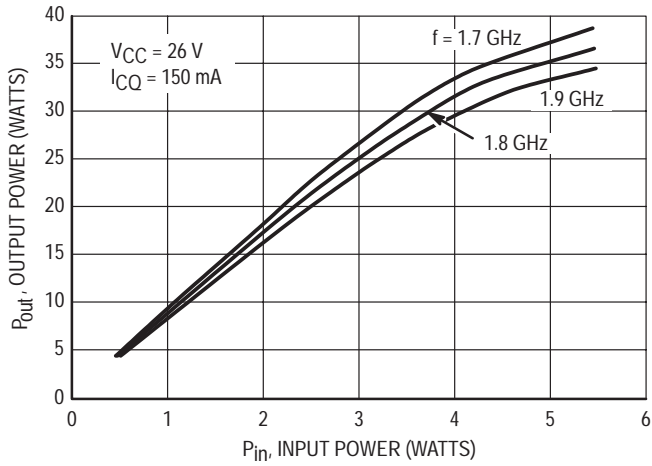


Figure 2. Output Power versus Input Power

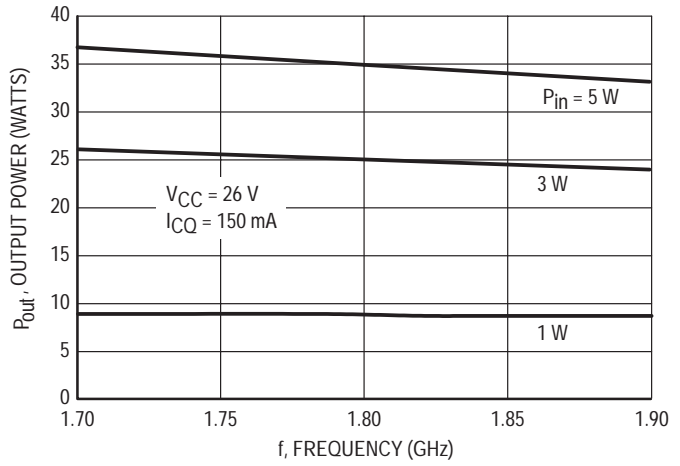


Figure 3. Output Power versus Frequency

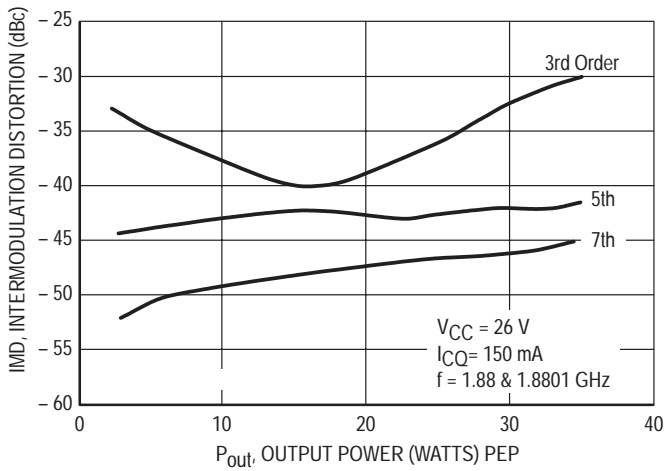


Figure 4. Intermodulation versus Output Power

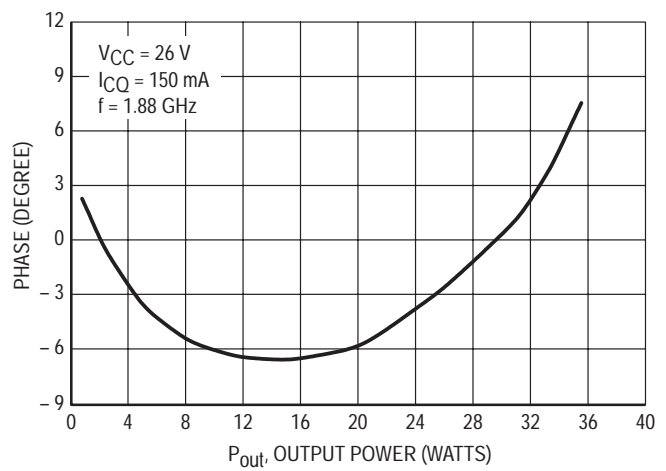
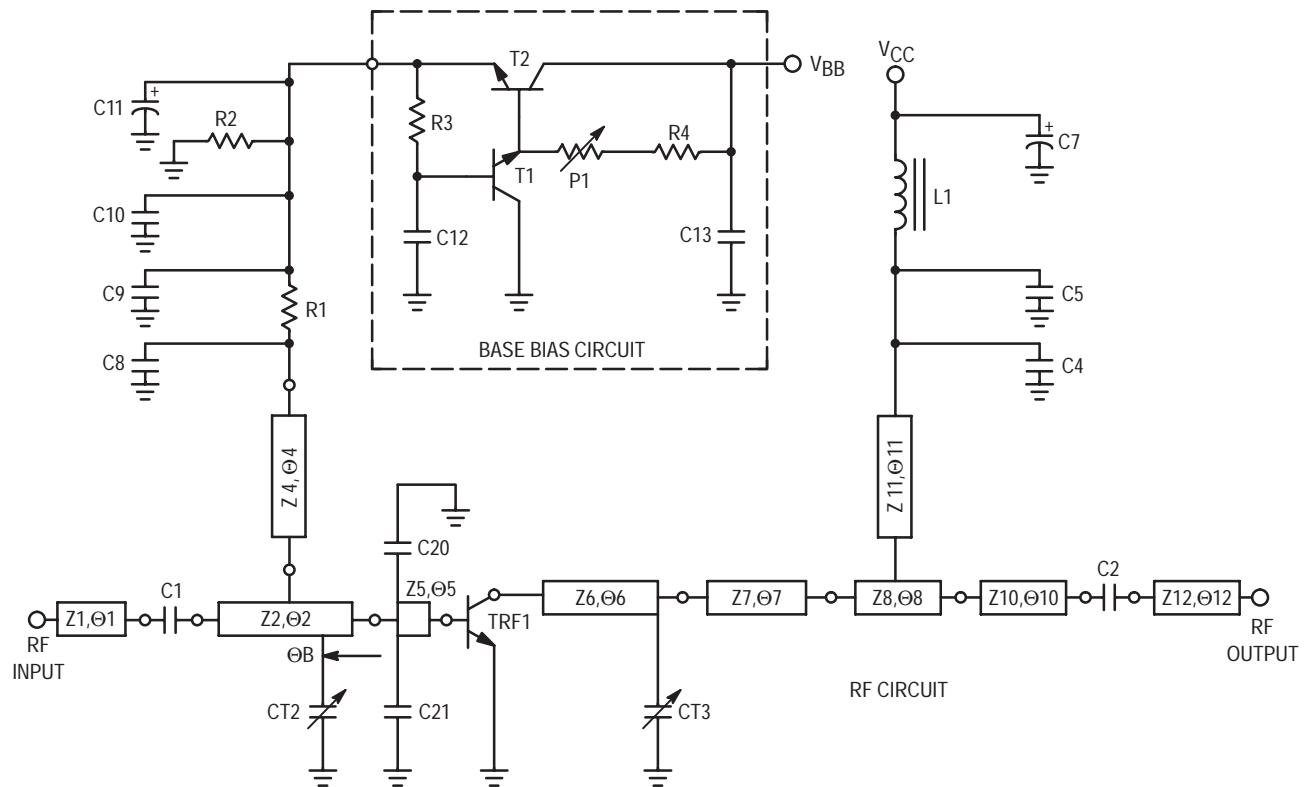


Figure 5. AM/PM Conversion



Base Bias Circuit

C12, C13	15 nF, Chip Capacitor, Vitramon (0805 A153 JXB)
P1	1 K Ω , Trimmer
R3	47 Ω , Chip Resistor, 0805
R4	330 Ω , Chip Resistor, 0805
T1, T2	Motorola MJD 31C

Decoupling Base Bias Circuit

C4	68 pF, Chip Capacitor, ATC 100A
C5, C9	330 pF, Chip Capacitor, Vitramon (0805 A331 JXB)
C7, C11	4.7 μ F, 63 V, Electrolytic Capacitor
C8	68 pF, Chip Capacitor, ATC 100A
C10	15 nF, Chip Capacitor, Vitramon (0805 A153 JXB)
R1	1.5 Ω , Chip Resistor, 0805
R2	56 Ω , Chip Resistor, 1206

RF Circuit

C1, C2	68 pF, Chip Capacitor, ATC 100A
C20, C21	1.3 pF, Chip Capacitor, ATC 100A
CT2	Trimmer Capacitor, Gigatrim, Ref 37281
CT3	Trimmer Capacitor, Gigatrim, Ref 37291
TRF1	MRF6404

PC Board Material:

$\epsilon_r = 2.55$, H = 0.508 mm, T = 0.035 mm

All Electrical Lengths Are Referenced from λ_g @ f = 1.9 GHz

Z1 : 50 Ω	$\Theta 1$: 10 $^\circ$
Z2 : 50 Ω	$\Theta 2$: 74.5 $^\circ$
ΘB : 16.5 $^\circ$	
Z4 : 74 Ω	$\Theta 4$: 68 $^\circ$
Z5 : 12.8 Ω	$\Theta 5$: 21 $^\circ$
Z6 : 10.4 Ω	$\Theta 6$: 49.5 $^\circ$
Z7 : 18 Ω	$\Theta 7$: 36.5 $^\circ$
Z8 : 45 Ω	$\Theta 8$: 20 $^\circ$
Z10 : 50 Ω	$\Theta 10$: 10 $^\circ$
Z11 : 74 Ω	$\Theta 11$: 74.5 $^\circ$
Z12 : 50 Ω	$\Theta 12$: 10 $^\circ$

Figure 6. 1.80–1.88 GHz Test Circuit Electrical Schematic and Components List



(Not to Scale)

Teflon® Glass 0.5 mm – Double Side 35 μm Cu.

Figure 7. 1.80–1.88 GHz PCN Test Circuit Photomaster

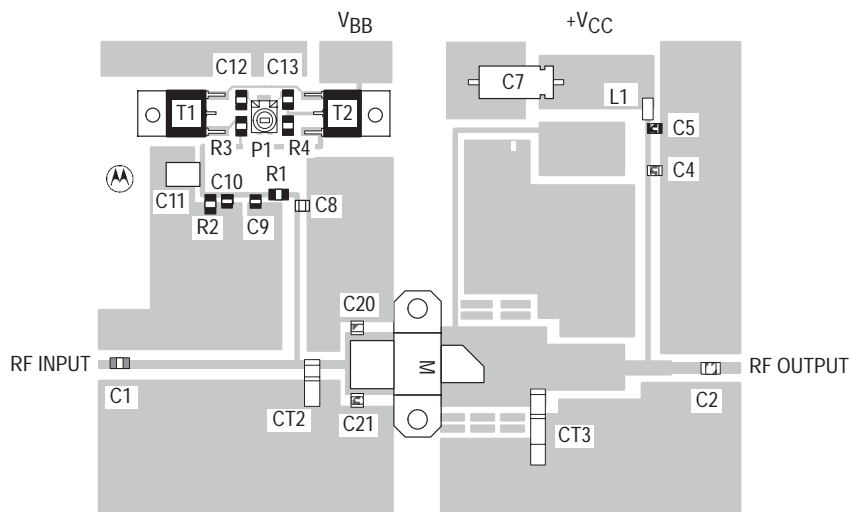
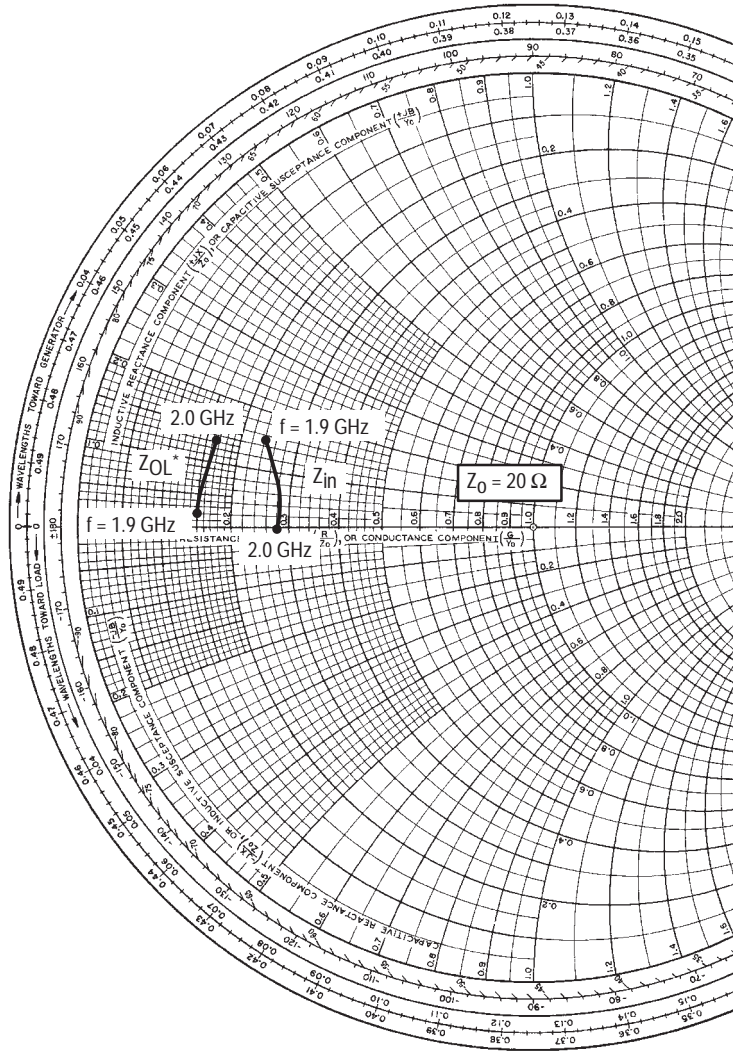


Figure 8. 1.80–1.88 GHz PCN Test Circuit Components Layout



PCS EVALUATION

f (GHz)	Z _{in} (Ω)	Z _{OL} * (Ω)
1.90	4.9 + j3.0	3.2 + j0.5
1.93	5.4 + j2.5	3.3 + j1.2
1.97	5.6 + j1.4	3.4 + j1.5
2.00	5.4 - j0.2	3.6 + j2.5

Z_{OL}*: Conjugate of optimum load impedance into which the device operates at a given output power, voltage, current and frequency.

Figure 9. Input and Output Impedances with Circuit Tuned for Maximum Gain
 @ V_{CC} = 26 V, I_{CQ} = 150 mA, P_{out} = 28 W

TYPICAL CHARACTERISTICS

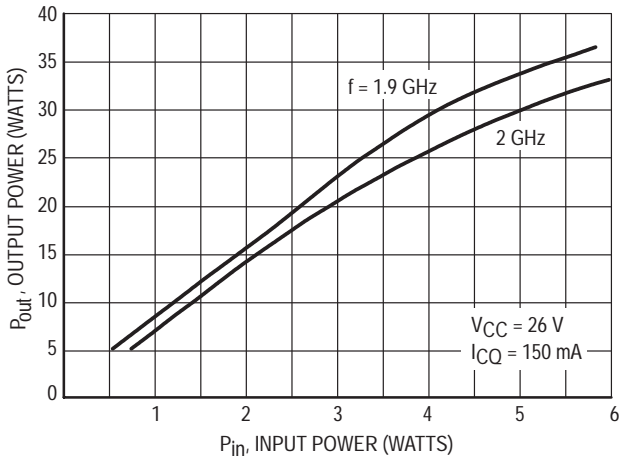


Figure 10. Output Power versus Input Power

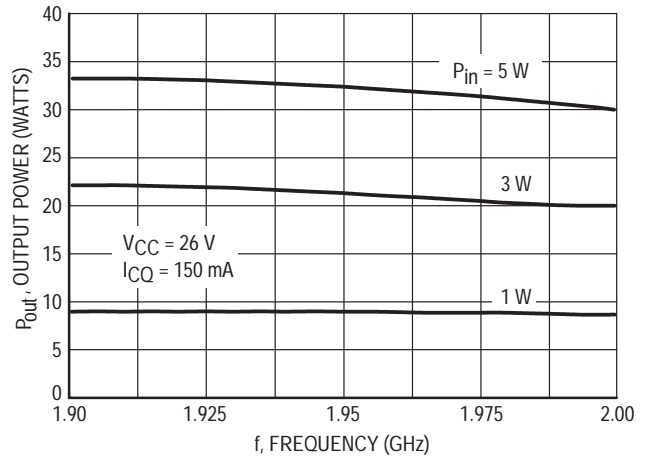


Figure 11. Output Power versus Frequency

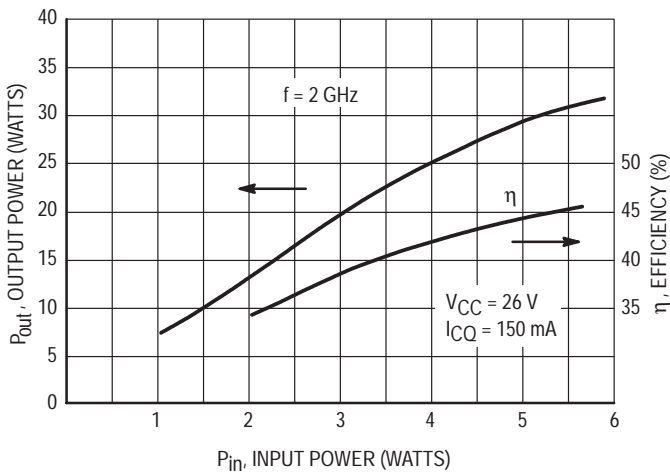


Figure 12. Output Power and Efficiency versus Input Power

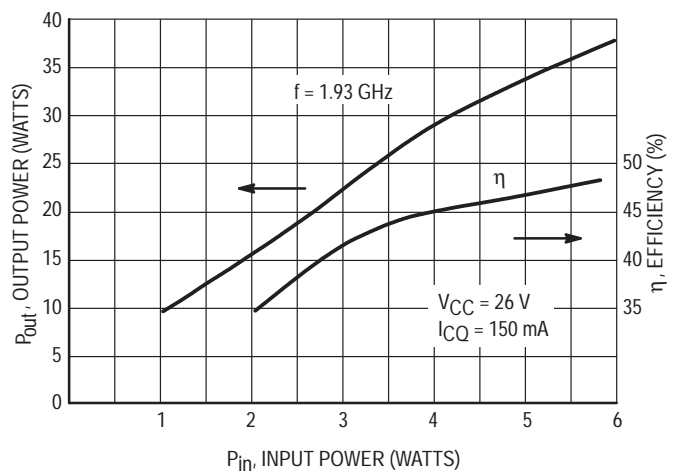


Figure 13. Output Power and Efficiency versus Input Power

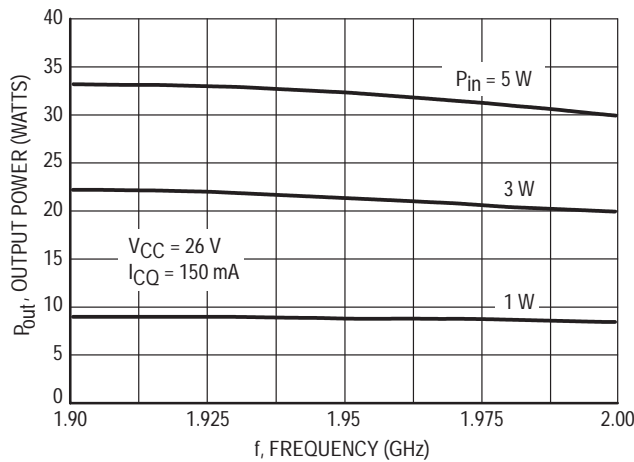
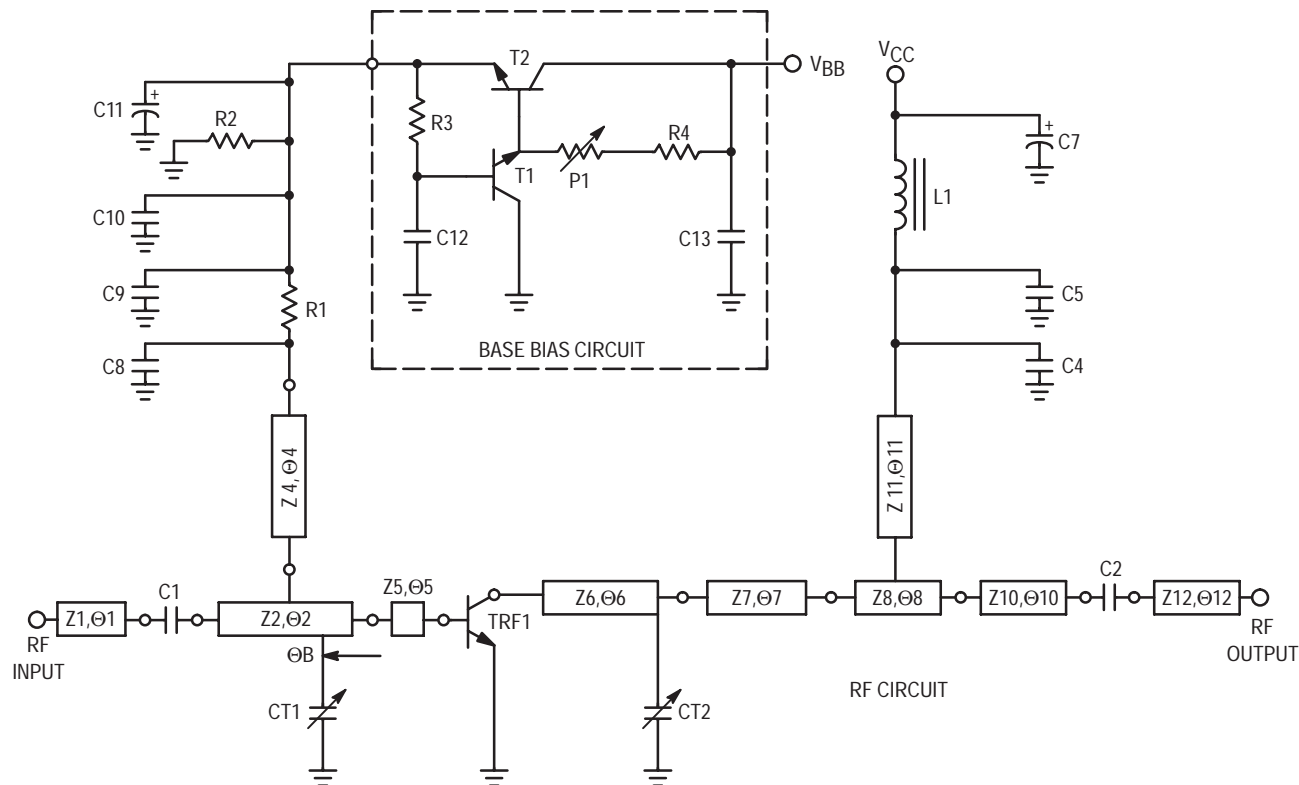


Figure 14. Output Power versus Frequency



Base Bias Circuit

C12, C13	15 nF, Chip Capacitor, Vitramon (0805 A153 JXB)
P1	1 K Ω , Trimmer
R3	47 Ω , Chip Resistor, 0805
R4	330 Ω , Chip Resistor, 0805
T1, T2	Motorola MJD 31C

Decoupling Base Bias Circuit

C4	68 pF, Chip Capacitor, ATC 100A
C5, C9	330 pF, Chip Capacitor, Vitramon (0805 A331 JXB)
C7, C11	4.7 μ F, 63 V, Electrolytic Capacitor
C8	68 pF, Chip Capacitor, ATC 100A
C10	15 nF, Chip Capacitor, Vitramon (0805 A153 JXB)
R1	1.2 Ω , Chip Resistor, 0805
R2	56 Ω , Chip Resistor, 1206

RF Circuit

C1, C2	68 pF, Chip Capacitor, ATC 100A
C20, C21	1.3 pF, Chip Capacitor, ATC 100A
CT1, CT2	Trimmer Capacitor, Gigatrim, Ref 37271
TRF1	MRF6404

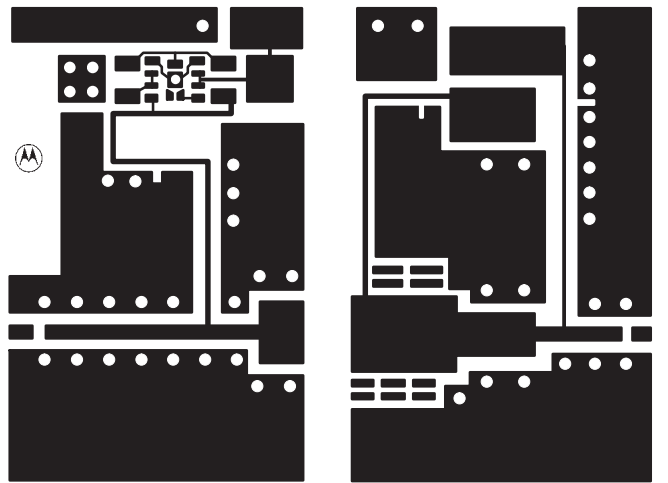
PC Board Material:

$\epsilon_r = 2.55$, H = 0.508 mm, T = 0.035 mm

All Electrical Lengths Are Referenced from λ_g @ f = 1.9 GHz

Z1 : 50 Ω	$\Theta 1$: 10 $^\circ$
Z2 : 50 Ω	$\Theta 2$: 74.5 $^\circ$ ΘB : 16.5 $^\circ$
Z4 : 74 Ω	$\Theta 4$: 68 $^\circ$
Z5 : 12.8 Ω	$\Theta 5$: 21 $^\circ$
Z6 : 10.4 Ω	$\Theta 6$: 49.5 $^\circ$
Z7 : 18 Ω	$\Theta 7$: 36.5 $^\circ$
Z8 : 45 Ω	$\Theta 8$: 20 $^\circ$
Z10 : 50 Ω	$\Theta 10$: 10 $^\circ$
Z11 : 74 Ω	$\Theta 11$: 60 $^\circ$
Z12 : 50 Ω	$\Theta 12$: 10 $^\circ$

Figure 15. 1.9–2.0 GHz Test Circuit Electrical Schematic and Components List



(Not to Scale)

Teflon® Glass 0.5 mm – Double Side 35 μm Cu.

Figure 16. 1.9–2.0 GHz Test Circuit Photomaster

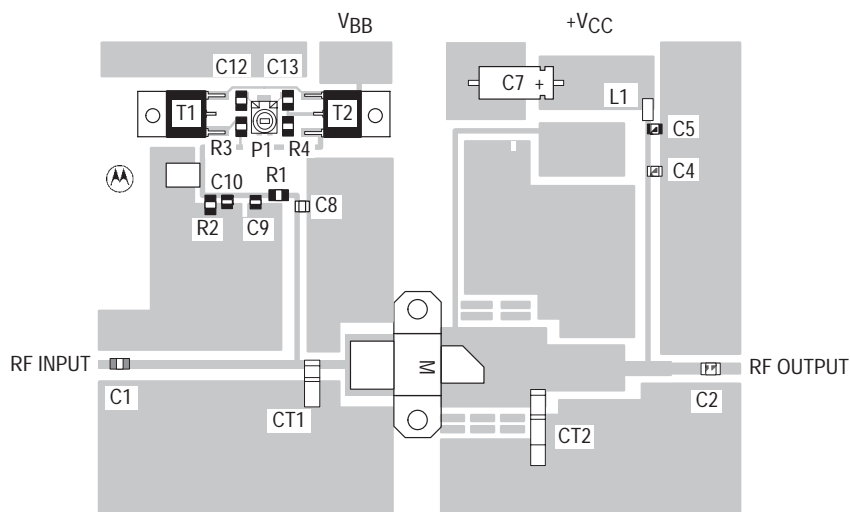
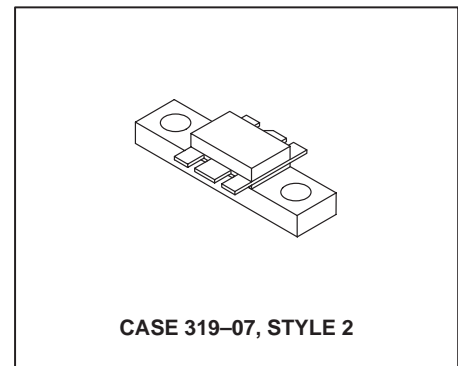
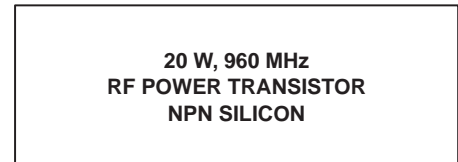


Figure 17. 1.9–2.0 GHz Test Circuit Components Layout

The RF Line
NPN Silicon
RF Power Transistor

The MRF6409 is designed for GSM base stations applications. It incorporates high value emitter ballast resistors, gold metallizations and offers a high degree of reliability and ruggedness.

- To be used in Class AB
- Specified 26 Volts, 960 MHz Characteristics
Output Power — 20 Watts CW
Gain — 11 dB Typ
Efficiency — 60% Typ



MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CEO}	24	Vdc
Collector–Emitter Voltage	V_{CES}	55	Vdc
Emitter–Base Voltage	V_{EBO}	4.0	Vdc
Collector–Current — Continuous	I_C	5.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	45 0.26	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (1)	$R_{\theta JC}$	3.8	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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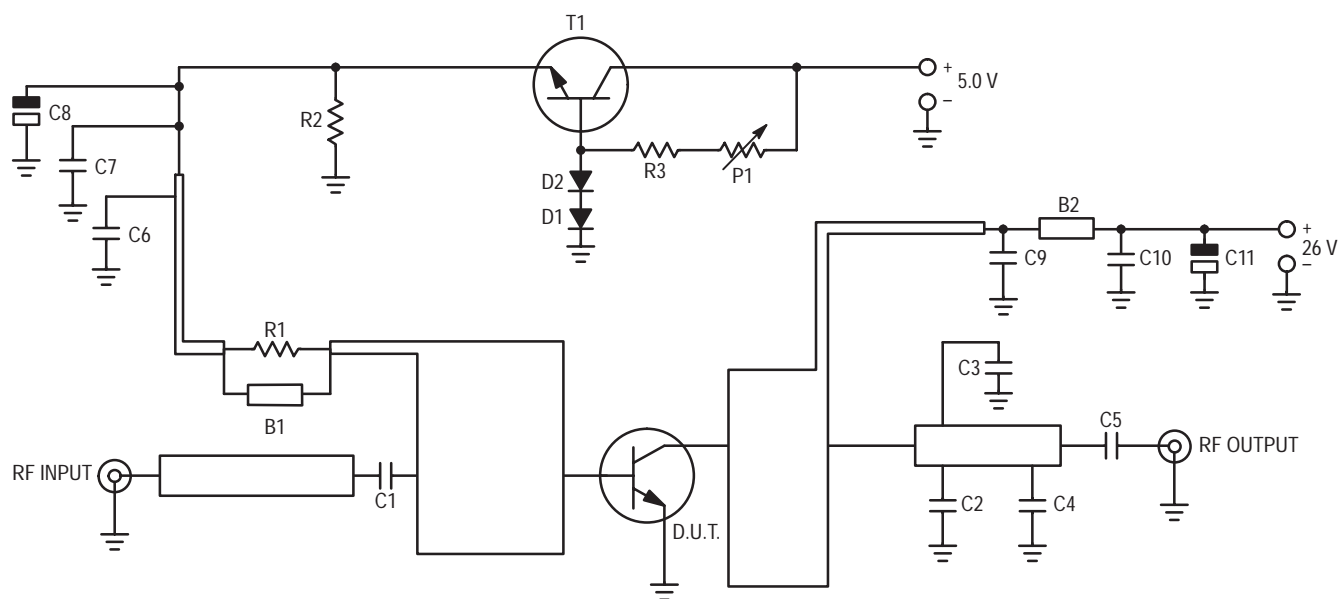
OFF CHARACTERISTICS

Collector–Emitter Breakdown Voltage ($I_C = 20\text{ mAdc}$, $I_B = 0$)	$V_{(BR)CEO}$	24	30	—	Vdc
Emitter–Base Breakdown Voltage ($I_B = 5.0\text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	5.0	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 20\text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	55	60	—	Vdc
Collector–Cutoff Current ($V_{CE} = 30\text{ Vdc}$, $V_{BE} = 0$)	I_{CES}	—	—	6.0	mA

(1) Thermal resistance is determined under specified RF operating condition.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
ON CHARACTERISTICS					
DC Current Gain ($I_{CE} = 1.0 \text{ A dc}$, $V_{CE} = 5.0 \text{ V dc}$)	h_{FE}	20	35	80	—
DYNAMIC CHARACTERISTICS					
Output Capacitance ($V_{CB} = 26 \text{ V dc}$, $I_E = 0$, $f = 1.0 \text{ MHz}$)	C_{ob}	—	18	—	pF
FUNCTIONAL TESTS					
Common-Emitter Amplifier Power Gain ($V_{CC} = 26 \text{ V dc}$, $P_{out} = 20 \text{ W (CW)}$, $I_{CQ} = 50 \text{ mA}$, $f = 960 \text{ MHz}$)	G_{pe}	10	11	—	dB
Collector Efficiency ($V_{CC} = 26 \text{ V dc}$, $P_{out} = 20 \text{ W (CW)}$, $I_{CQ} = 50 \text{ mA}$, $f = 960 \text{ MHz}$)	η	50	60	—	%
Load Mismatch ($V_{CC} = 26 \text{ V dc}$, $P_{out} = 15 \text{ W (CW)}$, $I_{CQ} = 50 \text{ mA}$, $f = 960 \text{ MHz}$, Load VSWR = 3:1, All Phase Angles at Frequency of Test)	Ψ	No Degradation in Output Power			



- | | | | |
|---------|---|--------|---|
| B1, B2 | Ferrite Bead | C11 | 4.7 μF , 50 V, Tantalum Capacitor |
| C1 | 3.3 pF, Chip Capacitor, High Q | D1, D2 | Diode BAS16 Type or Equivalent |
| C2, C3 | 4.7 pF, Chip Capacitor, High Q | P1 | 1.0 k Ω , Trimmer |
| C4 | 2.2 pF, Chip Capacitor, High Q | R1 | 3.3 Ω , Chip Resistor |
| C5 | 82 pF, Chip Capacitor, High Q | R2 | 68 Ω , Chip Resistor |
| C6, C9 | 330 pF, Chip Capacitor, High Q | R3 | 2.2 k Ω , Resistor |
| C7, C10 | 0.1 μF , Chip Capacitor | T1 | NPN Transistor |
| C8 | 22 μF , 16 V, Tantalum Capacitor | Board | Glass Teflon [®] , $\epsilon_r = 2.55$, H = 1/50 inch |

Figure 1. Test Circuit Electrical Schematic

TYPICAL CHARACTERISTICS

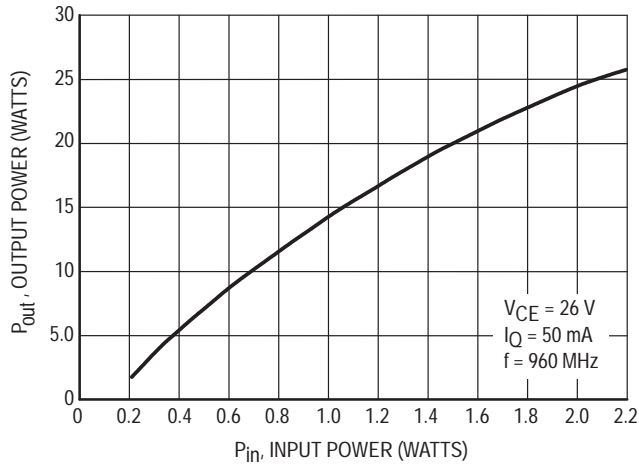


Figure 2. Output Power versus Input Power (CW)

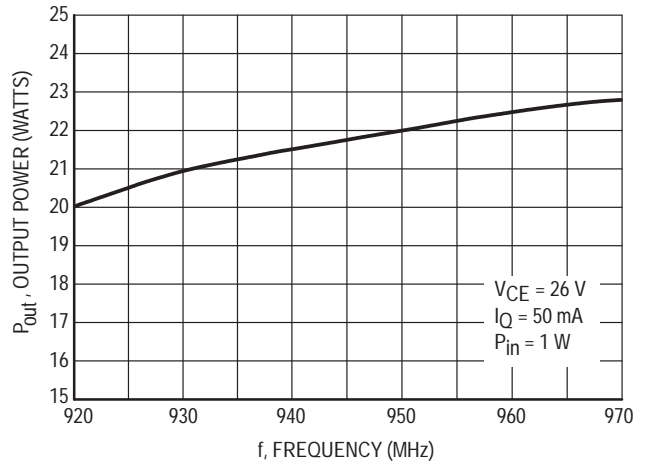


Figure 3. Output Power versus Frequency (CW)

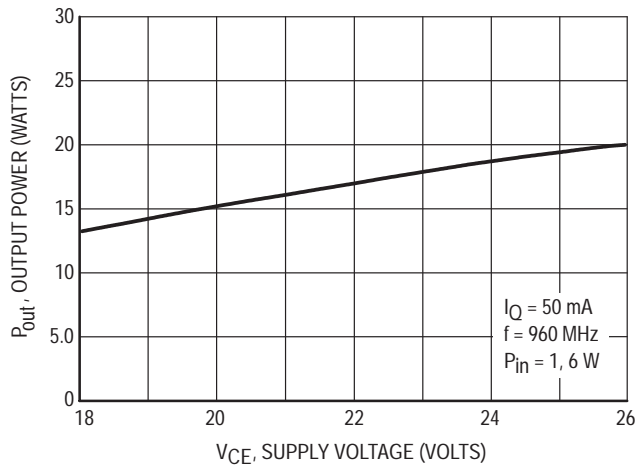


Figure 4. Output Power versus Supply Voltage (CW)

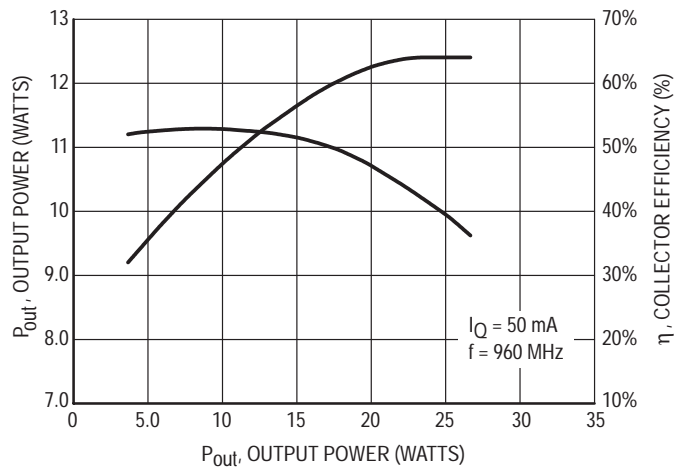


Figure 5. Power Gain and Efficiency versus Output Power

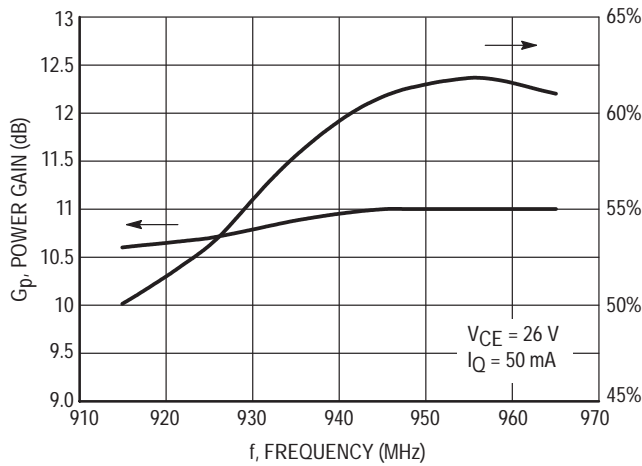


Figure 6. Typical Broadband Performances

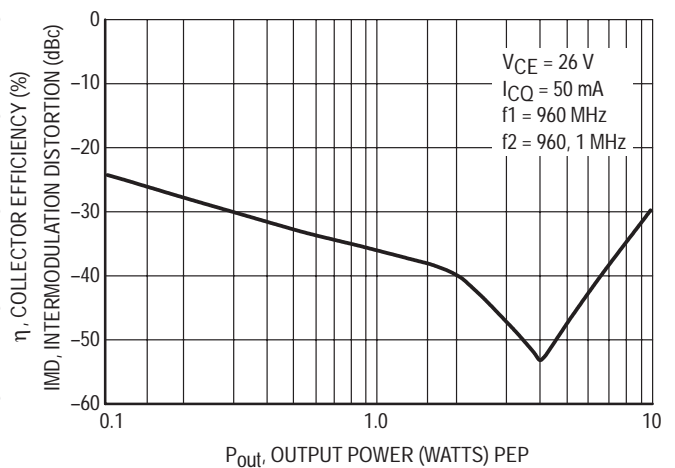
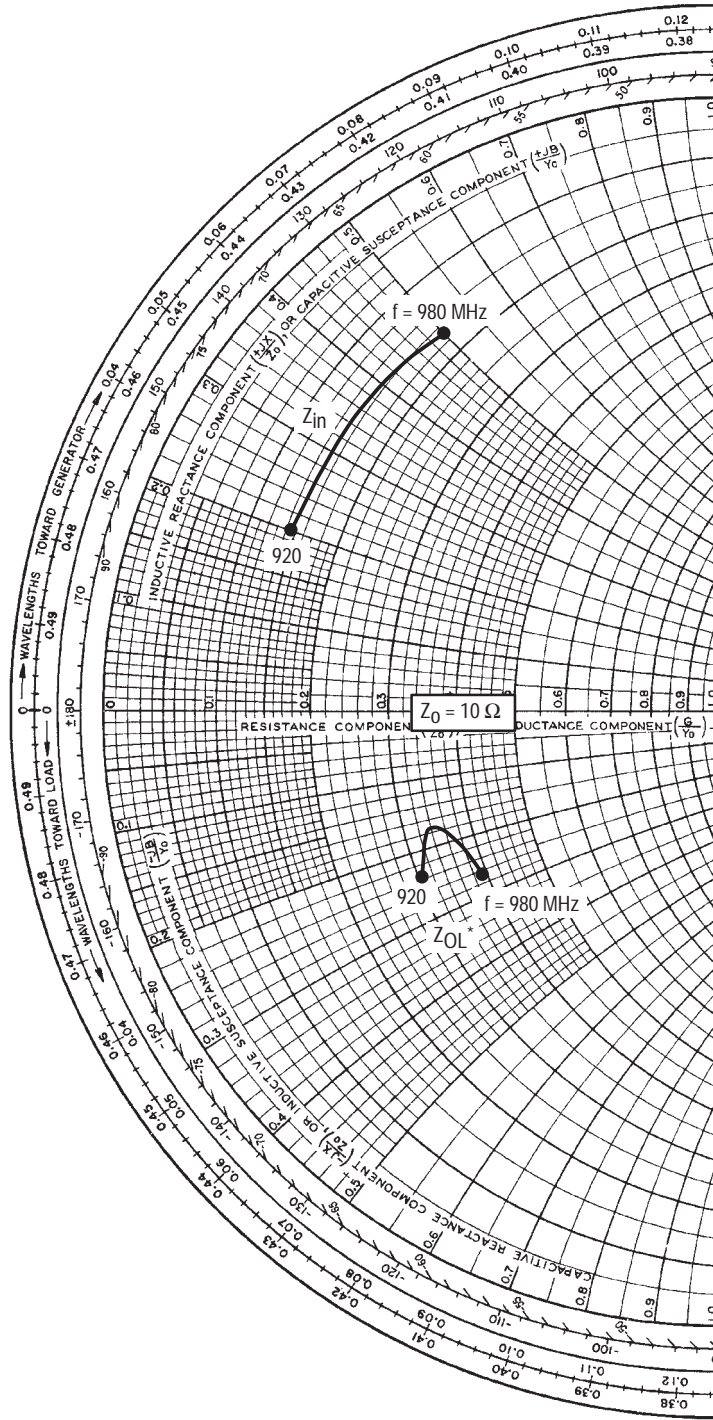


Figure 7. Intermodulation Distortion versus Output Power



f (MHz)	Z _{in} (Ω)	Z _{OL} * (Ω)
920	1.4 + j3.0	3.2 - j2.5
940	1.5 + j3.9	3.5 - j1.88
960	1.5 + j4.2	3.9 - j2.5
980	1.6 + j4.4	4.0 - j2.8

Z_{OL}*: Conjugate of optimum load impedance into which the device operates at a given output power, voltage, current and frequency.

Figure 8. Input and Output Impedances with Circuit Tuned for Maximum Gain @ V_{CC} = 26 V, I_{CQ} = 50 mA, P_{out} = 20 W (CW)

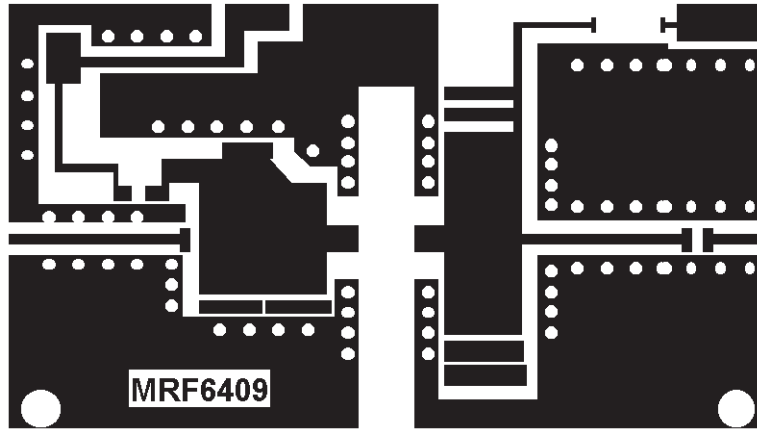


Figure 9. 960 MHz Test Circuit RF, Photomaster Scale 1:1
(Reduced 18% in printed data book, DL110/D)

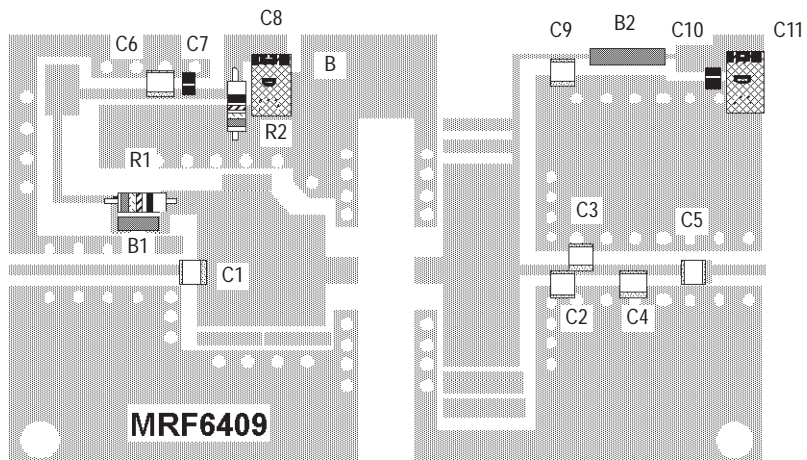


Figure 10. 960 MHz Test Circuit RF, Photomaster Scale 1:1
and Components Location
(Reduced 18% in printed data book, DL110/D)

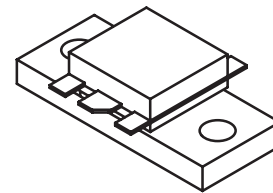
The RF Line
NPN Silicon
RF Power Transistor

MRF6414

50 W, 960 MHz
RF POWER TRANSISTOR
NPN SILICON

The MRF6414 is designed for 26 volt UHF large signal, common emitter, class AB linear amplifier applications.

- Specified 26 Volt, 960 MHz Characteristics
Output Power = 50 Watts
Minimum Gain = 8.5 dB @ 960 MHz, Class AB
Minimum Efficiency = 50% @ 960 MHz, 50 Watts
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration



CASE 333A-02, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CEO}	28	Vdc
Collector-Base Voltage	V_{CBO}	65	Vdc
Emitter-Base Voltage	V_{EBO}	4	Vdc
Collector-Current — Continuous	I_C	6	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	134 0.77	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.3	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector-Emitter Breakdown Voltage ($I_C = 20 \text{ mAdc}$, $I_B = 0$)	$V_{(BR)CEO}$	28	—	—	Vdc
Collector-Base Breakdown Voltage ($I_C = 20 \text{ mAdc}$, $I_E = 0$)	$V_{(BR)CBO}$	65	—	—	Vdc
Emitter-Base Breakdown Voltage ($I_E = 10 \text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	4	—	—	Vdc
Collector-Emitter Leakage Current ($V_{CE} = 30 \text{ Vdc}$, $R_{BE} = 75 \Omega$)	I_{CER}	—	—	10	mAdc

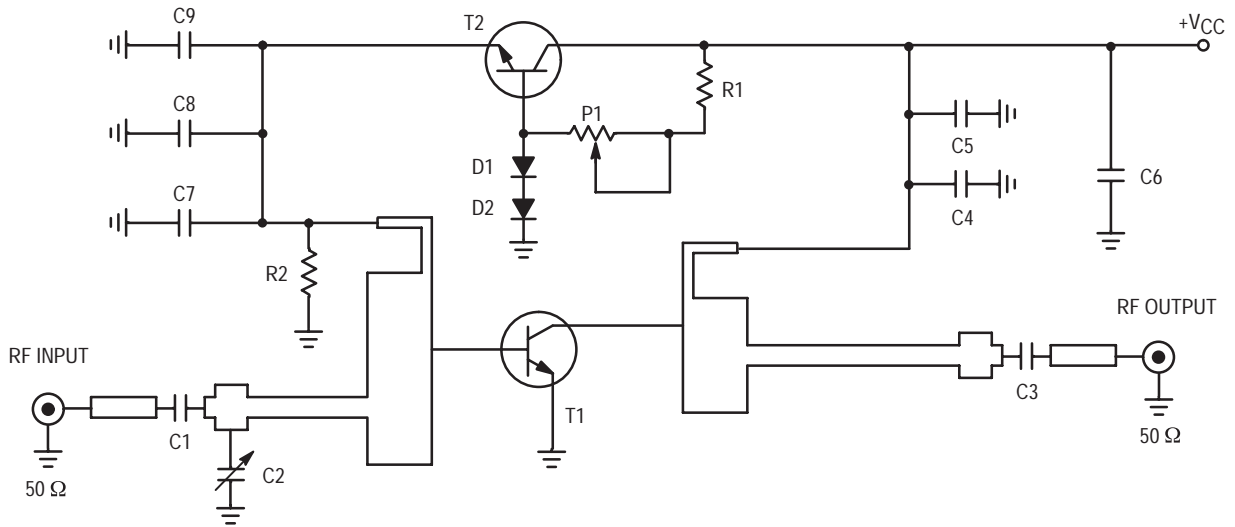
ON CHARACTERISTICS

DC Current Gain ($I_{CE} = 1 \text{ Adc}$, $V_{CE} = 5 \text{ Vdc}$)	h_{FE}	30	—	120	—
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ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
DYNAMIC CHARACTERISTICS					
Output Capacitance ($V_{CB} = 26 \text{ Vdc}$, $I_E = 0$, $f = 1 \text{ MHz}$) (1)	C_{ob}	—	45	—	pF
FUNCTIONAL TESTS					
Common-Emitter Amplifier Power Gain ($V_{CC} = 26 \text{ Vdc}$, $P_{out} = 50 \text{ W}$, $I_{CQ} = 200 \text{ mA}$, $f = 960 \text{ MHz}$)	G_{pe}	8.5	—	—	dB
Collector Efficiency ($V_{CC} = 26 \text{ Vdc}$, $P_{out} = 50 \text{ W}$, $I_{CQ} = 200 \text{ mA}$, $f = 960 \text{ MHz}$)	η	50	55	—	%
Output Mismatch Stress ($V_{CC} = 26 \text{ Vdc}$, $P_{out} = 50 \text{ W}$, $I_{CQ} = 200 \text{ mA}$, $f = 960 \text{ MHz}$) VSWR = 3:1; all phase angles at frequency of test	Ψ	No Degradation in Output Power			

(1) For information only. It is not measurable in MRF6414 because of internal matching network.



C1, C3	100 pF, Chip Capacitor, High Q	P1	1 k Ω , Trimmer
C2, C7	330 pF, Chip Capacitor, 0805	R1	1 k Ω , Resistor
C5, C8	10 nF, Chip Capacitor, 0805	R2	58 Ω , Resistor, 0805
C6	15 μF , Capacitor, 63 V	T1	MRF6414
C9	100 μF , Capacitor, 16 V	T2	Transistor NPN Type BD135
D1, D2	Diode 1N4007		

Figure 1. 960 MHz Test Circuit Schematic

TYPICAL CHARACTERISTICS

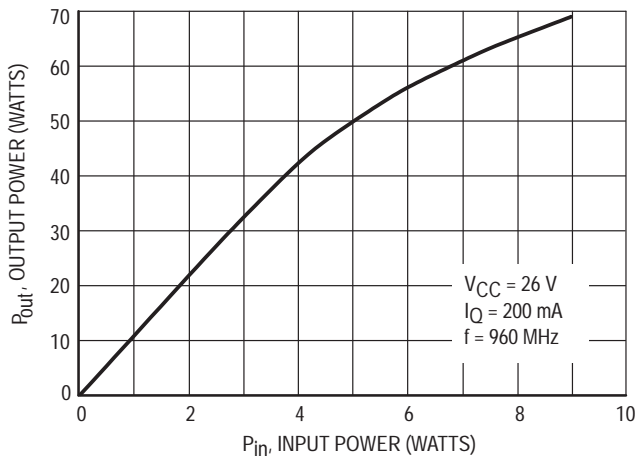


Figure 2. Output Power versus Input Power (Typical)

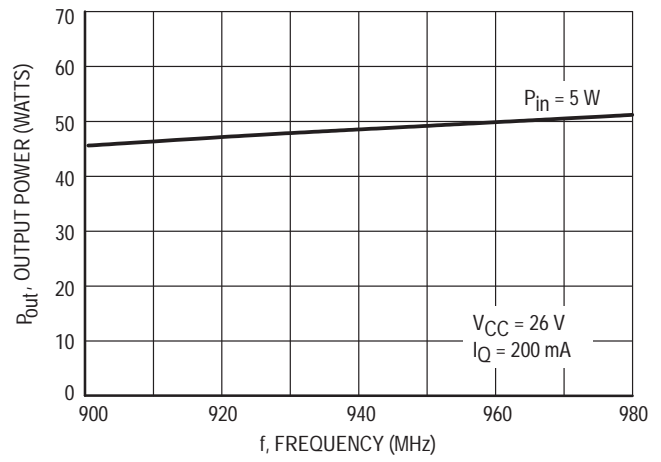


Figure 3. Output Power versus Frequency

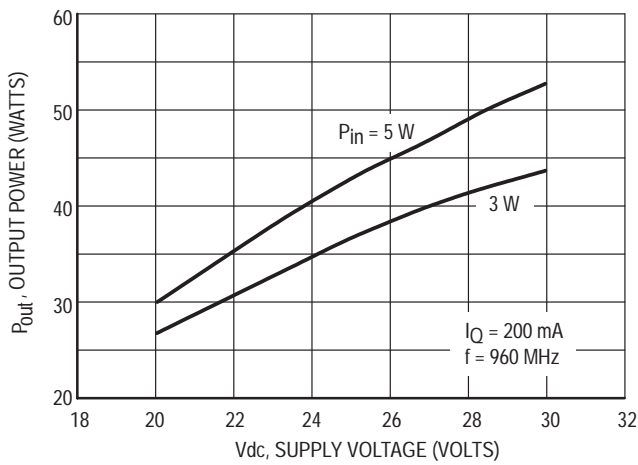


Figure 4. Output Power versus Supply Voltage

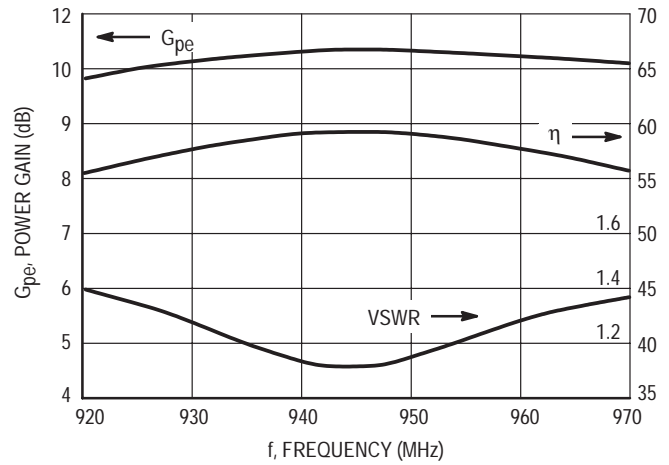
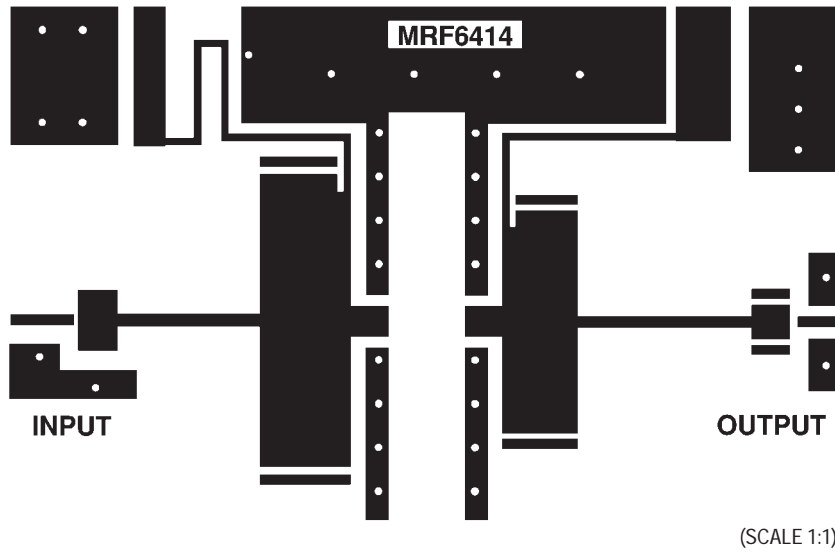


Figure 5. Typical Broadband Amplifier



TEST CIRCUIT @ $f = 960$ MHz
 TEFLON® GLASS 1/50 INCH $\epsilon_r = 2.55$

**Figure 6. MRF6414 Photomaster
 (Reduced 18% in printed data book, DL110/D)**

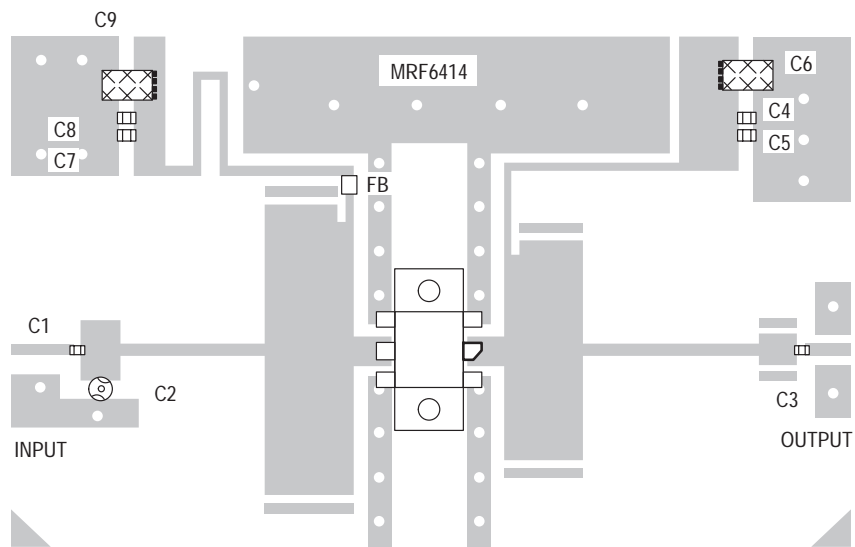
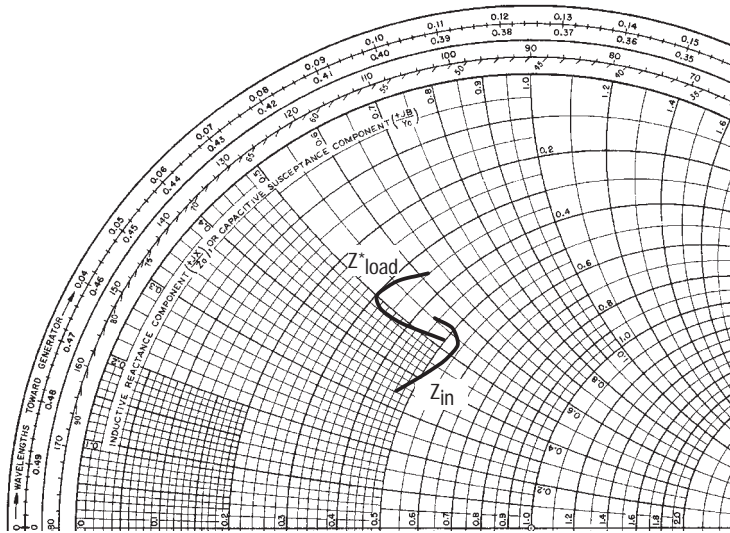


Figure 7. 960 MHz Test Circuit Components Layout



Normalized to 10 Ω

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
900	$4.4 + j4.6$	$4.7 + j4.7$
935	$5.1 + j4.8$	$4.0 + j3.9$
960	$5.4 + j3.6$	$3.7 + j4.5$
980	$4.7 + j2.5$	$3.4 + j4.7$

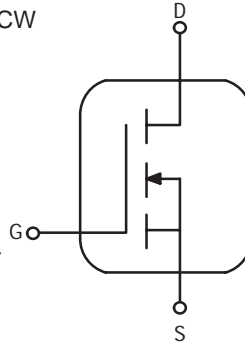
Z_{OL}^* : Conjugate of optimum load impedance into which the device operates at a given output power, voltage, current and frequency.

Figure 8. Input and Output Impedances with Circuit Tuned for Maximum Gain
 @ $V_{CC} = 26\text{ V}$, $I_Q = 200\text{ mA}$, $P_{out} = 50\text{ W}$

The RF MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

Designed for Class A-AB common source, linear power amplifiers in the 960 MHz range. The MRF6522-10R1 has been specifically designed for use in Communications Network (GSM) base stations. The package offers the advantage of SMD.

- Specified 26 Volts, 960 MHz, Class AB Characteristics
Output Power = 10 Watts CW
Power Gain = 15 dB Min @ 960 MHz, 10 Watts CW
Drain Efficiency = 48% Min @ 960 MHz, 10 Watts CW
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- S-Parameter Characterization at High Bias Levels
- Bottom Side Source Eliminates DC Isolators, Reducing Common Mode Inductances
- Available in Tape and Reel. R1 Suffix = 500 Units per 12 mm, 7 inch Reel.



MRF6522-10R1

**960 MHz, 10 W, 26 V
LATERAL N-CHANNEL
RF POWER MOSFET**



CASE 458C-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	± 20	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	29 0.17	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (1)	$R_{\theta JC}$	4.0	$^\circ\text{C/W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Drain-Source Breakdown Voltage ($V_{GS} = 0$ Vdc, $I_D = 0.2$ mA)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 26$ Vdc, $V_{GS} = 0$)	I_{DSS}	—	—	1.0	$\mu\text{A}dc$
Gate-Source Leakage Current ($V_{GS} = 20$ Vdc, $V_{DS} = 0$)	I_{GSS}	—	—	1.0	$\mu\text{A}dc$

(1) Thermal resistance is determined under specified RF operating condition.

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 50\ \mu\text{A}$)	$V_{GS(th)}$	1.25	3.0	4.0	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 100\text{ mA}$)	$V_{GS(Q)}$	2.25	4.0	5.0	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 0.5\text{ A}$)	$V_{DS(on)}$	—	—	0.9	Vdc

DYNAMIC CHARACTERISTICS

Input Capacitance ($V_{DS} = 26\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{iss}	—	17	—	pF
Output Capacitance ($V_{DS} = 26\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{oss}	—	10	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ V}$, $V_{GS} = 0\text{ V}$, $f = 1.0\text{ MHz}$)	C_{rss}	—	0.9	—	pF

FUNCTIONAL TESTS (In Motorola Test Fixture)

Common–Source Power Gain ($V_{DS} = 26\text{ V}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 100\text{ mA}$, $f = 960\text{ MHz}$)	G_{ps}	15	17	—	dB
Drain Efficiency ($V_{DS} = 26\text{ V}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 100\text{ mA}$, $f = 960\text{ MHz}$)	η	48	50	—	%
Input Return Loss ($V_{DS} = 26\text{ V}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 100\text{ mA}$, $f = 960\text{ MHz}$)	IRL	—	—	–9	dB

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

TYPICAL CHARACTERISTICS

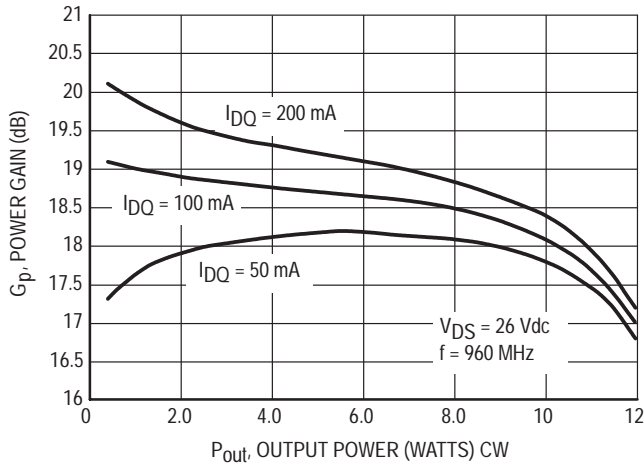


Figure 1. Power Gain versus Output Power

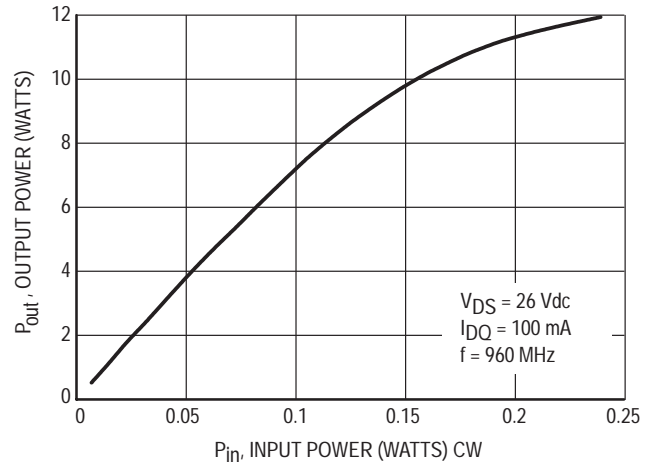


Figure 2. Output Power versus Input Power

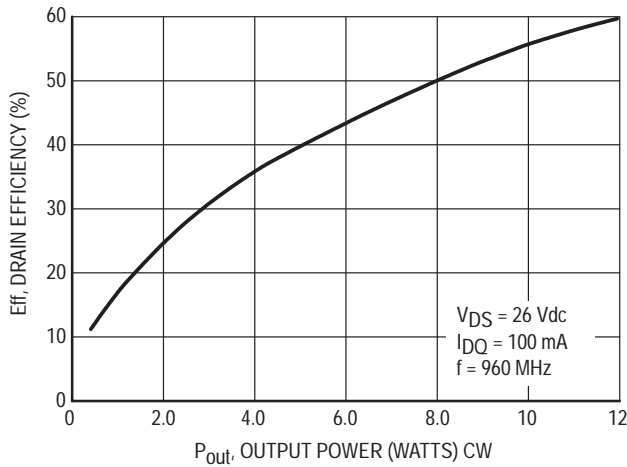


Figure 3. Drain Efficiency versus Output Power

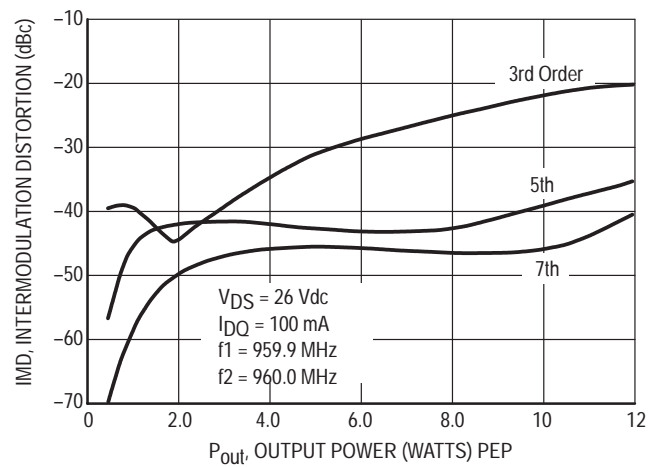
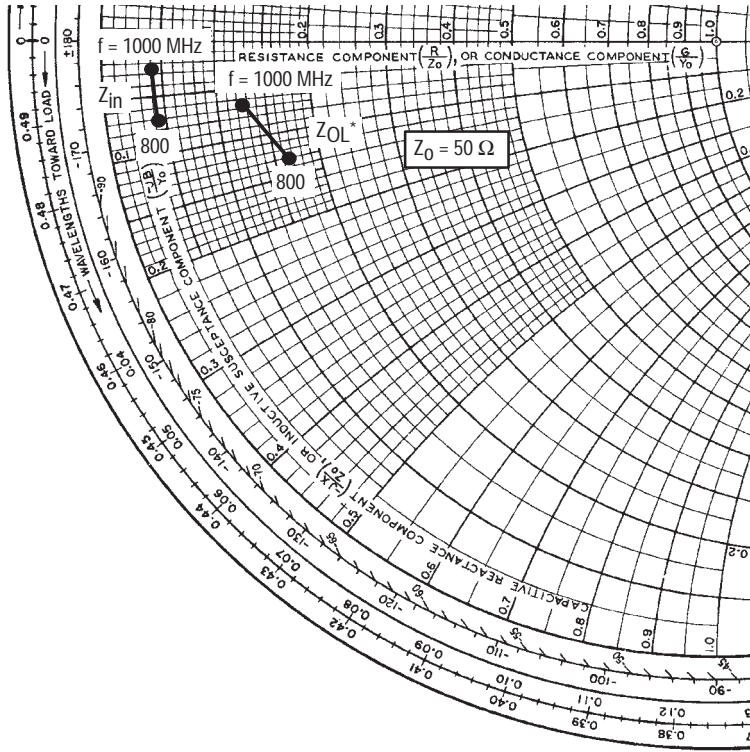


Figure 4. Intermodulation Distortion Products versus Output Power

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LAST ORDER 31JUL04 LAST SHIP 31JAN05



f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
800	$2.20 - j3.00$	$8.50 - j6.20$
825	$2.20 - j2.80$	$8.43 - j6.15$
850	$2.20 - j2.60$	$8.35 - j6.10$
875	$2.20 - j2.40$	$8.28 - j6.08$
900	$2.20 - j2.20$	$8.20 - j6.05$
925	$2.19 - j1.86$	$7.95 - j5.70$
950	$2.13 - j1.68$	$7.50 - j4.75$
975	$2.03 - j1.45$	$6.90 - j3.58$
1000	$2.00 - j1.00$	$6.50 - j3.00$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance into which the device operates at a given output power, voltage, current and frequency.

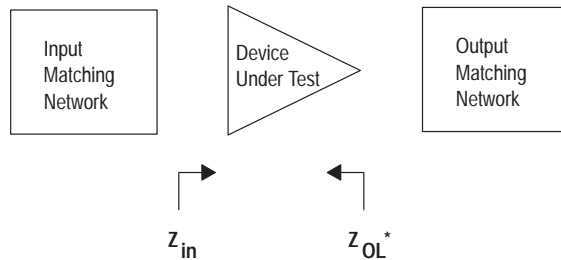


Figure 5. Series Equivalent Input and Output Impedance

Table 1. Common Source S-Parameters at $V_{DS} = 12$ Vdc, $I_D = 100$ mAdc

f GHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
0.500	0.794	-158	2.77	54	0.050	-29	0.720	-150
0.525	0.800	-159	2.61	52	0.049	-32	0.730	-151
0.550	0.807	-160	2.45	49	0.048	-33	0.738	-152
0.575	0.811	-161	2.31	48	0.047	-35	0.746	-153
0.600	0.816	-162	2.18	46	0.046	-37	0.755	-154
0.625	0.822	-163	2.06	44	0.045	-38	0.763	-155
0.650	0.826	-164	1.95	42	0.043	-40	0.770	-156
0.675	0.832	-165	1.85	40	0.042	-41	0.779	-157
0.700	0.836	-166	1.75	39	0.041	-41	0.785	-158
0.725	0.841	-166	1.66	37	0.040	-42	0.793	-159
0.750	0.846	-167	1.58	35	0.039	-44	0.800	-160
0.775	0.851	-168	1.51	34	0.038	-45	0.805	-161
0.800	0.855	-168	1.44	32	0.037	-46	0.812	-162
0.825	0.858	-169	1.37	31	0.036	-47	0.818	-163
0.850	0.863	-170	1.31	29	0.035	-48	0.824	-164
0.875	0.866	-171	1.25	28	0.034	-49	0.830	-165
0.900	0.869	-172	1.20	27	0.033	-50	0.835	-166
0.925	0.872	-172	1.15	25	0.031	-51	0.840	-166
0.950	0.876	-173	1.10	24	0.030	-52	0.846	-167
0.975	0.879	-174	1.06	23	0.029	-52	0.850	-168
1.000	0.882	-174	1.02	22	0.028	-53	0.853	-169

Table 2. Common Source S-Parameters at $V_{DS} = 12$ Vdc, $I_D = 250$ mAdc

f GHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
0.500	0.784	-164	3.49	59	0.041	-22	0.690	-158
0.525	0.789	-165	3.29	57	0.040	-25	0.697	-159
0.550	0.794	-166	3.11	55	0.040	-26	0.705	-160
0.575	0.798	-167	2.94	53	0.038	-26	0.711	-160
0.600	0.802	-167	2.79	51	0.037	-28	0.719	-161
0.625	0.806	-168	2.65	50	0.037	-30	0.726	-162
0.650	0.811	-169	2.52	48	0.036	-31	0.732	-162
0.675	0.814	-169	2.40	46	0.035	-32	0.740	-163
0.700	0.819	-170	2.28	45	0.034	-32	0.747	-164
0.725	0.823	-171	2.18	43	0.034	-34	0.753	-164
0.750	0.827	-171	2.08	42	0.032	-36	0.760	-165
0.775	0.831	-172	1.99	40	0.032	-36	0.765	-166
0.800	0.834	-172	1.90	39	0.031	-36	0.772	-166
0.825	0.838	-173	1.82	37	0.031	-38	0.778	-167
0.850	0.842	-174	1.74	36	0.029	-38	0.783	-168
0.875	0.845	-174	1.67	35	0.028	-39	0.790	-169
0.900	0.850	-175	1.61	33	0.028	-39	0.797	-169
0.925	0.852	-175	1.54	32	0.027	-41	0.801	-170
0.950	0.854	-176	1.48	31	0.027	-42	0.807	-170
0.975	0.859	-176	1.43	30	0.025	-41	0.810	-171
1.000	0.861	-177	1.38	28	0.025	-42	0.815	-171

Table 3. Common Source S-Parameters at $V_{DS} = 26$ Vdc, $I_D = 100$ mAdc

f GHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
0.500	0.832	-155	4.05	56	0.033	-25	0.687	-135
0.525	0.836	-156	3.81	54	0.033	-27	0.697	-137
0.550	0.841	-157	3.58	51	0.034	-28	0.707	-138
0.575	0.845	-159	3.38	49	0.032	-31	0.718	-140
0.600	0.849	-160	3.19	47	0.031	-32	0.728	-141
0.625	0.853	-161	3.02	45	0.030	-34	0.737	-143
0.650	0.856	-162	2.86	43	0.029	-35	0.746	-144
0.675	0.861	-163	2.71	42	0.028	-37	0.755	-145
0.700	0.865	-164	2.57	40	0.028	-37	0.762	-147
0.725	0.868	-165	2.44	38	0.026	-38	0.771	-148
0.750	0.871	-166	2.32	37	0.025	-40	0.779	-149
0.775	0.875	-166	2.21	35	0.025	-41	0.786	-150
0.800	0.877	-167	2.11	33	0.023	-41	0.793	-151
0.825	0.880	-168	2.02	32	0.022	-43	0.800	-152
0.850	0.884	-169	1.92	30	0.022	-43	0.808	-154
0.875	0.886	-170	1.84	29	0.021	-44	0.815	-155
0.900	0.889	-171	1.76	27	0.020	-43	0.820	-156
0.925	0.892	-171	1.68	26	0.020	-46	0.826	-157
0.950	0.894	-172	1.61	24	0.019	-45	0.832	-158
0.975	0.897	-173	1.55	23	0.018	-47	0.837	-159
1.000	0.899	-173	1.49	22	0.017	-48	0.842	-160

Table 4. Common Source S-Parameters at $V_{DS} = 26$ Vdc, $I_D = 250$ mAdc

f GHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	φ	S ₂₁	φ	S ₁₂	φ	S ₂₂	φ
0.500	0.824	-160	5.02	59	0.029	-21	0.627	-143
0.525	0.828	-161	4.74	57	0.027	-22	0.638	-144
0.550	0.832	-162	4.47	55	0.026	-22	0.648	-145
0.575	0.835	-163	4.23	53	0.027	-24	0.658	-146
0.600	0.838	-164	4.01	51	0.025	-26	0.669	-147
0.625	0.842	-165	3.81	50	0.025	-26	0.678	-148
0.650	0.844	-166	3.61	48	0.024	-25	0.687	-150
0.675	0.848	-167	3.43	46	0.023	-28	0.697	-150
0.700	0.851	-168	3.27	44	0.023	-30	0.706	-151
0.725	0.855	-168	3.12	43	0.022	-30	0.714	-152
0.750	0.858	-169	2.97	41	0.021	-31	0.723	-153
0.775	0.861	-170	2.84	39	0.021	-31	0.731	-154
0.800	0.863	-170	2.72	38	0.020	-32	0.738	-155
0.825	0.866	-171	2.60	36	0.019	-33	0.746	-156
0.850	0.870	-172	2.49	35	0.018	-34	0.754	-157
0.875	0.871	-173	2.38	33	0.018	-34	0.763	-158
0.900	0.875	-173	2.29	32	0.017	-35	0.768	-159
0.925	0.877	-174	2.20	30	0.016	-36	0.776	-160
0.950	0.879	-175	2.11	29	0.016	-36	0.782	-161
0.975	0.883	-175	2.03	28	0.016	-34	0.787	-161
1.000	0.885	-176	1.95	27	0.015	-34	0.793	-162

LIFETIME BUY

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Table 5. Common Source S-Parameters at $V_{DS} = 26$ Vdc, $I_D = 500$ mAdc

f GHz	S ₁₁		S ₂₁		S ₁₂		S ₂₂	
	S ₁₁	∠	S ₂₁	∠	S ₁₂	∠	S ₂₂	∠
0.500	0.832	-162	5.08	60	0.025	-17	0.612	-145
0.525	0.834	-162	4.80	58	0.025	-20	0.624	-146
0.550	0.838	-164	4.53	56	0.024	-21	0.635	-147
0.575	0.840	-164	4.29	54	0.024	-21	0.644	-148
0.600	0.844	-165	4.07	52	0.023	-23	0.655	-149
0.625	0.847	-166	3.86	50	0.023	-24	0.664	-150
0.650	0.849	-167	3.66	48	0.022	-25	0.673	-151
0.675	0.852	-168	3.48	46	0.021	-27	0.682	-152
0.700	0.856	-169	3.32	45	0.021	-28	0.690	-153
0.725	0.858	-170	3.17	43	0.020	-28	0.701	-154
0.750	0.861	-170	3.02	41	0.019	-30	0.709	-154
0.775	0.864	-171	2.89	40	0.019	-29	0.716	-155
0.800	0.866	-172	2.76	38	0.018	-29	0.723	-156
0.825	0.869	-172	2.65	37	0.017	-29	0.733	-157
0.850	0.872	-173	2.53	35	0.017	-31	0.742	-158
0.875	0.874	-174	2.43	34	0.016	-31	0.751	-159
0.900	0.878	-175	2.33	32	0.015	-31	0.757	-160
0.925	0.879	-175	2.24	31	0.015	-32	0.763	-161
0.950	0.881	-176	2.15	29	0.014	-31	0.770	-161
0.975	0.884	-176	2.07	28	0.014	-31	0.775	-162
1.000	0.886	-177	2.00	27	0.013	-30	0.781	-163

LIFETIME BUY

LAST SHIP 31JAN05
LAST ORDER 31JUL04

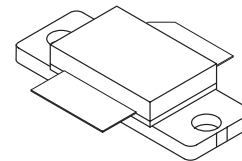
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for GSM 900 frequency band, the high gain and broadband performances of this device makes it ideal for large-signal, common source amplifier applications in 26 volt base station equipment.

- Specified Performance @ Full GSM Band, 921-960 MHz, 26 Volts
Output Power, P1dB — 80 Watts (Typ)
Power Gain @ P1dB — 16 dB (Typ)
Efficiency @ P1dB — 58% (Typ)
- MRF6522-70 Available in Tape and Reel by Adding R3 Suffix to Part Number. MRF6522-70R3 = 250 Units per 32 mm, 13 inch Reel.

MRF6522-70
MRF6522-70R3

921 – 960 MHz, 70 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 465D-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	65	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	7	Adc
Total Device Dissipation @ T _C ≥ 25°C Derate above 25°C	P _D	159 0.9	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	200	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	1.1	°C/W

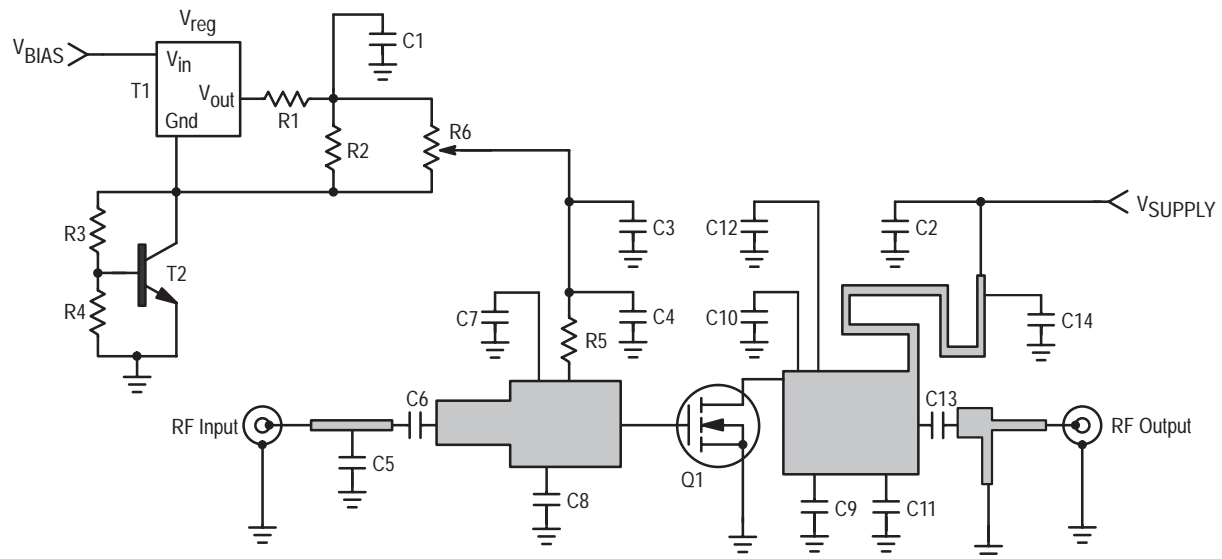
NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 20\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Gate–Source Leakage Current ($V_{GS} = 20\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 400\ \text{mAdc}$)	$V_{GS(Q)}$	3	4	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\ \text{Adc}$)	$V_{DS(on)}$	—	0.15	0.6	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\ \text{Adc}$)	g_{fs}	2	3	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{iss}	—	130	—	pF
Output Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{oss}	41	47	52	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{rss}	2.4	3	3.4	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Output Power (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 400\ \text{mA}$, $f = \text{Full GSM Band } 921 - 960\ \text{MHz}$)	P_{1dB}	73	80	—	W
Common–Source Amplifier Power Gain @ P1dB (Min) (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 400\ \text{mA}$, $f = \text{Full GSM Band } 921 - 960\ \text{MHz}$)	G_{ps}	14	16	18	dB
Drain Efficiency @ $P_{out} = 50\ \text{W}$ ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 400\ \text{mA}$, $f = \text{Full GSM Band } 921 - 960\ \text{MHz}$)	η_1	47	51	—	%
Drain Efficiency @ P1dB (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 400\ \text{mA}$, $f = \text{Full GSM Band } 921 - 960\ \text{MHz}$)	η_2	—	58	—	%
Input Return Loss @ $P_{out} = 50\ \text{W}$ ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 400\ \text{mA}$, $f = 921\ \text{MHz}$ and $960\ \text{MHz}$ $f = 940\ \text{MHz}$)	IRL	10 15	— —	— —	dB
Output Mismatch Stress (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 400\ \text{mA}$, $f = \text{Full GSM Band } 921 - 960\ \text{MHz}$, $V_{SWR} = 5:1$, All Phase Angles)	Ψ	No Degradation In Output Power Before and After Test			

(1) Value excludes the input matching.

(2) To meet application requirements, Motorola test fixtures have been designed to cover full GSM 900 band ensuring batch–to–batch consistency.



C1	1.0 μ F, Chip Capacitor 0805	R3	1.2 k Ω , Chip Resistor 0805
C2	10 μ F, 35 Vdc Tantalum Capacitor	R4	2.2 k Ω , Chip Resistor 0805
C3	100 nF, Chip Capacitor	R5	220 Ω , Chip Resistor 0805
C4, C6, C14	22 pF, ACCU-P Chip Capacitor 0805	R6	5.0 k Ω SMD Potentiometer
C5	2.7 pF, ACCU-P Chip Capacitor 0805	T1	LP2951 Micro-8
C7, C8, C13	4.7 pF, ACCU-P Chip Capacitor 0805	T2	BC847 SOT-23
C9, C10	8.2 pF, ACCU-P Chip Capacitor 0805		
C11, C12	2.2 pF, ACCU-P Chip Capacitor 0805		
R1	10 Ω , Chip Resistor 0805		
R2	1.0 k Ω , Chip Resistor 0805		
		SUBSTRATE	GI180 0.8 mm

Figure 1. MRF6522-70 Test Circuit Schematic

TYPICAL CHARACTERISTICS

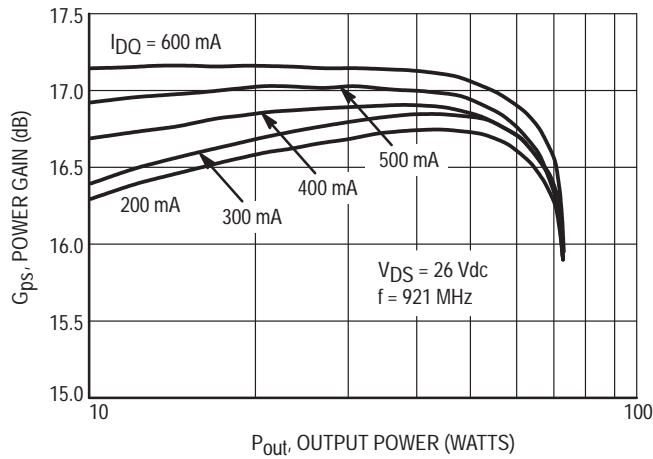


Figure 2. Power Gain versus Output Power

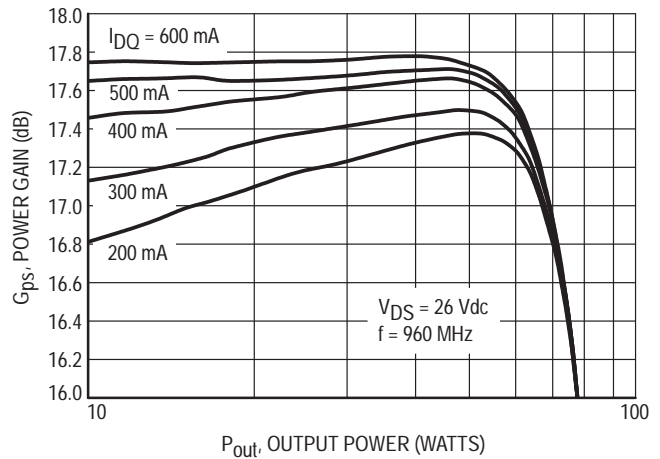


Figure 3. Power Gain versus Output Power

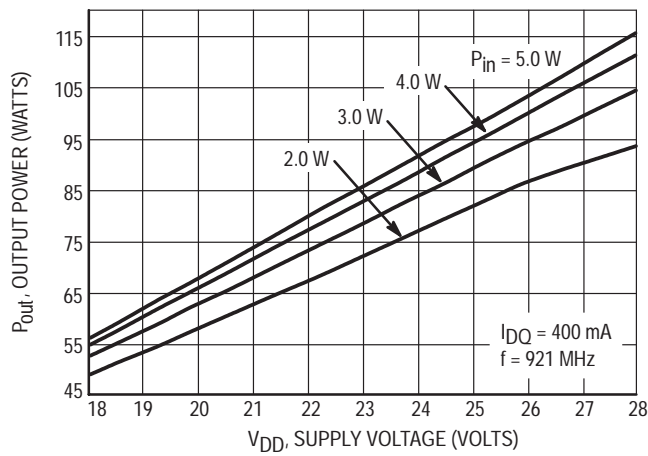


Figure 4. Output Power versus Supply Voltage

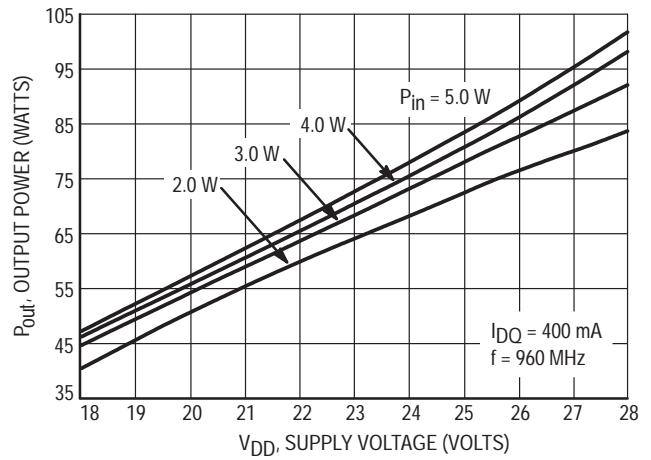


Figure 5. Output Power versus Supply Voltage

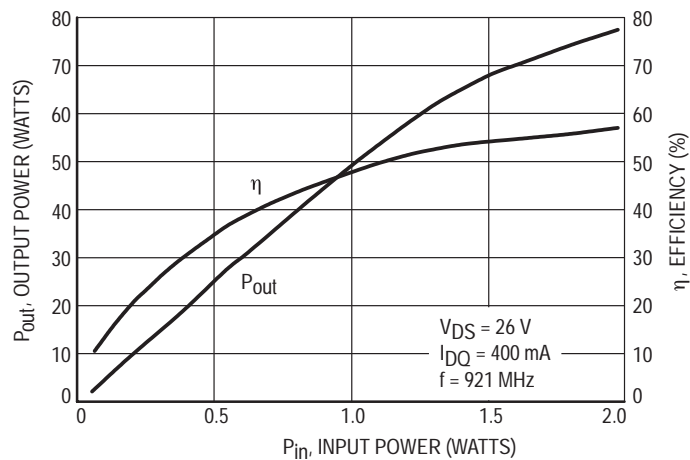


Figure 6. Efficiency and Output Power versus Input Power

TYPICAL CHARACTERISTICS

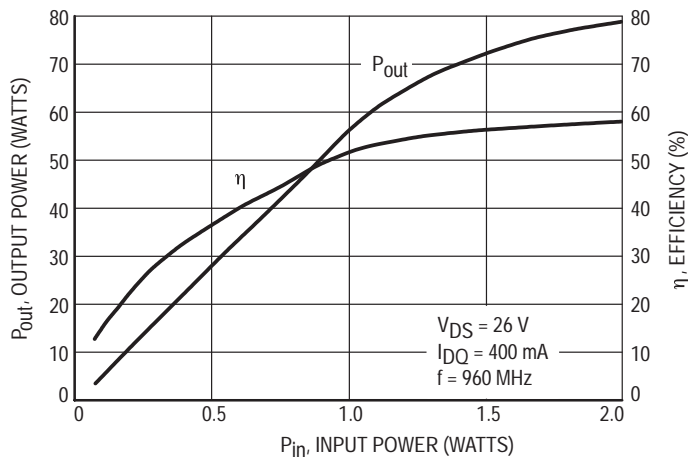


Figure 7. Efficiency and Output Power versus Input Power

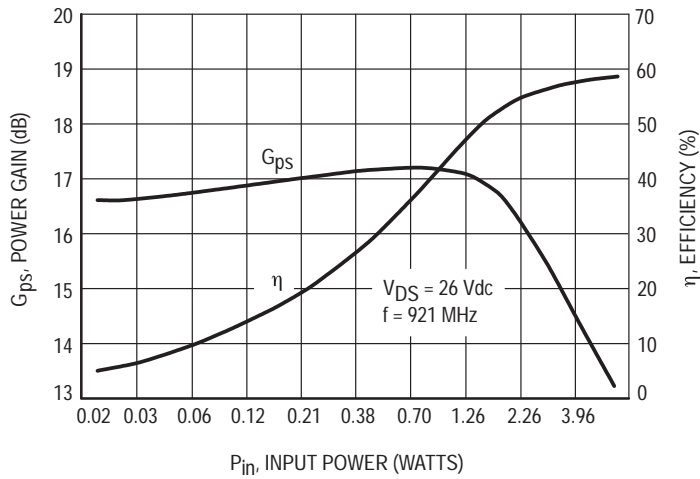


Figure 8. Power Gain and Efficiency versus Input Power

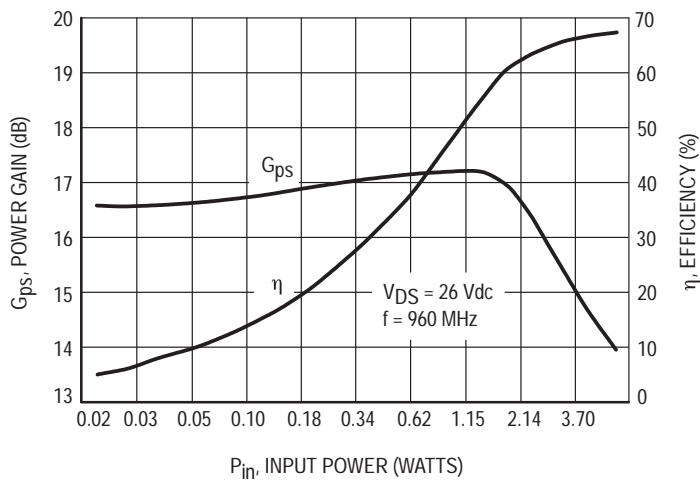


Figure 9. Power Gain and Efficiency versus Input Power

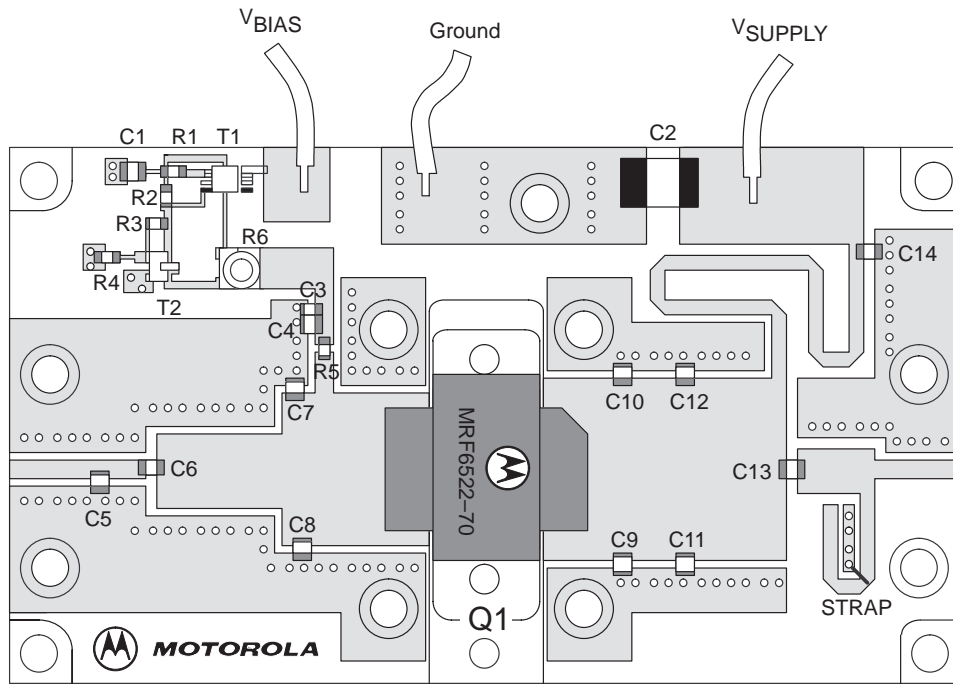


Figure 10. Component Parts Layout

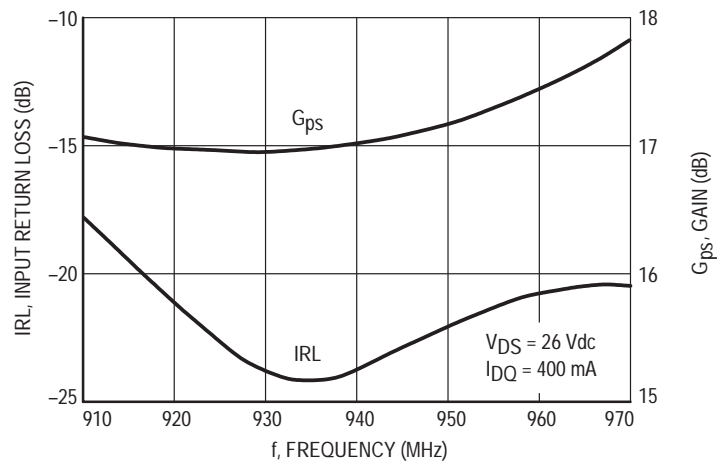
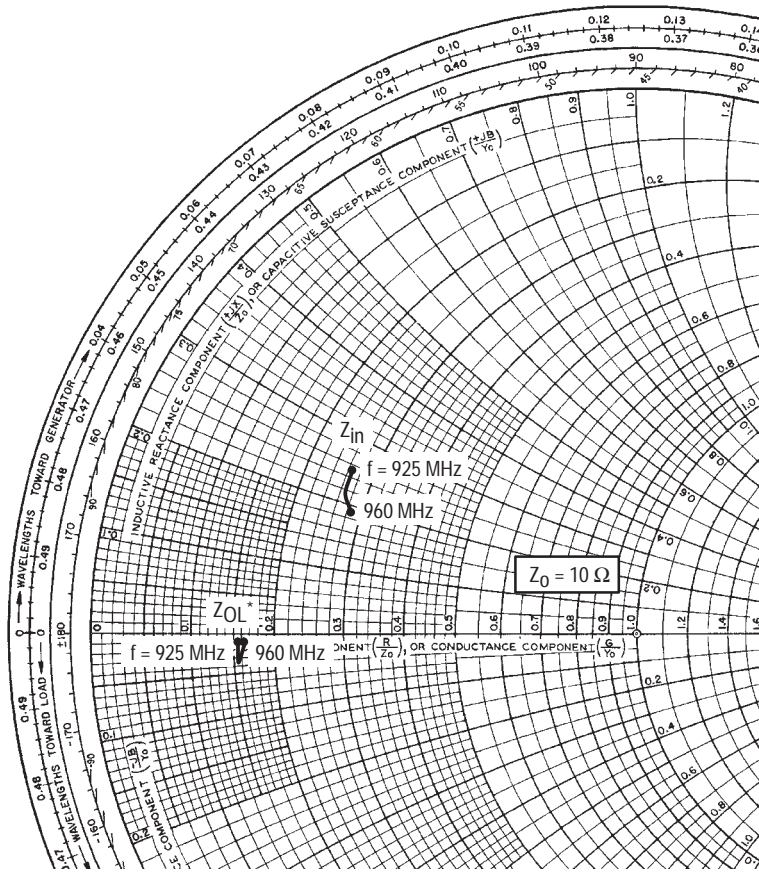


Figure 11. Performance in Broadband Circuit (at Small Signal)



VSUPPLY = 26 Vdc, IBIAS = 400 mA, CW = Room Temperature

f MHz	Z _{in} Ω	Z _{OL} [*] Ω
925	2.65 + j2.53	1.62 - j0.2
940	2.67 + j2.14	1.56 - j0.34
960	2.85 + j1.87	1.55 - j0.2

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^{*} = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^{*} was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

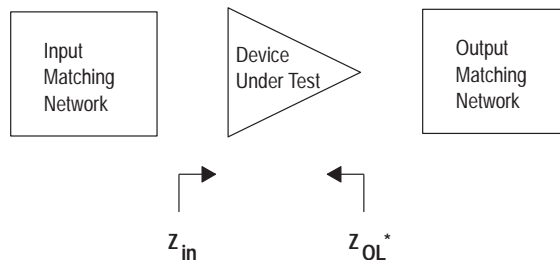


Figure 12. Series Equivalent Input and Output Impedance

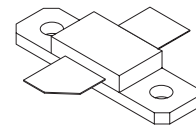
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for broadband commercial and industrial applications at frequencies up to 1.0 GHz. The high gain and broadband performance of these devices makes them ideal for large-signal, common-source amplifier applications in 28 volt base station equipment.

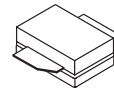
- Typical Two-Tone Performance at 945 MHz, 28 Volts
Output Power – 45 Watts PEP
Power Gain – 18.8 dB
Efficiency – 42%
IMD – -32 dBc
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 28 Vdc, 945 MHz, 45 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- MRF9045S Is Available in Tape and Reel. R1 Suffix = 500 Units per 24 mm, 13 inch Reel.

MRF9045
MRF9045S
MRF9045SR1

945 MHz, 45 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETS



CASE 360B-03, STYLE 1
(MRF9045)



CASE 360C-03, STYLE 1
(MRF9045S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	125 0.71	Watts $W/^\circ\text{C}$
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	175 1	Watts $W/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M1 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.4 1.0	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

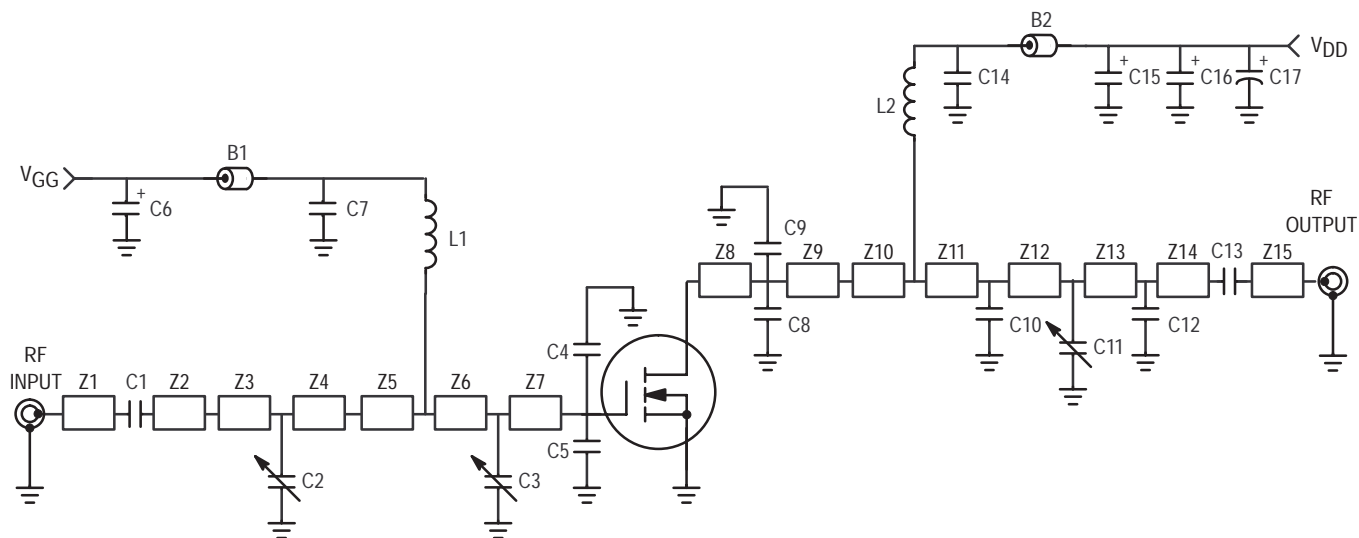
ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 65\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 150\ \mu\text{Adc}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ Vdc}$, $I_D = 350\ \text{mAdc}$)	$V_{GS(Q)}$	—	3.7	—	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\ \text{Adc}$)	$V_{DS(on)}$	—	0.19	0.4	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 3\ \text{Adc}$)	g_{fs}	—	4	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{iss}	—	69	—	pF
Output Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{oss}	—	37	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{rss}	—	1.5	—	pF

(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	G_{ps}	17	18.8	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	η	38	42	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	IMD	—	-32	-28	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	IRL	9	14	—	dB
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	G_{ps}	—	18.5	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	η	—	41	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	IMD	—	-33	—	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	IRL	—	13	—	dB
Power Output, 1 dB Compression Point ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W CW}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$)	P_{1dB}	—	55	—	W
Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W CW}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$)	G_{ps}	—	18	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W CW}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$)	η	—	60	—	%
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W CW}$, $I_{DQ} = 350\text{ mA}$, $f = 945.0\text{ MHz}$, $VSWR = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power			



B1	Short Ferrite Bead Surface Mount	Z4	T-Line, 0.360" x 0.320"
B2	Long Ferrite Bead Surface Mount	Z5	Taper, 0.240" x 0.320" x 0.620"
C1, C7, C13, C14	47 pF, Chip Capacitors, B Case	Z6	T-Line, 0.140" x 0.620"
C2, C3, C11	0.8–8.0 pF, Gigatrim Variable Trim Capacitors	Z7	T-Line, 0.510" x 0.620"
C4, C5, C8, C9	10 pF, Chip Capacitors, B Case	Z8	T-Line, 0.330" x 0.320"
C6, C15, C16	10 μ F, 35 V Tantalum Surface Mount Chip Capacitors	Z9	T-Line, 0.140" x 0.320"
C10	2.2 pF, Chip Capacitor, B Case	Z10	T-Line, 0.070" x 0.080"
C12	0.7 pF, Chip Capacitor, B Case – MRF9045S	Z11	T-Line, 0.240" x 0.080"
	1.3 pF, Chip Capacitor, B Case – MRF9045	Z12	T-Line, 0.140" x 0.080"
C17	220 μ F, 50 V Electrolytic Capacitor	Z13	T-Line, 0.930" x 0.080"
L1, L2	12.5 nH, Surface Mount Inductors, Coilcraft	Z14	T-Line, 0.180" x 0.080"
Z1	T-Line, 0.260" x 0.080"	Z15	T-Line, 0.350" x 0.080"
Z2	T-Line, 0.610" x 0.120"	Printed Circuit Board	0.03" Glass Teflon®, $\epsilon_r = 2.55$ ARLON GX-0300-55-22
Z3	T-Line, 0.260" x 0.320"		

Figure 1. 930 – 960 MHz Broadband Test Circuit Schematic

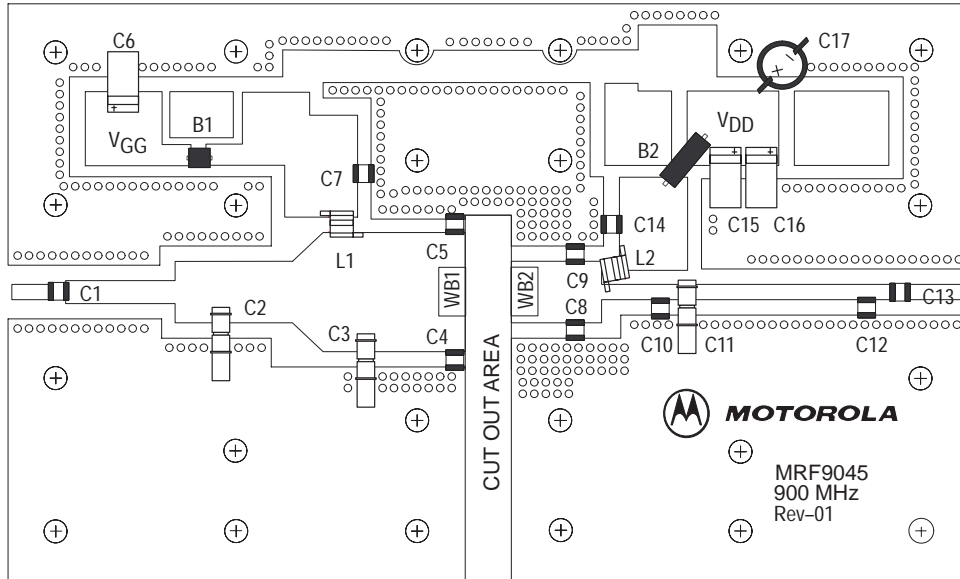


Figure 2. 930 – 960 MHz Broadband Test Circuit Component Layout

TYPICAL CHARACTERISTICS

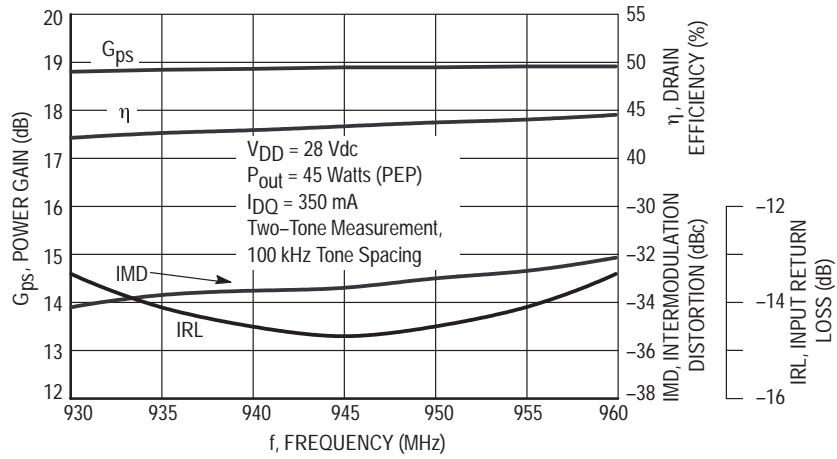


Figure 3. Class AB Broadband Circuit Performance

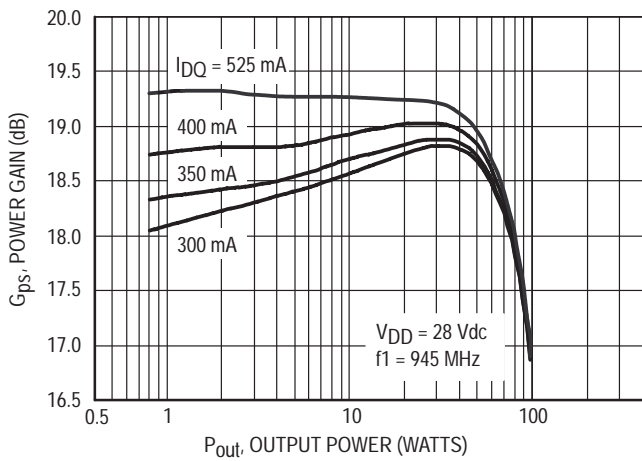


Figure 4. Power Gain versus Output Power

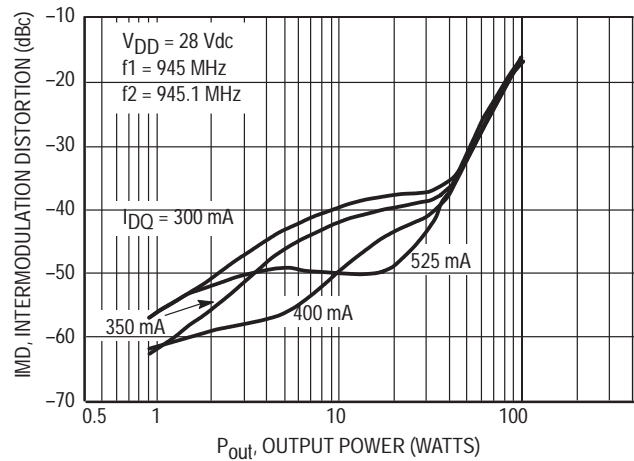


Figure 5. Intermodulation Distortion versus Output Power

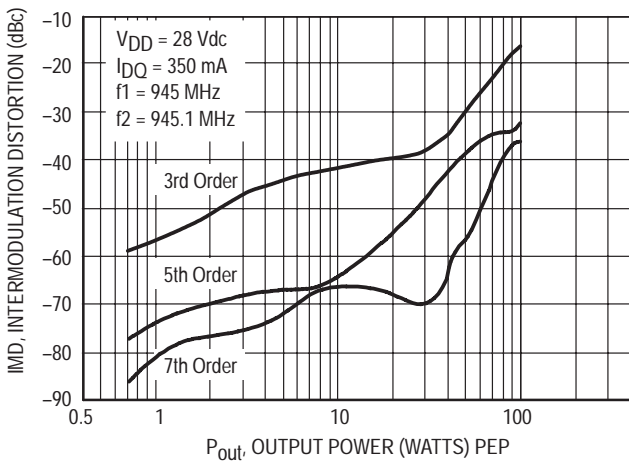


Figure 6. Intermodulation Distortion Products versus Output Power

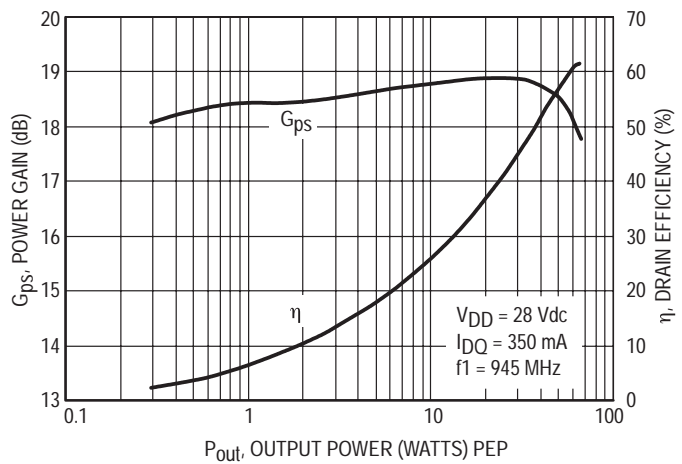
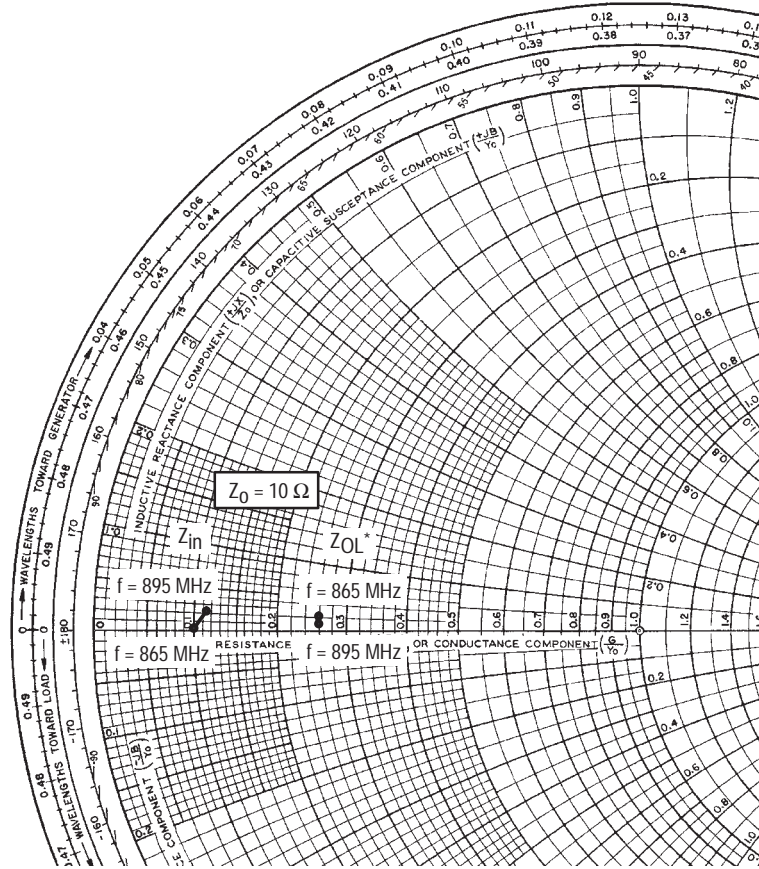


Figure 7. Power Gain, Efficiency versus Output Power



$V_{DD} = 28 \text{ V}$, $I_{DQ} = 350 \text{ mA}$, $P_{out} = 45 \text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
930	$1.02 + j0.06$	$2.6 + j0.20$
945	$1.10 + j0.11$	$2.6 + j0.16$
960	$1.15 + j0.25$	$2.6 + j0.10$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

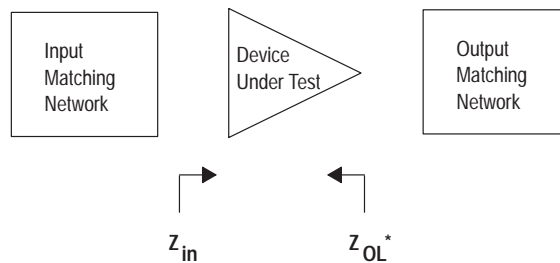


Figure 8. Series Equivalent Input and Output Impedance

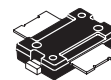
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

Designed for broadband commercial and industrial applications at frequencies up to 1.0 GHz. The high gain and broadband performance of this device make it ideal for large-signal, common-source amplifier applications in 28 volt base station equipment.

- Typical Performance at 945 MHz, 28 Volts
Output Power – 45 Watts PEP
Power Gain – 18.5 dB
Efficiency – 41% (Two Tones)
IMD – -31 dBc
- Integrated ESD Protection
- Guaranteed Ruggedness @ Load VSWR = 5:1, @ 28 Vdc, 945 MHz, 45 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- Moisture Sensitivity Level 3
- RF Power Plastic Surface Mount Package
- Available in Tape and Reel. R1 Suffix = 500 Units per 24 mm, 13 inch Reel.

MRF9045MR1

945 MHz, 45 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 1265-06, STYLE 1
(TO-270)
PLASTIC

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	156(1) 1.25(1)	Watts $W/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	150	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M2 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.8(1)	$^\circ\text{C/W}$

(1) Simulated

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

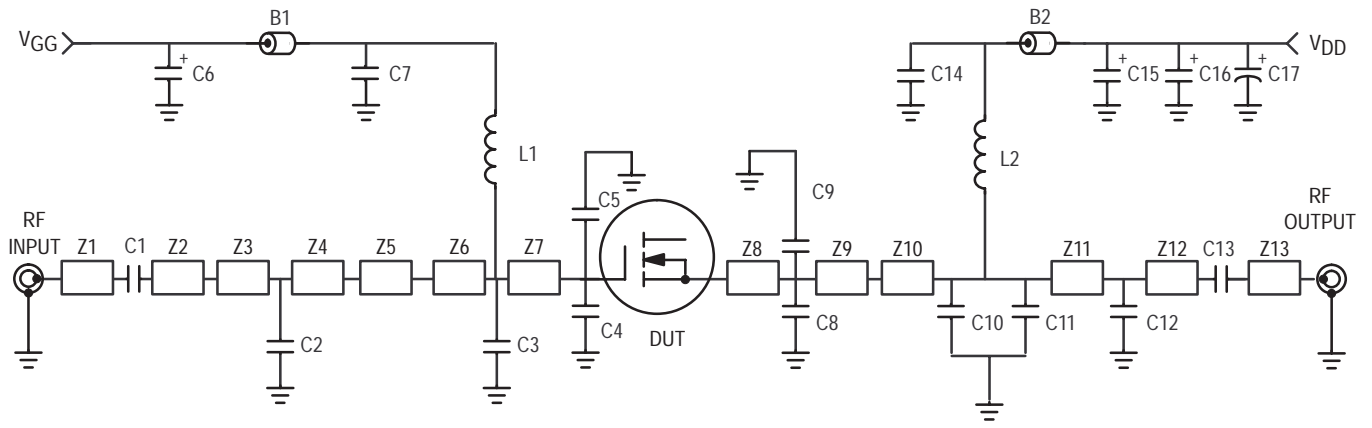
ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 65\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 150\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ Vdc}$, $I_D = 350\text{ mAdc}$)	$V_{GS(Q)}$	—	3.7	—	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.19	0.4	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$)	g_{fs}	—	4	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	74	—	pF
Output Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	39	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	1.9	—	pF

(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	G_{ps}	17	18.5	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	η	38	41	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	IMD	—	-31	-28	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 945.0\text{ MHz}$, $f_2 = 945.1\text{ MHz}$)	IRL	9	15	—	dB
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	G_{ps}	—	18.5	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	η	—	41	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	IMD	—	-31	—	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 350\text{ mA}$, $f_1 = 930.0\text{ MHz}$, $f_2 = 930.1\text{ MHz}$ and $f_1 = 960.0\text{ MHz}$, $f_2 = 960.1\text{ MHz}$)	IRL	—	13	—	dB



B1, B2	Short Ferrite Beads, Surface Mount	Z3	0.14" x 0.32"
C1, C7, C13, C14	47 pF, Chip Capacitors, B Case	Z4	0.47" x 0.32"
C2, C8	2.7 pF, Chip Capacitors, B Case	Z5	0.16" x 0.32" x 0.62" Tapered
C3	3.9 pF, Chip Capacitor, B Case	Z6	0.18" x 0.62"
C4, C5, C8, C9	10 pF, Chip Capacitors, B Case	Z7	0.56" x 0.62"
C6	10 μ F, 35 V Tantalum Surface Mount Capacitor	Z8	0.33" x 0.32"
C10	2.2 pF, Chip Capacitor, B Case	Z9	0.14" x 0.32"
C11	4.7 pF, Chip Capacitor, B Case	Z10	0.36" x 0.08"
C12	1.2 pF, Chip Capacitor, B Case	Z11	1.01" x 0.08"
C17	220 μ F, 50 V Electrolytic Capacitor	Z12	0.15" x 0.08"
L1, L2	12.5 nH, Inductors	Z13	0.29" x 0.08"
Z1	0.20" x 0.08"		
Z2	0.57" x 0.12"		

Figure 1. 945 MHz Broadband Test Circuit Schematic

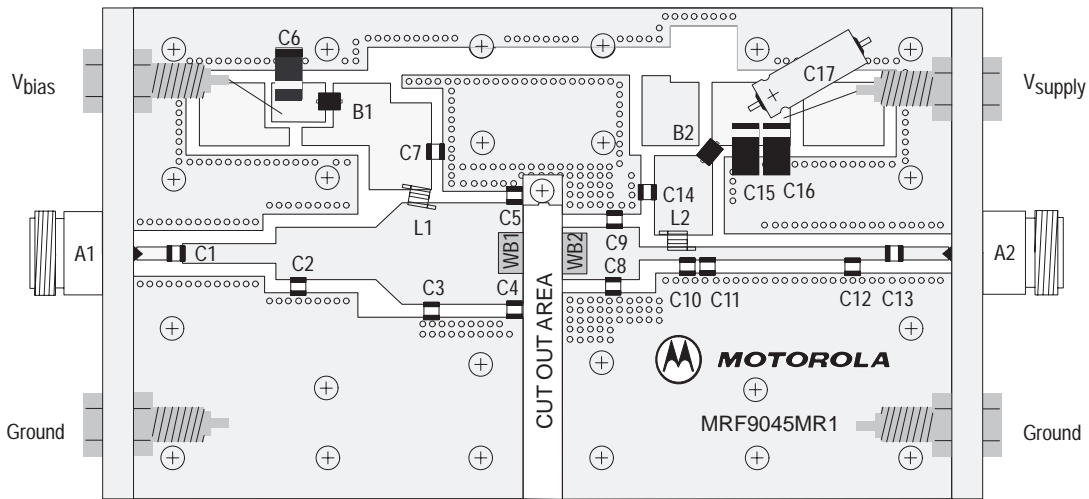


Figure 2. 945 MHz Broadband Test Circuit Components Layout

TYPICAL CHARACTERISTICS

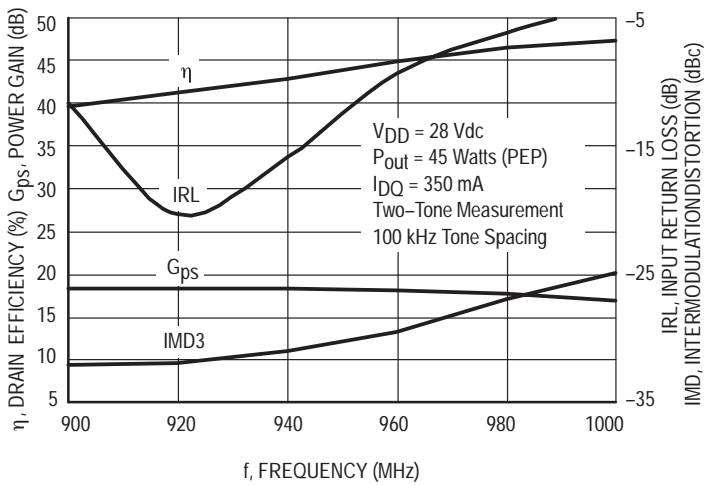


Figure 3. Class AB Test Circuit Performance

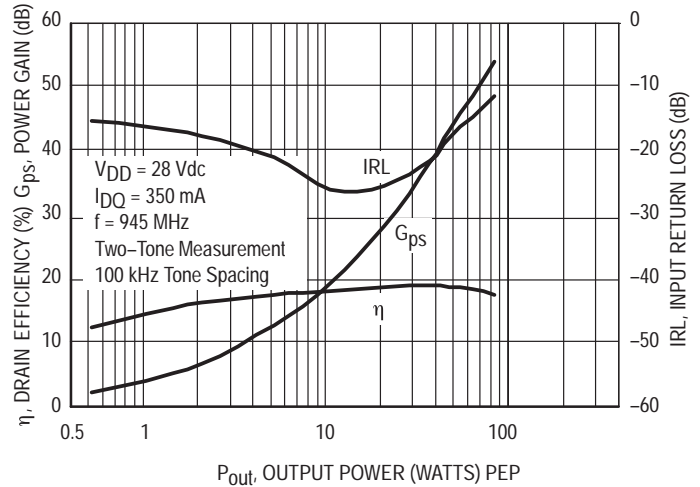


Figure 4. Power Gain, Efficiency and IRL versus Output Power

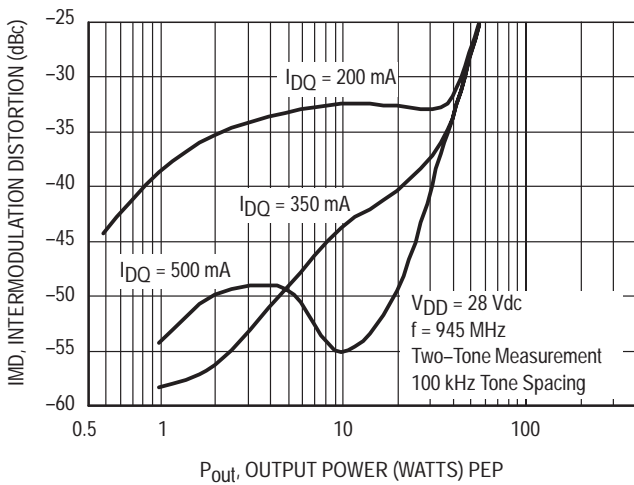


Figure 5. Intermodulation Distortion versus Output Power

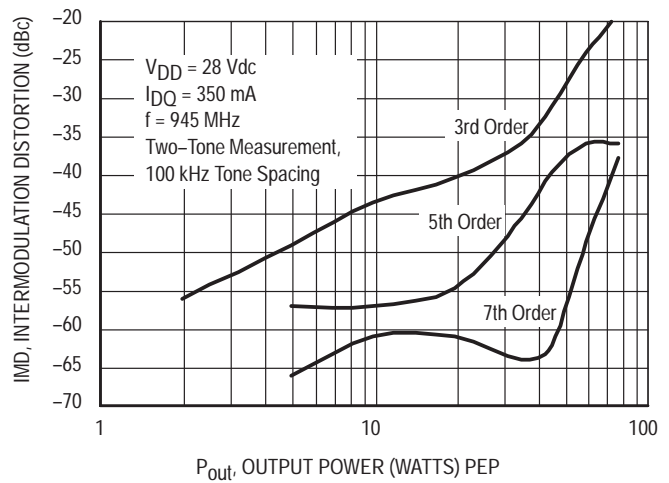


Figure 6. Intermodulation Distortion Products versus Output Power

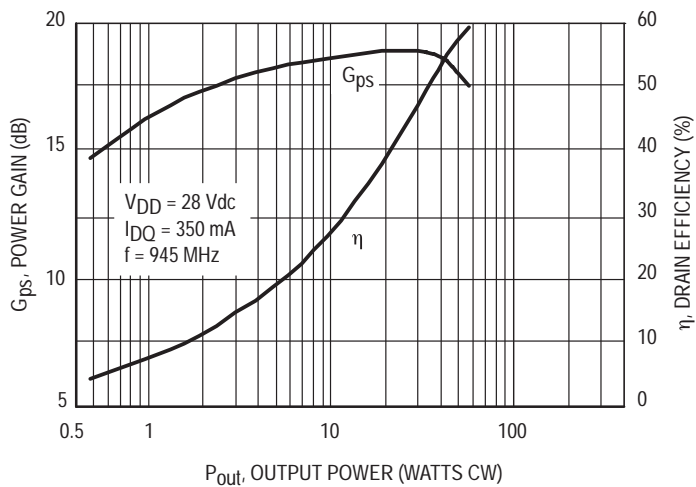


Figure 7. CW Power Gain and Drain Efficiency versus Output Power

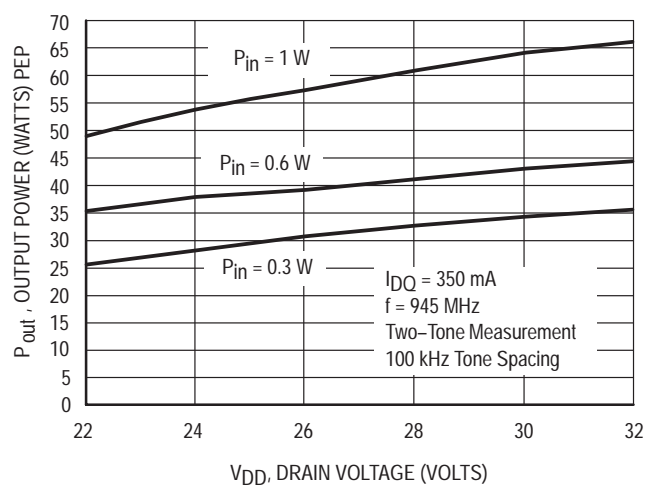
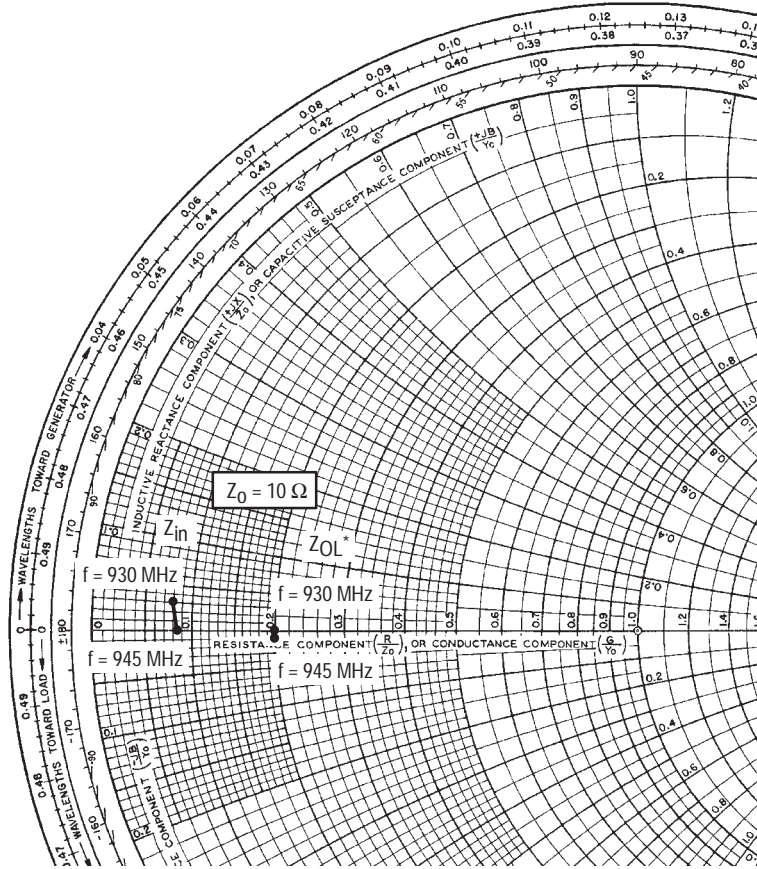


Figure 8. Output Voltage versus Supply Voltage



$V_{DD} = 28 \text{ V}$, $I_{DQ} = 350 \text{ mA}$, $P_{out} = 45 \text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
930	$0.81 + j0.25$	$2.03 - j0.09$
945	$0.85 + j0.05$	$2.03 - j0.28$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

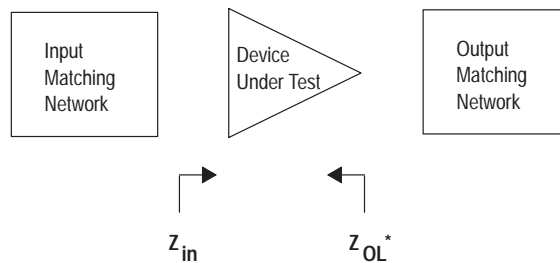


Figure 9. Series Equivalent Input and Output Impedance

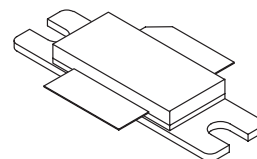
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

MRF9080
MRF9080S

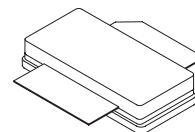
Designed for GSM 900 MHz frequency band, the high gain and broadband performance of these devices make them ideal for large-signal, common-source amplifier applications in 26 volt base station equipment.

- Typical Performance for GSM Frequencies, 921 to 960 MHz, 26 Volts
Output Power @ P1db: 75 Watts
Power Gain @ P1db: 18.5 dB
Efficiency @ P1db: 55%
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 5:1 VSWR, @ 26 Vdc, 921 MHz, 90 Watts CW Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

**GSM 900 MHz FREQUENCY BAND,
75 W, 26 V
LATERAL N-CHANNEL
BROADBAND RF POWER MOSFETs**



**CASE 465-04, STYLE 1
(MRF9080)**



**CASE 465A-04, STYLE 1
(MRF9080S)**

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	250 1.43	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M1 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.7	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 65 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μA_{dc}
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 26 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μA_{dc}
Gate–Source Leakage Current ($V_{GS} = 5 \text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μA_{dc}
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10 \text{ Vdc}$, $I_D = 300 \mu\text{A}_{dc}$)	$V_{GS(th)}$	2.0	—	4.0	Vdc
Gate Quiescent Voltage ($V_{DS} = 26 \text{ Vdc}$, $I_D = 700 \text{ mA}_{dc}$)	$V_{GS(Q)}$	—	3.7	—	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ Vdc}$, $I_D = 2 \text{ Adc}$)	$V_{DS(on)}$	—	0.19	0.4	Vdc
Forward Transconductance ($V_{DS} = 10 \text{ Vdc}$, $I_D = 6 \text{ Adc}$)	g_{fs}	—	8.0	—	S
DYNAMIC CHARACTERISTICS (1)					
Output Capacitance ($V_{DS} = 26 \text{ Vdc}$, $V_{GS} = 0$, $f = 1 \text{ MHz}$)	C_{oss}	—	73	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26 \text{ Vdc}$, $V_{GS} = 0$, $f = 1 \text{ MHz}$)	C_{rss}	—	2.9	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture) (2)					
Power Output, 1 dB Compression Point ($V_{DD} = 26 \text{ Vdc}$, $I_{DQ} = 600 \text{ mA}$, $f = 921$ and 960 MHz)	P_{1dB}	68	75	—	W
Common–Source Amplifier Power Gain @ 70 W (Min) ($V_{DD} = 26 \text{ Vdc}$, $I_{DQ} = 600 \text{ mA}$, $f = 921$ and 960 MHz)	G_{ps}	17	18.5	20	dB
Drain Efficiency @ $P_{out} = 70 \text{ W}$ ($V_{DD} = 26 \text{ Vdc}$, $I_{DQ} = 600 \text{ mA}$, $f = 921$ and 960 MHz)	η_1	47	52	—	%
Drain Efficiency @ P_{1dB} ($V_{DD} = 26 \text{ Vdc}$, $I_{DQ} = 600 \text{ mA}$, $f = 921$ and 960 MHz)	η_2	—	55	—	%
Input Return Loss ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 70 \text{ W}$, $I_{DQ} = 600 \text{ mA}$, $f = 921$ and 960 MHz)	IRL	9.5	12.5	—	dB
Output Mismatch Stress ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 90 \text{ W CW}$, $I_{DQ} = 600 \text{ mA}$, $f = 921 \text{ MHz}$, $VSWR = 5:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally input matched.

(2) To meet application requirements, Motorola test fixtures are designed to cover full GSM 900 band ensuring batch to batch consistency

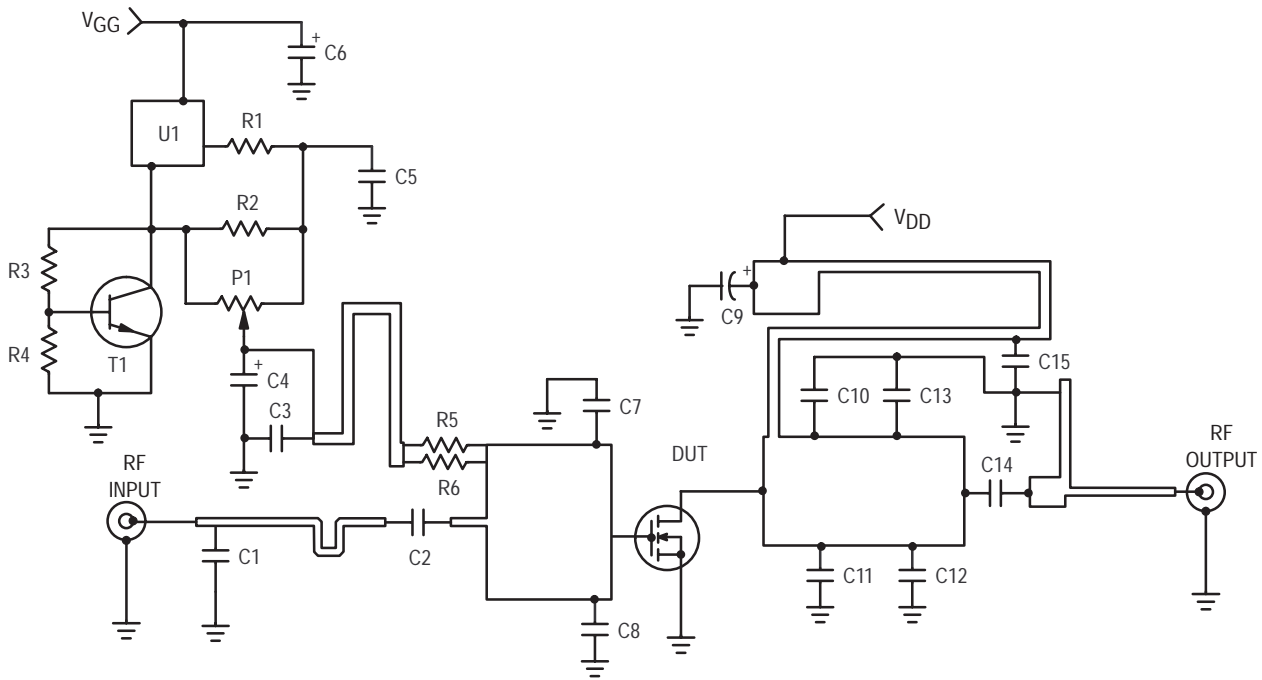


Figure 1. Broadband GSM 900 Optimized Demo Board Schematic

Table 1. Broadband GSM 900 Optimized Demo Board Component Designations and Values

Designators	Description
C1	4.7 pF Chip Capacitor, ACCU-P (0805) AVX #08051J3R9CBT
C2	3.9 pF Chip Capacitor, ACCU-P (0805) AVX #08051J3R9CBT
C3, C15	22 pF Chip Capacitors, ACCU-P (0805) AVX #08051J221
C4, C6	22 μ F, 35 V Tantalum Chip Capacitors, Kemet #T491X226K035AS4394
C5	1.0 μ F Chip Capacitor, ACCU-P (0805) AVX #08053G105ZATEA
C7, C8	5.6 pF Chip Capacitors, ACCU-P (0805) AVX #08051J5R18CBT
C9	220 μ F, 63 V Electrolytic Capacitor
C10, C11	3.3 pF Chip Capacitors, ACCU-P (0805) AVX #08051J8R2CBT
C12, C13	2.2 pF Chip Capacitors, ACCU-P (0805) AVX #08051J2R2CBT
C14	4.7 pF Chip Capacitor, ATC #100B
P1	5.0 k Ω Potentiometer CMS Cermet Multi-turn, Bourns #3224W
R1	10 Ω , 1/8 W Chip Resistor (0805)
R2	1.0 k Ω , 1/8 W Chip Resistor (0805)
R3	1.2 k Ω , 1/8 W Chip Resistor (0805)
R4	2.2 k Ω , 1/8 W Chip Resistor (0805)
R5, R6	1.0 k Ω , 1/8 W Chip Resistor (0805)
T1	Bipolar NPN Transistor, SOT-23, ON Semiconductor #BC847ALT1
U1	Voltage Regulator, Micro-8, ON Semiconductor #LP2951ACDM-5.0R2
	RF Connectors, Type SMA, Radial #R125510001
	Substrate = Taconic RF35, Thickness 0.5mm

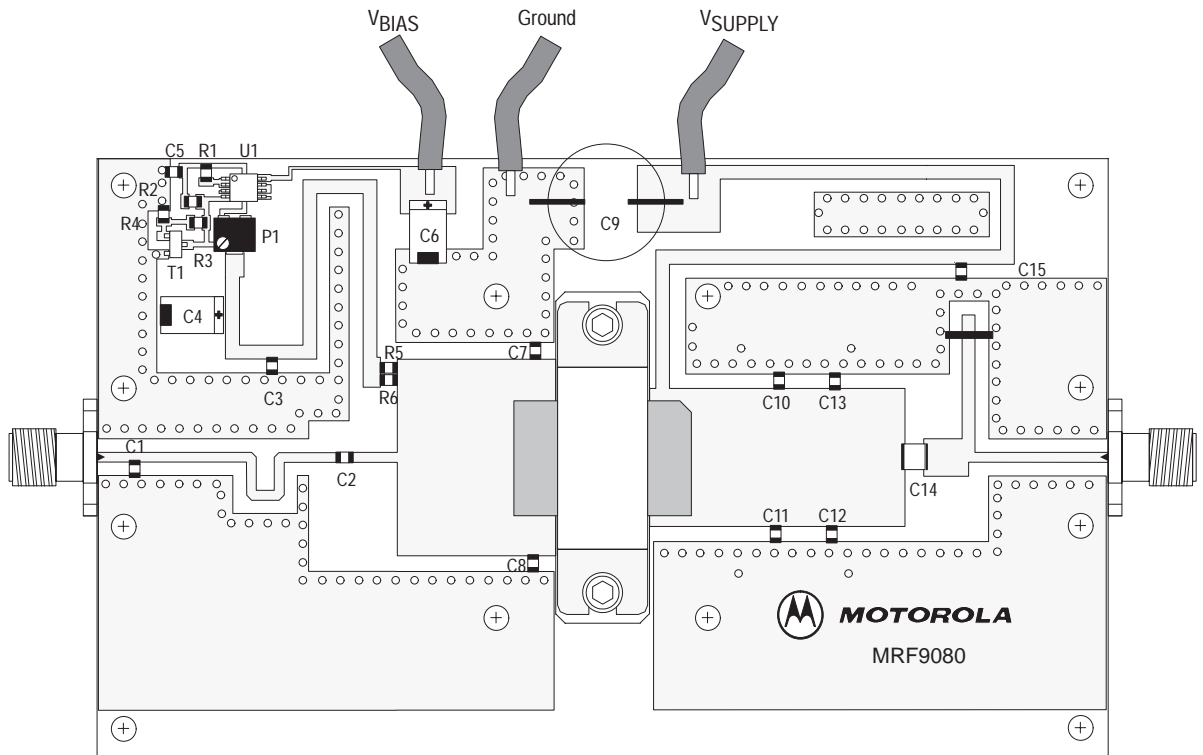


Figure 2. Broadband GSM 900 Optimized Demo Board Component Layout

**TYPICAL CHARACTERISTICS
(IN MOTOROLA BROADBAND GSM 900 OPTIMIZED DEMO BOARD)**

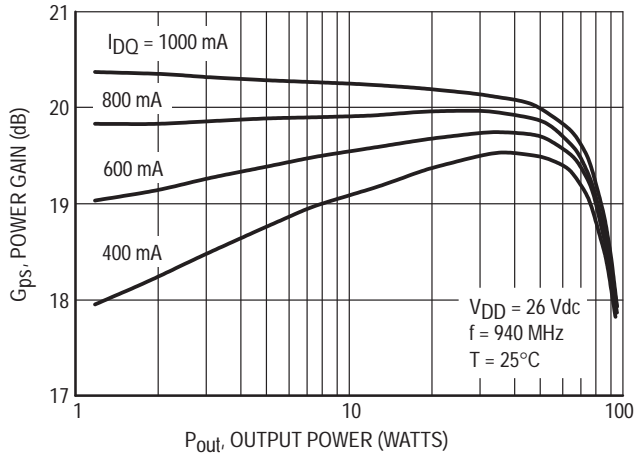


Figure 3. Power Gain versus Output Power

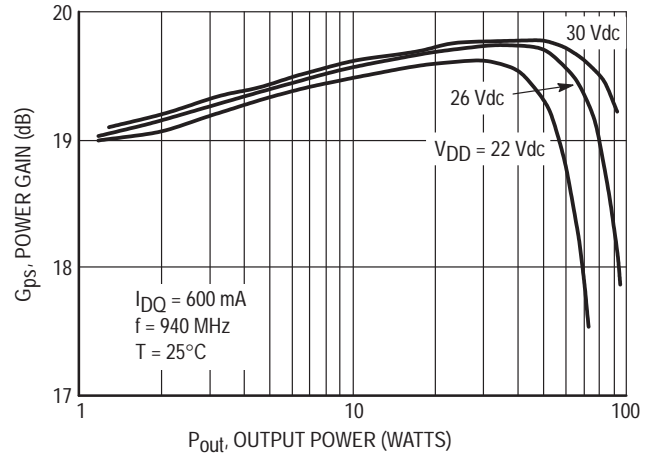


Figure 4. Power Gain versus Output Power

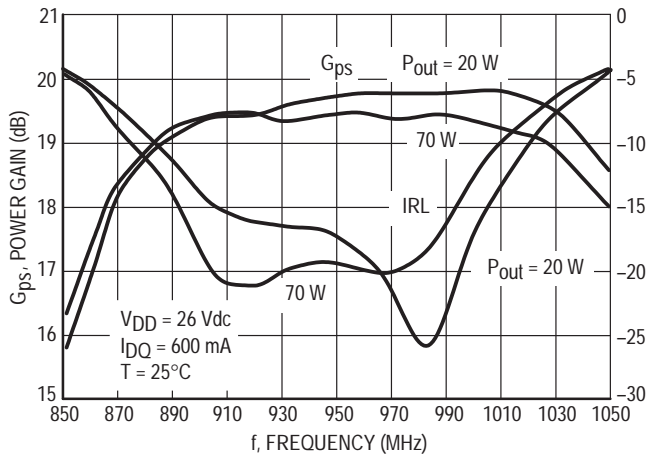


Figure 5. Power Gain and Input Return Loss versus Frequency

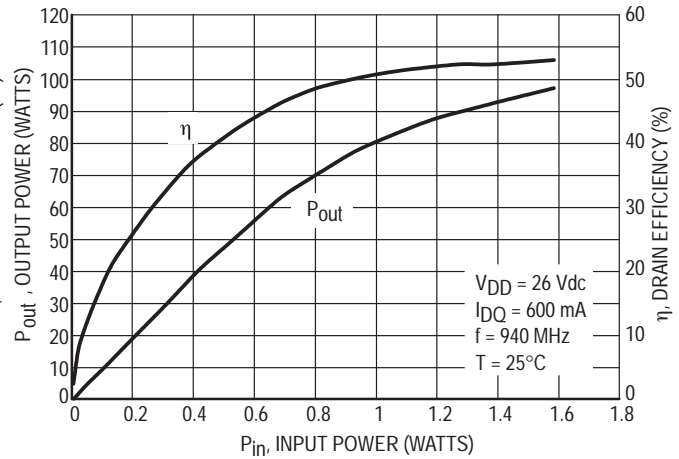


Figure 6. Output Power and Efficiency versus Input Power

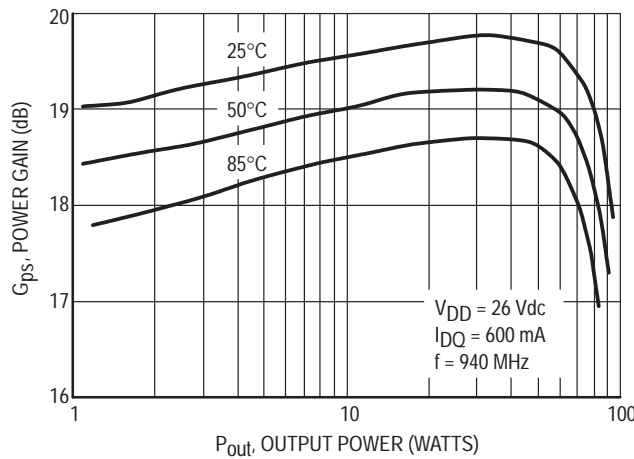


Figure 7. Power Gain versus Output Power

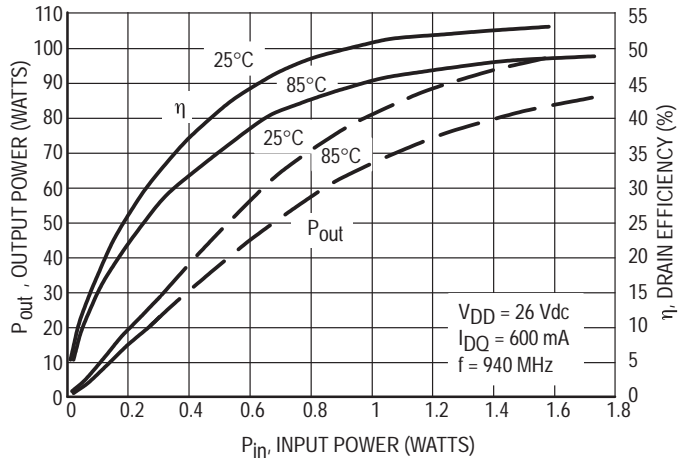
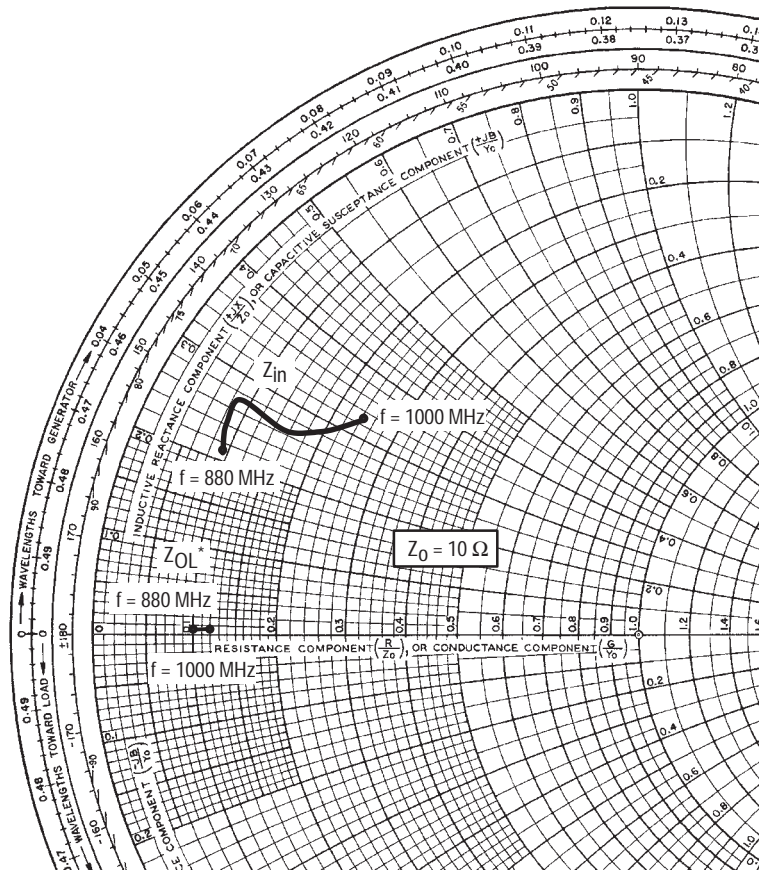


Figure 8. Output Power and Efficiency versus Input Power



$V_{DD} = 26\text{ V}$, $I_{DQ} = 600\text{ mA}$, $P_{out} = 90\text{ W (CW)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
880	$0.91 + j2.11$	$1.22 + j0.12$
920	$0.88 + j2.65$	$1.00 + j0.16$
960	$1.6 + j2.61$	$1.22 + j0.22$
1000	$2.45 + j3.38$	$1.14 + j0.41$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power and drain efficiency.

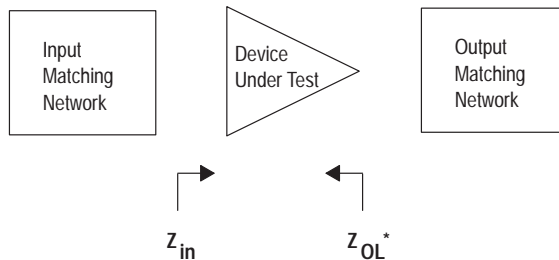


Figure 9. Series Equivalent Input and Output Impedance

The RF Sub-Micron MOSFET Line

RF Power Field Effect Transistors

N-Channel Enhancement-Mode Lateral MOSFETs

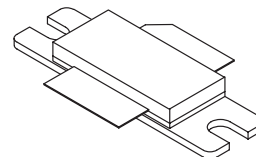
Designed for broadband commercial and industrial applications at frequencies in the 865 to 895 MHz band. The high gain and broadband performance of these devices makes them ideal for large-signal, common-source amplifier applications in 26 volt base station equipment.

- Typical CDMA Performance @ 880 MHz, 26 Volts, $I_{DQ} = 700$ mA
IS-97 CDMA Pilot, Sync, Paging, Traffic Codes 8 Through 13
Output Power = 20 Watts
Power Gain = 17.9 dB
Efficiency = 28%
Adjacent Channel Power –
750 kHz: -45.0 dBc @ 30 kHz BW
1.98 MHz: -60.0 dBc @ 30 kHz BW
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 880 MHz, 90 Watts CW Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

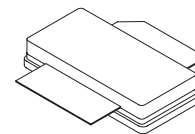
MRF9085

MRF9085S

880 MHz, 90 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465-04, STYLE 1
(MRF9085)



CASE 465A-04, STYLE 1
(MRF9085S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	250 1.43	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M2 (Typical) M1 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.7	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

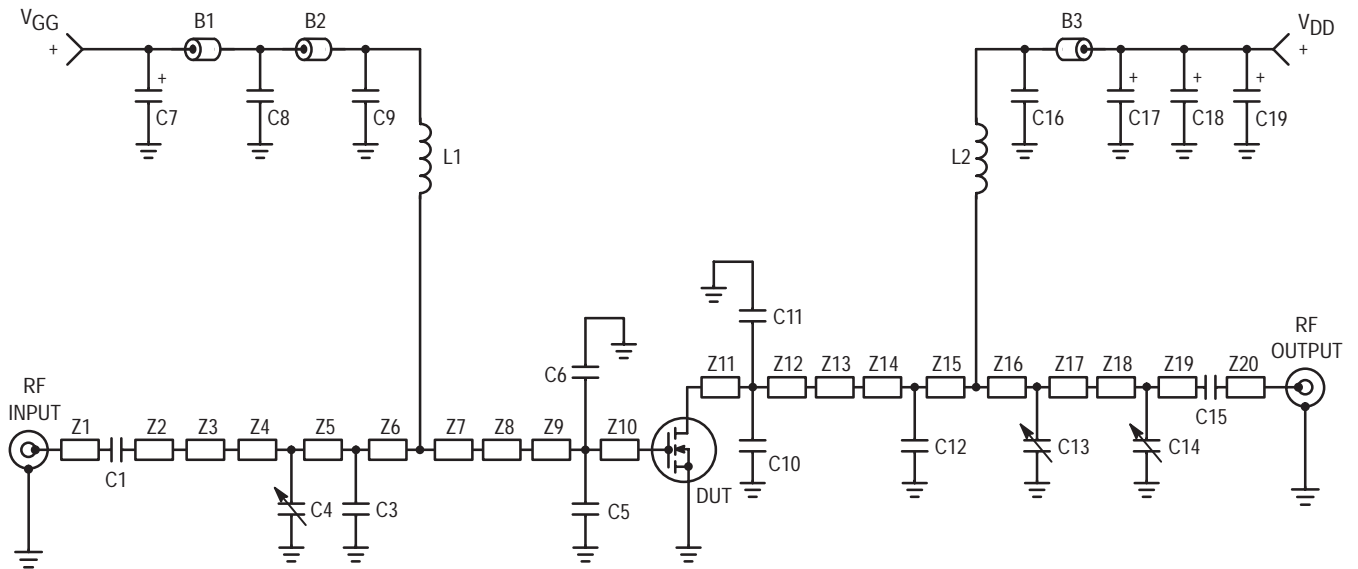
Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 65\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2.0	—	4.0	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 700\text{ mAdc}$)	$V_{GS(Q)}$	—	3.7	—	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	$V_{DS(on)}$	—	0.19	0.4	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 6\text{ Adc}$)	g_{fs}	—	8.0	—	S
DYNAMIC CHARACTERISTICS (1)					
Output Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	73	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	2.9	—	pF

(1) Part is internally input matched.

(continued)

ELECTRICAL CHARACTERISTICS – continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	G_{ps}	17	17.9	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	η	36	40	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	IMD	—	-31	-28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$, $f_2 = 880.1\text{ MHz}$)	IRL	9	21	—	dB
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$)	G_{ps}	—	17.9	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$)	η	—	40.0	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$)	IMD	—	-31	—	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 865.0\text{ MHz}$, $f_2 = 865.1\text{ MHz}$)	IRL	—	16	—	dB
Power Output, 1 dB Compression Point ($V_{DD} = 26\text{ Vdc}$, CW, $I_{DQ} = 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$)	P_{1dB}	—	105	—	W
Common-Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$)	G_{ps}	—	17.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$)	η	—	51	—	%
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 700\text{ mA}$, $f = 880.0\text{ MHz}$, VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power			



B1, B2, B3	Short Ferrite Bead, Surface Mount	Z6	0.076" x 0.220" Microstrip
C1, C9, C15, C16	47 pF, B Case Chip Capacitor, ATC	Z7	0.261" x 0.220" Microstrip
C3	5.6 pF, B Case Chip Capacitor, ATC	Z8	0.220" x 0.630" x 0.200" Taper
C4, C13	0.8 – 8.0 Gigatrim Variable Capacitor	Z9	0.240" x 0.630" Microstrip
C5, C6, C12	10 pF, B Case Chip Capacitor, ATC	Z10	0.060" x 0.630" Microstrip
C7, C17, C18, C19	10 μF, 35 V, Tantalum Surface Mount Capacitor, Kemet	Z11	0.067" x 0.630" Microstrip
C8	20 K pF, B Case Chip Capacitor, ATC	Z12	0.233" x 0.630" Microstrip
C10, C11	16 pF, B Case Chip Capacitor, ATC	Z13	0.630" x 0.220" x 0.200" Taper
C14	0.6 – 4.5 Gigatrim Variable Capacitor	Z14	0.200" x 0.220" Microstrip
L1	7.15 nH, Coilcraft Inductor	Z15	0.055" x 0.220" Microstrip
L2	18.5 nH, Coilcraft Inductor	Z16	0.088" x 0.220" Microstrip
N1, N2	N-Type Panel Mount, Stripline, M/A-Com	Z17	0.226" x 0.220" Microstrip
WB1, WB2	5 Mil BeCu Shim (0.225 x 0.525)	Z18	0.868" x 0.080" Microstrip
Z1	0.219" x 0.080" Microstrip	Z19	0.129" x 0.080" Microstrip
Z2	0.150" x 0.080" Microstrip	Z20	0.223" x 0.080" Microstrip
Z3	0.851" x 0.080" Microstrip	PCB	Etched Circuit Board, Glass, Teflon®
Z4	0.125" x 0.220" Microstrip		$\epsilon_r = 2.55, 30 \text{ Mils}$
Z5	0.123" x 0.220" Microstrip		

Figure 1. 865–895 MHz Broadband Test Circuit Schematic

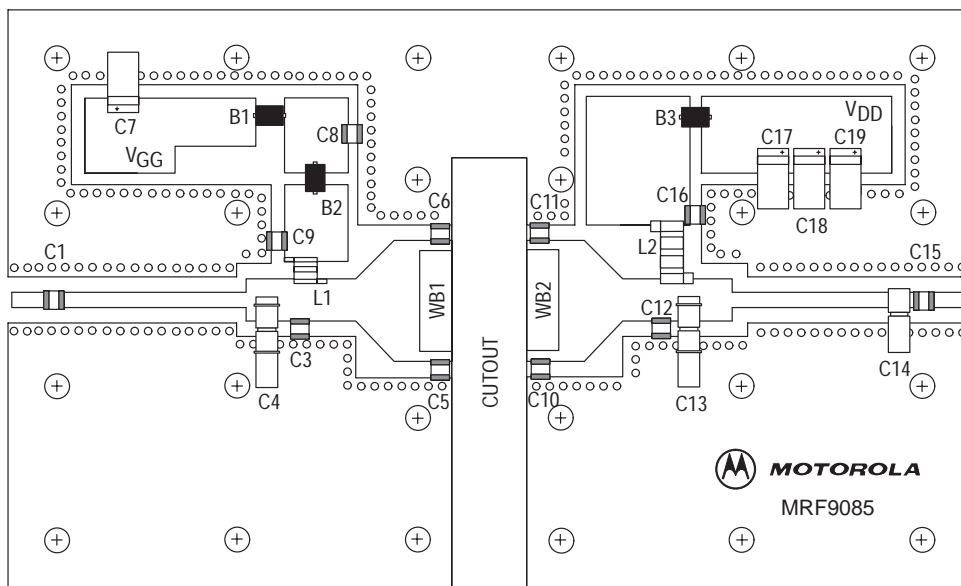


Figure 2. 865–895 MHz Broadband Test Circuit Layout

TYPICAL CHARACTERISTICS

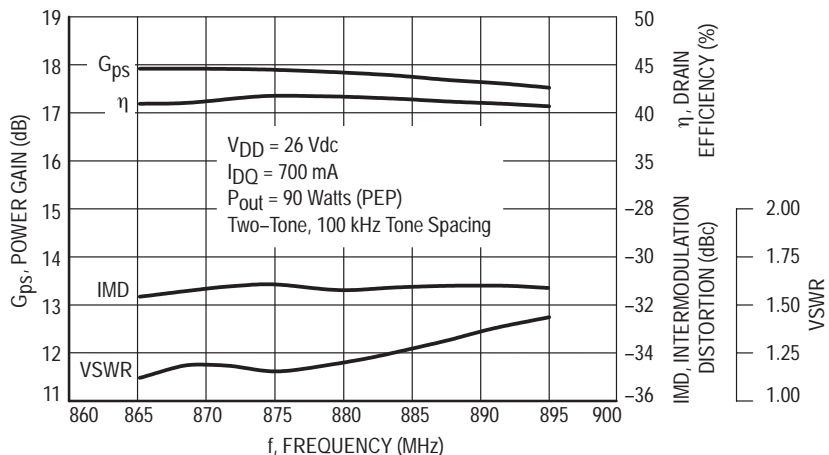


Figure 3. Class AB Broadband Circuit Performance

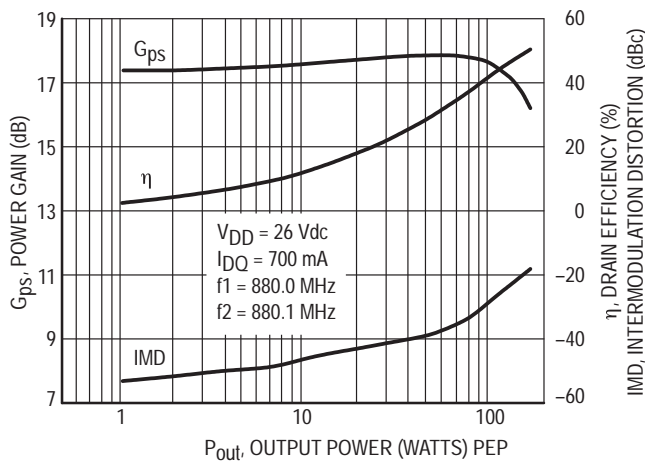


Figure 4. Power Gain, Efficiency, IMD versus Output Power

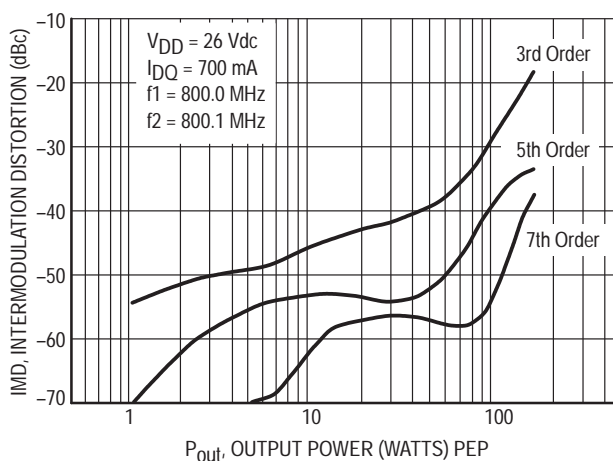


Figure 5. Intermodulation Distortion Products versus Output Power

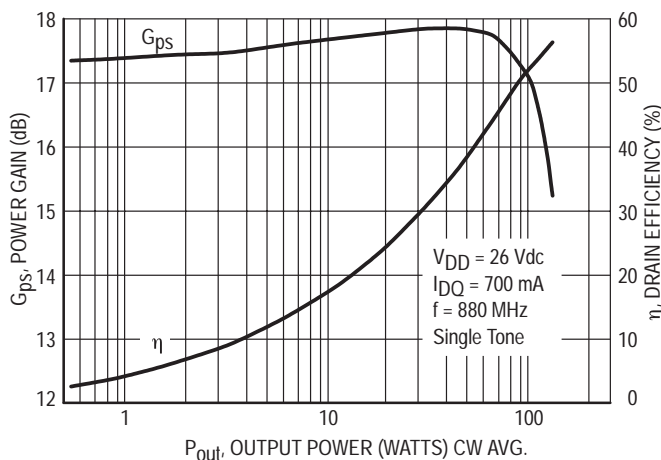


Figure 6. Power Gain, Efficiency versus Output Power

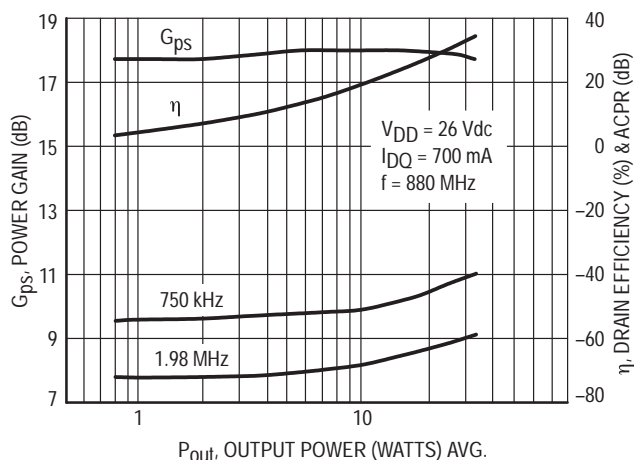
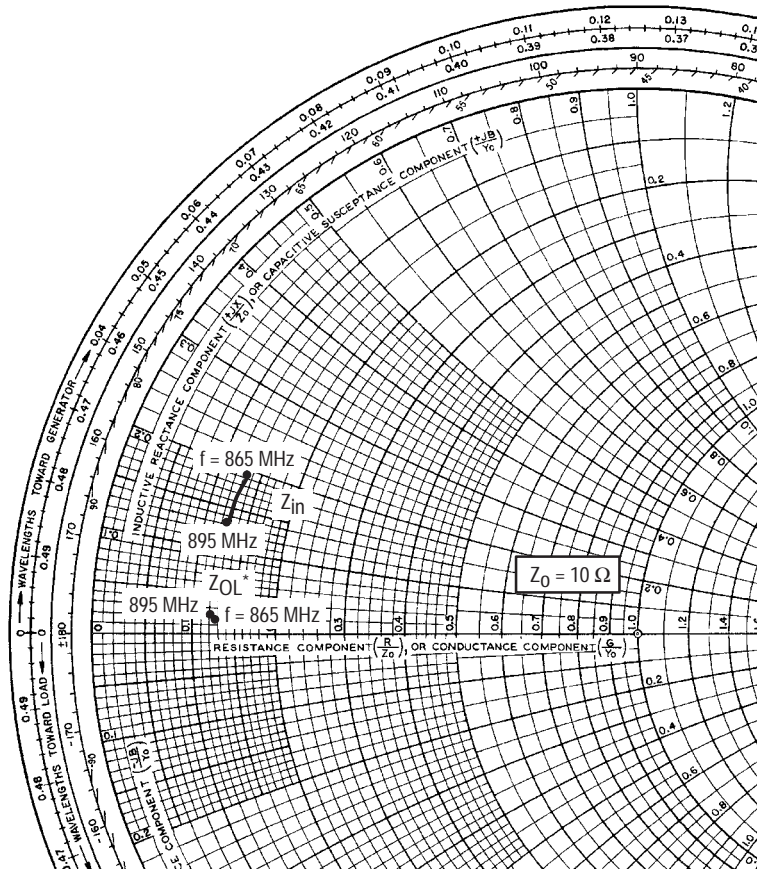


Figure 7. Power Gain, Efficiency, ACPR versus Output Power



$V_{DD} = 26\text{ V}$, $I_{DQ} = 700\text{ mA}$, $P_{out} = 90\text{ W PEP}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
865	$1.35 + j1.92$	$1.26 + j0.15$
880	$1.33 + j1.66$	$1.26 + j0.10$
895	$1.28 + j1.30$	$1.21 + j0.20$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

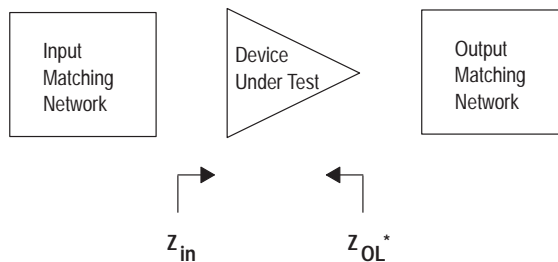


Figure 8. Series Equivalent Input and Output Impedance

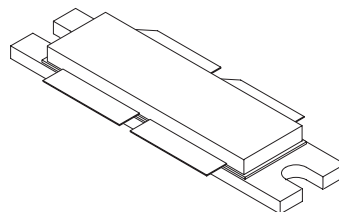
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

MRF9180
MRF9180S

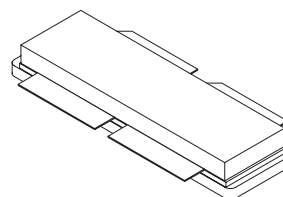
880 MHz, 170 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs

Designed for broadband commercial and industrial applications at frequencies in the 865 – 895 MHz band. The high gain and broadband performance of these devices makes them ideal for large-signal, common-source amplifier applications in 26 volt base station equipment.

- Typical CDMA Performance @ 880 MHz, 26 Volts, $I_{DQ} = 2 \times 700$ mA
IS-97 CDMA Pilot, Sync, Paging, Traffic Codes 8 Through 13
Output Power — 40 Watts
Power Gain — 17 dB
Efficiency — 26%
Adjacent Channel Power –
750 kHz: –45.0 dBc @ 30 kHz BW
1.98 MHz: –60.0 dBc @ 30 kHz BW
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 880 MHz, 170 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters



CASE 375D-01, STYLE 2
(MRF9180)



CASE 375E-01, STYLE 2
(MRF9180S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, –0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	388 2.22	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M1 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.45	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)					
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 65\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS (1)					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2	2.9	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 700\ \text{mAdc}$)	$V_{GS(Q)}$	—	3.7	—	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\ \text{Adc}$)	$V_{DS(on)}$	—	0.19	0.5	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 6\ \text{Adc}$)	g_{fs}	—	6	—	S
DYNAMIC CHARACTERISTICS (1)					
Output Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{oss}	—	77	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{rss}	—	3.8	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture) (2)					
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 880.0\ \text{MHz}$, $f_2 = 880.1\ \text{MHz}$)	G_{ps}	16	17.5	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 880.0\ \text{MHz}$, $f_2 = 880.1\ \text{MHz}$)	η	35	39	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 880.0\ \text{MHz}$, $f_2 = 880.1\ \text{MHz}$)	IMD	—	–31	–28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 880.0\ \text{MHz}$, $f_2 = 880.1\ \text{MHz}$)	IRL	9	15	—	dB
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 865.0\ \text{MHz}$, $f_2 = 865.1\ \text{MHz}$)	G_{ps}	—	17.5	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 865.0\ \text{MHz}$, $f_2 = 865.1\ \text{MHz}$)	η	—	38.5	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 865.0\ \text{MHz}$, $f_2 = 865.1\ \text{MHz}$)	IMD	—	–31	—	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\ \text{W PEP}$, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 865.0\ \text{MHz}$, $f_2 = 865.1\ \text{MHz}$)	IRL	—	13	—	dB
Power Output, 1 dB Compression Point ($V_{DD} = 26\text{ Vdc}$, CW, $I_{DQ} = 2 \times 700\ \text{mA}$, $f_1 = 880.0\ \text{MHz}$)	P_{1dB}	—	170	—	W

(1) Each side of device measured separately.

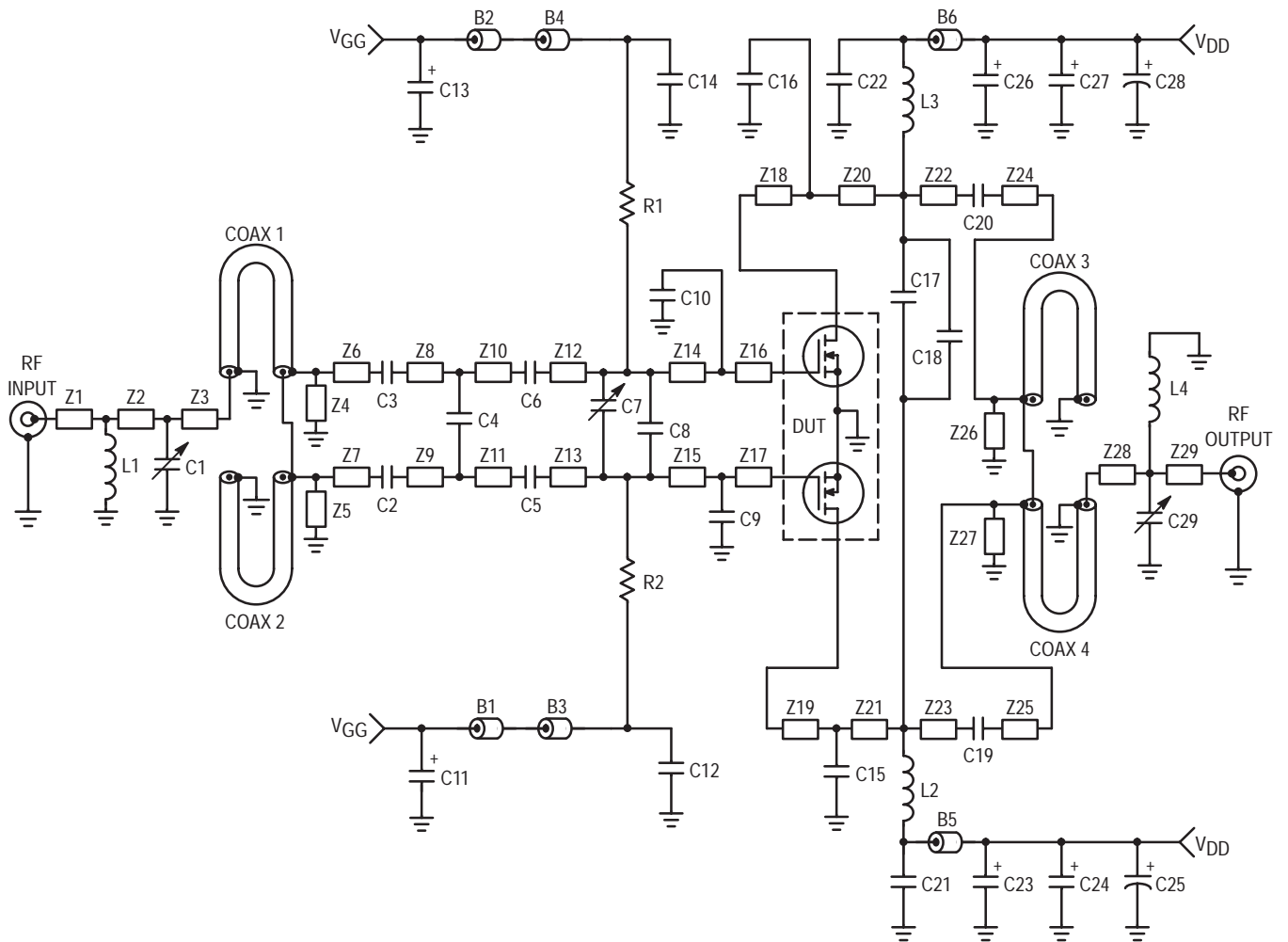
(2) Device measured in push–pull configuration.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted) (continued)**FUNCTIONAL TESTS** (In Motorola Test Fixture) (2) (continued)

Characteristic	Symbol	Min	Typ	Max	Unit
Common-Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\text{ W CW}$, $I_{DQ} = 2 \times 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$)	G_{ps}	—	16.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\text{ W CW}$, $I_{DQ} = 2 \times 700\text{ mA}$, $f_1 = 880.0\text{ MHz}$)	η	—	55	—	%
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 170\text{ W CW}$, $I_{DQ} = 2 \times 700\text{ mA}$, $f = 880\text{ MHz}$, $VSWR = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Each side of device measured separately.

(2) Device measured in push-pull configuration.



B1, B2, B5, B6	Long Ferrite Beads, Surface Mount	Z1	T-Line, 0.420" x 0.080"
B3, B4	Short Ferrite Beads, Surface Mount	Z2	T-Line, 0.190" x 0.080"
C1	0.6–4.5 pF, Variable Capacitor	Z3	T-Line, 0.097" x 0.080"
C2, C3, C5, C6, C12, C14, C19, C20, C21, C22	47 pF, Chip Capacitors, B Case	Z4, Z5, Z26, Z27	T-Line, 2.170" x 0.080"
C4, C9, C10, C15, C16	12 pF, Chip Capacitors, B Case	Z6, Z7	T-Line, 0.075" x 0.080"
C7	0.8–9.1 pF, Variable Capacitor	Z8, Z9	T-Line, 0.088" x 0.220"
C8	7.5 pF, Chip Capacitor, B Case	Z10, Z11	T-Line, 0.088" x 0.220"
C11, C13	10 μF, 35 V Tantalum Surface Mount Chip Capacitors	Z12, Z13	T-Line, 0.460" x 0.220"
C17	3.6 pF, Chip Capacitor, B Case	Z14, Z15	T-Line, 0.685" x 0.625"
C18	5.1 pF, Chip Capacitor, B Case	Z16, Z17	T-Line, 0.055" x 0.625"
C23, C24, C26, C27	22 μF, 35 V Tantalum Surface Mount Chip Capacitors	Z18, Z19	T-Line, 0.055" x 0.632"
C25, C28	220 μF, 50 V Electrolytic Capacitors	Z20, Z21	T-Line, 0.685" x 0.632"
C29	0.4–2.5 pF, Variable Capacitor	Z22, Z23	T-Line, 0.732" x 0.080"
Coax1, Coax2	25 Ω, Semi Rigid Coax, 70 mil OD, 1.05" Long	Z24, Z25	T-Line, 0.060" x 0.080"
Coax3, Coax4	50 Ω, Semi Rigid Coax, 85 mil OD, 1.05" Long	Z28	T-Line, 0.230" x 0.080"
L1, L2, L3	18.5 nH, Mini Spring Inductors, Coilcraft	Z29	T-Line, 0.460" x 0.080"
L4	12.5 nH, Mini Spring Inductor, Coilcraft	Board	30 mil Teflon®, εr = 2.55, Copper Clad, 2 oz Cu
R1, R2	510 Ω, 1/10 W Chip Resistors		

Figure 1. 880 MHz Broadband Test Circuit Schematic

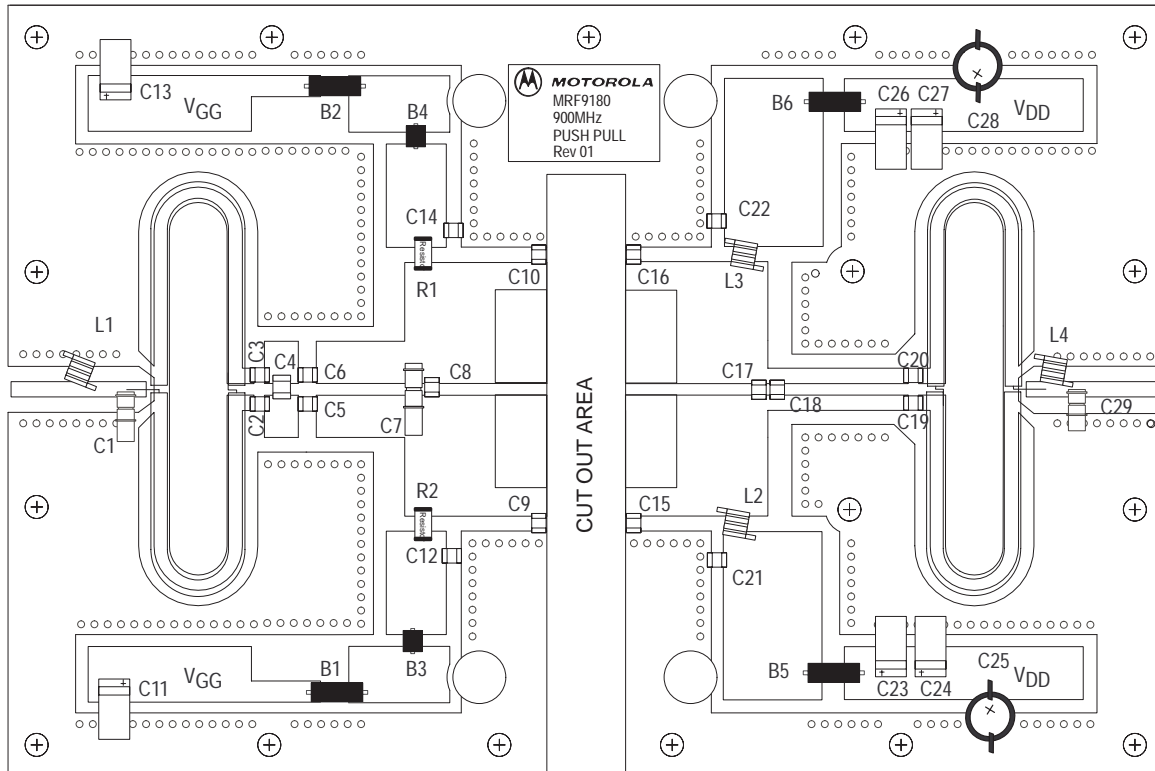


Figure 2. 880 MHz Broadband Test Circuit Component Layout

TYPICAL CHARACTERISTICS

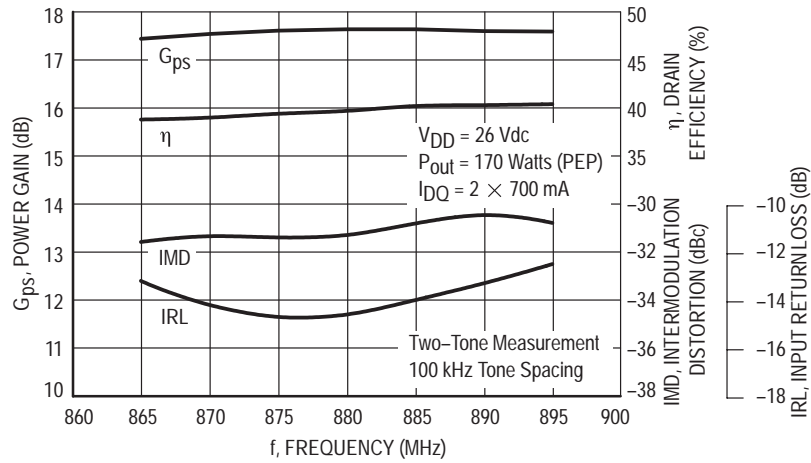


Figure 3. Class AB Broadband Circuit Performance

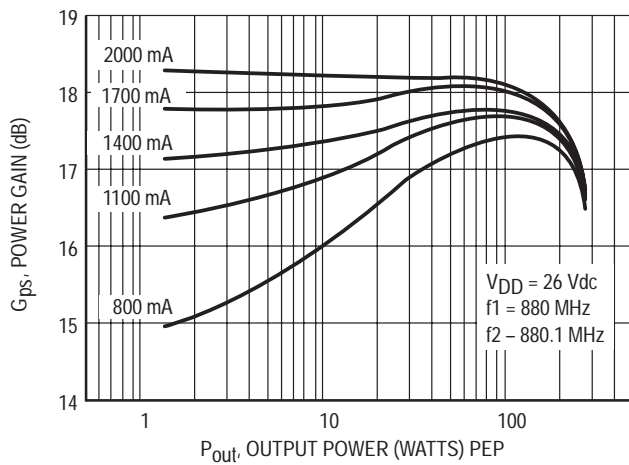


Figure 4. Power Gain versus Output Power

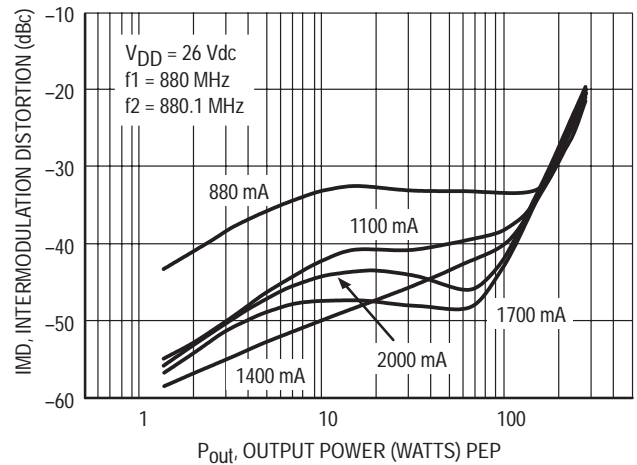


Figure 5. Intermodulation Distortion versus Output Power

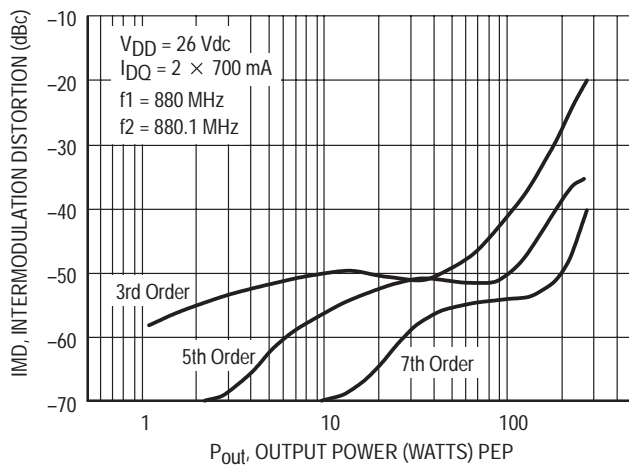


Figure 6. Intermodulation Distortion Products versus Output Power

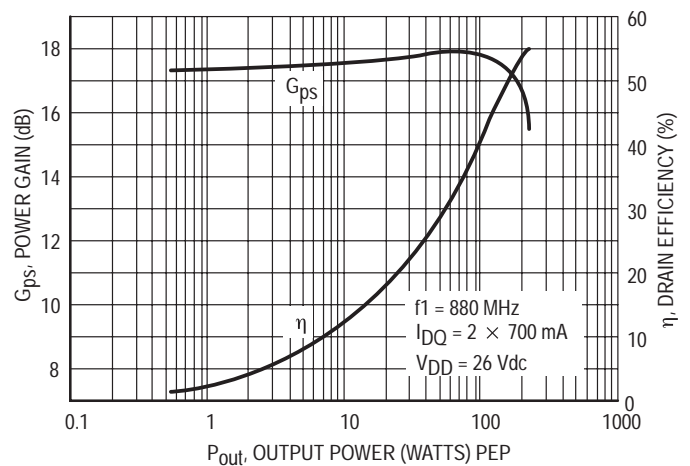


Figure 7. Power Gain and Efficiency versus Output Power

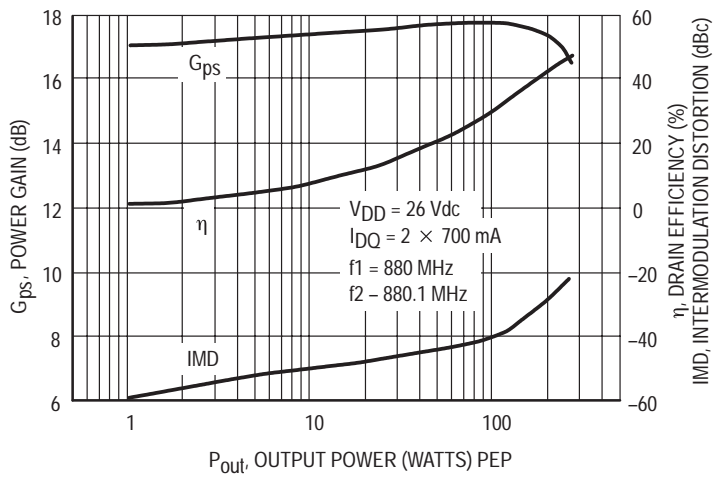


Figure 8. Power Gain, Efficiency and IMD versus Output Power

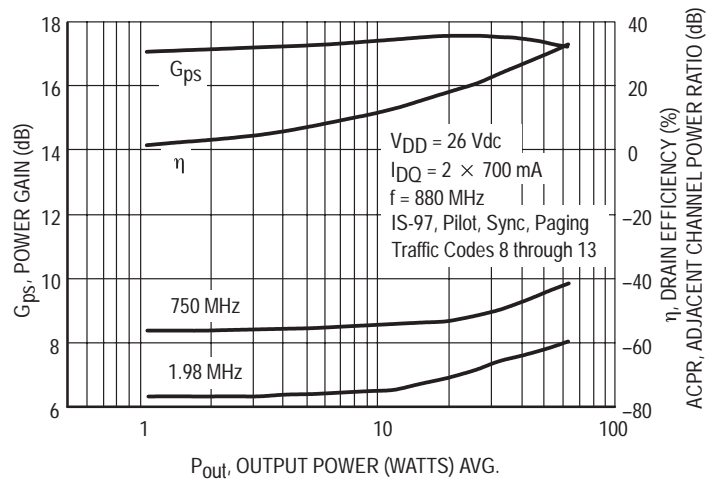
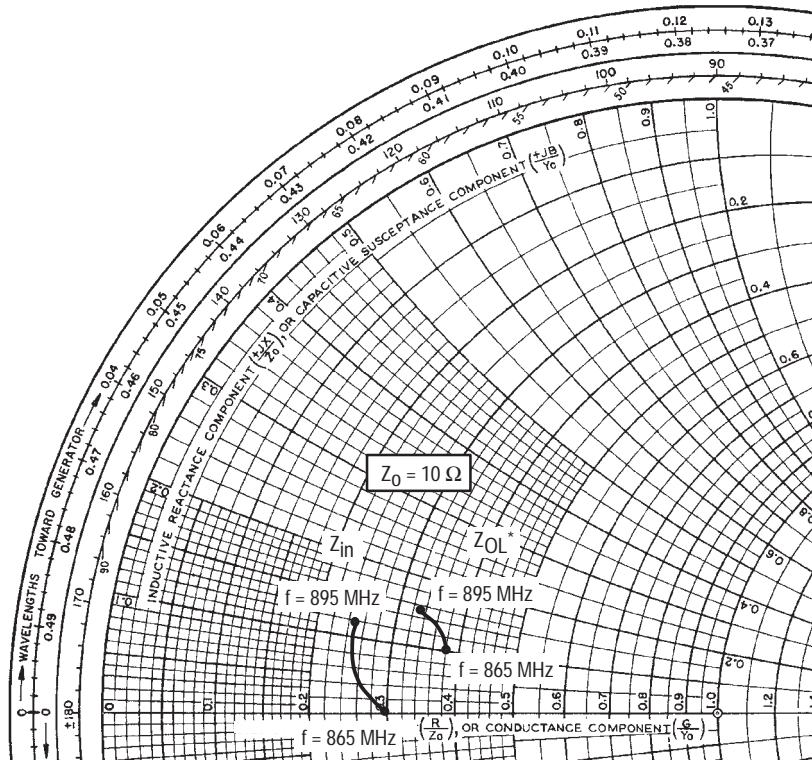


Figure 9. Power Gain, Efficiency and ACPR versus Output Power



$V_{DD} = 26 \text{ V}$, $I_{DQ} = 2 \times 700 \text{ mA}$, $P_{out} = 170 \text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
865	$2.95 + j0.00$	$3.83 + j1.02$
880	$2.48 + j0.67$	$3.55 + j1.38$
895	$2.44 + j1.18$	$3.34 + j1.51$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

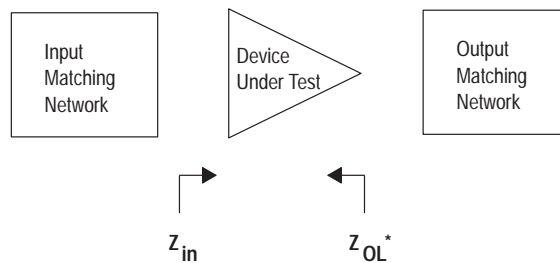


Figure 10. Series Equivalent Input and Output Impedance

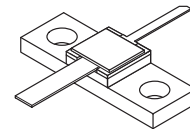
The RF Line Microwave Power Transistor

... designed for CW and long pulsed common base amplifier applications, such as JTIDS and Mode S, in the 0.96 to 1.215 GHz frequency range at high overall duty cycles.

- Guaranteed Performance @ 1.215 GHz, 28 Vdc
Output Power = 5.0 Watts CW
Minimum Gain = 8.5 dB, 10.3 dB (Typ)
- RF Performance Curves given for 28 Vdc and 36 Vdc Operation
- 100% Tested for Load Mismatch at All Phase Angles with 10:1 VSWR
- Hermetically Sealed Industry Standard Package
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Internal Input Matching for Broadband Operation
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MRF10005

**5.0 W, 960–1215 MHz
MICROWAVE POWER
TRANSISTOR
NPN SILICON**



CASE 336E-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CES}	55	Vdc
Collector–Base Voltage	V_{CBO}	55	Vdc
Emitter–Base Voltage	V_{EBO}	3.5	Vdc
Collector Current — Continuous (1)	I_C	1.25	mAdc
Total Device Dissipation @ $T_A = 25^\circ\text{C}$ (1) Derate above 25°C	P_D	25 143	Watt mW/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +200	$^\circ\text{C}$
Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (2)	$R_{\theta JC}$	7.0	$^\circ\text{C}/\text{W}$

NOTES:

1. These devices are designed for RF operation. The total device dissipation rating applies only when the devices are operated as RF amplifiers.
2. Thermal Resistance is determined under specified RF operating conditions by infrared measurement techniques.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Collector–Emitter Breakdown Voltage ($I_C = 25\text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	55	—	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 25\text{ mAdc}$, $I_E = 0$)	$V_{(BR)CBO}$	55	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 0.5\text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	3.5	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 28\text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	1.0	mAdc

ON CHARACTERISTICS

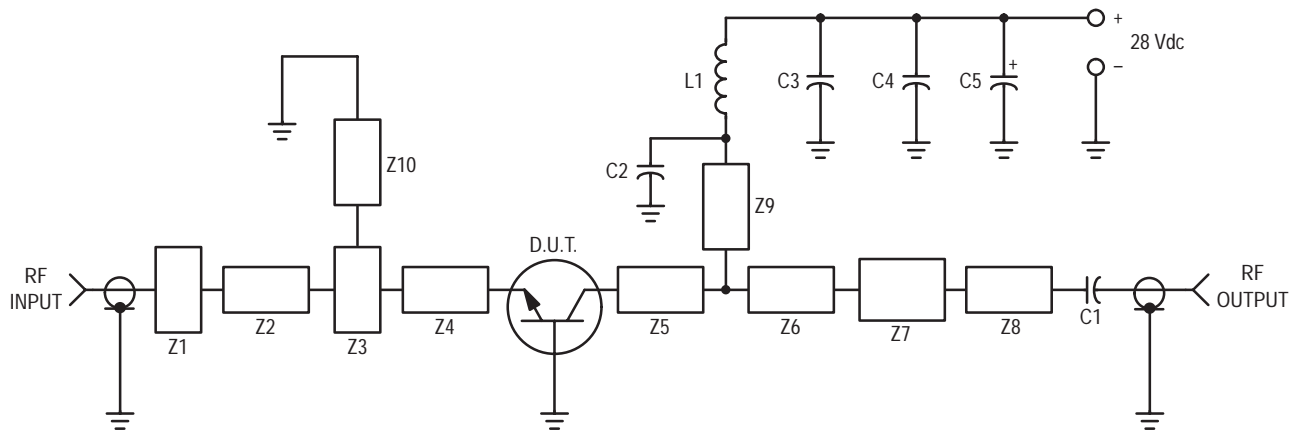
DC Current Gain ($I_C = 500\text{ mAdc}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	20	—	100	—
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DYNAMIC CHARACTERISTICS

Output Capacitance ($V_{CB} = 28\text{ Vdc}$, $I_E = 0$, $f = 1.0\text{ MHz}$)	C_{ob}	—	7.0	10	pF
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FUNCTIONAL TESTS

Common–Base Amplifier Power Gain ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 5.0\text{ W}$, $f = 1215\text{ MHz}$)	G_{PB}	8.5	10.3	—	dB
Collector Efficiency ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 5.0\text{ W}$, $f = 1215\text{ MHz}$)	η	45	55	—	%
Load Mismatch ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 5.0\text{ W}$, $f = 1215\text{ MHz}$, $VSWR = 10:1$ All Phase Angles)	ψ	No Degradation in Output Power			



C1, C2, C3 — 220 pF 100 mil Chip Capacitor
 C4 — 0.1 μF
 C5 — 47 $\mu\text{F}/50\text{ V}$ Electrolytic
 L1 — 3 turn #18 AWG, 1/8" ID, 0.18" Long

Z1–Z10 — Microstrip, see details below
 Board Material — 0.030" Glass Teflon,
 2.0 oz. Copper, $\epsilon_r = 2.55$

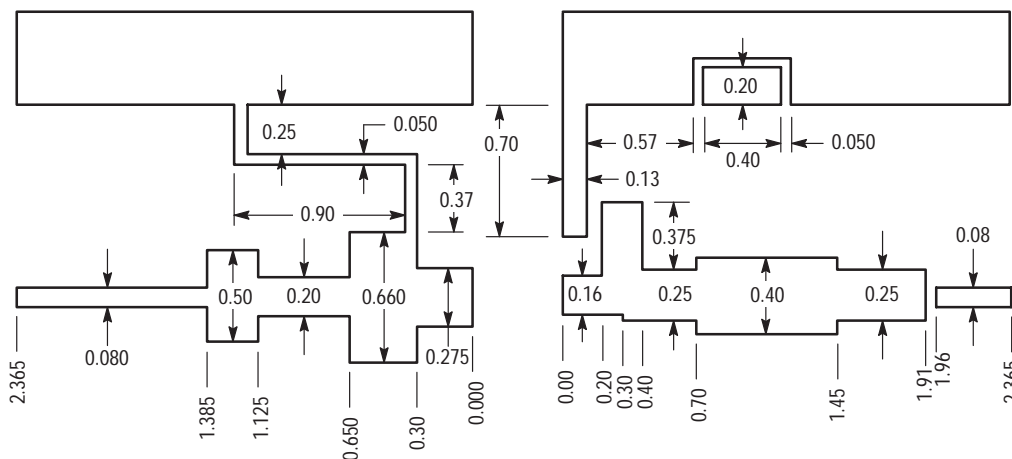


Figure 1. Test Circuit

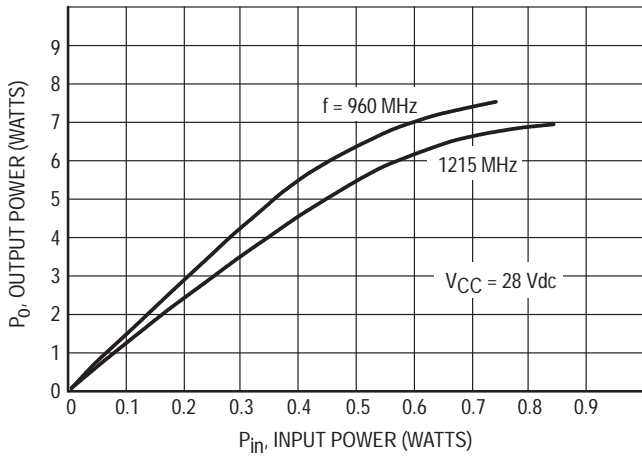


Figure 2. Output Power versus Input Power

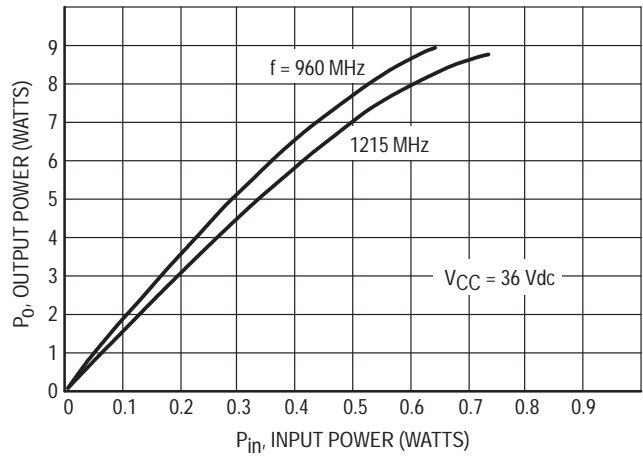


Figure 3. Output Power versus Input Power

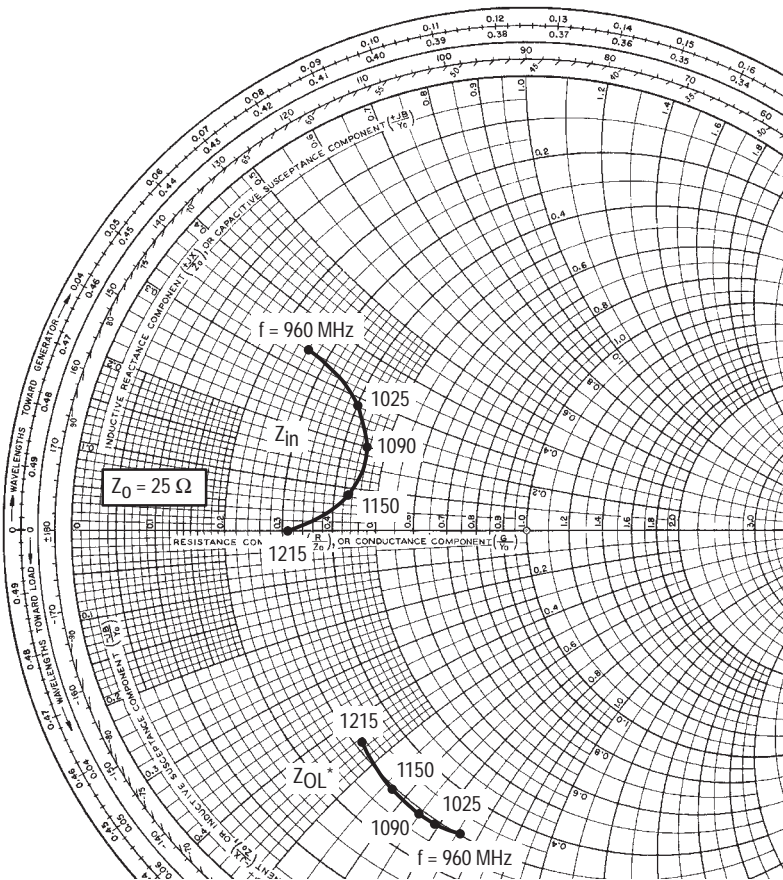


Figure 4. Series Equivalent Input/Output Impedances

$P_{out} = 5 \text{ W}, V_{CC} = 28 \text{ V}$

f MHz	Z_{in} OHMS	Z_{OL}^* OHMS
960	$6.5 + j8.5$	$7.4 - j18.9$
1025	$10.0 + j7.0$	$7.2 - j17.4$
1090	$11.2 + j4.9$	$7.1 - j16.3$
1150	$10.8 + j2.0$	$7.15 - j14.3$
1215	$7.8 + j0.0$	$7.8 - j11.2$

Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

The RF Line

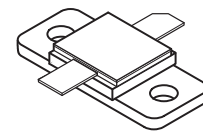
Microwave Long Pulse Power Transistor

Designed for 960–1215 MHz long or short pulse common base amplifier applications such as JTIDS and Mode-S transmitters.

- Guaranteed Performance @ 960 MHz, 36 Vdc
Output Power = 30 Watts Peak
Minimum Gain = 9.0 dB Min (9.5 dB Typ)
- 100% Tested for Load Mismatch at All Phase Angles with 10:1 VSWR
- Hermetically Sealed Industry Standard Package
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Internal Input Matching for Broadband Operation

MRF10031

**30 W (PEAK)
960–1215 MHz
MICROWAVE POWER
TRANSISTOR
NPN SILICON**



CASE 376B-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CES}	55	Vdc
Collector–Base Voltage (1)	V_{CBO}	55	Vdc
Emitter–Base Voltage	V_{EBO}	3.5	Vdc
Collector Current — Continuous (1)	I_C	3.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1), (2) Derate above 25°C	P_D	110 0.625	Watts mW/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	– 65 to + 200	$^\circ\text{C}$
Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (3)	$R_{\theta JC}$	1.6	$^\circ\text{C}/\text{W}$

NOTES:

1. Under pulse RF operating conditions.
2. These devices are designed for RF operation. The total device dissipation rating applies only when the devices are operated as pulsed RF amplifiers.
3. Thermal Resistance is determined under specified RF operating conditions by infrared measurement techniques. (Worst case θ_{JC} value measured @ 23% duty cycle)

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

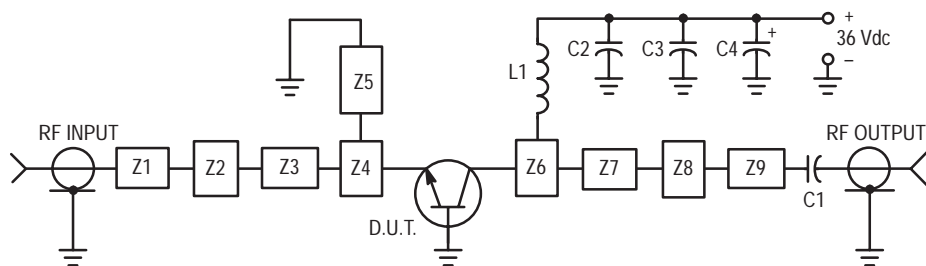
Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Collector-Emitter Breakdown Voltage ($I_C = 25\text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	55	—	—	Vdc
Collector-Base Breakdown Voltage ($I_C = 25\text{ mAdc}$, $I_E = 0$)	$V_{(BR)CBO}$	55	—	—	Vdc
Emitter-Base Breakdown Voltage ($I_E = 5.0\text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	3.5	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 36\text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	2.0	mAdc

ON CHARACTERISTICS

DC Current Gain ($I_C = 500\text{ mAdc}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	20	—	—	—
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FUNCTIONAL TESTS (10 μs Pulses @ 50% duty cycle for 3.5 ms; overall duty cycle – 25%)

Common-Base Amplifier Power Gain ($V_{CC} = 36\text{ Vdc}$, $P_{out} = 30\text{ W Peak}$, $f = 960\text{ MHz}$)	G_{PB}	9.0	9.5	—	dB
Collector Efficiency ($V_{CC} = 36\text{ Vdc}$, $P_{out} = 30\text{ W Peak}$, $f = 960\text{ MHz}$)	η	40	45	—	%
Load Mismatch ($V_{CC} = 36\text{ Vdc}$, $P_{out} = 30\text{ W Peak}$, $f = 960\text{ MHz}$, $VSWR = 10:1$ All Phase Angles)	ψ	No Degradation in Output Power			



- C1 — 75 pF 100 Mil Chip Capacitor
- C2 — 39 pF 100 Mil Chip Capacitor
- C3 — 0.1 μF
- C4 — 1000 μF , 50 Vdc, Electrolytic
- L1 — 3 Turns #18 AWG, 1/8" ID, 0.18 Long

- Z1–Z9 — Microstrip, See Details
- Board Material — Teflon, Glass Laminate
- Dielectric Thickness = 0.030"
- $\epsilon_r = 2.55$, 2 Oz. Copper

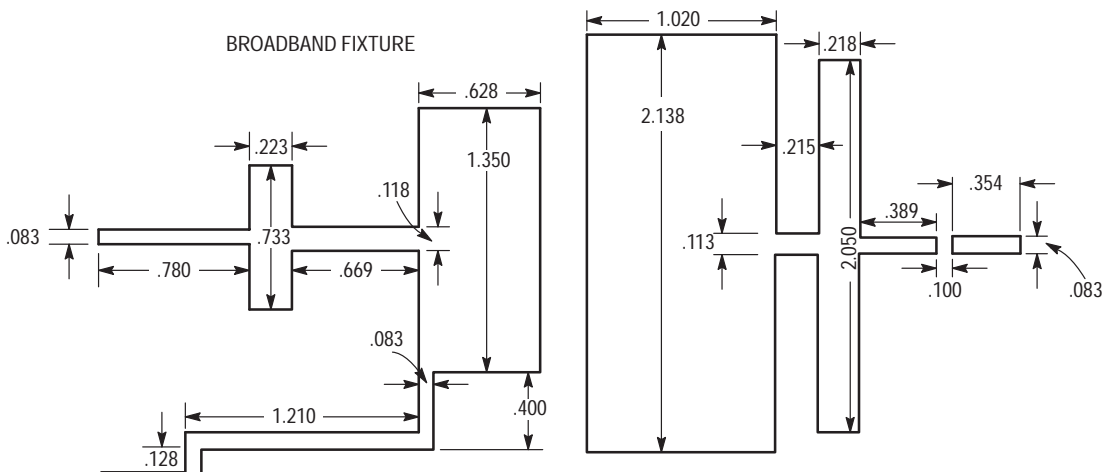


Figure 1. Test Circuit

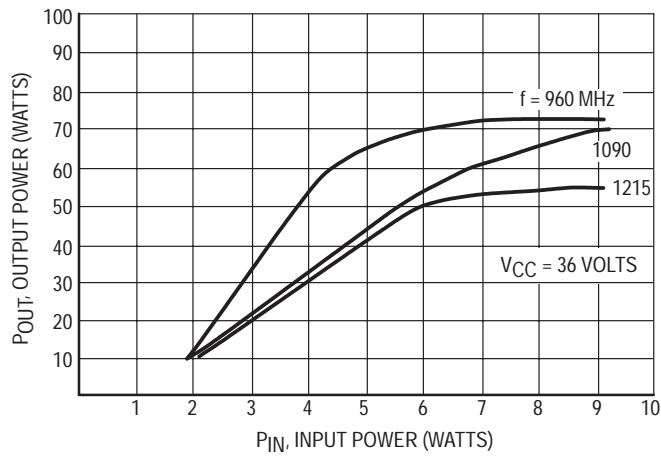
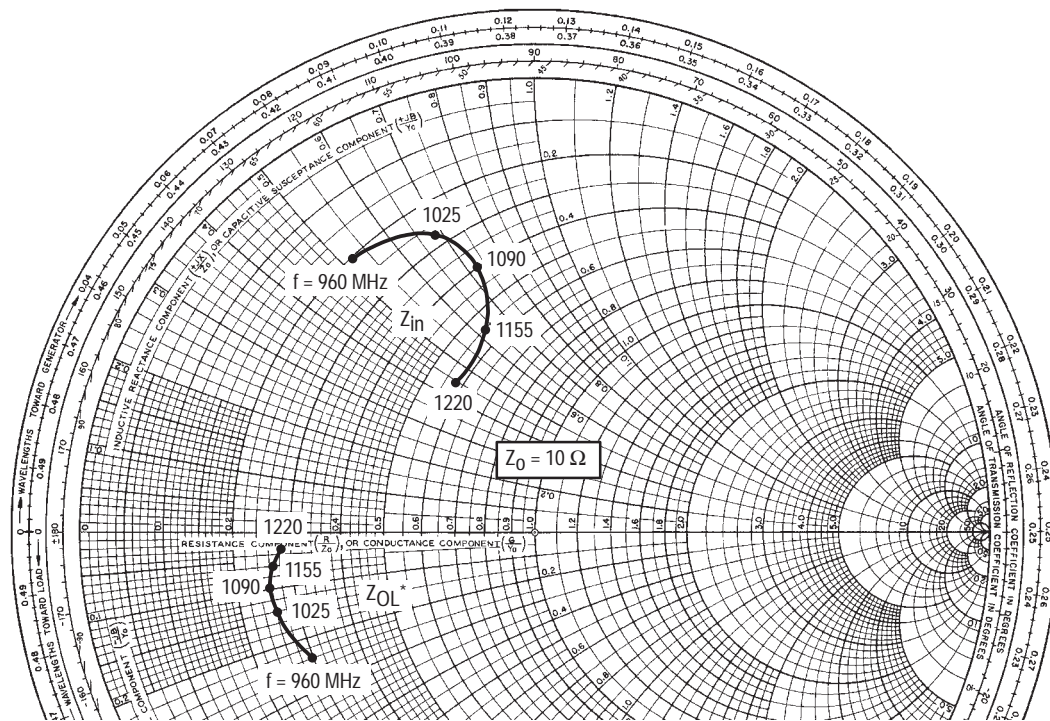


Figure 2. Output Power versus Input Power



$P_{out} = 30 \text{ W Pk}$ $V_{CC} = 36 \text{ V}$

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
960	$2.05 + j5.2$	$2.9 - j2.35$
1025	$2.67 + j6.34$	$2.55 - j1.3$
1090	$4.0 + j7.1$	$2.52 - j0.9$
1155	$5.5 + j6.2$	$2.6 - j0.6$
1220	$5.7 + j4.3$	$2.8 - j0.3$

Z_{OL}^* = Conjugate of the optimum load impedance into which the device operates at a given output power, voltage, and frequency.

Figure 3. Series Equivalent Input/Output Impedances

The RF Line

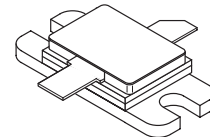
Microwave Long Pulse Power Transistor

Designed for 960–1215 MHz long pulse common base amplifier applications such as JTIDS and Mode S transmitters.

- Guaranteed Performance @ 1.215 GHz, 36 Vdc
Output Power = 120 Watts Peak
Gain = 8.0 dB Min., 9.2 dB (Typ)
- 100% Tested for Load Mismatch at All Phase Angles with 3:1 VSWR
- Hermetically Sealed Industry Standard Package
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Internal Input and Output Matching for Broadband Operation
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MRF10120

**120 W (PEAK), 960–1215 MHz
MICROWAVE POWER
TRANSISTOR
NPN SILICON**



CASE 355C-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CES}	55	Vdc
Collector–Base Voltage	V_{CBO}	55	Vdc
Emitter–Base Voltage	V_{EBO}	3.5	Vdc
Collector Current — Peak (1)	I_C	15	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1), (2) Derate above 25°C	P_D	380 2.17	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +200	$^\circ\text{C}$
Junction Temperature	T_J	200	

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (3)	$R_{\theta JC}$	0.46	$^\circ\text{C}/\text{W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector–Emitter Breakdown Voltage ($I_C = 60 \text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	55	—	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 60 \text{ mAdc}$, $I_E = 0$)	$V_{(BR)CBO}$	55	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 10 \text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	3.5	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 36 \text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	25	mAdc

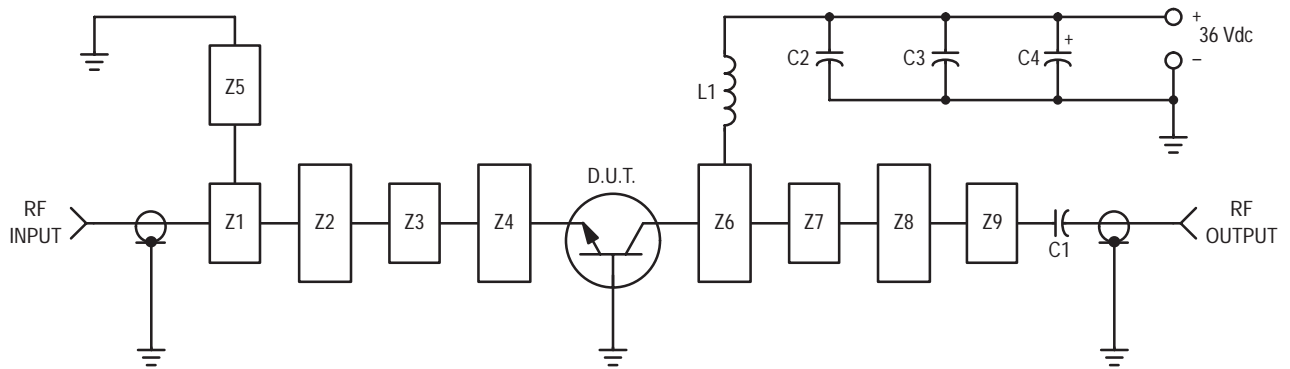
NOTES:

1. Under pulse RF operating conditions.
2. These devices are designed for RF operation. The total device dissipation rating applies only when the device is operated as RF amplifiers.
3. Thermal Resistance is determined under specified RF operating conditions by infrared measurement techniques.

(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
ON CHARACTERISTICS					
DC Current Gain ($I_C = 5.0 \text{ Adc}$, $V_{CE} = 5.0 \text{ Vdc}$)	h_{FE}	20	—	—	—
FUNCTIONAL TESTS (7.0 μs Pulses @ 54% duty cycle for 3.4 ms; then off for 4.5 ms; overall duty cycle = 23%)					
Common-Base Amplifier Power Gain ($V_{CC} = 36 \text{ Vdc}$, $P_{out} = 120 \text{ W Peak}$, $f = 1215 \text{ MHz}$)	GPB	8.0	9.2	—	dB
Collector Efficiency ($V_{CC} = 36 \text{ Vdc}$, $P_{out} = 120 \text{ W Peak}$, $f = 1215 \text{ MHz}$)	η	50	55	—	%
Load Mismatch ($V_{CC} = 36 \text{ Vdc}$, $P_{out} = 120 \text{ W Peak}$, $f = 1215 \text{ MHz}$, $VSWR = 3:1$ All Phase Angles)	ψ	No Degradation in Output Power			



C1 — 270 pF 100 Mil Chip Capacitor
 C2 — 220 pF 100 Mil Chip Capacitor
 C3 — 0.1 μF
 C4 — 47 μF 50 V Electrolytic
 L1 — 3 Turns #18 AWG, 1/8" ID, 0.18 Long

Z1–Z9 — Microstrip, See Details
 Board Material — Teflon®/Glass Laminate,
 Dielectric Thickness = 0.030",
 $\epsilon_r = 2.55$, 2 Oz. Copper

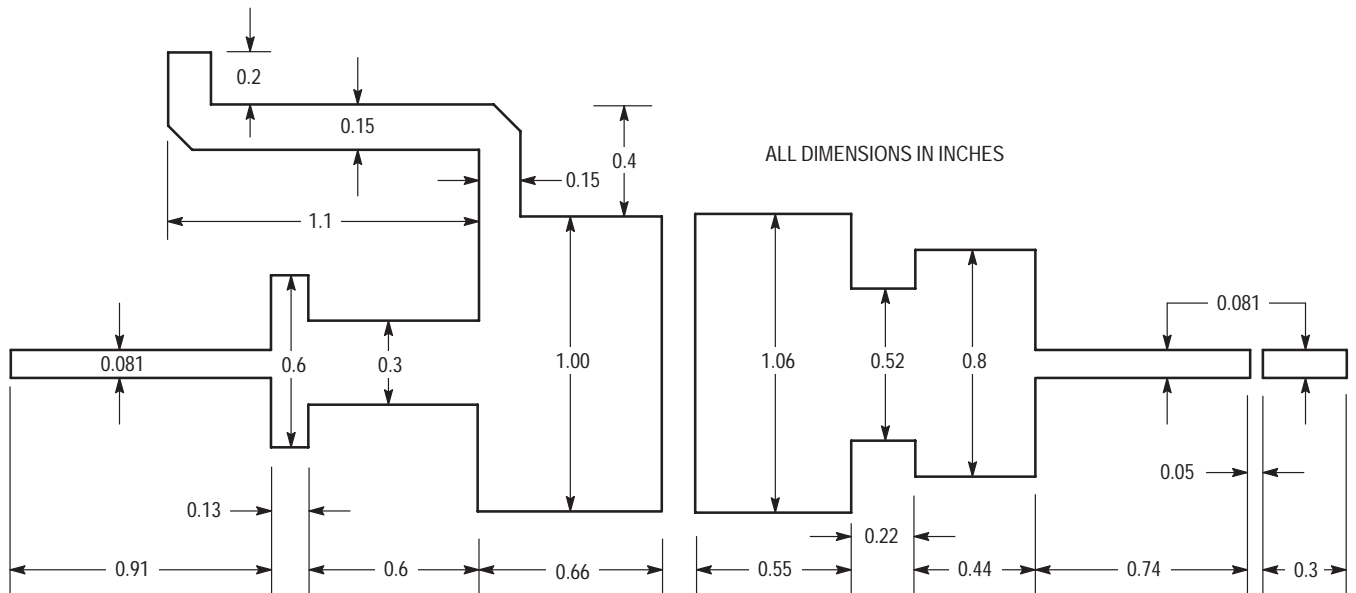


Figure 1. Test Circuit

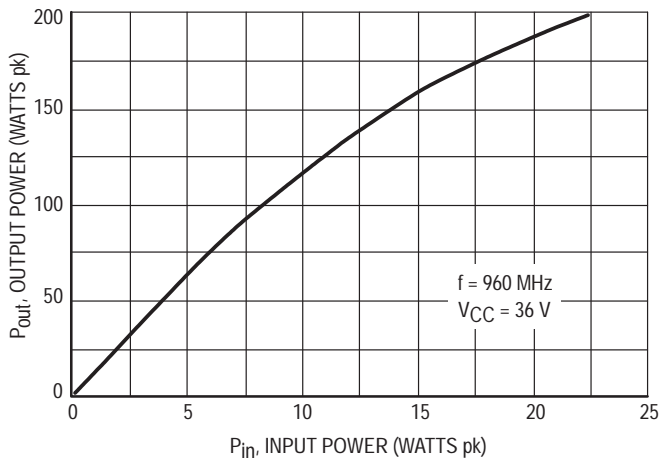


Figure 2. Output Power versus Input Power

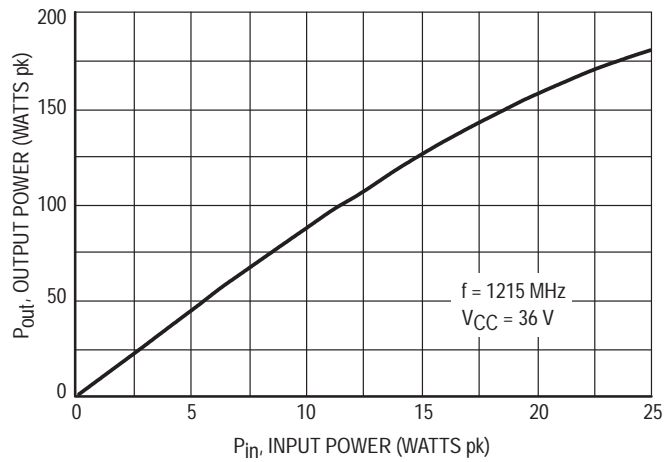


Figure 3. Output Power versus Input Power

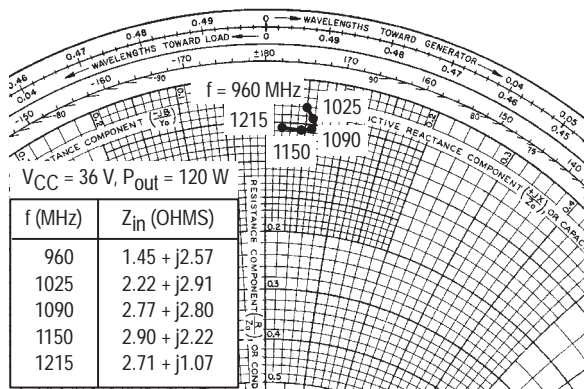
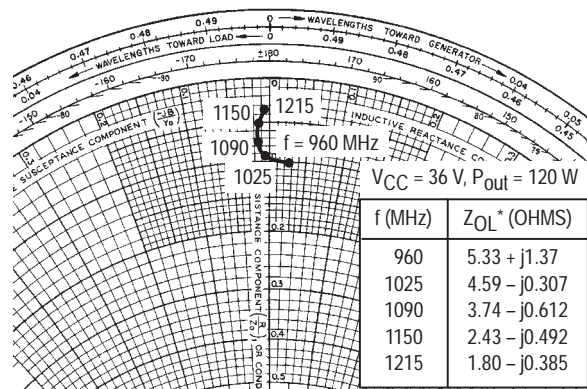


Figure 4. Series Equivalent Input Impedances



Z_{OL}* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

Figure 5. Series Equivalent Output Impedance

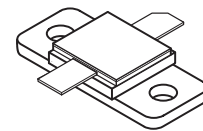
The RF Line Microwave Pulse Power Transistor

... designed for 1025–1150 MHz pulse common base amplifier applications such as TCAS, TACAN and Mode-S transmitters.

- Guaranteed Performance @ 1090 MHz
Output Power = 150 Watts Peak
Gain = 9.5 dB Min, 10.0 dB (Typ)
- 100% Tested for Load Mismatch at All Phase Angles with 10:1 VSWR
- Hermetically Sealed Package
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Internal Input and Output Matching
- Characterized with 10 μ s, 10% Duty Cycle Pulses
- Recommended Driver for a Pair of MRF10500 Transistors

MRF10150

**150 W (PEAK)
1025–1150 MHz
MICROWAVE POWER
TRANSISTOR
NPN SILICON**



CASE 376B-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CES}	65	Vdc
Collector–Base Voltage	V_{CBO}	65	Vdc
Emitter–Base Voltage	V_{EBO}	3.5	Vdc
Collector Current — Peak (1)	I_C	14	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1), (2) Derate above 25°C	P_D	700 4.0	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +200	$^\circ\text{C}$
Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (3)	$R_{\theta JC}$	0.25	$^\circ\text{C}/\text{W}$

NOTES:

1. Under pulse RF operating conditions.
2. These devices are designed for RF operation. The total device dissipation rating applies only when the devices are operated as pulsed RF amplifiers.
3. Thermal Resistance is determined under specified RF operating conditions by infrared measurement techniques. (Worst case θ_{JC} value measured @ 10 μ s, 10%.)

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Collector–Emitter Breakdown Voltage ($I_C = 60\text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	65	—	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 60\text{ mAdc}$, $I_E = 0$)	$V_{(BR)CBO}$	65	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 10\text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	3.5	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 36\text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	25	mAdc

ON CHARACTERISTICS

DC Current Gain ($I_C = 5.0\text{ Adc}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	20	—	—	—
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FUNCTIONAL TESTS

Common–Base Amplifier Power Gain ($V_{CC} = 50\text{ Vdc}$, $P_{out} = 150\text{ W Peak}$, $f = 1090\text{ MHz}$)	G_{PB}	9.5	10	—	dB
Collector Efficiency ($V_{CC} = 50\text{ Vdc}$, $P_{out} = 150\text{ W Peak}$, $f = 1090\text{ MHz}$)	η	40	—	—	%
Load Mismatch ($V_{CC} = 50\text{ Vdc}$, $P_{out} = 150\text{ W Peak}$, $f = 1090\text{ MHz}$, $VSWR = 10:1$ All Phase Angles)	ψ	No Degradation in Output Power			

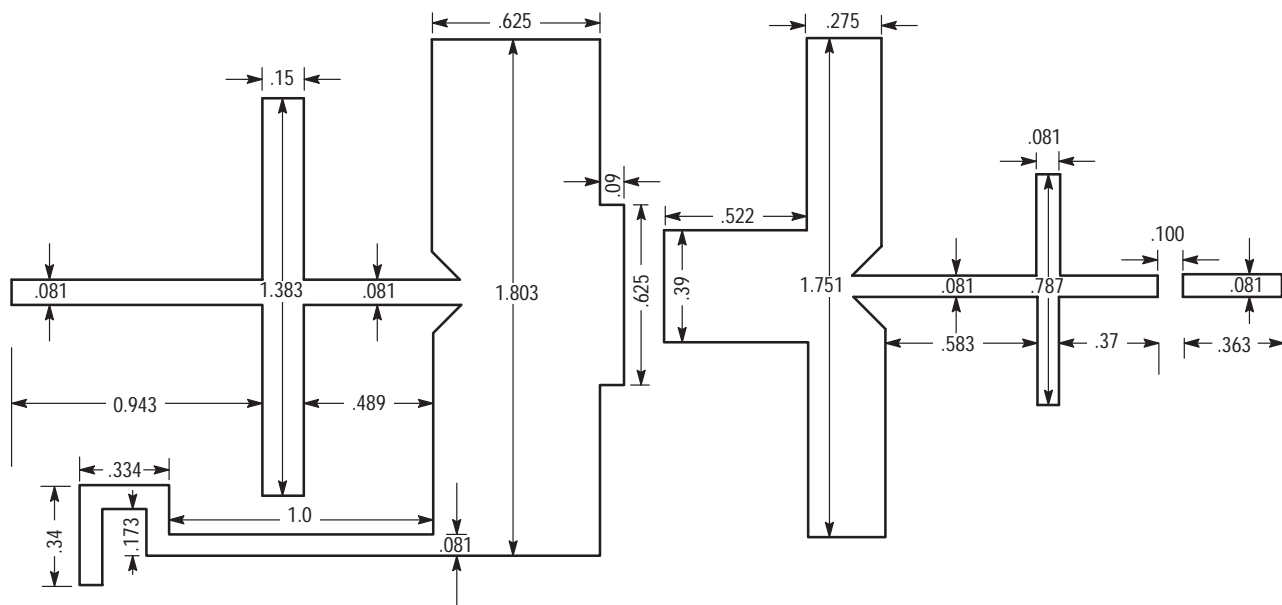
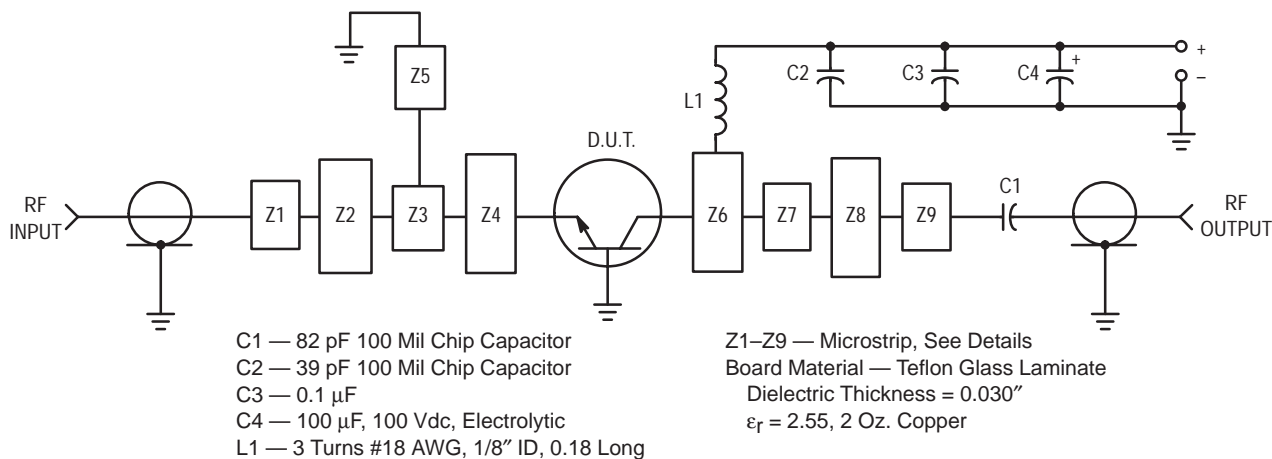


Figure 1. Test Circuit

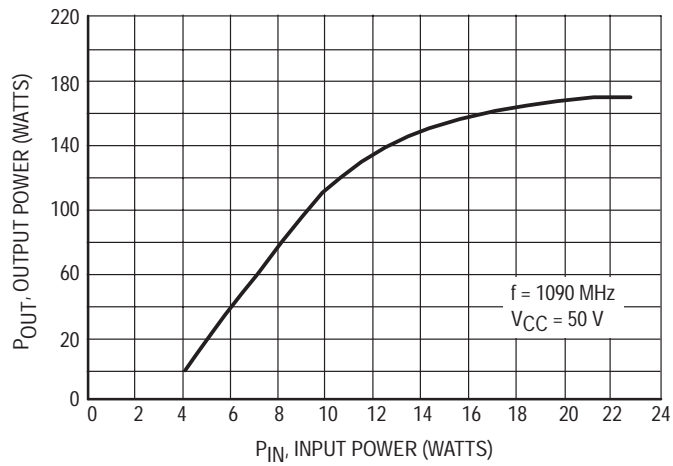
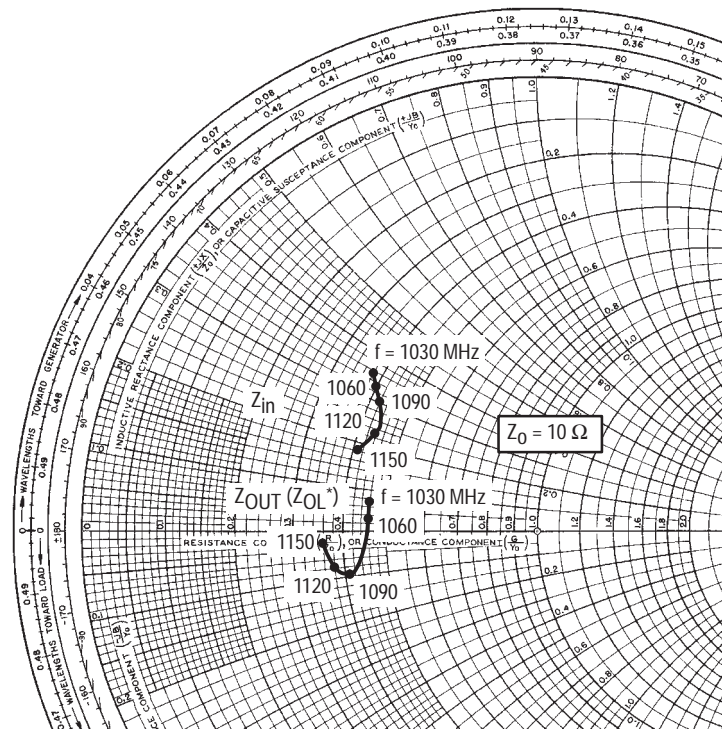


Figure 2. Output Power versus Input Power



P_{OUT} = 150 W Pk V_{CC} = 50 V

f MHz	Z _{in} OHMS	Z _{OL} * (Z _{OUT}) OHMS
1030	3.8 + j3.5	4.6 + j0.7
1060	4.0 + j3.3	4.6 + j0.3
1090	4.2 + j3.0	4.1 - j1.0
1120	4.4 + j2.3	3.8 - j0.8
1150	4.1 + j1.8	3.6 - j0.3

Z_{OL}* is the conjugate of the optimum load impedance into which the device operates at a given output power voltage and frequency.

Figure 3. Series Equivalent Input/Output Impedances

The RF Line

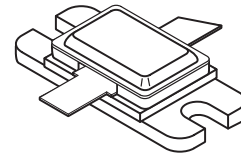
Microwave Pulse Power Transistor

Designed for 1025–1150 MHz pulse common base amplifier applications such as TCAS, TACAN and Mode-S transmitters.

- Guaranteed Performance @ 1090 MHz
Output Power = 350 Watts Peak
Gain = 8.5 dB Min, 9.0 dB (Typ)
- 100% Tested for Load Mismatch at All Phase Angles with 10:1 VSWR
- Hermetically Sealed Package
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Internal Input and Output Matching
- Characterized using Mode-S Pulse Format

MRF10350

350 W (PEAK)
1025–1150 MHz
MICROWAVE POWER
TRANSISTOR
NPN SILICON



CASE 355E-01, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CES}	65	Vdc
Collector–Base Voltage	V_{CBO}	65	Vdc
Emitter–Base Voltage	V_{EBO}	3.5	Vdc
Collector Current — Peak (1)	I_C	31	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1), (2) Derate above 25°C	P_D	1590 9.1	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +200	$^\circ\text{C}$
Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (3)	$R_{\theta JC}$	0.11	$^\circ\text{C}/\text{W}$

NOTES:

1. Under pulse RF operating conditions.
2. These devices are designed for RF operation. The total device dissipation rating applies only when the devices are operated as pulsed RF amplifiers.
3. Thermal Resistance is determined under specified RF operating conditions by infrared measurement techniques. (Worst Case θ_{JC} measured using Mode-S pulse train, 128 μs burst 0.5 μs on, 0.5 μs off repeating at 6.4 ms interval.)

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

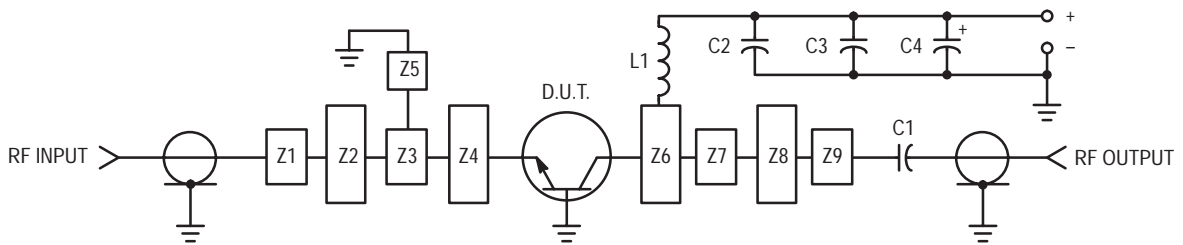
Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Collector–Emitter Breakdown Voltage ($I_C = 60\text{ mA dc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	65	—	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 60\text{ mA dc}$, $I_E = 0$)	$V_{(BR)CBO}$	65	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 10\text{ mA dc}$, $I_C = 0$)	$V_{(BR)EBO}$	3.5	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 36\text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	25	mA dc

ON CHARACTERISTICS

DC Current Gain ($I_C = 5.0\text{ A dc}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	20	—	—	—
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FUNCTIONAL TESTS

Common–Base Amplifier Power Gain ($V_{CC} = 50\text{ Vdc}$, $P_{out} = 350\text{ W Peak}$, $f = 1090\text{ MHz}$)	G_{PB}	8.5	9.0	—	dB
Collector Efficiency ($V_{CC} = 50\text{ Vdc}$, $P_{out} = 350\text{ W Peak}$, $f = 1090\text{ MHz}$)	η	40	—	—	%
Load Mismatch ($V_{CC} = 50\text{ Vdc}$, $P_{out} = 350\text{ W Peak}$, $f = 1090\text{ MHz}$, $VSWR = 10:1$ All Phase Angles)	ψ	No Degradation in Output Power			



- C1 — 75 pF 100 Mil Chip Capacitor
- C2 — 39 pF 100 Mil Chip Capacitor
- C3 — 0.1 μF
- C4 — 100 μF , 100 Vdc, Electrolytic
- L1 — 3 Turns #18 AWG, 1/8" ID, 0.18 Long

- Z1–Z9 — Microstrip, See Details
- Board Material — Teflon, Glass Laminate
- Dielectric Thickness = 0.030"
- $\epsilon_r = 2.55$, 2 Oz. Copper

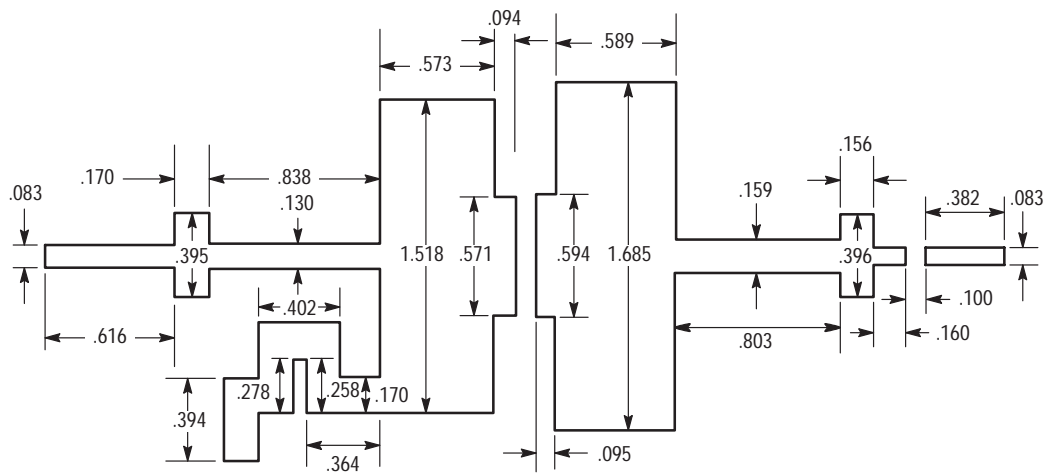
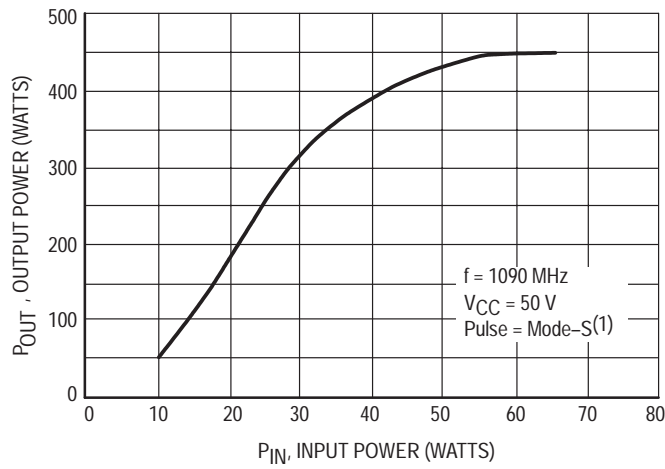
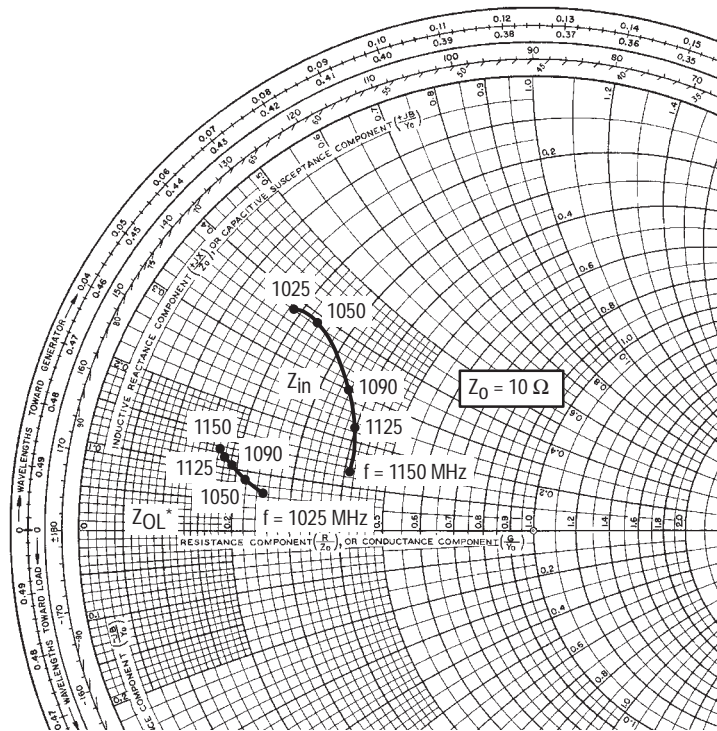


Figure 1. Test Circuit



(1) 128 μ s burst 0.5 μ s on, 0.5 μ s off repeating at 6.4 ms interval.

Figure 2. Output Power versus Input Power



$P_{OUT} = 350$ W Pk $V_{CC} = 50$ V

f MHz	Z_{in} OHMS	Z_{OL}^* (1) OHMS
1025	$1.92 + j3.80$	$2.52 + j0.70$
1050	$2.44 + j3.92$	$2.18 + j0.85$
1090	$3.55 + j3.02$	$1.94 + j1.13$
1125	$4.11 + j2.27$	$1.80 + j1.22$
1150	$4.13 + j1.35$	$1.71 + j1.31$

Z_{OL}^* is the conjugate of the optimum load impedance into which the device operates at a given output power voltage and frequency.

Figure 3. Series Equivalent Input/Output Impedances

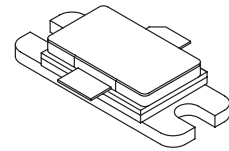
The RF Line Microwave Pulse Power Transistor

Designed for 1025–1150 MHz pulse common base amplifier applications such as TCAS, TACAN and Mode-S transmitters.

- Guaranteed Performance @ 1090 MHz
Output Power = 500 Watts Peak
Gain = 8.5 dB Min, 9.0 dB (Typ)
- 100% Tested for Load Mismatch at All Phase Angles with 10:1 VSWR
- Hermetically Sealed Industry Package
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Internal Input and Output Matching
- Characterized with 10 μ s, 1% Duty Cycle Pulses

MRF10502

**500 W (PEAK)
1025–1150 MHz
MICROWAVE POWER
TRANSISTOR
NPN SILICON**



CASE 355J-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CES}	65	Vdc
Collector–Base Voltage	V_{CBO}	65	Vdc
Emitter–Base Voltage	V_{EBO}	3.5	Vdc
Collector Current — Peak (1)	I_C	29	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (1), (2) Derate above 25°C	P_D	1460 8.3	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	–65 to +200	$^\circ\text{C}$
Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (3)	$R_{\theta JC}$	0.12	$^\circ\text{C}/\text{W}$

NOTES:

1. Under pulse RF operating conditions.
2. These devices are designed for RF operation. The total device dissipation rating applies only when the devices are operated as pulsed RF amplifiers.
3. Thermal Resistance is determined under specified RF operating conditions by infrared measurement techniques. (Worst case θ_{JC} value measured @ 32 μ s, 2%.)

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted.)

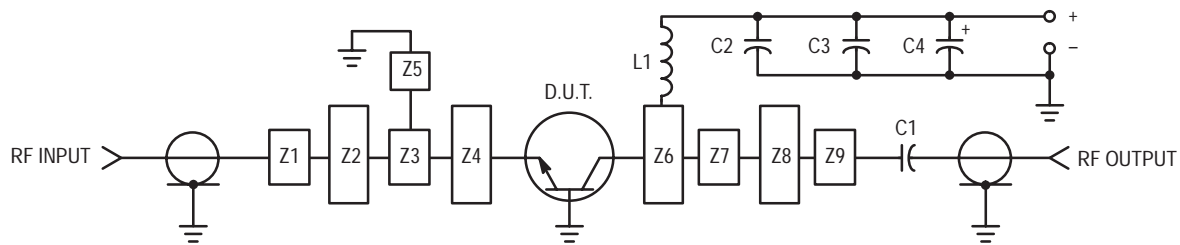
Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Collector-Emitter Breakdown Voltage ($I_C = 60 \text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	65	—	—	Vdc
Collector-Base Breakdown Voltage ($I_C = 60 \text{ mAdc}$, $I_E = 0$)	$V_{(BR)CBO}$	65	—	—	Vdc
Emitter-Base Breakdown Voltage ($I_E = 10 \text{ mAdc}$, $I_C = 0$)	$V_{(BR)EBO}$	3.5	—	—	Vdc
Collector Cutoff Current ($V_{CB} = 36 \text{ Vdc}$, $I_E = 0$)	I_{CBO}	—	—	25	mAdc

ON CHARACTERISTICS

DC Current Gain ($I_C = 5.0 \text{ Adc}$, $V_{CE} = 5.0 \text{ Vdc}$)	h_{FE}	20	—	—	—
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FUNCTIONAL TESTS

Common-Base Amplifier Power Gain ($V_{CC} = 50 \text{ Vdc}$, $P_{Out} = 500 \text{ W Peak}$, $f = 1090 \text{ MHz}$)	G_{PB}	8.5	9.0	—	dB
Collector Efficiency ($V_{CC} = 50 \text{ Vdc}$, $P_{Out} = 500 \text{ W Peak}$, $f = 1090 \text{ MHz}$)	η	40	45	—	%
Load Mismatch ($V_{CC} = 50 \text{ Vdc}$, $P_{Out} = 500 \text{ W Peak}$, $f = 1090 \text{ MHz}$, $VSWR = 10:1$ All Phase Angles)	ψ	No Degradation in Output Power			



- C1 — 82 pF 100 Mil Chip Capacitor
- C2 — 39 pF 100 Mil Chip Capacitor
- C3 — 0.1 μF
- C4 — 100 μF , 100 Vdc, Electrolytic
- L1 — 3 Turns #18 AWG, 1/8" ID, 0.18 Long

- Z1–Z9 — Microstrip, See Details
- Board Material — Teflon, Glass Laminate
- Dielectric Thickness = 0.030"
- $\epsilon_r = 2.55$, 2 Oz. Copper

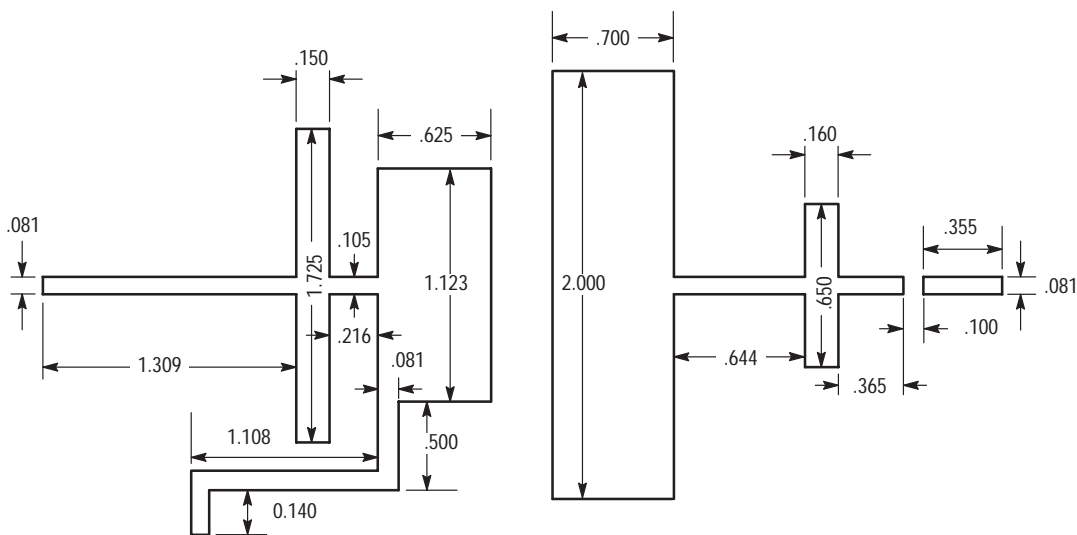


Figure 1. Test Circuit

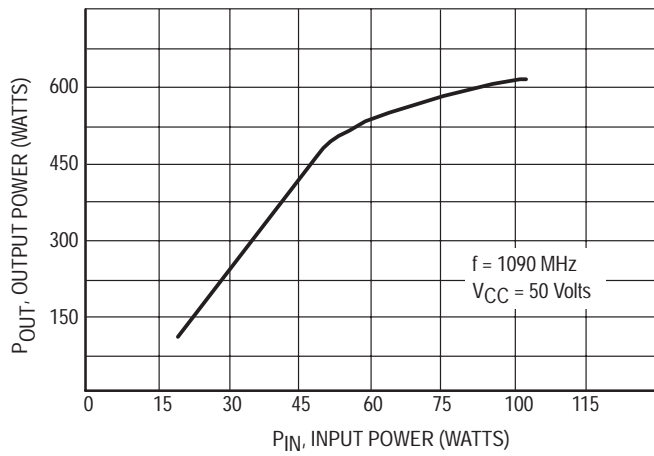
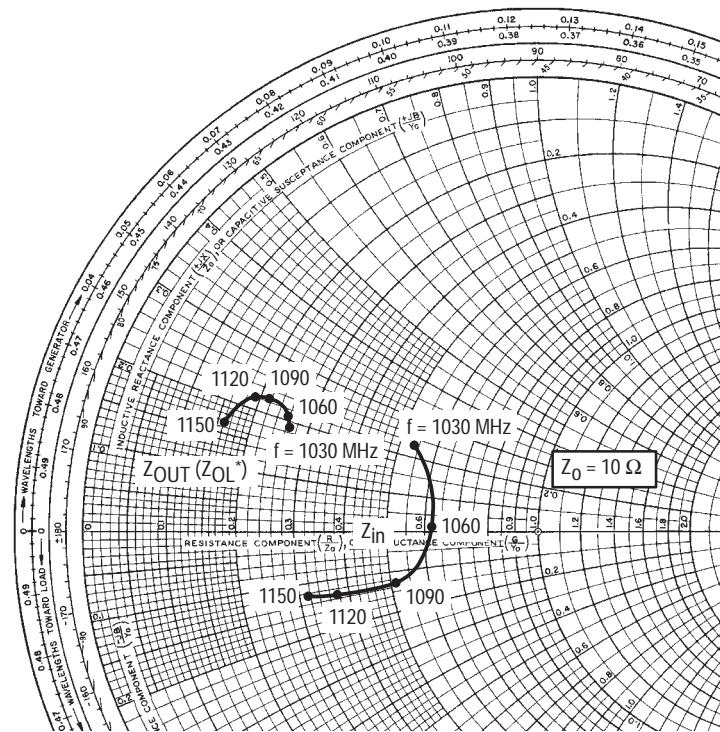


Figure 2. Output Power versus Input Power



$P_{OUT} = 500 \text{ W Pk}$ $V_{CC} = 50 \text{ V}$

f MHz	Z_{in} OHMS	$Z_{OL}^* (Z_{OUT})$ OHMS
1030	$5.3 + j2.25$	$2.6 + j1.89$
1060	$6.2 + j0.2$	$2.56 + j2.0$
1090	$5.2 - j1.4$	$2.12 + j2.2$
1120	$3.7 - j1.35$	$1.9 + j2.15$
1150	$3.15 - j1.3$	$1.6 + j1.62$

Z_{OL}^* is the conjugate of the optimum load impedance into which the device operates at a given output power voltage and frequency.

Figure 3. Series Equivalent Input/Output Impedances

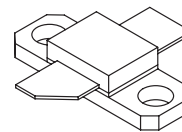
The RF Line
NPN Silicon
RF Power Transistor

Designed for 28 Volt microwave large-signal, common base, Class-C CW amplifier applications in the range 1600 – 1640 MHz.

- Specified 28 Volt, 1.6 GHz Class-C Characteristics
Output Power = 6 Watts
Minimum Gain = 7.4 dB, @ 6 Watts
Minimum Efficiency = 40% @ 6 Watts
- Characterized with Series Equivalent Large-Signal Parameters from 1500 MHz to 1700 MHz
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MRF16006

6.0 WATTS, 1.6 GHz
RF POWER TRANSISTOR
NPN SILICON



CASE 395C-01, STYLE 2

MAXIMUM RATINGS ($T_J = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CES}	60	Vdc
Emitter-Base Voltage	V_{EBO}	4.0	Vdc
Collector-Current	I_C	1.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	26 0.15	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

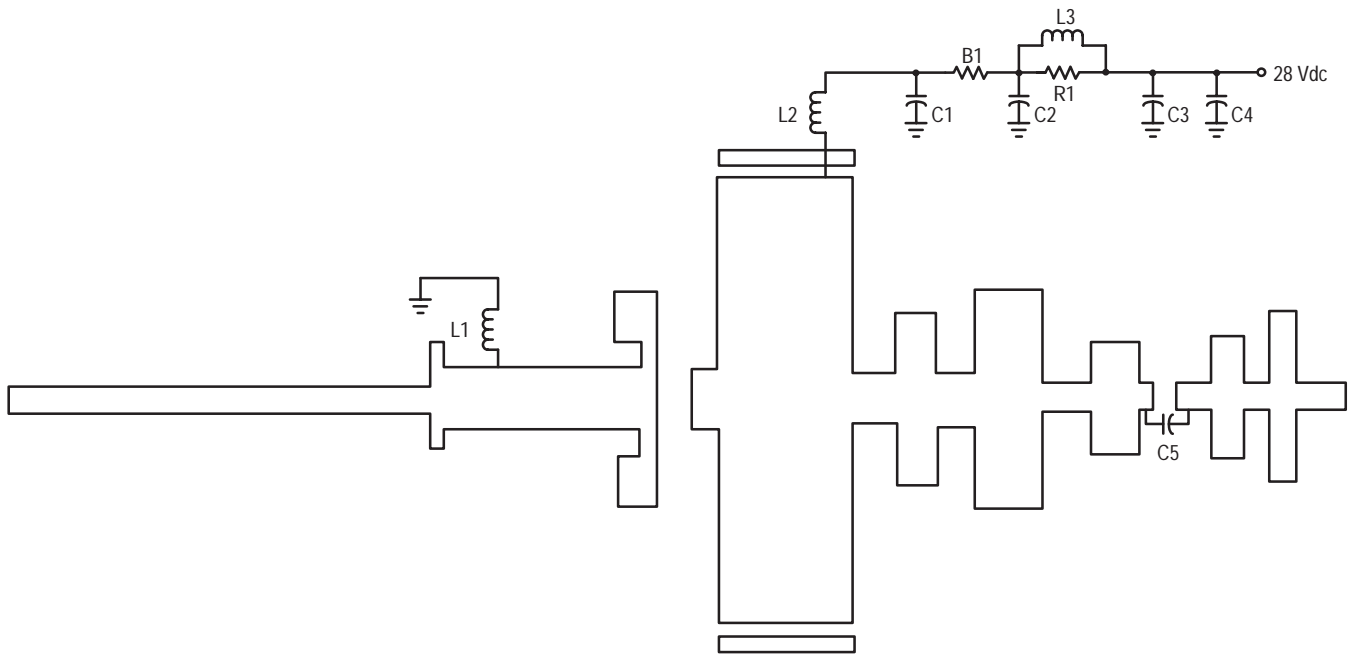
Thermal Resistance — Junction to Case (1) (2)	$R_{\theta JC}$	6.8	$^\circ\text{C/W}$
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(1) Thermal measurement performed using CW RF operating condition.

(2) Thermal resistance is determined under specified RF operating conditions by infrared measurement techniques.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

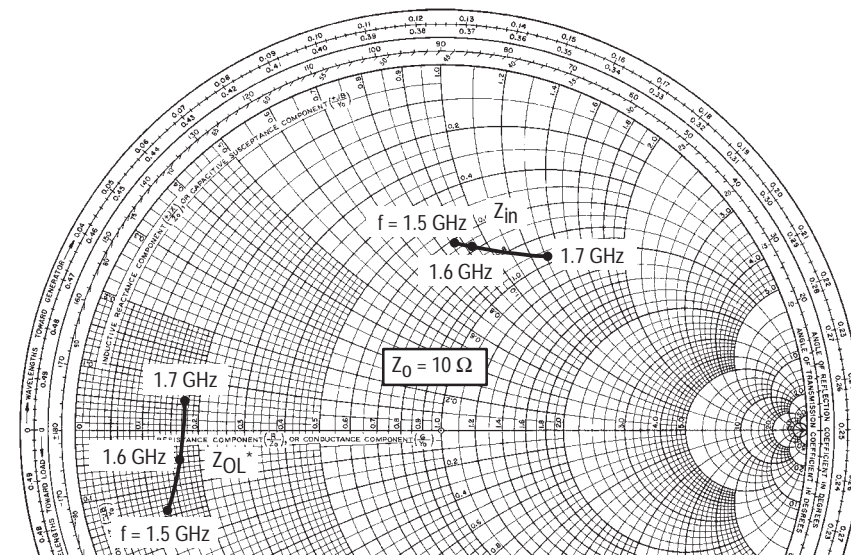
Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Collector–Emitter Breakdown Voltage ($I_C = 40\text{ mA}$, $V_{BE} = 0$)	$V_{(BR)CES}$	55	—	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 40\text{ mA}$, $I_E = 0$)	$V_{(BR)CBO}$	55	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 2.5\text{ mA}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	—	—	Vdc
Collector Cutoff Current ($V_{CE} = 28\text{ Vdc}$, $V_{BE} = 0$)	I_{CES}	—	—	2.5	mA
ON CHARACTERISTICS					
DC Current Gain ($I_{CE} = 0.2\text{ A}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	20	—	80	—
DYNAMIC CHARACTERISTICS					
Output Capacitance ($V_{CB} = 28\text{ Vdc}$, $f = 1.0\text{ MHz}$)	C_{ob}	11	—	—	pf
FUNCTIONAL TESTS					
Common–Base Amplifier Power Gain ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 6\text{ Watts}$, $f = 1600/1640\text{ MHz}$)	G_{pe}	7.4	—	—	dB
Collector Efficiency ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 6\text{ Watts}$, $f = 1600/1640\text{ MHz}$)	η	40	45	—	%
Return Loss ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 6\text{ Watts}$, $f = 1600/1640\text{ MHz}$)	I_{RL}	—	8.0	—	dB
Output Mismatch Stress ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 6\text{ Watts}$, $f = 1600\text{ MHz}$, Load VSWR = 3:1 all phase angles at frequency of test)	ψ	No Degradation in Output Power			



Board Material – Teflon® Glass Laminate Dielectric
 Thickness – 0.30", $\epsilon_r = 2.55$ ", 2.0 oz. Copper

- | | | | |
|--------|------------------------------|--------|--------------------------------------|
| B1 | Fair Rite Bead on #24 Wire | C4 | 47 μ F, 50 V, Electrolytic Cap |
| C1, C5 | 100 pF, B Case, ATC Chip Cap | L1, L2 | 3 Turns, #18, 0.133" ID, 0.15" Long |
| C2 | 0.1 μ F, Dipped Mica Cap | L3 | 9 Turns, #24 Enamel |
| C3 | 0.1 μ F, Chip Cap | R1 | 82 Ω , 1.0 W, Carbon Resistor |

Figure 1. MRF16006 Test Fixture Schematic



$V_{CC} = 28 \text{ Vdc}$, $P_{out} = 6 \text{ W}$

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
1500	6.28 + j 8.53	1.22 - j 1.37
1600	7.04 + j 9.00	1.58 - j 0.53
1700	9.55 + j 12.86	1.71 + j 0.39

Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

Figure 2. Series Equivalent Input/Output Impedance

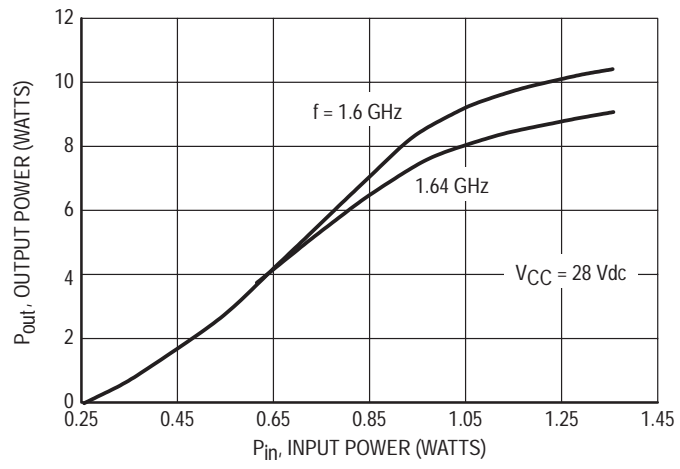


Figure 3. Output Power versus Input Power

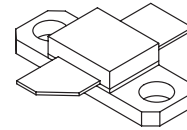
The RF Line
NPN Silicon
RF Power Transistor

Designed for 28 Volt microwave large-signal, common base, Class-C CW amplifier applications in the range 1600 – 1640 MHz.

- Specified 28 Volt, 1.6 GHz Class-C Characteristics
Output Power = 30 Watts
Minimum Gain = 7.5 dB, @ 30 Watts
Minimum Efficiency = 40% @ 30 Watts
- Characterized with Series Equivalent Large-Signal Parameters from 1500 MHz to 1700 MHz
- Silicon Nitride Passivated
- Gold Metallized, Emitter Ballasted for Long Life and Resistance to Metal Migration
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

MRF16030

30 WATTS, 1.6 GHz
RF POWER TRANSISTOR
NPN SILICON



CASE 395C-01, STYLE 2

MAXIMUM RATINGS ($T_J = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CES}	60	Vdc
Emitter-Base Voltage	V_{EBO}	4.0	Vdc
Collector-Current	I_C	4.0	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	103 0.58	Watts $^\circ\text{C}/\text{W}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Thermal Resistance — Junction to Case (1) (2)	$R_{\theta JC}$	1.7	$^\circ\text{C}/\text{W}$
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(1) Thermal measurement performed using CW RF operating condition.

(2) Thermal resistance is determined under specified RF operating conditions by infrared measurement techniques.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

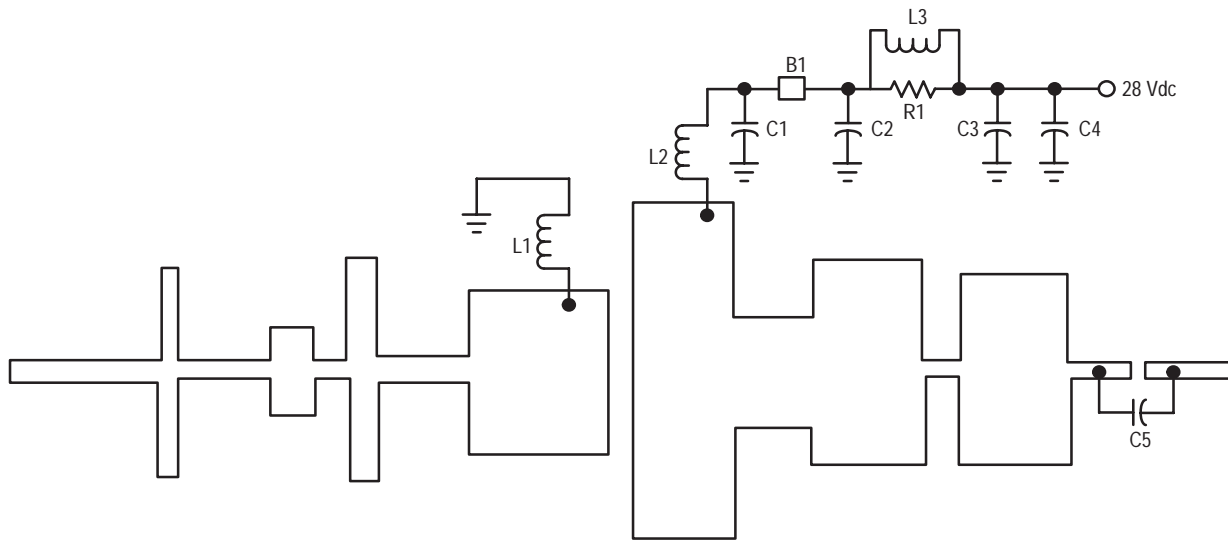
Collector–Emitter Breakdown Voltage ($I_C = 100\text{ mA}_{dc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	55	—	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 100\text{ mA}_{dc}$, $I_E = 0$)	$V_{(BR)CBO}$	55	—	—	Vdc
Emitter–Base Breakdown Voltage ($I_E = 10\text{ mA}_{dc}$, $I_C = 0$)	$V_{(BR)EBO}$	4.0	—	—	Vdc
Collector Cutoff Current ($V_{CE} = 28\text{ Vdc}$, $V_{BE} = 0$)	I_{CES}	—	—	10	mAdc

ON CHARACTERISTICS

DC Current Gain ($I_{CE} = 1.0\text{ Adc}$, $V_{CE} = 5.0\text{ Vdc}$)	h_{FE}	20	35	80	—
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FUNCTIONAL TESTS

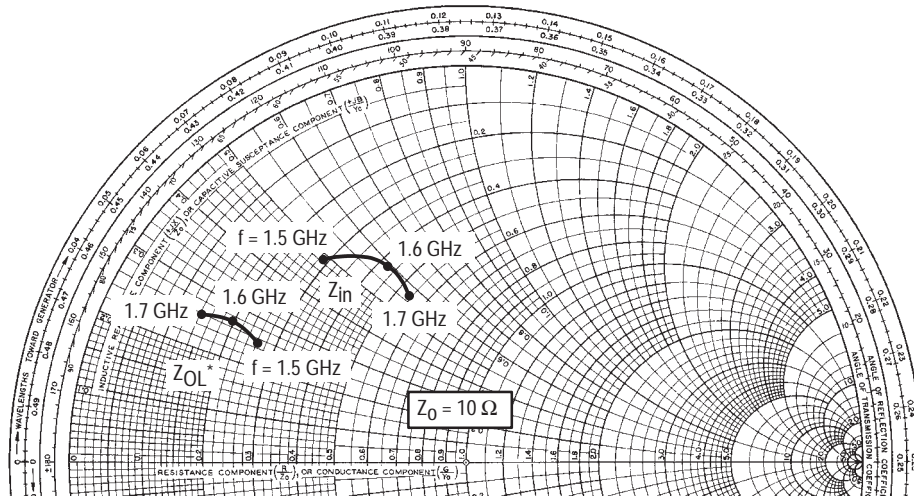
Collector–Base Amplifier Power Gain ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $f = 1600/1640\text{ MHz}$)	G_{pe}	7.5	7.7	—	dB
Collector Efficiency ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $f = 1600/1640\text{ MHz}$)	η	40	45	—	%
Input Return Loss ($V_{CC} = 28\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $f = 1600/1640\text{ MHz}$)	I_{RL}	8.0	—	—	dB
Output Mismatch Stress $V_{CC} = 28\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $f = 1600\text{ MHz}$, Load VSWR = 3:1, All phase angles at frequency of test	Ψ	No Degradation in Output Power			



Board Material – Teflon® Glass Laminate Dielectric
 Thickness = 0.30", $\epsilon_r = 2.55$ ", 2.0 oz. Copper

- | | | | |
|--------|------------------------------|--------|-------------------------------------|
| B1 | Fair Rite Bead on #24 Wire | C4 | 47 μ F, 50 V, Electrolytic |
| C1, C5 | 100 pF, B Case, ATC Chip Cap | L1, L2 | 3 Turns, #18, 0.133" ID, 0.15" Long |
| C2 | 0.1 μ F, Dipped Mica Cap | L3 | 9 Turns, #24 Enamel |
| C3 | 0.1 μ F, Chip Cap | R1 | 82 Ω , 1.0 W, Carbon |

Figure 1. MRF16030 Test Fixture Schematic



$V_{CC} = 28 \text{ Vdc}$, $P_{out} = 30 \text{ W}$

f MHz	Z_{in} Ohms	Z_{OL}^* Ohms
1500	3.05 + j 4.88	2.66 + j 2.53
1600	4.32 + j 6.00	1.79 + j 2.80
1700	5.62 + j 5.79	1.51 + j 2.64

Z_{OL}^* = Conjugate of the optimum load impedance into which the device output operates at a given output power, voltage and frequency.

Figure 2. Series Equivalent Input/Output Impedance

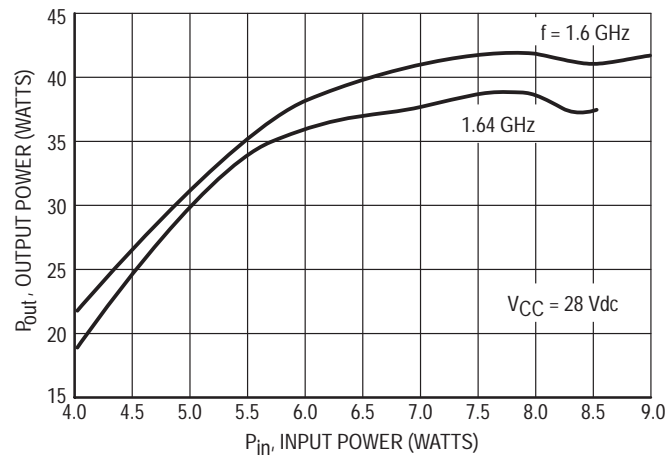


Figure 3. Output Power versus Input Power

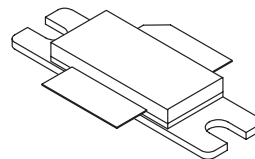
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for PCN and PCS base station applications from frequencies up to 1.8 to 2.0 GHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications. To be used in class AB for PCN-PCS/cellular radio and WLL applications. Specified for GSM1805 – 1880 MHz.

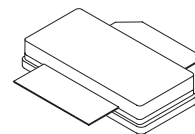
- Typical GSM Performance, Full Frequency Band (1805 – 1880 MHz)
Power Gain — 13 dB (Typ) @ 60 Watts
Efficiency — 45% (Typ) @ 60 Watts
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 60 Watts (CW) Output Power
- Excellent Thermal Stability

MRF18060A
MRF18060AS

60 W, 1.80 – 1.88 GHz, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465-04, STYLE 1
(MRF18060A)



CASE 465A-04, STYLE 1
(MRF18060AS)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C \geq 25^\circ\text{C}$ Derate above 25°C	P_D	180 1.03	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.97	$^\circ\text{C}/\text{W}$

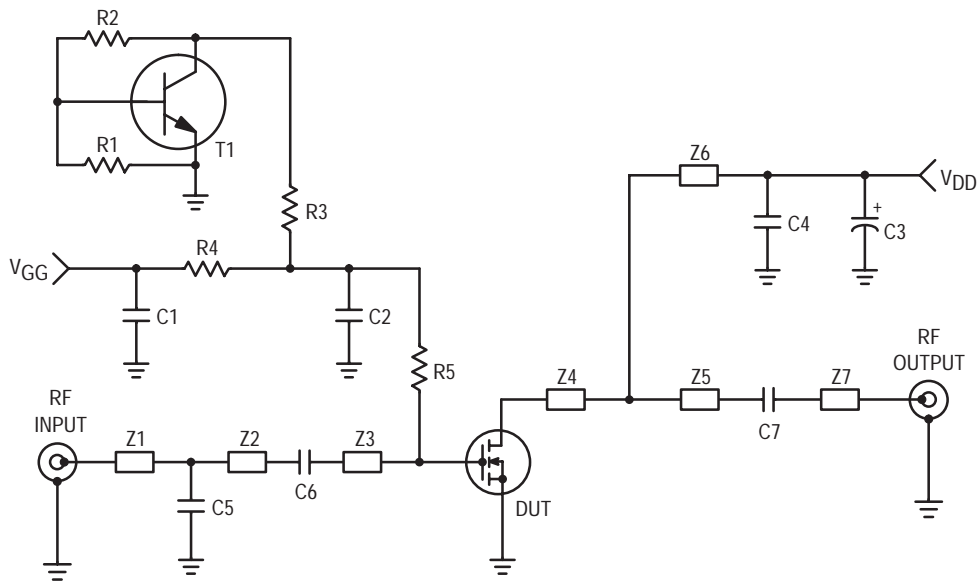
NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 10\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	6	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 500\ \text{mAdc}$)	$V_{GS(Q)}$	2.5	3.9	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\ \text{Adc}$)	$V_{DS(on)}$	—	0.27	—	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\ \text{Adc}$)	g_{fs}	—	4.7	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance (Including Input Matching Capacitor in Package) (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{iss}	—	160	—	pF
Output Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{oss}	—	740	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{rss}	—	2.7	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain @ 60 W (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 500\ \text{mA}$, $f = 1805 - 1880\ \text{MHz}$)	G_{ps}	11.5	13	—	dB
Drain Efficiency @ 60 W (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 500\ \text{mA}$, $f = 1805 - 1880\ \text{MHz}$)	η	43	45	—	%
Input Return Loss (2) ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\ \text{W CW}$, $I_{DQ} = 500\ \text{mA}$, $f = 1805 - 1880\ \text{MHz}$)	IRL	10	—	—	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\ \text{W CW}$, $I_{DQ} = 500\ \text{mA}$ VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.

(2) To meet application requirements, Motorola test fixtures have been designed to cover the full GSM1800 band, ensuring batch–to–batch consistency.



C1	100 nF, Chip Capacitor 1203	R1, R3	2.2 k Ω , Chip Resistor 0805
C2, C4, C7	10 pF, Chip Capacitor	R2, R4	2.7 k Ω , Chip Resistor 0805
C3	10 μ F, 35 V Electrolytic Tantalum Capacitor	R5	1.1 k Ω , Chip Resistor 0805
C5	1.2 pF, Chip Capacitor	T1	BC847 Transistor SOT-23
C6	1.0 pF, Chip Capacitor	Z1 to Z7	Microstrip Transmission Lines

Figure 1. 1805 – 1880 MHz Test Fixture Schematic

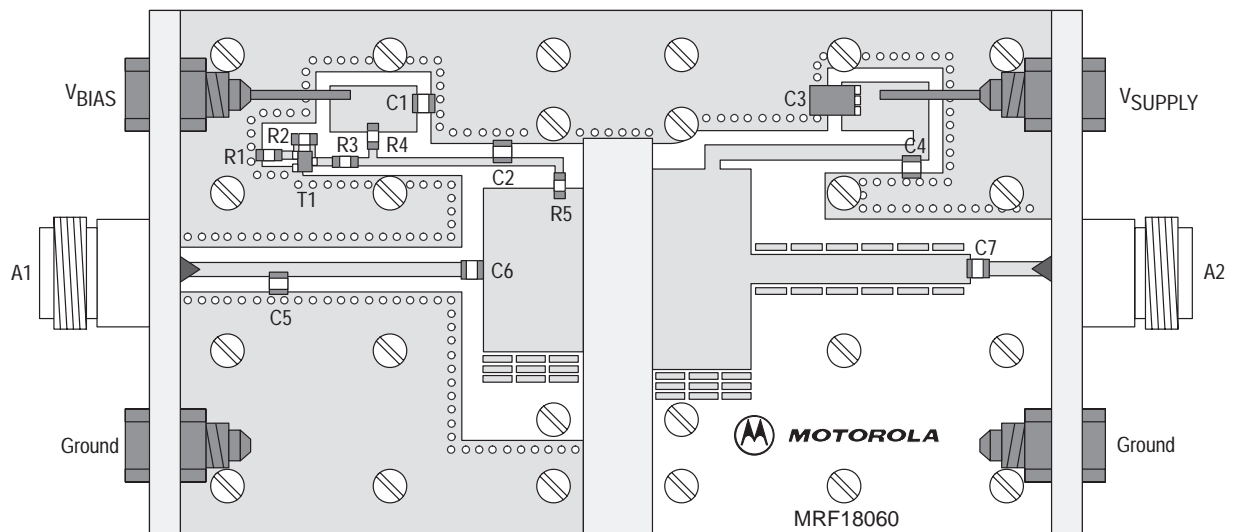
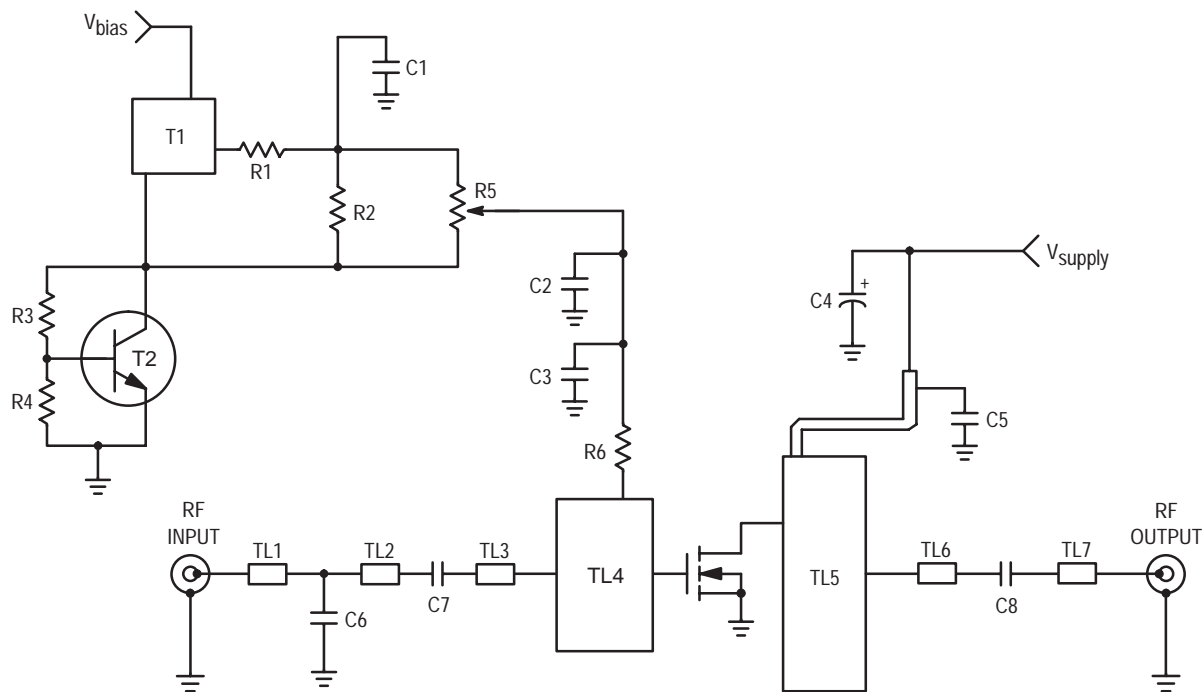


Figure 2. 1805 – 1880 MHz Test Fixture Component Layout



C1	1 μ F, Chip Capacitor 0805	R1	10 Ω , Chip Resistor 0805
C2	100 nF, Chip Capacitor 0805	R2, R6	1 k Ω , Chip Resistor 0805
C3, C5, C8	10 pF, ACCU-P Chip Capacitor 0805	R3	1.2 k Ω , Chip Resistor 0805
C4	10 μ F, 35 V Tantalum Electrolytic Capacitor	R4	2.2 k Ω , Chip Resistor 0805
C6	1.8 pF, ACCU-P Chip Capacitor 0805	R5	5 k Ω , SMD Potentiometer
C7	1 pF, ACCU-P Chip Capacitor 0805	T1	LP2951 Micro-8 Voltage Regulator
		T2	BC847 SOT-23 NPN Transistor
		Substrate = 0.5 mm Teflon [®] Glass, $\epsilon_r = 2.55$	

Figure 3. 1800 – 2000 MHz Demo Board Schematic

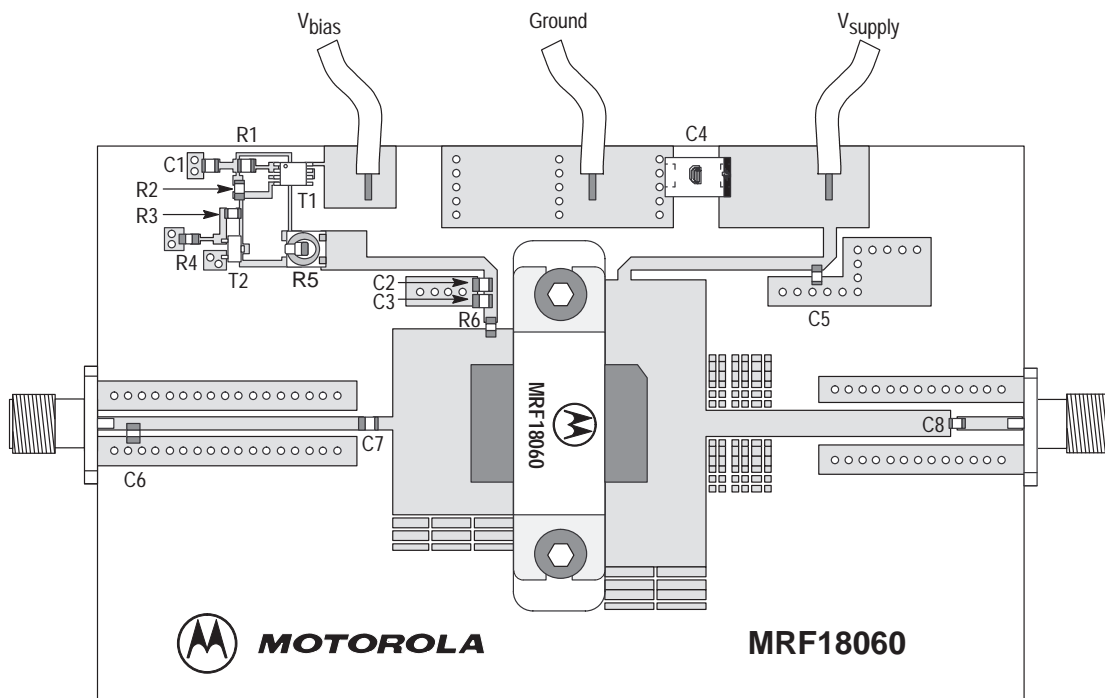


Figure 4. 1800 – 2000 MHz Demo Board Component Layout

$V_{DD} = 26 \text{ V}$, $I_{DQ} = 500 \text{ mA}$, $P_{out} = 60 \text{ Watts (CW)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1700	$0.60 + j2.53$	$2.27 + j3.44$
1800	$0.80 + j3.20$	$2.05 + j3.05$
1900	$0.92 + j3.42$	$1.90 + j2.90$
2000	$1.07 + j3.59$	$1.64 + j2.88$
2100	$1.31 + j4.00$	$1.29 + j2.99$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load at a given voltage, P1dB, gain, efficiency, bias current and frequency.

Table 1. Series Equivalent Input and Output Impedance

TYPICAL CHARACTERISTICS (DATA TAKEN USING WIDEBAND DEMONSTRATION BOARD)

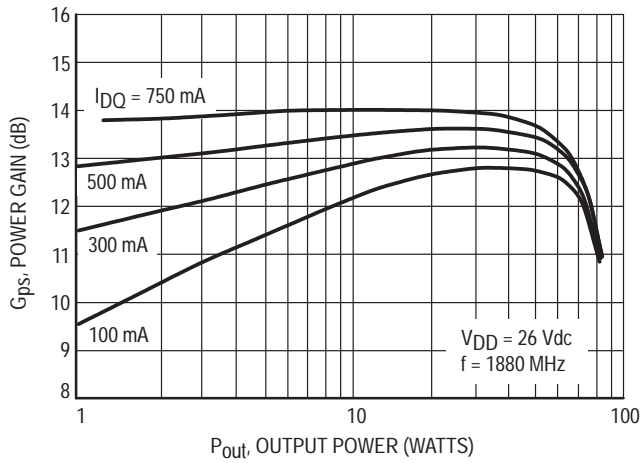


Figure 5. Power Gain versus Output Power

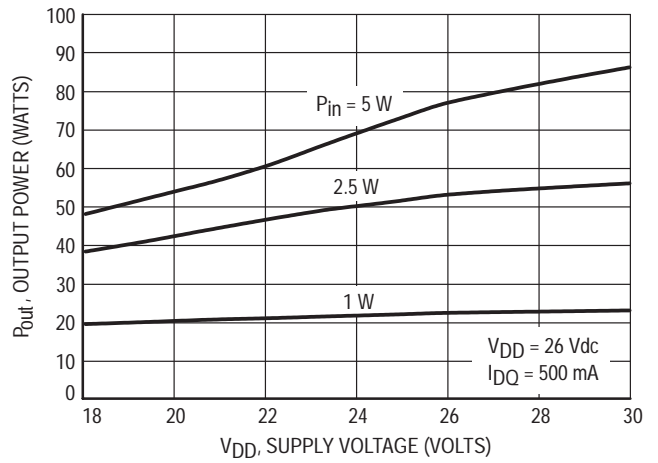


Figure 6. Output Power versus Supply Voltage

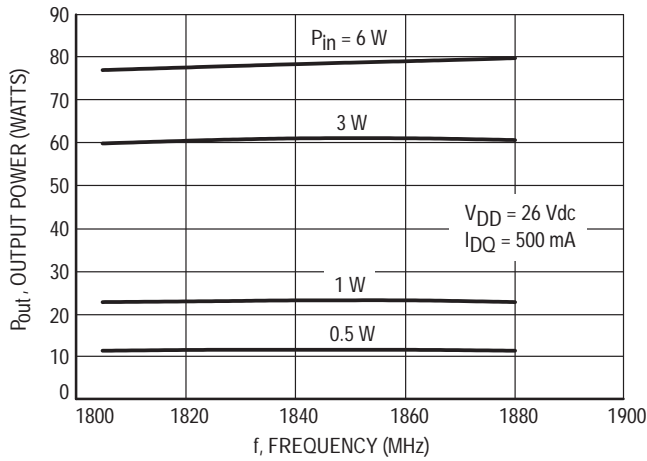


Figure 7. Output Power versus Frequency

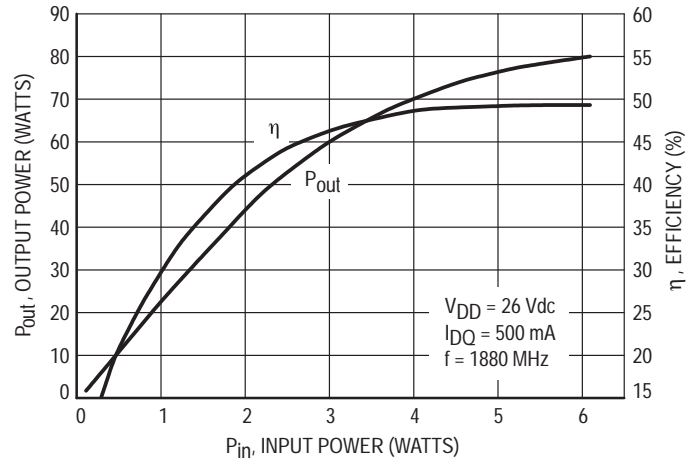


Figure 8. Output Power and Efficiency versus Input Power

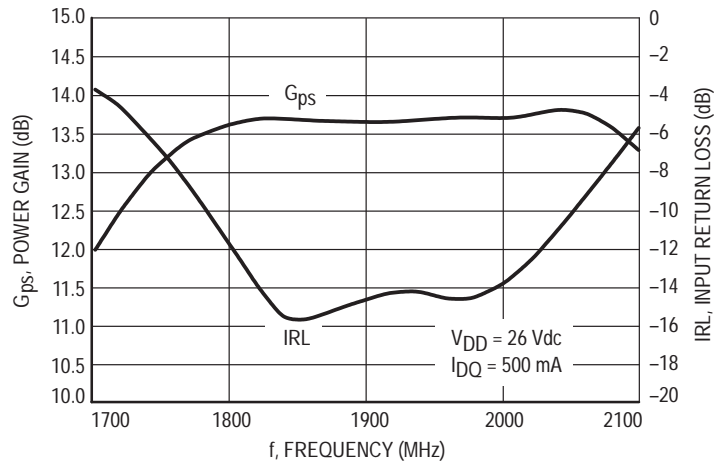


Figure 9. Wideband Gain and IRL (at Small Signal)

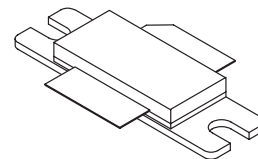
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for PCN and PCS base station applications from frequencies up to 1.8 to 2.0 GHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications. To be used in class AB for PCN-PCS/cellular radio and WLL applications. Specified for GSM1930 – 1990 MHz.

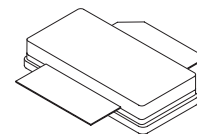
- GSM Performance, Full Frequency Band (1930 – 1990 MHz)
Power Gain — 13 dB (Typ) @ 60 Watts (CW)
Efficiency — 45% (Typ) @ 60 Watts (CW)
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 60 Watts (CW) Output Power
- Excellent Thermal Stability

MRF18060B
MRF18060BS

60 W, 1.90 – 1.99 GHz, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465-04, STYLE 1
(MRF18060B)



CASE 465A-04, STYLE 1
(MRF18060BS)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C > = 25^\circ\text{C}$ Derate above 25°C	P_D	180 1.03	Watts W/°C
Storage Temperature Range	T_{stg}	-65 to +150	°C
Operating Junction Temperature	T_J	200	°C

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.97	°C/W

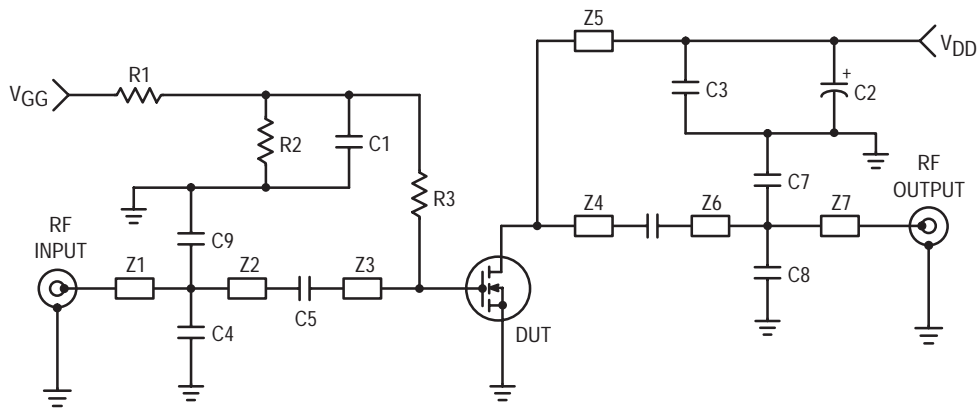
NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 10\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	6	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 500\ \text{mAdc}$)	$V_{GS(Q)}$	2.5	3.9	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\ \text{Adc}$)	$V_{DS(on)}$	—	0.27	—	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\ \text{Adc}$)	g_{fs}	—	4.7	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance (Including Input Matching Capacitor in Package) (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{iss}	—	160	—	pF
Output Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{oss}	—	740	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\ \text{MHz}$)	C_{rss}	—	2.7	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain @ 60 W (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 500\ \text{mA}$, $f = 1930 - 1990\ \text{MHz}$)	G_{ps}	11.5	13	—	dB
Drain Efficiency @ 60 W (2) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 500\ \text{mA}$, $f = 1930 - 1990\ \text{MHz}$)	η	40	45	—	%
Input Return Loss (2) ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\ \text{W CW}$, $I_{DQ} = 500\ \text{mA}$, $f = 1930 - 1990\ \text{MHz}$)	IRL	10	—	—	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\ \text{W CW}$, $I_{DQ} = 500\ \text{mA}$ VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.

(2) To meet application requirements, Motorola test fixtures have been designed to cover the full GSM1900 band, ensuring batch–to–batch consistency.



C1, C3	10 pF, 100B Chip Capacitor	C7, C9	0.3 pF, 100B Chip Capacitor
C2	10 μ F, 35 V Electrolytic Tantalum Capacitor	R1, R2	10 k Ω , Chip Resistor 0805
C4, C8	1.2 pF, 100B Chip Capacitor	R3	1.0 k Ω , Chip Resistor 0805
C5	1.0 pF, 100B Chip Capacitor	PCB	Teflon [®] Glass
C6	2.2 pF, 100B Chip Capacitor		

Figure 1. 1930 – 1990 MHz Test Fixture Schematic

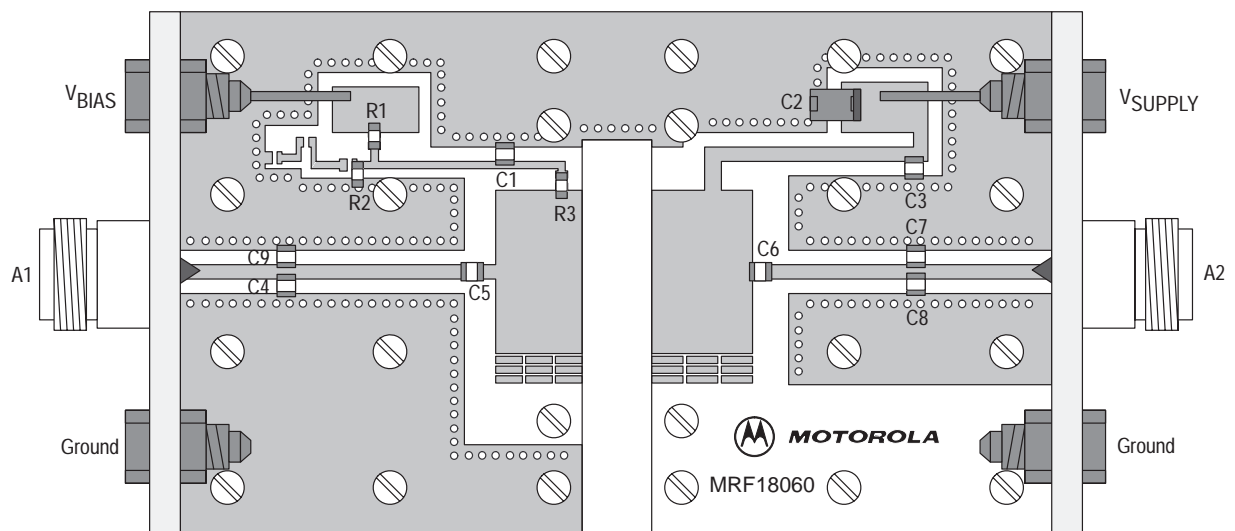
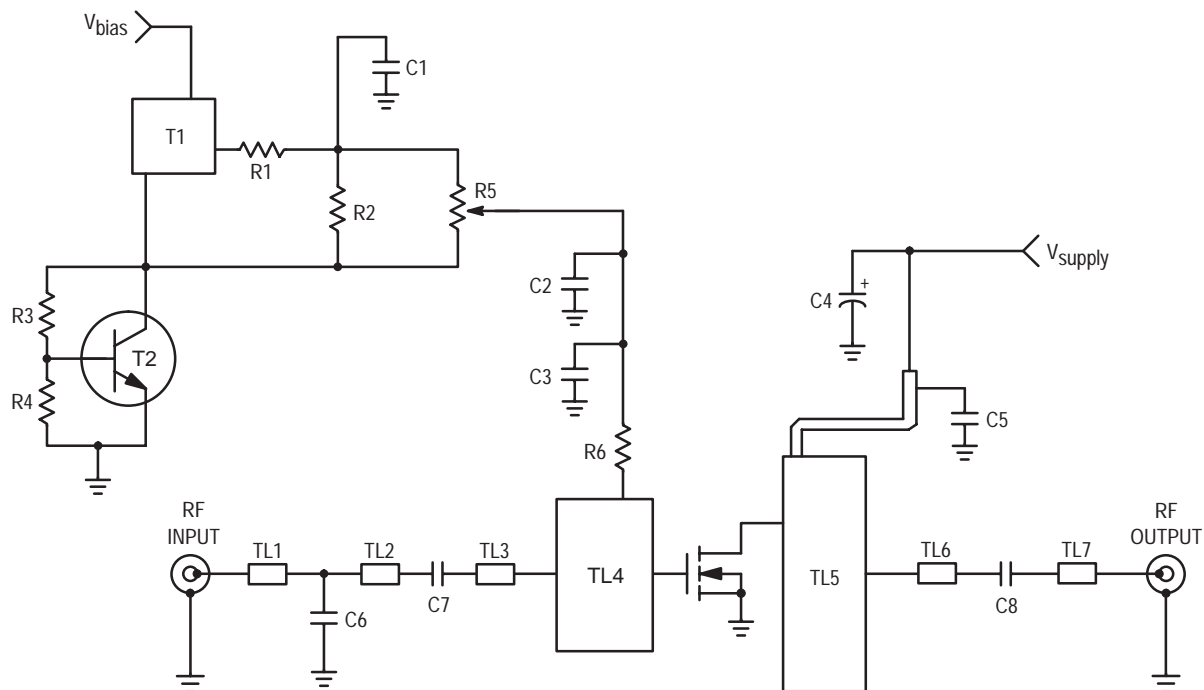


Figure 2. 1930 – 1990 MHz Test Fixture Component Layout



- | | | | |
|------------|--|--------|-------------------------------------|
| C1 | 1 μ F, Chip Capacitor 0805 | R1 | 10 Ω , Chip Resistor 0805 |
| C2 | 100 nF, Chip Capacitor 0805 | R2, R6 | 1 k Ω , Chip Resistor 0805 |
| C3, C5, C8 | 10 pF, ACCU-P Chip Capacitor 0805 | R3 | 1.2 k Ω , Chip Resistor 0805 |
| C4 | 10 μ F, 35 V Tantalum Electrolytic Capacitor | R4 | 2.2 k Ω , Chip Resistor 0805 |
| C6 | 1.8 pF, ACCU-P Chip Capacitor 0805 | R5 | 5 k Ω , SMD Potentiometer |
| C7 | 1 pF, ACCU-P Chip Capacitor 0805 | T1 | LP2951 Micro-8 Voltage Regulator |
| | | T2 | BC847 SOT-23 NPN Transistor |
- Substrate = 0.5 mm Teflon[®] Glass, $\epsilon_r = 2.55$

Figure 3. 1800 – 2000 MHz Demo Board Schematic

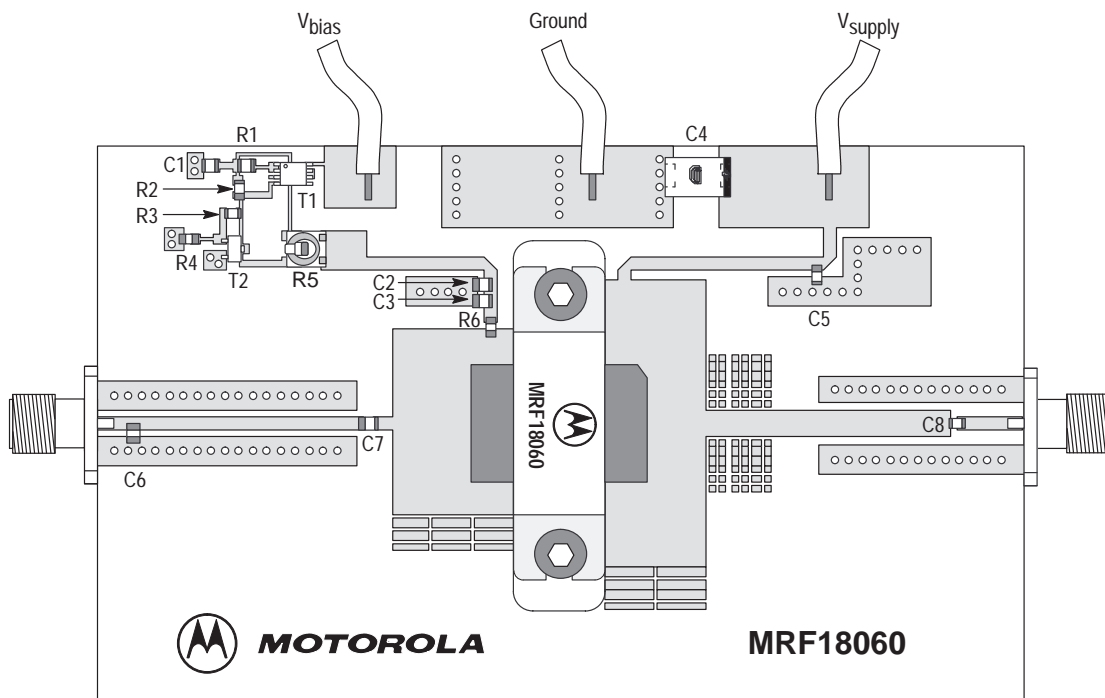


Figure 4. 1800 – 2000 MHz Demo Board Component Layout

TYPICAL CHARACTERISTICS (DATA TAKEN USING WIDEBAND DEMONSTRATION BOARD)

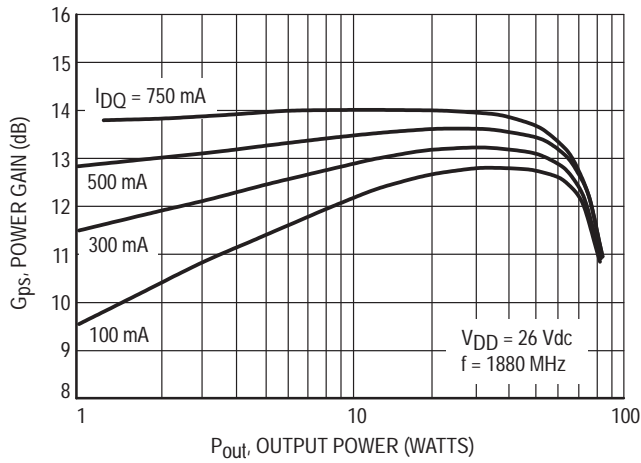


Figure 5. Power Gain versus Output Power

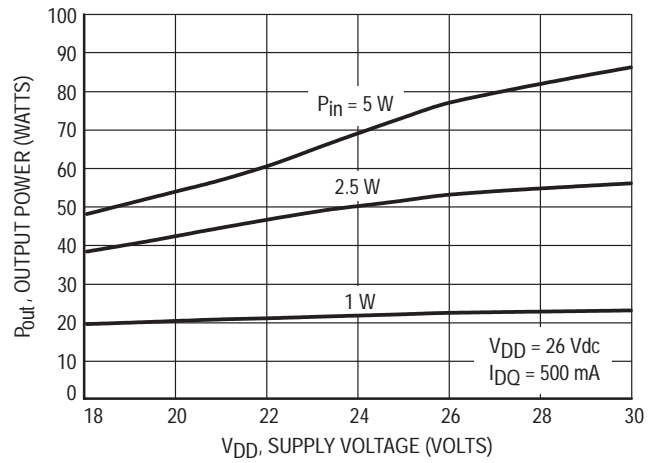


Figure 6. Output Power versus Supply Voltage

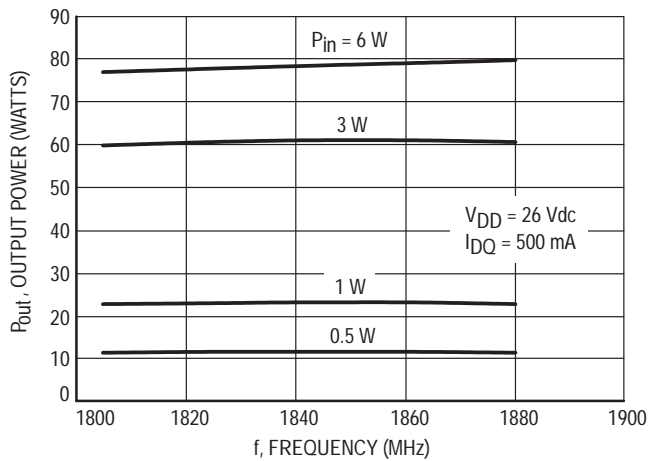


Figure 7. Output Power versus Frequency

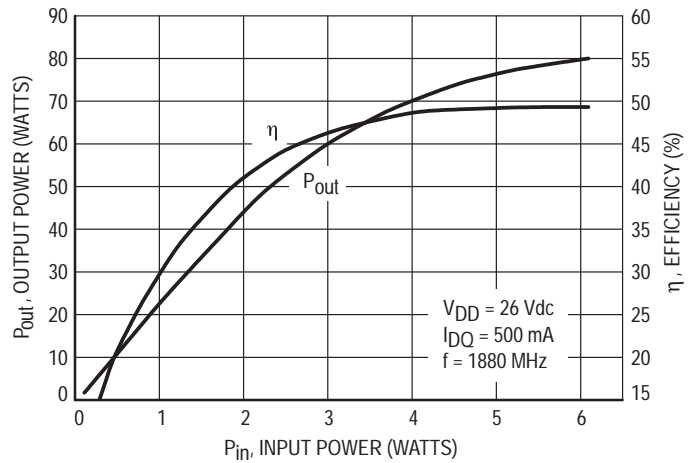


Figure 8. Output Power and Efficiency versus Input Power

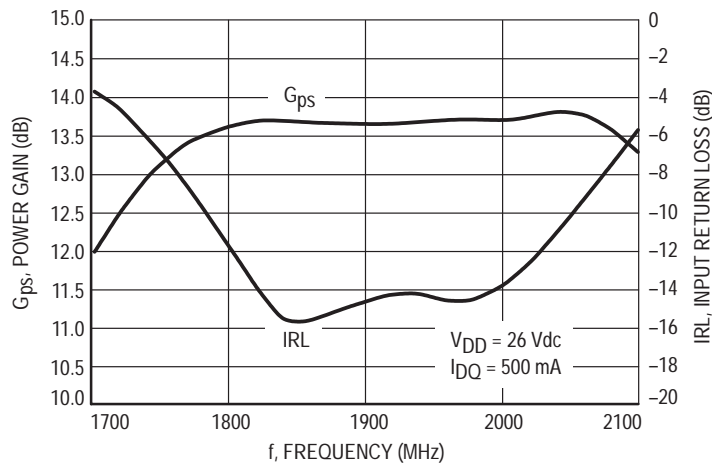


Figure 9. Wideband Gain and IRL (at Small Signal)

$V_{DD} = 26\text{ V}$, $I_{DQ} = 500\text{ mA}$, $P_{out} = 60\text{ Watts (CW)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1700	$0.60 + j2.53$	$2.27 + j3.44$
1800	$0.80 + j3.20$	$2.05 + j3.05$
1900	$0.92 + j3.42$	$1.90 + j2.90$
2000	$1.07 + j3.59$	$1.64 + j2.88$
2100	$1.31 + j4.00$	$1.29 + j2.99$

Z_{in} = Complex conjugate of source impedance.
 Z_{OL}^* = Complex conjugate of the optimum load at a given voltage, P1dB, gain, efficiency, bias current and frequency.

Table 1. Series Equivalent Input and Output Impedance

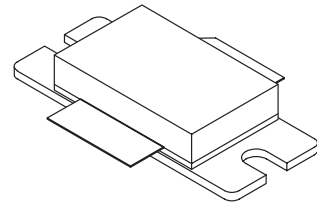
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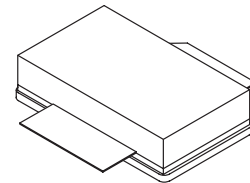
- GSM and EDGE Performances, Full Frequency Band
Power Gain — 13.5 dB (Typ) @ 90 Watts (CW)
Efficiency — 52% (Typ) @ 90 Watts (CW)
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 90 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF18090A
MRF18090AS

1.80 – 1.88 GHz, 90 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETS



CASE 465B-02, STYLE 1
(MRF18090A)



CASE 465C-01, STYLE 1
(MRF18090AS)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	250 1.43	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.7	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 750\text{ mA}$)	$V_{GS(Q)}$	2.5	3.7	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.1	—	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$)	g_{fs}	—	7.2	—	S
DYNAMIC CHARACTERISTICS					
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	4.2	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain @ 90 W (1) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 750\text{ mA}$, $f = 1805 - 1880\text{ MHz}$)	G_{ps}	12.0	13.5	—	dB
Drain Efficiency @ 90 W (1) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 750\text{ mA}$, $f = 1805 - 1880\text{ MHz}$)	η	47	52	—	%
Input Return Loss (1) ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 750\text{ mA}$, $f = 1805 - 1880\text{ MHz}$)	IRL	10	—	—	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 750\text{ mA}$ VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) To meet application requirements, Motorola test fixtures have been designed to cover the full GSM1800 band, ensuring batch–to–batch consistency.

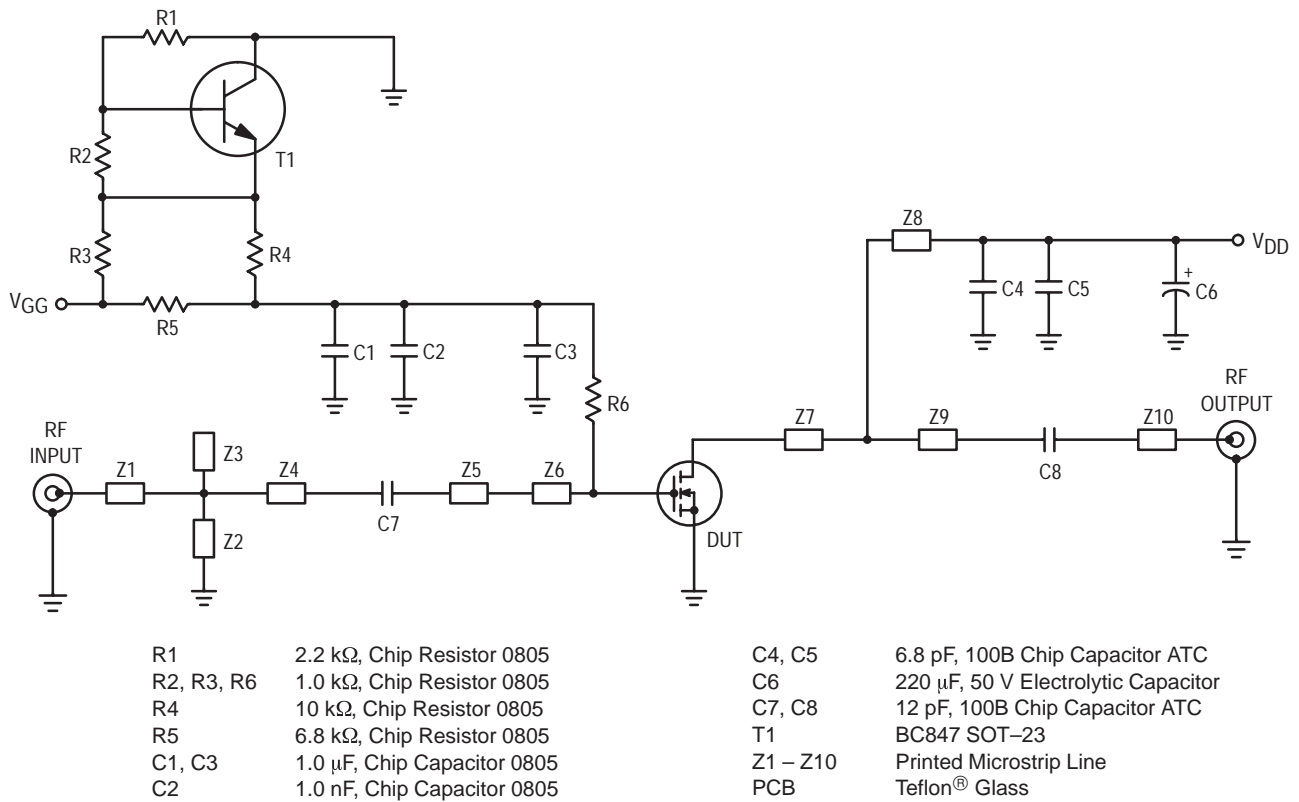


Figure 1. 1.80 – 1.88 GHz Test Fixture Schematic

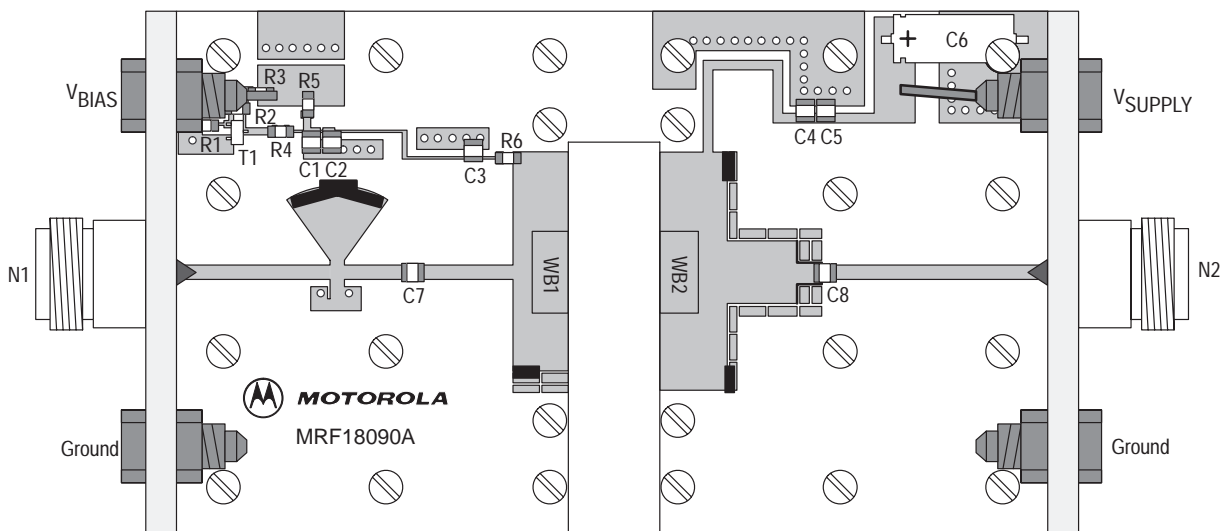
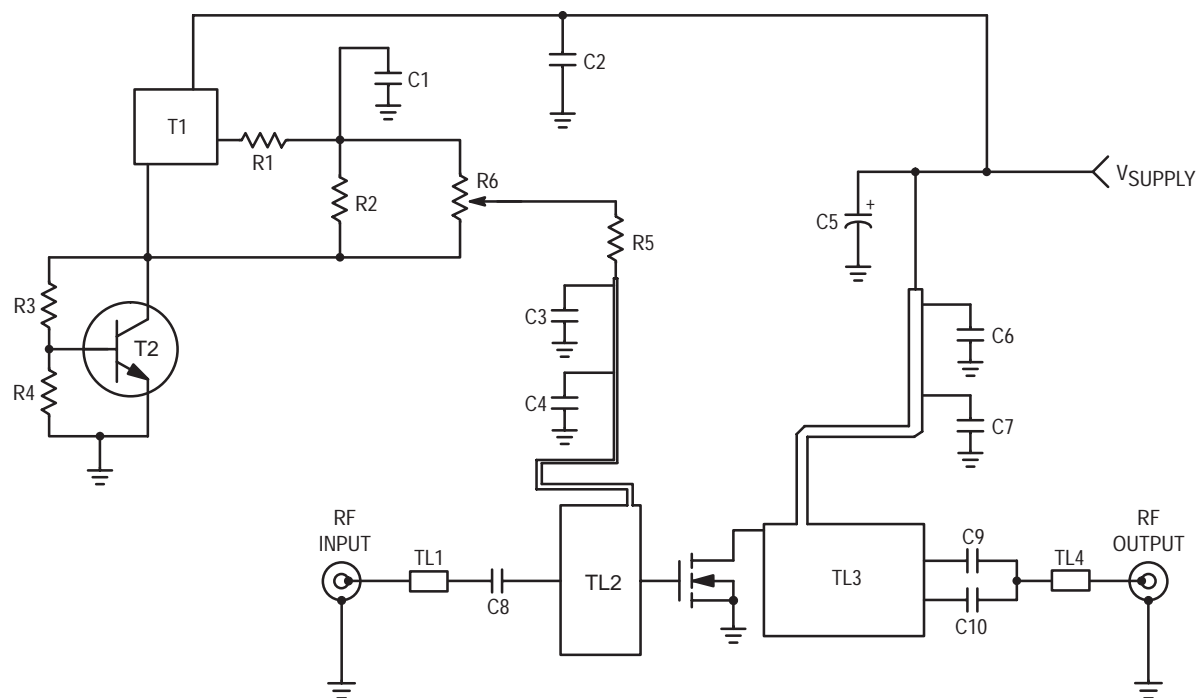


Figure 2. 1.80 – 1.88 GHz Test Fixture Component Layout



C1, C3	1 μ F, Chip Capacitor 0805	R1	10 Ω , Chip Resistor 0805
C2	0.1 μ F, Chip Capacitor 0805	R2, R3	1 k Ω , Chip Resistor 0805
C4	1 nF, Chip Capacitor 0805	R4	2.2 k Ω , Chip Resistor 0805
C5	220 μ F, 50 V Electrolytic Capacitor	R5	10 k Ω , Chip Resistor 0603
C6, C7	8.2 pF, 100A Chip Capacitor	R6	5 k Ω , SMD Potentiometer
C8, C9, C10	22 pF, 100A Chip Capacitor	T1	LP2951 Micro-8 Voltage Regulator
		T2	BC847 SOT-23 NPN Transistor
		TL1 - TL4	Printed Transmission Lines
			Substrate = 0.5 mm Teflon [®] Glass

Figure 3. 1.80 – 1.88 GHz Demo Board Schematic

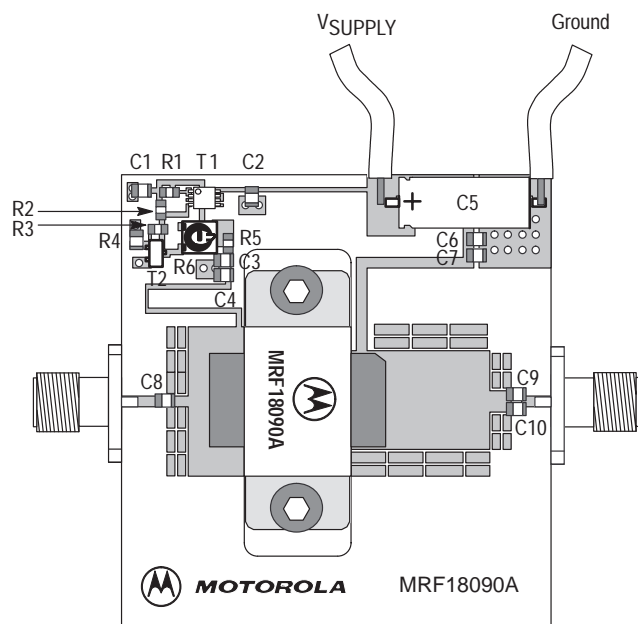


Figure 4. 1.80 – 1.88 GHz Demo Board Component Layout

TYPICAL CHARACTERISTICS

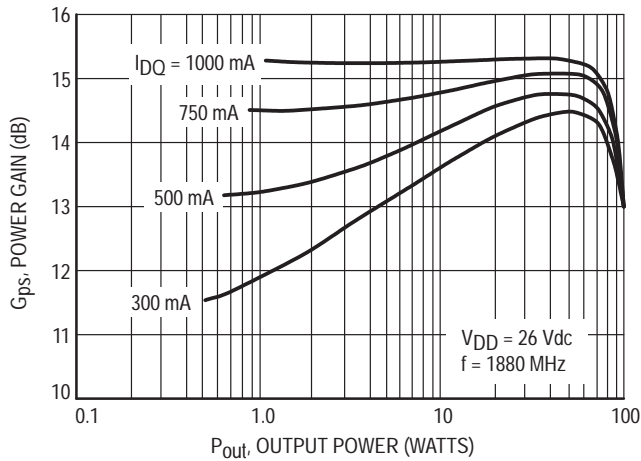


Figure 5. Power Gain versus Output Power

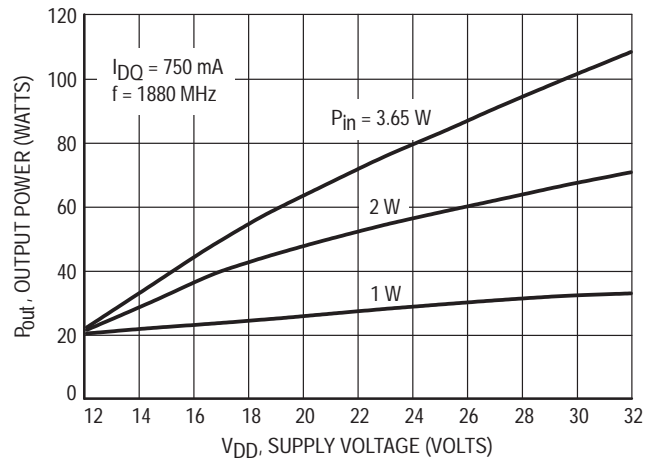


Figure 6. Output Power versus Supply Voltage

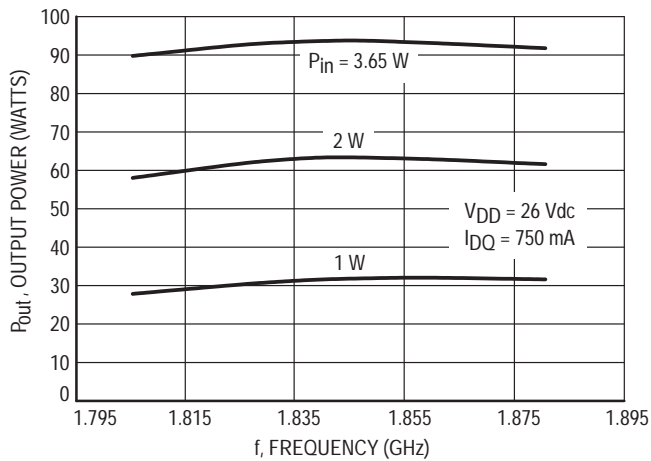


Figure 7. Output Power versus Frequency

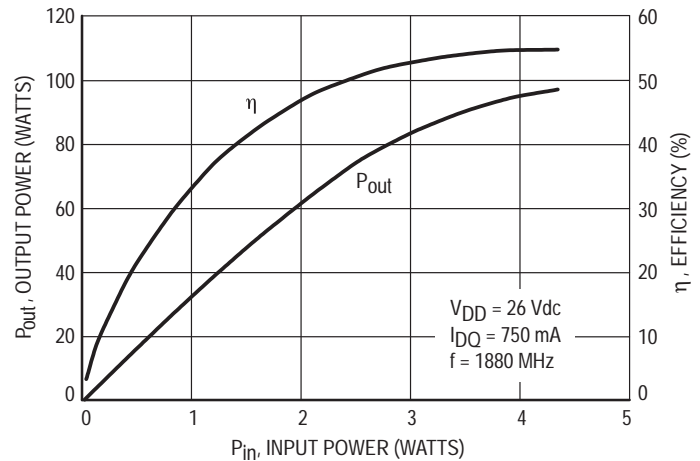


Figure 8. Output Power and Efficiency versus Input Power

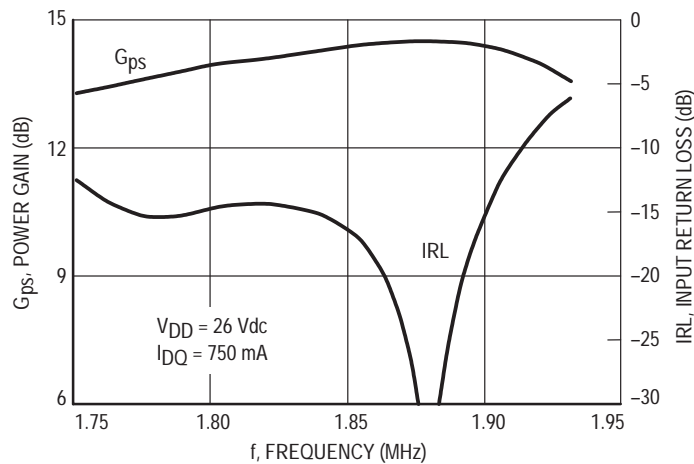


Figure 9. Wideband Gain and IRL (at Small Signal)

$V_{DD} = 26 \text{ V}$, $I_{DQ} = 750 \text{ mA}$, $P_{out} = 90 \text{ Watts (CW)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1805	$1.1 + j5.85$	$1.15 + j2.16$
1880	$1.56 + j6.75$	$1.13 + j2.6$
1930	$2.05 + j8.0$	$1.30 + j2.23$
1990	$2.3 + j7.3$	$0.82 + j2.90$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load
at a given voltage, P1dB, gain, efficiency,
bias current and frequency.

Table 1. Large Signal Input and Output Impedance

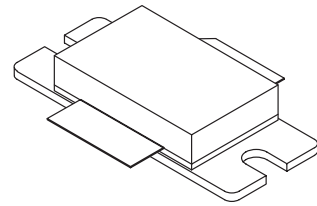
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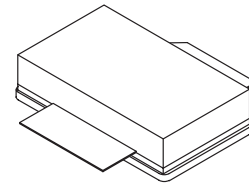
- GSM and EDGE Performances, Full Frequency Band
Power Gain — 13.5 dB (Typ) @ 90 Watts (CW)
Efficiency — 45% (Typ) @ 90 Watts (CW)
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 90 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF18090B
MRF18090BS

1.90 – 1.99 GHz, 90 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETS



CASE 465B-02, STYLE 1
(MRF18090B)



CASE 465C-01, STYLE 1
(MRF18090BS)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	250 1.43	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

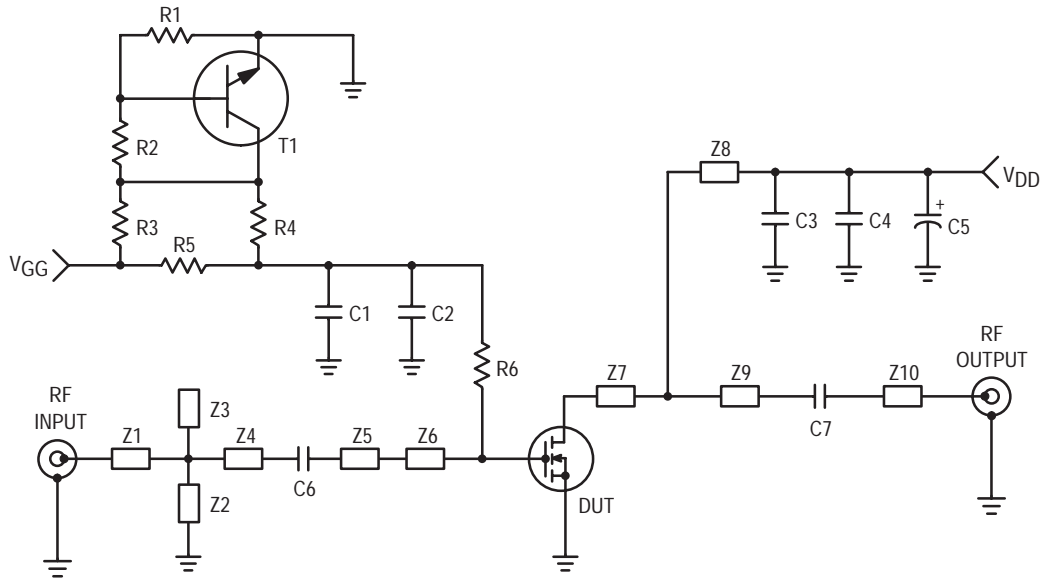
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.7	$^\circ\text{C/W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μA
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μA
ON CHARACTERISTICS					
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 750\text{ mA}$)	$V_{GS(Q)}$	2.5	3.7	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ A}$)	$V_{DS(on)}$	—	0.1	—	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 3\text{ A}$)	g_{fs}	—	7.2	—	S
DYNAMIC CHARACTERISTICS					
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	4.2	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain @ 90 W (1) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 750\text{ mA}$, $f = 1930 - 1990\text{ MHz}$)	G_{ps}	12	13.5	—	dB
Drain Efficiency @ 90 W (1) ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 750\text{ mA}$, $f = 1930 - 1990\text{ MHz}$)	η	40	45	—	%
Input Return Loss (1) ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 750\text{ mA}$, $f = 1930 - 1990\text{ MHz}$)	IRL	10	—	—	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 750\text{ mA}$ VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) To meet application requirements, Motorola test fixtures have been designed to cover the full GSM1900 band, ensuring batch–to–batch consistency.



C1	1.0 μ F, Chip Capacitor 0805	R2, R3, R6	1.0 k Ω , Chip Resistor 0805
C2	1.0 nF, Chip Resistor 0805	R4	10 k Ω , Chip Resistor 0805
C3, C4	6.8 pF, 100B Chip Capacitor	R5	6.8 k Ω , Chip Resistor 0805
C5	220 μ F, 50 V Electrolytic Capacitor	T1	BC847 SOT-23
C6, C7	12 pF, 100B Chip Capacitor	Z1 - Z10	Printed Microstrip Line
R1	2.2 k Ω , Chip Resistor 0805	PCB	Teflon [®] Glass

Figure 1. 1.93 - 1.99 MHz Test Fixture Schematic

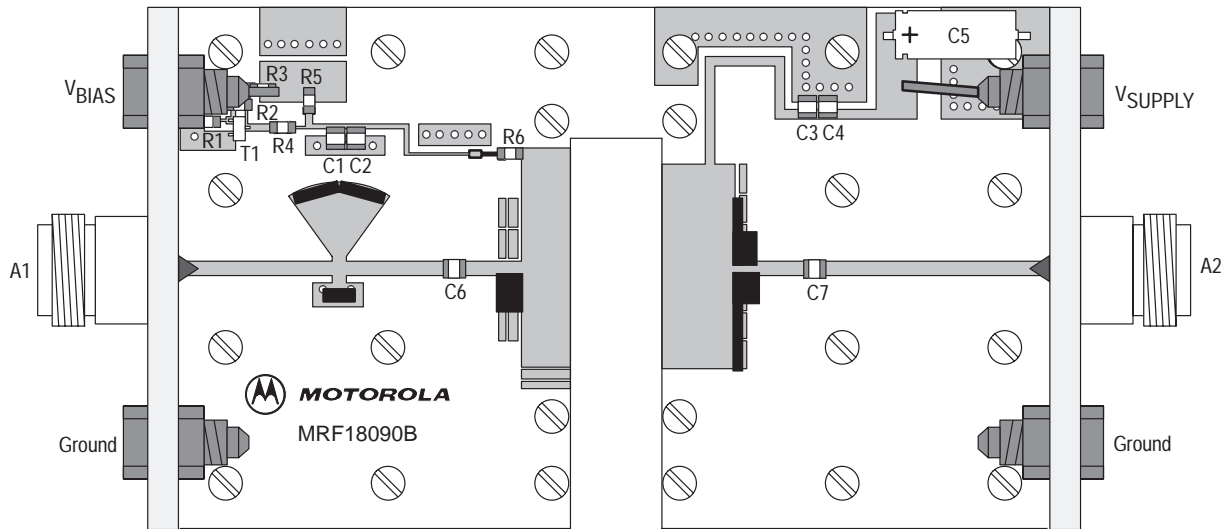
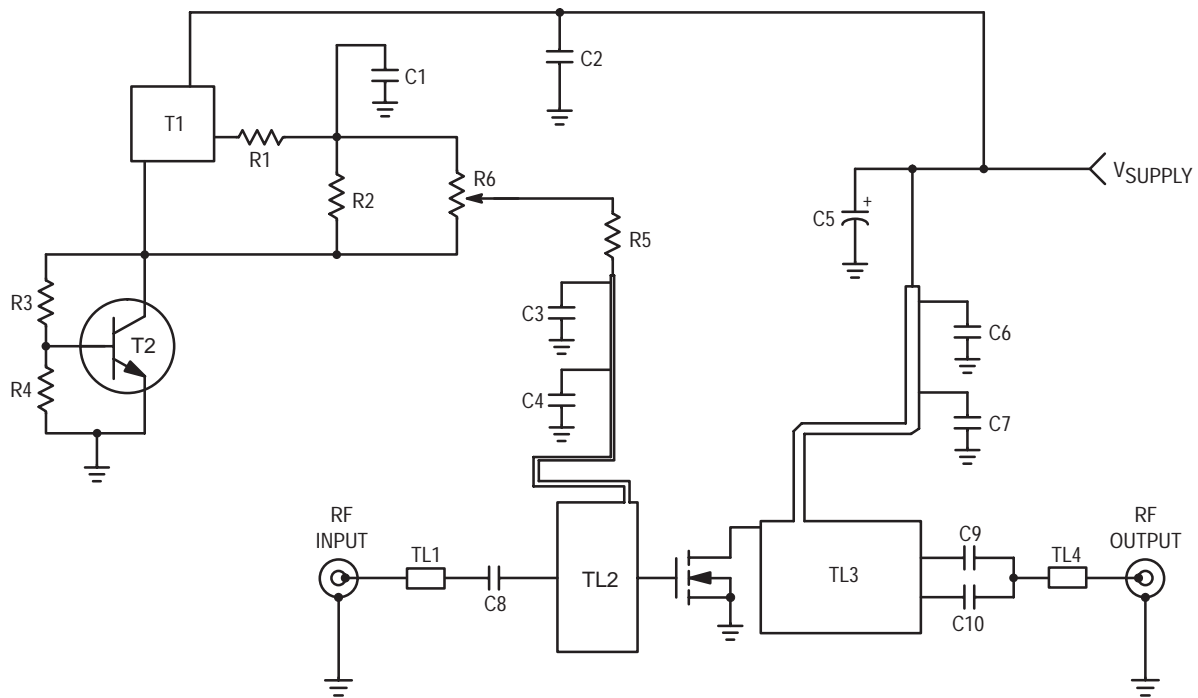


Figure 2. 1.93 - 1.99 GHz Test Fixture Component Layout



C1, C3	1 μ F, Chip Capacitor 0805	R1	10 Ω , Chip Resistor 0805
C2	0.1 μ F, Chip Capacitor 0805	R2, R3	1 k Ω , Chip Resistor 0805
C4	1 nF, Chip Capacitor 0805	R4	2.2 k Ω , Chip Resistor 0805
C5	220 μ F, 50 V Electrolytic Capacitor	R5	10 k Ω , Chip Resistor 0603
C6, C7	8.2 pF, 100A Chip Capacitor	R6	5 k Ω , SMD Potentiometer
C8, C9, C10	22 pF, 100A Chip Capacitor	T1	LP2951 Micro-8 Voltage Regulator
		T2	BC847 SOT-23 NPN Transistor
		TL1 – TL4	Printed Transmission Lines
			Substrate = 0.5 mm Teflon [®] Glass

Figure 3. 1.93 – 1.99 GHz Demo Board Schematic

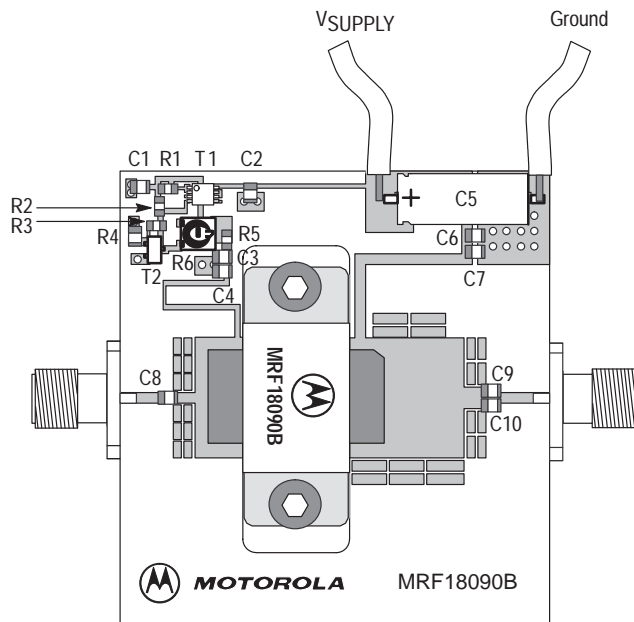


Figure 4. 1.93 – 1.99 GHz Demo Board Component Layout

TYPICAL CHARACTERISTICS

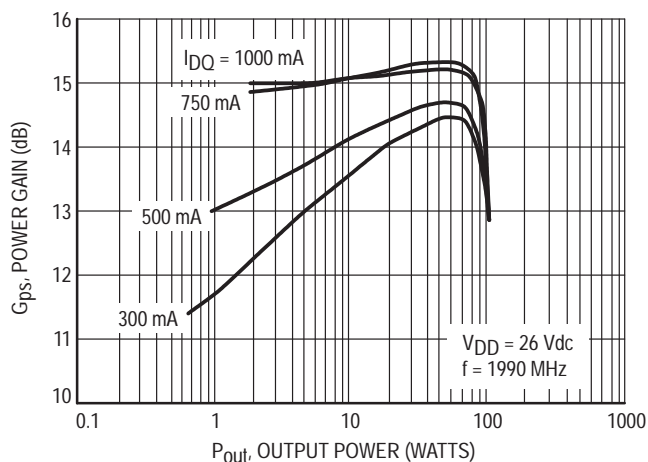


Figure 5. Power Gain versus Output Power

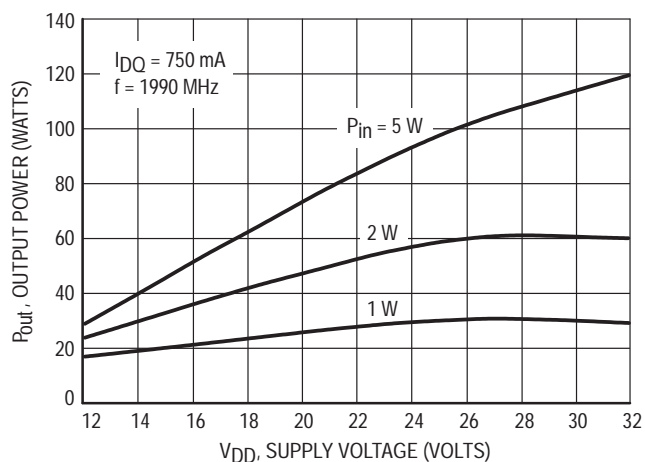


Figure 6. Output Power versus Supply Voltage

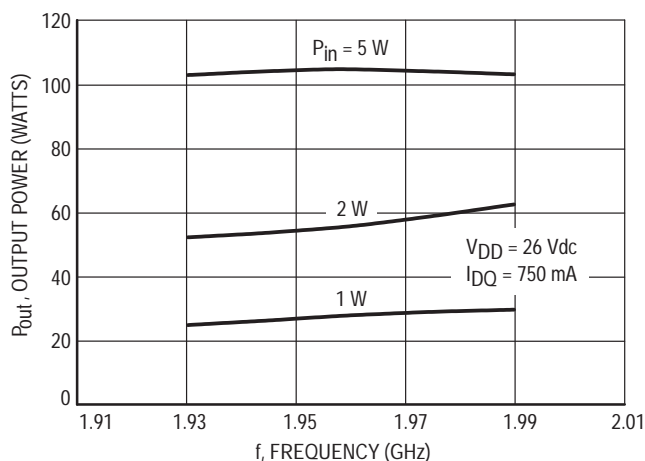


Figure 7. Output Power versus Frequency

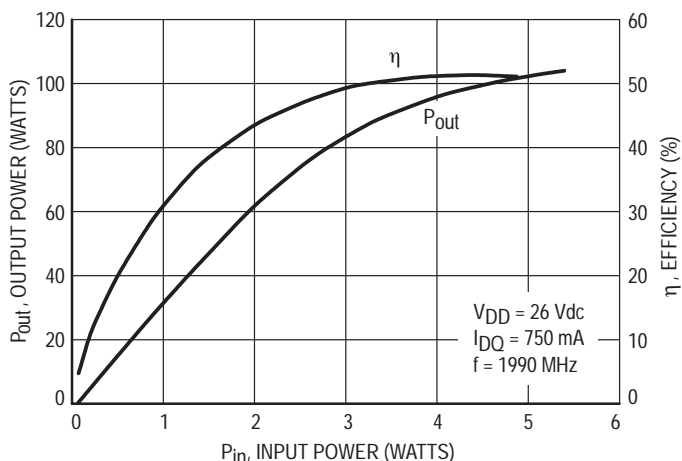


Figure 8. Output Power and Efficiency versus Input Power

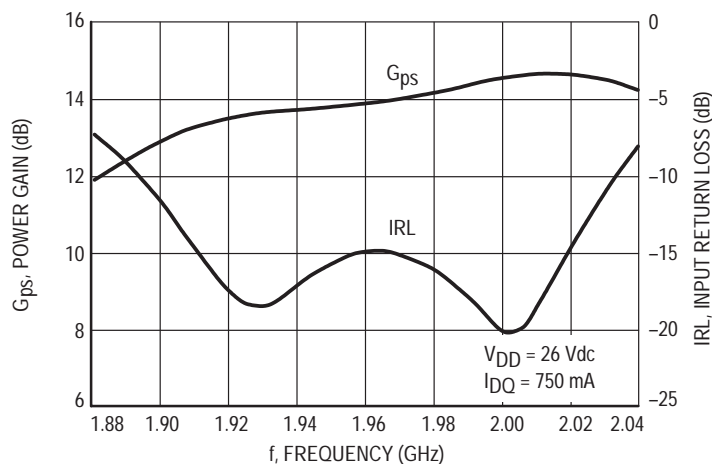


Figure 9. Wideband Gain and IRL (at Small Signal)

$V_{DD} = 26\text{ V}$, $I_{DQ} = 750\text{ mA}$, $P_{out} = 90\text{ Watts (CW)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1805	$1.1 + j5.85$	$1.15 + j2.16$
1880	$1.56 + j6.75$	$1.13 + j2.6$
1930	$2.05 + j8.0$	$1.30 + j2.23$
1990	$2.3 + j7.3$	$0.82 + j2.90$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load at a given voltage, P1dB, gain, efficiency, bias current and frequency.

Table 1. Large Signal Input and Output Impedance

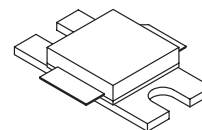
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RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for class AB PCN and PCS base station applications from 1.8 to 2.0 GHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications.

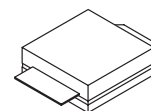
- CDMA Performance @ 1990 MHz, 26 Volts
IS-97 CDMA Pilot, Sync, Paging, Traffic Codes 8 Thru 13
885 kHz — -47 dBc @ 30 kHz BW
1.25 MHz — -55 dBc @ 12.5 kHz BW
2.25 MHz — -55 dBc @ 1 MHz BW
Output Power — 4.5 Watts (Avg.)
Power Gain — 13.5 dB
Efficiency — 17%
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 1.93 GHz, 30 Watts CW Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF19030
MRF19030S

2.0 GHz, 30 W, 26 V
LATERAL N-CHANNEL
RF POWER MOSFETs



CASE 465E-02, STYLE 1
(MRF19030)



CASE 465F-01, STYLE 1
(MRF19030S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	65	Vdc
Gate-Source Voltage	V _{GS}	+15, -0.5	Vdc
Total Device Dissipation @ T _C = 25°C Derate above 25°C	P _D	83.3 0.48	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +200	°C
Operating Junction Temperature	T _J	200	°C

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

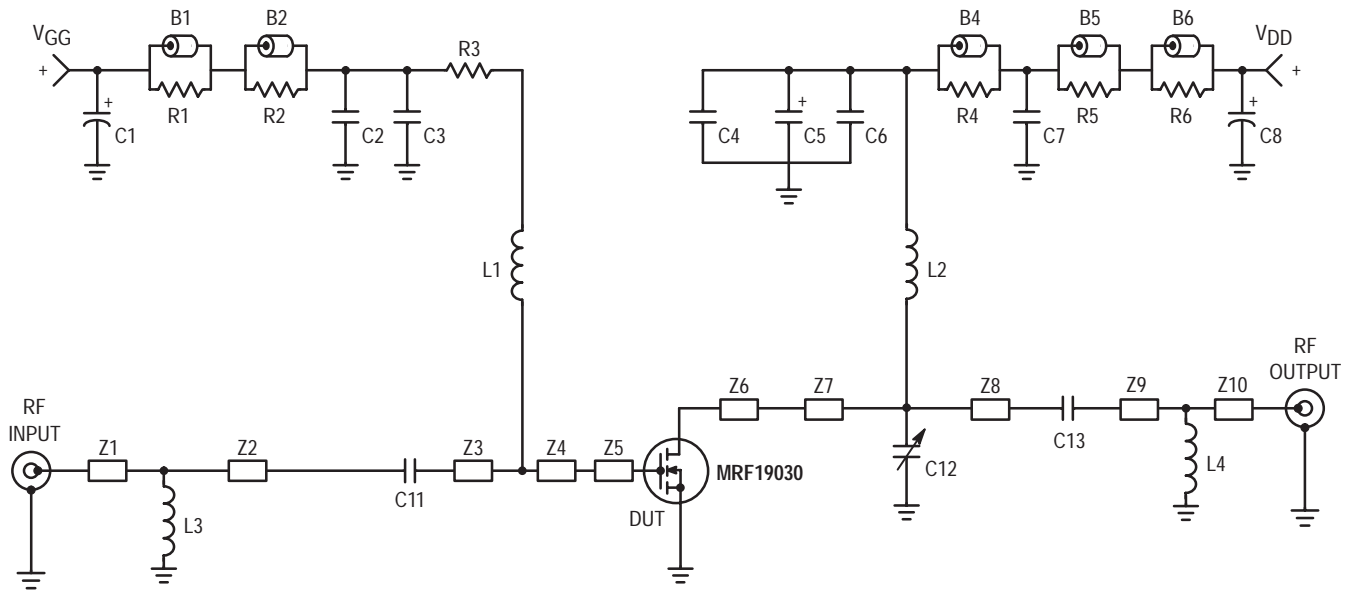
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	2.1	°C/W

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 20\ \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μA dc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μA dc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 100\ \mu\text{A}$ dc)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ Vdc}$, $I_D = 300\text{ mA}$)	$V_{GS(Q)}$	2	3.3	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ A}$ dc)	$V_{DS(on)}$	—	0.29	0.4	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 1\text{ A}$ dc)	g_{fs}	—	2	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance (Including Input Matching Capacitor in Package) (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	98.5	—	pF
Output Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	37	—	pF
Reverse Transfer Capacitance ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	1.3	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1960.0\text{ MHz}$, $f_2 = 1960.1\text{ MHz}$)	G_{ps}	—	13	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1960.0\text{ MHz}$, $f_2 = 1960.1\text{ MHz}$)	η	—	36	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1960.0\text{ MHz}$, $f_2 = 1960.1\text{ MHz}$)	IMD	—	–31	—	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1960.0\text{ MHz}$, $f_2 = 1960.1\text{ MHz}$)	IRL	—	–13	—	dB
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$ and $f_1 = 1990.0\text{ MHz}$, $f_2 = 1990.1\text{ MHz}$)	G_{ps}	12	13	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$ and $f_1 = 1990.0\text{ MHz}$, $f_2 = 1990.1\text{ MHz}$)	η	33	36	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$ and $f_1 = 1990.0\text{ MHz}$, $f_2 = 1990.1\text{ MHz}$)	IMD	—	–31	–28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 300\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$ and $f_1 = 1990.0\text{ MHz}$, $f_2 = 1990.1\text{ MHz}$)	IRL	—	–13	–9	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 30\text{ W CW}$, $I_{DQ} = 300\text{ mA}$, $f = 1930\text{ MHz}$, $V_{SWR} = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.



B1 – B6	Ferrite Bead, Fair Rite #2743019447	Z1	0.595" x 0.080" Microstrip
C1, C8	470 μ F, 63 V, Electrolytic Capacitor, Panasonic #ECEV1HV100R	Z2	0.600" x 0.080" Microstrip
C2, C7	0.10 μ F, RF Chip Capacitor, B Case, Kemet	Z3	0.480" x 0.080" Microstrip
C3	5.1 pF, RF Chip Capacitor, B Case, ATC	Z4	0.280" x 0.325" Microstrip
C4	5.1 pF, RF Chip Capacitor, B Case, ATC	Z5	0.200" x 0.510" Microstrip
C5	22 μ F, 35 V, Tantalum Surface Mount Chip Capacitor, Sprague	Z6	0.200" x 0.510" Microstrip
C6	91 pF, RF Chip Capacitor, B Case, ATC	Z7	0.280" x 0.325" Microstrip
C11, C13	10 pF, RF Chip Capacitor, B Case, ATC	Z8	0.480" x 0.080" Microstrip
C12	0.4 – 2.5 pF, Variable Capacitor, Johanson Gigatrim	Z9	0.530" x 0.080" Microstrip
L1 – L4	8.0 nH Inductors, 3 Turn, Coilcraft	Z10	0.720" x 0.080" Microstrip
R1, R2	12 Ω , Fixed Film Chip Resistor, 0.08" x 0.13"	Board	0.030" Glass Teflon® Arlon
R3	3.75 Ω , Fixed Film Chip Resistor, 0.08" x 0.13"		GX-0300-55-22, 2 oz. Cu
R4 – R6	10 Ω , Fixed Film Chip Resistor, 0.08" x 0.13"		

Figure 1. MRF19030 Schematic

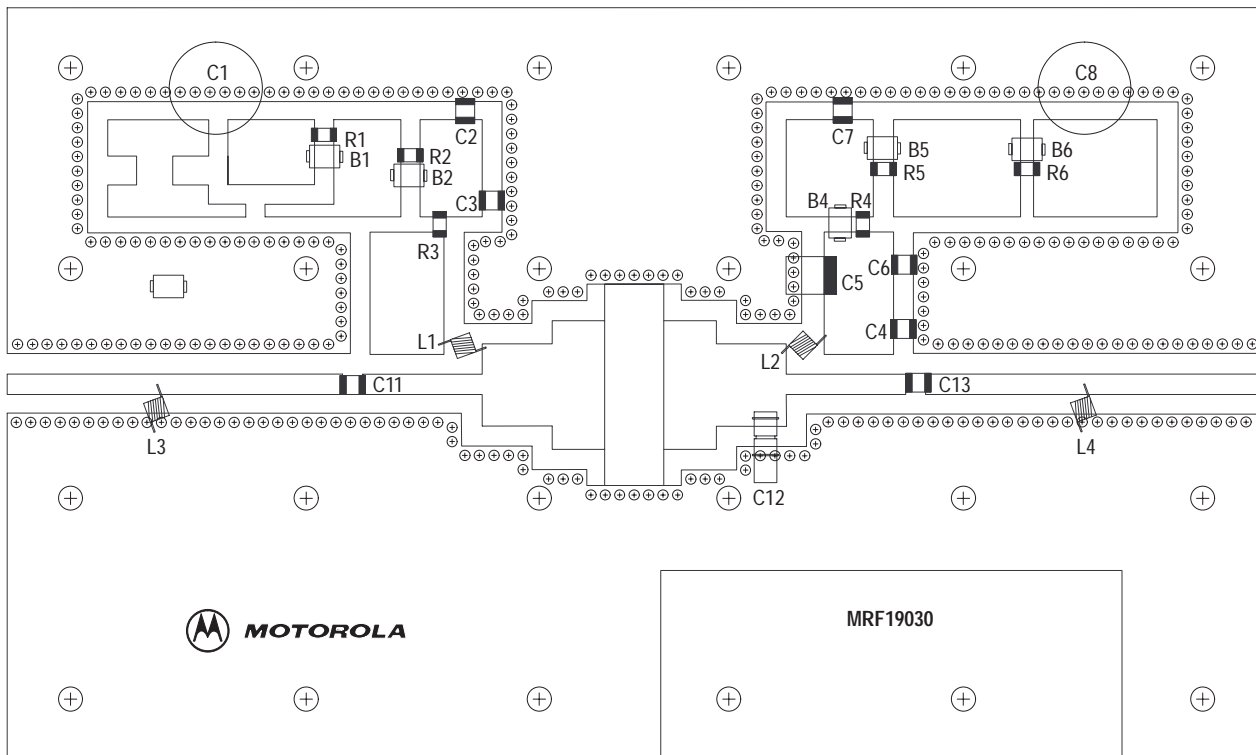


Figure 2. MRF19030 Populated PC Board Layout Diagram

TYPICAL CHARACTERISTICS

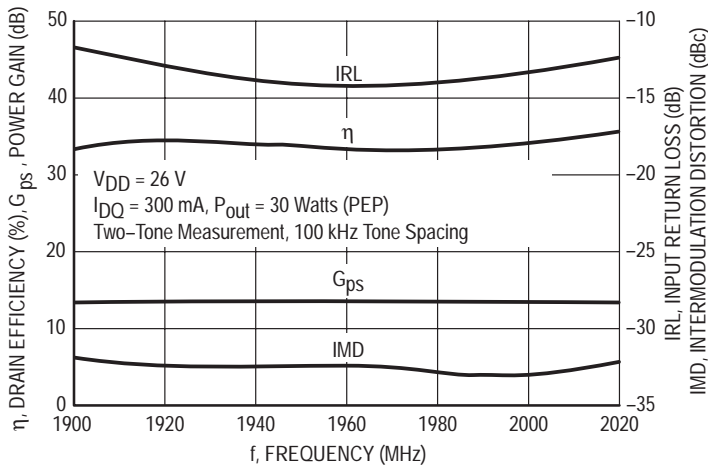


Figure 3. Class AB Broadband Circuit Performance

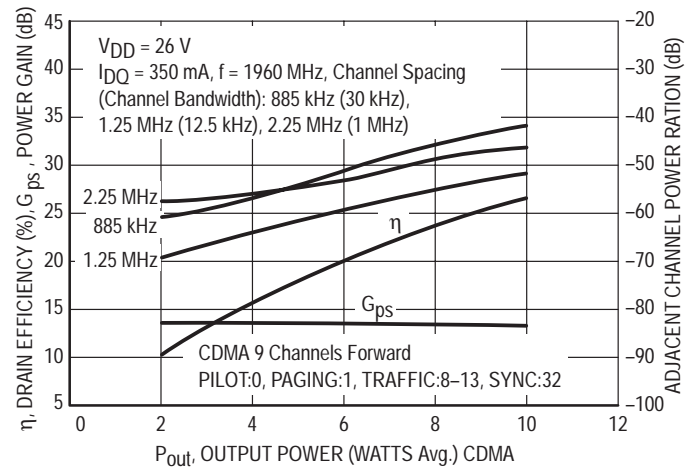


Figure 4. CDMA ACPR, Power Gain and Drain Efficiency versus Output Power

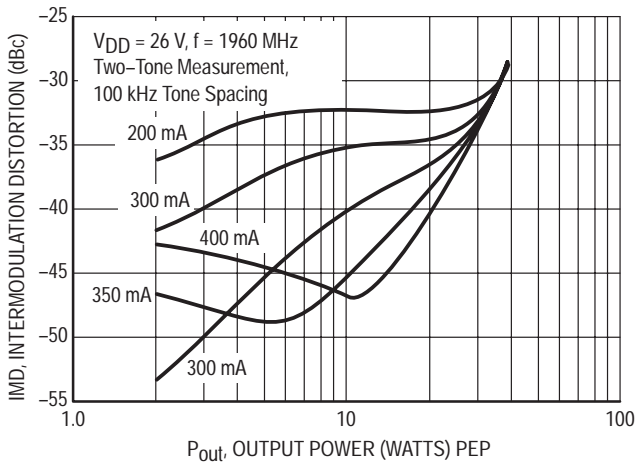


Figure 5. Intermodulation Distortion versus Output Power

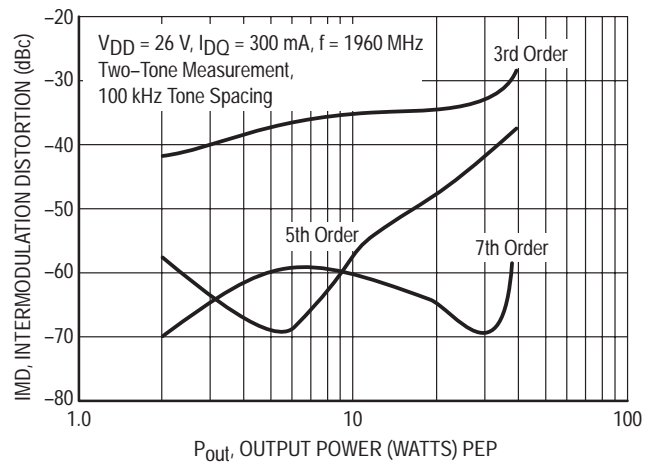


Figure 6. Intermodulation Distortion Products versus Output Power

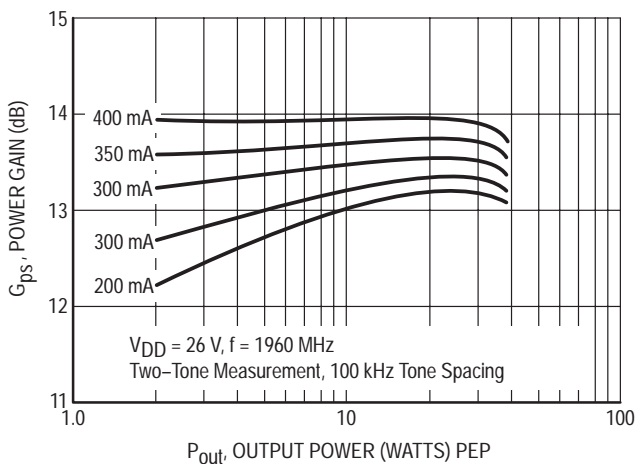


Figure 7. Power Gain versus Output Power

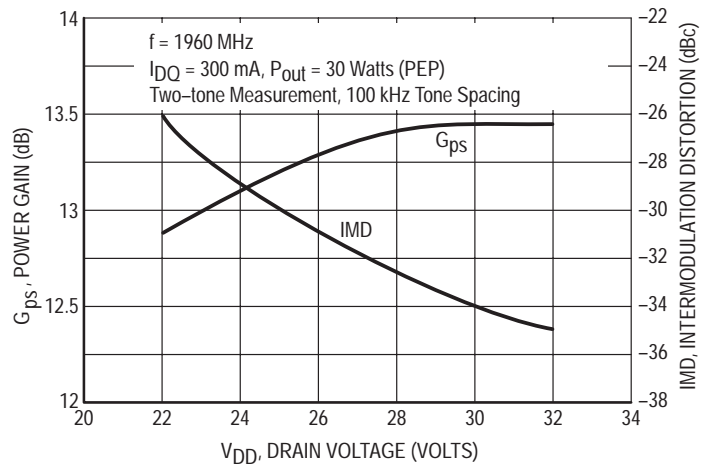
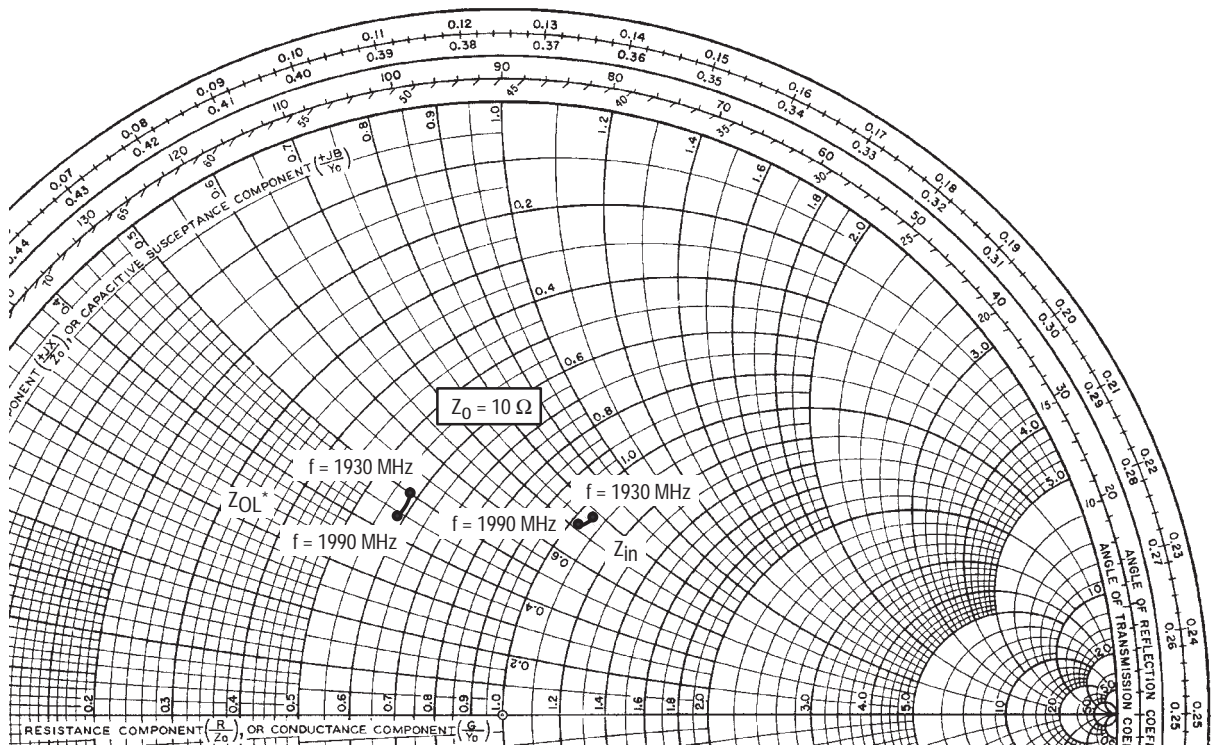


Figure 8. Power Gain and Intermodulation Distortion versus Supply Voltage



$V_{DD} = 26\text{ V}$, $I_{DQ} = 300\text{ mA}$, $P_{out} = 30\text{ Watts (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1930	$10.57 + j7.69$	$5.81 + j5.01$
1960	$10.54 + j7.43$	$5.84 + j4.67$
1990	$10.47 + j7.21$	$5.84 + j4.35$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

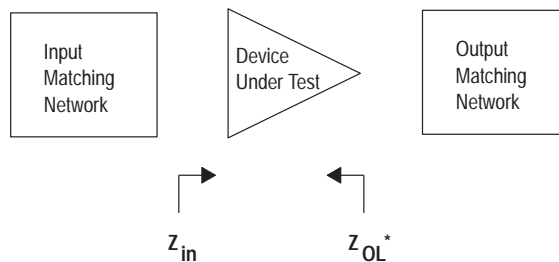


Figure 9. Series Equivalent Input and Output Impedance

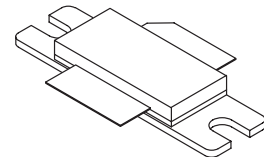
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for PCN and PCS base station applications from frequencies up to 1.9 to 2.0 GHz. Suitable for CDMA, TDMA, GSM and multicarrier amplifier applications.

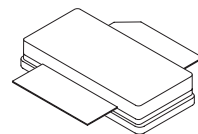
- Typical CDMA Performance: 1960 MHz, 26 Volts
IS-97 CDMA Pilot, Sync, Paging, Traffic Codes 8 Through 13
Output Power — 7.5 Watts
Power Gain — 12.5 dB
Adjacent Channel Power —
885 kHz: -47 dBc @ 30 kHz BW
1.25 MHz: -55 dBc @ 12.5 kHz BW
2.25 MHz: -55 dBc @ 1 MHz BW
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 1.93 GHz, 60 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF19060
MRF19060S

1990 MHz, 60 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465-04, STYLE 1
(MRF19060)



CASE 465A-04, STYLE 1
(MRF19060S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V _{DSS}	65	Vdc
Gate-Source Voltage	V _{GS}	+15, -0.5	Vdc
Total Device Dissipation @ T _C ≥ 25°C Derate above 25°C	P _D	180 1.03	Watts W/°C
Storage Temperature Range	T _{stg}	-65 to +150	°C
Operating Junction Temperature	T _J	200	°C

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

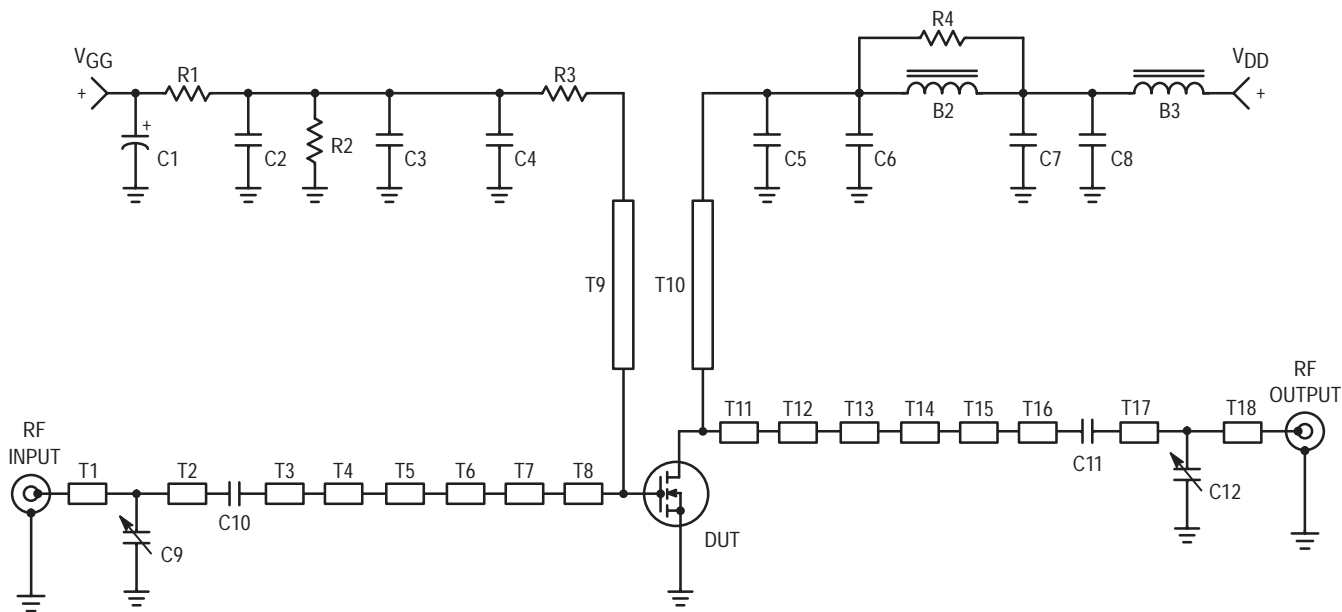
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	R _{θJC}	0.97	°C/W

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 10\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	6	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	g_{fs}	—	4.7	—	S
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	V
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 500\text{ mAdc}$)	$V_{GS(Q)}$	2.5	3.9	4.5	V
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	$V_{DS(on)}$	—	0.27	—	V
DYNAMIC CHARACTERISTICS					
Reverse Transfer Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	2.7	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	G_{ps}	11	12.5	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	η	33	36	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	IMD	—	–31	–28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	IRL	—	–12	—	dB
P_{out} , 1 dB Compression Point ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\text{ W CW}$, $f = 1990\text{ MHz}$)	P1dB	—	60	—	W
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 60\text{ W CW}$, $I_{DQ} = 500\text{ mA}$, $f = 1930\text{ MHz}$, VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.



B2 – B3	Ferrite Bead, Fair Rite, 2743019447	T4	0.152" x 0.140" Microstrip
C1	10 μ F, 50 V Electrolytic, ECEV1HV100R Panasonic	T5	0.090" x 0.102" Microstrip
C2, C7	1000 pF, B Case Chip Capacitor, 100B102JCA500X, ATC	T6	0.245" x 0.217" Microstrip
C3, C8	0.10 μ F, B Case Chip Capacitor, CDR33BX104AKWS, Kemet	T7	0.090" x 0.737" Microstrip
C4	5.1 pF, B Case Chip Capacitor, 100B5R1JCA500X, ATC	T8	0.530" x 0.941" Microstrip
C5	6.2 pF, B Case Chip Capacitor, 100B6R2JCA500X, ATC	T9	1.010" x 0.050" Microstrip
C6	22 μ F, 35 V Tantalum, SMT, Sprague	T10	1.060" x 0.050" Microstrip
C9	0.8 pF – 8.0 pF, Variable Capacitor, Johanson Gigatrim	T11	0.446" x 1.137" Microstrip
C10, C11	10 pF, B Case Chip Capacitor, 100B100JCA500X, ATC	T12	0.152" x 0.567" Microstrip
C12	0.4 pF – 2.5 pF, Variable Capacitor, Johanson Gigatrim	T13	0.183" x 0.220" Microstrip
R1	1 k Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T14	0.100" x 0.338" Microstrip
R2	560 k Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T15	0.480" x 0.142" Microstrip
R3	15 Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T16	0.140" x 0.080" Microstrip
R4	10 Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T17	0.173" x 0.080" Microstrip
T1	0.580" x 0.074" Microstrip	T18	0.420" x 0.080" Microstrip
T2	0.100" x 0.074" Microstrip	Board	0.030" Glass Teflon [®] Arlon GX-0300-55-22, 2 oz Cu
T3	0.384" x 0.074" Microstrip		

Figure 1. MRF19060 Schematic

TYPICAL CHARACTERISTICS

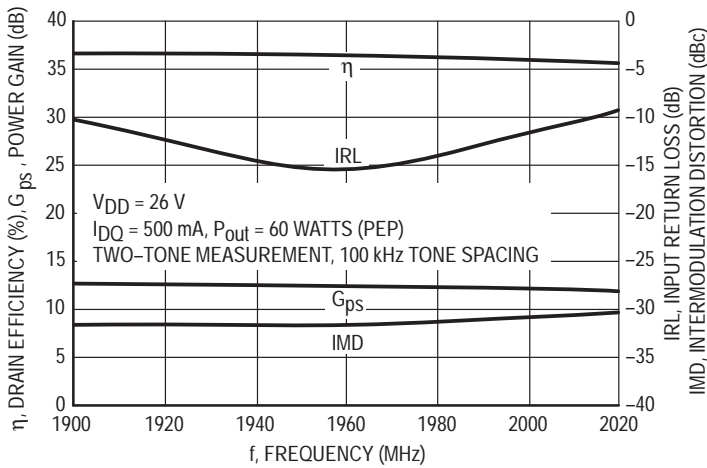


Figure 2. Class AB Broadband Circuit Performance

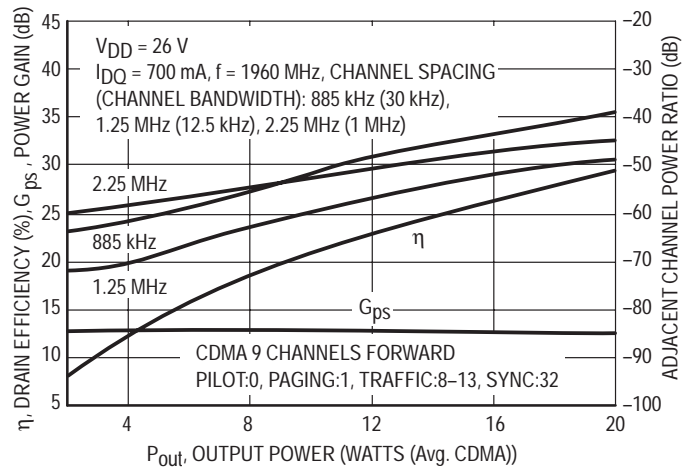


Figure 3. CDMA ACPR, Power Gain and Drain Efficiency versus Output Power

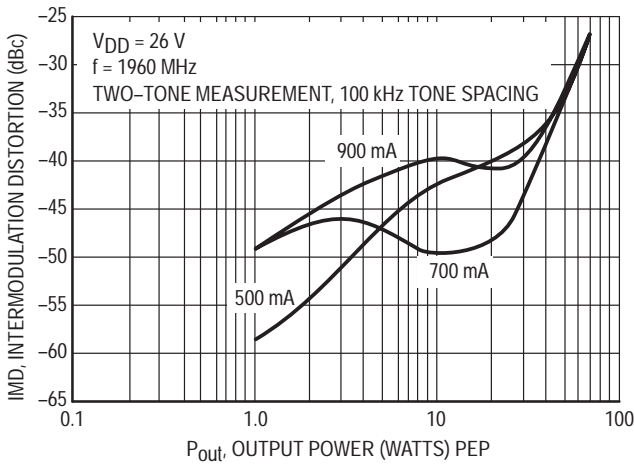


Figure 4. Intermodulation Distortion versus Output Power

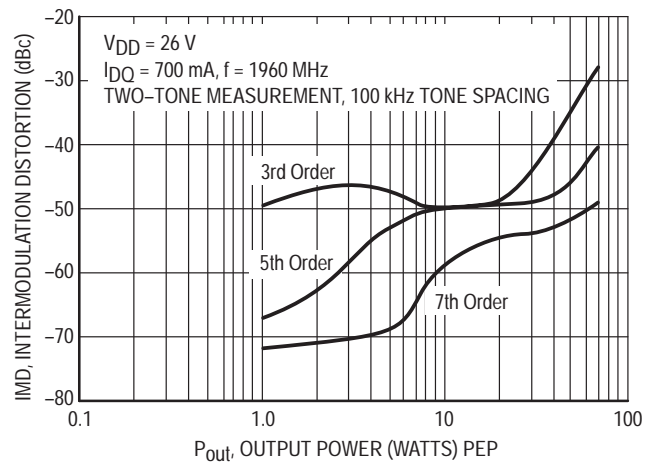


Figure 5. Intermodulation Products versus Output Power

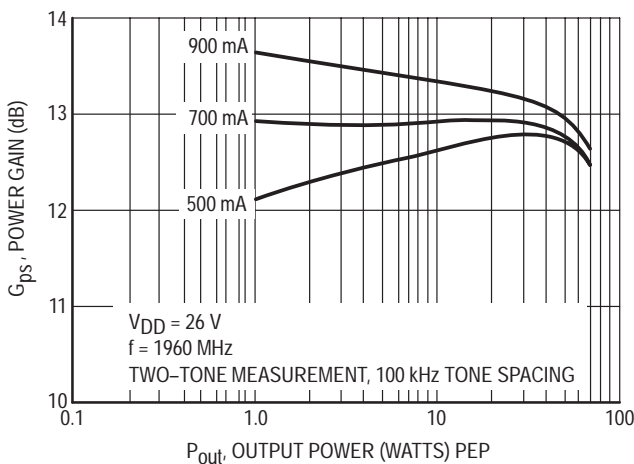


Figure 6. Power Gain versus Output Power

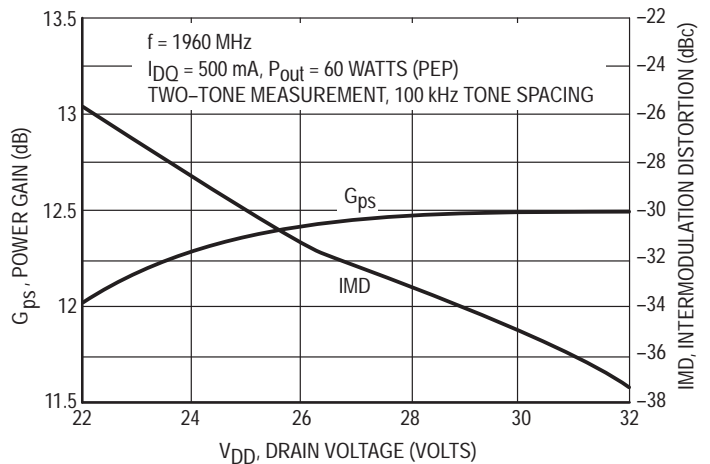
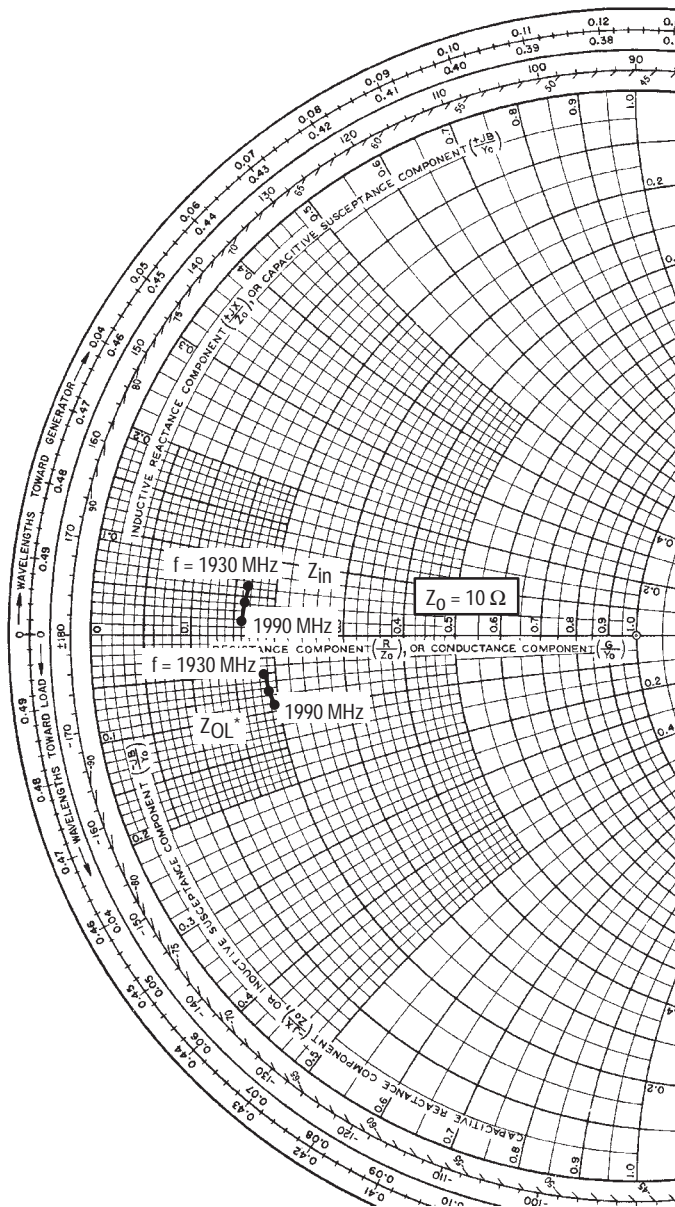


Figure 7. Power Gain and Intermodulation Distortion versus Supply Voltage



$V_{DD} = 26 \text{ V}$, $I_{DQ} = 500 \text{ mA}$, $P_{out} = 60 \text{ Watts (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1930	$1.65 + j0.67$	$1.85 - j0.50$
1960	$1.64 + j0.45$	$1.89 - j0.74$
1990	$1.60 + j0.20$	$1.96 - j0.94$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

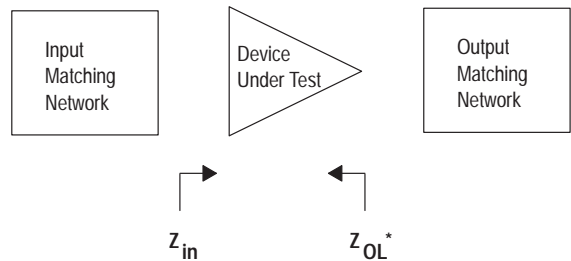


Figure 8. Series Equivalent Input and Output Impedance

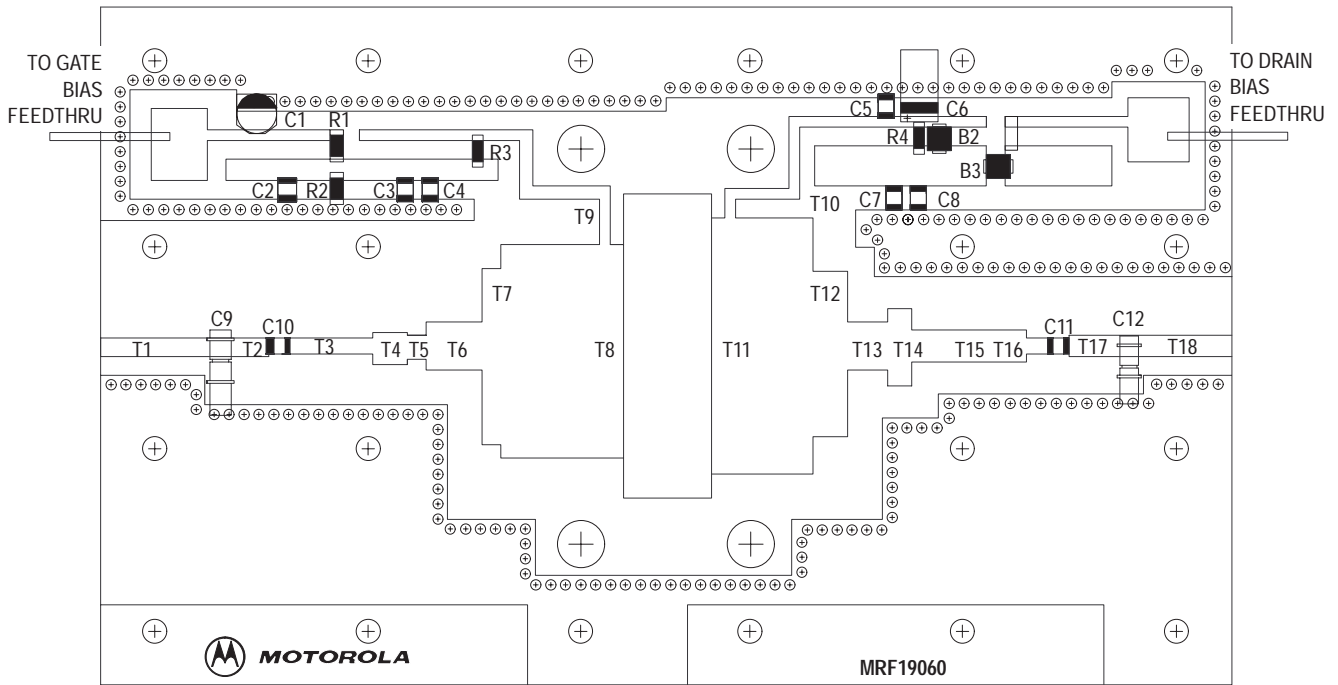


Figure 9. MRF19060 Populated PC Board Layout Diagram

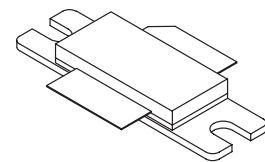
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for PCN and PCS base station applications from frequencies up to 1.9 to 2.0 GHz. Suitable for TDMA, CDMA and multicarrier amplifier applications.

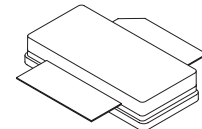
- Typical 2-Carrier N-CDMA Performance for $V_{DD} = 26$ Volts, $I_{DQ} = 850$ mA, $P_{Out} = 18$ Watts Avg., $f_1 = 1960$ MHz, $f_2 = 1962.5$ MHz IS-95 CDMA (Pilot, Sync, Paging, Traffic Codes 8 Through 13) 1.2288 MHz Channel Bandwidth Carrier. Adjacent Channels Measured over a 30 kHz Bandwidth at $f_1 - 885$ KHz and $f_2 + 885$ kHz. Distortion Products Measured over 1.2288 MHz Bandwidth at $f_1 - 2.5$ MHz and $f_2 + 2.5$ MHz. Peak/Avg. = 9.8 dB @ 0.01% Probability on CCDF.
Output Power = 18 Watts Avg.
Power Gain = 13.0 dB
Efficiency = 23%
ACPR = -51 dB
IM3 = -36.5 dBc
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 5:1 VSWR, @ 26 Vdc, 1.93 GHz, 90 Watts (CW) Output Power
- Excellent Thermal Stability

MRF19085
MRF19085S

1990 MHz, 90 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465-04, STYLE 1
(MRF19085)



CASE 465A-04, STYLE 1
(MRF19085S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	273 1.56	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.64	$^\circ\text{C/W}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
----------------	--------	-----	-----	-----	------

OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc

ON CHARACTERISTICS (DC)

Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 200\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 850\text{ mAdc}$)	$V_{GS(Q)}$	2.5	3.5	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	$V_{DS(on)}$	—	0.18	0.210	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	g_{fs}	—	6	—	S

DYNAMIC CHARACTERISTICS

Reverse Transfer Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{rss}	—	3.6	—	pF
--	-----------	---	-----	---	----

FUNCTIONAL TESTS (In Motorola Test Fixture) 2–Carrier N–CDMA, 1.2288 MHz Channel Bandwidth Carriers. Peak/Avg. Ratio = 9.8 dB @ 0.01% Probability on CCDF.

Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 18\text{ W Avg.}$, $I_{DQ} = 850\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$)	G_{ps}	12	13	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 18\text{ W Avg.}$, $I_{DQ} = 850\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$)	η	21	23	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 18\text{ W Avg.}$, $I_{DQ} = 850\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$); IM3 measured over 1.2288 MHz bandwidth @ $f_1 - 2.5\text{ MHz}$ and $f_2 = +2.5\text{ MHz}$)	IMD	—	–36.5	–35	dBc
Adjacent Channel Power Ratio ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 18\text{ W Avg.}$, $I_{DQ} = 850\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$); ACPR measured over 30 kHz bandwidth @ $f_1 - 885\text{ MHz}$ and $f_2 = +885\text{ MHz}$)	ACPR	—	–51	–48	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 18\text{ W Avg.}$, $I_{DQ} = 850\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$)	IRL	—	–12	–9	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 850\text{ mA}$, $f = 1930\text{ MHz}$, $V_{SWR} = 5:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 850\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	G_{ps}	—	13	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 850\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	η	—	36	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 850\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	IMD	—	-31	—	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 850\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	IRL	—	-12	—	dB
P_{out} , 1 dB Compression Point ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 850\text{ mA}$, $f = 1990\text{ MHz}$)	P1dB	—	90	—	W

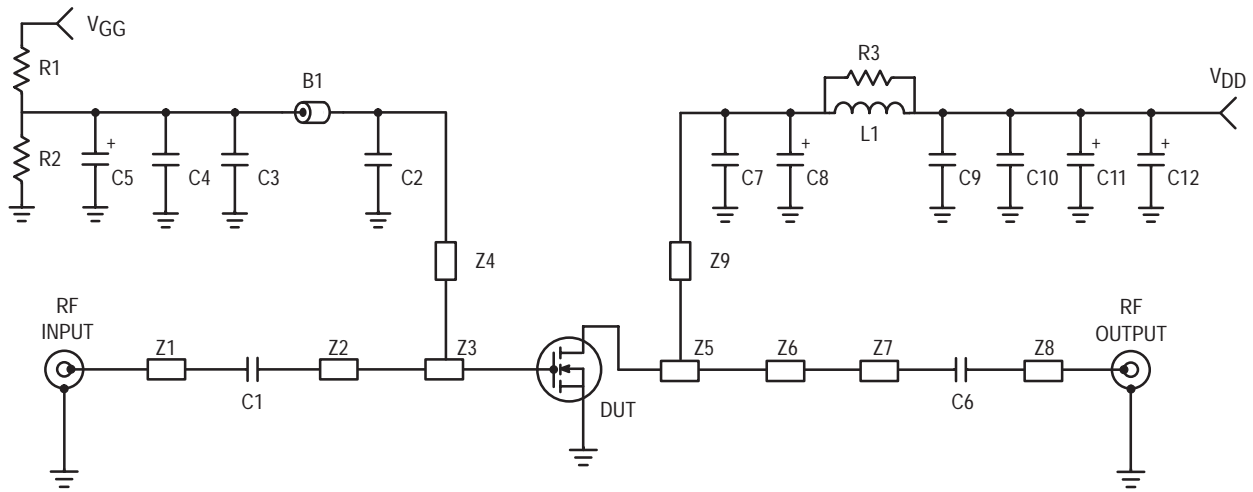


Figure 1. 1930 – 1990 MHz 2-Carrier N-CDMA Test Circuit Schematic

Table 1. 1930 – 1990 MHz 2-Carrier N-CDMA Test Circuit Component Designations and Values

Part	Description	Value, P/N or DWG	Manufacturer
B1	Short Ferrite Bead	2743019447	Fair Rite
C1	51 pF, Chip Capacitor	100B510JCA500X	ATC
C2, C7	5.1 pF, Chip Capacitors	100B5R1JCA500X	ATC
C3, C9	1000 pF, Chip Capacitors	100B102JCA500X	ATC
C4, C10	0.1 μ F, Chip Capacitors	CDR33BX104AKWS	Kemet
C5	0.1 μ F, Tantalum Surface Mount Capacitor	T491C105M050	Kemet
C6	10 pF, Chip Capacitor	100B100JCA500X	ATC
C8	10 μ F, Tantalum Surface Mount Capacitor	T495X106K035AS4394	Kemet
C11, C12	22 μ F, Tantalum Surface Mount Capacitors	T491X226K035AS4394	Kemet
L1	1 Turn, 20 AWG, 0.100" ID		Motorola
N1, N2	Type N Flange Mounts	3052-1648-10	Omni Spectra
R1	1.0 k Ω , 1/8 W Chip Resistor		
R2	220 k Ω , 1/8 W Chip Resistor		
R3	10 Ω , 1/8 W Chip Resistor		
Z1	Transmission Line	0.750" x 0.0840"	
Z2	Transmission Line	1.090" x 0.0840"	
Z3	Transmission Line	0.400" x 1.400"	
Z4	Transmission Line	0.520" x 0.050"	
Z5	Transmission Line	0.540" x 1.133"	
Z6	Transmission Line	0.400" x 0.140"	
Z7	Transmission Line	0.555" x 0.0840"	
Z8	Transmission Line	0.720" x 0.0840"	
Z9	Transmission Line	0.560" x 0.070"	
Board	0.030" Glass Teflon [®]	GX-0300-55-22, $\epsilon_r = 2.55$	Keene
PCB	Etched Circuit Boards	MRF19085 Rev. 4	CMR

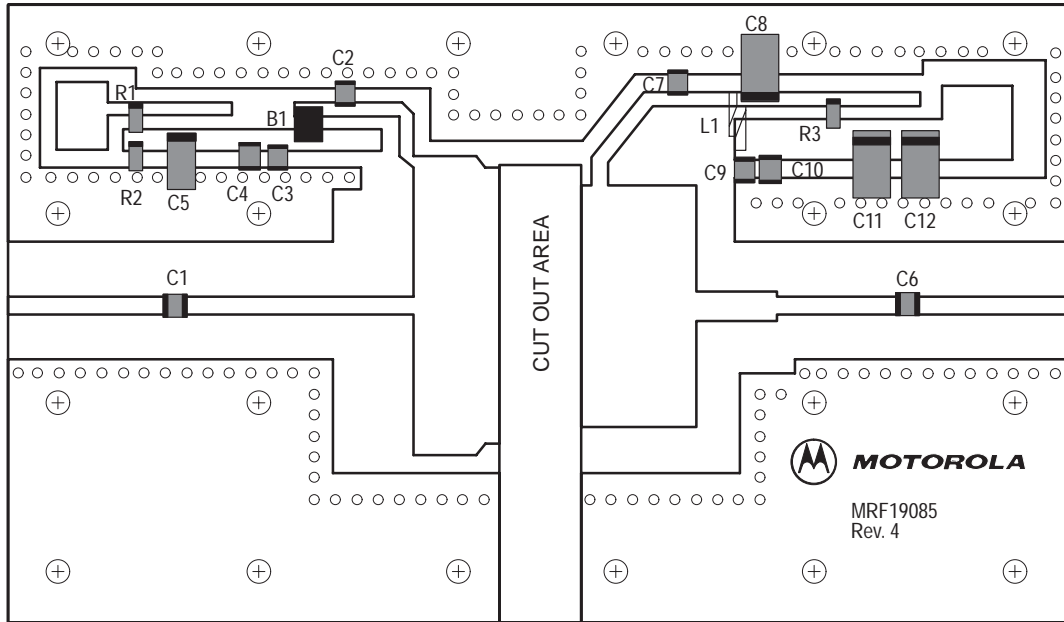


Figure 2. 1930 – 1990 MHz 2-Carrier N-CDMA Test Circuit

TYPICAL CHARACTERISTICS

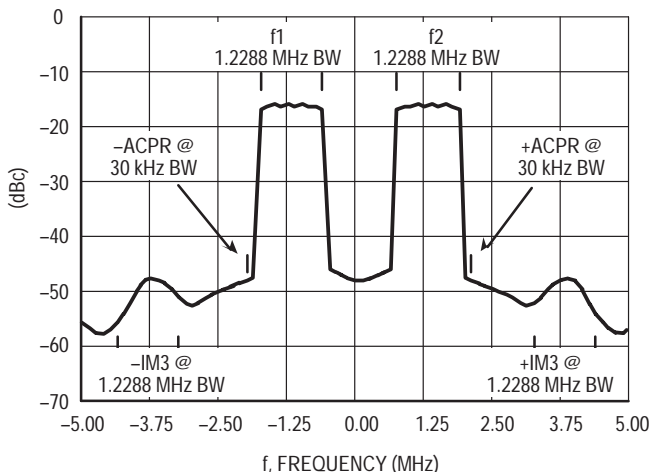


Figure 3. 2-Carrier N-CDMA Spectrum

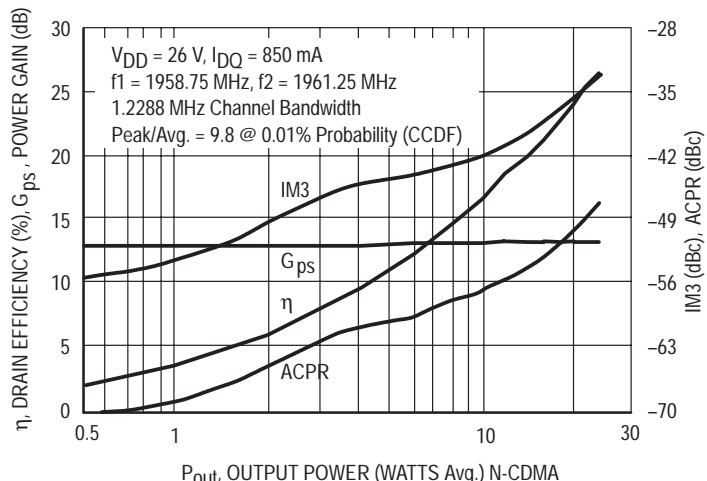


Figure 4. 2-Carrier N-CDMA ACPR, IM3, Power Gain and Drain Efficiency versus Output Power

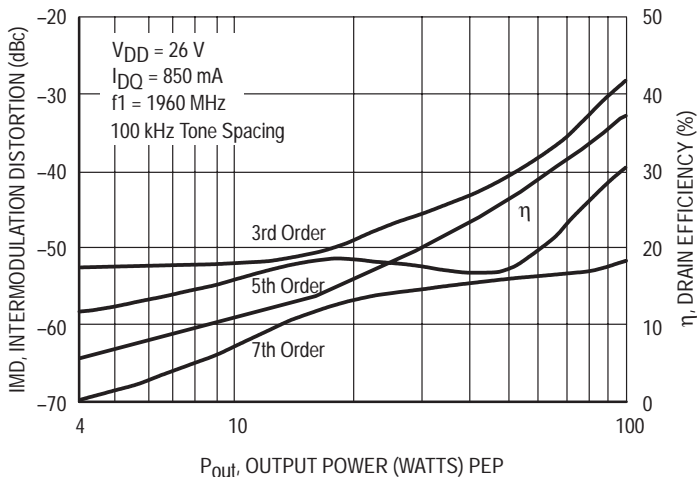


Figure 5. Intermodulation Distortion Products versus Output Power

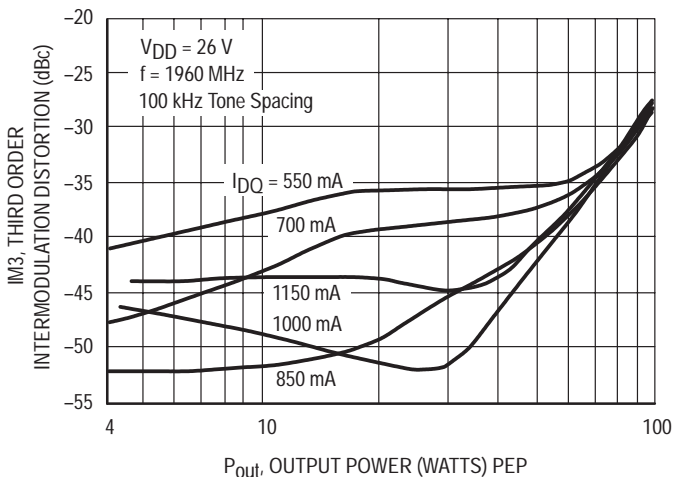


Figure 6. Third Order Intermodulation Distortion versus Output Power and IDQ

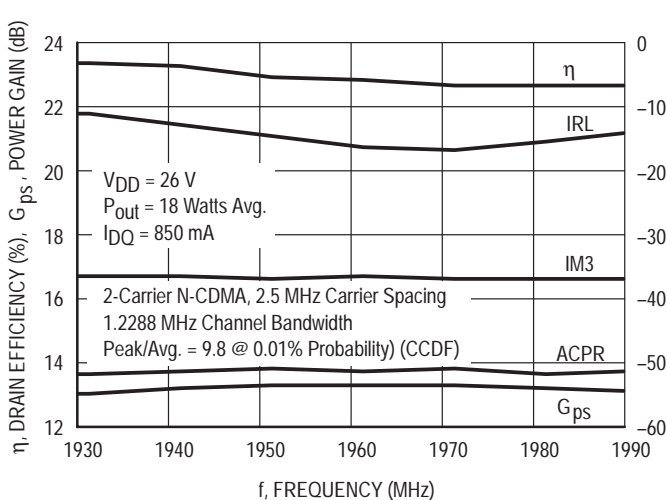


Figure 7. 2-Carrier N-CDMA Broadband Performance

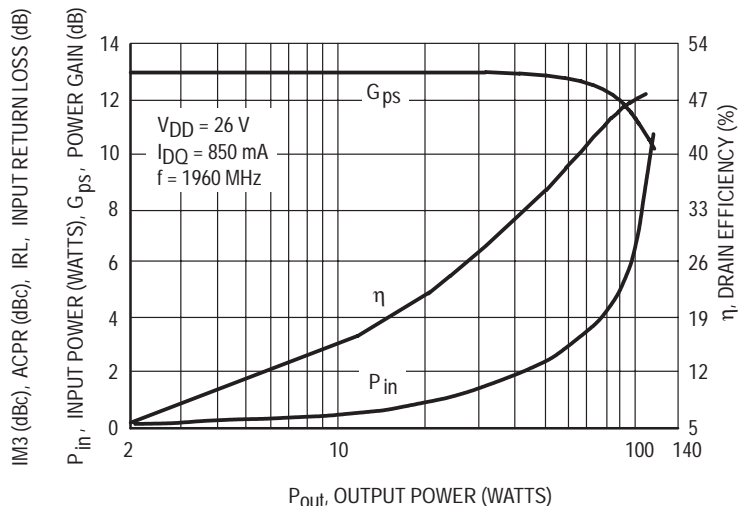


Figure 8. CW Performance

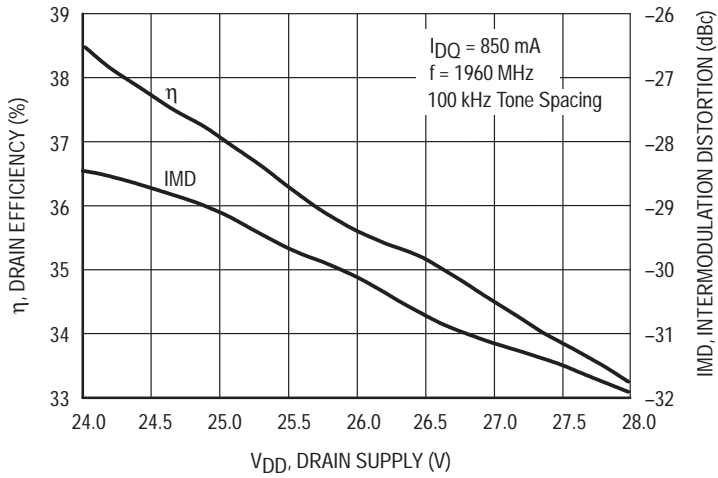


Figure 9. Two-Tone Intermodulation Distortion and Drain Efficiency versus Drain Supply

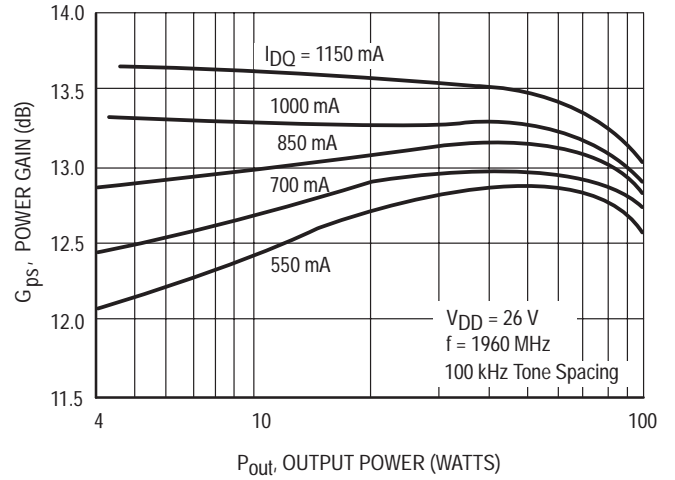


Figure 10. Two-Tone Power Gain versus Output Power

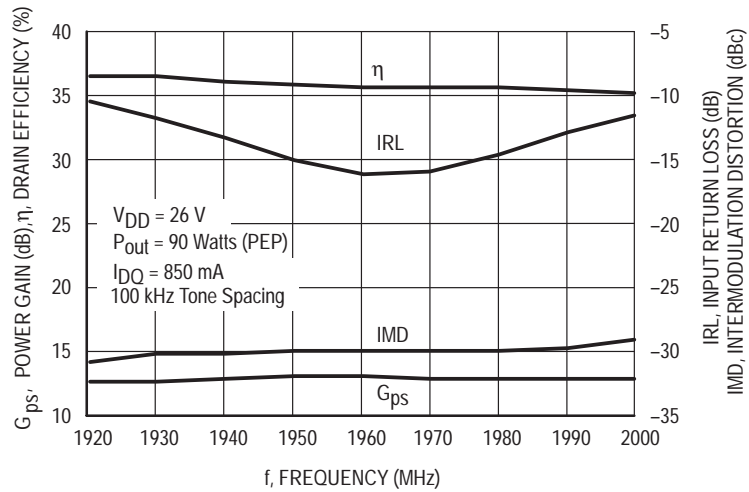
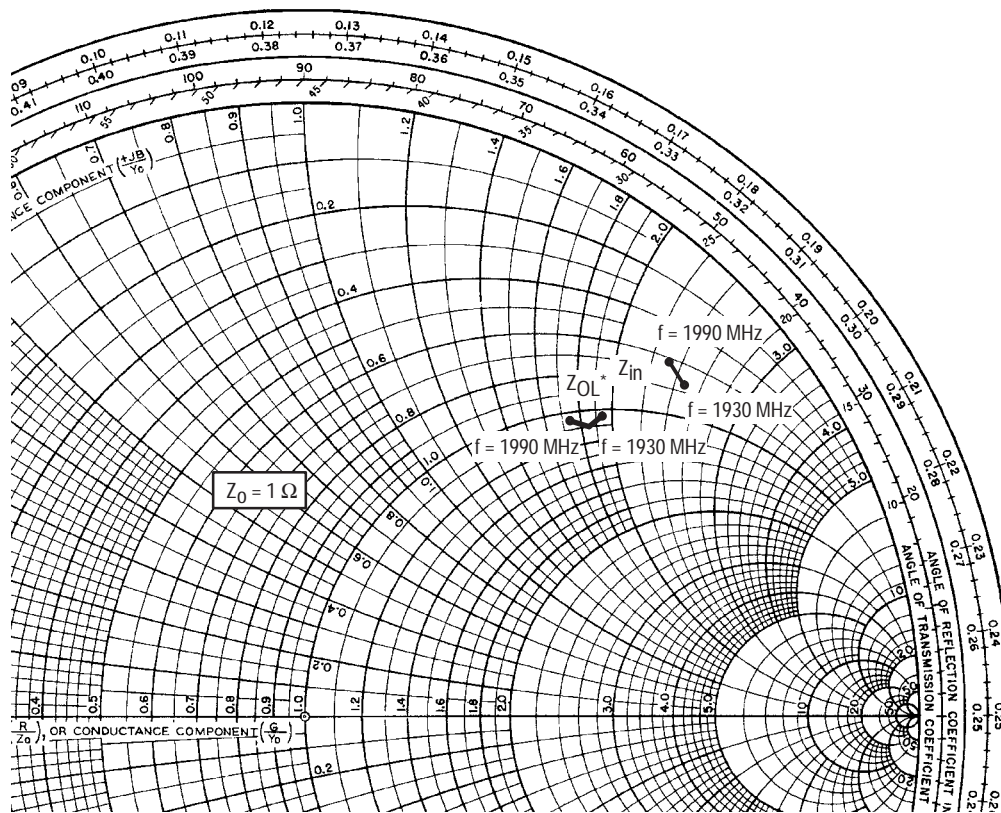


Figure 11. Two-Tone Broadband Performance



$V_{DD} = 26 \text{ V}$, $I_{DQ} = 850 \text{ mA}$, $P_{out} = 18 \text{ W (Avg.)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1930	$0.75 + j2.50$	$1.05 + j1.95$
1960	$0.70 + j2.40$	$1.10 + j1.85$
1990	$0.65 + j2.35$	$1.05 + j1.75$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

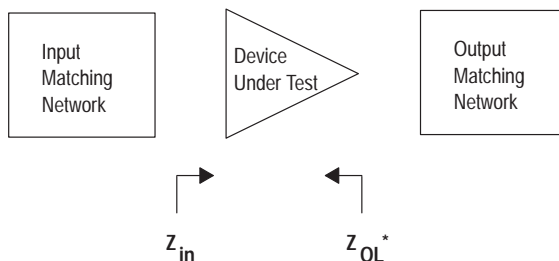


Figure 12. Series Equivalent Input and Output Impedance

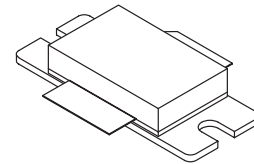
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for class AB PCN and PCS base station applications from 1.9 to 2.0 GHz. Suitable for CDMA, TDMA, GSM, and multicarrier amplifier applications.

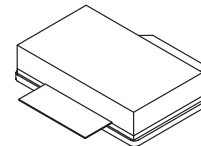
- Typical CDMA Performance: 1990 MHz, 26 Volts
IS-97 CDMA Pilot, Sync, Paging, Traffic Codes 8 Through 13
Output Power — 9 Watts
Power Gain — 10 dB
Adjacent Channel Power —
885 kHz: -47 dBc @ 30 kHz BW
1.25 MHz: -55 dBc @ 12.5 kHz BW
2.25 MHz: -55 dBc @ 1 MHz BW
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 1.93 GHz, 90 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF19090
MRF19090S

1990 MHz, 90 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465B-02, STYLE 1
(MRF19090)



CASE 465C-01, STYLE 1
(MRF19090S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C > = 25^\circ\text{C}$ Derate above 25°C	P_D	270 1.54	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

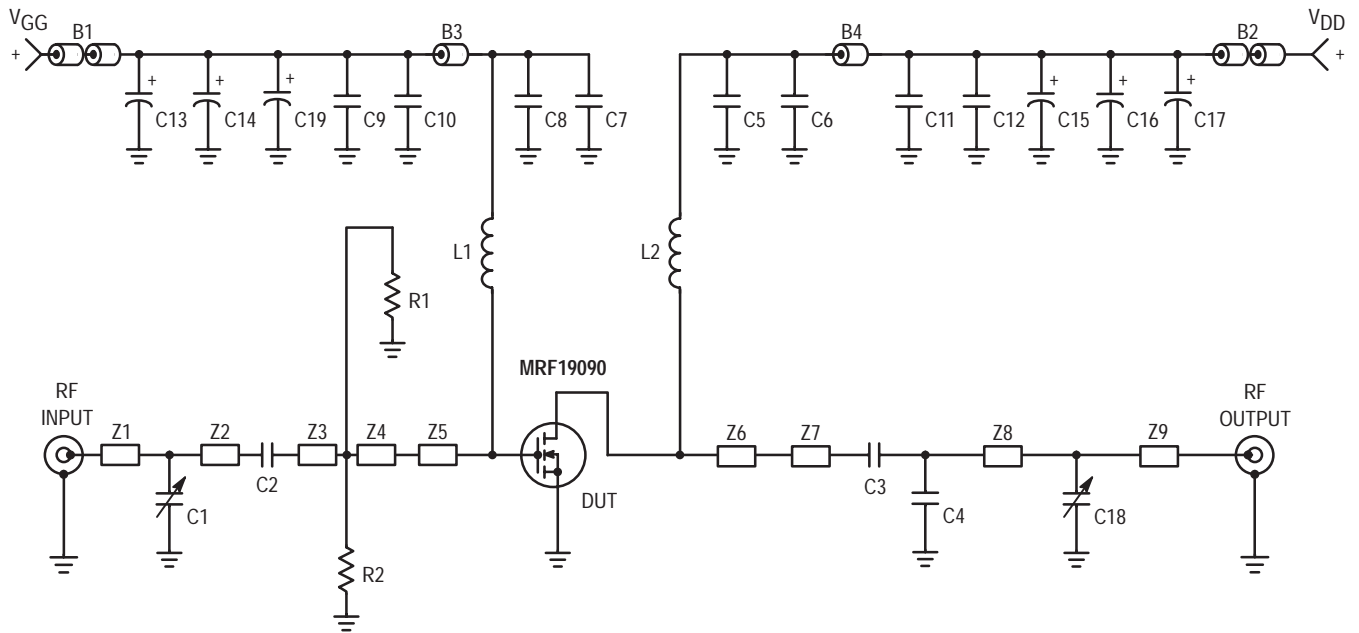
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.65	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$)	g_{fs}	—	7.2	—	S
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2.0	—	4.0	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 750\text{ mAdc}$)	$V_{GS(Q)}$	2.5	3.8	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.10	—	Vdc
DYNAMIC CHARACTERISTICS					
Reverse Transfer Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	4.2	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 750\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	G_{ps}	10	11.5	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 750\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	η	33	35	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 750\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	IMD	—	–30	–28	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 750\text{ mA}$, $f = 1930\text{ MHz}$ and 1990 MHz , Tone Spacing = 100 kHz)	IRL	—	–12	—	dB
P_{out} , 1 dB Compression Point ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $f = 1990\text{ MHz}$)	P1dB	—	90	—	W
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 750\text{ mA}$, $f = 1930\text{ MHz}$, VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.



B1 – B4	2 Ferrite Beads, Round, Ferroxcube 56–590–65–3B	L1, L2	8 Turns, #26 AWG, 0.085" OD, 0.330" Long, Copper Wire
B2 – B3	Ferrite Bead, Surface Mount Ferrite Bead, Ferroxcube	R1, R2	270 Ω , 1/4 W Chip Resistor, Garrett Instruments RM73B2B271JT
C1, C18	0.4 – 2.5 pF, Gigatrim Variable Capacitors, Johanson 27285	Z1	ZO = 50 Ohms
C2, C5, C8	10 pF, ATC RF Chip Capacitors, Case "B", 100B100CCA500X	Z2	ZO = 50 Ohms, Lambda = 0.123
C3	12 pF, ATC RF Chip Capacitors, Case "B", 100B120CCA500X	Z3	ZO = 15.24 Ohms, Lambda = 0.0762
C4	0.3 pF, ATC RF Chip Capacitors, Case "B", 100B0R3CCA500X	Z4	ZO = 10.11 Ohms, Lambda = 0.0392
C6, C7	120 pF, ATC RF Chip Capacitors, Case "B", 100B12R1CCA500X	Z5	ZO = 6.34 Ohms, Lambda = 0.0711
C9, C12	0.1 μ F, Chip Capacitor, CDR33BX104AKWS, KEMET	Z6	ZO = 5.02 Ohms, Lambda = 0.0476
C10, C11	1000 pF, ATC RF Chip Capacitors, Case "B", 100B102JCA50X	Z7	ZO = 5.54 Ohms, Lambda = 0.0972
C13, C17	22 μ F, 35 V Tantalum Surface Mount Electrolytic Chip Capacitor, T491X226K035AS4394, KEMET	Z8	ZO = 50.0 Ohms, Lambda = 0.194
C14, C16	10 μ F, 35 V Tantalum Surface Mount Electrolytic Chip Capacitor, T495X106K035AS4394, KEMET	Z9	ZO = 50.0 Ohms
C15, C19	1 μ F, 35 V Tantalum Surface Mount Electrolytic Chip Capacitor, T495X105K035AS4394, KEMET	Raw PCB Material	0.030" Glass Teflon [®] , $\epsilon_r = 2.55$, 2 oz Copper, 3" x 5" Dimensions

Figure 1. MRF19090 Test Circuit Schematic

TYPICAL CHARACTERISTICS

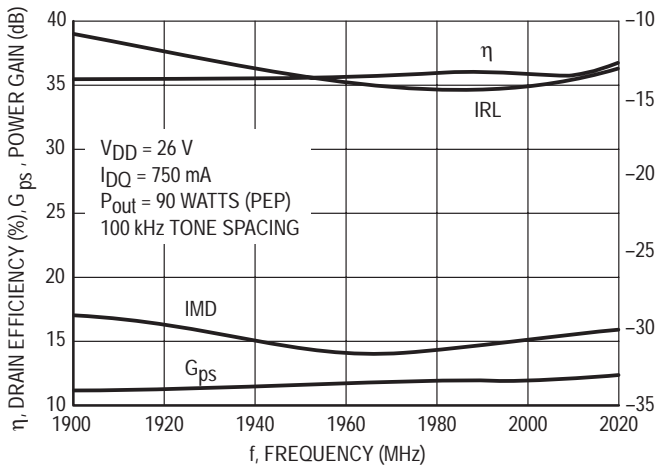


Figure 2. Class AB Performance versus Frequency

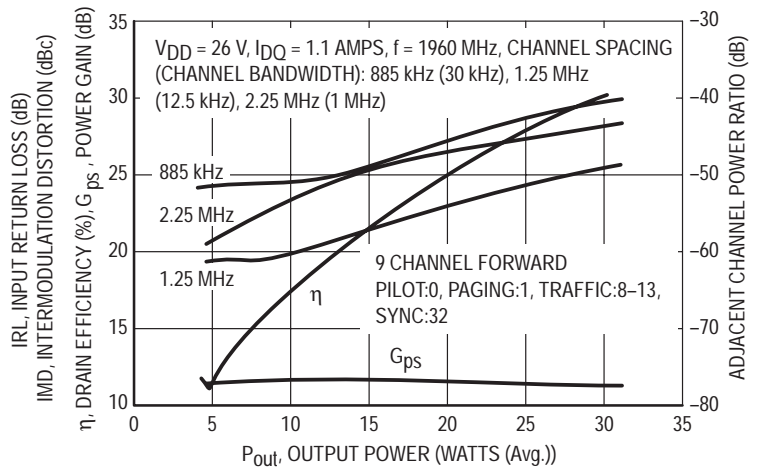


Figure 3. CDMA Performance ACPR, Gain and Drain Efficiency versus Output Power

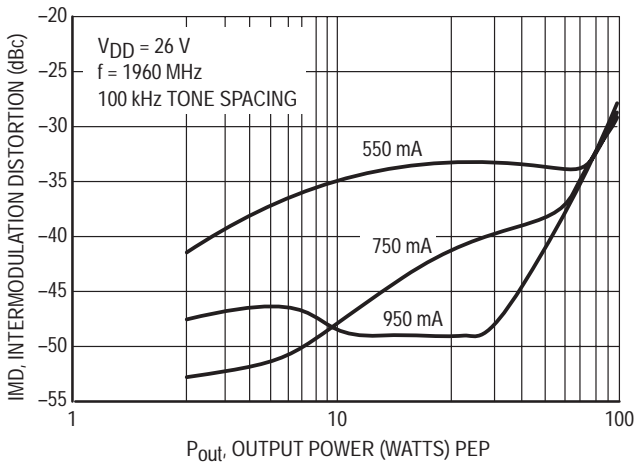


Figure 4. Third Order Intermodulation Distortion versus Output Power

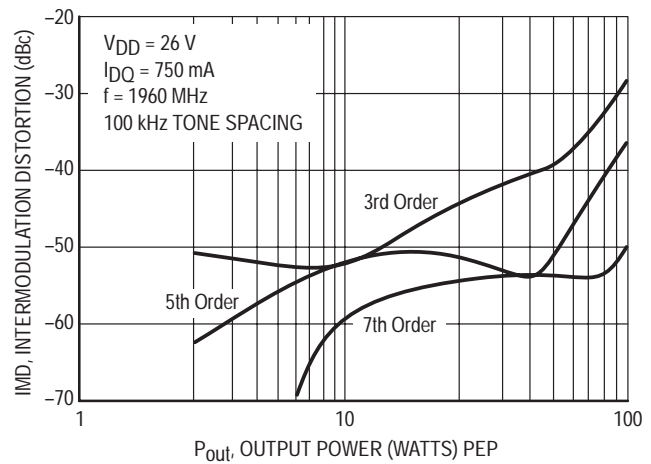


Figure 5. Intermodulation Products versus Output Power

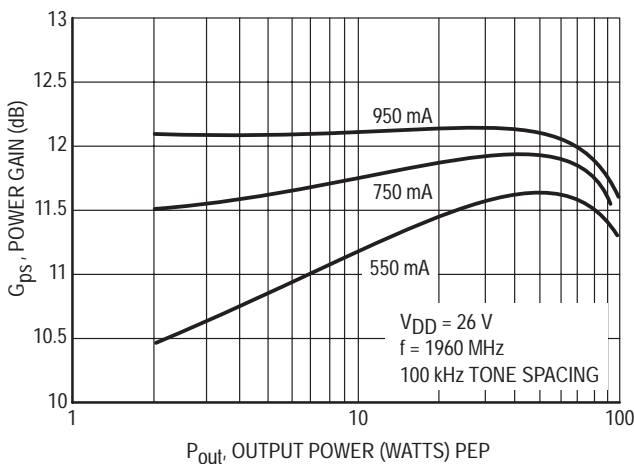


Figure 6. Power Gain versus Output Power

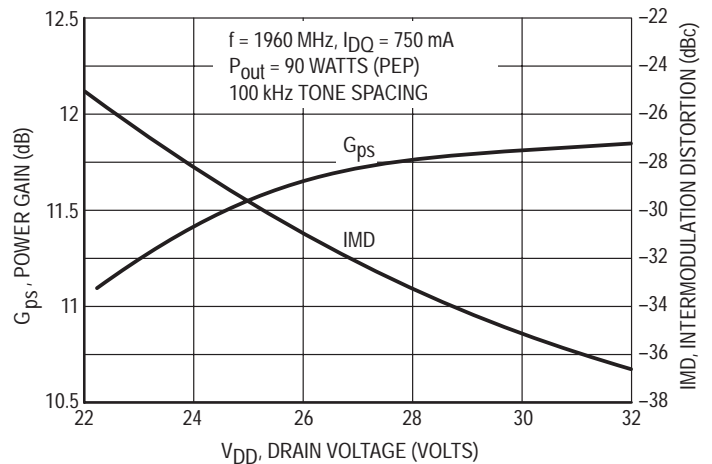
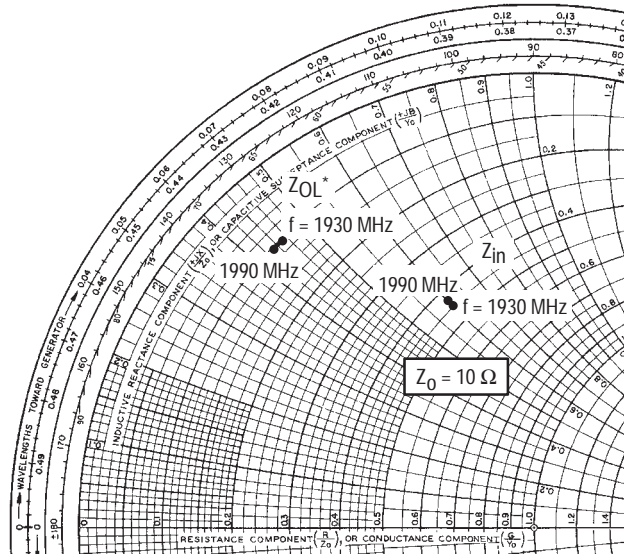


Figure 7. Third Order Intermodulation Distortion and Gain versus Supply Voltage



$V_{DD} = 26 \text{ V}$, $I_{DQ} = 750 \text{ mA}$, $P_{out} = 90 \text{ Watts (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1930	$4.5 + j6.1$	$1.1 + j4.5$
1960	$4.4 + j6.0$	$1.1 + j4.4$
1990	$4.3 + j6.1$	$1.1 + j4.3$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

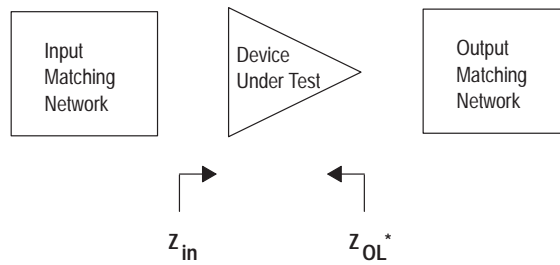


Figure 8. Series Equivalent Input and Output Impedance

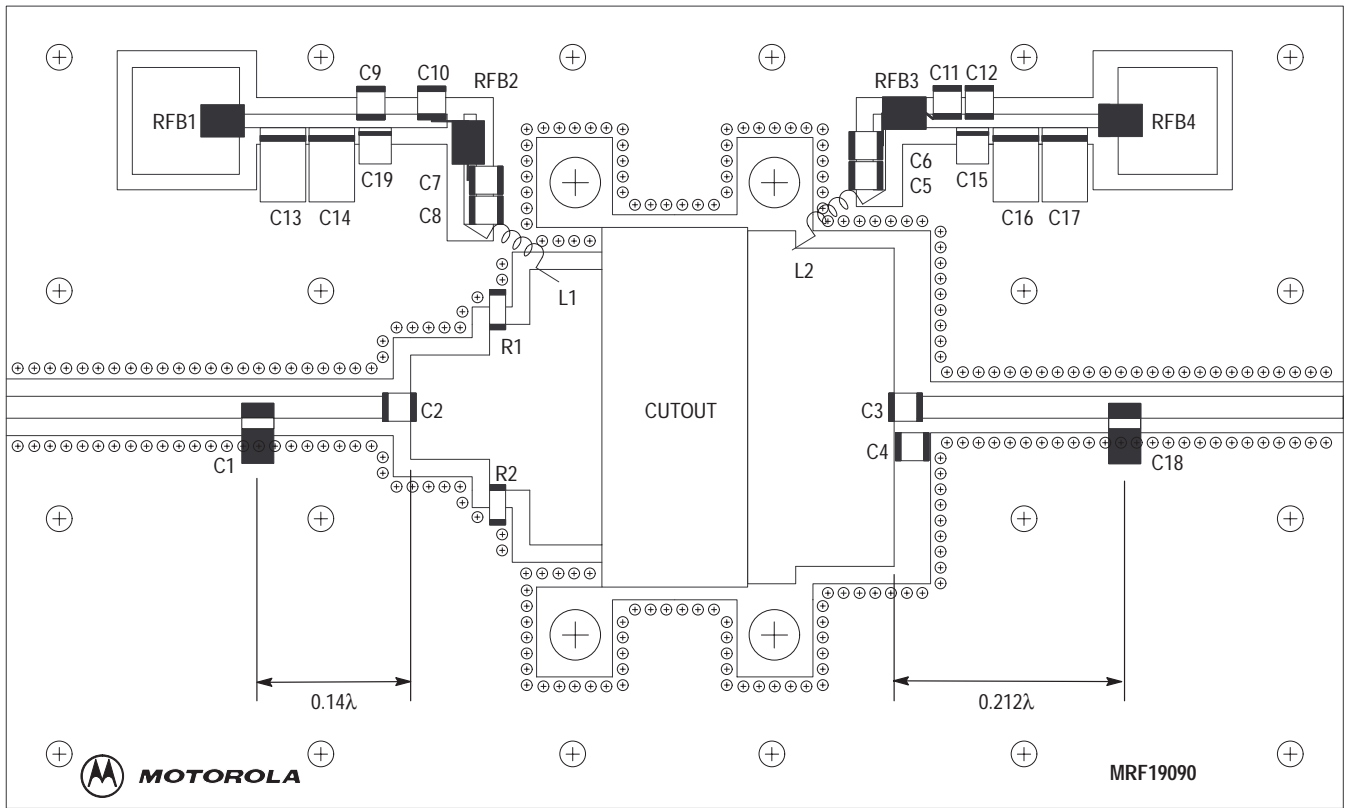


Figure 9. MRF19090 Populated PC Board Layout Diagram

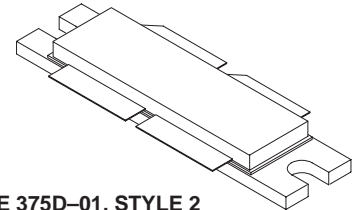
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for CDMA base station applications at frequencies from 1930 to 1990 MHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications. To be used in class AB for PCN-PCS/cellular radio and WLL applications.

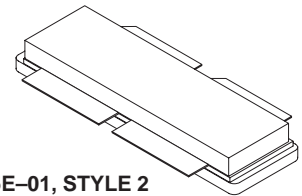
- CDMA Performance @ 1990 MHz, 26 Volts
 - IS-97 CDMA Pilot, Sync, Paging, Traffic Codes 8 Thru 13
 - 885 kHz — -47 dBc @ 30 kHz BW
 - 1.25 MHz — -55 dBc @ 12.5 kHz BW
 - 2.25 MHz — -55 dBc @ 1 MHz BW
 - Output Power — 15 Watts (Avg.)
 - Power Gain — 11.7 dB
 - Efficiency — 16%
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency, High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 26 Vdc, 1990 MHz, 120 Watts (CW) Output Power
- S-Parameter Characterization at High Bias Levels
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF19120
MRF19120S

1990 MHz, 120 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 375D-01, STYLE 2
(MRF19120)



CASE 375E-01, STYLE 2
(MRF19120S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	389 2.22	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.45	$^\circ\text{C}/\text{W}$

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

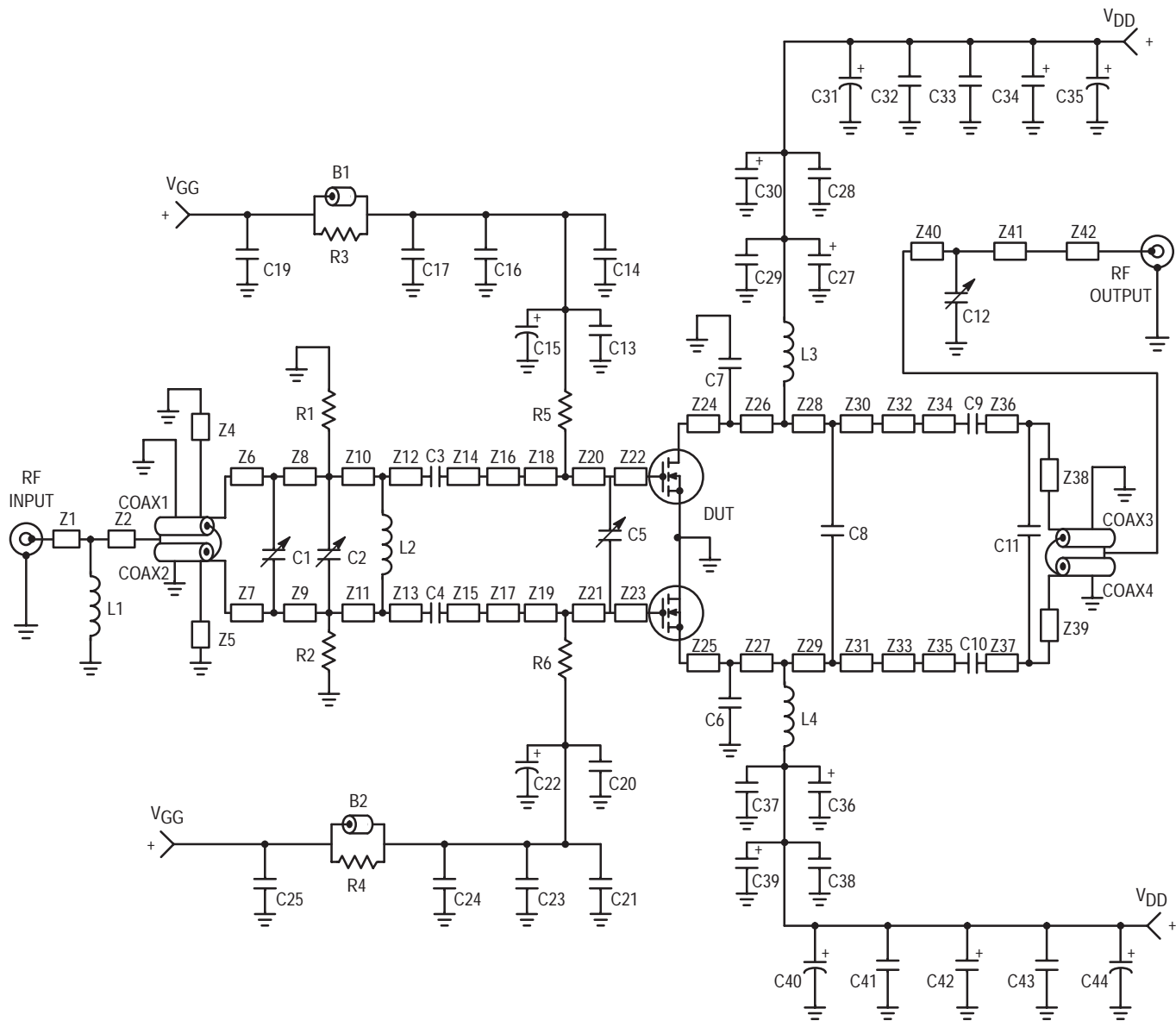
ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)					
Drain–Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 10 \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Gate–Source Leakage Current ($V_{GS} = 5 \text{ Vdc}$, $V_{DS} = 0 \text{ Vdc}$)	I_{GSS}	—	—	1	μA
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 26 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μA
ON CHARACTERISTICS (1)					
Forward Transconductance ($V_{DS} = 10 \text{ Vdc}$, $I_D = 2 \text{ A}$)	g_{fs}	—	4.8	—	S
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}$, $I_D = 200 \mu\text{A}$)	$V_{GS(th)}$	2.5	3	3.8	Vdc
Gate Quiescent Voltage ($V_{DS} = 26 \text{ V}$, $I_D = 500 \text{ mA}$)	$V_{GS(Q)}$	3	3.9	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}$, $I_D = 2 \text{ A}$)	$V_{DS(on)}$	—	0.38	0.5	Vdc
DYNAMIC CHARACTERISTICS (1)					
Reverse Transfer Capacitance ($V_{DS} = 26 \text{ Vdc}$, $V_{GS} = 0$, $f = 1 \text{ MHz}$)	C_{rss}	—	2.8	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture) (2)					
Common–Source Amplifier Power Gain ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1990.0 \text{ MHz}$, $f_2 = 1990.1 \text{ MHz}$)	G_{ps}	10.7 10.5	11.7 11.7	— —	dB
Drain Efficiency ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1990.0 \text{ MHz}$, $f_2 = 1990.1 \text{ MHz}$)	η	30	34	—	%
Intermodulation Distortion ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1990.0 \text{ MHz}$, $f_2 = 1990.1 \text{ MHz}$)	IMD	— —	–31 –31	–28 –27	dB
Input Return Loss ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1990.0 \text{ MHz}$, $f_2 = 1990.1 \text{ MHz}$)	IRL	9	12	—	dB
Common–Source Amplifier Power Gain ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1930.0 \text{ MHz}$, $f_2 = 1930.1 \text{ MHz}$)	G_{ps}	—	11.7	—	dB
Drain Efficiency ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1930.0 \text{ MHz}$, $f_2 = 1930.1 \text{ MHz}$)	η	—	34	—	%
Intermodulation Distortion ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1930.0 \text{ MHz}$, $f_2 = 1930.1 \text{ MHz}$)	IMD	—	–31	—	dB
Input Return Loss ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W PEP}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1930.0 \text{ MHz}$, $f_2 = 1930.1 \text{ MHz}$)	IRL	—	14	—	dB
Power Output, 1 dB Compression Point ($V_{DD} = 26 \text{ Vdc}$, CW, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1990.0 \text{ MHz}$)	P_{1dB}	—	120	—	Watts
Common–Source Amplifier Power Gain ($V_{DD} = 26 \text{ Vdc}$, $P_{out} = 120 \text{ W CW}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $f_1 = 1990.0 \text{ MHz}$)	G_{ps}	—	11	—	dB

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 120\text{ W CW}$, $I_{DQ} = 2 \times 500\text{ mA}$, $f_1 = 1990.0\text{ MHz}$)	η	—	45	—	%
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 120\text{ W CW}$, $I_{DQ} = 2 \times 500\text{ mA}$, $f = 1990\text{ MHz}$, $V_{SWR} = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

- (1) Each side of device measured separately.
(2) Device measured in push-pull configuration.



B1, B2	Ferrite Bead, Fair Rite	Z2	0.320" x 0.080" Microstrip
C1, C2	0.6 – 4.5 pF, Variable Capacitor, Johanson Gigatrim	Z4, Z5	1.050" x 0.080" Microstrip
C3, C4, C9, C10	10 pF, B Case Chip Capacitor, ATC	Z6, Z7	0.120" x 0.080" Microstrip
C5, C12	0.4 – 2.5 pF, Variable Capacitor, Johanson Gigatrim	Z8, Z9	0.140" x 0.080" Microstrip
C6, C7	2.0 pF, B Case Chip Capacitor, ATC	Z10, Z11	0.610" x 0.080" Microstrip
C8	1.1 pF, B Case Chip Capacitor, ATC	Z12, Z13	0.135" x 0.080" Microstrip
C11	0.1 pF, B Case Chip Capacitor, ATC	Z14, Z15	0.130" x 0.080" Microstrip
C13, C20, C29, C37	5.1 pF, B Case Chip Capacitor, ATC	Z16, Z17	0.300" x 0.350" Microstrip
C14, C21, C28, C38	91 pF, B Case Chip Capacitor, ATC	Z18, Z19	0.150" x 0.500" Microstrip
C15, C22, C31, C40	100 μF, 50 V, Electrolytic Capacitor, Sprague	Z20, Z21	0.075" x 0.500" Microstrip
C16, C23, C33, C43	0.039 μF, B Case Chip Capacitor, ATC	Z22, Z23	0.330" x 0.500" Microstrip
C17, C24, C32, C41	1000 pF, B Case Chip Capacitor, ATC	Z24, Z25	0.100" x 0.550" Microstrip
C19, C25	0.020 μF, B Case Chip Capacitor, ATC	Z26, Z27	0.175" x 0.550" Microstrip
C27, C34, C36, C42	22 μF, 35 V, Tantalum Surface Mount Chip Capacitor, Kemet	Z28, Z29	0.045" x 0.550" Microstrip
C30, C39	1.0 μF, 35 V, Tantalum Surface Mount Chip Capacitor, Kemet	Z30, Z31	0.190" x 0.325" Microstrip
C35, C44	470 μF, 63 V, Electrolytic Capacitor, Sprague	Z32, Z33	0.080" x 0.325" Microstrip
Coax1, Coax2	25 Ω, Semi Rigid Coax, 70 mil OD, 1.05" Long	Z34, Z35	0.515" x 0.080" Microstrip
Coax3, Coax4	50 Ω, Semi Rigid Coax, 85 mil OD, 1.05" Long	Z36, Z37	0.020" x 0.080" Microstrip
L1	5.0 nH, Minispring Inductor, Coilcraft	Z38, Z39	0.565" x 0.080" Microstrip
L2	8.0 nH, Minispring Inductor, Coilcraft	Z40	0.100" x 0.080" Microstrip
L3, L4	5.60 nH, Microspring Inductor, Coilcraft	Z41	0.470" x 0.080" Microstrip
R1, R2	1 kΩ, Fixed Metal Film Resistor, 1/2 W, Dale	Z42	0.100" x 0.080" Microstrip
R3, R4	270 Ω, Fixed Film Chip Resistor, 1/8 W, Dale	Board Material	0.03" Teflon®, ε _r = 2.55 Copper Clad, 2 oz. Cu
R5, R6	1.0 kΩ, Fixed Film Chip Resistor, 1/8 W, Dale	Connectors	N-Type Panel Mount, Stripline
Z1	0.150" x 0.080" Microstrip		

Figure 1. 1.93 – 1.99 GHz Broadband Test Circuit Schematic

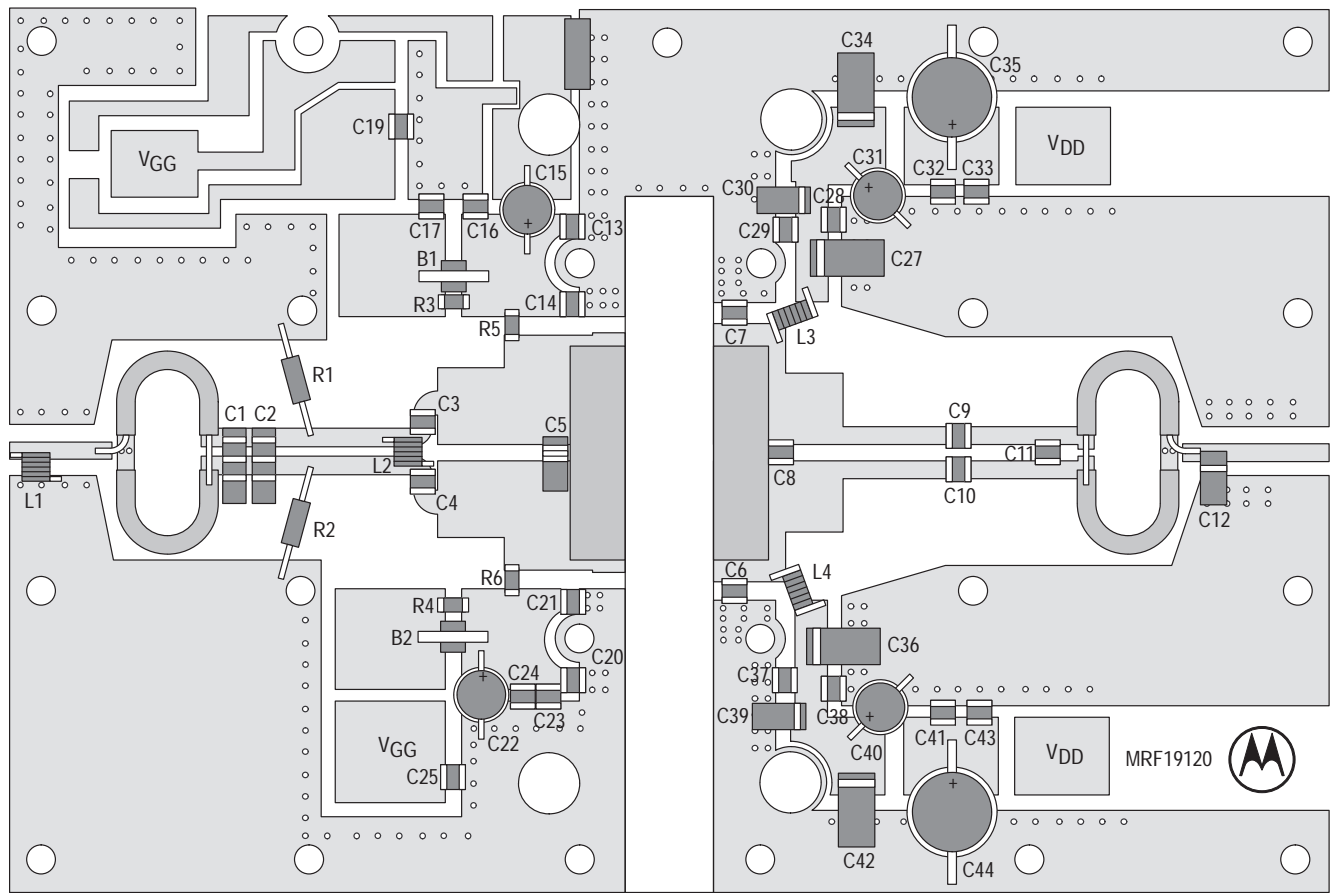


Figure 2. MRF19120 Component Part Layout

TYPICAL CHARACTERISTICS

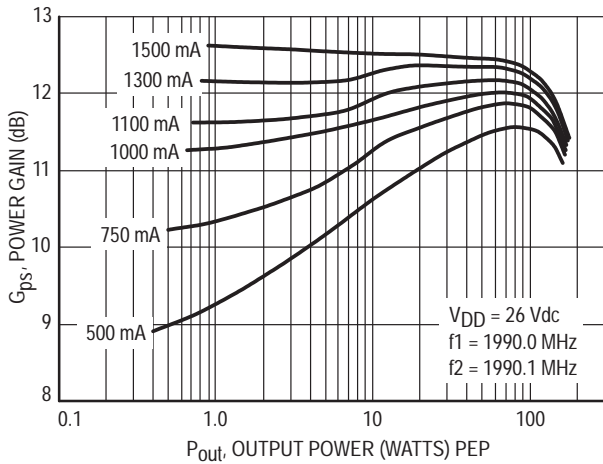


Figure 3. Power Gain versus Output Power

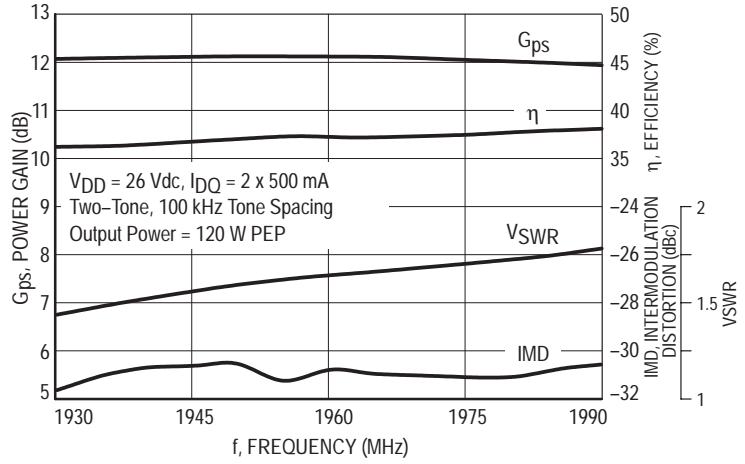


Figure 4. Class AB Broadband Circuit Performance

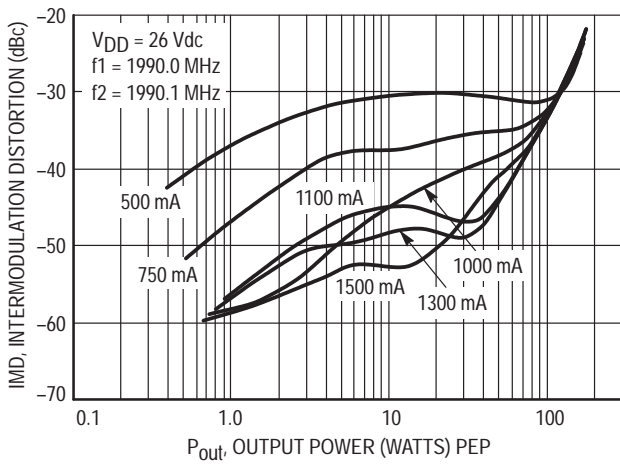


Figure 5. Intermodulation Distortion versus Output Power

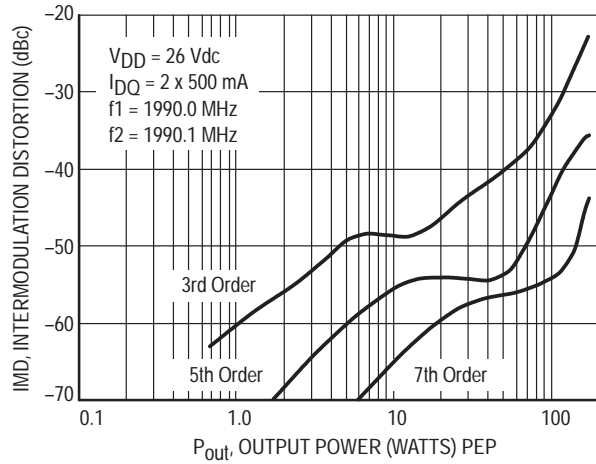


Figure 6. Intermodulation Distortion Products versus Output Power

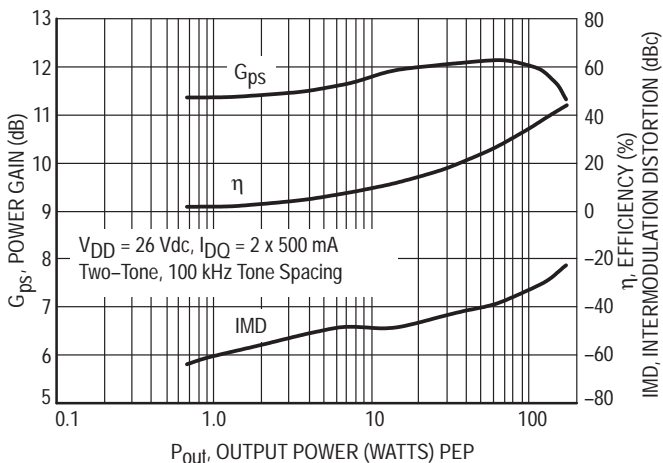


Figure 7. Power Gain, Efficiency, and IMD versus Output Power

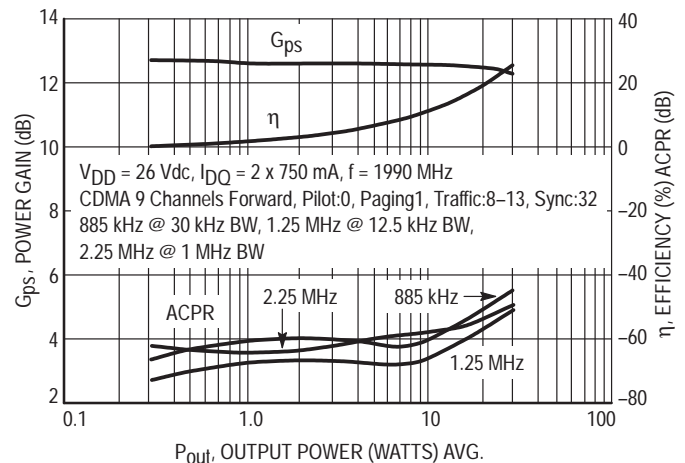
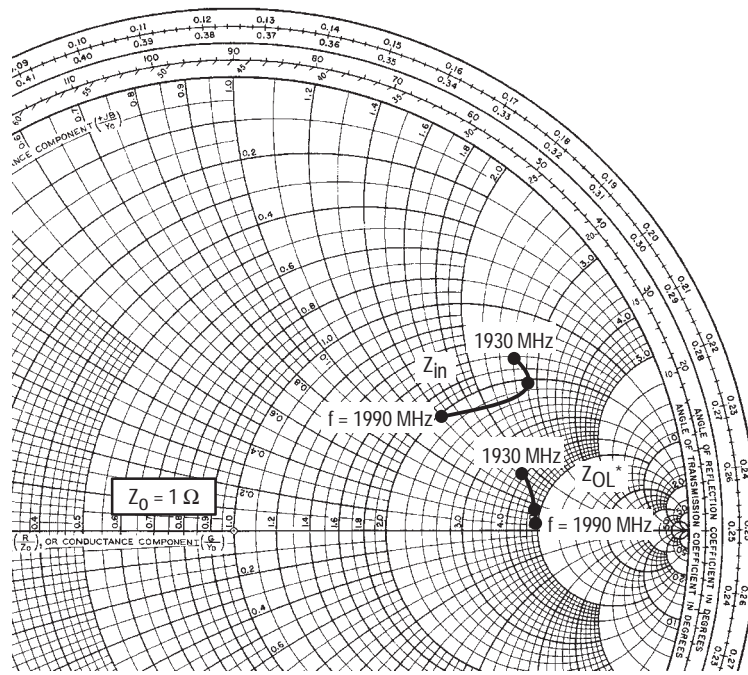


Figure 8. Power Gain, Efficiency, and ACPR versus Output Power



$V_{DD} = 26\text{ V}$, $I_{DQ} = 2 \times 500\text{ mA}$, $P_{out} = 120\text{ Watts PEP}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1930	$1.64 + j2.6$	$3.9 + j1.7$
1960	$2.10 + j2.8$	$4.8 + j0.8$
1990	$2.10 + j1.4$	$4.9 + j0.3$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

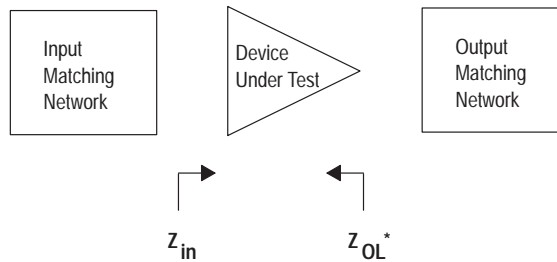


Figure 9. Series Equivalent Input and Output Impedance

The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

MRF19125
MRF19125S

Designed for PCN and PCS base station applications at frequencies from 1.9 to 2.0 GHz. Suitable for TDMA, CDMA and multicarrier amplifier applications.

1990 MHz, 125 W, 26 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs

- Typical 2-Carrier N-CDMA Performance for $V_{DD} = 26$ Volts, $I_{DQ} = 1300$ mA, $f_1 = 1958.75$ MHz, $f_2 = 1961.25$ MHz IS-95 CDMA (Pilot, Sync, Paging, Traffic Codes 8 Through 13) 1.2288 MHz Channel Bandwidth Carrier. Adjacent Channels Measured over a 30 kHz Bandwidth at $f_1 - 885$ kHz and $f_2 + 885$ kHz. Distortion Products Measured over 1.2288 MHz Bandwidth at $f_1 - 2.5$ MHz and $f_2 + 2.5$ MHz. Peak/Avg. = 9.8 dB @ 0.01% Probability on CCDF.

Output Power — 24 Watts Avg.

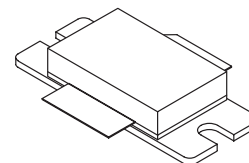
Power Gain — 13.6 dB

Efficiency — 22%

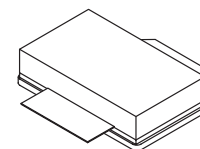
ACPR — -51 dB

IM3 — -37.0 dBc

- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 5:1 VSWR, @ 26 Vdc, 1990 MHz, 125 Watts (CW) Output Power
- Excellent Thermal Stability



CASE 465B-02, STYLE 1
(MRF19125)



CASE 465C-01, STYLE 1
(MRF19125S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	330 1.89	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.53	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc

ON CHARACTERISTICS

Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$)	g_{fs}	—	9	—	S
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 26\text{ Vdc}$, $I_D = 1300\text{ mAdc}$)	$V_{GS(Q)}$	2.5	3.9	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 3\text{ Adc}$)	$V_{DS(on)}$	—	0.185	0.21	Vdc

DYNAMIC CHARACTERISTICS

Reverse Transfer Capacitance (1) ($V_{DS} = 26\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	5.4	—	pF
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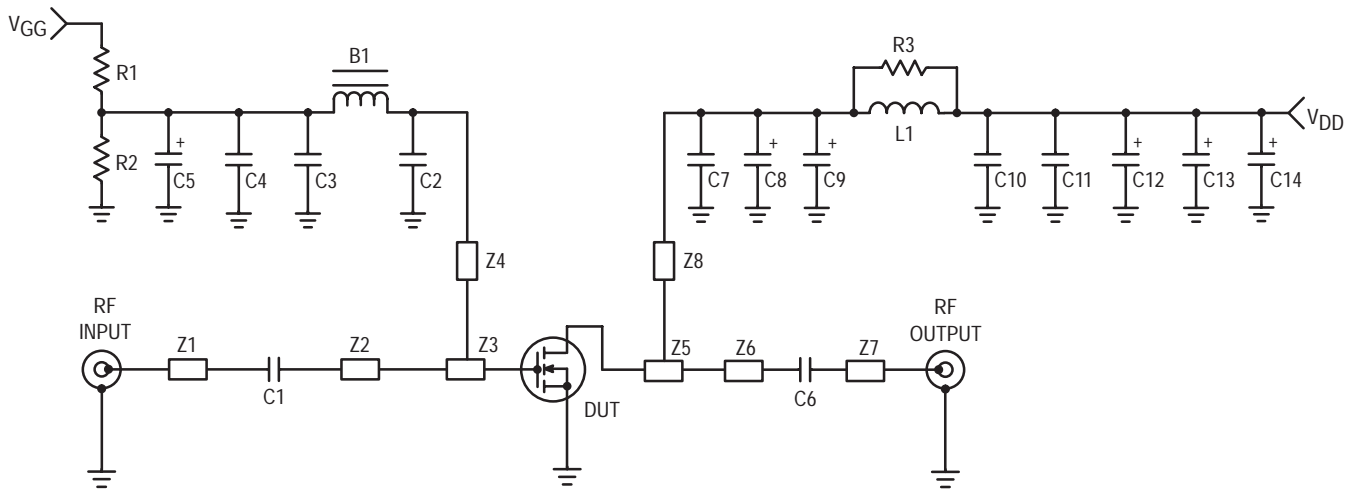
FUNCTIONAL TESTS (In Motorola Test Fixture) 2–Carrier N–CDMA, 1.2288 MHz Channel Bandwidth Carriers. Peak/Avg = 9.8 dB @ 0.01% Probability on CCDF.

Common–Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 24\text{ W Avg}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$)	G_{ps}	12	13.5	—	dB
Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 24\text{ W Avg}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$)	η	19	22	—	%
Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 24\text{ W Avg}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$; IM3 measured over 1.2288 MHz Bandwidth at $f_1 - 2.5\text{ MHz}$ and $f_2 + 2.5\text{ MHz}$)	IMD	—	–37	–35	dBc
Adjacent Channel Power Ratio ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 24\text{ W Avg}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$; ACPR measured over 30 kHz Bandwidth at $f_1 - 885\text{ MHz}$ and $f_2 + 885\text{ MHz}$)	ACPR	—	–51	–47	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 24\text{ W Avg}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1932.5\text{ MHz}$ and $f_1 = 1987.5\text{ MHz}$, $f_2 = 1990\text{ MHz}$)	IRL	—	–13	–9	dB
Output Mismatch Stress ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 125\text{ W CW}$, $I_{DQ} = 1300\text{ mA}$, $f = 1930\text{ MHz}$, VSWR = 5:1, All Phase Angles at Frequency of Test)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 125\text{ W PEP}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1990\text{ MHz}$, Tone Spacing = 100 kHz)	G_{ps}	—	13.5	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 125\text{ W PEP}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1990\text{ MHz}$, Tone Spacing = 100 kHz)	η	—	35	—	%
Third Order Intermodulation Distortion ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 125\text{ W PEP}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1990\text{ MHz}$, Tone Spacing = 100 kHz)	IMD	—	-30	—	dBc
Input Return Loss ($V_{DD} = 26\text{ Vdc}$, $P_{out} = 125\text{ W PEP}$, $I_{DQ} = 1300\text{ mA}$, $f_1 = 1930\text{ MHz}$, $f_2 = 1990\text{ MHz}$, Tone Spacing = 100 kHz)	IRL	—	-13	—	dB
P_{out} , 1 dB Compression Point ($V_{DD} = 26\text{ Vdc}$, $I_{DQ} = 1300\text{ mA}$, $f = 1990\text{ MHz}$)	P1dB	—	130	—	W



Z1, Z7	0.500" x 0.084" Transmission Line	Board	0.030" Glass Teflon [®] ,
Z2	1.105" x 0.084" Transmission Line	PCB	Keene GX-0300-55-22, $\epsilon_r = 2.55$
Z3	0.360" x 0.895" Transmission Line		Etched Circuit Boards
Z4	0.920" x 0.048" Transmission Line		MRF19125 Rev. 5, CMR
Z5	0.605" x 1.195" Transmission Line		
Z6	0.800" x 0.084" Transmission Line		
Z8	0.660" x 0.095" Transmission Line		

Figure 1. MRF19125 Test Circuit Schematic

Table 1. MRF19125 Component Designations and Values

Designators	Description
B1	Short Ferrite Bead, Fair Rite, #2743019447
C1	51 pF Chip Capacitor, ATC #100B510JCA500X
C2, C7	5.1 pF Chip Capacitors, ATC #100B5R1JCA500X
C3, C10	1000 pF Chip Capacitors, ATC #100B102JCA500X
C4, C11	0.1 μ F Chip Capacitors, Kemet #CDR33BX104AKWS
C5	0.1 μ F Tantalum Chip Capacitor, Kemet #T491C105M050
C6	10 pF Chip Capacitor, ATC #100B100JCA500X
C8	10 μ F Tantalum Chip Capacitor, Kemet #T491X106K035AS4394
C9, C12, C13, C14	22 μ F Tantalum Chip Capacitors, Kemet #T491X226K035AS4394
L1	1 Turn, #20 AWG, 0.100" ID, Motorola
N1, N2	Type N Flange Mounts, Omni Spectra #3052-1648-10
R1	1.0 k Ω , 1/8 W Chip Resistor
R2	220 k Ω , 1/8 W Chip Resistor
R3	10 Ω , 1/8 W Chip Resistor

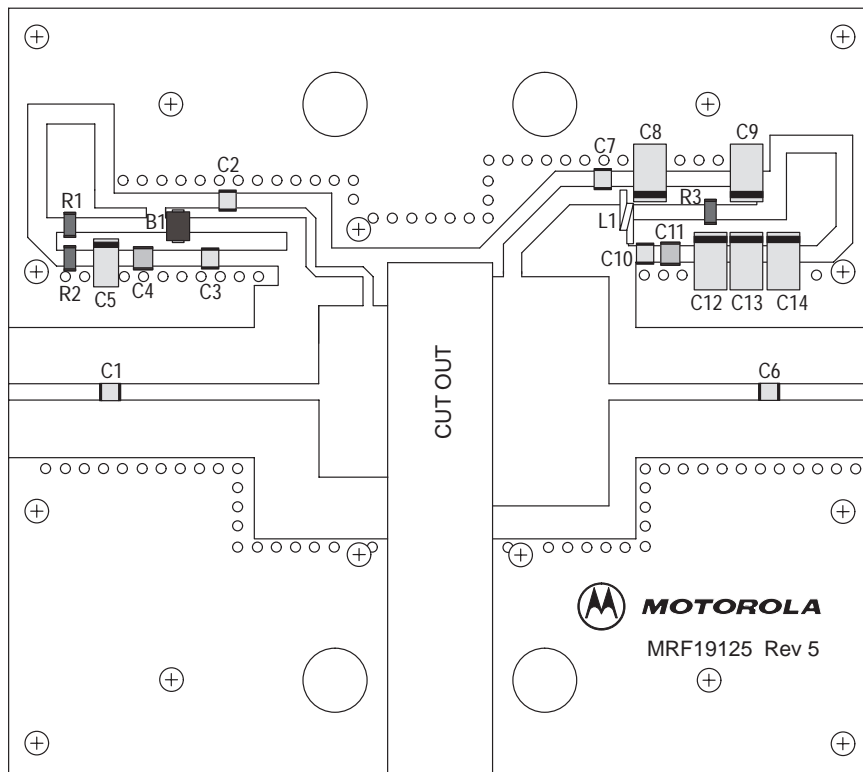


Figure 2. MRF19125 Test Circuit Component Layout

TYPICAL CHARACTERISTICS

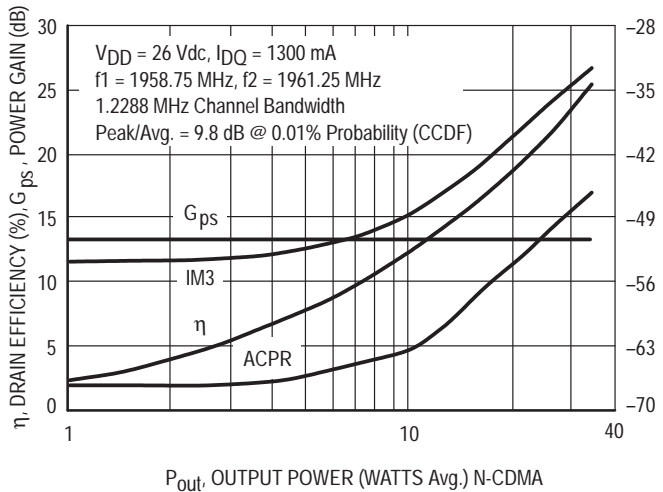


Figure 3. 2-Carrier CDMA ACPR, IM3, Power Gain and Drain Efficiency versus Output Power

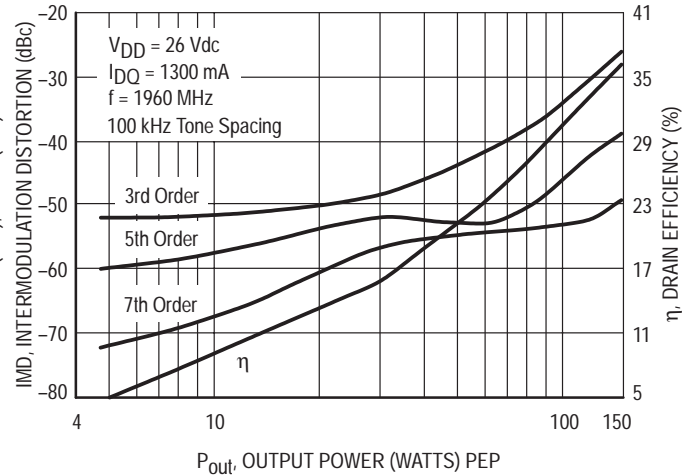


Figure 4. Intermodulation Distortion Products versus Output Power

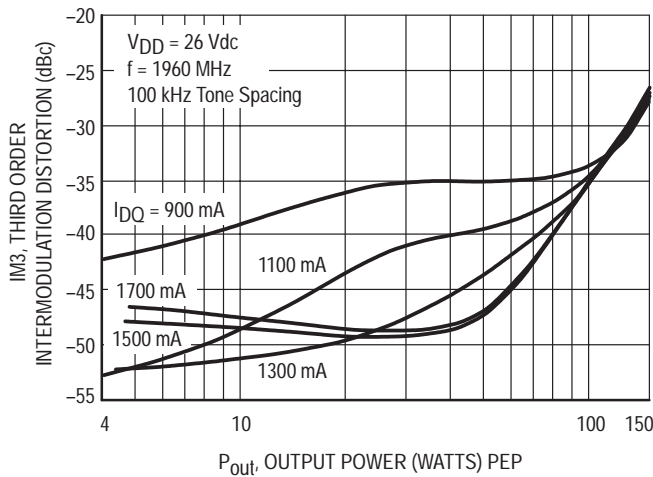


Figure 5. Third Order Intermodulation Distortion versus Output Power

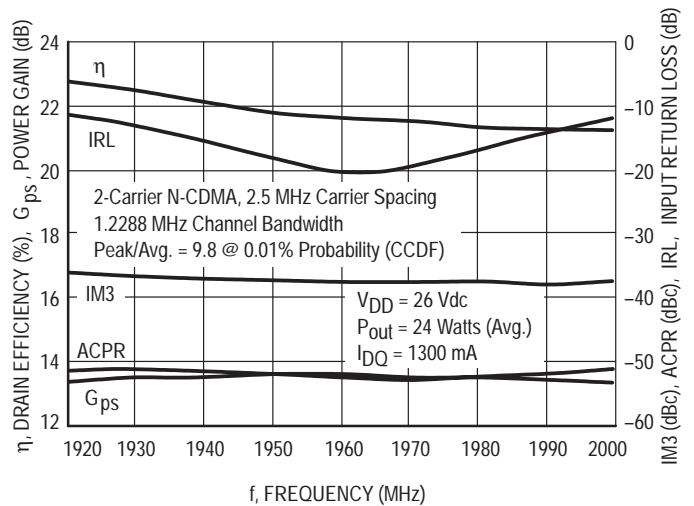


Figure 6. 2-Carrier N-CDMA Broadband Performance

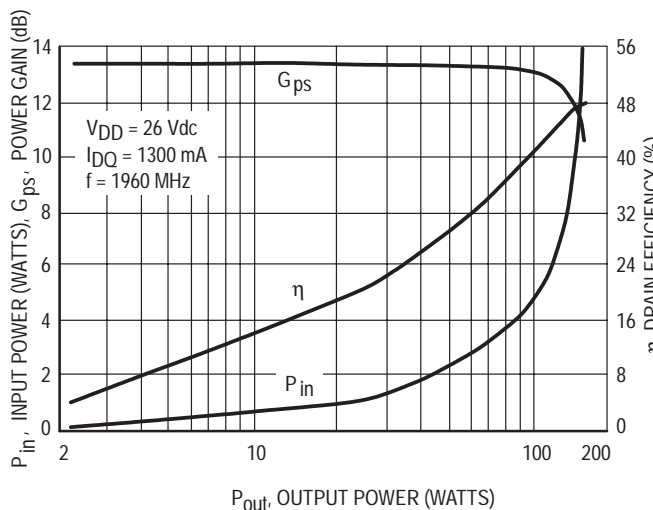


Figure 7. CW Performance

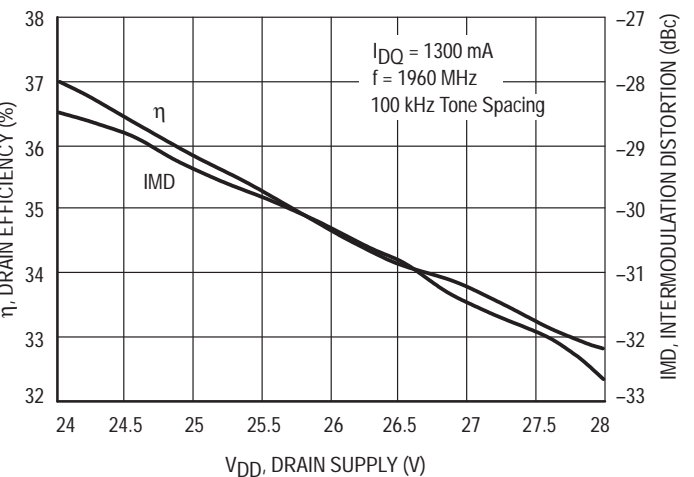


Figure 8. Two-Tone Intermodulation Distortion and Drain Efficiency versus Drain Supply

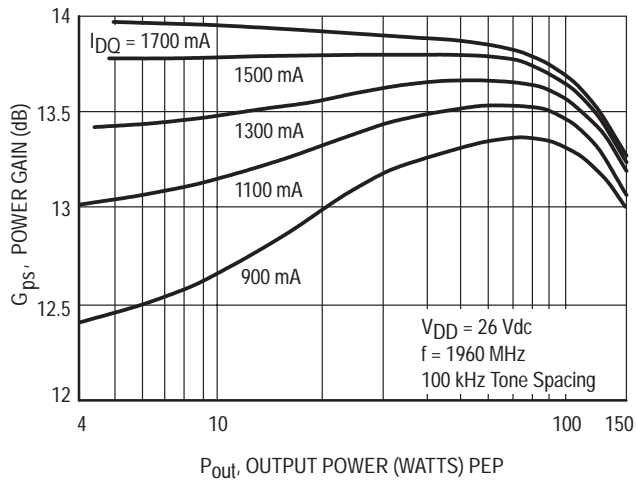


Figure 9. Two-Tone Power Gain versus Output Power

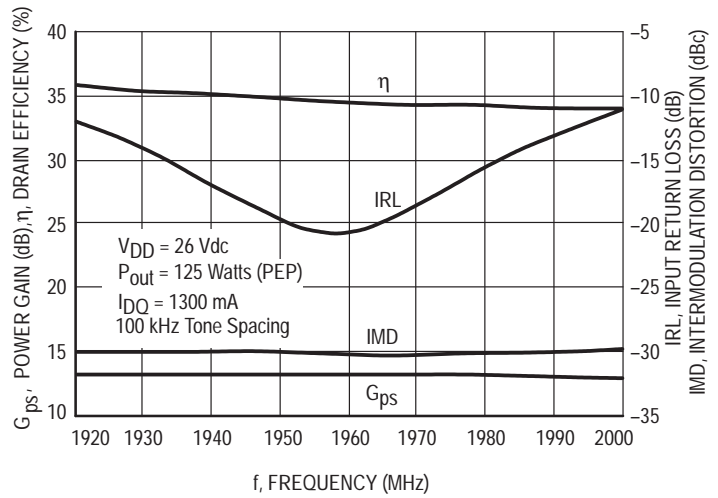


Figure 10. Two-Tone Broadband Performance

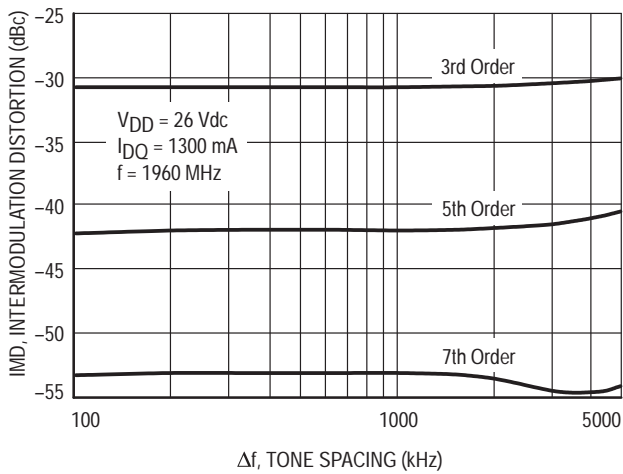


Figure 11. Intermodulation Distortion Products versus Two-Tone Tone Spacing

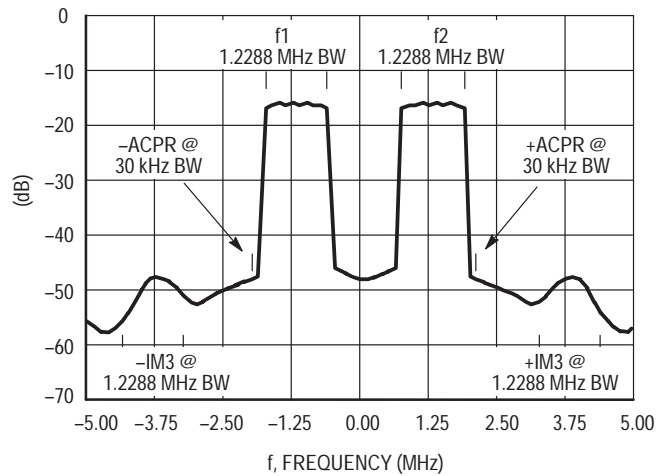
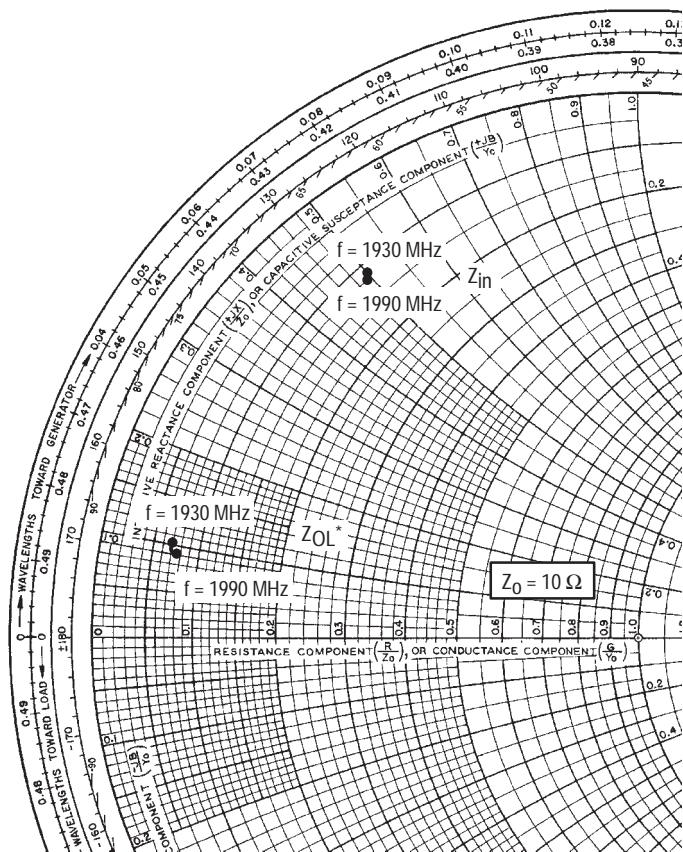


Figure 12. 2-Carrier N-CDMA Spectrum



$V_{DD} = 26\text{ V}$, $I_{DQ} = 1300\text{ mA}$, $P_{Out} = 24\text{ W (Avg.)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1930	$1.43 + j5.01$	$0.75 + j0.93$
1960	$1.51 + j4.88$	$0.71 + j0.89$
1990	$1.56 + j4.93$	$0.68 + j1.02$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

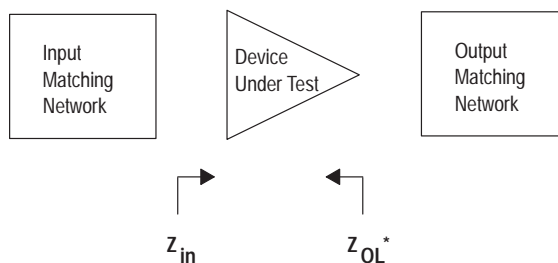


Figure 13. Series Equivalent Input and Output Impedance

The RF Sub-Micron Bipolar Line RF Power Bipolar Transistor

Designed for broadband commercial and industrial applications at frequencies from 1800 to 2000 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common-emitter class AB amplifier applications. Suitable for frequency modulated, amplitude modulated and multi-carrier base station RF power amplifiers.

- Specified 26 Volts, 2.0 GHz, Class AB, Two-Tones Characteristics
 - Output Power — 30 Watts (PEP)
 - Power Gain — 9.8 dB
 - Efficiency — 34%
 - Intermodulation Distortion — -28 dBc
- Typical 26 Volts, 1.88 GHz, Class AB, CW Characteristics
 - Output Power — 30 Watts
 - Power Gain — 11 dB
 - Efficiency — 40%
 - Intermodulation Distortion — -30 dBc
- Excellent Thermal Stability
- Capable of Handling 3:1 VSWR @ 26 Vdc, 2000 MHz, 30 Watts (PEP) Output Power
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- S-Parameter Characterization at High Bias Levels
- Designed for FM, TDMA, CDMA, and Multi-Carrier Applications

Note: Not suitable for class A operation.

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage	V_{CEO}	25	Vdc
Collector-Emitter Voltage	V_{CES}	60	Vdc
Collector-Base Voltage	V_{CBO}	60	Vdc
Collector-Emitter Voltage ($R_{BE} = 100 \Omega$)	V_{CER}	30	Vdc
Emitter-Base Voltage	V_{EB}	-3	Vdc
Collector Current - Continuous	I_C	4	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	125 0.71	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Rating	Symbol	Max	Unit
Thermal Resistance, Junction to Case (1)	$R_{\theta JC}$	1.4	$^\circ\text{C}/\text{W}$

(1) Thermal resistance is determined under specified RF operating condition.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

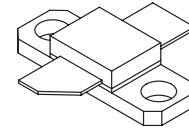
Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector-Emitter Breakdown Voltage ($I_C = 25 \text{ mAdc}$, $I_B = 0$)	$V_{(BR)CEO}$	25	28	—	Vdc
Collector-Emitter Breakdown Voltage ($I_C = 25 \text{ mAdc}$, $V_{BE} = 0$)	$V_{(BR)CES}$	60	70	—	Vdc
Collector-Base Breakdown Voltage ($I_C = 25 \text{ mAdc}$, $I_E = 0$)	$V_{(BR)CBO}$	60	70	—	Vdc

MRF20030R

**30 W, 2.0 GHz
NPN SILICON
BROADBAND
RF POWER TRANSISTOR**

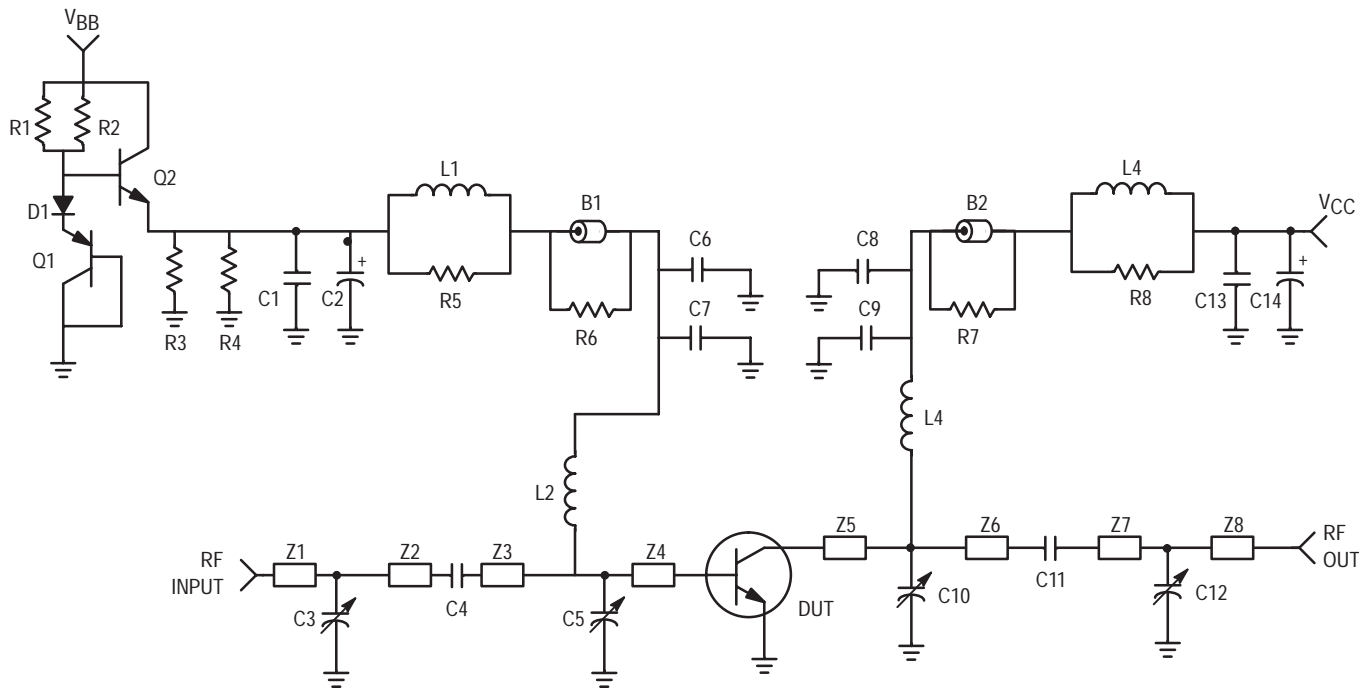


CASE 395C-01, STYLE 1

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Emitter–Base Breakdown Voltage ($I_B = 5\text{ mA}$, $I_C = 0$)	$V_{(BR)EBO}$	3	3.8	—	Vdc
Collector Cutoff Current ($V_{CE} = 30\text{ Vdc}$, $V_{BE} = 0$)	I_{CES}	—	—	10	mAdc
ON CHARACTERISTICS					
DC Current Gain ($V_{CE} = 5\text{ Vdc}$, $I_{CE} = 1\text{ Adc}$)	h_{FE}	20	40	80	—
DYNAMIC CHARACTERISTICS					
Output Capacitance ($V_{CB} = 26\text{ Vdc}$, $I_E = 0$, $f = 1.0\text{ MHz}$) (1)	C_{ob}	—	28	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Emitter Amplifier Power Gain ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $I_{CQ} = 120\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	G_{pe}	9.8	11	—	dB
Collector Efficiency ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 120\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	η	34	38	—	%
Intermodulation Distortion ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 120\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IMD	—	– 30	– 28	dBc
Input Return Loss ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IRL	10	17	—	dB
Load Mismatch ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 120\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$, Load VSWR = 3:1, All Phase Angles at Frequency of Test)	ψ	No Degradation in Output Power			
Common–Emitter Amplifier Power Gain ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	G_{pe}	—	11	—	dB
Collector Efficiency ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	η	—	34	—	%
Intermodulation Distortion ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	IMD	—	– 32	—	dBc
Input Return Loss ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts (PEP)}$, $I_{CQ} = 125\text{ mA}$, $f_1 = 1930.0\text{ MHz}$, $f_2 = 1930.1\text{ MHz}$)	IRL	—	14	—	dB
GUARANTEED BUT NOT TESTED (In Motorola Test Fixture)					
Common–Emitter Amplifier Power Gain ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $I_{CQ} = 125\text{ mA}$, $f = 1880\text{ MHz}$)	G_{pe}	—	10.5	—	dB
Collector Efficiency ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $I_{CQ} = 125\text{ mA}$, $f = 1880\text{ MHz}$)	η	—	40	—	%
Input Return Loss ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $I_{CQ} = 125\text{ mA}$, $f = 1880\text{ MHz}$)	IRL	—	14	—	dB
Output Mismatch Stress ($V_{CC} = 25\text{ Vdc}$, $P_{out} = 30\text{ Watts}$, $I_{CQ} = 125\text{ mA}$, $f = 1880\text{ MHz}$, VSWR = 3:1, All Phase Angles at Frequency of Test)	ψ	Typically No Degradation in Output Power			

(1) For Information Only. This Part Is Collector Matched.



B1, B2	Ferrite Bead, P/N 5659065/3B, Ferroxcube	N1, N2	Type N Flange Mount RF Connector MA/COM 3052-1648-10
C1, C13	0.1 μ F, Chip Capacitor, Kermet	R1, R2	130 Ω , 1/8 W Chip Resistor, Rohm
C2	100 μ F, 50 V, Electrolytic Capacitor, Mallory	R3, R4	100 Ω , 1/8 W Chip Resistor, Rohm
C3, C5, C12	0.6–4 pF, Variable Capacitor, Johanson, Gigatrim	R5, R8	10 Ω , 1/2 W Resistor
C4, C11	10 pF, B Case Chip Capacitor, ATC	R6, R7	10 Ω , 1/8 W Chip Resistor, Rohm (10J)
C6, C8	24 pF, B Case Chip Capacitor, ATC	Q1	Transistor, PNP Motorola (BD136)
C7, C9	75 pF, B Case Chip Capacitor, ATC	Q2	Transistor, NPN Motorola (MJD47)
C10	0.4–2.5 pF, Variable Capacitor, Johanson, Gigatrim	Board	30 Mil Glass Teflon [®] , Arlon GX-0300-55-22, $\epsilon_r = 2.55$
C14	470 μ F, 63 V, Electrolytic Capacitor, Mallory		
D1	Diode, Motorola (MUR3160T3)		
L1, L4	12 Turns, 22 AWG, IDIA. 0.195"		
L2, L3	0.750" 20 AWG		

Figure 1. Class AB Test Fixture Electrical Schematic

TYPICAL CHARACTERISTICS

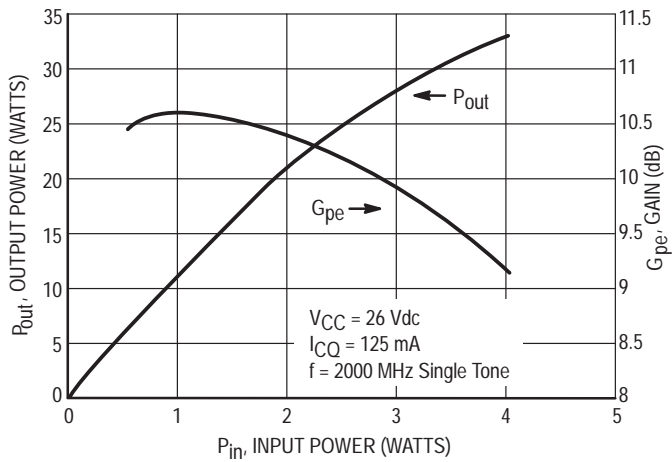


Figure 2. Output Power & Power Gain versus Input Power

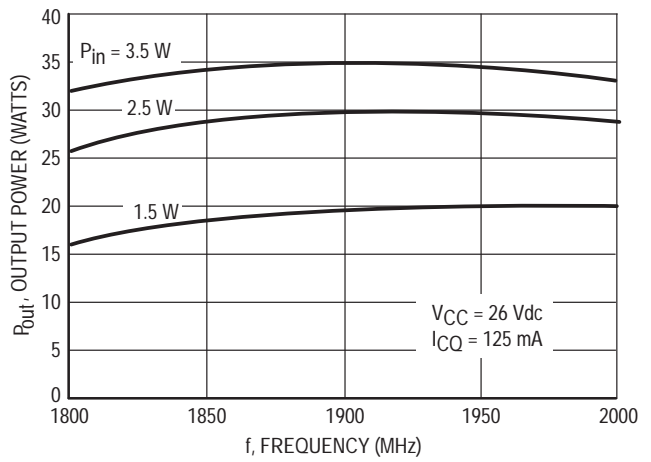


Figure 3. Output Power versus Frequency

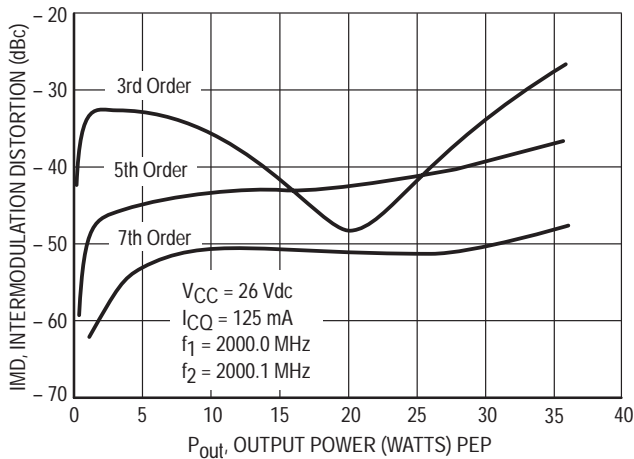


Figure 4. Intermodulation Distortion versus Output Power

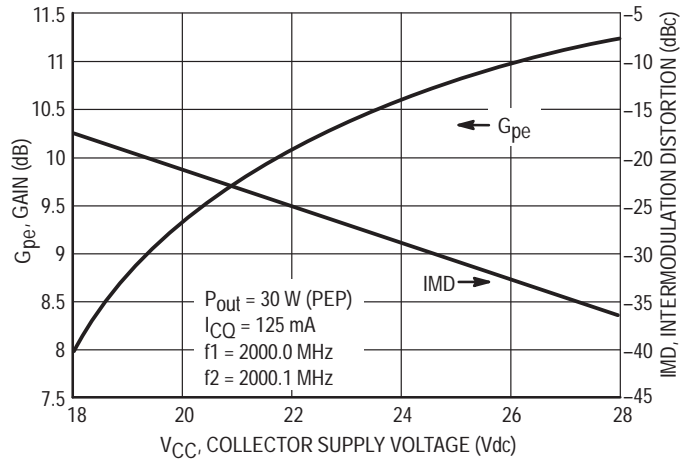


Figure 5. Power Gain and Intermodulation Distortion versus Supply Voltage

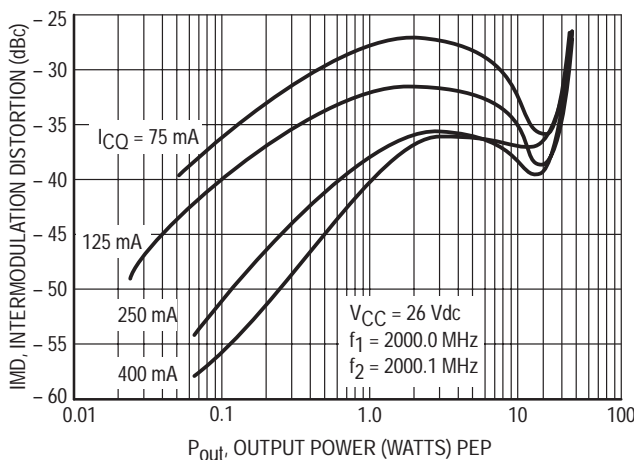


Figure 6. Intermodulation Distortion versus Output Power

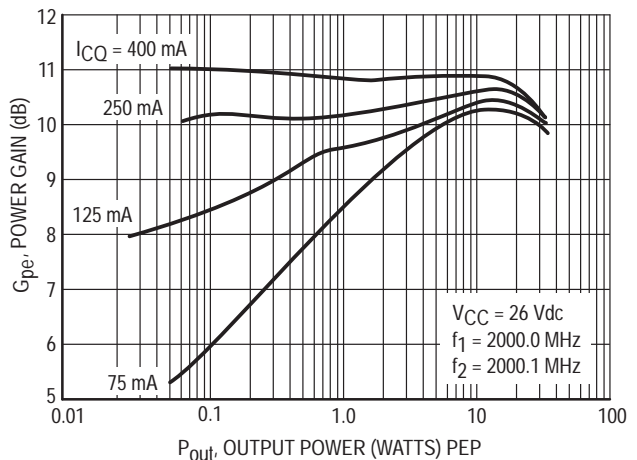


Figure 7. Power Gain versus Output Power

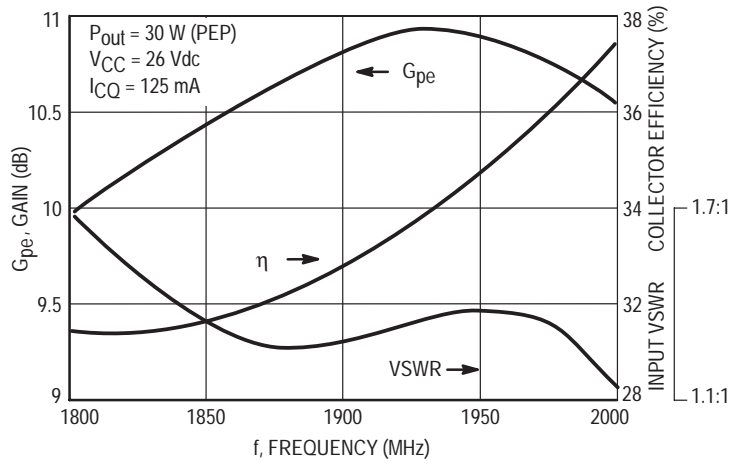
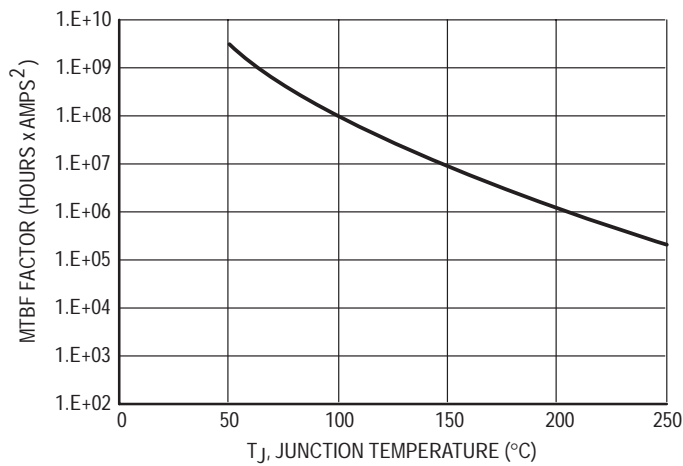
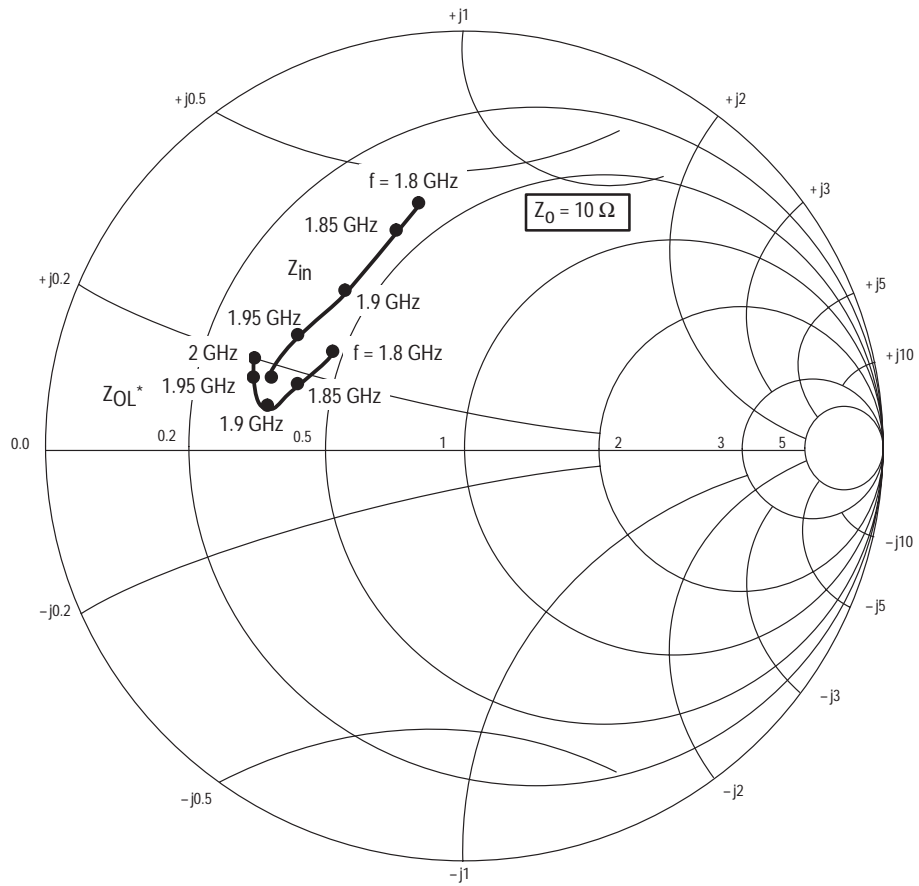


Figure 8. Performance in Broadband Circuit



This above graph displays calculated MTBF in hours x ampere² emitter current. Life tests at elevated temperatures have correlated to better than $\pm 10\%$ of the theoretical prediction for metal failure. Divide MTBF factor by I_C^2 for MTBF in a particular application.

Figure 9. MTBF Factor versus Junction Temperature



$V_{CC} = 26 \text{ V}$, $I_{CQ} = 125 \text{ mA}$, $P_{out} = 30 \text{ W (PEP)}$

f MHz	$Z_{in(1)}$ Ω	Z_{OL}^* Ω
1800	$4.5 + j7.0$	$4.7 + j2.4$
1850	$4.5 + j6.0$	$4.4 + j1.6$
1900	$4.5 + j4.6$	$3.4 + j1.2$
1950	$3.7 + j2.4$	$3.3 + j1.6$
2000	$3.5 + j1.5$	$3.5 + j2.0$

$Z_{in(1)}$ = Conjugate of fixture base impedance.

Z_{OL}^* = Conjugate of the optimum load impedance at given output power, voltage, bias current and frequency.

Figure 10. Series Equivalent Input and Output Impedance

Table 1. Common Emitter S-Parameters at $V_{CE} = 24$ Vdc, $I_C = 1.8$ Adc

f GHz	S11		S21		S12		S22	
	S11	ϕ	S21	ϕ	S12	ϕ	S22	ϕ
1.5	.964	158	.65	74	.046	60	.859	161
1.55	.960	156	.74	68	.047	56	.841	161
1.6	.952	155	.87	60	.049	53	.815	160
1.65	.933	153	1.05	50	.048	46	.787	161
1.7	.892	149	1.32	35	.047	40	.744	163
1.75	.804	149	1.64	13	.040	29	.719	168
1.8	.727	157	1.78	-18	.026	21	.778	175
1.85	.787	163	1.50	-50	.015	54	.883	174
1.9	.873	163	1.14	-73	.020	81	.937	171
1.95	.921	160	.84	-89	.026	88	.949	168
2	.941	157	.62	-102	.031	93	.950	165
2.05	.943	155	.48	-109	.036	93	.946	164
2.1	.940	153	.38	-118	.040	92	.942	163
2.15	.928	151	.30	-127	.042	97	.939	162
2.2	.917	150	.24	-133	.049	99	.935	161
2.25	.907	150	.20	-140	.056	101	.933	160
2.3	.888	148	.17	-150	.066	100	.926	159
2.35	.861	148	.14	-159	.077	98	.916	157
2.4	.853	149	.11	-167	.087	92	.909	157
2.45	.860	146	.10	-176	.095	89	.900	155
2.5	.880	146	.10	156	.119	84	.880	155

The RF Sub-Micron Bipolar Line RF Power Bipolar Transistors

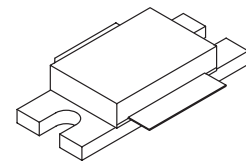
The MRF20060R and MRF20060RS are designed for class AB broadband commercial and industrial applications at frequencies from 1800 to 2000 MHz. The high gain, excellent linearity and broadband performance of these devices make them ideal for large-signal, common emitter class AB amplifier applications. These devices are suitable for frequency modulated, amplitude modulated and multi-carrier base station RF power amplifiers.

- Guaranteed Two-tone Performance at 2000 MHz, 26 Volts
Output Power — 60 Watts (PEP)
Power Gain — 9 dB
Efficiency — 33%
Intermodulation Distortion — -30 dBc
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- S-Parameter Characterization at High Bias Levels
- Excellent Thermal Stability
- Capable of Handling 3:1 VSWR @ 26 Vdc, 2000 MHz, 60 Watts (PEP) Output Power
- Designed for FM, TDMA, CDMA and Multi-Carrier Applications
- Test Fixtures Available at: <http://mot-sps.com/rf/designtds/>

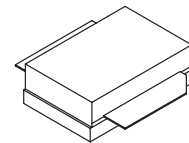
Note: Not suitable for class A operation.

MRF20060R
MRF20060RS

60 W, 2000 MHz
RF POWER
BROADBAND
NPN BIPOLAR



CASE 451-06, STYLE 1
(MRF20060R)



CASE 451A-03, STYLE 1
(MRF20060RS)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector-Emitter Voltage ($I_B = 0$ mA)	V_{CEO}	25	Vdc
Collector-Emitter Voltage	V_{CES}	60	Vdc
Collector-Base Voltage	V_{CBO}	60	Vdc
Collector-Emitter Voltage ($R_{BE} = 100$ Ohm)	V_{CER}	30	Vdc
Base-Emitter Voltage	V_{EB}	- 3	Vdc
Collector Current - Continuous	I_C	8	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	250 1.43	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	- 65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

THERMAL CHARACTERISTICS

Rating	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.7	$^\circ\text{C/W}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector–Emitter Breakdown Voltage ($I_C = 50\text{ mA}$, $I_B = 0$)	$V_{(BR)CEO}$	25	28	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 50\text{ mA}$, $V_{BE} = 0$)	$V_{(BR)CES}$	60	69	—	Vdc
Collector–Base Breakdown Voltage ($I_C = 50\text{ mA}$, $I_E = 0$)	$V_{(BR)CBO}$	60	69	—	Vdc
Reverse Base–Emitter Breakdown Voltage ($I_B = 10\text{ mA}$, $I_C = 0$)	$V_{(BR)EBO}$	3	3.5	—	Vdc
Zero Base Voltage Collector Leakage Current ($V_{CE} = 30\text{ Vdc}$, $V_{BE} = 0$)	I_{CES}	—	—	10	mAdc

ON CHARACTERISTICS

DC Current Gain ($V_{CE} = 5\text{ Vdc}$, $I_C = 1\text{ Adc}$)	h_{FE}	20	40	80	—
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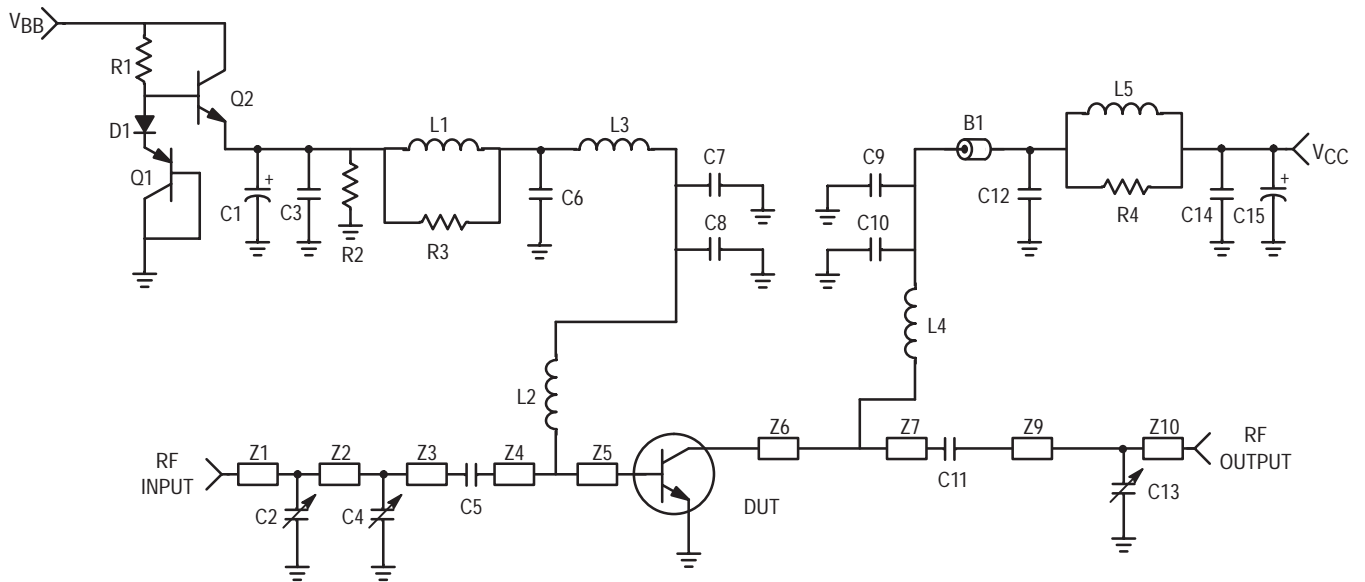
DYNAMIC CHARACTERISTICS

Output Capacitance ($V_{CB} = 26\text{ Vdc}$, $I_E = 0$, $f = 1.0\text{ MHz}$) (1)	C_{ob}	—	55	—	pF
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FUNCTIONAL TESTS (In Motorola Test Fixture)

Common–Emitter Amplifier Power Gain ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 60\text{ Watts (PEP)}$, $I_{CQ} = 200\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	G_{pe}	9	9.8	—	dB
Collector Efficiency ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 60\text{ Watts (PEP)}$, $I_{CQ} = 200\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	η	33	35	—	%
Intermodulation Distortion ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 60\text{ Watts (PEP)}$, $I_{CQ} = 200\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IMD	—	– 32	– 30	dB
Input Return Loss ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 60\text{ Watts (PEP)}$, $I_{CQ} = 200\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$)	IRL	12	19	—	dB
Output Mismatch Stress ($V_{CC} = 26\text{ Vdc}$, $P_{out} = 60\text{ Watts (PEP)}$, $I_{CQ} = 200\text{ mA}$, $f_1 = 2000.0\text{ MHz}$, $f_2 = 2000.1\text{ MHz}$, VSWR = 3:1, All Phase Angles at Frequency of Test)	ψ	No Degradation in Output Power			

(1) For Information Only. This Part Is Collector Matched.



B1	Ferrite Bead, P/N 5659065/3B, Ferroxcube	D1	Diode, Motorola (MURS160T3)
C1	100 μ F, 50 V, Electrolytic Capacitor, Mallory	L1, L5	12 Turns, 22 AWG, 0.140" Choke
C2, C4, C13	0.6–4.0 pF, Variable Capacitor, Gigatrim, Johanson	L2, L4	.5 inch of 20 AWG
C3, C14	0.1 μ F, Chip Capacitor, Kermit	L3	12.5 nH Inductor
C5	15 pF, B Case Chip Capacitor, ATC	R1	2 x 130 Ω , 1/8 W Chip Resistor, Rohm
C6, C12	1000 pF, B Case Chip Capacitor, ATC	R2	2 x 100 Ω , 1/8 W Chip Resistor, Rohm
C7, C9	91 pF, B Case Chip Capacitor, ATC	R3, R4	10 Ω , 1/2 W, Resistor
C8, C10	24 pF, B Case Chip Capacitor, ATC	Q1	Transistor, PNP Motorola (BD136)
C11	13 pF, B Case Chip Capacitor, ATC	Q2	Transistor, NPN Motorola (MJD47)
C15	470 μ F, 50 V, Electrolytic Capacitor, Mallory	Board	Glass Teflon [®] , Arlon GX-0300-55-22, ϵ_r

Figure 1. 1.93 – 2 GHz Test Fixture Electrical Schematic

TYPICAL CHARACTERISTICS

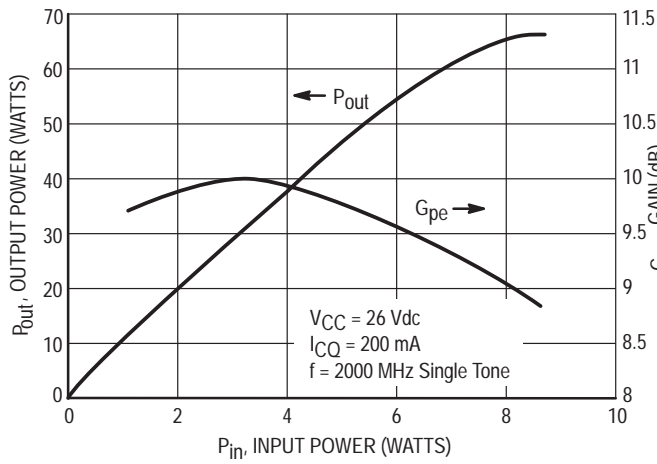


Figure 2. Output Power & Power Gain versus Input Power

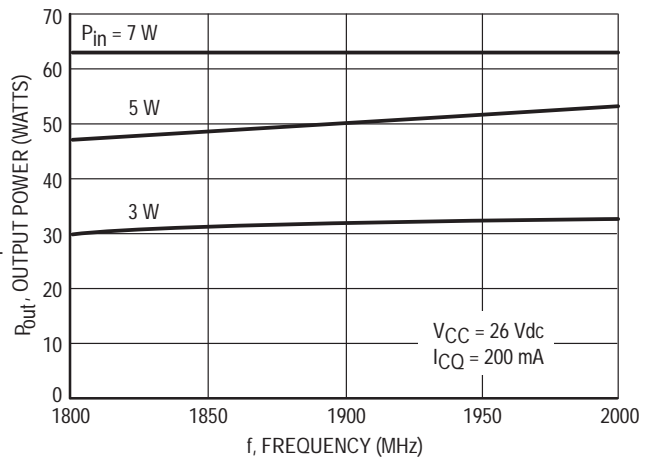


Figure 3. Output Power versus Frequency

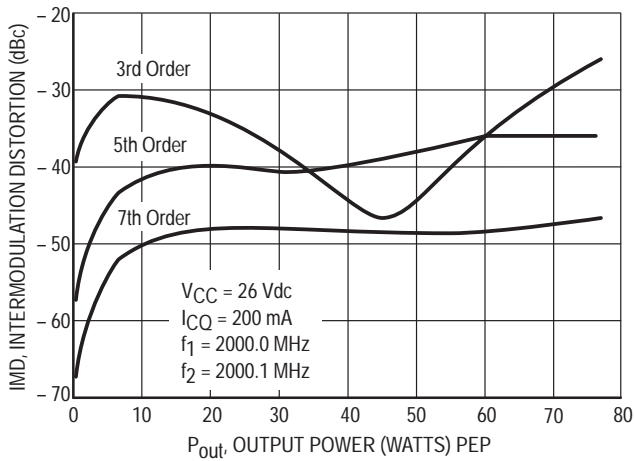


Figure 4. Intermodulation Distortion versus Output Power

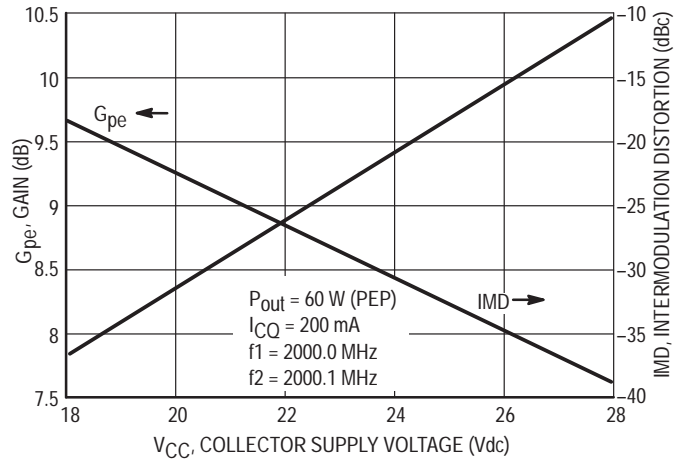


Figure 5. Power Gain and Intermodulation Distortion versus Supply Voltage

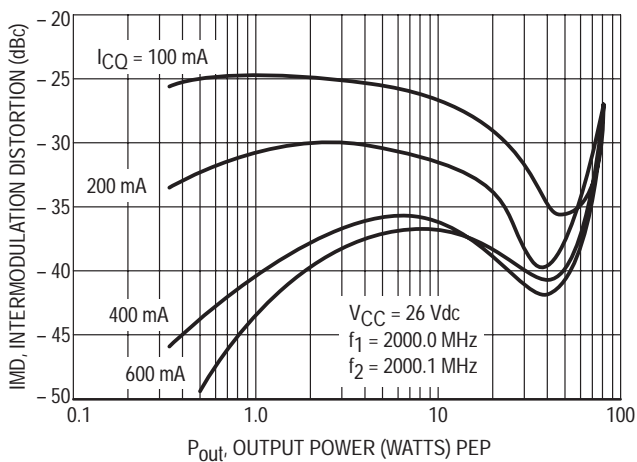


Figure 6. Intermodulation Distortion versus Output Power

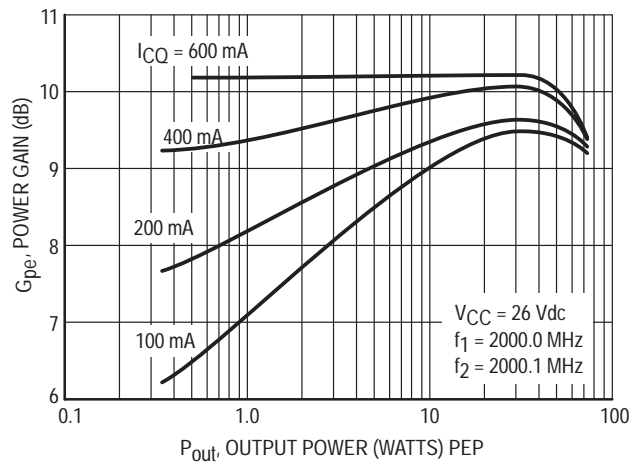


Figure 7. Power Gain versus Output Power

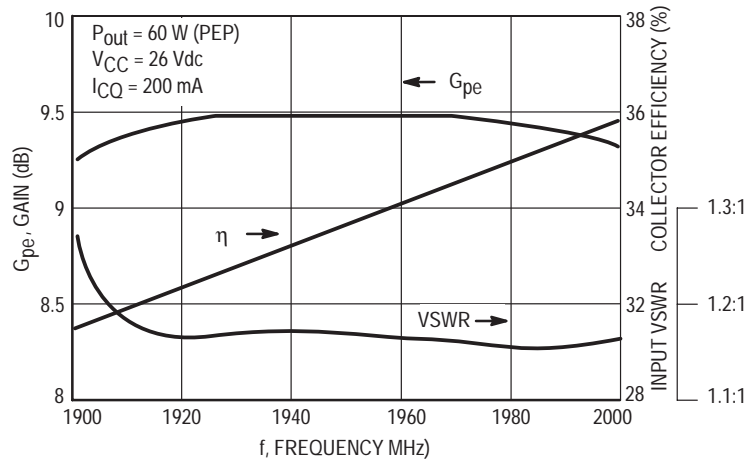
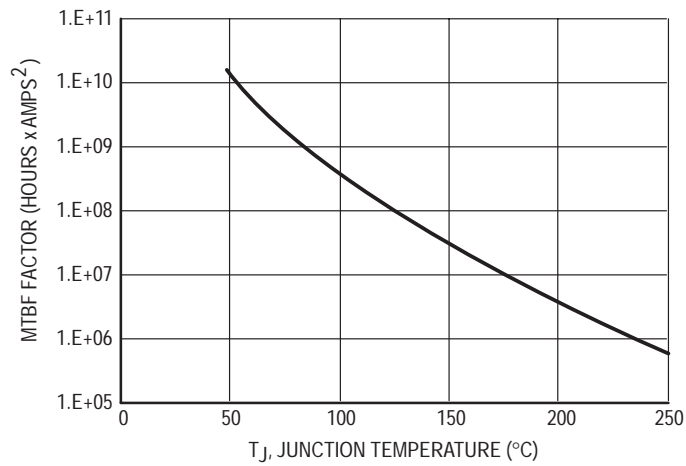
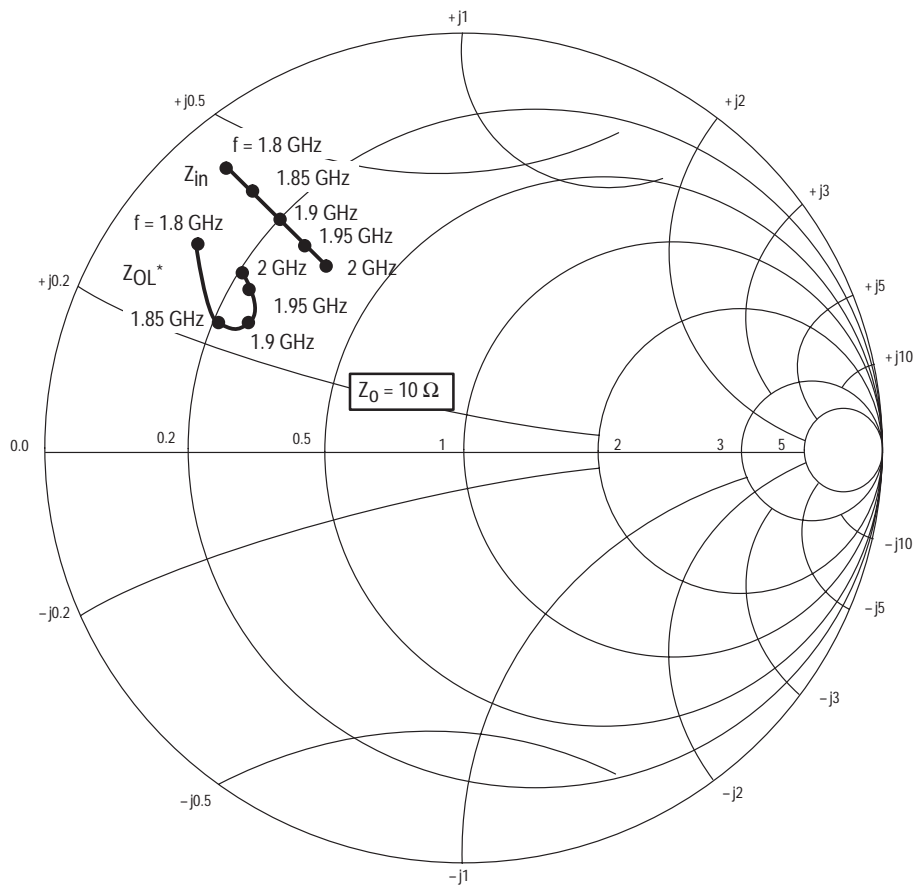


Figure 8. Performance in Broadband Circuit



This above graph displays calculated MTBF in hours x ampere² emitter current. Life tests at elevated temperatures have correlated to better than $\pm 10\%$ of the theoretical prediction for metal failure. Divide MTBF factor by I_C^2 for MTBF in a particular application.

Figure 9. MTBF Factor versus Junction Temperature



$V_{CC} = 26 \text{ V}$, $I_{CQ} = 200 \text{ mA}$, $P_{out} = 60 \text{ W (PEP)}$

f MHz	$Z_{in}(1)$ Ω	Z_{OL}^* Ω
1800	$1.0 + j4.8$	$1.7 + j3.3$
1850	$1.5 + j4.8$	$2.2 + j2.7$
1900	$2.0 + j4.7$	$2.4 + j3.0$
1950	$2.5 + j4.7$	$2.3 + j3.2$
2000	$3.5 + j4.7$	$2.0 + j3.4$

$Z_{in}(1)$ = Conjugate of fixture base terminal impedance.

Z_{OL}^* = Conjugate of the optimum load impedance at given output power, voltage, bias current and frequency.

Figure 10. Series Equivalent Input and Output Impedance

Table 1. Common Emitter S-Parameters at $V_{CE} = 24$ Vdc, $I_C = 3.5$ Adc

f GHz	S11		S21		S12		S22	
	S11	ϕ	S21	ϕ	S12	ϕ	S22	ϕ
1.5	0.986	168	0.32	81	0.031	60	0.923	169
1.55	0.985	167	0.35	76	0.031	63	0.918	169
1.6	0.981	167	0.40	70	0.032	61	0.908	169
1.65	0.973	166	0.45	63	0.030	53	0.897	169
1.7	0.968	165	0.52	56	0.033	50	0.889	168
1.75	0.951	163	0.62	46	0.028	47	0.880	169
1.8	0.914	161	0.76	32	0.027	39	0.871	170
1.85	0.851	161	0.91	12	0.024	26	0.863	171
1.9	0.789	164	1.02	-15	0.015	5	0.888	174
1.95	0.810	170	0.94	-44	0.005	-7	0.931	174
2	0.880	172	0.75	-68	0.006	-151	0.953	172
2.05	0.934	170	0.57	-85	0.010	152	0.967	170
2.1	0.964	168	0.45	-98	0.015	158	0.965	169
2.15	0.977	165	0.36	-109	0.022	164	0.955	168
2.2	0.975	163	0.30	-118	0.033	165	0.950	167
2.25	0.961	161	0.25	-128	0.049	160	0.947	167
2.3	0.942	160	0.22	-139	0.066	149	0.938	166
2.35	0.919	157	0.19	-149	0.077	142	0.931	165
2.4	0.860	156	0.17	-163	0.100	137	0.922	165
2.45	0.821	159	0.15	177	0.128	122	0.914	165
2.5	0.781	161	0.14	157.0	0.156	108	0.907	165

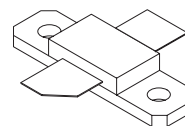
The RF MOSFET Line
RF Power
Field Effect Transistor
N-Channel Enhancement-Mode Lateral MOSFET

Designed for W-CDMA base station applications at frequencies from 2110 to 2170 MHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications. To be used in class AB for PCN-PCS/cellular radio and WLL applications.

- Typical W-CDMA Performance: -45 dBc ACPR, 2140 MHz, 28 Volts, 5 MHz Offset/4.096 MHz BW, 15 DTCH
Output Power — 2.1 Watts
Power Gain — 13.5 dB
Efficiency — 21%
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR @ 28 Vdc, 2170 MHz, 10 Watts CW Output Power
- Excellent Thermal Stability

MRF21010

2170 MHz, 10 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFET



CASE 360B-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	43.75 0.25	W W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M1 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	5.5	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ V}$, $I_D = 10\ \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μA_{dc}
Gate–Source Leakage Current ($V_{GS} = 5\text{ V}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μA_{dc}

ON CHARACTERISTICS

Gate Threshold Voltage ($V_{DS} = 10\text{ V}$, $I_D = 50\ \mu\text{A}$)	$V_{GS(th)}$	2.5	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ V}$, $I_D = 100\text{ mA}$)	$V_{GS(Q)}$	2.5	4	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ V}$, $I_D = 0.5\text{ A}$)	$V_{DS(on)}$	—	0.4	0.5	Vdc
Forward Transconductance ($V_{DS} = 10\text{ V}$, $I_D = 1\text{ A}$)	g_{fs}	—	0.95	—	S

DYNAMIC CHARACTERISTICS

Reverse Transfer Capacitance ($V_{DS} = 28\text{ V}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	1	—	pF
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FUNCTIONAL TESTS (In Motorola Test Fixture)

Two–Tone Common Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 100\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2170\text{ MHz}$, Tone Spacing = 100 KHz)	G_{ps}	12	13.5	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 100\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2170\text{ MHz}$, Tone Spacing = 100 KHz)	η	31	35	—	%
Third Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 100\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2170\text{ MHz}$, Tone Spacing = 100 KHz)	IMD	—	–35	–30	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W PEP}$, $I_{DQ} = 100\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2170\text{ MHz}$, Tone Spacing = 100 KHz)	IRL	—	–12	–10	dB
Output Power, 1 dB Compression Point, CW ($V_{DD} = 28\text{ Vdc}$, $I_{DQ} = 100\text{ mA}$, $f = 2170\text{ MHz}$)	P1dB	—	11	—	W
Common–Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 100\text{ mA}$, $f = 2170\text{ MHz}$)	G_{ps}	—	12	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 100\text{ mA}$, $f = 2170\text{ MHz}$)	η	—	42	—	%
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W CW}$, $I_{DQ} = 100\text{ mA}$, $f = 2170\text{ MHz}$, VSWR = 10:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

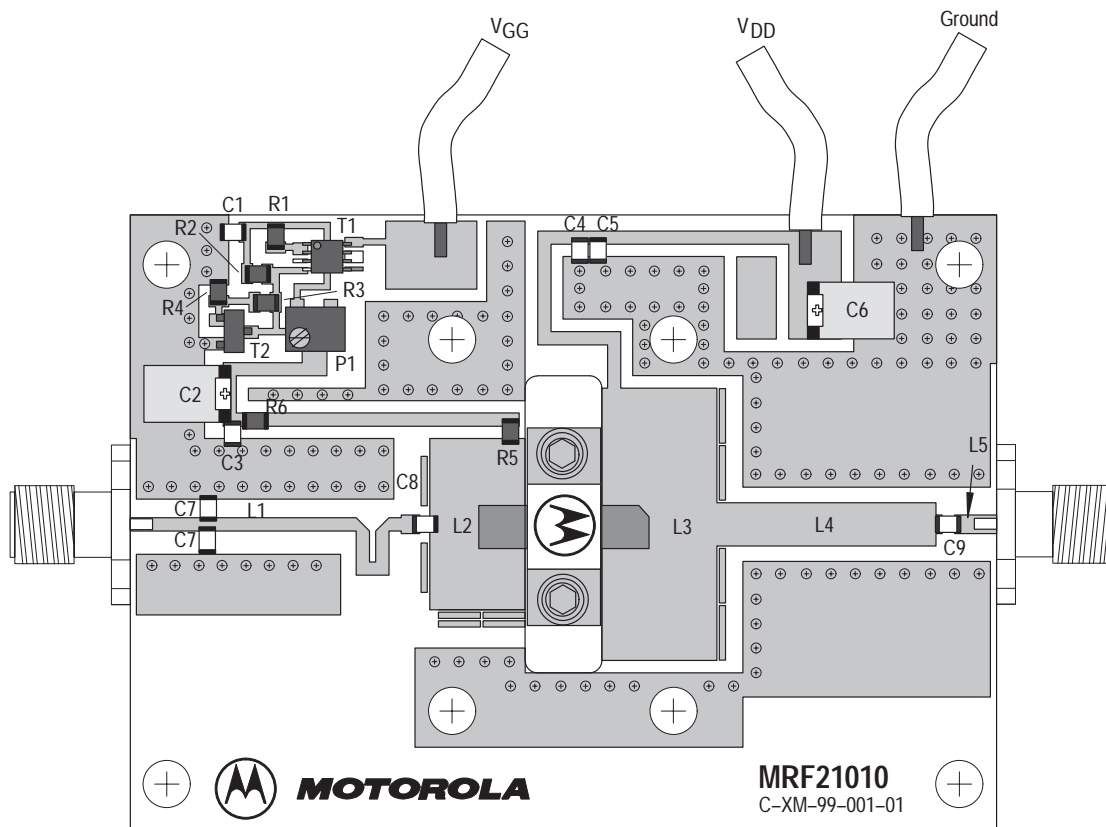


Figure 1. MRF21010 Demonstration Board Component Layout

Table 1. MRF21010 Demonstration Board Component Designations and Values

Designators	Description
C1	1 μ F, Chip Capacitor, 0805, AVX #08053G105ZATEA
C2, C6	10 μ F, 35 V, Tantalum Capacitors, Vishay–Sprague #293D106X9035D
C3, C4	6.8 pF, ACCU–P Chip Capacitors, 0805, AVX #08051J6R8CBT
C5	10 nF, Chip Capacitor, 0805, AVX #08055C103KATDA
C7	2.2 pF, ACCU–P Chip Capacitor, 0805, AVX #08051J2R2BBT
C8, C10	0.5 pF, ACCU–P Chip Capacitors, 0805, AVX #08051J0R5BBT
C9	10 pF, ACCU–P Chip Capacitor, 0805, AVX #08055J100GBT
L1	19 mm \times 1.07 mm
L2	7.7 mm \times 13.8 mm
L3	9.3 mm \times 22 mm
L4	17.7 mm \times 3.5 mm
L5	22 mm \times 1.07 mm
R1, R6	10 Ω , 1/8 W Chip Resistors, 0805
R2, R3	1 k Ω , 1/8 W Chip Resistors, 0805
R4	2.2 k Ω , 1/8 W Chip Resistor, 0805
R5	0 Ω , 1/8 W Chip Resistor, 0805
P1	5 k Ω , Potentiometer CMS Cermet Multi–Turn, Bourns #3224W
T1	Voltage Regulator Micro8, Motorola #LP2951
T2	Bipolar NPN Transistor SOT23, Motorola #BC847
	RF Connectors Type SMA, Johnson #142–0701–631
	Substrate: Rogers RO4350, Thickness 0.5 mm, $\epsilon_r = 3.53$

TYPICAL CHARACTERISTICS

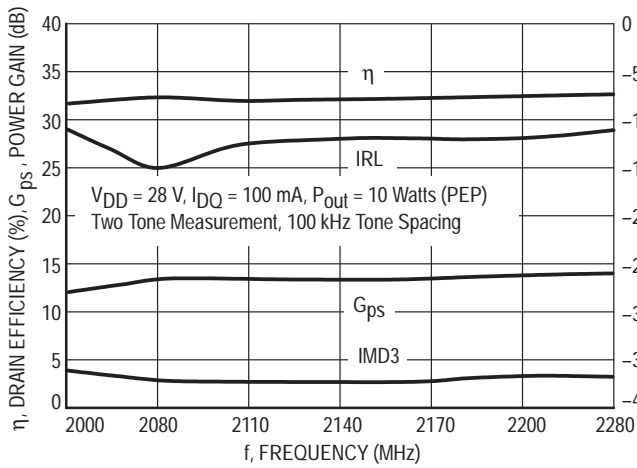


Figure 2. Class AB Broadband Circuit Performance

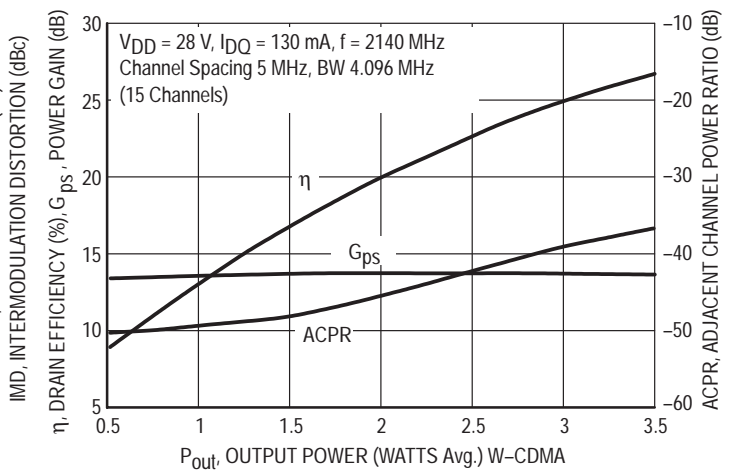


Figure 3. W-CDMA ACPR, Power Gain and Drain Efficiency versus Output Power

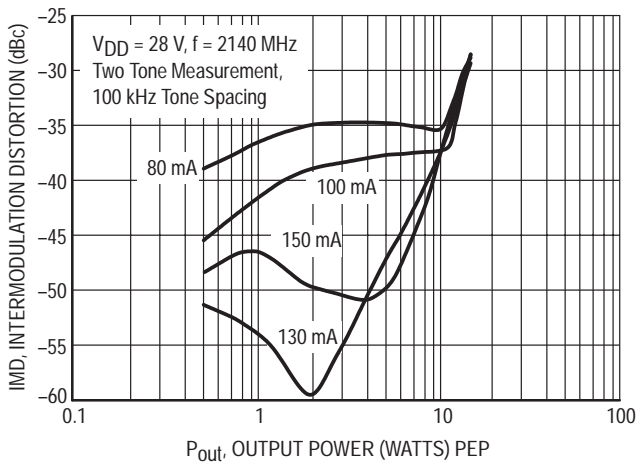


Figure 4. Intermodulation Distortion versus Output Power

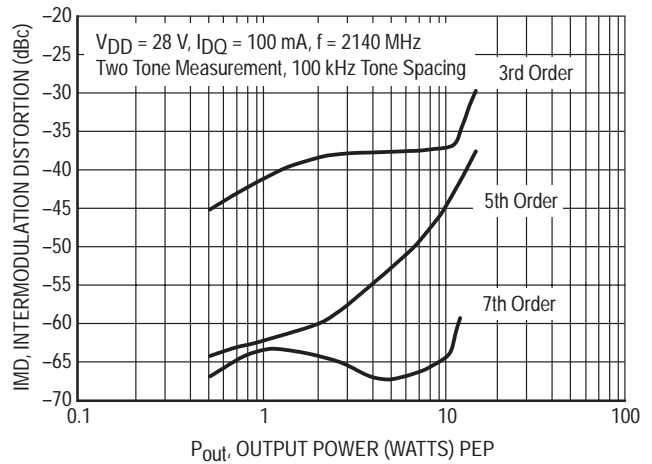


Figure 5. Intermodulation Distortion Products versus Output Power

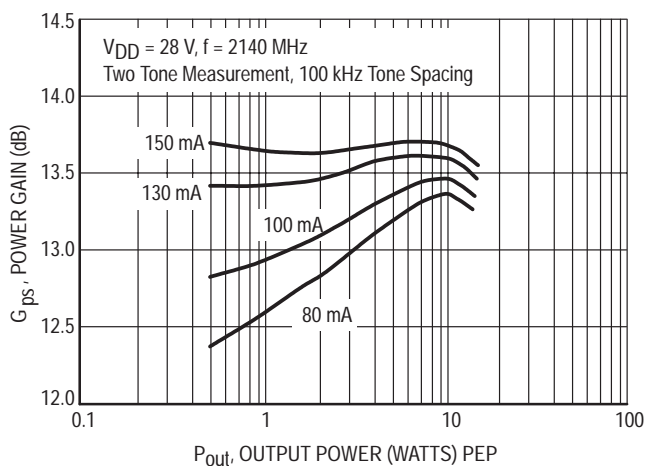


Figure 6. Power Gain versus Output Power

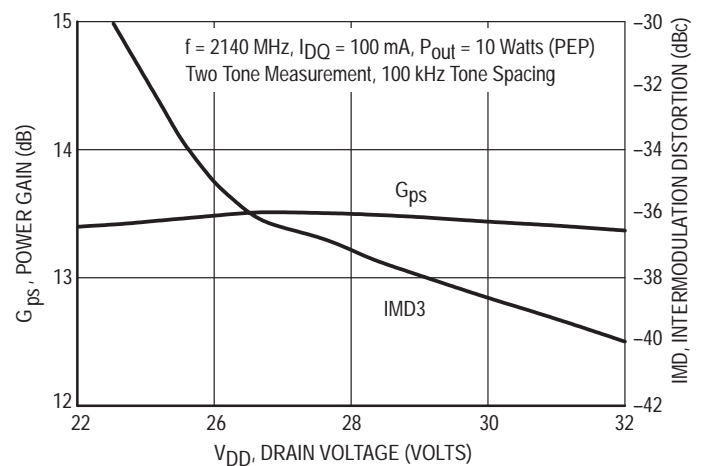
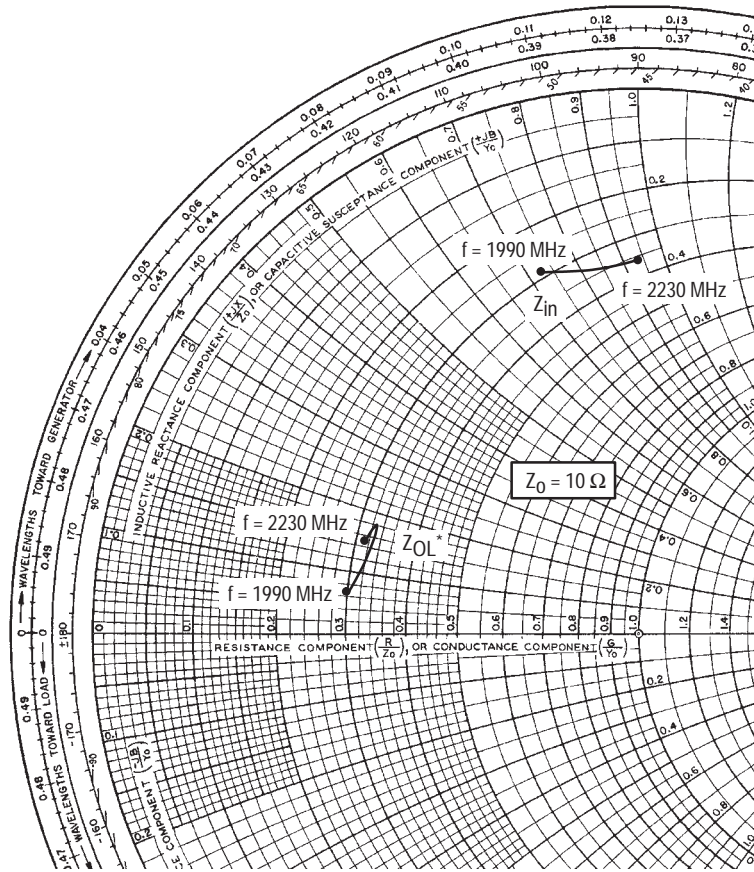


Figure 7. Intermodulation and Gain versus Supply Voltage



$V_{DD} = 28 \text{ V}$, $I_{DQ} = 100 \text{ mA}$, $P_{out} = \text{P1dB (CW)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
1990	$2.89 + j7.37$	$3.00 + j0.73$
2110	$3.46 + j8.57$	$3.29 + j1.88$
2230	$3.64 + j9.40$	$3.18 + j1.50$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

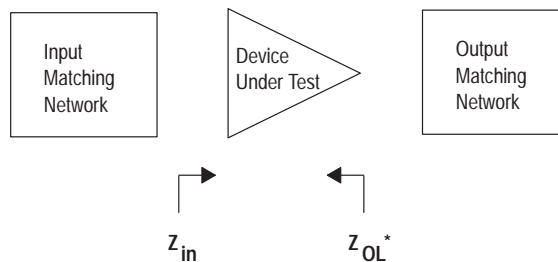


Figure 8. Series Equivalent Input and Output Impedance

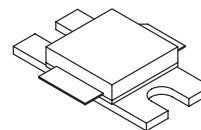
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for PCN and PCS base station applications from frequencies up to 2.0 to 2.2 GHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications. To be used in class AB for PCN-PCS/cellular radio and WLL applications.

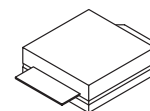
- Wideband CDMA Performance: -45 dB ACPR @ 4.096 MHz, 28 Volts
Output Power — 3.5 Watts
Power Gain — 14 dB
Efficiency — 15%
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 28 Vdc, 2.11 GHz, 30 Watts CW Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF21030
MRF21030S

2.2 GHz, 30 W, 28 V
LATERAL N-CHANNEL
RF POWER MOSFETs



CASE 465E-02, STYLE 1
(MRF21030)



CASE 465F-01, STYLE 1
(MRF21030S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	83.3 0.48	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

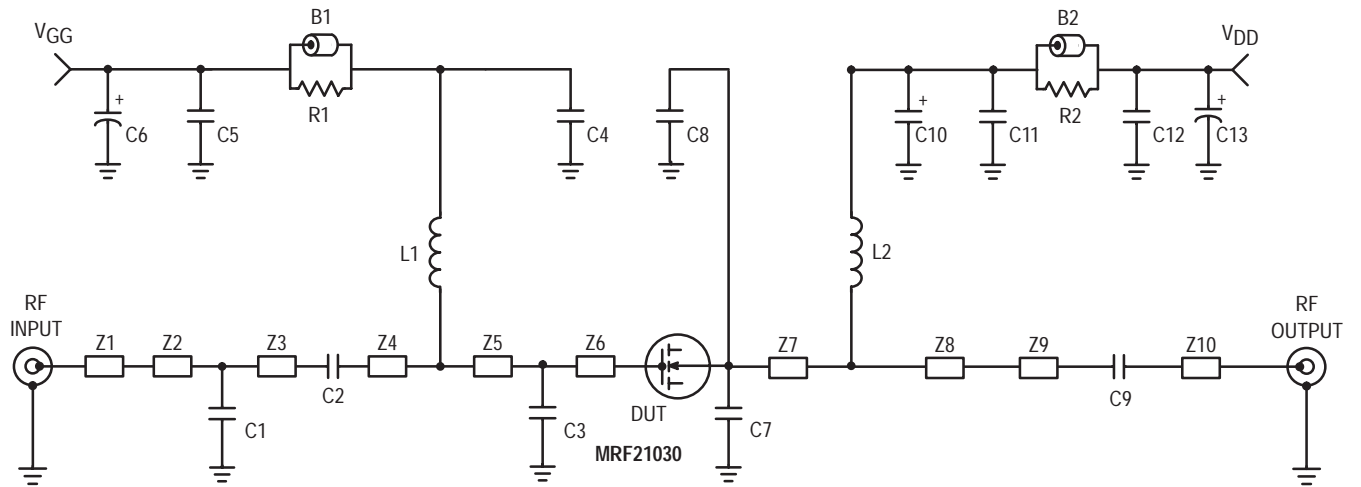
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	2.1	$^\circ\text{C}/\text{W}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 20\ \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	1	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ Vdc}$, $I_D = 250\text{ mA}$)	$V_{GS(Q)}$	2	3.3	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.29	0.4	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	g_{fs}	—	2	—	S
DYNAMIC CHARACTERISTICS					
Input Capacitance (Including Input Matching Capacitor in Package) (1) ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{iss}	—	98.5	—	pF
Output Capacitance (1) ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{oss}	—	37	—	pF
Reverse Transfer Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	1.3	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2140.0\text{ MHz}$, $f_2 = 2140.1\text{ MHz}$)	G_{ps}	—	13	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2140.0\text{ MHz}$, $f_2 = 2140.1\text{ MHz}$)	η	—	33	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2140.0\text{ MHz}$, $f_2 = 2140.1\text{ MHz}$)	IMD	—	–30	—	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2140.0\text{ MHz}$, $f_2 = 2140.1\text{ MHz}$)	IRL	—	–13	—	dB
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2110.0\text{ MHz}$, $f_2 = 2110.1\text{ MHz}$ and $f_1 = 2170.0\text{ MHz}$, $f_2 = 2170.1\text{ MHz}$)	G_{ps}	12	13	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2110.0\text{ MHz}$, $f_2 = 2110.1\text{ MHz}$ and $f_1 = 2170.0\text{ MHz}$, $f_2 = 2170.1\text{ MHz}$)	η	31	33	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2110.0\text{ MHz}$, $f_2 = 2110.1\text{ MHz}$ and $f_1 = 2170.0\text{ MHz}$, $f_2 = 2170.1\text{ MHz}$)	IMD	—	–30	–27.5	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W PEP}$, $I_{DQ} = 250\text{ mA}$, $f_1 = 2110.0\text{ MHz}$, $f_2 = 2110.1\text{ MHz}$ and $f_1 = 2170.0\text{ MHz}$, $f_2 = 2170.1\text{ MHz}$)	IRL	—	–13	–9	dB
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 30\text{ W CW}$, $I_{DQ} = 250\text{ mA}$, $f = 2110\text{ MHz}$, $V_{SWR} = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.



B1, B2	Short Ferrite Beads	Z1	0.153" x 0.087" Microstrip
C1	1 pF, Chip Capacitor	Z2	0.509" x 0.156" Microstrip
C2	4.7 pF, Chip Capacitor	Z3	0.572" x 0.087" Microstrip
C3	0.5 pF, Chip Capacitor	Z4	0.509" x 0.232" Microstrip
C4	3.9 pF, Chip Capacitor	Z5	0.277" x 0.143" Microstrip
C5, C12	0.1 μ F, Chip Capacitors	Z6	0.200" x 0.305" Microstrip
C6, C13	470 μ F, 63 V, Electrolytic Chip Capacitors	Z7	0.200" x 0.511" Microstrip
C7, C8	0.3 pF, Chip Capacitors	Z8	0.510" x 0.328" Microstrip
C9	3.6 pF, Chip Capacitor	Z9	0.608" x 0.081" Microstrip
C10	22 μ F, Tantalum Chip Capacitor	Board	0.030" Glass Teflon [®] , TLX8-0300 Taconix ($\epsilon_r = 2.55$)
C11	5.1 pF, Chip Capacitor		
L1, L2	12.5 nH, Inductors		
R1, R2	12 Ω , Chip Resistors, 1206		

Figure 1. MRF21030 Schematic

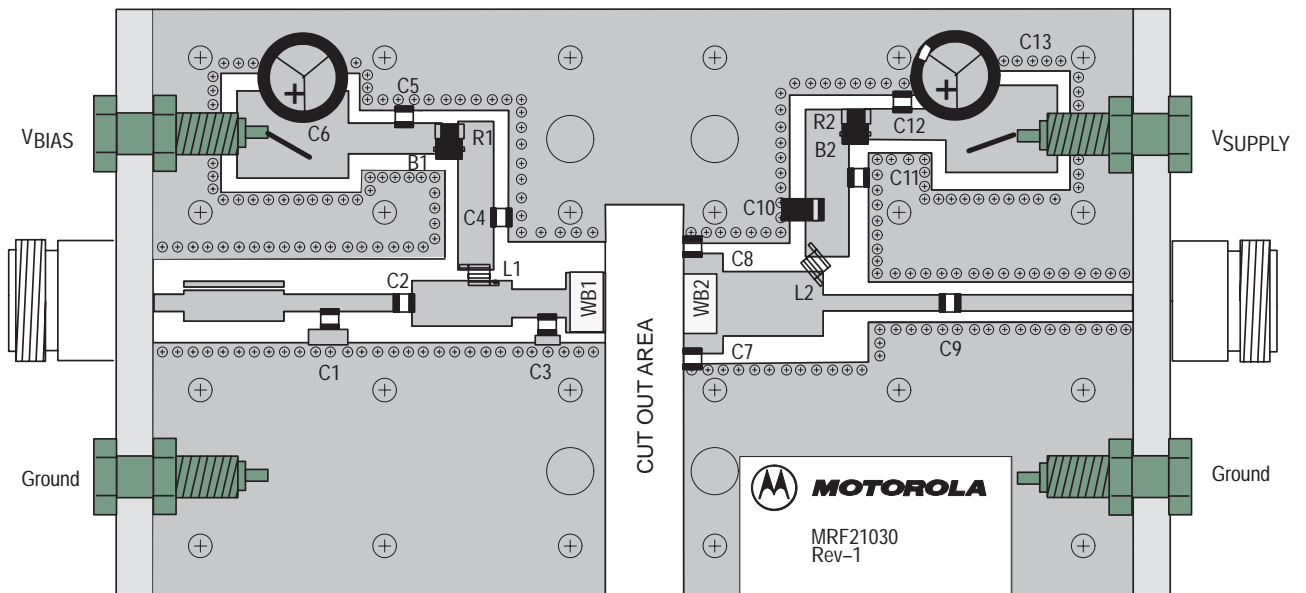


Figure 2. MRF21030 Populated PC Board Layout Diagram

TYPICAL CHARACTERISTICS

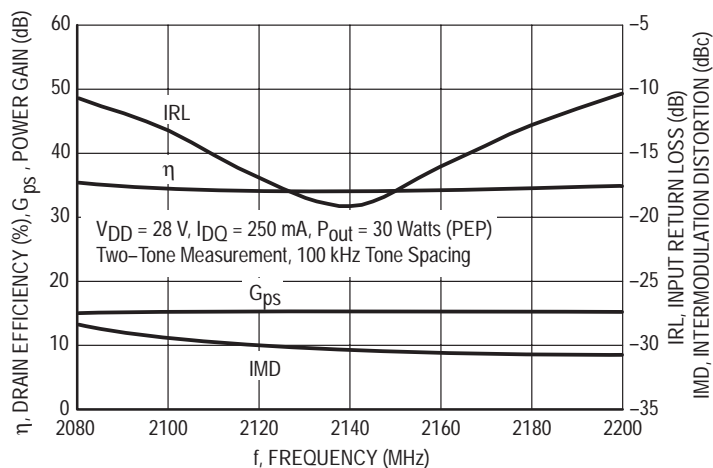


Figure 3. Class AB Broadband Circuit Performance

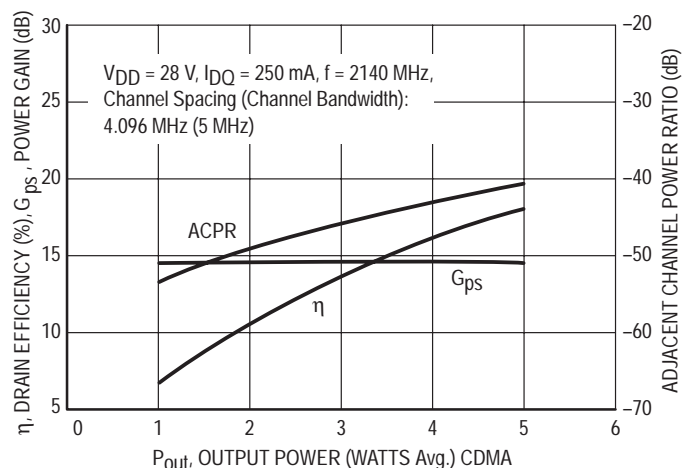


Figure 4. CDMA ACPR, Power Gain and Drain Efficiency versus Output Power

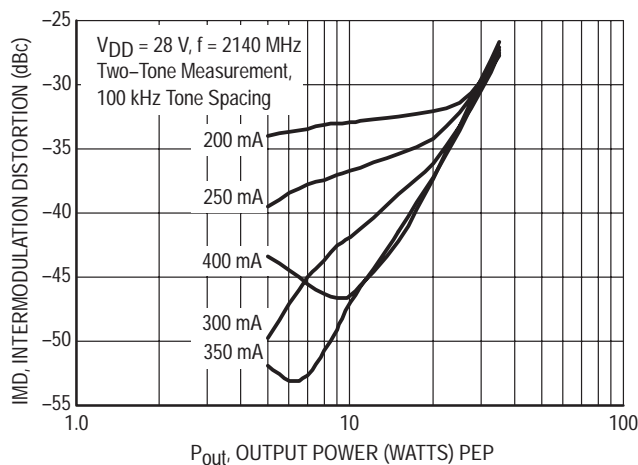


Figure 5. Intermodulation Distortion versus Output Power

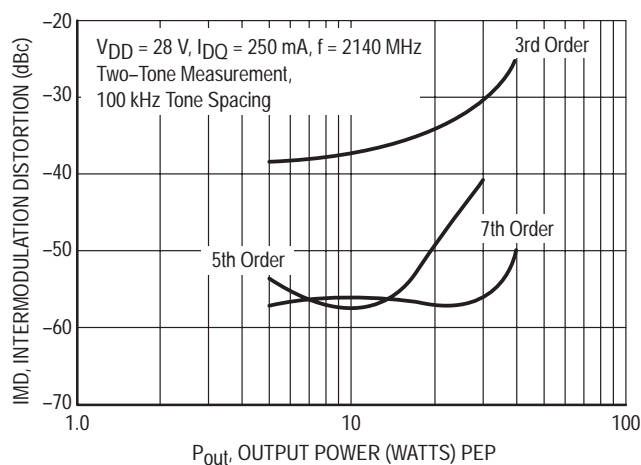


Figure 6. Intermodulation Distortion Products versus Output Power

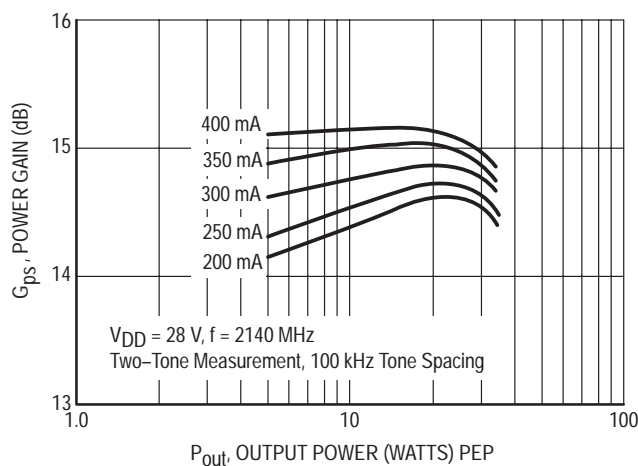


Figure 7. Power Gain versus Output Power

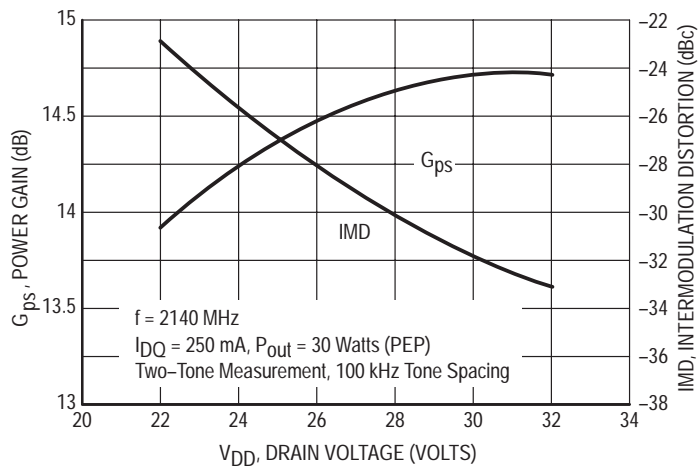
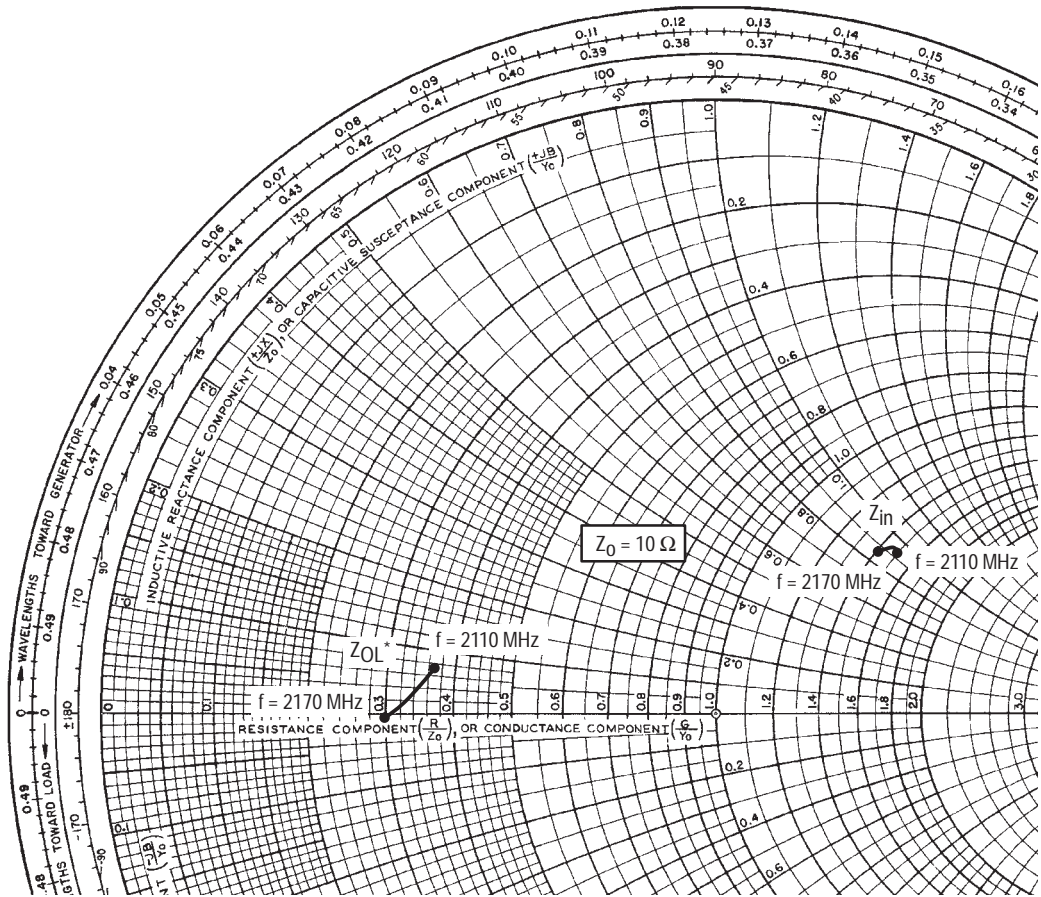


Figure 8. Power Gain and Intermodulation Distortion versus Supply Voltage



$V_{DD} = 28\text{ V}$, $I_{DQ} = 250\text{ mA}$, $P_{out} = 30\text{ Watts (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
2110	$15.3 + j9.4$	$3.7 + j0.78$
2140	$14.6 + j9.4$	$3.4 + j0.37$
2170	$14.3 + j8.8$	$3.0 - j0.13$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

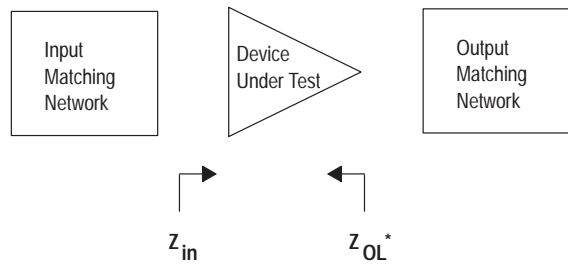


Figure 9. Series Equivalent Input and Output Impedance

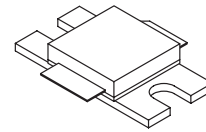
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for W-CDMA base station applications at frequencies from 2110 to 2170 MHz. Suitable for TDMA, CDMA and multicarrier amplifier applications. To be used in Class AB for PCN-PCS/cellular radio and WLL applications.

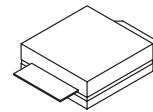
- Typical 2-carrier W-CDMA Performance for $V_{DD} = 28$ Volts, $I_{DQ} = 500$ mA, $f_1 = 2135$ MHz, $f_2 = 2145$ MHz, Channel Bandwidth = 3.84 MHz, Adjacent Channels measured over 3.84 MHz Bandwidth at $f_1 - 5$ MHz and $f_2 + 5$ MHz, Distortion Products measured over a 3.84 MHz Bandwidth at $f_1 - 10$ MHz and $f_2 + 10$ MHz, Peak/Avg. = 8.3 dB @ 0.01% Probability on CCDF.
 - Output Power = 10 Watts Avg.
 - Efficiency = 23.5%
 - Gain = 15 dB
 - IM3 = -37.5 dBc
 - ACPR = -41 dBc
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 5:1 VSWR, @ 28 Vdc, 2170 MHz, 45 Watts CW Output Power
- Excellent Thermal Stability

MRF21045
MRF21045S

2170 MHz, 45 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465E-02, STYLE 1
(MRF21045)



CASE 465F-02, STYLE 1
(MRF21045S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	98 0.51	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M2 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.97	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

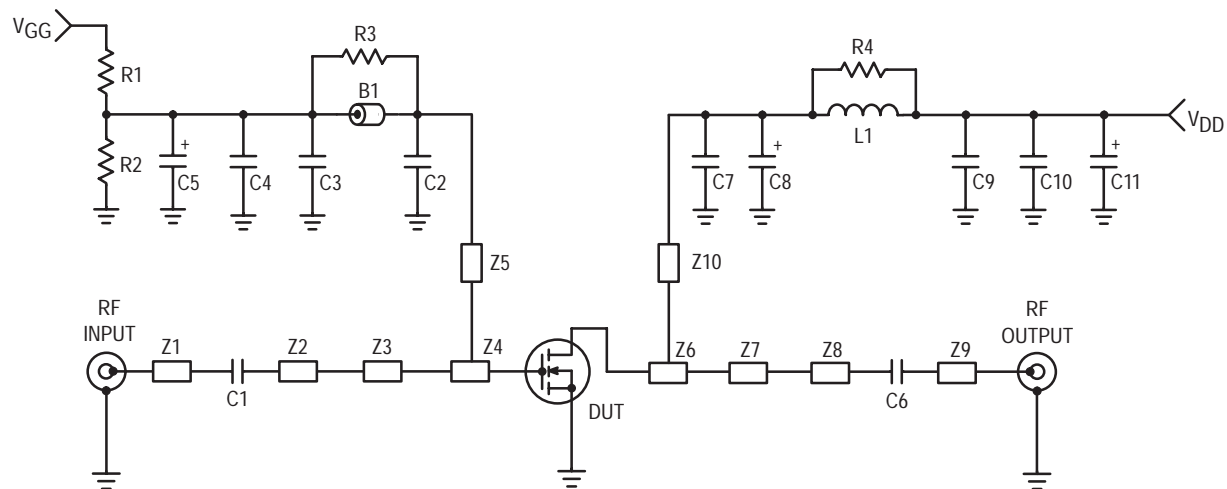
ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS (DC)					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ Vdc}$, $I_D = 500\text{ mAdc}$)	$V_{GS(Q)}$	3	3.9	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	$V_{DS(on)}$	—	0.19	0.21	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 1\text{ Adc}$)	g_{fs}	—	3	—	S
DYNAMIC CHARACTERISTICS (1)					
Reverse Transfer Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	1.8	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture) 2–carrier W–CDMA. Peak/Avg. ratio = 8.3 dB @ 0.01% Probability on CCDF.					
Common–Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W Avg.}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$)	G_{ps}	13.5	15	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W Avg.}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$)	η	21	23.5	—	%
Third Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W Avg.}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$; IM3 measured over 3.84 MHz Bandwidth at $f_1 - 10\text{ MHz}$ and $f_2 + 10\text{ MHz}$.)	IM3	—	–37.5	–35	dBc
Adjacent Channel Power Ratio ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W Avg.}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$; ACPR measured over 3.84 MHz Bandwidth at $f_1 - 5\text{ MHz}$ and $f_2 + 5\text{ MHz}$.)	ACPR	—	–41	–38	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 10\text{ W Avg.}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$)	IRL	—	–12	–9	dB
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W CW}$, $I_{DQ} = 500\text{ mA}$, $f = 2170\text{ MHz}$ $V_{SWR} = 5:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL TESTS (In Motorola Test Fixture) — continued					
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	G_{ps}	—	14.9	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	η	—	36	—	%
Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	IMD	—	-30	—	dBc
Two-Tone Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 45\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	IRL	—	-12	—	dB
P_{out} , 1 dB Compression Point ($V_{DD} = 28\text{ Vdc}$, $I_{DQ} = 500\text{ mA}$, $f = 2170\text{ MHz}$)	P1dB	—	50	—	W



Z1, Z9	0.750" x 0.084" Transmission Line	Board	0.030" Glass Teflon [®] ,
Z2	0.160" x 0.084" Transmission Line	PCB	Keene GX-0300-55-22, $\epsilon_r = 2.55$
Z3	1.195" x 0.176" Transmission Line		Etched Circuit Boards
Z4	0.125" x 0.320" Transmission Line		MRF21045 Rev. 3, CMR
Z5	1.100" x 0.045" Transmission Line		
Z6	0.442" x 0.650" Transmission Line		
Z7	0.490" x 0.140" Transmission Line		
Z8	0.540" x 0.084" Transmission Line		
Z10	0.825" x 0.055" Transmission Line		

Figure 1. MRF21045 Test Circuit Schematic

Table 1. MRF21045 Component Designations and Values

Designators	Description
B1	Short Ferrite Bead, Fair Rite, #2743019447
C1, C2, C6	43 pF Chip Capacitors, ATC #100B430JCA500X
C7	5.6 pF Chip Capacitor, ATC #100B5R6JCA500X
C3, C9	1000 pF Chip Capacitors, ATC #100B102JCA500X
C4, C10	0.1 μ F Chip Capacitors, Kemet #CDR33BX104AKWS
C5	1.0 μ F Tantalum Chip Capacitor, Kemet #T491C105M050
C8	10 μ F Tantalum Chip Capacitor, Kemet #T495X106K035AS4394
C11	22 μ F Tantalum Chip Capacitor, Kemet #T491X226K035AS4394
L1	1 Turn, #20 AWG, 0.100" ID, Motorola
N1, N2	Type N Flange Mounts, Omni Spectra #3052-1648-10
R1	1.0 k Ω , 1/8 W Chip Resistor
R2	180 k Ω , 1/8 W Chip Resistor
R3, R4	10 Ω , 1/8 W Chip Resistors

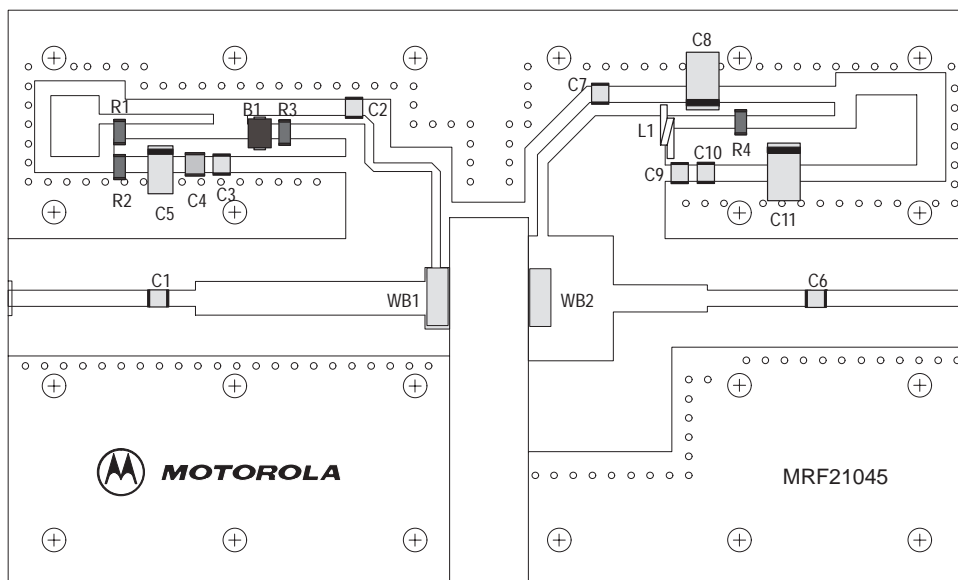


Figure 2. MRF21045 Test Circuit Component Layout

TYPICAL CHARACTERISTICS

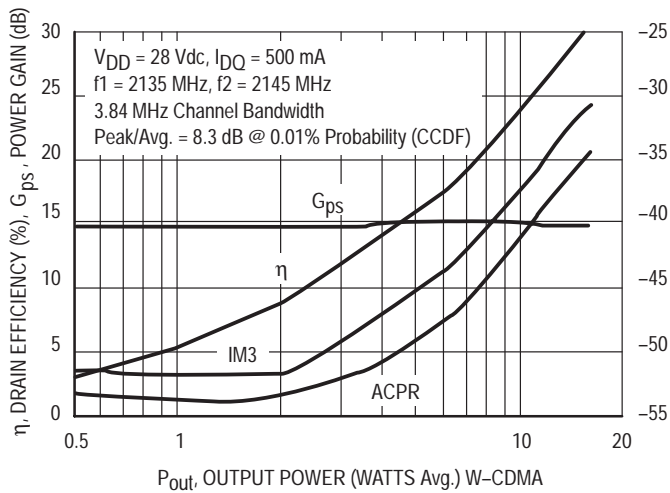


Figure 3. 2-Carrier W-CDMA ACPR, IM3, Power Gain and Drain Efficiency versus Output Power

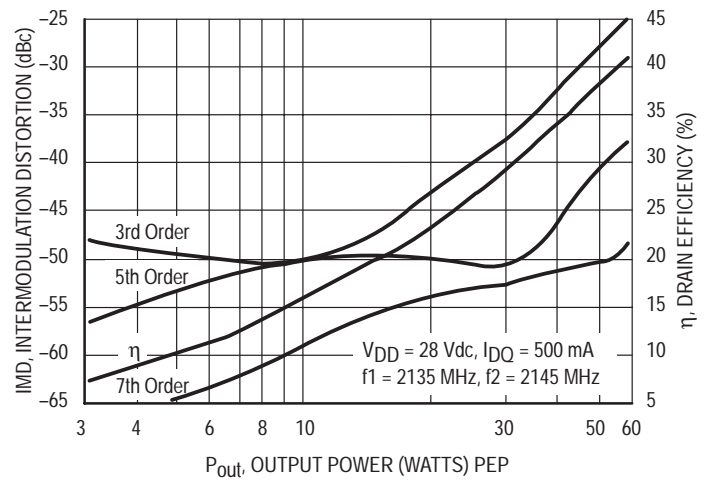


Figure 4. Intermodulation Distortion Products versus Output Power

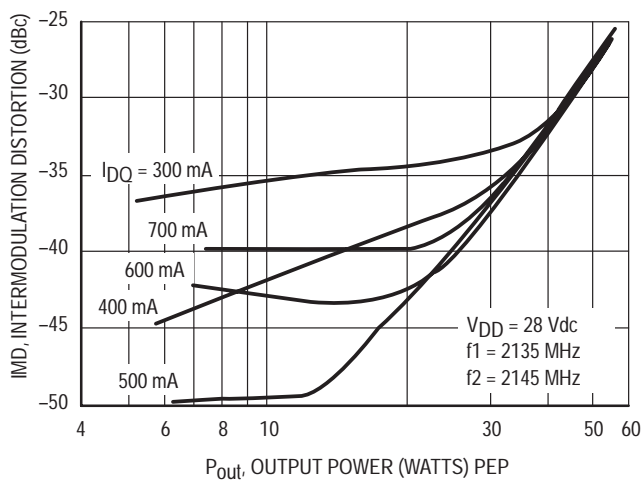


Figure 5. Intermodulation Distortion versus Output Power

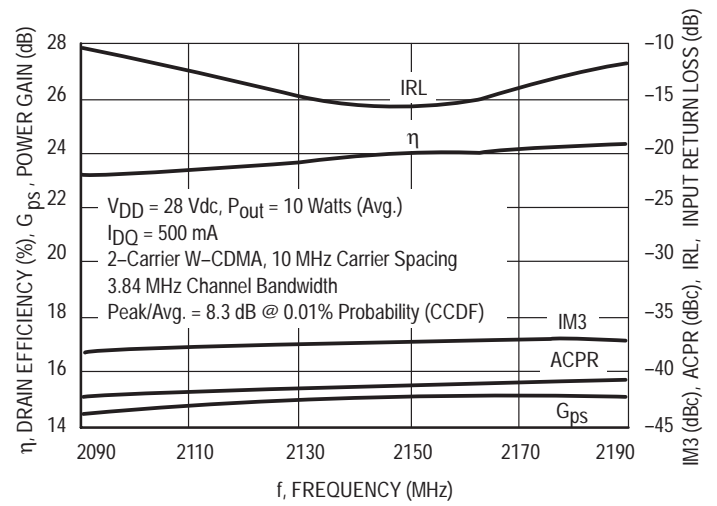


Figure 6. 2-Carrier W-CDMA Broadband Performance

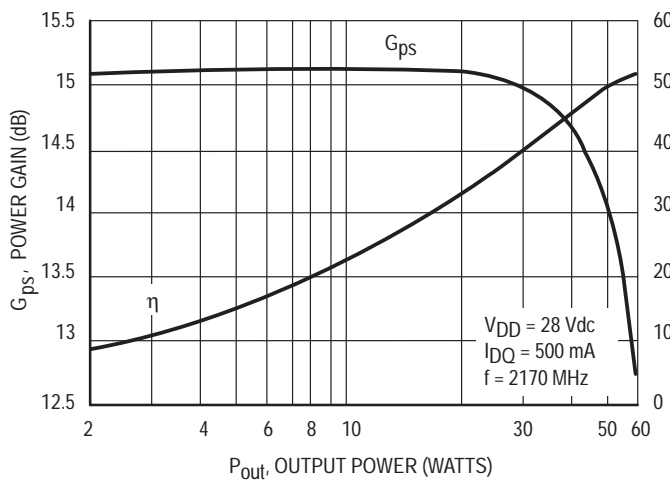


Figure 7. CW Performance

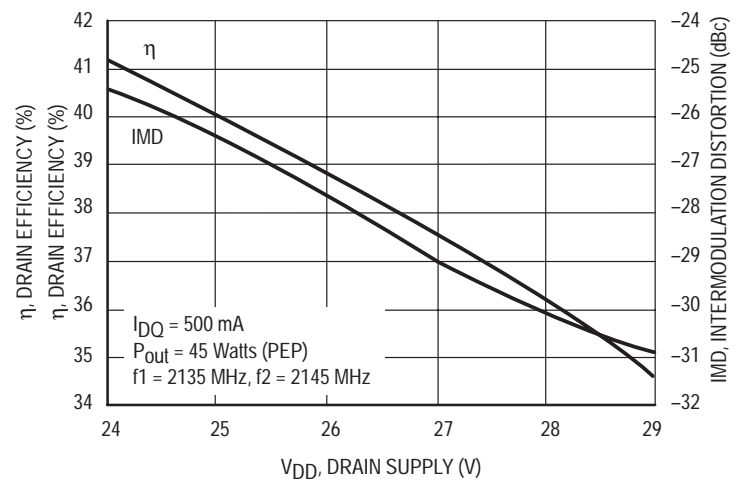


Figure 8. Two-Tone Intermodulation Distortion and Drain Efficiency versus Drain Supply

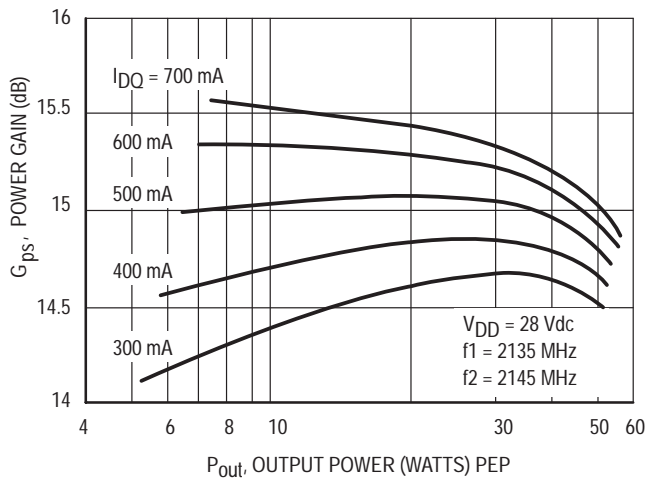


Figure 9. Two-Tone Power Gain versus Output Power

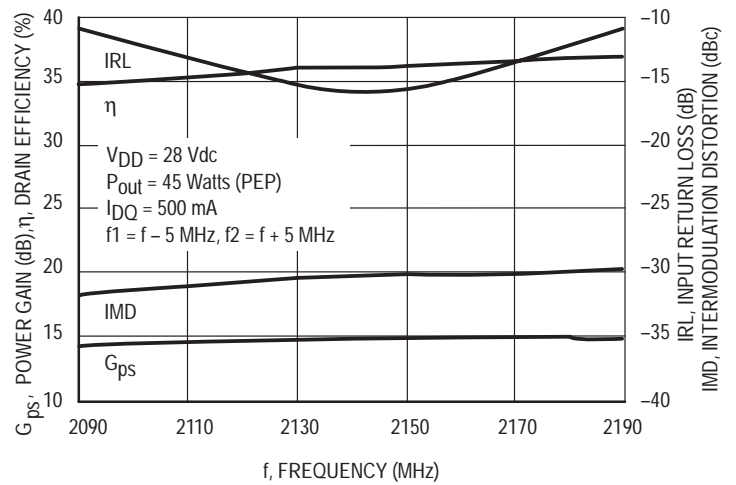


Figure 10. Two-Tone Broadband Performance

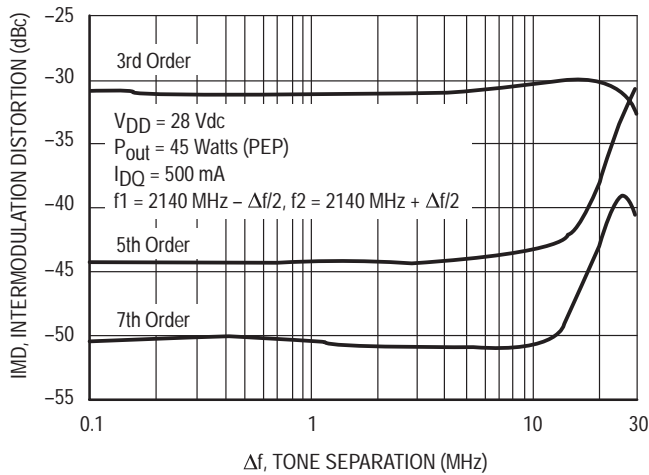


Figure 11. Intermodulation Distortion Products versus Two-Tone Spacing

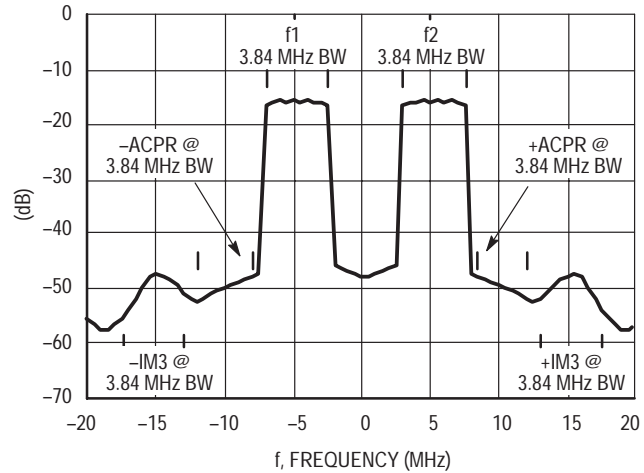
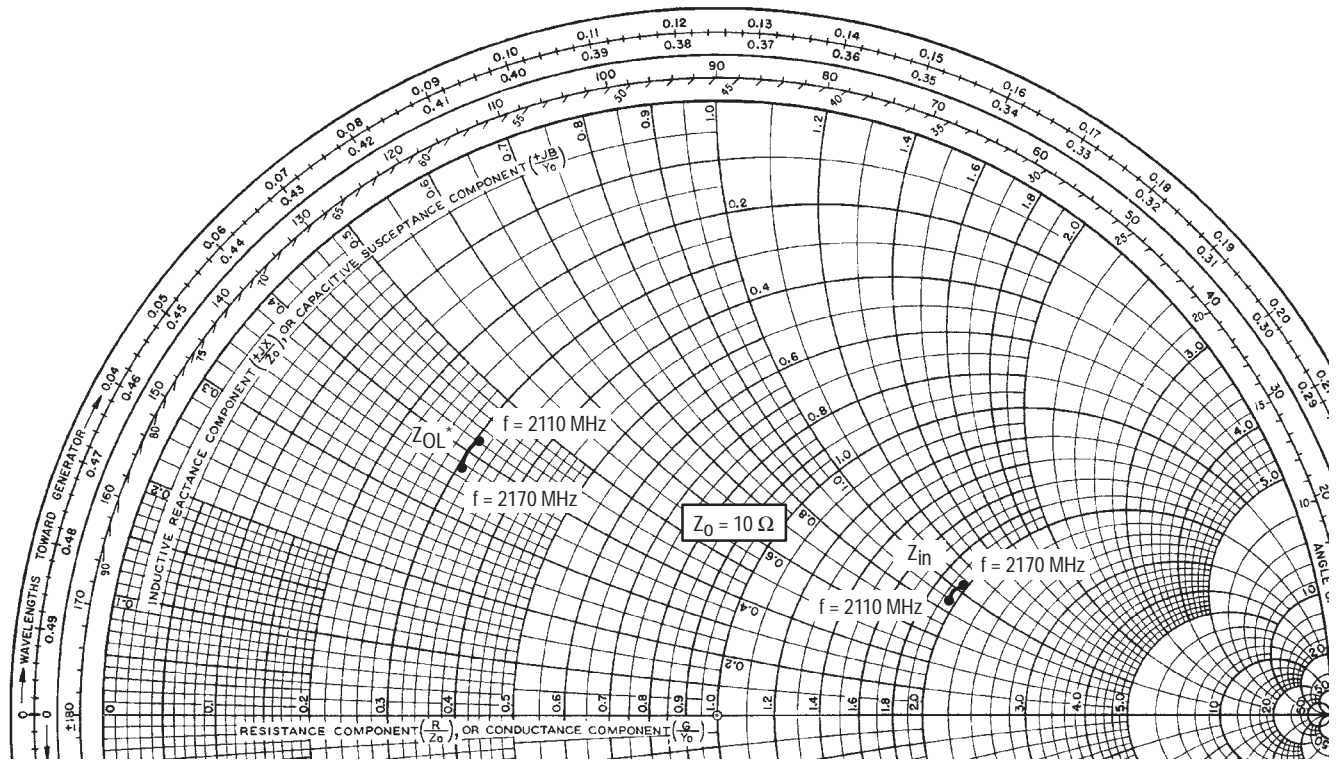


Figure 12. 2-Carrier W-CDMA Spectrum



$V_{DD} = 28 \text{ Vdc}$, $I_{DQ} = 500 \text{ mA}$, $P_{out} = 10 \text{ W (Avg.)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
2110	$18.88 + j8.86$	$3.11 + j4.18$
2140	$19.83 + j9.93$	$3.09 + j3.87$
2170	$19.68 + j10.44$	$3.12 + j3.72$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

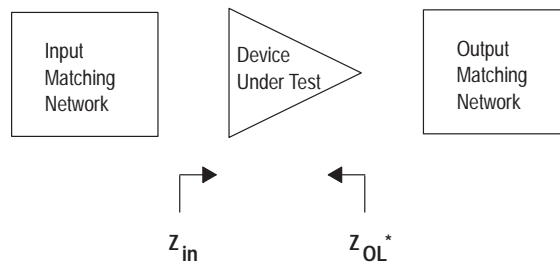


Figure 13. Series Equivalent Input and Output Impedance

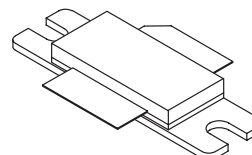
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for PCN and PCS base station applications from frequencies up to 2.1 to 2.2 GHz. Suitable for W-CDMA, CDMA, TDMA, GSM and multicarrier amplifier applications.

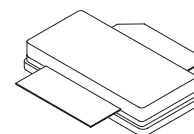
- Typical W-CDMA Performance: 2140 MHz, 28 Volts
5 MHz Offset @ 4.096 MHz BW, 15 DTCH
Output Power — 6.0 Watts
Power Gain — 12.5 dB
Drain Efficiency — 15%
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 28 Vdc, 2.11 GHz, 60 Watts (CW)
Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF21060
MRF21060S

2170 MHz, 60 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465-04, STYLE 1
(MRF21060)



CASE 465A-04, STYLE 1
(MRF21060S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	180 0.98	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

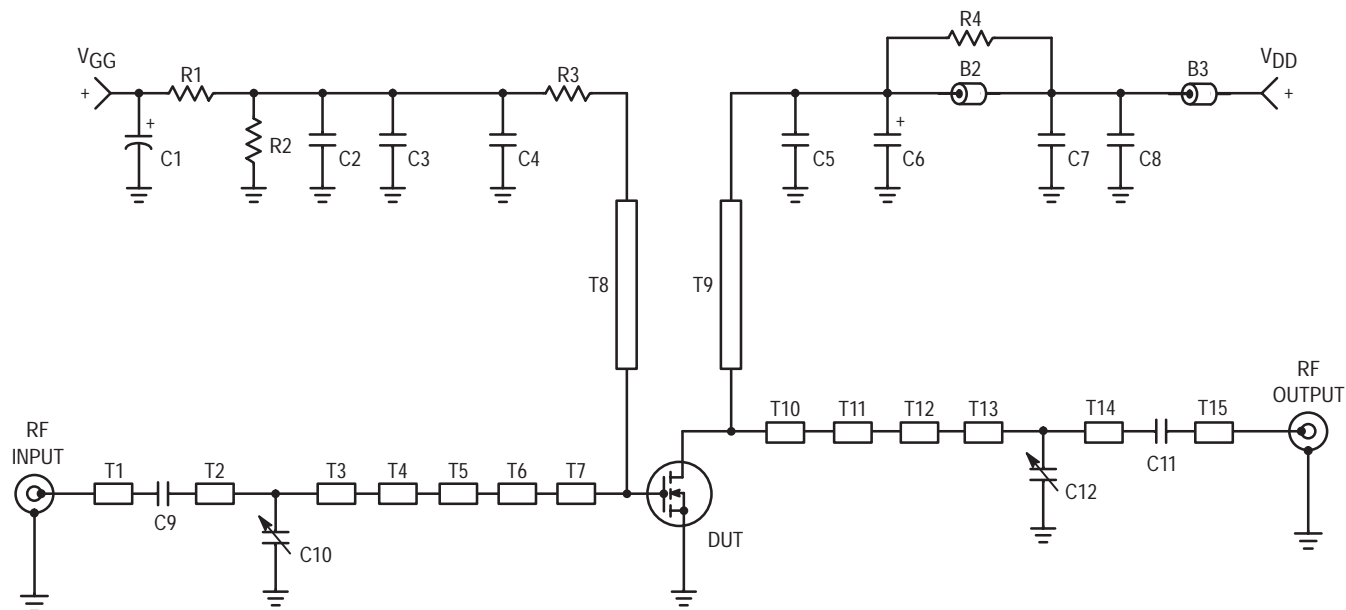
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1.02	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 10\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	6	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc
ON CHARACTERISTICS					
Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 300\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ Vdc}$, $I_D = 500\text{ mAdc}$)	$V_{GS(Q)}$	2.5	3.9	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	$V_{DS(on)}$	—	0.27	—	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	g_{fs}	—	4.7	—	S
DYNAMIC CHARACTERISTICS					
Reverse Transfer Capacitance (1) ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1\text{ MHz}$)	C_{rss}	—	2.7	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two–Tone Common–Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 2110\text{ MHz}$ and 2170 MHz , Tone Spacing = 100 kHz)	G_{ps}	11	12.5	—	dB
Two–Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 2110\text{ MHz}$ and 2170 MHz , Tone Spacing = 100 kHz)	η	31	34	—	%
3rd Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 2110\text{ MHz}$ and 2170 MHz , Tone Spacing = 100 kHz)	IMD	—	–30	–28	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 60\text{ W PEP}$, $I_{DQ} = 500\text{ mA}$, $f = 2110\text{ MHz}$ and 2170 MHz , Tone Spacing = 100 kHz)	IRL	—	–12	—	dB
P_{out} , 1 dB Compression Point ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 60\text{ W CW}$, $f = 2170\text{ MHz}$)	P_{1dB}	—	60	—	W
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 60\text{ W CW}$, $I_{DQ} = 500\text{ mA}$, $f = 2110\text{ MHz}$, $V_{SWR} = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.



B2 – B3	Ferrite Bead, Fair Rite #2743019447	T3	0.180" x 0.100" Microstrip
C1	10 μ F, 50 V Electrolytic Chip Capacitor, Panasonic #ECEV1HV100R	T4	0.152" x 0.293" Microstrip
C2, C7	1000 pF, Chip Capacitors, ATC #100B102JCA500X	T5	0.216" x 0.100" Microstrip
C3, C8	0.10 μ F, Chip Capacitors, Kemet #CDR33BX104AKWS	T6	0.114" x 0.410" Microstrip
C4, C5	4.7 pF, Chip Capacitors, ATC #100B4R7JCA500X	T7	0.626" x 0.872" Microstrip
C6	22 μ F, 35 V Tantalum Surface Mount Chip Capacitor, Sprague	T8	1.050" x 0.050" Microstrip
C9, C11	9.1 pF, Chip Capacitors, ATC #100B9R1JCA500X	T9	0.830" x 0.050" Microstrip
C10	0.8 pF – 8.0 pF, Variable Capacitor, Johanson Gigatrim	T10	0.596" x 1.040" Microstrip
C12	0.4 pF – 4.5 pF, Variable Capacitor, Johanson Gigatrim	T11	0.186" x 0.315" Microstrip
R1	1 k Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T12	0.097" x 0.525" Microstrip
R2	560 k Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T13	0.353" x 0.138" Microstrip
R3	10 Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T14	0.112" x 0.080" Microstrip
R4	10 Ω , 1/4 W, Fixed Film Chip Resistor, 0.08" x 0.13"	T15	0.722" x 0.080" Microstrip
T1	0.743" x 0.080" Microstrip	Board	0.030" Glass Teflon [®] , Arlon GX-0300-55-22, 2 oz Cu
T2	0.070" x 0.100" Microstrip		

Figure 1. MRF21060 Test Circuit Schematic

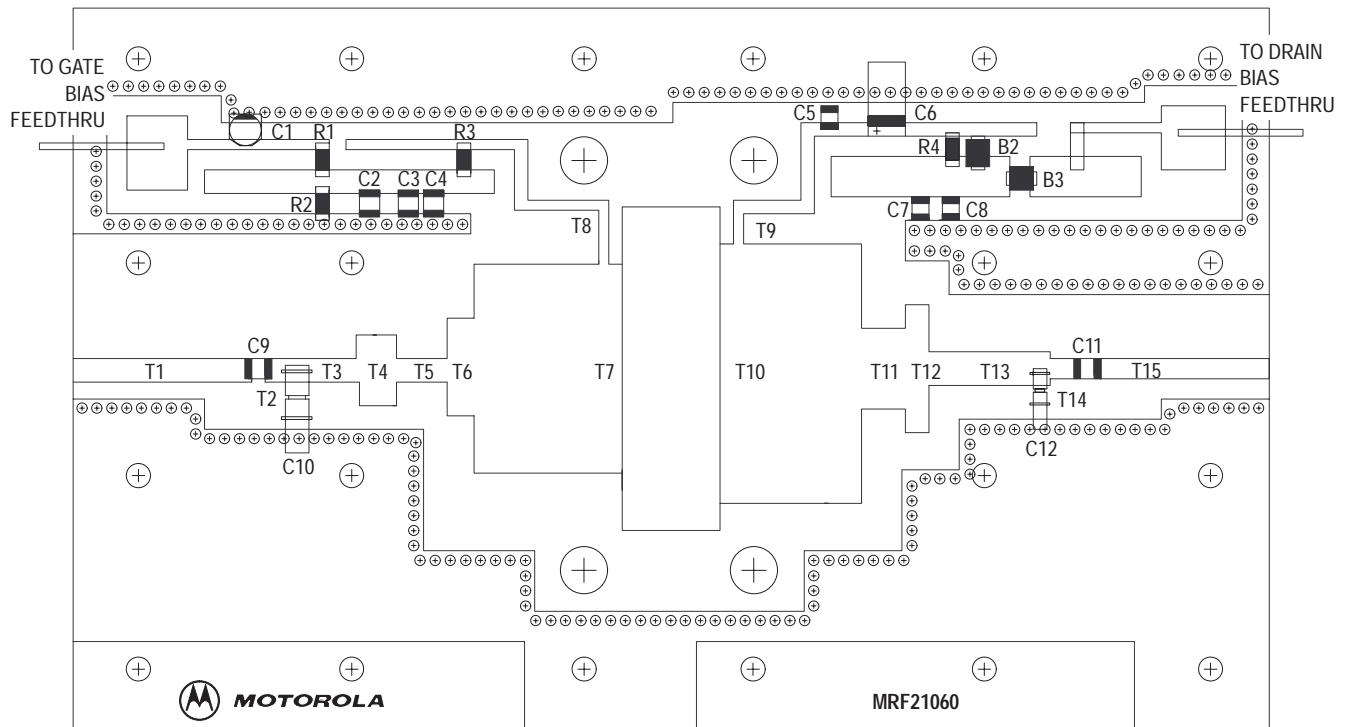


Figure 2. MRF21060 Populated PC Board Layout Diagram

TYPICAL CHARACTERISTICS

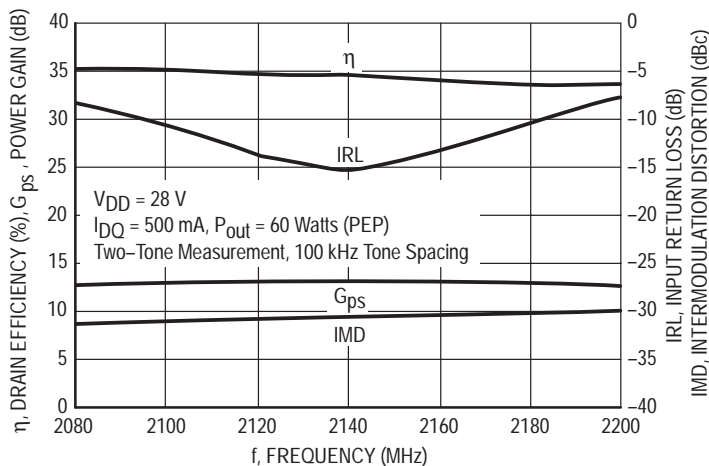


Figure 3. Class AB Broadband Circuit Performance

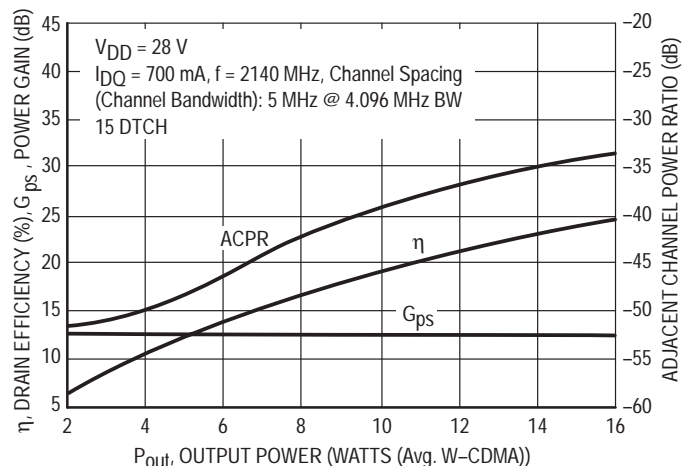


Figure 4. W-CDMA ACPR, Power Gain and Drain Efficiency versus Output Power

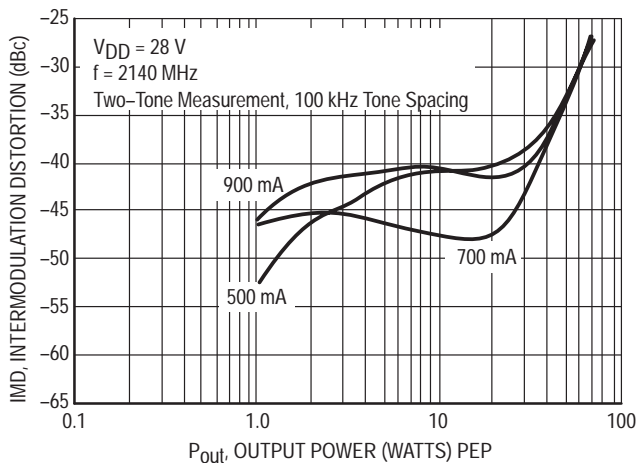


Figure 5. Intermodulation Distortion versus Output Power

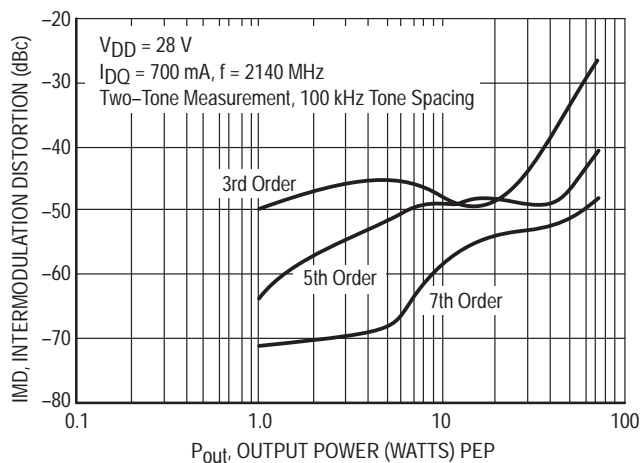


Figure 6. Intermodulation Distortion Products versus Output Power

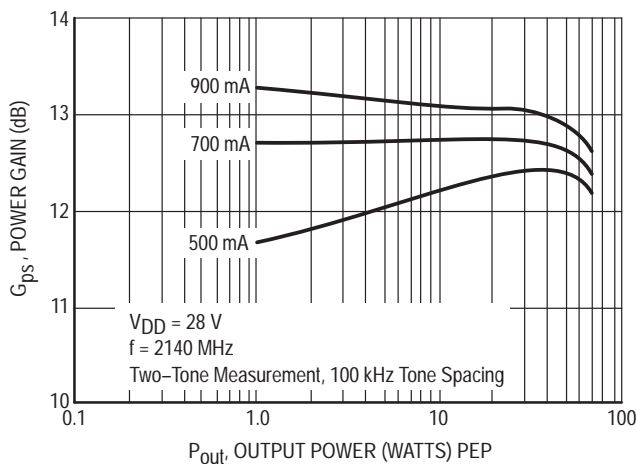


Figure 7. Power Gain versus Output Power

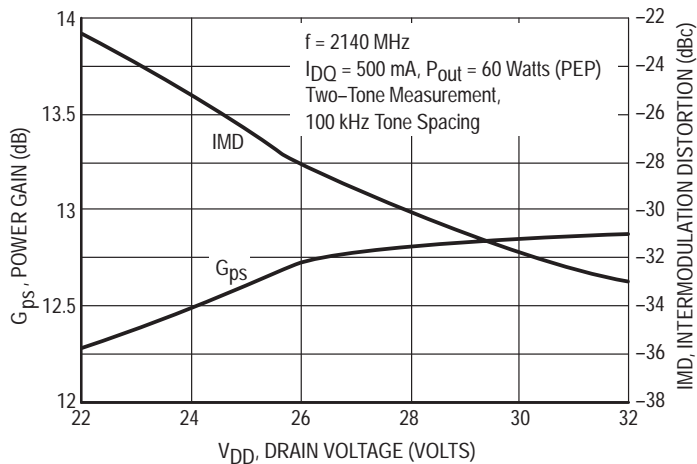
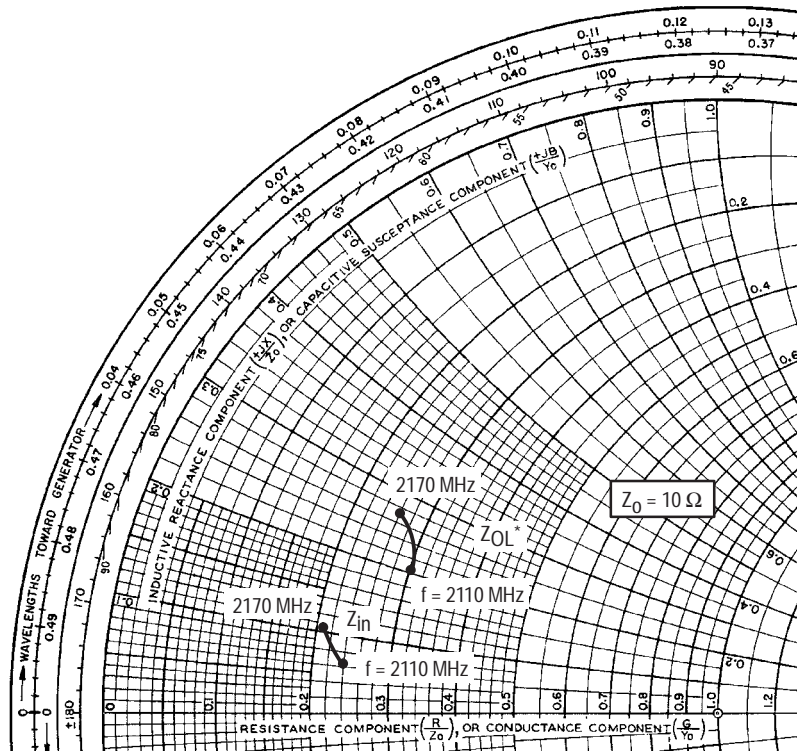


Figure 8. Power Gain and Intermodulation Distortion versus Supply Voltage



$V_{DD} = 28\text{ V}$, $I_{DQ} = 500\text{ mA}$, $P_{out} = 60\text{ Watts (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
2110	$2.40 + j0.55$	$3.07 + j2.05$
2140	$2.26 + j0.87$	$2.89 + j2.38$
2170	$2.08 + j1.23$	$2.66 + j2.71$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

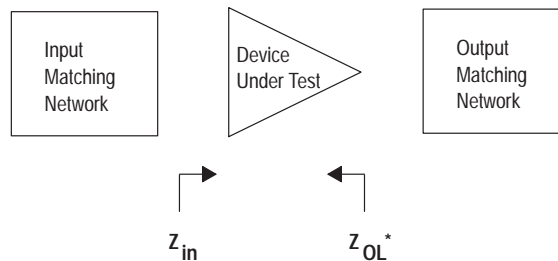


Figure 9. Series Equivalent Input and Output Impedance

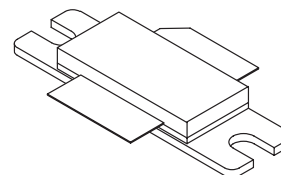
The RF MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

MRF21085
MRF21085S

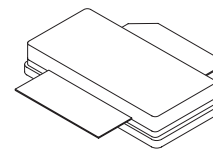
Designed for W-CDMA base station applications at frequencies from 2110 to 2170 MHz. Suitable for TDMA, CDMA and multicarrier amplifier applications. To be used in Class AB for PCN-PCS/cellular radio and WLL applications.

2170 MHz, 90 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs

- Typical 2-carrier W-CDMA Performance for $V_{DD} = 28$ Volts, $I_{DQ} = 1000$ mA, $f_1 = 2135$ MHz, $f_2 = 2145$ MHz, Channel Bandwidth = 3.84 MHz, Adjacent Channels Measured over 3.84 MHz BW @ $f_1 -5$ MHz and $f_2 +5$ MHz, Distortion Products Measured over a 3.84 MHz BW @ $f_1 -10$ MHz and $f_2 +10$ MHz, Peak/Avg. = 8.3 dB @ 0.01% Probability on CCDF.
 - Output Power = 19 Watts Avg.
 - Power Gain = 13.6 dB
 - Efficiency = 23%
 - IM3 = -37.5 dBc
 - ACPR = -41 dBc
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 5:1 VSWR, @ 28 Vdc, 2170 MHz, 90 Watts CW Output Power
- Excellent Thermal Stability



CASE 465-04, STYLE 1
(MRF21085)



CASE 465A-04, STYLE 1
(MRF21085S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	273 1.56	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +200	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	1 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.64	$^\circ\text{C}/\text{W}$

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Drain–Source Breakdown Voltage ($V_{GS} = 0\text{ Vdc}$, $I_D = 100\ \mu\text{Adc}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Zero Gate Voltage Drain Current ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μAdc
Gate–Source Leakage Current ($V_{GS} = 5\text{ Vdc}$, $V_{DS} = 0$)	I_{GSS}	—	—	1	μAdc

ON CHARACTERISTICS (DC)

Gate Threshold Voltage ($V_{DS} = 10\text{ Vdc}$, $I_D = 200\ \mu\text{Adc}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28\text{ Vdc}$, $I_D = 1000\ \text{mAdc}$)	$V_{GS(Q)}$	3	3.9	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	$V_{DS(on)}$	—	0.18	0.21	Vdc
Forward Transconductance ($V_{DS} = 10\text{ Vdc}$, $I_D = 2\text{ Adc}$)	g_{fs}	—	6	—	S

DYNAMIC CHARACTERISTICS (1)

Reverse Transfer Capacitance ($V_{DS} = 28\text{ Vdc}$, $V_{GS} = 0$, $f = 1.0\text{ MHz}$)	C_{rss}	—	3.6	—	pF
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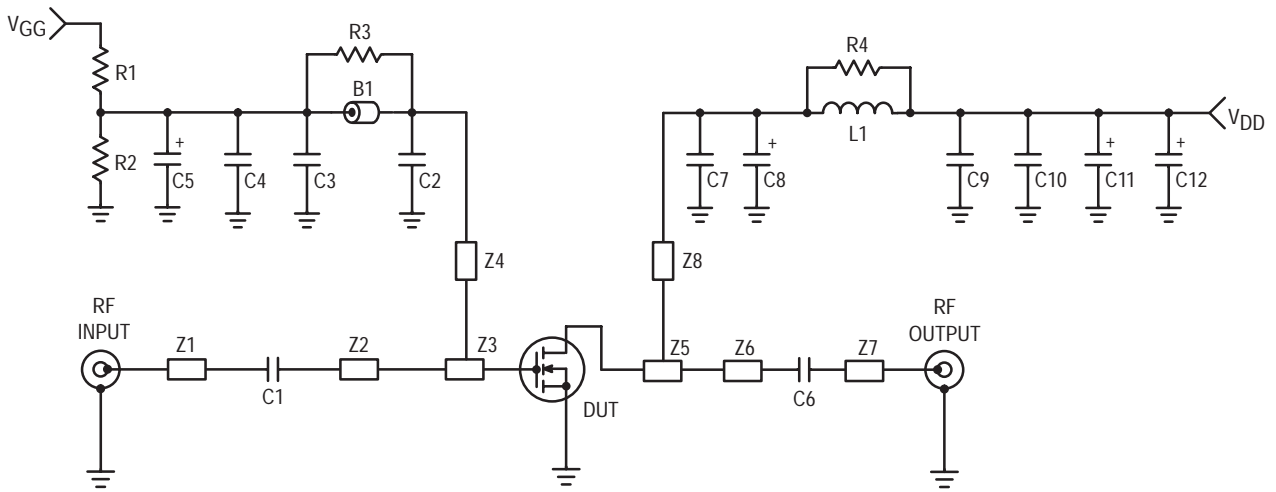
FUNCTIONAL TESTS (In Motorola Test Fixture) 2–carrier W–CDMA, 3.84 MHz Channel Bandwidth Carriers, ACPR and IM3 measured in 3.84 MHz Bandwidth. Peak/Avg. = 8.3 dB @ 0.01% Probability on CCDF.

Common–Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 19\text{ W Avg.}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$)	G_{ps}	12	13.6	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 19\text{ W Avg.}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$)	η	20	23	—	%
Third Order Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 19\text{ W Avg.}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$; IM3 measured over 3.84 MHz BW at $f_1 -10\text{ MHz}$ and $f_2 +10\text{ MHz}$ referenced to carrier channel power.)	IM3	—	–37.5	–35	dBc
Adjacent Channel Power Ratio ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 19\text{ W Avg.}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$; ACPR measured over 3.84 MHz at $f_1 -5\text{ MHz}$ and $f_2 +5\text{ MHz}$.)	ACPR	—	–41	–38	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 19\text{ W Avg.}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2112.5\text{ MHz}$, $f_2 = 2122.5\text{ MHz}$ and $f_1 = 2157.5\text{ MHz}$, $f_2 = 2167.5\text{ MHz}$)	IRL	—	–12	–9	dB
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 90\text{ W CW}$, $I_{DQ} = 1000\text{ mA}$, $f = 2170\text{ MHz}$ VSWR = 5:1, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Two-Tone Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	G_{ps}	—	13.6	—	dB
Two-Tone Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	η	—	36	—	%
Two-Tone Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	IMD	—	-31	—	dBc
Input Return Loss ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 90\text{ W PEP}$, $I_{DQ} = 1000\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	IRL	—	-12	—	dB
P_{out} , 1 dB Compression Point ($V_{DD} = 28\text{ Vdc}$, $I_{DQ} = 1000\text{ mA}$, $f = 2170\text{ MHz}$)	P1dB	—	100	—	W



Z1	0.750" x 0.084" Transmission Line
Z2	1.015" x 0.084" Transmission Line
Z3	0.480" x 0.800" Transmission Line
Z4	0.750" x 0.050" Transmission Line
Z5	0.610" x 0.800" Transmission Line
Z6	0.885" x 0.084" Transmission Line
Z7	0.720" x 0.084" Transmission Line
Z8	0.800" x 0.070" Transmission Line

Board 0.030" Glass Teflon[®],
Keene GX-0300-55-22, $\epsilon_r = 2.55$
PCB Etched Circuit Boards
MRF21085 Rev. 3, CMR

Figure 1. MRF21085 Test Circuit Schematic

Table 1. MRF21085 Component Designations and Values

Designators	Description
B1	Short Ferrite Bead, Fair Rite, #2743019447
C1, C6	43 pF Chip Capacitors, ATC #100B430JCA500X
C2	10 pF Chip Capacitor, ATC #100B100JCA500X
C7	2.7 pF Chip Capacitor, ATC #100B2R7JCA500X
C3, C9	1000 pF Chip Capacitors, ATC #100B102JCA500X
C4, C10	0.1 μ F Chip Capacitors, Kemet #CDR33BX104AKWS
C5	1.0 μ F Tantalum Chip Capacitor, Kemet #T491C105M050
C8	10 μ F Tantalum Chip Capacitor, Kemet #T495X106K035AS4394
C11, C12	22 μ F Tantalum Chip Capacitors, Kemet #T491X226K035AS4394
L1	1 Turn, #20 AWG, 0.100" ID, Motorola
N1, N2	Type N Flange Mounts, Omni Spectra #3052-1648-10
R1	1.0 k Ω , 1/8 W Chip Resistor
R2	180 k Ω , 1/8 W Chip Resistor
R3, R4	10 Ω , 1/8 W Chip Resistors

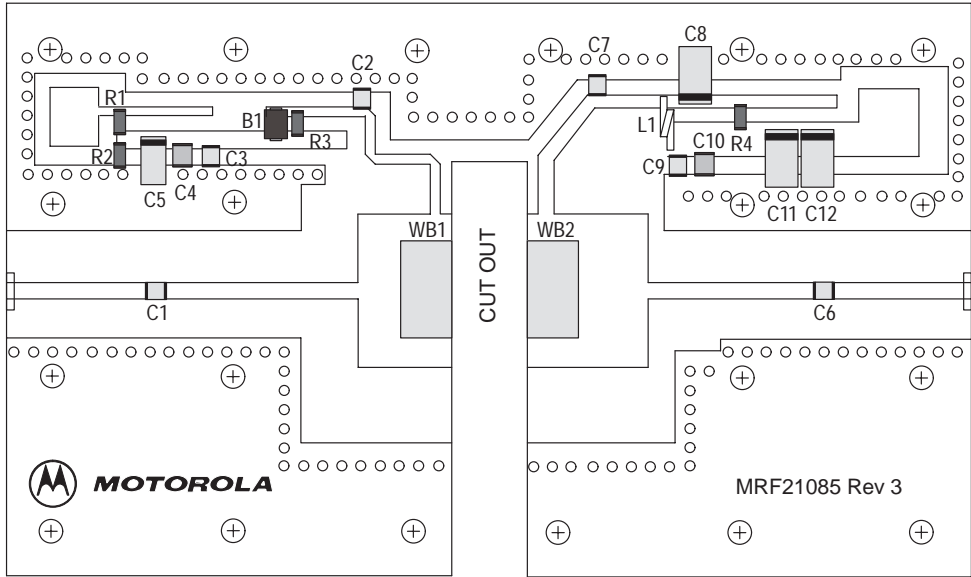


Figure 2. MRF21085 Test Circuit Component Layout

TYPICAL CHARACTERISTICS

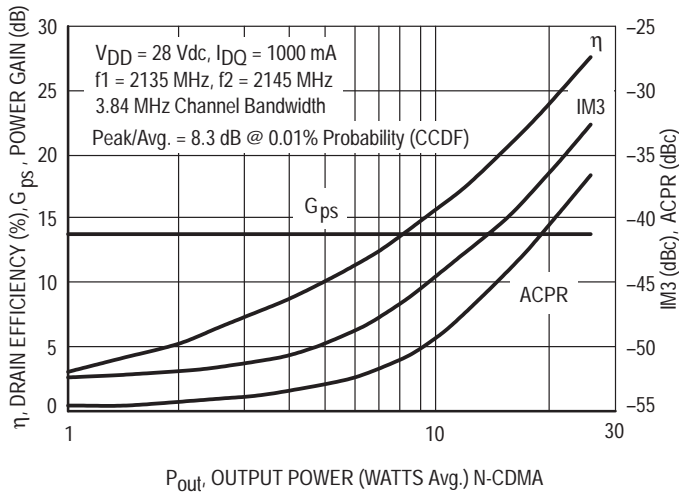


Figure 3. 2-Carrier W-CDMA ACPR, IM3, Power Gain and Drain Efficiency versus Output Power

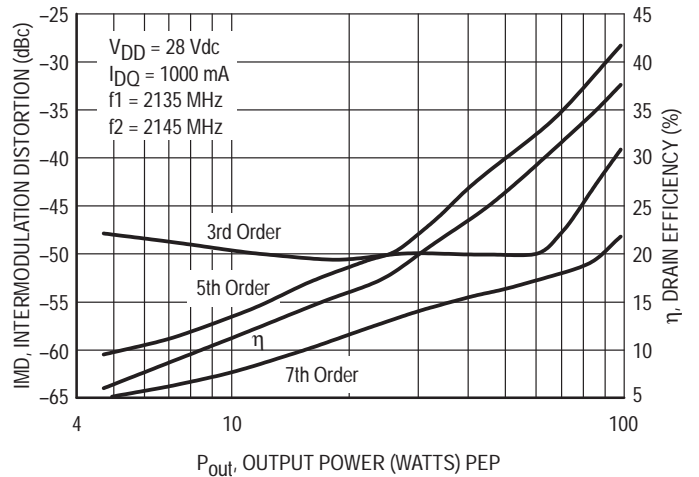


Figure 4. Intermodulation Distortion Products versus Output Power

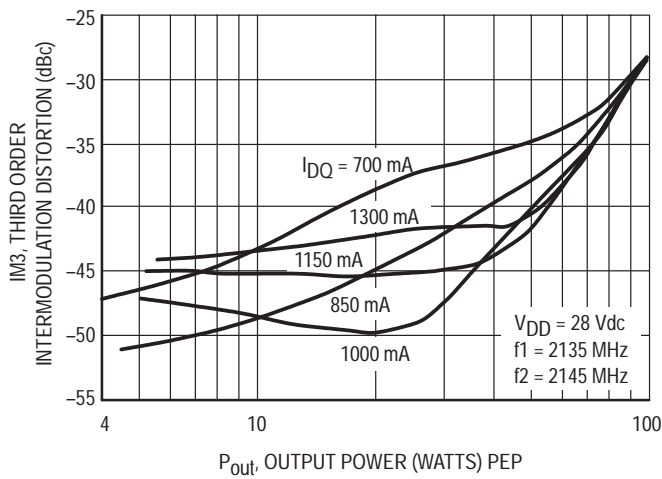


Figure 5. Third Order Intermodulation Distortion versus Output Power

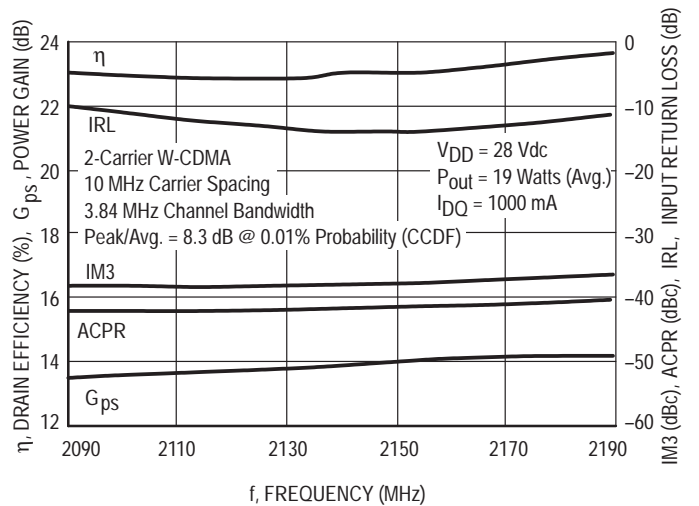


Figure 6. 2-Carrier W-CDMA Broadband Performance

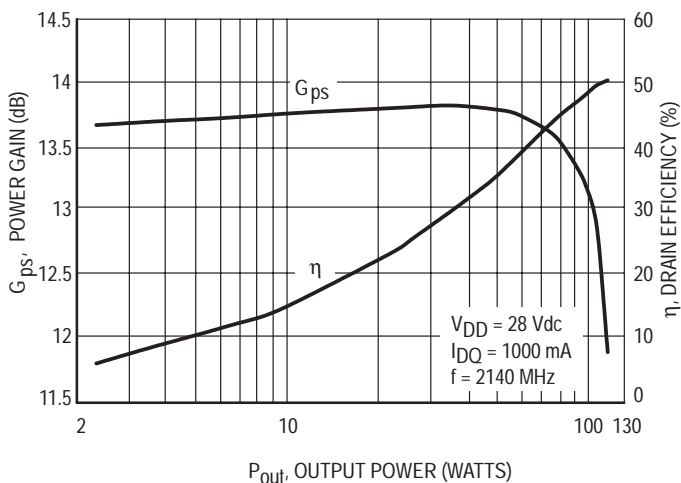


Figure 7. CW Performance

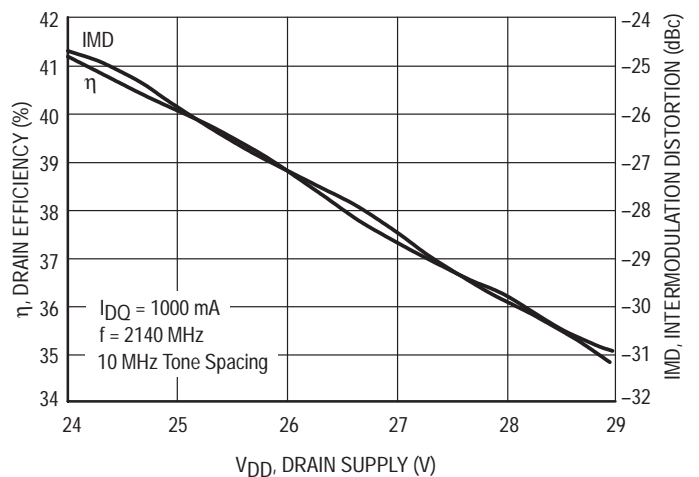


Figure 8. Two-Tone Intermodulation Distortion and Drain Efficiency versus Drain Supply

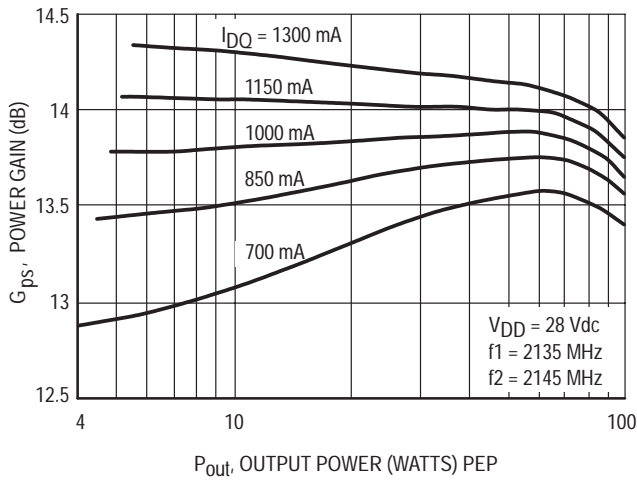


Figure 9. Two-Tone Power Gain versus Output Power

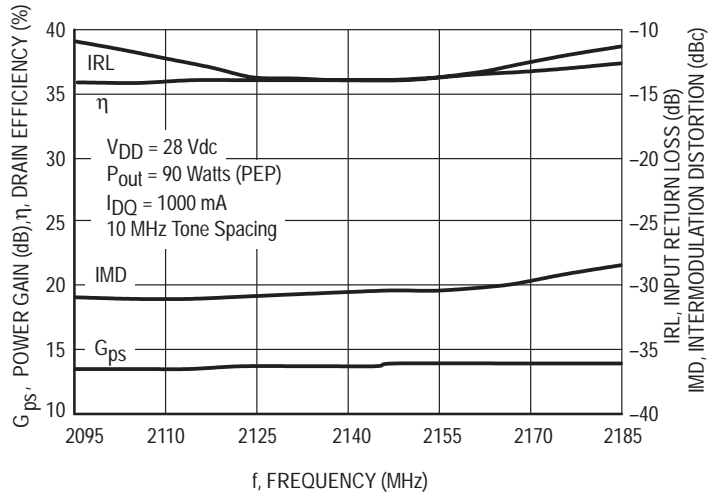


Figure 10. Two-Tone Broadband Performance

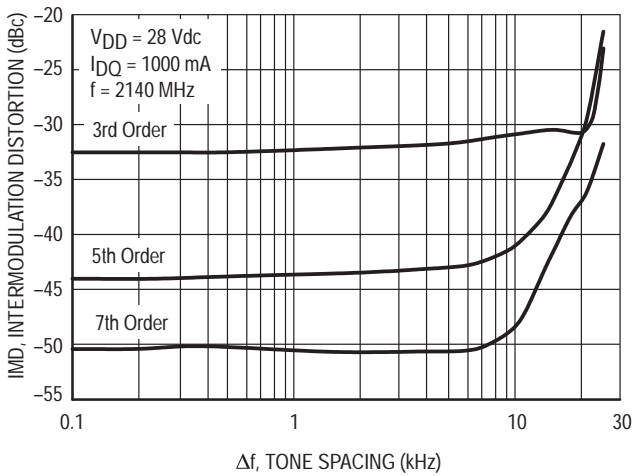


Figure 11. Intermodulation Distortion Products versus Two-Tone Spacing

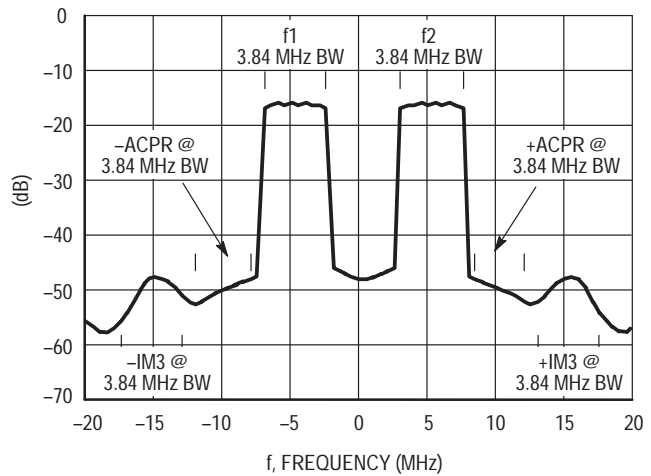
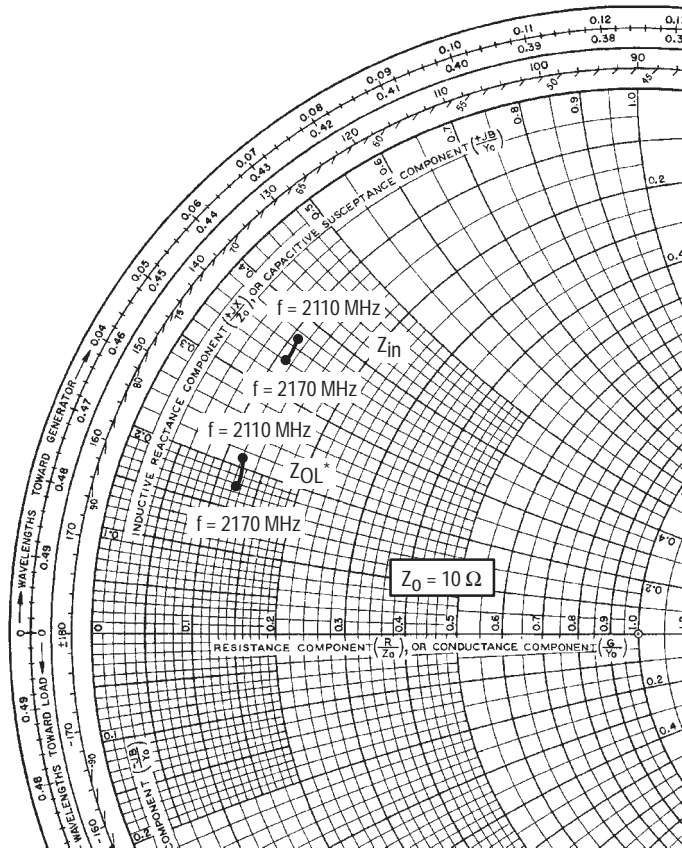


Figure 12. 2-Carrier W-CDMA Spectrum



$V_{DD} = 28\text{ V}$, $I_{DQ} = 1000\text{ mA}$, $P_{Out} = 19\text{ W (Avg.)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
2110	$1.10 + j3.71$	$1.23 + j2.10$
2140	$1.11 + j3.57$	$1.26 + j1.92$
2170	$1.12 + j3.40$	$1.25 + j1.76$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

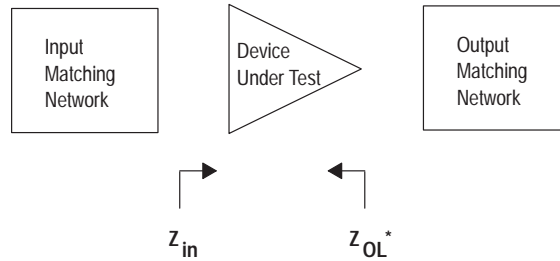


Figure 13. Series Equivalent Input and Output Impedance

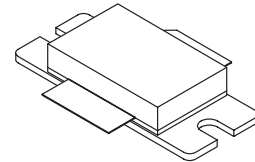
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for W-CDMA base station applications at frequencies from 2110 to 2170 MHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications.

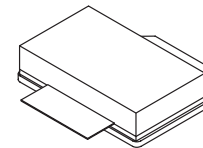
- Typical W-CDMA Performance for 2140 MHz, 28 Volts
4.096 MHz BW @ 5 MHz offset, 1 PERCH 15 DTCH:
Output Power: 11.5 Watts
Efficiency: 16%
Gain: 12.2 dB
ACPR: -45 dBc
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 28 Vdc, 2110 MHz, 90 Watts CW Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF21090
MRF21090S

2170 MHz, 90 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465B-02, STYLE 1
(MRF21090)



CASE 465C-01, STYLE 1
(MRF21090S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	270 1.54	Watts W/ $^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model MRF21090 MRF21090S	2 (Typical) 1 (Typical)
Machine Model MRF21090 MRF21090S	M3 (Typical) M4 (Typical)

THERMAL CHARACTERISTICS

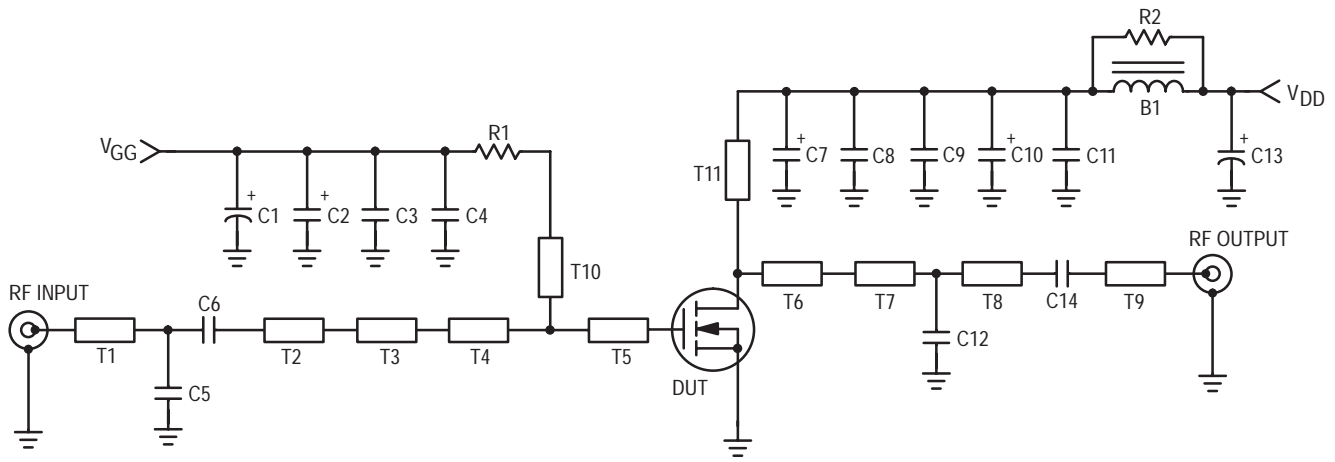
Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.65	$^\circ\text{C}/\text{W}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 100 \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Gate–Source Leakage Current ($V_{GS} = 5 \text{ Vdc}$, $V_{DS} = 0 \text{ Vdc}$)	I_{GSS}	—	—	1	μA
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μA
ON CHARACTERISTICS					
Forward Transconductance ($V_{DS} = 10 \text{ Vdc}$, $I_D = 3 \text{ A}$)	g_{fs}	—	7.2	—	S
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}$, $I_D = 300 \mu\text{A}$)	$V_{GS(th)}$	2	3	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28 \text{ V}$, $I_D = 750 \text{ mA}$)	$V_{GS(Q)}$	3	3.8	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}$, $I_D = 1 \text{ A}$)	$V_{DS(on)}$	—	0.1	0.6	Vdc
DYNAMIC CHARACTERISTICS					
Reverse Transfer Capacitance (1) ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$, $f = 1 \text{ MHz}$)	C_{rss}	—	4.2	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture)					
Common–Source Amplifier Power Gain ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 90 \text{ W PEP}$, $I_{DQ} = 750 \text{ mA}$, $f_1 = 2110.0 \text{ MHz}$, $f_2 = 2110.1 \text{ MHz}$ and $f_1 = 2170.0 \text{ MHz}$, $f_2 = 2170.1 \text{ MHz}$)	G_{ps}	10	11.7	—	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 90 \text{ W PEP}$, $I_{DQ} = 750 \text{ mA}$, $f_1 = 2110.0 \text{ MHz}$, $f_2 = 2110.1 \text{ MHz}$ and $f_1 = 2170.0 \text{ MHz}$, $f_2 = 2170.1 \text{ MHz}$)	η	30	33	—	%
Intermodulation Distortion ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 90 \text{ W PEP}$, $I_{DQ} = 750 \text{ mA}$, $f_1 = 2110.0 \text{ MHz}$, $f_2 = 2110.1 \text{ MHz}$ and $f_1 = 2170.0 \text{ MHz}$, $f_2 = 2170.1 \text{ MHz}$)	IMD	—	–30	–27.5	dBc
Input Return Loss ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 90 \text{ W PEP}$, $I_{DQ} = 750 \text{ mA}$, $f_1 = 2110.0 \text{ MHz}$, $f_2 = 2110.1 \text{ MHz}$ and $f_1 = 2170.0 \text{ MHz}$, $f_2 = 2170.1 \text{ MHz}$)	IRL	—	–12	–9.0	dB
Common–Source Amplifier Power Gain ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 75 \text{ W CW}$, $I_{DQ} = 750 \text{ mA}$, $f = 2170 \text{ MHz}$)	G_{ps}	—	11.7	—	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 75 \text{ W CW}$, $I_{DQ} = 750 \text{ mA}$, $f = 2170 \text{ MHz}$)	η	—	41	—	%
Output Mismatch Stress ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 90 \text{ W CW}$, $I_{DQ} = 750 \text{ mA}$, $f = 2110 \text{ MHz}$, $VSWR = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.



B1	Ferrite Bead, Fair Rite, 2743019447	T7	10.23 x 2.09 mm Microstrip Line
C1, C13	470 μ F, 50 V Electrolytic Capacitor	T8	6.03 x 2.09 mm Microstrip Line
C2, C10	22 μ F, 35 V Tantalum Surface Mount Chip Capacitor, Kemet	T9	23.98 x 2.09 mm Microstrip Line
C3, C9	20 nF, RF Chip Capacitor, 100B203MCA500X, ATC	T10	29.82 x 1.15 mm Microstrip Line
C4, C8	5.1 pF, RF Chip Capacitor, 100B5R1CCA500X, ATC	T11	17.08 x 1.15 mm Microstrip Line
C5, C12	0.4 – 2.5 pF, Variable Capacitor, Johanson Gigatrim	WS1, WS2	Beryllium Copper Wear Blocks 5 mils Thick
C6	10 pF, RF Chip Capacitor, 100B100JCA500X, ATC		Brass Banana Jack and Nut
C7	1 μ F, 35 V Tantalum Surface Mount Chip Capacitor, Kemet		Red Banana Jack and Nut
C11	1 nF, RF Chip Capacitor, 100B102JCA500X, ATC		Green Banana Jack and Nut
C14	8.2 pF, RF Chip Capacitor, 100B8R2CCA500X, ATC		Type N Jack Connectors, 3052–1648–10, Omni Specra
R1	13 Ω , 1/4 W Chip Resistor, RM73B2B130JT, Garret Instrument		4–40 Head Screws 0.125" Long
R2	12 Ω , 1/4 W Chip Resistor, RM73B2B120JT, Garret Instrument		4–40 Head Screws 0.188" Long
T1	30.7 x 2.09 mm Microstrip Line		4–40 Head Screws 0.312" Long
T2	5.99 x 2.09 mm Microstrip Line		4–40 Head Screws 0.438" Long
T3	7.55 x 9.89 mm Microstrip Line	Endplates Brass	Endplates for Copper Bedstead
T4	3.77 x 15.71 mm Microstrip Line	Bedstead	Copper Bedstead/Heatsink
T5	6.89 x 26.17 mm Microstrip Line	Insert	Copper Bedstead Insert
T6	14.93 x 32.05 mm Microstrip Line	Raw PCB	0.030" Glass Teflon [®] , 2 oz Copper Clad
			3" x 5" Arion
		RF Circuit	3" x 5" Copper Clad PCB Teflon [®] , MRF21090, CMR

Figure 1. MRF21090 Test Circuit Schematic

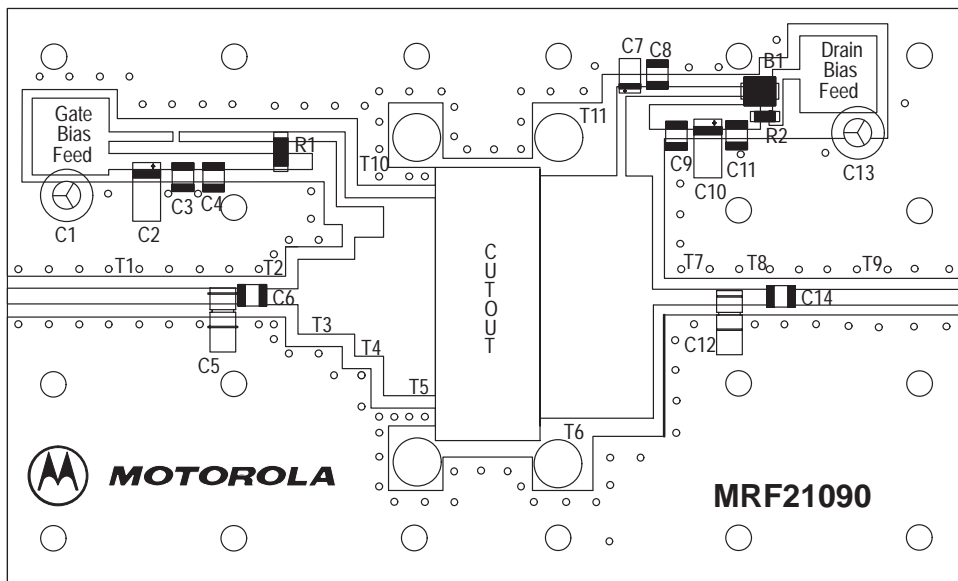


Figure 2. Component Parts Layout

TYPICAL PERFORMANCE (IN MOTOROLA TEST FIXTURE)

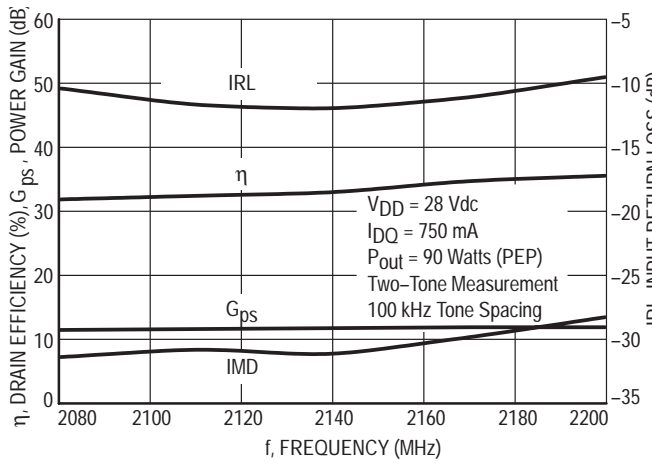


Figure 3. Class AB Broadband Circuit Performance

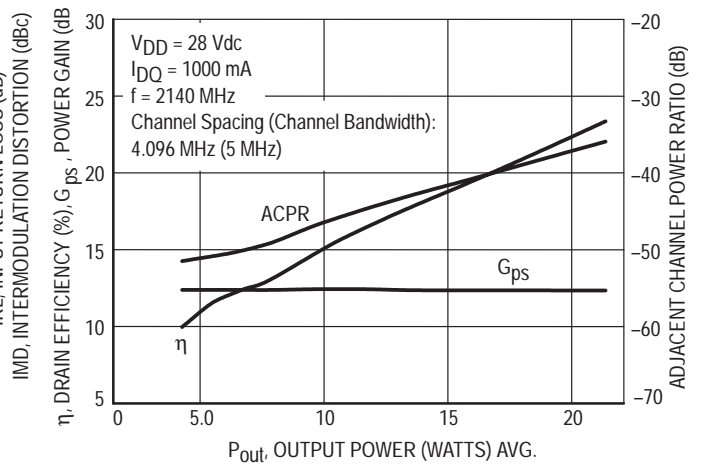


Figure 4. CDMA ACPR, Power Gain and Drain Efficiency versus Output Power

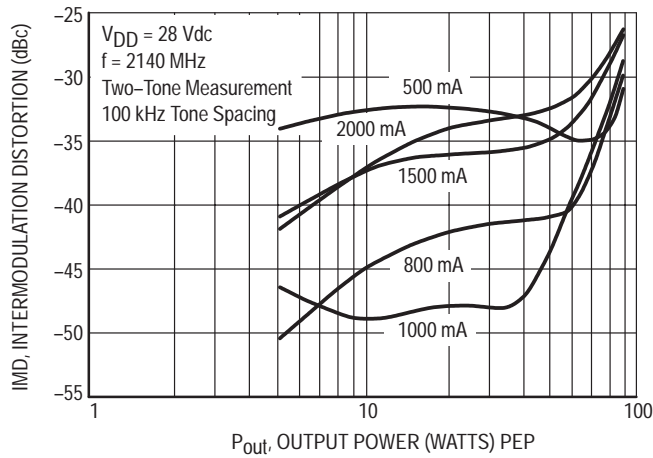


Figure 5. Intermodulation Distortion versus Output Power

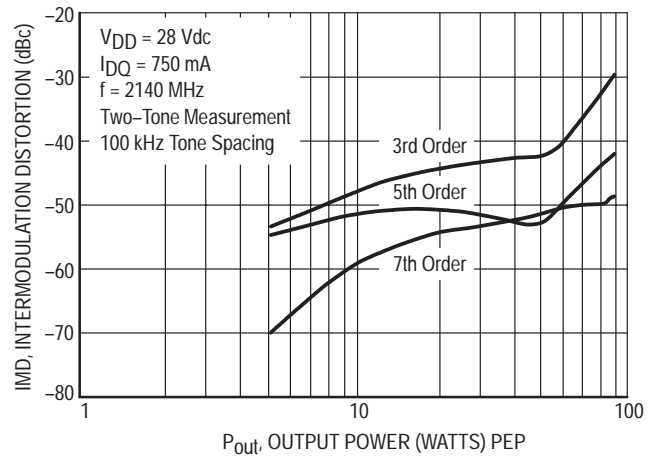


Figure 6. Intermodulation Distortion Products versus Output Power

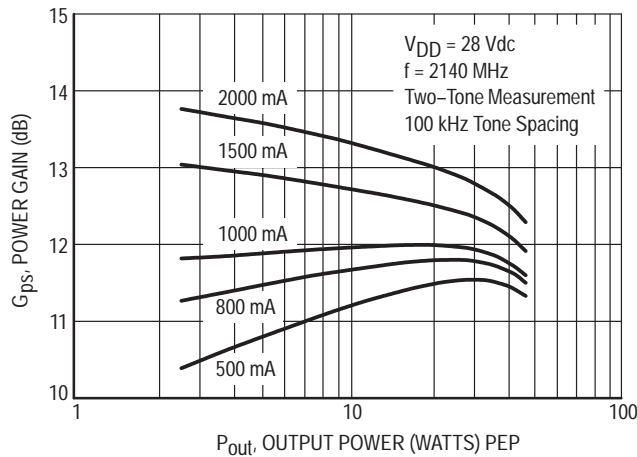


Figure 7. Power Gain versus Output Power

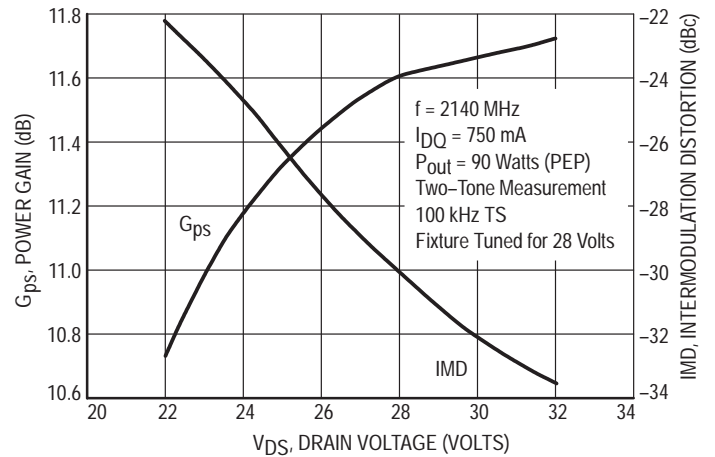
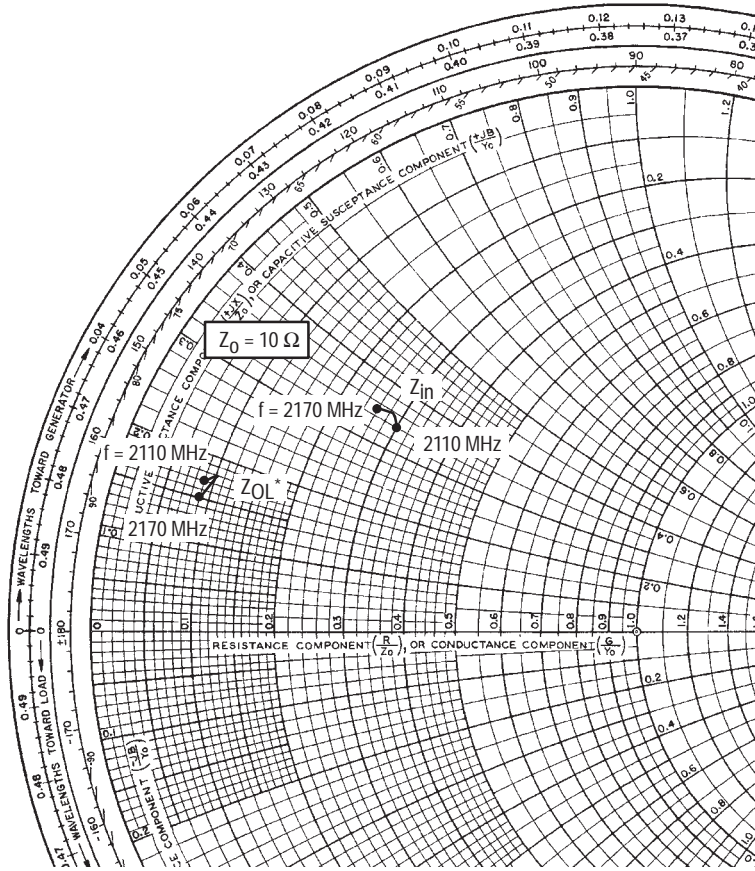


Figure 8. Power Gain and Intermodulation Distortion versus Supply Voltage



$V_{DD} = 28\text{ V}$, $I_{DQ} = 750\text{ mA}$, $P_{out} = 90\text{ W (PEP)}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
2110	$3.03 + j3.40$	$0.92 + j1.67$
2140	$3.02 + j3.46$	$0.97 + j1.80$
2170	$2.60 + j3.50$	$0.90 + j1.52$

Z_{in} = Complex conjugate of the source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given power, voltage, IMD, bias current and frequency.

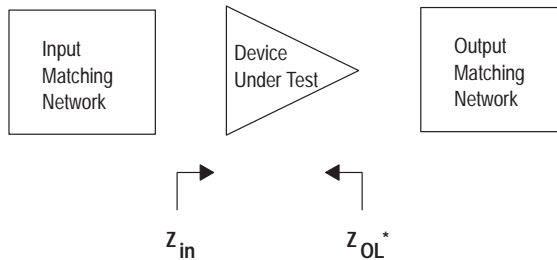


Figure 9. Series Equivalent Input and Output Impedance

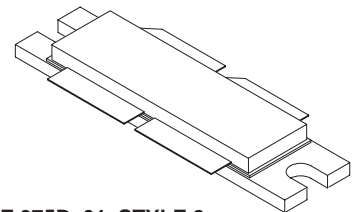
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for W-CDMA base station applications at frequencies from 2110 to 2170 MHz. Suitable for FM, TDMA, CDMA and multicarrier amplifier applications. To be used in Class AB for PCN-PCS/cellular radio and WLL applications.

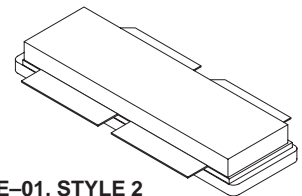
- W-CDMA Performance @ -45 dBc, 5 MHz Offset, 15 DTCH, 1 Perch
Output Power — 14 Watts (Avg.)
Power Gain — 11.5 dB
Efficiency — 16%
- Internally Matched, Controlled Q, for Ease of Use
- High Gain, High Efficiency, High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 10:1 VSWR, @ 28 Vdc, 2170 MHz, 120 Watts (CW) Output Power
- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters

MRF21120
MRF21120S

2170 MHz, 120 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 375D-01, STYLE 2
(MRF21120)



CASE 375E-01, STYLE 2
(MRF21120S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	389 2.22	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.45	$^\circ\text{C}/\text{W}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

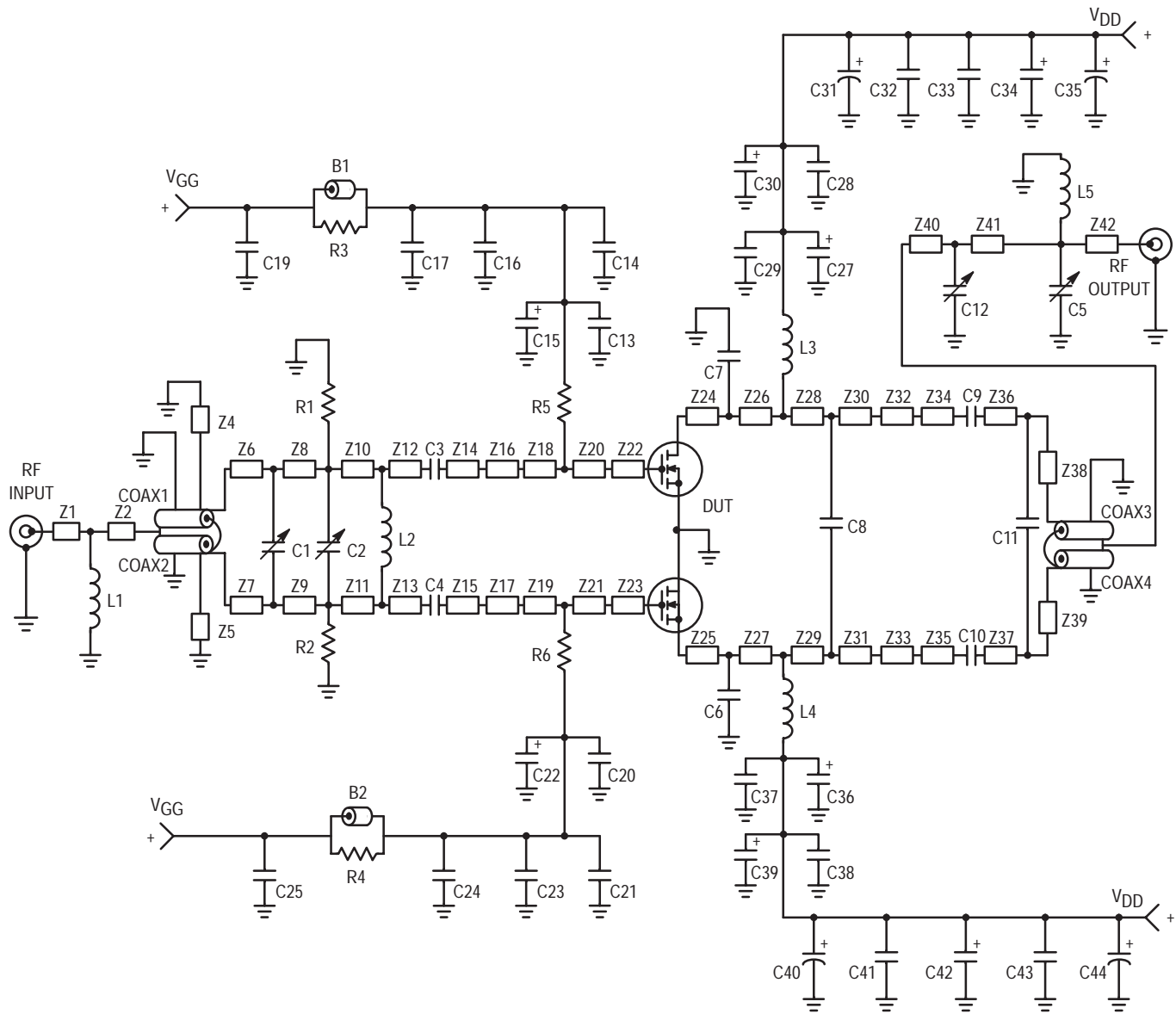
ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)					
Drain–Source Breakdown Voltage ($V_{GS} = 0, I_D = 20 \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Gate–Source Leakage Current ($V_{GS} = 5 \text{ Vdc}, V_{DS} = 0 \text{ Vdc}$)	I_{GSS}	—	—	1	μA
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 28 \text{ Vdc}, V_{GS} = 0$)	I_{DSS}	—	—	10	μA
ON CHARACTERISTICS (1)					
Forward Transconductance ($V_{DS} = 10 \text{ Vdc}, I_D = 2 \text{ A}$)	g_{fs}	—	4.8	—	S
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}, I_D = 200 \mu\text{A}$)	$V_{GS(th)}$	2.5	3	3.8	Vdc
Gate Quiescent Voltage ($V_{DS} = 28 \text{ V}, I_D = 500 \text{ mA}$)	$V_{GS(Q)}$	3	3.9	5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}, I_D = 2 \text{ A}$)	$V_{DS(on)}$	—	0.38	0.5	Vdc
DYNAMIC CHARACTERISTICS (1)					
Reverse Transfer Capacitance ($V_{DS} = 28 \text{ Vdc}, V_{GS} = 0, f = 1 \text{ MHz}$)	C_{rss}	—	2.8	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture) (2)					
Common–Source Amplifier Power Gain ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2170.0 \text{ MHz}, f_2 = 2170.1 \text{ MHz}$)	G_{ps}	10.5 10.4	11.4 11.2	— —	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2170.0 \text{ MHz}, f_2 = 2170.1 \text{ MHz}$)	η	30	34.5	—	%
Intermodulation Distortion ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2170.0 \text{ MHz}, f_2 = 2170.1 \text{ MHz}$)	IMD	— —	–31 –31	–28 –27	dB
Input Return Loss ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2170.0 \text{ MHz}, f_2 = 2170.1 \text{ MHz}$)	IRL	9	12	—	dB
Common–Source Amplifier Power Gain ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2140.0 \text{ MHz}, f_2 = 2140.1 \text{ MHz}$)	G_{ps}	—	11.5	—	dB
Common–Source Amplifier Power Gain ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2110.0 \text{ MHz}, f_2 = 2110.1 \text{ MHz}$)	G_{ps}	—	11.5	—	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2110.0 \text{ MHz}, f_2 = 2110.1 \text{ MHz}$)	η	—	34.5	—	%
Intermodulation Distortion ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2110.0 \text{ MHz}, f_2 = 2110.1 \text{ MHz}$)	IMD	—	–31	—	dB
Input Return Loss ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W PEP}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2110.0 \text{ MHz}, f_2 = 2110.1 \text{ MHz}$)	IRL	—	12	—	dB
Power Output, 1 dB Compression Point ($V_{DD} = 28 \text{ Vdc}, CW, I_{DQ} = 2 \times 500 \text{ mA}, f_1 = 2170.0 \text{ MHz}$)	P_{1dB}	—	120	—	Watts
Common–Source Amplifier Power Gain ($V_{DD} = 28 \text{ Vdc}, P_{out} = 120 \text{ W CW}, I_{DQ} = 2 \times 500 \text{ mA},$ $f_1 = 2170.0 \text{ MHz}$)	G_{ps}	—	10.5	—	dB

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W CW}$, $I_{DQ} = 2 \times 500\text{ mA}$, $f_1 = 2170.0\text{ MHz}$)	η	—	42	—	%
Output Mismatch Stress ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 120\text{ W CW}$, $I_{DQ} = 2 \times 500\text{ mA}$, $f = 2.17\text{ GHz}$, $VSWR = 10:1$, All Phase Angles at Frequency of Tests)	Ψ	No Degradation In Output Power Before and After Test			

- (1) Each side of device measured separately.
(2) Device measured in push-pull configuration.



B1, B2	Ferrite Bead, Fair Rite	Z2	0.320" x 0.080" Microstrip
C1, C2, C12	0.6 – 4.5 pF, Variable Capacitor, Johanson Gigatrim	Z4, Z5	1.050" x 0.080" Microstrip
C3, C4, C9, C10	10 pF, B Case Chip Capacitor, ATC	Z6, Z7	0.120" x 0.080" Microstrip
C5	0.4 – 2.5 pF, Variable Capacitor, Johanson Gigatrim	Z8, Z9	0.140" x 0.080" Microstrip
C6, C7	2.0 pF, B Case Chip Capacitor, ATC	Z10, Z11	0.610" x 0.080" Microstrip
C8	0.5 pF, B Case Chip Capacitor, ATC	Z12, Z13	0.135" x 0.080" Microstrip
C11	0.2 pF, B Case Chip Capacitor, ATC	Z14, Z15	0.130" x 0.080" Microstrip
C13, C20, C29, C37	5.1 pF, B Case Chip Capacitor, ATC	Z16, Z17	0.300" x 0.350" Microstrip
C14, C21, C28, C38	91 pF, B Case Chip Capacitor, ATC	Z18, Z19	0.150" x 0.080" Microstrip
C15, C22, C27, C34, C36, C42	22 μ F, 35 V, Tantalum Surface Mount Chip Capacitor, Kemet	Z20, Z21	0.075" x 0.500" Microstrip
C16, C23, C33, C43	0.039 μ F, B Case Chip Capacitor, ATC	Z22, Z23	0.330" x 0.500" Microstrip
C17, C24, C32, C41	1000 pF, B Case Chip Capacitor, ATC	Z24, Z25	0.100" x 0.550" Microstrip
C19, C25	0.022 μ F, B Case Chip Capacitor, ATC	Z26, Z27	0.175" x 0.550" Microstrip
C30, C39	1.0 μ F, 35 V, Tantalum Surface Mount Chip Capacitor, Kemet	Z28, Z29	0.045" x 0.550" Microstrip
C31, C40	100 μ F, 50 V, Electrolytic Capacitor, Sprague	Z30, Z31	0.190" x 0.325" Microstrip
C35, C44	470 μ F, 63 V, Electrolytic Capacitor, Sprague	Z32, Z33	0.080" x 0.325" Microstrip
Coax1, Coax2	25 Ω , Semi Rigid Coax, 70 mil OD, 1.05" Long	Z34, Z35	0.515" x 0.080" Microstrip
Coax3, Coax4	50 Ω , Semi Rigid Coax, 85 mil OD, 1.05" Long	Z36, Z37	0.020" x 0.080" Microstrip
L1, L5	5.0 nH, Minispring Inductor, Coilcraft	Z38, Z39	0.565" x 0.080" Microstrip
L2	8.0 nH, Minispring Inductor, Coilcraft	Z40	0.100" x 0.080" Microstrip
L3, L4	7.15 nH, Microspring Inductor, Coilcraft	Z41	0.470" x 0.080" Microstrip
R1, R2	1 k Ω , Fixed Metal Film Resistor, 1/4 W, Dale	Z42	0.100" x 0.080" Microstrip
R3, R4	270 Ω , Fixed Film Chip Resistor, 1/8 W, Dale	Board Material	0.03" Teflon [®] , $\epsilon_r = 2.55$ Copper Clad, 2 oz. Cu
R5, R6	1.2 k Ω , Fixed Film Chip Resistor, 1/8 W, Dale	Connectors	N-Type Panel Mount, Stripline
Z1	0.150" x 0.080" Microstrip		

Figure 1. 2.1 – 2.2 GHz Broadband Test Circuit Schematic

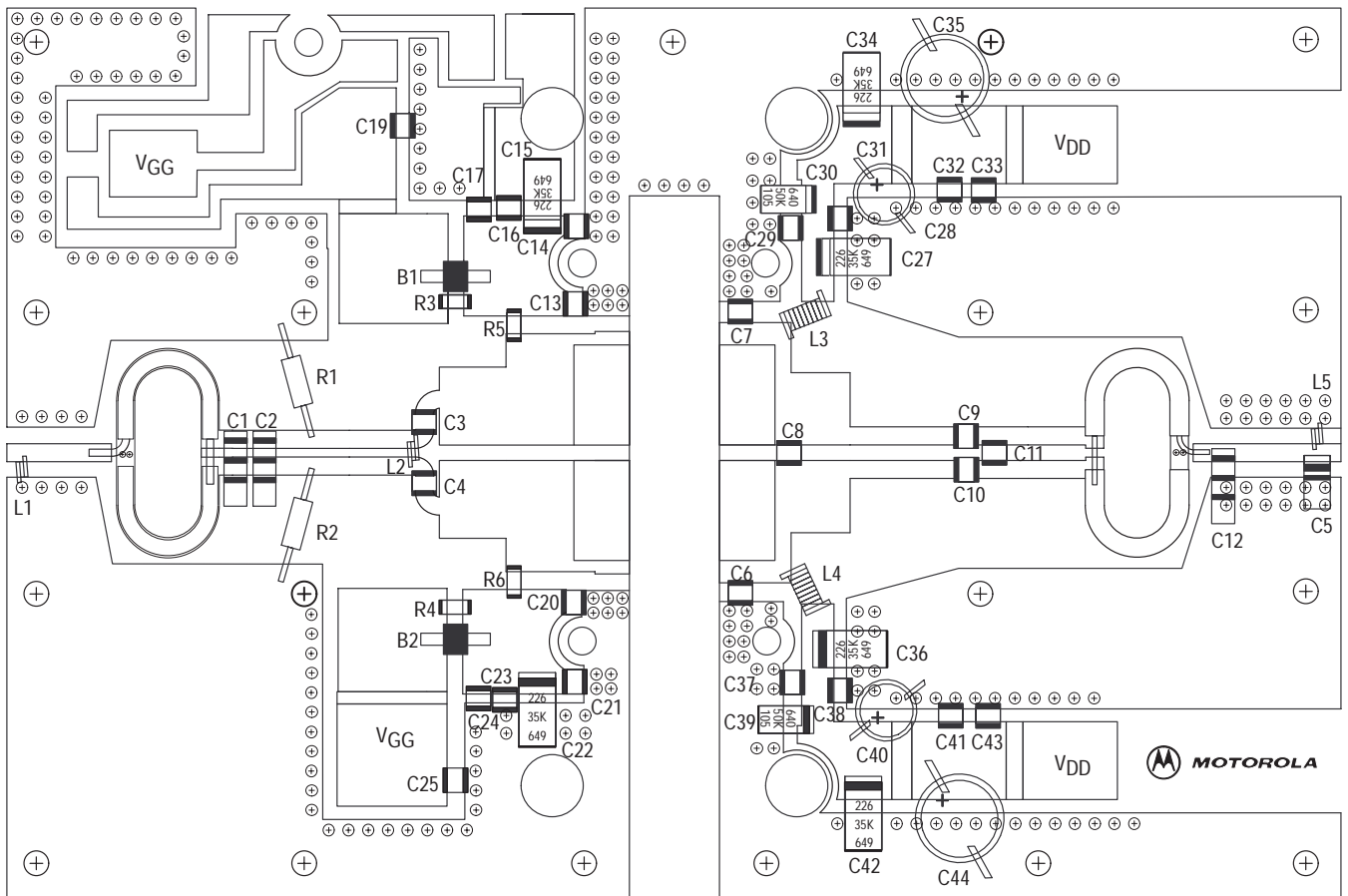


Figure 2. Component Parts Layout

TYPICAL CHARACTERISTICS

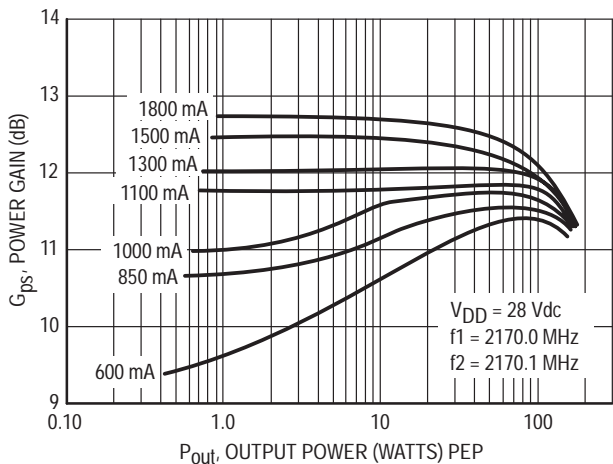


Figure 3. Power Gain versus Output Power

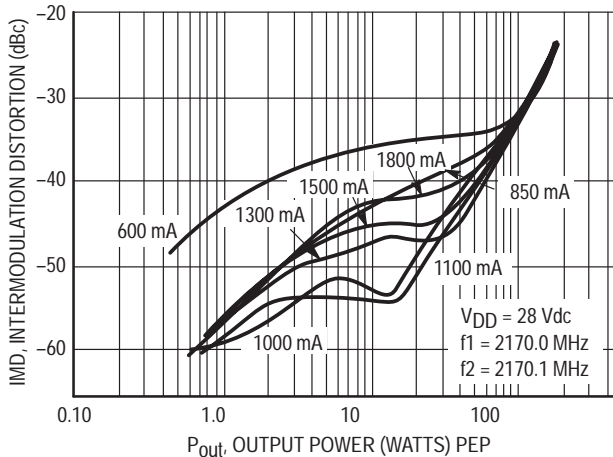


Figure 4. Intermodulation Distortion versus Output Power

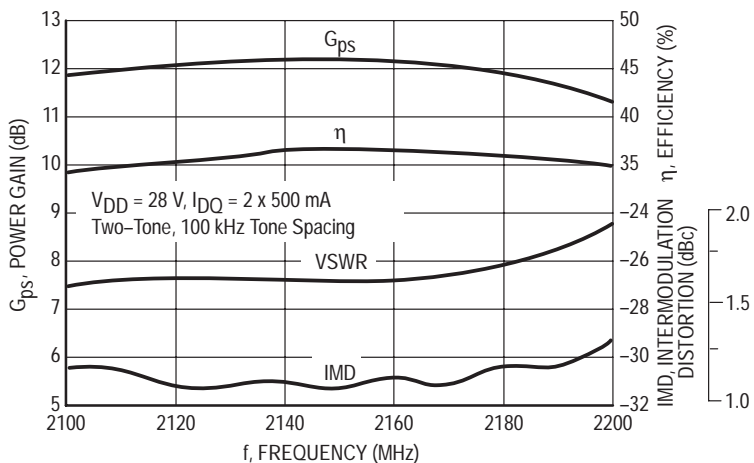


Figure 5. Class AB Broadband Circuit Performance

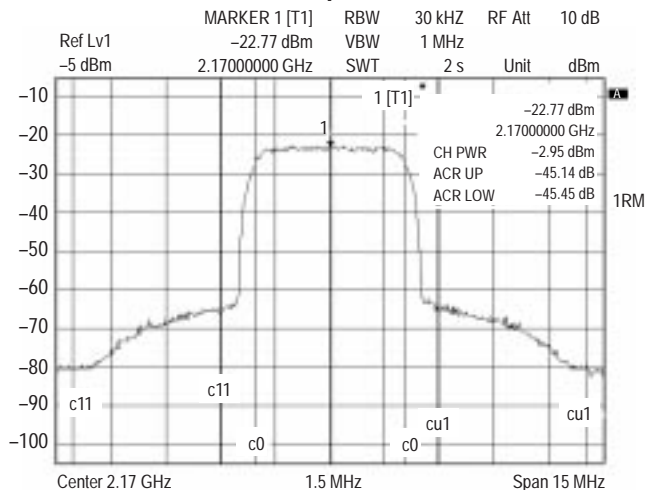


Figure 6. 2.17 GHz W-CDMA Mask at 14 Watts (Avg.), 5 MHz Offset, 15 DTCH, 1 Perch

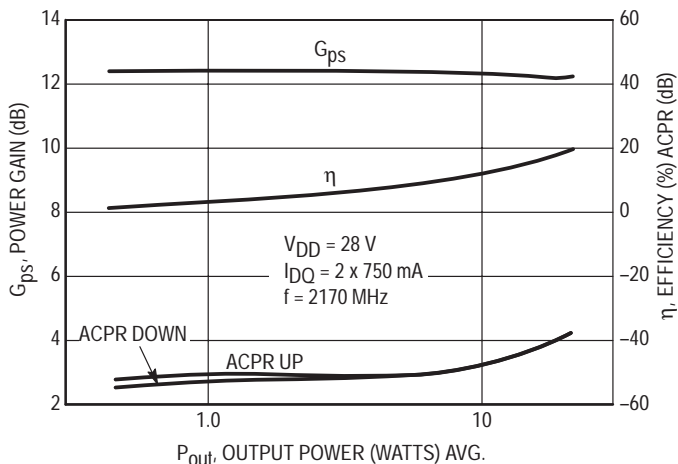


Figure 7. Power Gain, Efficiency, ACPR versus Output Power (W-CDMA)

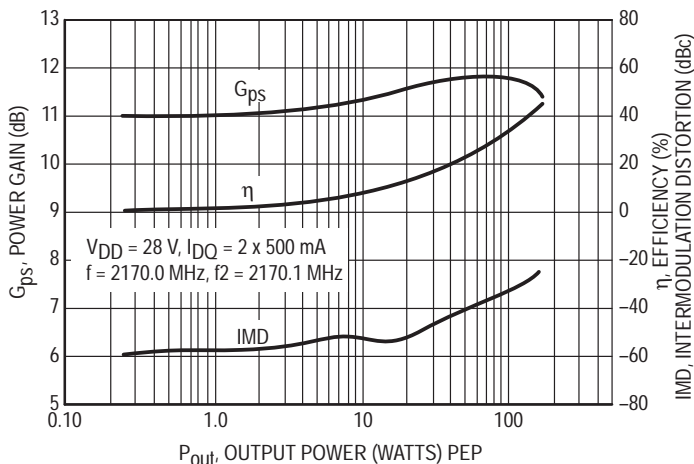
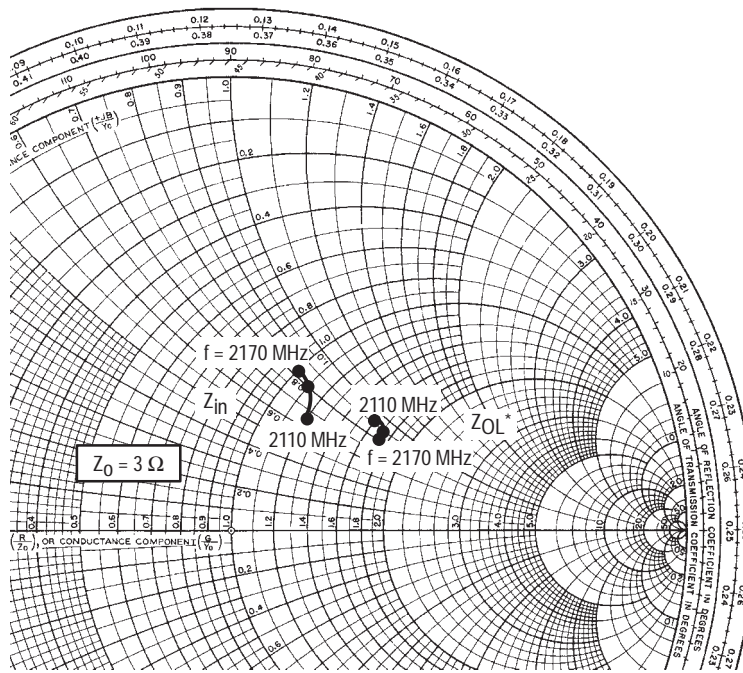


Figure 8. Power Gain, Efficiency, IMD versus Output Power



$V_{DD} = 28 \text{ V}$, $I_{DQ} = 2 \times 500 \text{ mA}$, $P_{out} = 120 \text{ Watts PEP}$

f MHz	Z_{in} Ω	Z_{OL}^* Ω
2110	$3.7 + j2.0$	$4.9 + j2.8$
2140	$3.5 + j2.4$	$5.1 + j2.7$
2170	$3.1 + j2.5$	$5.2 + j2.5$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

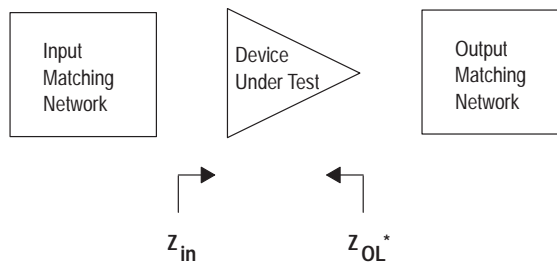


Figure 9. Series Equivalent Input and Output Impedance

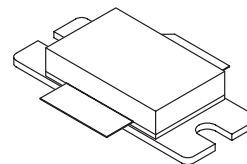
The RF Sub-Micron MOSFET Line
RF Power Field Effect Transistors
N-Channel Enhancement-Mode Lateral MOSFETs

Designed for W-CDMA base station applications at frequencies from 2110 to 2170 MHz. Suitable for TDMA, CDMA and multicarrier amplifier applications. To be used in class AB for PCN-PCS/cellular radio and WLL applications.

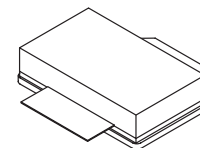
- Typical 2-carrier W-CDMA Performance for $V_{DD} = 28$ Volts, $I_{DQ} = 1600$ mA, $f_1 = 2.1125$ GHz, $f_2 = 2.1225$ GHz, Channel bandwidth = 3.84 MHz, adjacent channels at ± 5 MHz, ACPR and IM3 measured in 3.84 MHz bandwidth. Peak/Avg = 8.5 dB @ 0.01% probability on CCDF.
Output Power: 20 Watts
Efficiency: 18%
Gain: 13 dB
IM3: -43 dBc
ACPR: -45 dBc
- 100% Tested under 2-carrier W-CDMA
- Internally Matched for Ease of Use
- High Gain, High Efficiency and High Linearity
- Integrated ESD Protection
- Ease of Design for Gain and Insertion Phase Flatness
- Capable of Handling 5:1 VSWR, @ 28 Vdc, 2170 MHz, 125 Watts (CW) Output Power
- Excellent Thermal Stability

MRF21125
MRF21125S

2170 MHz, 125 W, 28 V
LATERAL N-CHANNEL
BROADBAND
RF POWER MOSFETs



CASE 465B-02, STYLE 1
(MRF21125)



CASE 465C-01, STYLE 1
(MRF21125S)

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Drain-Source Voltage	V_{DSS}	65	Vdc
Gate-Source Voltage	V_{GS}	+15, -0.5	Vdc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ Derate above 25°C	P_D	330 1.89	Watts $\text{W}/^\circ\text{C}$
Storage Temperature Range	T_{stg}	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	T_J	200	$^\circ\text{C}$

ESD PROTECTION CHARACTERISTICS

Test Conditions	Class
Human Body Model	2 (Typical)
Machine Model	M3 (Typical)

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.53	$^\circ\text{C}/\text{W}$

NOTE - **CAUTION** - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS					
Drain–Source Breakdown Voltage ($V_{GS} = 0$, $I_D = 100 \mu\text{A}$)	$V_{(BR)DSS}$	65	—	—	Vdc
Gate–Source Leakage Current ($V_{GS} = 5 \text{ Vdc}$, $V_{DS} = 0 \text{ Vdc}$)	I_{GSS}	—	—	1	μA
Zero Gate Voltage Drain Leakage Current ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$)	I_{DSS}	—	—	10	μA
ON CHARACTERISTICS					
Forward Transconductance ($V_{DS} = 10 \text{ Vdc}$, $I_D = 3 \text{ A}$)	g_{fs}	—	10.8	—	S
Gate Threshold Voltage ($V_{DS} = 10 \text{ V}$, $I_D = 300 \mu\text{A}$)	$V_{GS(th)}$	2	—	4	Vdc
Gate Quiescent Voltage ($V_{DS} = 28 \text{ V}$, $I_D = 1300 \text{ mA}$)	$V_{GS(Q)}$	2.5	3.9	4.5	Vdc
Drain–Source On–Voltage ($V_{GS} = 10 \text{ V}$, $I_D = 1 \text{ A}$)	$V_{DS(on)}$	—	0.12	—	Vdc
DYNAMIC CHARACTERISTICS					
Reverse Transfer Capacitance (1) ($V_{DS} = 28 \text{ Vdc}$, $V_{GS} = 0$, $f = 1 \text{ MHz}$)	C_{rss}	—	5.4	—	pF
FUNCTIONAL TESTS (In Motorola Test Fixture) 2–carrier W–CDMA, 3.84 MHz Channel Bandwidth, IM3 measured in 3.84 MHz Bandwidth. Peak/Avg = 8.5 dB @ 0.01% probability on CCDF.					
Common–Source Amplifier Power Gain ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 20 \text{ W Avg}$, 2–carrier W–CDMA, $I_{DQ} = 1600 \text{ mA}$, $f_1 = 2112.5 \text{ MHz}$, $f_2 = 2122.5 \text{ MHz}$ and $f_1 = 2157.5 \text{ MHz}$, $f_2 = 2167.5 \text{ MHz}$)	G_{ps}	12	13	—	dB
Drain Efficiency ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 20 \text{ W Avg}$, 2–carrier W–CDMA, $I_{DQ} = 1600 \text{ mA}$, $f_1 = 2112.5 \text{ MHz}$, $f_2 = 2122.5 \text{ MHz}$ and $f_1 = 2157.5 \text{ MHz}$, $f_2 = 2167.5 \text{ MHz}$)	η	17	18	—	%
Third Order Intermodulation Distortion ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 20 \text{ W Avg}$, 2–carrier W–CDMA, $I_{DQ} = 1600 \text{ mA}$, $f_1 = 2112.5 \text{ MHz}$, $f_2 = 2122.5 \text{ MHz}$ and $f_1 = 2157.5 \text{ MHz}$, $f_2 = 2167.5 \text{ MHz}$; IM3 measured at $f_1 -15 \text{ MHz}$ and $f_2 +15 \text{ MHz}$ referenced to carrier channel power.)	IM3	—	–43	–40	dBc
Adjacent Channel Power Ratio ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 20 \text{ W Avg}$, 2–carrier W–CDMA, $I_{DQ} = 1600 \text{ mA}$, $f_1 = 2112.5 \text{ MHz}$, $f_2 = 2122.5 \text{ MHz}$ and $f_1 = 2157.5 \text{ MHz}$, $f_2 = 2167.5 \text{ MHz}$; ACPR measured at $f_1 -10 \text{ MHz}$ and $f_2 +10 \text{ MHz}$ referenced to carrier channel power.)	ACPR	—	–45	–40	dBc
Input Return Loss ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 20 \text{ W Avg}$, 2–carrier W–CDMA, $I_{DQ} = 1600 \text{ mA}$, $f_1 = 2112.5 \text{ MHz}$, $f_2 = 2122.5 \text{ MHz}$ and $f_1 = 2157.5 \text{ MHz}$, $f_2 = 2167.5 \text{ MHz}$)	IRL	—	–12	–9.0	dB
Output Mismatch Stress ($V_{DD} = 28 \text{ Vdc}$, $P_{out} = 125 \text{ W CW}$, $I_{DQ} = 1600 \text{ mA}$, $f = 2170 \text{ MHz}$, $V_{SWR} = 5:1$, All Phase Angles at Frequency of Test)	Ψ	No Degradation In Output Power Before and After Test			

(1) Part is internally matched both on input and output.

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

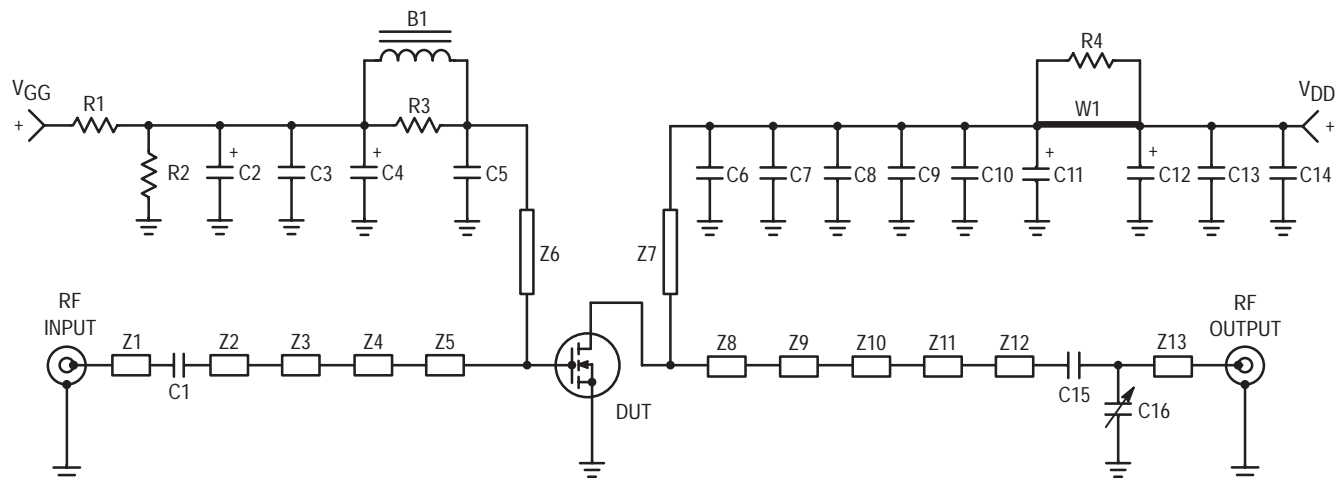
Characteristic	Symbol	Min	Typ	Max	Unit
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TYPICAL TWO-TONE PERFORMANCE (In Motorola Test Fixture)

Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 125\text{ W PEP}$, $I_{DQ} = 1600\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	G_{ps}	—	12	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 125\text{ W PEP}$, $I_{DQ} = 1600\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	η	—	34	—	%
Intermodulation Distortion ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 125\text{ W PEP}$, $I_{DQ} = 1600\text{ mA}$, $f_1 = 2110\text{ MHz}$, $f_2 = 2120\text{ MHz}$ and $f_1 = 2160\text{ MHz}$, $f_2 = 2170\text{ MHz}$)	IMD	—	-30	—	dBc

TYPICAL CW PERFORMANCE

Common-Source Amplifier Power Gain ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 125\text{ W CW}$, $I_{DQ} = 1600\text{ mA}$, $f = 2170.0\text{ MHz}$)	G_{ps}	—	11.5	—	dB
Drain Efficiency ($V_{DD} = 28\text{ Vdc}$, $P_{out} = 125\text{ W CW}$, $I_{DQ} = 1600\text{ mA}$, $f = 2170.0\text{ MHz}$)	η	—	46	—	%



Z1	1.212" x 0.082" Microstrip	Z9	0.179" x 0.219" Microstrip
Z2	0.236" x 0.082" Microstrip	Z10	0.100" x 0.336" Microstrip
Z3	0.086" x 0.254" Microstrip	Z11	0.534" x 0.142" Microstrip
Z4	0.357" x 0.082" Microstrip	Z12	0.089" x 0.080" Microstrip
Z5	0.274" x 1.030" Microstrip	Z13	0.620" x 0.080" Microstrip
Z6	0.466" x 0.050" Microstrip	Raw Board	0.030" Glass Teflon®, 2 oz Copper,
Z7	0.501" x 0.050" Microstrip	Material	3" x 5" Dimensions,
Z8	0.600" x 1.056" Microstrip		Arlon GX0300-55-22, $\epsilon_r = 2.55$

Figure 1. MRF21125 Test Circuit Schematic

Table 1. MRF21125 Component Designations and Values

Designators	Description
C1	9.1 pF, ATC RF Chip Capacitor, Case "B", #100B9R1CCA500X
C2, C4, C11, C12	22 μ F, 35 V, Tantalum Surface Mount Chip Capacitors, Kemet, #T491X226K035AS4394
C3, C7	20000 pF, ATC RF Chip Capacitors, Case "B", #100B203JCA50X
C5, C14	5.1 pF, ATC RF Chip Capacitors, Case "B", #100B5R1CCA500X
C6	100000 pF, ATC RF Chip Capacitor, Case "B", #100B104JCA50X
C8	10000 pF, ATC RF Chip Capacitor, Case "B", #100B103JCA50X
C9	7.5 pF, ATC RF Chip Capacitor, Case "B", #100B7R5CCA500X
C10	1.2 pF, ATC RF Chip Capacitor, Case "B", #100B1R2CCA500X
C13	0.1 μ F, Chip Capacitor, Kemet, #CDR33BX104AKWS
C15	16 pF, ATC RF Chip Capacitor, Case "B", #100B160KP500X
C16	0.6 – 4.5 pF, Variable Capacitor, Johanson Gigatrim, #27271SL
R1	1.0 k Ω , 1/8 W Chip Resistor
R2	560 k Ω , 1/8 W Chip Resistor
R3	4.7 Ω , 1/8 W Chip Resistor
R4	12 Ω , 1/8 W Chip Resistor
B1	Ferrite Bead (Square), Fair Rite, #2743019447
W1	Solid Copper Buss Wire, 16 AWG

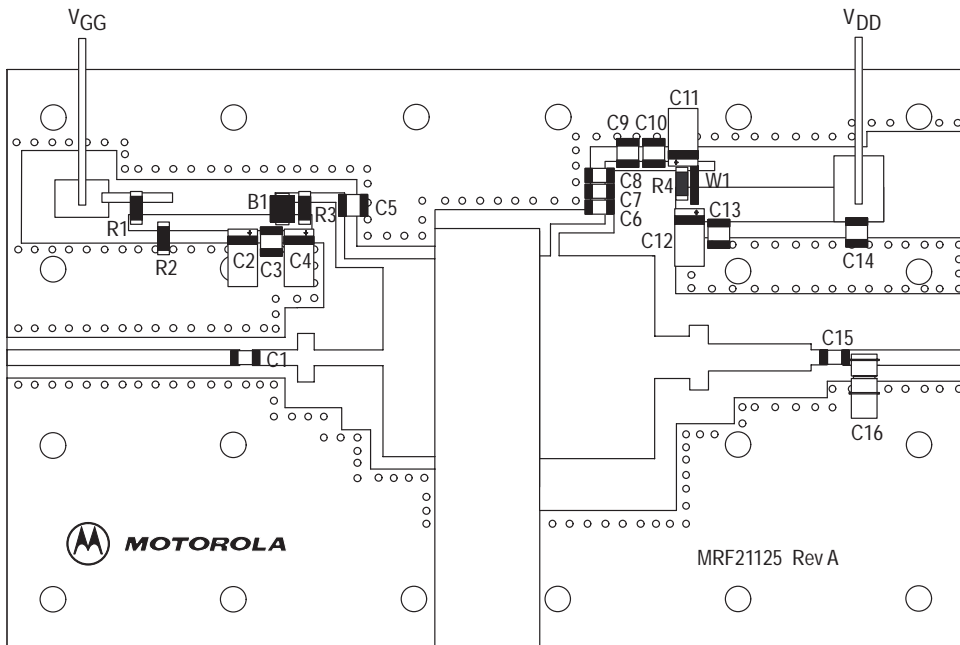


Figure 2. MRF21125 Test Circuit Component Layout

TYPICAL CHARACTERISTICS

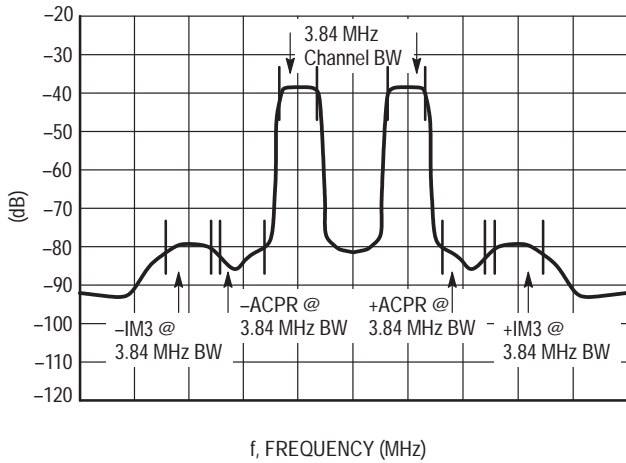


Figure 3.2 Carrier (10 MHz spacing) W-CDMA Spectrum

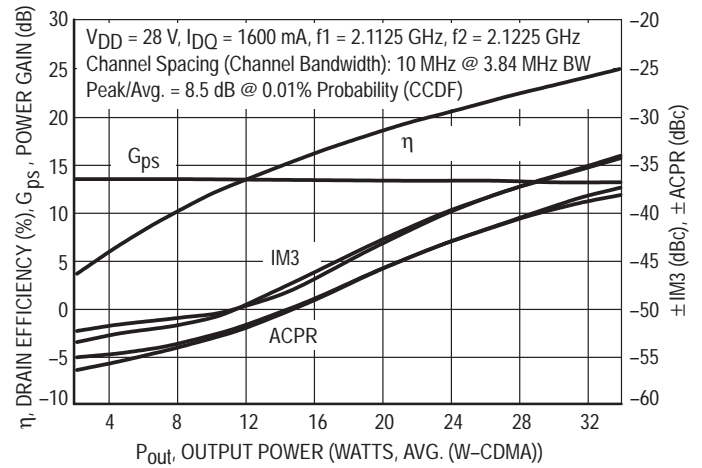


Figure 4.2 Carrier W-CDMA ACPR, IM3, Power Gain and Drain Efficiency versus Output Power

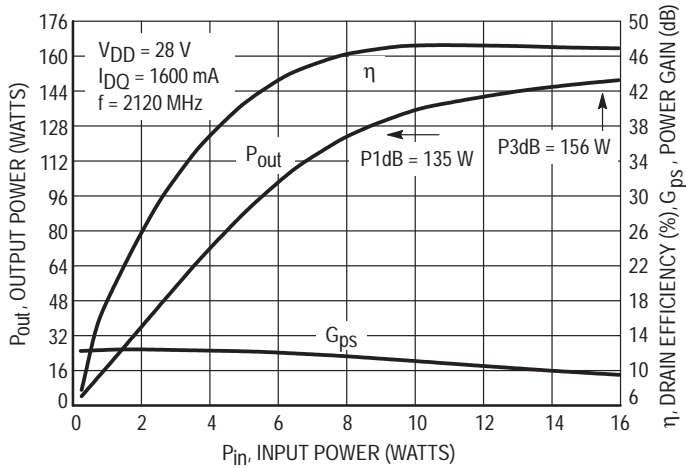


Figure 5. CW Performance

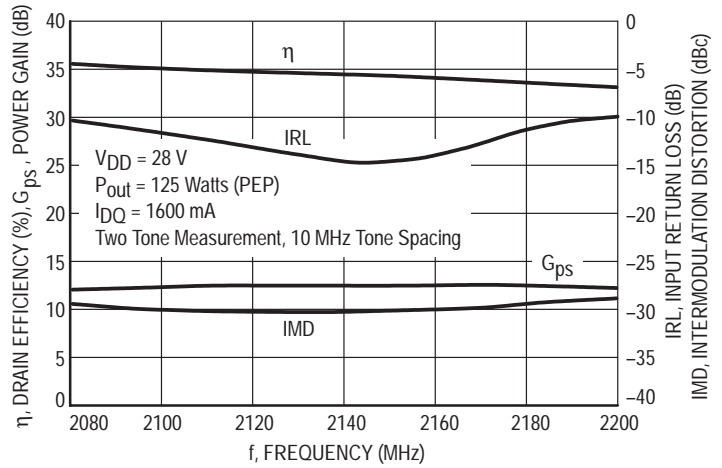


Figure 6. Broadband Linearity Performance

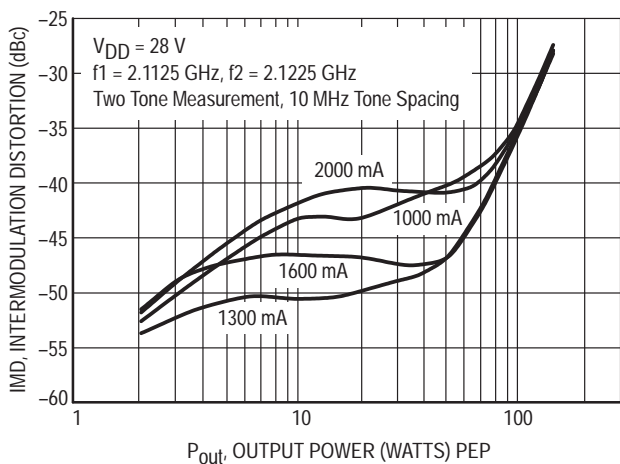


Figure 7. Intermodulation Distortion versus Output Power

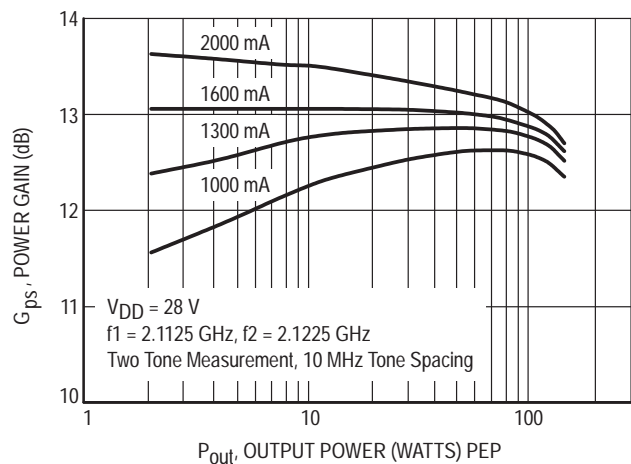
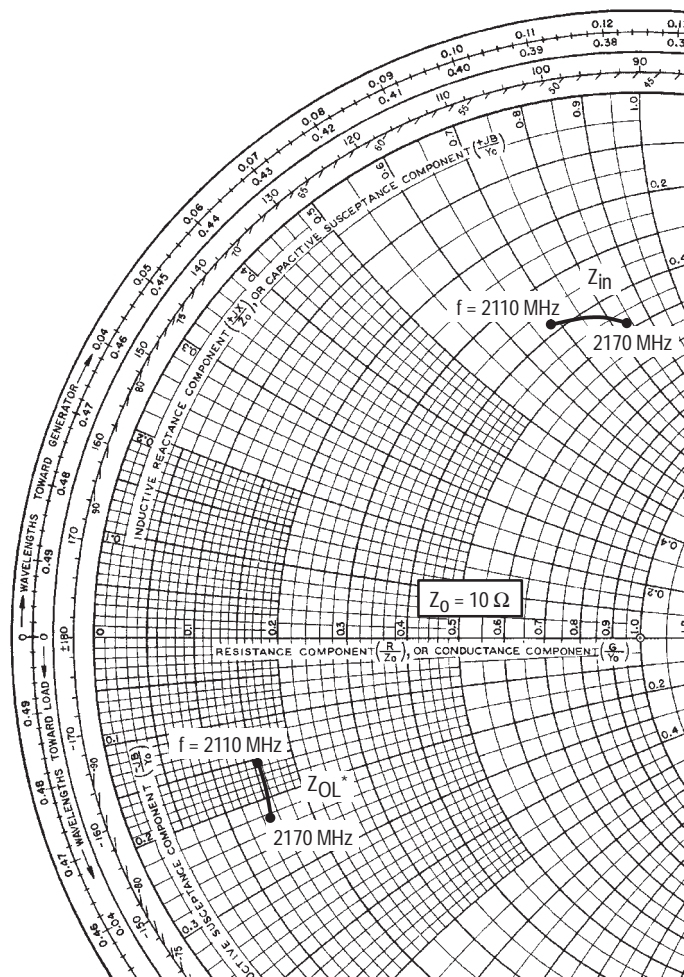


Figure 8. Power Gain versus Output Power



$V_{DD} = 28\text{ V}$, $I_{DQ} = 1600\text{ mA}$, $P_{out} = 20\text{ W}_{avg}$,
 2 – Carrier W-CDMA

f MHz	Z_{in} Ω	Z_{OL}^* Ω
2110	$3.81 + j6.86$	$1.56 - j1.58$
2140	$4.33 + j7.90$	$1.53 - j1.90$
2170	$4.84 + j8.46$	$1.48 - j2.26$

Z_{in} = Complex conjugate of source impedance.

Z_{OL}^* = Complex conjugate of the optimum load impedance at a given output power, voltage, IMD, bias current and frequency.

Note 1: Z_{OL}^* was chosen based on tradeoffs between gain, output power, drain efficiency and intermodulation distortion.

Note 2: Measurements were taken on the MRF21125 test circuit with SMA Launchers.

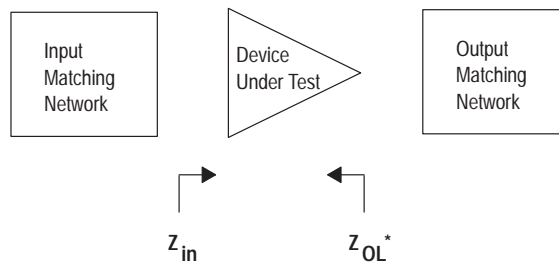


Figure 9. Series Equivalent Input and Output Impedance

The RF Line

NPN Silicon

RF Power Transistor

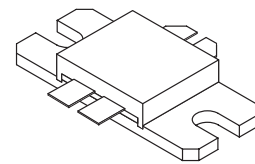
The TPV8100B is designed for output stages in band IV and V TV transmitter amplifiers. It incorporates high value emitter ballast resistors, gold metallizations and offers a high degree of reliability and ruggedness.

Including double input and output matching networks, the TPV8100B features high impedances. It can easily operate in a full 470 MHz to 860 MHz bandwidth in a single and simple circuit.

- To be used class AB for TV band IV and V.
- Specified 28 Volts, 860 MHz Characteristics
Output Power = 125 Watts (peak sync.)
Output Power = 100 Watts (CW)
Minimum Gain = 8.5 dB
- Specified 32 Volts, 860 MHz Characteristics
Output Power = 150 Watts (peak sync.)
- Circuit board photomaster available upon request by contacting RF Tactical Marketing in Phoenix, AZ.

TPV8100B

**150 W, 470–860 MHz
NPN SILICON
RF POWER TRANSISTOR**



CASE 398–03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Collector–Emitter Voltage	V_{CER}	40	Vdc
Collector–Base Voltage	V_{CBO}	65	Vdc
Emitter–Base Voltage	V_{EBO}	4	Vdc
Collector–Current — Continuous	I_C	12	Adc
Total Device Dissipation @ 25°C Case Derate above 25°C	P_D	215 1.25	Watts W/°C
Operating Junction Temperature	T_J	200	°C
Storage Temperature Range	T_{stg}	–65 to +150	°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case (1)	$R_{\theta JC}$	0.8	°C/W

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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OFF CHARACTERISTICS

Collector–Emitter Breakdown Voltage ($I_C = 10\text{ mA}$, $R_{be} = 75\ \Omega$)	$V_{(BR)CER}$	30	—	—	Vdc
Collector–Emitter Breakdown Voltage ($I_C = 10\text{ mAdc}$)	$V_{(BR)EBO}$	4	—	—	Vdc
Collector–Base Breakdown Voltage ($I_E = 20\text{ mAdc}$)	$V_{(BR)CBO}$	65	—	—	Vdc
Collector–Emitter Leakage ($V_{CE} = 28\text{ V}$, $R_{be} = 75\ \Omega$)	I_{CER}	—	—	10	mA

NOTE:

1. Thermal resistance is determined under specified RF operating condition.

(continued)

ELECTRICAL CHARACTERISTICS — continued ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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ON CHARACTERISTICS

DC Current Gain ($I_C = 2 \text{ Adc}$, $V_{CE} = 10 \text{ Vdc}$)	h_{FE}	30	—	120	—
--	----------	----	---	-----	---

DYNAMIC CHARACTERISTICS

Output Capacitance (each side) (2) ($V_{CB} = 28 \text{ V}$, $I_E = 0$, $f = 1 \text{ MHz}$)	C_{ob}	—	44	—	pF
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FUNCTIONAL TESTS IN CW (SOUND)

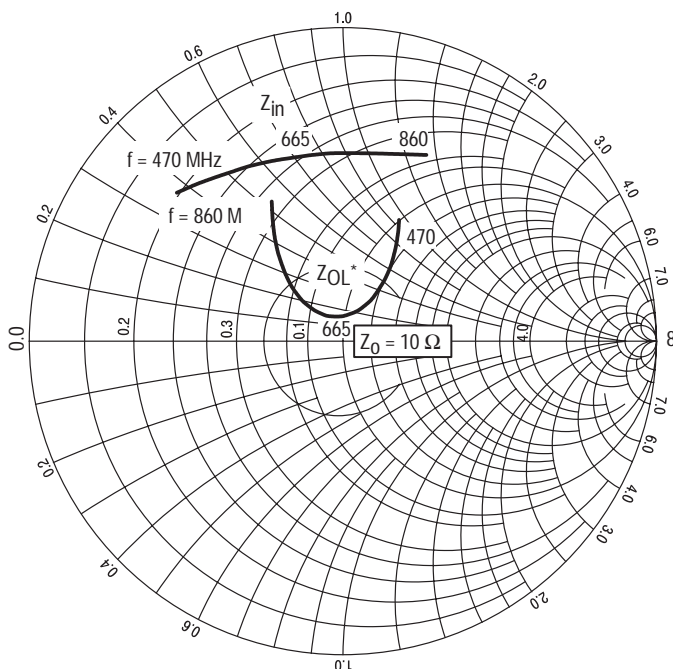
Common-Emitter Amplifier Power Gain ($V_{CC} = 28 \text{ V}$, $P_{out} = 100 \text{ W}$, $I_{CQ} = 2 \times 50 \text{ mA}$, $f = 860 \text{ MHz}$)	G_p	8.5	9.5	—	dB
Collector Efficiency ($V_{CC} = 28 \text{ V}$, $P_{out} = 100 \text{ W}$, $I_Q = 2 \times 50 \text{ mA}$, $f = 860 \text{ MHz}$)	η	55	58	—	%
Output Power @ 1 dB Compression ($P_{ref} = 25 \text{ W}$) ($V_{CC} = 28 \text{ V}$, $I_{CQ} = 2 \times 50 \text{ mA}$, $f = 860 \text{ MHz}$)	P_{out}	100	110	—	W

FUNCTIONAL TESTS IN VIDEO (STANDARD BLACK LEVEL)

Peak Output Power (synch.) ($V_{CC} = 28 \text{ V}$, $I_{CQ} = 2 \times 50 \text{ mA}$, $f = 860 \text{ MHz}$)	P_{out}	125	135	—	W
Peak Output Power (synch.) ($V_{CC} = 32 \text{ V}$, $I_{CQ} = 2 \times 25 \text{ mA}$, $f = 860 \text{ MHz}$)	P_{out}	150	160	—	W
Recommended Quiescent Current	I_{CQ}	—	—	2×0.3	A

NOTE:

2. Value of " C_{ob} " is that of die only. It is not measurable in TPV8100B because of internal matching network.



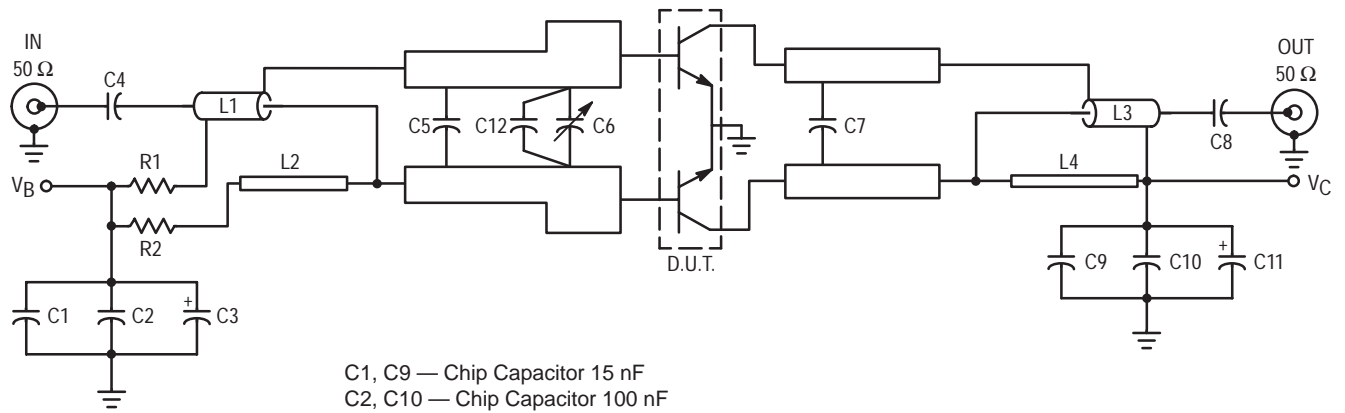
f (MHz)	Z_{in} (Ohms)	Z_{OL}^* (Ohms)
470	$1.95 + j3.67$	$10.0 + j9.50$
665	$3.65 + j6.82$	$9.23 + j1.30$
860	$6.66 + j13.8$	$4.45 + j5.22$

Z_{OL}^* = Conjugate of optimum load impedance into which the device operates at a given output power, voltage, current and frequency.

NOTE: Z_{in} & Z_{OL}^* are given from base-to-base and collector-to-collector respectively.

Input and Output impedances with circuit tuned for maximum linearity @ $V_{CC} = 28 \text{ V}$ / $I_{CQ} = 2 \times 50 \text{ mA}$ / $P_{out} = 100 \text{ W}$

Figure 1. Series Equivalent Input/Output Impedances



- C1, C9 — Chip Capacitor 15 nF
- C2, C10 — Chip Capacitor 100 nF
- C3, C11 — Chip Capacitor 100 μ F/40 V
- C4 — Chip Capacitor 15 pF ATC 100A
- C5 — Chip Capacitor 5.6 pF ATC 100A
- C6 — Trimmer Capacitor 1–4 pF
- C7 — Chip Capacitor 12 pF ATC 100B
- C8 — Chip Capacitor 15 pF ATC 100A
- C12 — Chip Capacitor 12 pF ATC 100A
- L1, L3 — Coaxial Wire 25 Ω /85 Mils/40 mm
- L2, L4 — Printed Board Inductance
- R1, R2 — Chip Resistor 1 Ω 0805 5%

Figure 2. Test Circuit

TYPICAL CHARACTERISTICS
CW — WIDEBAND

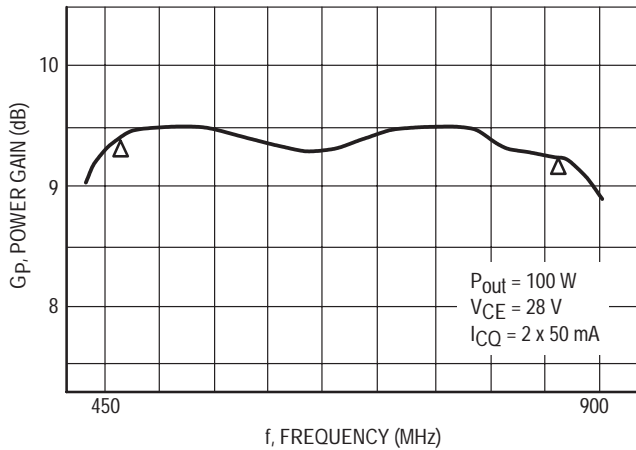


Figure 3. Power Gain versus Frequency

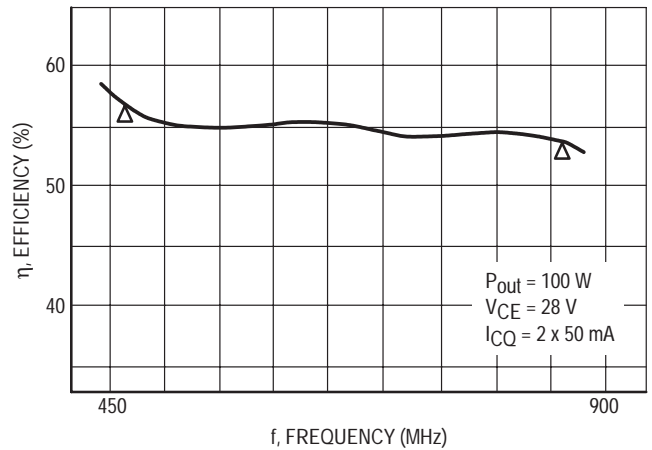


Figure 4. Collector Efficiency versus Frequency

TYPICAL VIDEO CHARACTERISTICS @ $f = 800 \text{ MHz}$
 $V_{CE} = 28 \text{ V}$

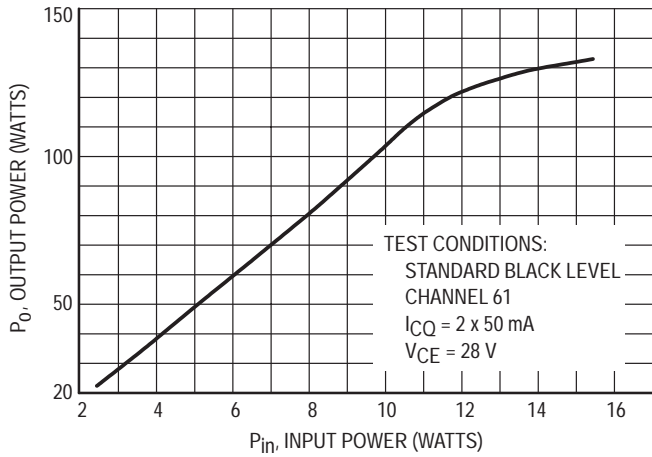
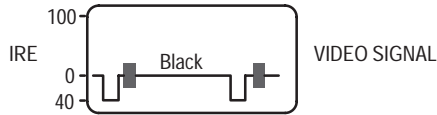


Figure 5. Peak Output Power versus Peak Input Power

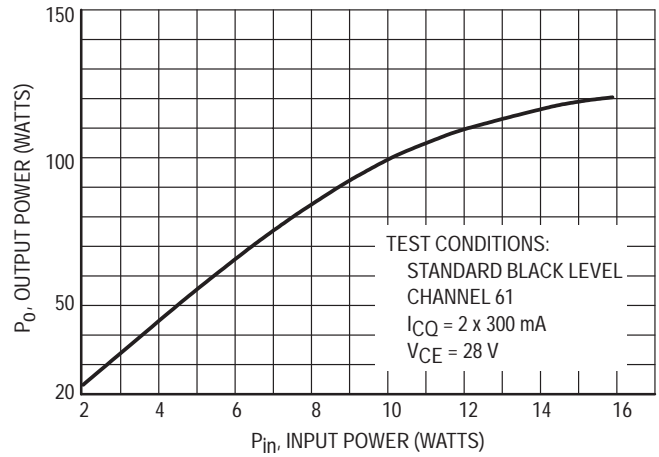


Figure 6. Peak Output Power versus Peak Input Power

TEST CONDITIONS:
 DIFF. Gain, 10 Steps
 Channel 61
 $V_{CE} = 28 \text{ V}$

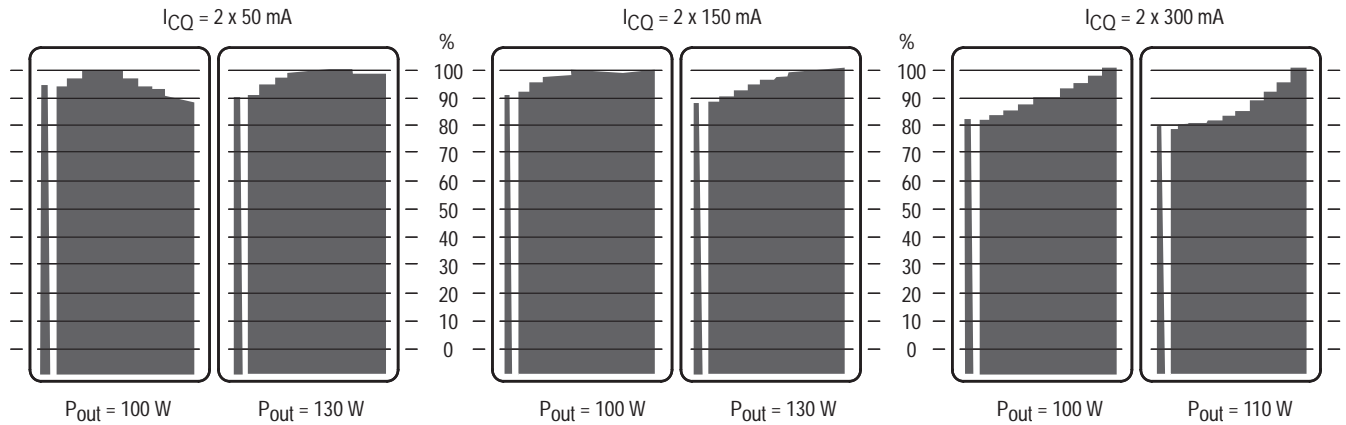
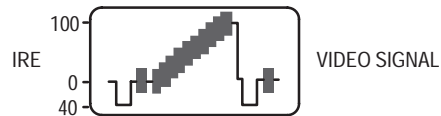


Figure 7. Gain versus Output Power

TYPICAL VIDEO CHARACTERISTICS @ $f = 800 \text{ MHz}$
 $V_{CE} = 32 \text{ V}$

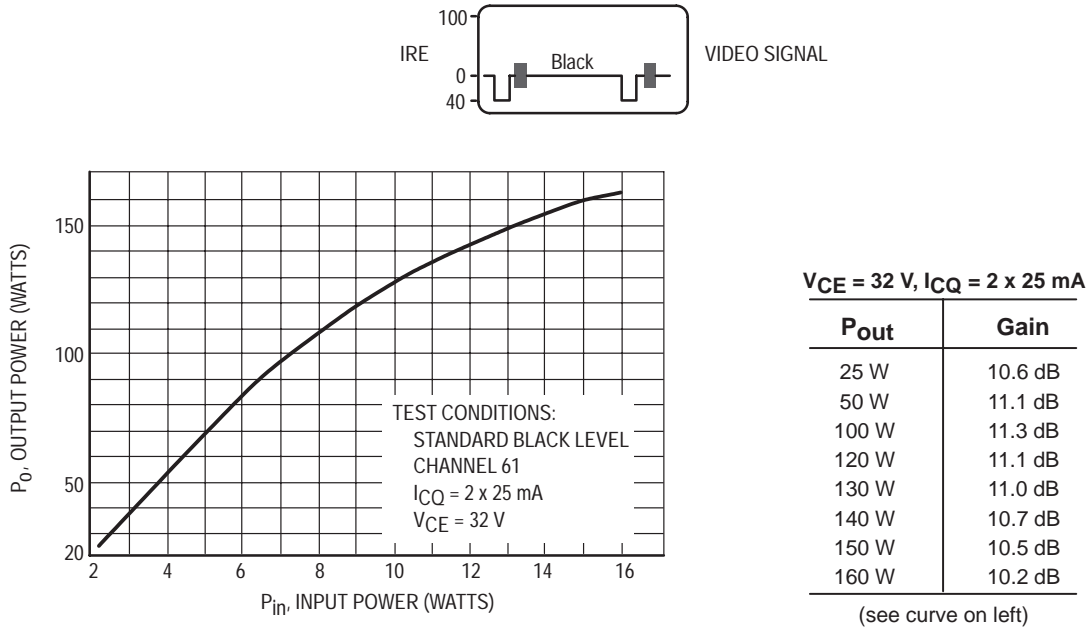


Figure 8. Peak Output Power versus Peak Input Power

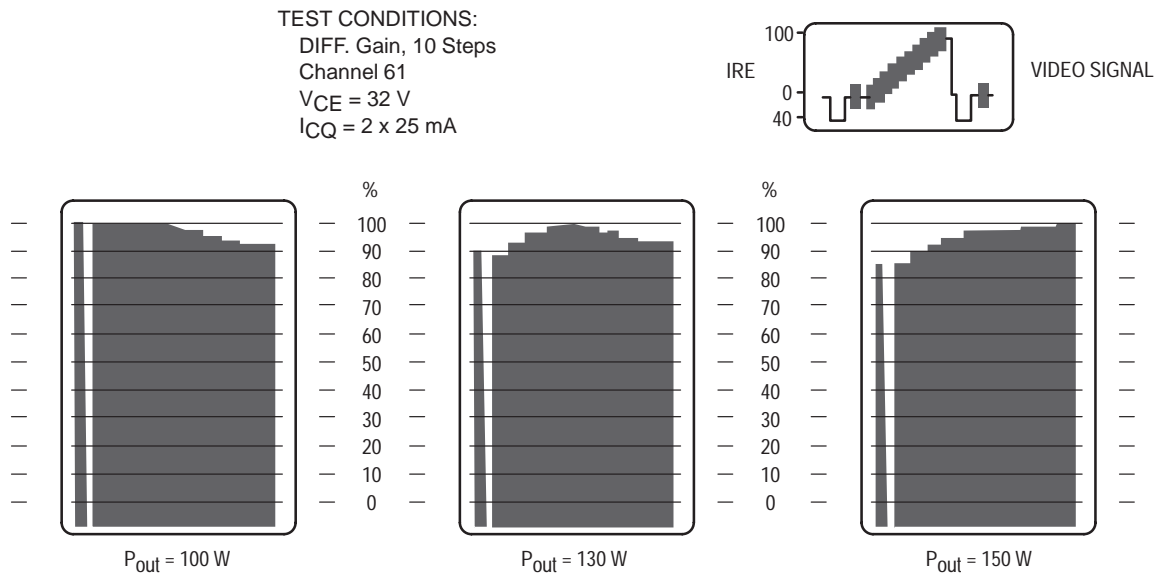


Figure 9. Differential Gain

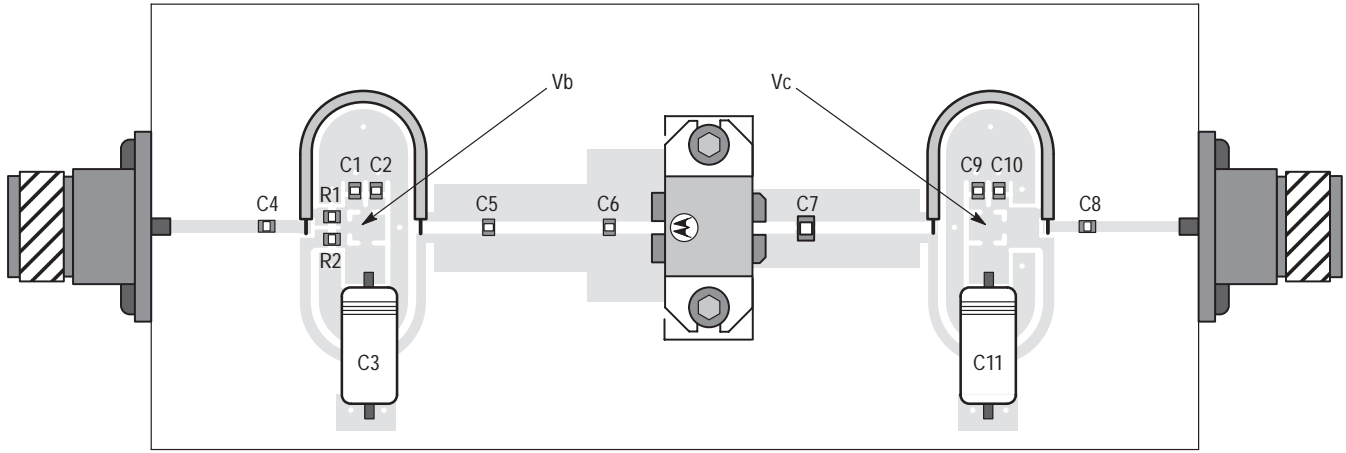


Figure 10. Components View

Chapter Six

RF Amplifier Modules

Section One **6.1–0**

RF Amplifier Modules – Selector Guide

Section Two **6.2–0**

RF Amplifier Modules – Data Sheets

Section One Selector Guide

Motorola RF Amplifier Modules/ICs

Motorola's RF portfolio includes many hybrid designs optimized to perform either in narrowband base station transmitter applications, or in broadband linear amplifiers. Motorola modules feature two or more active transistors (LDMOS, GaAs, or Bipolar die technology) and their associated 50 ohm matching networks. Circuit substrate and metallization have been selected for optimum performance and reliability. For PA designers, hybrid modules offer the benefits of small and less complex system designs, in less time and at a lower overall cost.

Table of Contents

	Page
RF Amplifier Modules/ICs	6.1-1
Base Stations	6.1-2
Wideband Linear Amplifiers	6.1-3
Packages	6.1-4

Motorola RF Amplifier Modules/ICs

Complete amplifiers with 50 ohm input and output impedances are available for all popular base station transmitter systems, including GSM and CDMA, covering frequencies from 800 MHz up to 2.2 GHz.

Base Stations

Designed for applications such as macrocell drivers and microcell output stage, these class AB amplifiers are ideal for base station systems at 900, 1800 and 1900 MHz, with power requirements up to 30 watts.

Table 1. Base Stations

Device	Frequency MHz	P1dB Watts	Gain (Min) dB	Supply Voltage Volts	Class	System Application	Die Technology	Package/Style
MHVIC910HR2(18e,46a)	921–960	10	38	26	AB	GSM900	LDMOS–IC	978/–
MHW1810–1	1805–1880	10	24	26	AB	GSM1800	LDMOS	301AW/1
MHW1810–2	1805–1880	10	32	26	AB	GSM1800	LDMOS	301AW/1
MHW1910–1	1930–1990	10	24	26	AB	GSM1900	LDMOS	301AW/1
MHPA19030(46a)	1930–1990	30	25	26	AB	PCS1900	LDMOS	301AP/1
MHPA21030(46a)	2110–2170	30	25	26	AB	W–CDMA	LDMOS	301AP/1

Table 2. Base Station Drivers

These 50 ohm amplifiers are recommended for modern multi–tone CDMA, TDMA and UMTS base station pre–driver applications. Their high third–order intercept point, tight phase and gain control, and excellent group delay characteristics make these devices ideal for use in high–power feedforward loops.

Ultra–Linear (for CDMA, W–CDMA, TDMA, Analog) – Class A (LDMOS Die) – Lateral MOSFETs

Device	Frequency Band MHz	V _{DD} (Nom.) Volts	I _{DD} (Nom.) mA	Gain (Nom.) dB	Gain Flatness (Typ) ±dB	P1dB (Typ) dBm	3rd Order Intercept (Typ) dBm	NF (Typ) dB	Case/Style
MHL9838	800–925	28	770	31	.1	39	50	3.7	301AP/1
MHL9236	800–960	26	550	30.5	.1	34	47	3.5	301AP/1
MHL9236M	800–960	26	550	30.5	.1	34	47	3.5	301AP/2
MHL9318	860–900	28	500	17.5	.1	35.5	49	3.0	301AS/1
MHL18336(46a)	1800–1900	26	500	30	.2	36	46	4.2	301AP/1
MHL18936(46a)	1800–1900	26	1400	30	.2	41	51	4.2	301AY/1
MHL19338	1900–2000	28	500	30	.1	36	46	4.2	301AP/1
MHL19936★	1900–2000	26	1400	29	.2	41	49.5	4.2	301AY/1
MHL21336	2110–2170	26	500	31	.15	35	45	4.5	301AP/1

(18)Tape and Reel Packaging Option Available by adding suffix: a) R1 = 500 units; b) R2 = 2,500 units; c) T1 = 3,000 units; d) T3 = 10,000 units; e) R2 = 1,500 units; f) T1 = 1,000 units; g) R2 = 4,000 units; h) R1 = 1,000 units; i) R3 = 250 units; j) T1 = 500 units; k) R2 = 450 units.

(46)To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

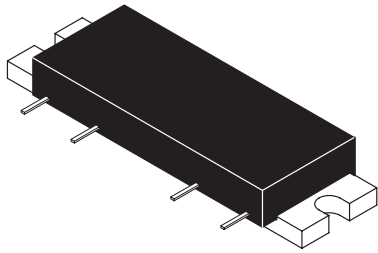
Wideband Linear Amplifiers

Table 1. Standard 50 Ohm Linear Hybrid

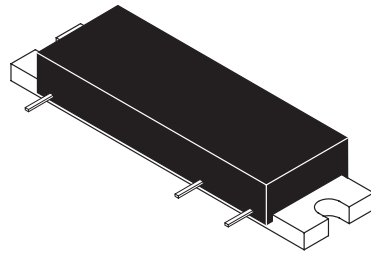
This series of RF linear hybrid amplifier has been optimized for wideband, 50 ohm applications. These amplifiers were designed for multi-purpose RF applications where linearity, dynamic range and wide bandwidth are of primary concern. The MHL series utilizes a new case style that provides microstrip input and output connections.

Device	Frequency Band MHz	V _{CC} (Nom.) Volts	I _{CC} (Nom.) mA	Gain/Freq. (Typ) dB/MHz	Gain Flatness (Typ) ±dB	P _{1dB} (Typ) dBm	3rd Order Intercept Point/Freq. (Typ) dBm/MHz	NF/Freq. (Typ) dB/MHz	Case/ Style
MHL8018	40– 1000	28	210	18.5/900	1	26	38/1000	7.5/1000	448/1
MHL8115	40–1000	15	700	17.5/900	1	30	41.5/1000	8.5/1000	448/2
MHL8118	40–1000	28	400	17.5/900	1	30	41.5/1000	8.5/1000	448/1

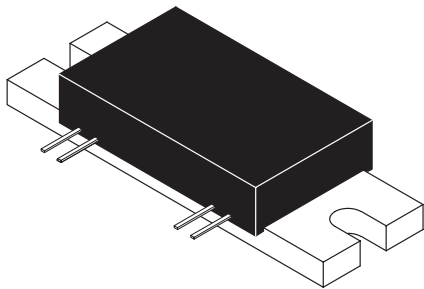
RF Amplifier Modules Packages



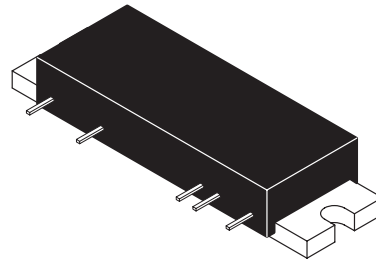
CASE 301AP
STYLE 1, 2



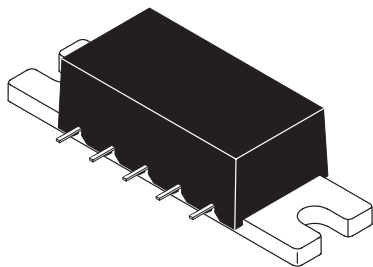
CASE 301AS
STYLE 1



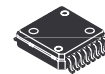
CASE 301AW
STYLE 1



CASE 301AY
STYLE 1



CASE 448
STYLE 1, 2



CASE 978

SCALE 1:1

Section Two

Motorola RF Amplifier Modules – Data Sheets

Device Number	Page Number
MHL8018	6.2-3
MHL8115	6.2-5
MHL8118	6.2-7
MHL9236	6.2-9
MHL9236M	6.2-9
MHL9318	6.2-12
MHL9838	6.2-15
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MHL19936	6.2-19
MHL21336	6.2-20
MHW1810-1	6.2-21
MHW1810-2	6.2-21
MHW1910-1	6.2-27

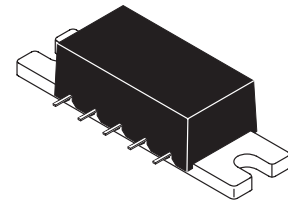
The RF Line UHF Linear Amplifier

Designed for linear amplifier applications in 50 ohm systems requiring wide bandwidth, low noise, and low distortion. Internal DC blocking on RF ports reduces external component count and related circuit area. This hybrid utilizes push-pull circuit design.

- Supply Voltage: 28 Vdc
- Third Order Intercept: 38 dBm Typ
- Power Gain: 18.5 dB Typ (@ f = 900 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- 50 Ohm Input/Output Impedances

MHL8018

**400 mW, 18.5 dB
40–1000 MHz
LINEAR AMPLIFIERS**



CASE 448-02, STYLE 1

ABSOLUTE MAXIMUM RATINGS (T_C = 25°C unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V _{CC}	32	Vdc
RF Input Power	P _{in}	+14	dBm
Storage Temperature Range	T _{stg}	-40 to +100	°C
Operating Case Temperature Range	T _C	-20 to +100	°C

ELECTRICAL CHARACTERISTICS (T_C = +25°C; V_{CC} = 28 Vdc; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I _{DC}	—	210	240	mA
Power Gain (f = 900 MHz)	P _G	17.5	18.5	19.5	dB
Gain Flatness (f = 40–1000 MHz)	FL	—	1.0	2.0	dB
Power Output @ 1 dB Comp. (f = 900 MHz)	P _{out} 1 dB	25	26	—	dBm
Third Order Intercept (f ₁ = 879 MHz, f ₂ = 884 MHz)	ITO	37	38	—	dBm
Input/Output VSWR (f = 40–900 MHz) (f = 900–1000 MHz)	VSWR	—	—	2.0:1 2.6:1	
Noise Figure, Broadband (f = 500 MHz) (f = 1000 MHz)	NF	—	6.5 7.5	8.0 9.0	dB
Second Harmonic Distortion (P _O = 100 mW, f _{2H} = 1000 MHz)	d _{so}	—	-50	-40	dB
Second Order Intermodulation Distortion (P _O = 2.75 dBm, f ₁ = 373 MHz, f ₂ = 450 MHz)	IM2	—	—	-60	dB
Intermodulation Distortion, 3 Tone (f = 860 MHz, P _{sync} = 200 mW)	IM3	—	-60	—	dB

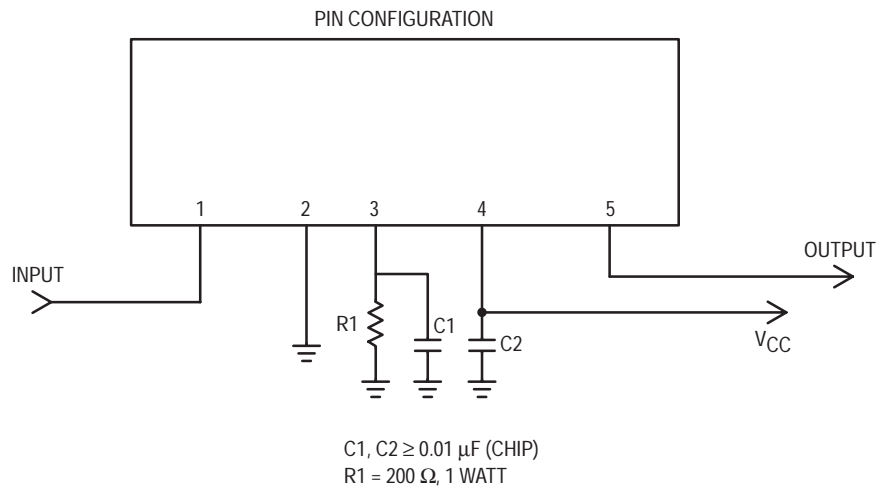


Figure 1. MHL8018 External Connections

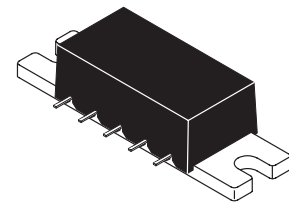
The RF Line UHF Linear Amplifier

Designed for linear amplifier applications in 50 Ohm systems requiring wide bandwidth, low noise, and low distortion. Internal DC blocking on RF ports reduces external component count and related circuit area. This hybrid utilizes push-pull circuit design.

- Supply Voltage: 15 Vdc
- Third Order Intercept: 41.5 dBm Typ
- Power Gain: 17.5 dB Typ (@ 900 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- 50 Ohm Input/Output Impedances

MHL8115

**1 W, 17.5 dB
50–1000 MHz
LINEAR AMPLIFIERS**



CASE 448-02, STYLE 2

ABSOLUTE MAXIMUM RATINGS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	18	Vdc
RF Input Power	P_{in}	+20	dBm
Storage Temperature Range	T_{stg}	-40 to +100	$^\circ\text{C}$
Operating Case Temperature Range	T_C	-20 to +100	$^\circ\text{C}$

ELECTRICAL CHARACTERISTICS ($T_C = +25^\circ\text{C}$; $V_{CC} = 15$ Vdc; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I_{DC}	—	700	760	mA
Power Gain (f = 900 MHz)	P_G	16.5	17.5	—	dB
Gain Flatness (f = 50–1000 MHz)	FL	—	1.0	2.0	dB
Power Output @ 1 dB Comp. (f = 900 MHz)	P_{out} 1 dB	29	30	—	dBm
Third Order Intercept (f ₁ = 879 MHz, f ₂ = 884 MHz)	ITO	40.5	41.5	—	dBm
Input/Output VSWR (f = 50–900 MHz) (f = 900–1000 MHz)	VSWR	—	—	2.0:1 2.6:1	
Noise Figure, Broadband (f = 500 MHz) (f = 1000 MHz)	NF	—	7.5 8.5	8.5 9.5	dB
Second Harmonic Distortion ($P_O = 100$ mW, f _{2H} = 1000 MHz)	d _{so}	—	-55	-45	dB
Second Order Intermodulation Distortion ($P_O = 2.75$ dBm, f ₁ = 373 MHz, f ₂ = 450 MHz)	IM ₂	—	-65	-60	dB
Intermodulation Distortion, 3 Tone (f = 860 MHz, $P_{sync} = 200$ mW)	IM ₃	—	-60	—	dB

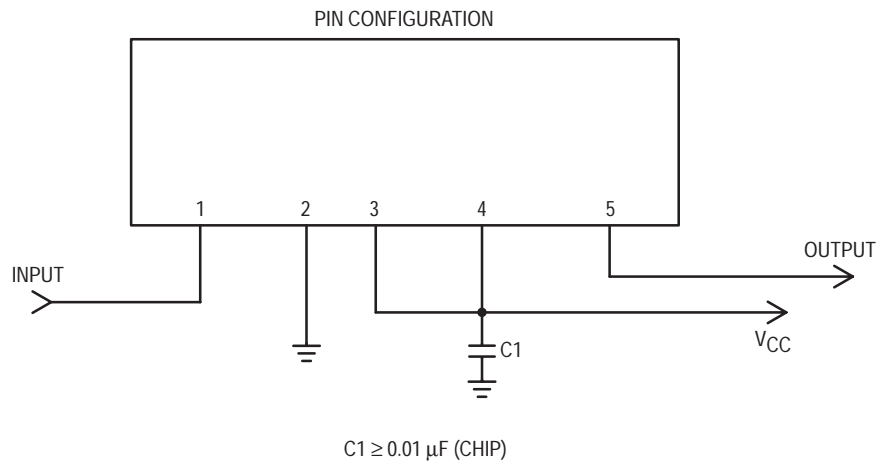


Figure 1. MHL8115 External Connections

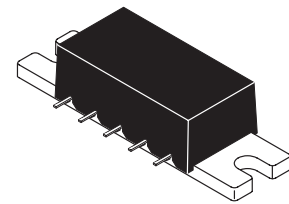
The RF Line UHF Linear Amplifier

Designed for linear amplifier applications in 50 Ohm systems requiring wide bandwidth, low noise, and low distortion. Internal DC blocking on RF ports reduces external component count and related circuit area. This hybrid utilizes push-pull circuit design.

- Supply Voltage: 28 Vdc
- Third Order Intercept: 41.5 dBm Typ
- Power Gain: 17.5 dB Typ (@ 900 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- 50 Ohm Input/Output Impedances

MHL8118

**1 W, 17.5 dB
50–1000 MHz
LINEAR AMPLIFIERS**



CASE 448-02, STYLE 1

ABSOLUTE MAXIMUM RATINGS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	32	Vdc
RF Input Power	P_{in}	+20	dBm
Storage Temperature Range	T_{stg}	-40 to +100	$^\circ\text{C}$
Operating Case Temperature Range	T_C	-20 to +100	$^\circ\text{C}$

ELECTRICAL CHARACTERISTICS ($T_C = +25^\circ\text{C}$; $V_{CC} = 28$ Vdc; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I_{DC}	—	400	440	mA
Power Gain (f = 900 MHz)	P_G	16.5	17.5	—	dB
Gain Flatness (f = 50–1000 MHz)	FL	—	1.0	2.0	dB
Power Output @ 1 dB Comp. (f = 900 MHz)	P_{out} 1 dB	29	30	—	dBm
Third Order Intercept (f ₁ = 879 MHz, f ₂ = 884 MHz)	ITO	40.5	41.5	—	dBm
Input/Output VSWR (f = 50–900 MHz) (f = 900–1000 MHz)	VSWR	—	—	2.0:1 2.6:1	
Noise Figure, Broadband (f = 500 MHz) (f = 1000 MHz)	NF	—	7.5 8.5	8.5 9.5	dB
Second Harmonic Distortion ($P_O = 100$ mW, f _{2H} = 1000 MHz)	dso	—	-55	-45	dB
Second Order Intermodulation Distortion ($P_O = 2.75$ dBm, f ₁ = 373 MHz, f ₂ = 450 MHz)	IM2	—	-65	-60	dB
Intermodulation Distortion, 3 Tone (f = 860 MHz, $P_{sync} = 200$ mW)	IM3	—	-60	—	dB

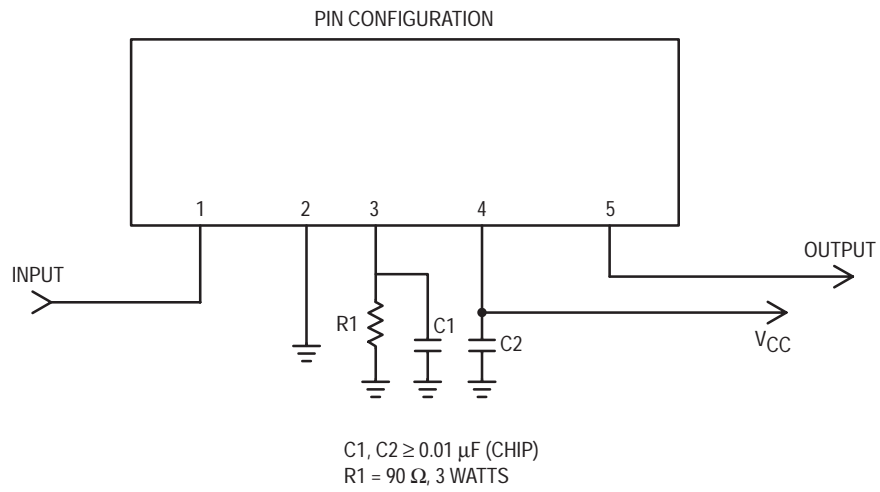


Figure 1. MHL8118 External Connections

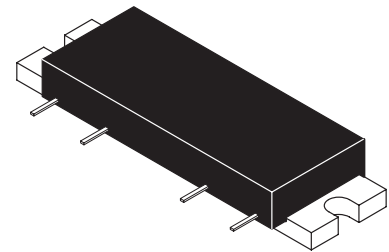
The RF Line Cellular Band Linear Amplifiers

Designed for ultra-linear amplifier applications in 50 ohm systems operating in the cellular frequency band. A silicon FET Class A design provides outstanding linearity and gain. In addition, the excellent group delay and phase linearity characteristics are ideal for the most demanding analog or digital modulation systems, such as TDMA, CDMA or QPSK.

- Third Order Intercept: 47 dBm Typ
- Power Gain: 30.5 dB Typ (@ f = 880 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- Ideal for Feedforward Base Station Applications
- For Use in TDMA, CDMA, QPSK or Analog Systems

MHL9236
MHL9236M

2.5 W, 30.5 dB
800–960 MHz
LINEAR AMPLIFIERS



CASE 301AP-01 STYLE 1, 2

ABSOLUTE MAXIMUM RATINGS (T_C = 25°C unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V _{DD}	30	Vdc
RF Input Power	P _{in}	+10	dBm
Storage Temperature Range	T _{stg}	-40 to +100	°C
Operating Case Temperature Range	T _C	-20 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{DD} = 26 Vdc, T_C = 25°C; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I _{DD}	—	550	620	mA
Power Gain (f = 880 MHz)	P _G	29.5	30.5	31.5	dB
Gain Flatness (f = 800–960 MHz)	G _F	—	0.1	0.3	dB
Power Output @ 1 dB Comp. (f = 880 MHz)	P _{out} 1 dB	33.0	34.0	—	dBm
Input VSWR (f = 800–960 MHz)	VSWR _{in}	—	1.2:1	1.5:1	
Output VSWR (f = 800–960 MHz)	VSWR _{out}	—	1.2:1	1.5:1	
Third Order Intercept (f ₁ = 879 MHz, f ₂ = 884 MHz)	ITO	46.0	47.0	—	dBm
Noise Figure (f = 800–960 MHz)	NF	—	3.5	4.5	dB

TYPICAL CHARACTERISTICS

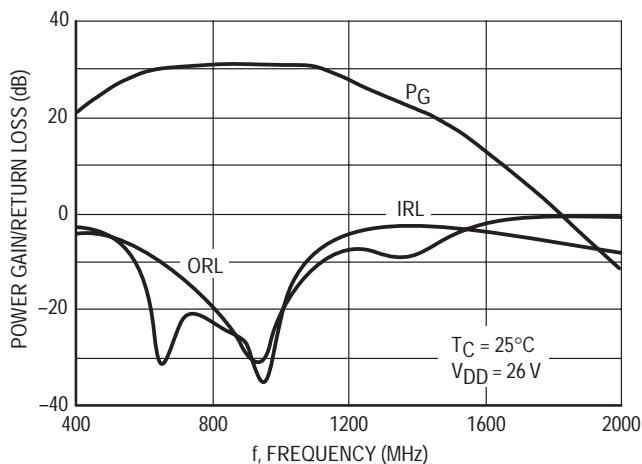


Figure 1. Power Gain, Input Return Loss, Output Return Loss versus Frequency

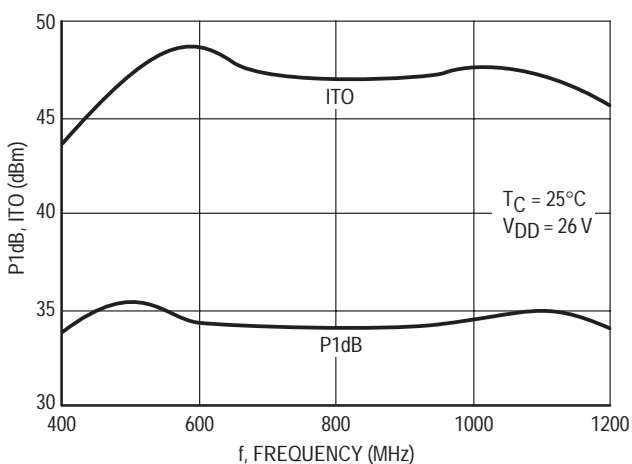


Figure 2. P1dB, ITO versus Frequency

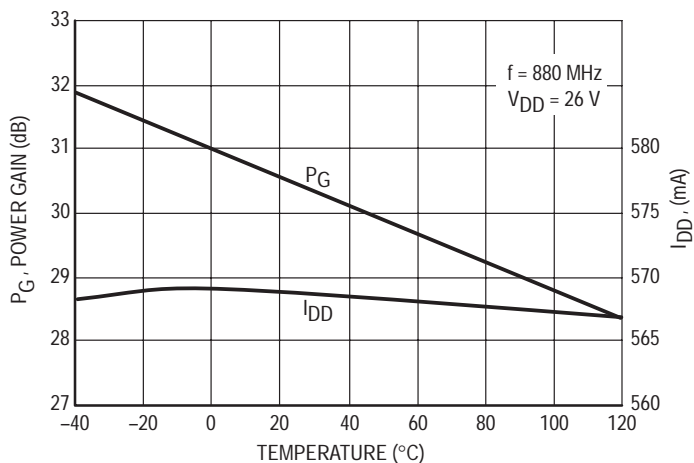


Figure 3. Power Gain, I_{DD} versus Temperature

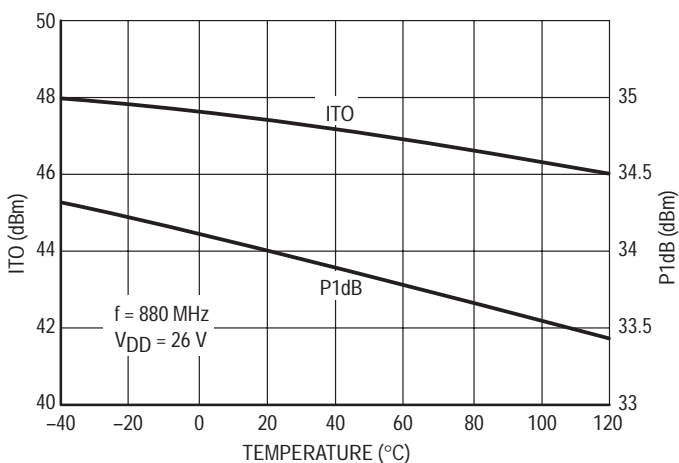


Figure 4. ITO, P1dB versus Temperature

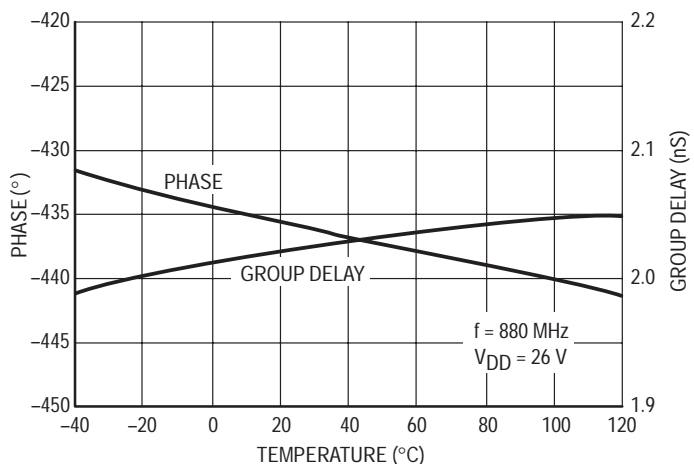


Figure 5. Phase(1), Group Delay(1) versus Temperature
(1)In Production Test Fixture

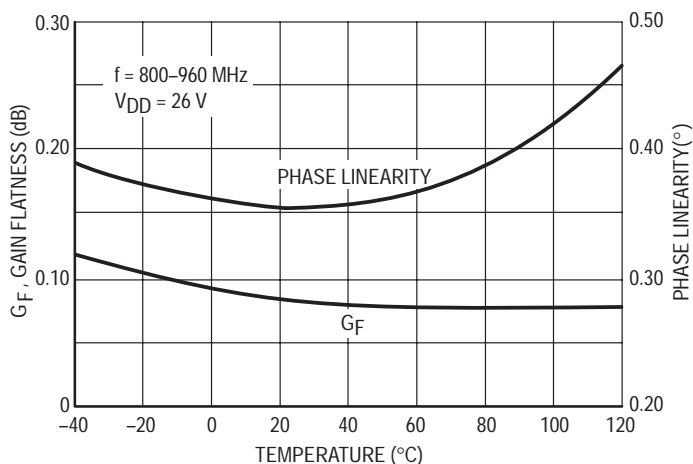


Figure 6. Gain Flatness, Phase Linearity versus Temperature

TYPICAL CHARACTERISTICS

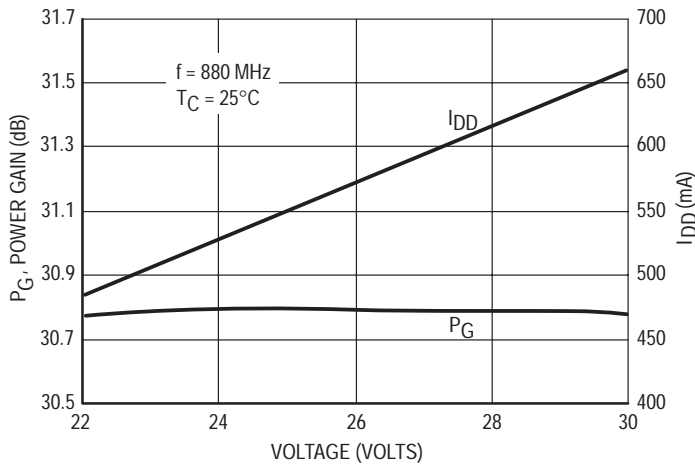


Figure 7. Power Gain, I_{DD} versus Voltage

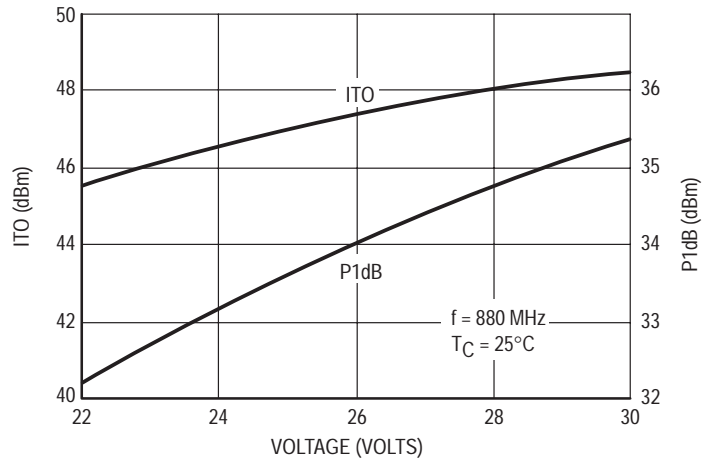


Figure 8. ITO, P1dB versus Voltage

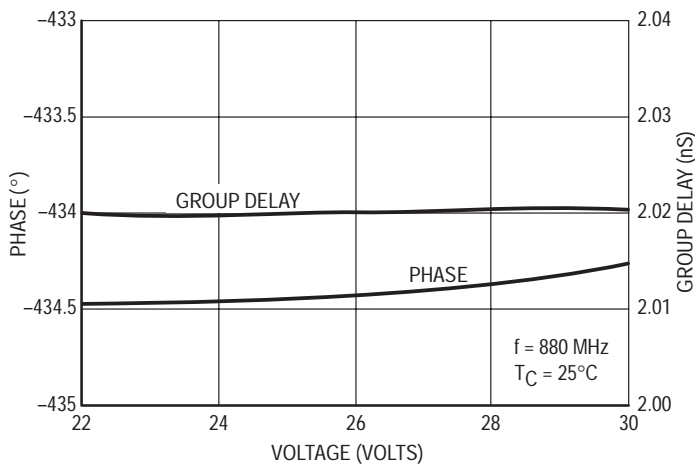


Figure 9. Phase(1), Group Delay(1) versus Voltage
(1) In Production Test Fixture

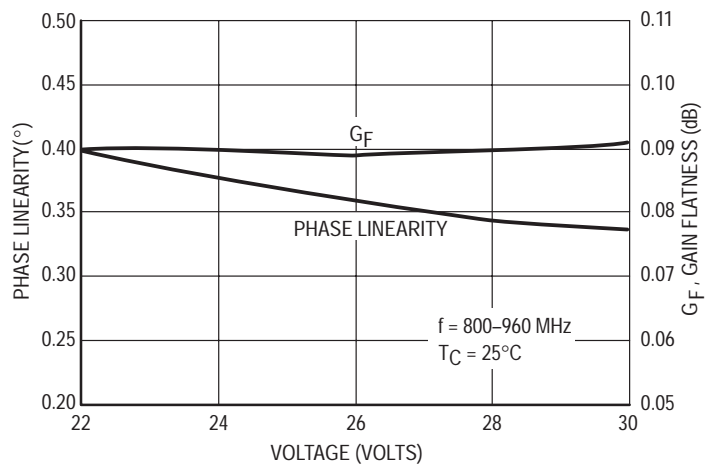


Figure 10. Phase Linearity, Gain Flatness versus Voltage

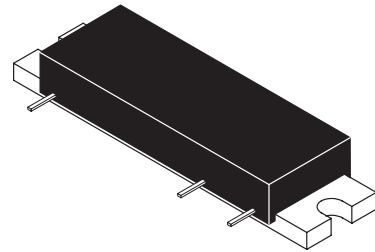
The RF Line Cellular Band Linear Amplifier

Designed for ultra-linear amplifier applications in 50 ohm systems operating in the cellular frequency band. A silicon FET Class A design provides outstanding linearity and gain. In addition, the excellent group delay and phase linearity characteristics are ideal for the most demanding analog or digital modulation systems, such as TDMA and CDMA.

- Third Order Intercept: 49 dBm Typ
- Power Gain: 17.5 dB Typ (@ f = 880 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- Ideal for Feedforward Base Station Applications
- For Use in TDMA and CDMA Multi-Carrier Applications

MHL9318

**3.0 W, 17.5 dB
860–900 MHz
LINEAR AMPLIFIER**



CASE 301AS-01, STYLE 1

ABSOLUTE MAXIMUM RATINGS (T_C = 25°C unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V _{DD}	30	Vdc
RF Input Power	P _{in}	+20	dBm
Storage Temperature Range	T _{stg}	-40 to +100	°C
Operating Case Temperature Range	T _C	-20 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{DD} = 28 Vdc, T_C = 25°C; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I _{DD}	—	500	560	mA
Power Gain (f = 880 MHz)	P _G	17	17.5	18.5	dB
Gain Flatness (f = 860–900 MHz)	G _F	—	0.1	0.2	dB
Power Output @ 1 dB Comp. (f = 880 MHz)	P _{out} 1 dB	—	35.5	—	dBm
Input VSWR (f = 860–900 MHz)	VSWR _{in}	—	1.2:1	1.5:1	
Output VSWR (f = 860–900 MHz)	VSWR _{out}	—	1.2:1	1.5:1	
Third Order Intercept (f ₁ = 879 MHz, f ₂ = 884 MHz)	ITO	47	49	—	dBm
Noise Figure (f = 960 MHz)	NF	—	3	4.5	dB

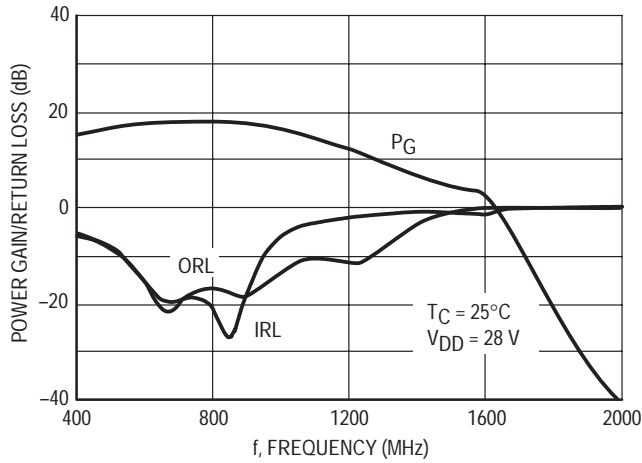


Figure 1. Power Gain, Input Return Loss, Output Return Loss versus Frequency

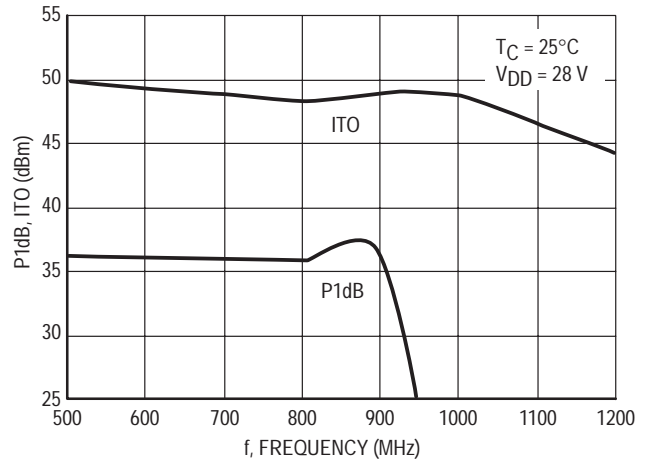


Figure 2. P1dB, ITO versus Frequency

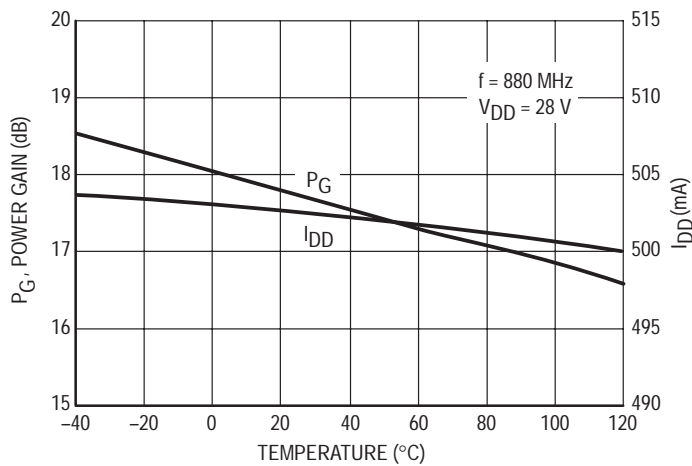


Figure 3. Power Gain, IDD versus Temperature

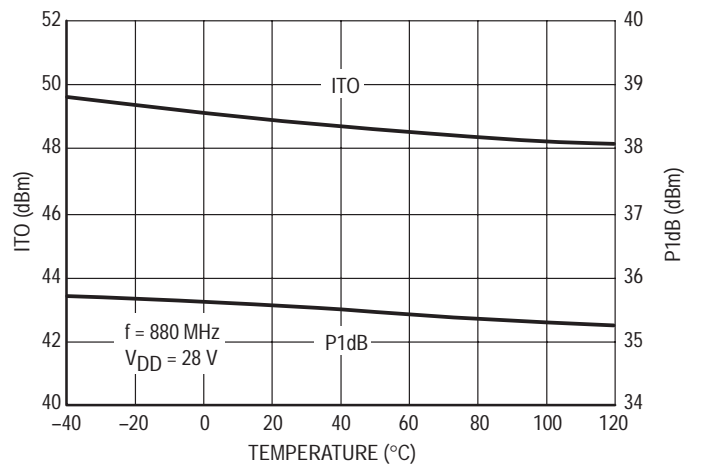


Figure 4. ITO, P1dB versus Temperature

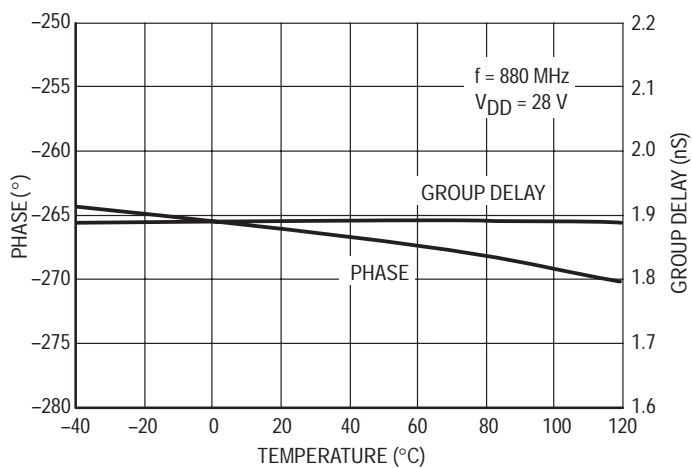


Figure 5. Phase(1), Group Delay(1) versus Temperature
(1)In Production Test Fixture

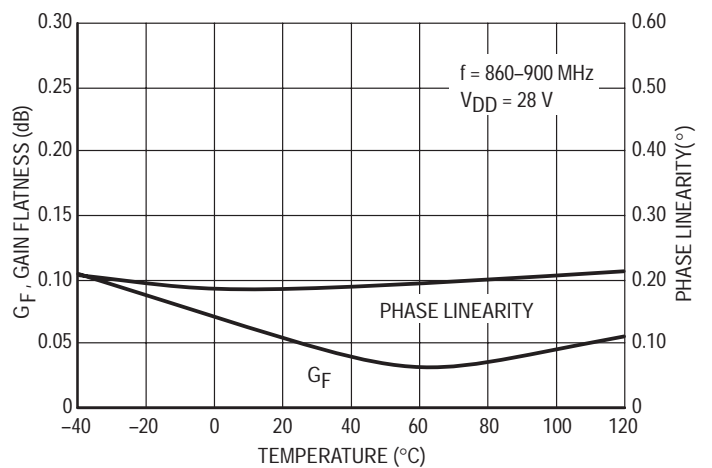


Figure 6. Gain Flatness, Phase Linearity versus Temperature

TYPICAL CHARACTERISTICS

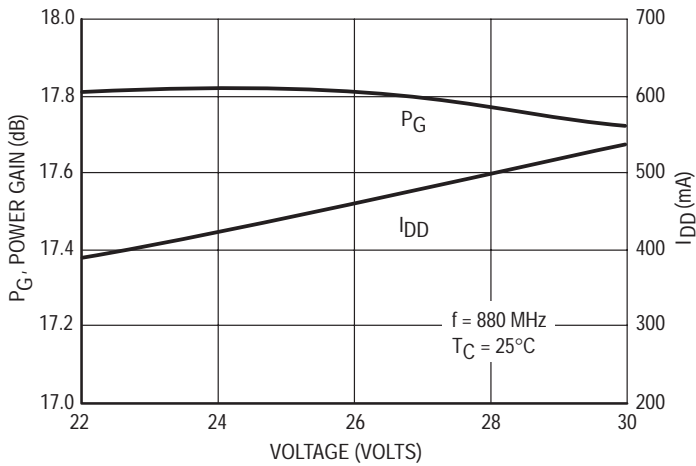


Figure 7. Power Gain, I_{DD} versus Voltage

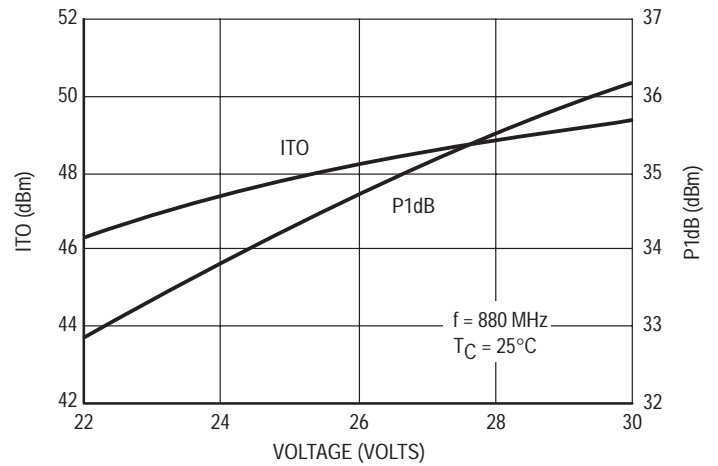


Figure 8. I_{TO} , P_{1dB} versus Voltage

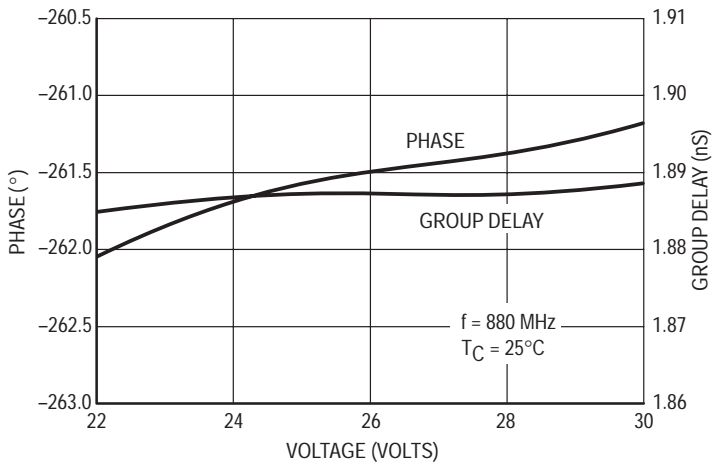


Figure 9. Phase⁽¹⁾, Group Delay⁽¹⁾ versus Voltage
(¹)In Production Test Fixture

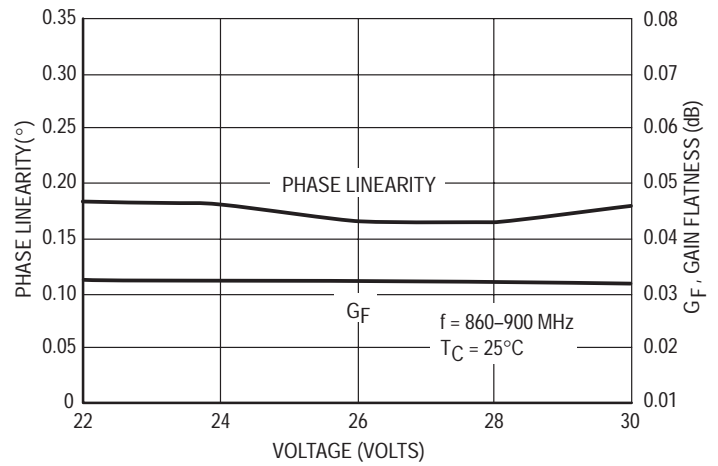


Figure 10. Phase Linearity, Gain Flatness versus Voltage

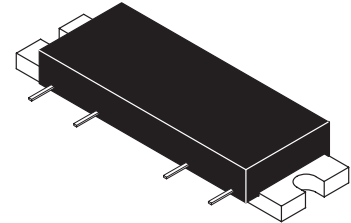
The RF Line Cellular Band Linear Amplifier

Designed for ultra-linear amplifier applications in 50 ohm systems operating in the cellular frequency band. A silicon FET Class A design provides outstanding linearity and gain. In addition, the excellent group delay and phase linearity characteristics are ideal for the most demanding analog or digital modulation systems, such as TDMA and CDMA.

- Third Order Intercept: 50 dBm Typ
- Power Gain: 31 dB Typ (@ f = 880 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- Ideal for Feedforward Base Station Applications
- For Use in TDMA and CDMA Multi-Carrier Applications

MHL9838

8.0 W, 31 dB
800–925 MHz
LINEAR AMPLIFIER



CASE 301AP-01, STYLE 1

ABSOLUTE MAXIMUM RATINGS (T_C = 25°C unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V _{DD}	30	Vdc
RF Input Power	P _{in}	+6	dBm
Storage Temperature Range	T _{stg}	-40 to +100	°C
Operating Case Temperature Range	T _C	-20 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{DD} = 28 Vdc, T_C = 25°C; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I _{DD}	—	770	800	mA
Power Gain (f = 880 MHz)	P _G	30	31	32	dB
Gain Flatness (f = 800–925 MHz)	G _F	—	0.1	0.3	dB
Power Output @ 1 dB Comp. (f = 880 MHz)	P _{out} 1 dB	—	39	—	dBm
Input VSWR (f = 800–925 MHz)	VSWR _{in}	—	1.2:1	1.5:1	
Output VSWR (f = 800–925 MHz)	VSWR _{out}	—	1.2:1	1.5:1	
Third Order Intercept (f ₁ = 879 MHz, f ₂ = 884 MHz)	ITO	49	50	—	dBm
Noise Figure (f = 925 MHz)	NF	—	3.7	4.5	dB

TYPICAL CHARACTERISTICS

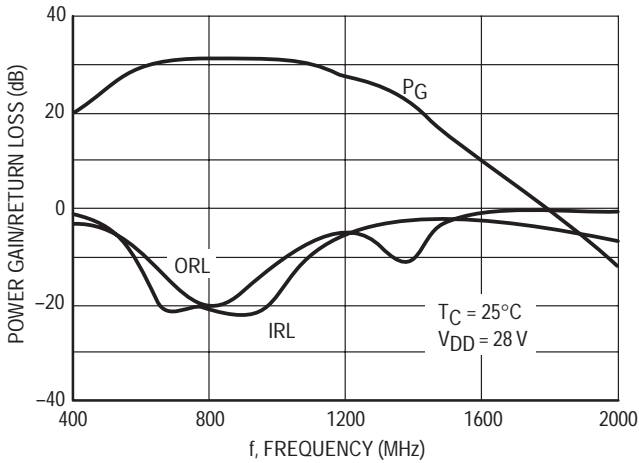


Figure 1. Power Gain, Input Return Loss, Output Return Loss versus Frequency

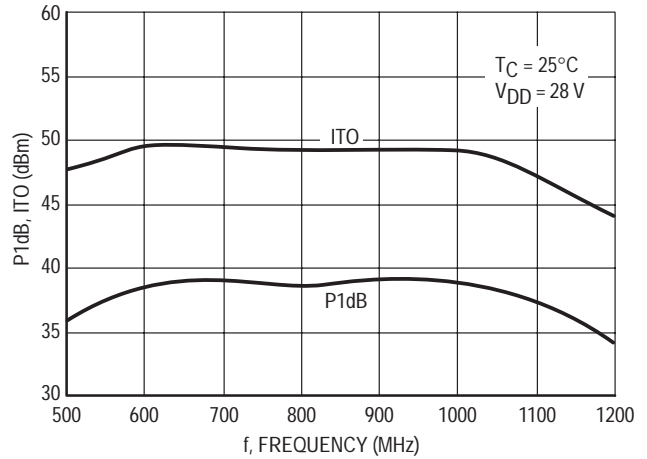


Figure 2. P1dB, ITO versus Frequency

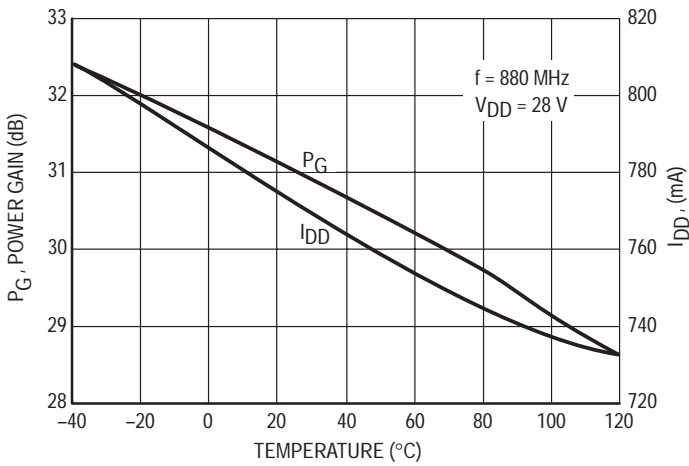


Figure 3. Power Gain, I_{DD} versus Temperature

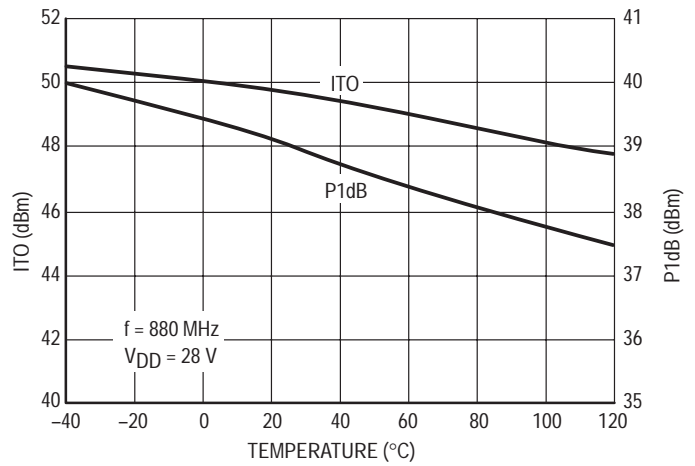


Figure 4. ITO, P1dB versus Temperature

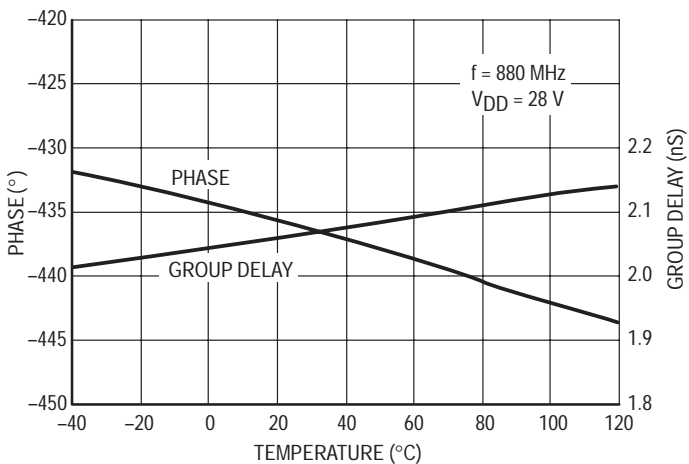


Figure 5. Phase(1), Group Delay(1) versus Temperature
(1)In Production Test Fixture

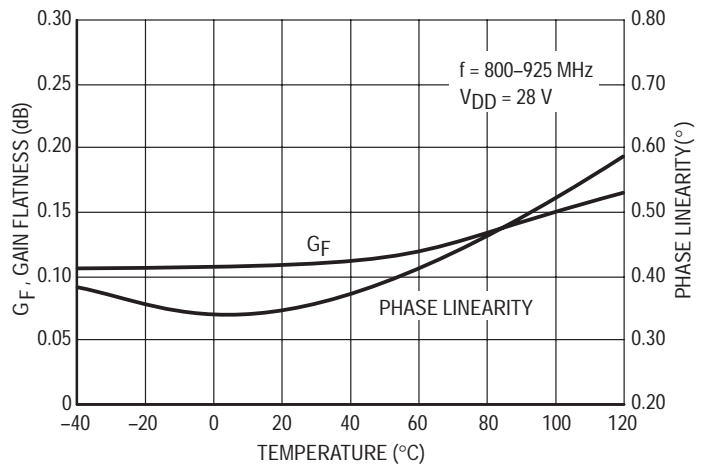


Figure 6. Gain Flatness, Phase Linearity versus Temperature

TYPICAL CHARACTERISTICS

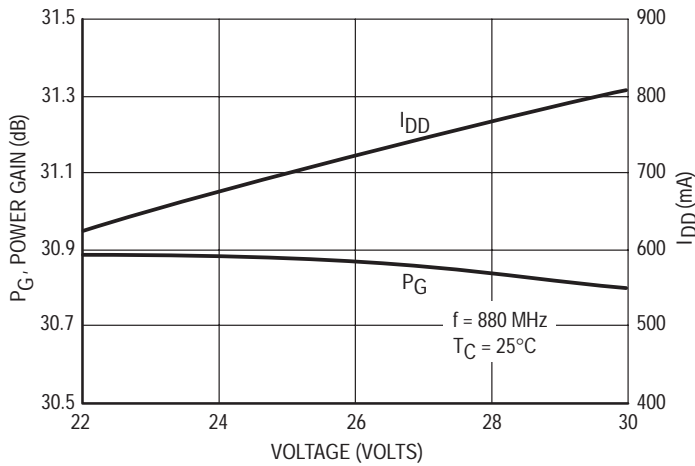


Figure 7. Power Gain, I_{DD} versus Voltage

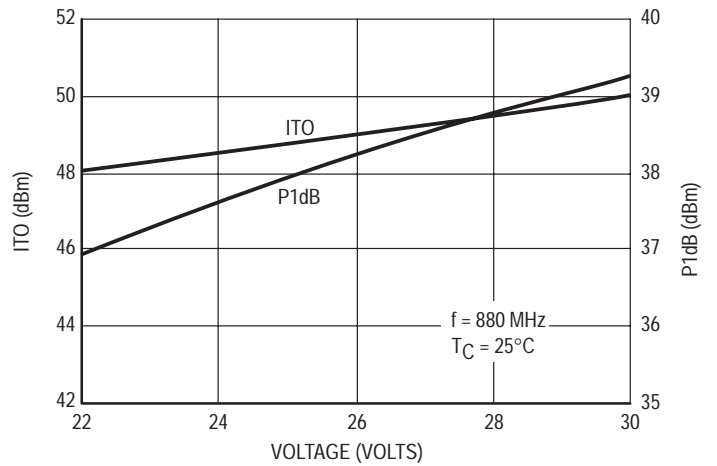


Figure 8. ITO, P1dB versus Voltage

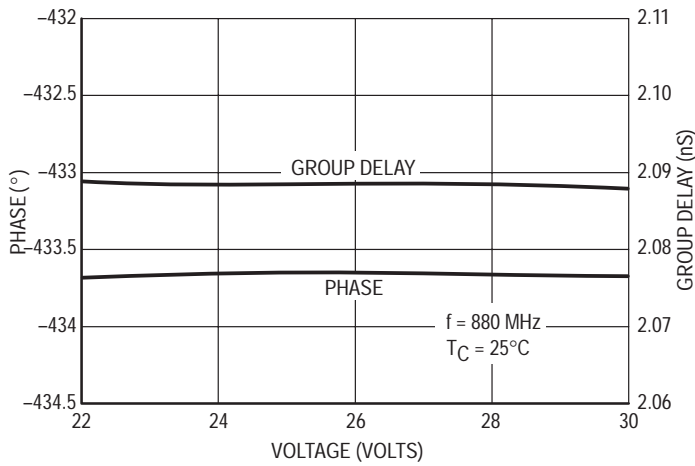


Figure 9. Phase(1), Group Delay(1) versus Voltage
(1)In Production Test Fixture

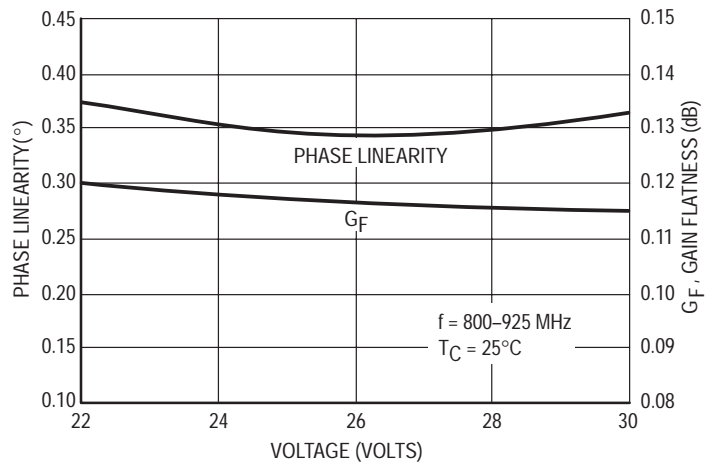


Figure 10. Phase Linearity, Gain Flatness versus Voltage

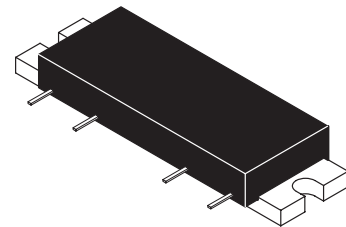
The RF Line
PCS Band
Linear Amplifier

Designed for ultra-linear amplifier applications in 50 ohm systems operating in the PCS frequency band. A silicon FET Class A design provides outstanding linearity and gain. In addition, the excellent group delay and phase linearity characteristics are ideal for digital modulation systems, such as TDMA and CDMA.

- Third Order Intercept: 46 dBm Typ
- Power Gain: 30 dB Typ (@ f = 1960 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- Ideal for Feedforward Base Station Applications

MHL19338

4.0 W, 30 dB
1900–2000 MHz
LINEAR AMPLIFIER



CASE 301AP-01 STYLE 1

ABSOLUTE MAXIMUM RATINGS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V_{DD}	30	Vdc
RF Input Power	P_{in}	+10	dBm
Storage Temperature Range	T_{stg}	-40 to +100	$^\circ\text{C}$
Operating Case Temperature Range	T_C	-20 to +100	$^\circ\text{C}$

ELECTRICAL CHARACTERISTICS ($V_{DD} = 28$ Vdc, $T_C = 25^\circ\text{C}$; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I_{DD}	—	500	525	mA
Power Gain (f = 1960 MHz)	P_G	29	30	31	dB
Gain Flatness (f = 1900–2000 MHz)	G_F	—	0.1	0.4	dB
Power Output @ 1 dB Comp. (f = 1950 MHz)	P_{out} 1 dB	35	36	—	dBm
Input VSWR (f = 1900–2000 MHz)	$VSWR_{in}$	—	1.2:1	1.5:1	
Third Order Intercept (f1 = 1950 MHz, f2 = 1955 MHz)	ITO	45	46	—	dBm
Noise Figure (f = 2000 MHz)	NF	—	4.2	4.5	dB

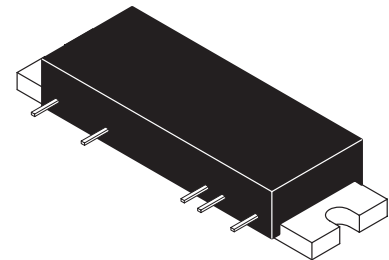
The RF Line
PCS Band
Linear Amplifier

Designed for ultra-linear amplifier applications in 50 ohm systems operating in the PCS frequency band. A silicon FET Class A design provides outstanding linearity and gain. In addition, the excellent group delay and phase linearity characteristics are ideal for digital modulation systems, such as TDMA and CDMA.

- Third Order Intercept: 49.5 dBm Typ
- Power Gain: 29 dB Typ (@ f = 1960 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- Ideal for Feedforward Base Station Applications

MHL19936

1900–2000 MHz
12 W, 29 dB
LINEAR AMPLIFIER



CASE 301AY-01, STYLE 1

ABSOLUTE MAXIMUM RATINGS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V_{DD}	30	Vdc
RF Input Power	P_{in}	+10	dBm
Storage Temperature Range	T_{stg}	-40 to +100	$^\circ\text{C}$
Operating Case Temperature Range	T_C	-20 to +100	$^\circ\text{C}$

ELECTRICAL CHARACTERISTICS ($V_{DD} = 26$ Vdc, $T_C = 25^\circ\text{C}$; 50 Ω System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I_{DD}	—	1.4	1.45	A
Power Gain (f = 1960 MHz)	P_G	28	29	30	dB
Gain Flatness (f = 1900–2000 MHz)	G_F	—	0.2	0.4	dB
Power Output @ 1 dB Comp. (f = 1950 MHz)	P_{out} 1 dB	40	41	—	dBm
Input VSWR (f = 1900–2000 MHz)	$VSWR_{in}$	—	1.2:1	1.5:1	
Third Order Intercept (f1 = 1950 MHz, f2 = 1955 MHz)	ITO	49	49.5	—	dBm
Noise Figure (f = 2000 MHz)	NF	—	4.2	4.5	dB

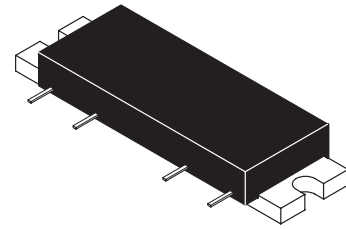
The RF Line
3G Band
Linear Amplifier

Designed for ultra-linear amplifier applications in 50 ohm systems operating in the 3G frequency band. A silicon FET Class A design provides outstanding linearity and gain. In addition, the excellent group delay and phase linearity characteristics are ideal for digital CDMA modulation systems.

- Third Order Intercept: 45 dBm Typ
- Power Gain: 31 dB Typ (@ f = 2140 MHz)
- Excellent Phase Linearity and Group Delay Characteristics
- Ideal for Feedforward Base Station Applications

MHL21336

3.0 W, 31 dB
2110–2170 MHz
LINEAR AMPLIFIER



CASE 301AP-01 STYLE 1

ABSOLUTE MAXIMUM RATINGS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
DC Supply Voltage	V_{DD}	30	Vdc
RF Input Power	P_{in}	+5	dBm
Storage Temperature Range	T_{stg}	-40 to +100	$^\circ\text{C}$
Operating Case Temperature Range	T_C	-20 to +100	$^\circ\text{C}$

ELECTRICAL CHARACTERISTICS ($V_{DD} = 26\text{ Vdc}$, $T_C = 25^\circ\text{C}$; 50 Ω System)

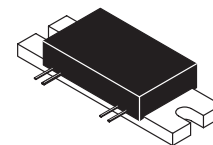
Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I_{DD}	—	500	525	mA
Power Gain (f = 2140 MHz)	P_G	30	31	32	dB
Gain Flatness (f = 2110–2170 MHz)	G_F	—	0.15	0.4	dB
Power Output @ 1 dB Comp. (f = 2140 MHz)	$P_{out\ 1\ dB}$	34	35	—	dBm
Input VSWR (f = 2110–2170 MHz)	$VSWR_{in}$	—	1.2:1	1.5:1	
Third Order Intercept (f1 = 2137 MHz, f2 = 2142 MHz)	ITO	44	45	—	dBm
Noise Figure (f = 2170 MHz)	NF	—	4.5	5	dB

The RF MOSFET Line
RF Power Field Effect Amplifiers
N-Channel Enhancement-Mode Lateral MOSFETs

MHW1810-1
MHW1810-2

- Specified 26 Volts, 1805–1880 MHz, Class AB Characteristics
Output Power = 16 Watts CW Typ
Power Gain = 26 dB Typ @ 10 Watts (MHW1810-1)
Power Gain = 34 dB Typ @ 10 Watts (MHW1810-2)
Efficiency = 34% Min @ 10 Watts
- 50 Ω Input/Output System
- Designed for GSM Linearity Requirements

10 W, 1805–1880 MHz
RF POWER AMPLIFIER



CASE 301AW-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
DC Supply Voltage	V_S	28	Vdc
DC Bias Voltage	V_{bias}	28	Vdc
RF Input Power	P_{in}	21 16	dBm
		MHW1810-1 MHW1810-2	
RF Output Power	P_{out}	20	W
Operating Case Temperature Range	T_C	- 10 to +90	°C
Storage Temperature Range	T_{stg}	- 30 to +100	°C

ELECTRICAL CHARACTERISTICS ($T_C = +25^\circ\text{C}$, $V_S = 26\text{ Vdc}$; $V_{bias} = 5\text{ Vdc}$; 50 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	1805	—	1880	MHz
Quiescent Current ($P_{in} = 0\text{ mW}$)	I_{DQ}	100	—	150	mA
Bias Current	I_{bias}	—	—	2	mA
Output Power at 1 dB Compression	P_{1dB}	10	14	—	W
Power Gain ($P_{out} = 10\text{ W}$)	G_p	24	26	28	dB
		32	34	36	
		MHW1810-1 MHW1810-2			
Efficiency ($P_{out} = 10\text{ W}$)	η	34	—	—	%
Input VSWR ($P_{out} = 10\text{ W}$)	$VSWR_{in}$	—	—	1.8:1	—
Harmonics at $2f_o$ ($P_{out} = 10\text{ W}$)	H_2	—	—	- 35	dBc
Harmonics at $3f_o$ ($P_{out} = 10\text{ W}$)	H_3	—	—	- 45	dBc
Reverse IMD; $P_{out} = 10\text{ W}$; Preverse = -40 dBc ($F_1 = F_0 \pm 200\text{ kHz}$ @ -40 dBc)	IMD_r	—	—	- 50	dBc
Load Mismatch Stress Load VSWR = 5:1, All Phase Angles	ψ	No Degradation in Output Power			
Stability ($P_{out} = 10\text{ mW}$ to 10 W , $V_S \leq 26\text{ Vdc}$) Load VSWR = 5:1, All Phase Angles	—	All Spurious Outputs More Than 60 dB Below Desired Signal			

NOTE – CAUTION – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

EXTREME CASE ELECTRICAL CHARACTERISTICS ($T_C = -10$ to $+85^\circ\text{C}$, $V_S = 23.5$ to 26 Vdc, $V_{\text{bias}} = 3$ to 26 Vdc, $50\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	1805	—	1880	MHz
Quiescent Current ($P_{\text{in}} = 0$ mW)	I_{DQ}	100	—	160	mA
Bias Current	I_{bias}	—	—	2	mA
Output Power at 1 dB Compression	$P_{1\text{dB}}$	8	—	—	W
Power Gain Variation for a Given Part ($P_{\text{out}} = 10$ W)	G_P	—	5	6.5	dB
Efficiency ($P_{\text{out}} = 10$ W)	η	32	—	—	%
Input VSWR	VSWR_{in}	—	—	2:1	—
Harmonics at $2f_0$	H_2	—	—	-35	dBc
Harmonics at $3f_0$	H_3	—	—	-45	dBc
Reverse IMD; $P_{\text{out}} = 10$ W; Preverse = -40 dBc ($F_1 = F_0 \pm 200$ kHz @ -40 dBc)	IMD_r	—	—	-50	dBc
Load Mismatch Stress Load VSWR = 5:1, All Phase Angles	ψ	No Degradation in Output Power			
Stability ($P_{\text{out}} = 10$ mW to 10 W, $V_S \leq 26$ Vdc) Load VSWR = 5:1, All Phase Angles	—	All Spurious Outputs More Than 60 dB Below Desired Signal			

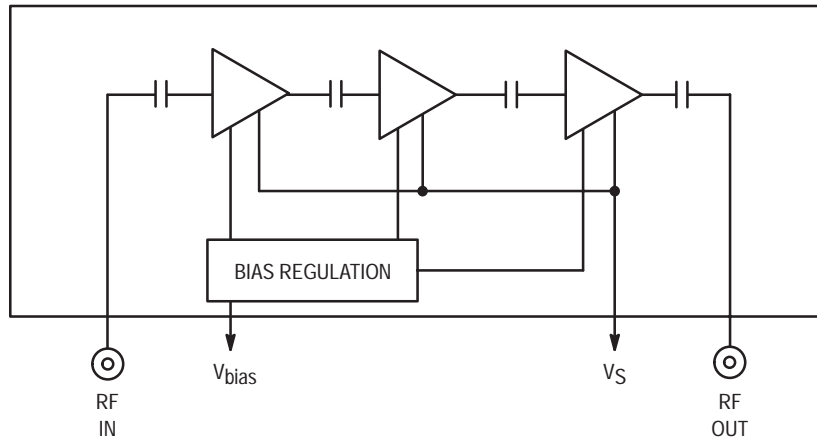


Figure 1. Internal Diagram

TYPICAL CHARACTERISTICS MHW1810-1

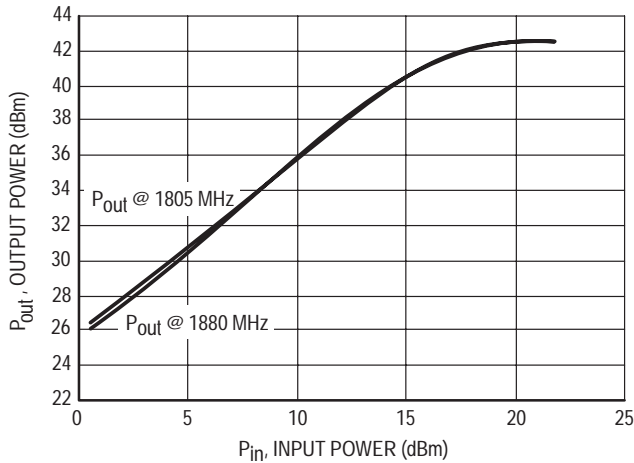


Figure 2. Output Power versus Input Power

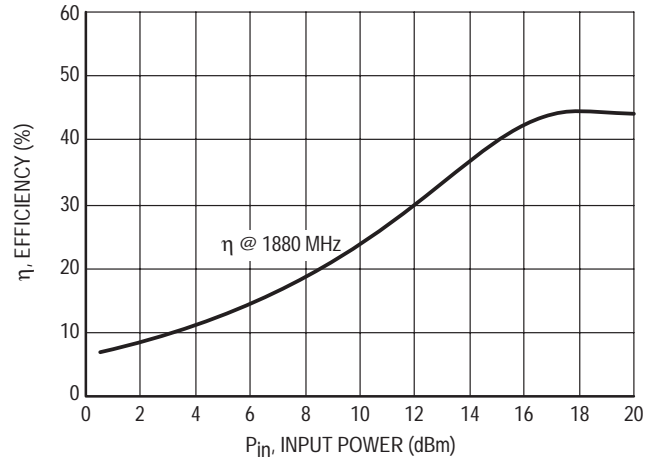


Figure 3. Efficiency versus Input Power

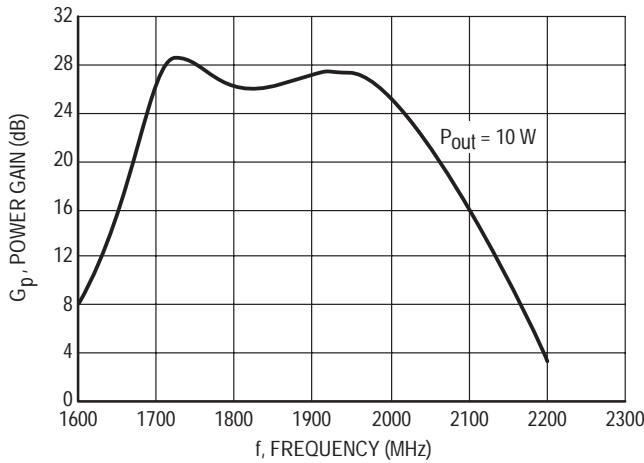


Figure 4. Power Gain versus Frequency

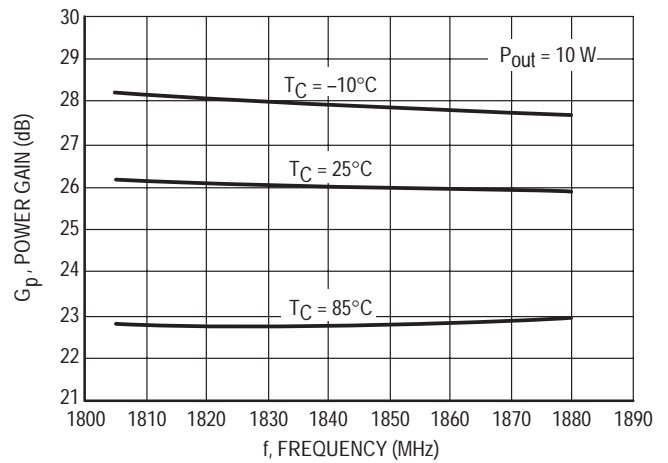


Figure 5. Gain versus Frequency

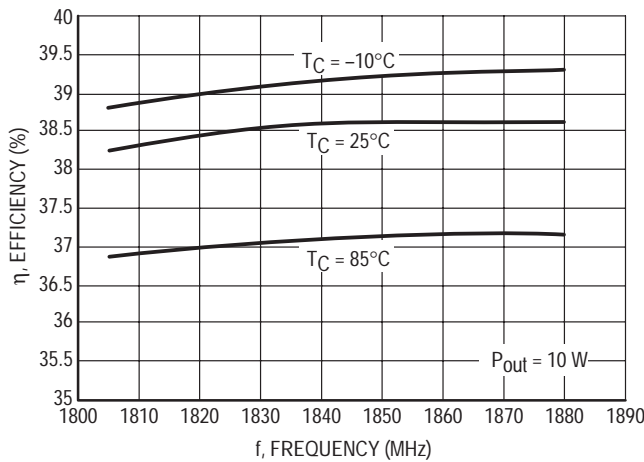


Figure 6. Efficiency versus Frequency

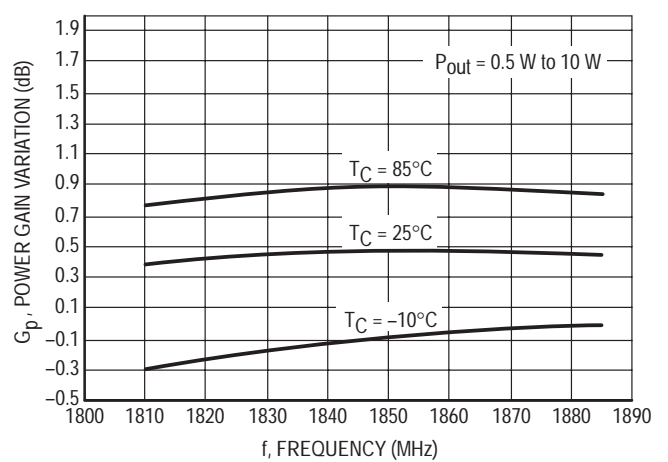


Figure 7. Power Gain Variation versus Frequency

TYPICAL CHARACTERISTICS
MHW1810-1

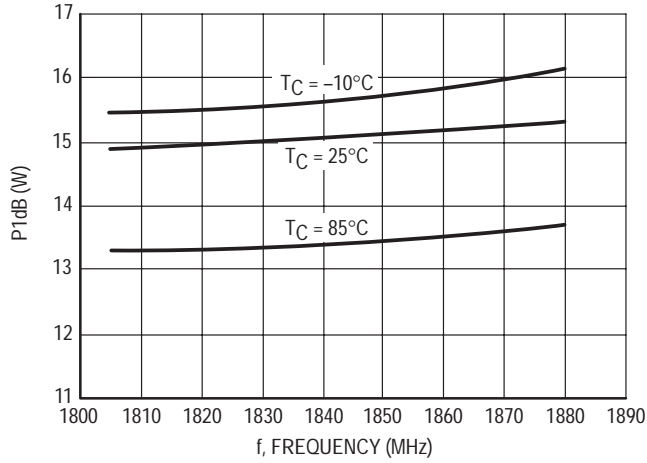


Figure 8. P1dB versus Frequency

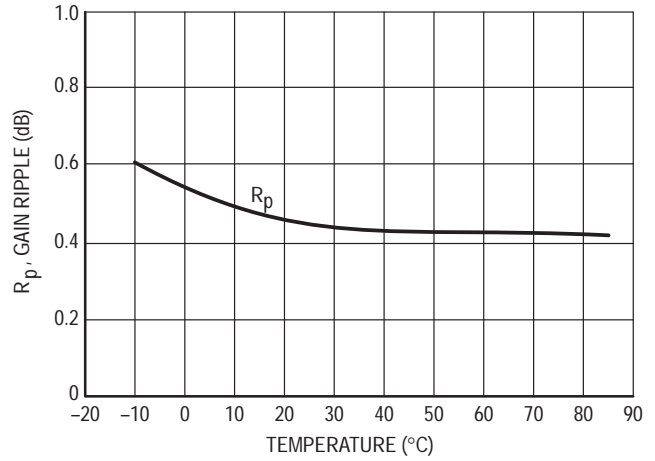


Figure 9. Gain Ripple versus Temperature

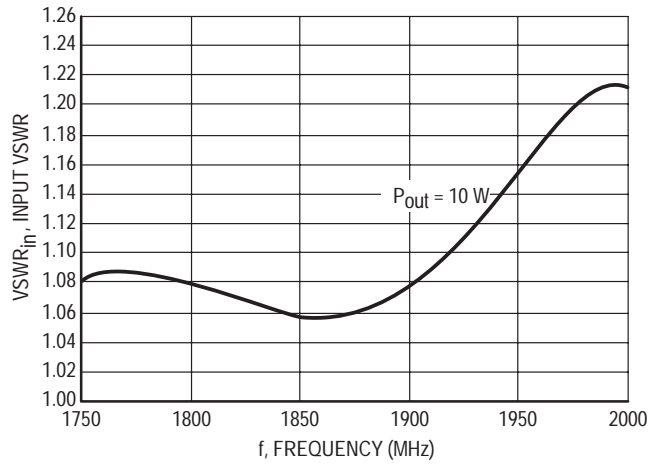


Figure 10. Input VSWR

TYPICAL CHARACTERISTICS MHW1810-2

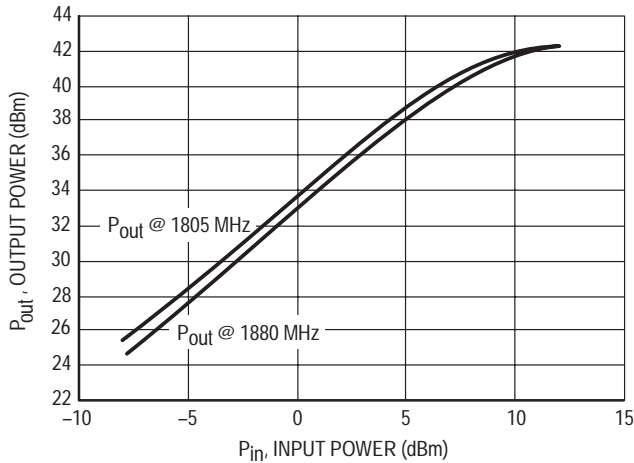


Figure 11. Output Power versus Input Power

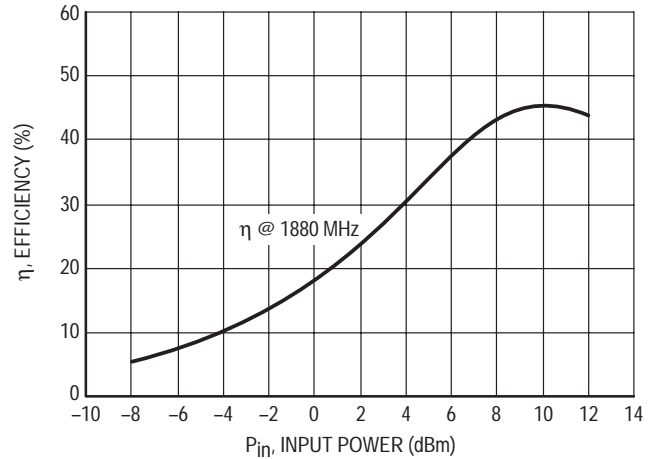


Figure 12. Efficiency versus Input Power

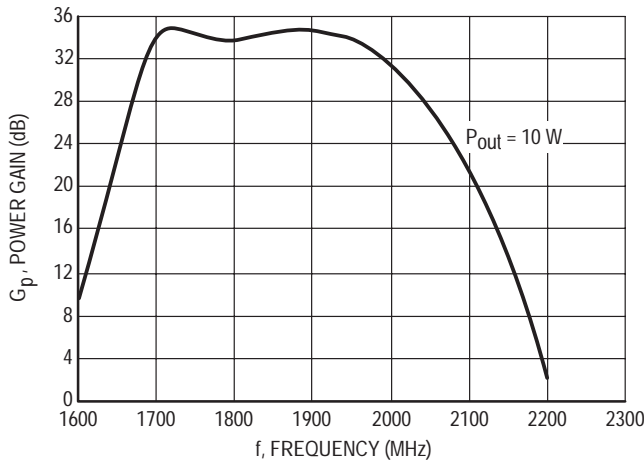


Figure 13. Power Gain versus Frequency

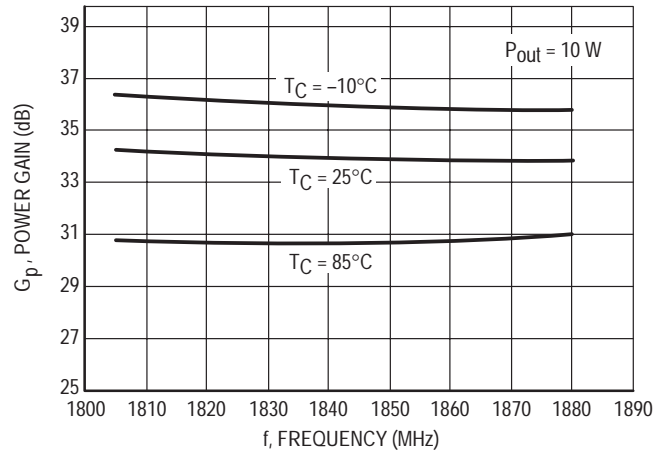


Figure 14. Gain versus Frequency

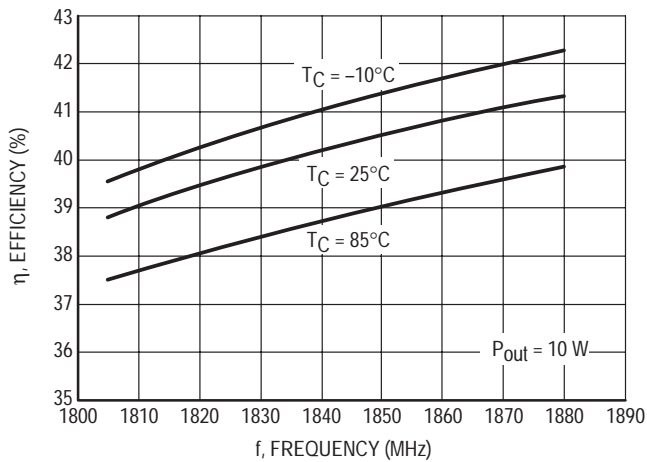


Figure 15. Efficiency versus Frequency

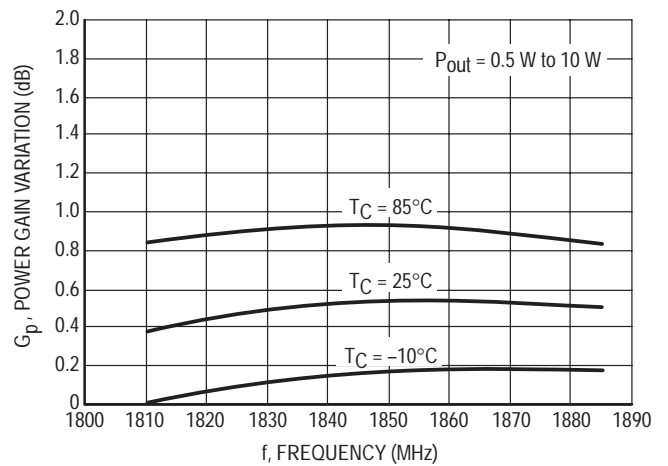


Figure 16. Power Gain Variation versus Frequency

TYPICAL CHARACTERISTICS
MHW1810-2

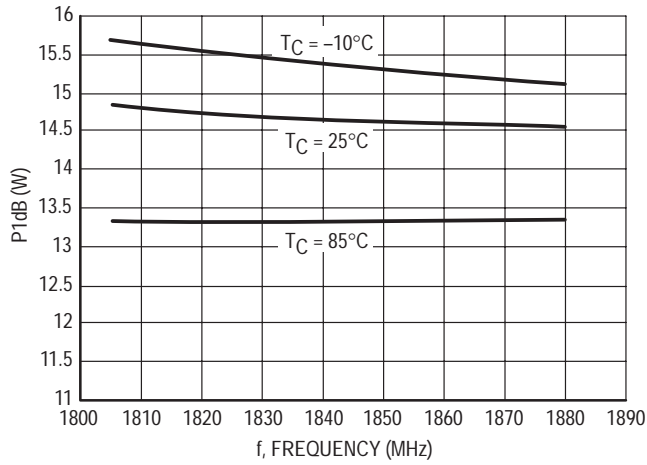


Figure 17. P1dB versus Frequency

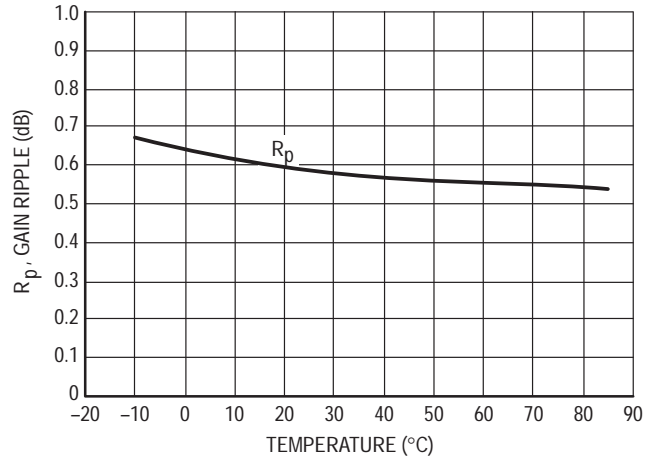


Figure 18. Gain Ripple versus Temperature

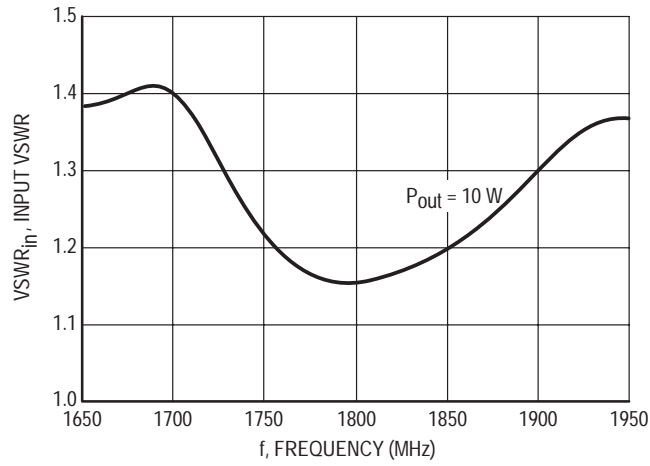


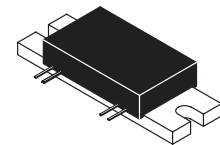
Figure 19. Input VSWR

The RF MOSFET Line
RF Power Field Effect Amplifier
N-Channel Enhancement-Mode Lateral MOSFET

MHW1910-1

- Specified 26 Volts, 1930–1990 MHz, Class AB Characteristics
Output Power = 14 Watts CW Typ
Power Gain = 26 dB Typ @ 10 Watts
Efficiency = 34% Min @ 10 Watts
- 50 Ω Input/Output System
- Designed for GSM Linearity Requirements

**10 W, 1930–1990 MHz
RF POWER AMPLIFIER**



CASE 301AW-02, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
DC Supply Voltage	V_S	28	Vdc
DC Bias Voltage	V_{bias}	28	Vdc
RF Input Power	P_{in}	21	dBm
RF Output Power	P_{out}	20	W
Operating Case Temperature Range	T_C	- 10 to +90	°C
Storage Temperature Range	T_{stg}	- 30 to +100	°C

ELECTRICAL CHARACTERISTICS ($T_C = +25^\circ\text{C}$, $V_S = 26\text{ Vdc}$; $V_{bias} = 5\text{ Vdc}$; 50 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	1930	—	1990	MHz
Quiescent Current ($P_{in} = 0\text{ mW}$)	I_{DQ}	100	—	150	mA
Bias Current	I_{bias}	—	—	2	mA
Output Power at 1 dB Compression	P_{1dB}	10	14	—	W
Power Gain ($P_{out} = 10\text{ W}$)	G_P	24	26	28	dB
Efficiency ($P_{out} = 10\text{ W}$)	η	34	—	—	%
Input VSWR	$VSWR_{in}$	—	—	1.8:1	—
Harmonics at $2f_0$	H_2	—	—	- 35	dBc
Harmonics at $3f_0$	H_3	—	—	- 45	dBc
Reverse IMD; $P_{out} = 10\text{ W}$; Preverse = -40 dBc ($F_1 = F_0 \pm 200\text{ kHz}$ @ -40 dBc)	IMD_r	—	—	- 50	dBc
Load Mismatch Stress Load VSWR = 5:1, All Phase Angles	ψ	No Degradation in Output Power			
Stability ($P_{out} = 10\text{ mW}$ to 10 W, $V_S \leq 26\text{ Vdc}$) Load VSWR = 5:1, All Phase Angles	—	All Spurious Outputs More Than 60 dB Below Desired Signal			

NOTE – **CAUTION** – MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

EXTREME CASE ELECTRICAL CHARACTERISTICS ($T_C = -10$ to $+85^\circ\text{C}$, $V_S = 23.5$ to 26 Vdc, $V_{\text{bias}} = 3$ to 26 Vdc, $50\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	1930	—	1990	MHz
Quiescent Current ($P_{\text{in}} = 0$ mW)	I_{DQ}	100	—	160	mA
Bias Current	I_{bias}	—	—	2	mA
Output Power at 1 dB Compression	$P_{1\text{dB}}$	8	—	—	W
Power Gain Variation for a Given Part ($P_{\text{out}} = 10$ W)	G_P	—	5	6.5	dB
Efficiency ($P_{\text{out}} = 10$ W)	η	32	—	—	%
Input VSWR	VSWR_{in}	—	—	2:1	—
Harmonics at $2f_0$	H_2	—	—	-35	dBc
Harmonics at $3f_0$	H_3	—	—	-45	dBc
Reverse IMD; $P_{\text{out}} = 10$ W; Preverse = -40 dBc ($F_1 = F_0 \pm 200$ kHz @ -40 dBc)	IMD_r	—	—	-46	dBc
Load Mismatch Stress Load VSWR = 5:1, All Phase Angles	ψ	No Degradation in Output Power			
Stability ($P_{\text{out}} = 10$ mW to 10 W, $V_S \leq 26$ Vdc) Load VSWR = 5:1, All Phase Angles	—	All Spurious Outputs More Than 60 dB Below Desired Signal			

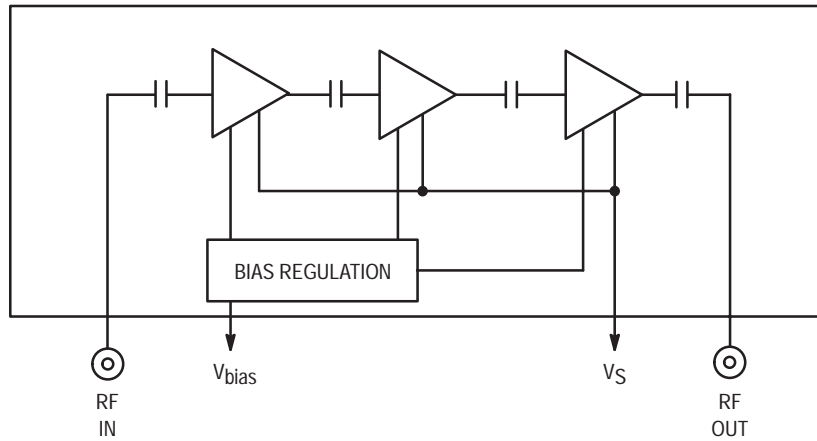


Figure 1. Internal Diagram

TYPICAL CHARACTERISTICS

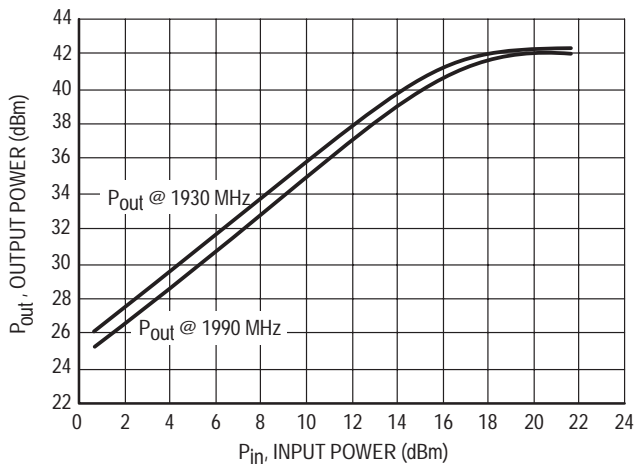


Figure 2. Output Power versus Input Power

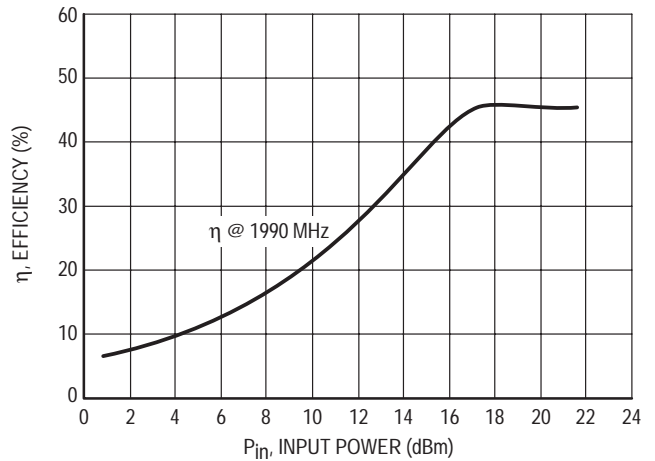


Figure 3. Efficiency versus Input Power

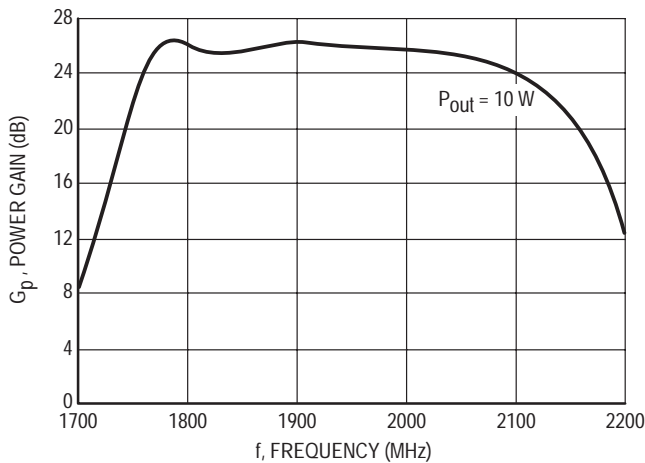


Figure 4. Power Gain versus Frequency

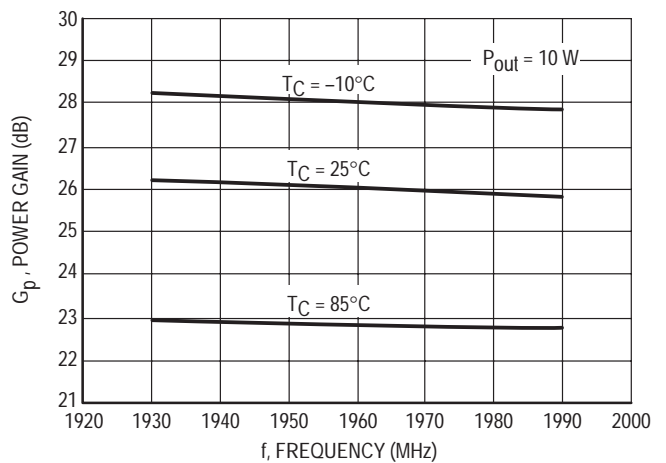


Figure 5. Gain versus Frequency

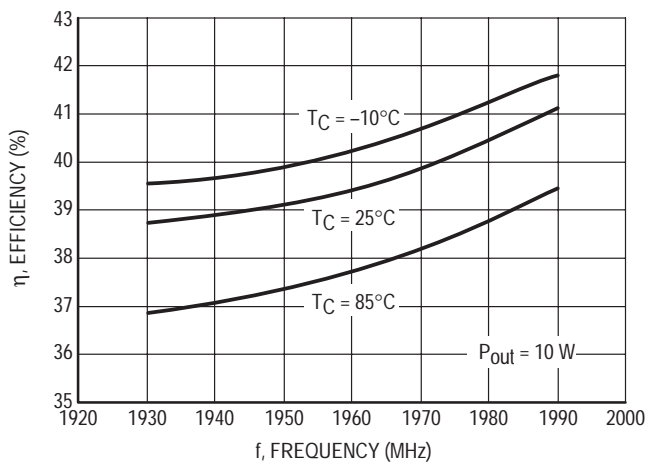


Figure 6. Efficiency versus Frequency

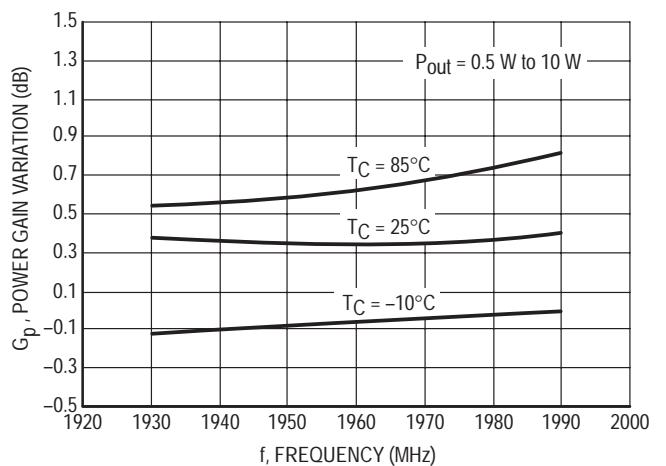


Figure 7. Power Gain Variation versus Frequency

TYPICAL CHARACTERISTICS

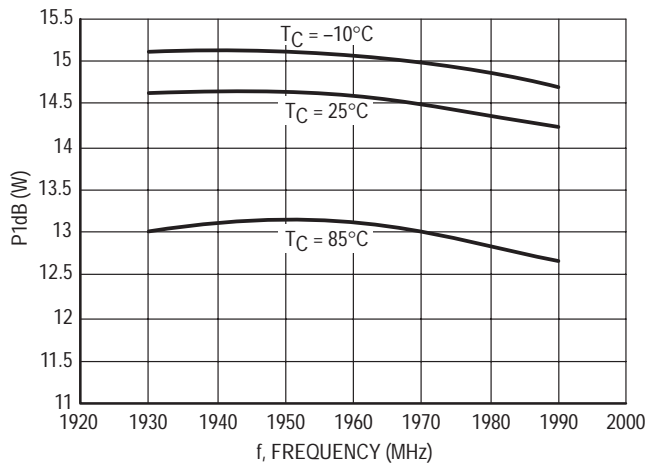


Figure 8. P1dB versus Frequency

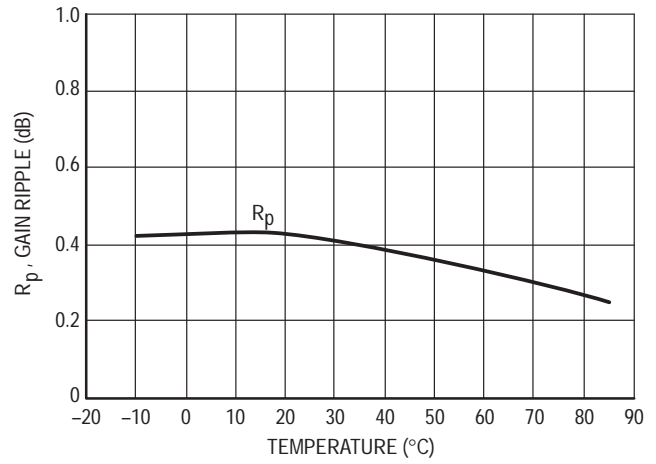


Figure 9. Gain Ripple versus Temperature

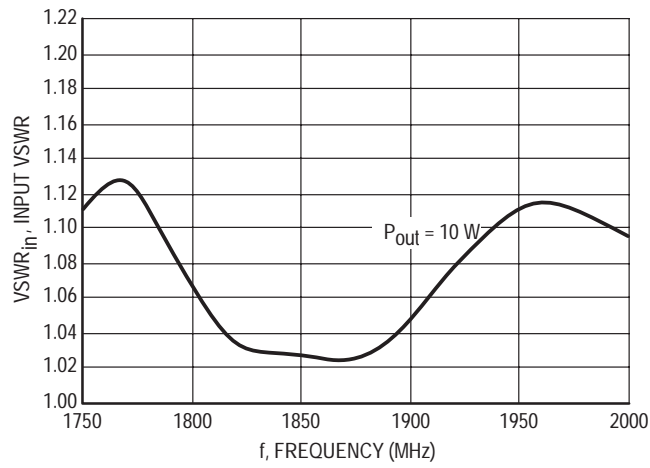


Figure 10. Input VSWR

Chapter Seven

RF CATV Distribution Amplifiers

Section One **7.1-0**
RF CATV Distribution Amplifiers –
Selector Guide

Section Two **7.2-0**
RF CATV Distribution Amplifiers –
Data Sheets

Section One Selector Guide

Motorola RF CATV Distribution Amplifiers

Motorola Hybrids are manufactured using the latest CATV generation technology which has set new standards for CATV system performance and reliability. These hybrids have been optimized to provide premium performance in all CATV systems up to 152 channels. Additions to our CATV product family include 40–870 MHz high output gallium arsenide (GaAs) power doublers as well as low distortion, low power consumption reverse amplifiers.

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	Page
RF CATV Distribution Amplifiers	7.1–1
Forward Amplifiers	7.1–2
Reverse Amplifiers	7.1–4
Packages	7.1–6

Motorola RF CATV Distribution Amplifiers

Motorola Hybrids are manufactured using the latest generation technology which has set new standards for CATV system performance and reliability. These hybrids have been optimized to provide premium performance in all CATV systems up to 152 channels.

Forward Amplifiers

40–1000 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 1000 MHz dB Max	Package/Style
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat	Cross Modulation		
					dB 152 CH	dB 152 CH		
MHW9182B	18.5	152	+38	-63 ⁽⁴⁰⁾	-61	-61	7.5	714Y/1
MHW9242A	24	152	+38	-61 ⁽⁴⁰⁾	-58	-59	8.0	714Y/1

40–870 MHz High Output Gallium Arsenide Power Doubler

Device	Hybrid Gain (Nom.) @ 870 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 870 MHz dB Max	Package/Style
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat	Cross Modulation		
					dB 132 CH	dB 132 CH		
MHW9187 ^(46b)	20	132	+48	-62 ⁽³⁴⁾	-58	-55	4.5	1302/1

40–860 MHz Hybrids

Device	Gain dB Typ @ 50 MHz	Frequency MHz	V_{CC} Volts	2nd Order IMD @ $V_{out} = 50$ dBmV/ch Max	DIN45004B @ $f=860$ MHz dB μ V Min	Noise Figure @ 860 MHz dB Max	Package/Style
CA901	17	40 – 860	24	-60	120	8.0	714P/2

Power Doubling Hybrids

CA922	17	40 – 860	24	-63	123	9.5	714P/2
CA922A	17	40 – 860	24	-67	123	9.5	714P/2

40–860 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 860 MHz dB Max	Package/Style
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat	Cross Modulation FM = 55 MHz dB		
					dB 128 CH	dB 128 CH		
MHW8182B	18.5	128	+38	-64 ⁽⁴⁰⁾	-66	-65	7.5	714Y/1
MHW8222B★	21.9	128	+38	-60 ⁽⁴⁰⁾	-64	-63	7.0	1302/1
MHW8242A	24	128	+38	-62 ⁽⁴⁰⁾	-64	-62	7.5	714Y/1
MHW8272A	27.2	128	+38	-64 ⁽⁴⁰⁾	-64	-62	7.0	714Y/1
MHW8292	29	128	+38	-56 ⁽⁴⁰⁾	-60	-60	7.0	714Y/1

⁽³⁴⁾Composite 2nd Order; $V_{out} = +48$ dBmV/ch

⁽⁴⁰⁾Composite 2nd Order; $V_{out} = +38$ dBmV/ch

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

CATV Distribution: Forward Amplifiers (continued)

40–860 MHz Hybrids, V_{CC} = 24 Vdc, Class A (continued)

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 860 MHz dB Max	Package/Style
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat	Cross Modulation FM = 55 MHz dB		
					dB	dB		
					128 CH	128 CH		

Power Doubling Hybrids

MHW8185L ⁽²¹⁾	18.5	128	+40	-62 ⁽³⁹⁾	-63	-64	8.5*	714Y/1
MHW8185LR ⁽²⁸⁾	18.5	128	+40	-62 ⁽³⁹⁾	-63	-64	8.5*	714Y/2
MHW8185	18.8	128	+40	-62 ⁽³⁹⁾	-64	-64	8.0	714Y/1
MHW8185R ⁽¹⁴⁾	18.8	128	+40	-62 ⁽³⁹⁾	-64	-64	8.0	714Y/2
MHW8205L ⁽²²⁾	19.5	128	+40	-60 ⁽³⁹⁾	-63	-64	8.5*	714Y/1
MHW8205	19.8	128	+40	-60 ⁽³⁹⁾	-63	-64	8.0	714Y/1
MHW8205R ⁽²⁴⁾	19.8	128	+40	-60 ⁽³⁹⁾	-63	-64	8.0	714Y/2

*@ 870 MHz

40–750 MHz Hybrids, V_{CC} = 24 Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 750 MHz dB Max	Package/Style
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat	Cross Modulation FM = 55 MHz dB		
					dB	dB		
					110 CH	110 CH		

Power Doubling Hybrids

MHW7185CL ⁽²³⁾	18.5	110	+44	-64 ⁽³⁶⁾	-61	-63	7.5	714Y/1
MHW7185C	18.8	110	+44	-64 ⁽³⁶⁾	-62	-63	7.5	714Y/1
MHW7205CL ⁽²⁷⁾	19.5	110	+44	-63 ⁽³⁶⁾	-61	-62	7.5	714Y/1
MHW7205C	19.8	110	+44	-63 ⁽³⁶⁾	-61	-62	7.5	714Y/1

⁽¹⁴⁾Mirror Amplifier Version of MHW8185

⁽²¹⁾Low DC Current Version of MHW8185; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²²⁾Low DC Current Version of MHW8205; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²³⁾Low I_{CC} Version of MHW7185C; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²⁴⁾Mirror Amplifier Version of MHW8205

⁽²⁷⁾Low I_{CC} Version of MHW7205C; Typical I_{CC} @ V_{dc} = 24 V is 365 mA.

⁽²⁸⁾Mirror Amplifier Version of MHW8185L

⁽³⁶⁾Composite 2nd order; V_{out} = +44 dBmV/ch

⁽³⁹⁾Composite 2nd order; V_{out} = +40 dBmV/ch

⁽⁴⁶⁾To be introduced: a) 1Q01; b) 2Q01; c) 3Q01

★New Product

CATV Distribution: Forward Amplifiers (continued)

40–550 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) @ 50 MHz dB	Channel Loading Capacity	Maximum Distortion Specifications				Noise Figure @ 550 MHz dB Max	Package/Style	
			Output Level dBmV	2nd Order Test dB	Composite Triple Beat dB				Cross Modulation dB 77 CH
					77 CH				
MHW6342T	34.5	77	+44	-64 ⁽³⁵⁾	-57		-57	6.5	1302/1

Reverse Amplifiers

5–200 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications						Noise Figure @ 175 MHz dB Max	Package/Style
			Output Level dBmV	2nd Order Test ⁽³⁰⁾ dB	Composite Triple Beat dB		Cross Modulation dB			
					22 CH	26 CH	22 CH	26 CH		
MHW1224	22	22	+50	-72	-69	-68.5 ⁽¹⁹⁾	-62	-62 ⁽¹⁹⁾	5.5	714Y/1
MHW1244	24	22	+50	-72	-68	-67.5 ⁽¹⁹⁾	-61	-61 ⁽¹⁹⁾	5.0	714Y/1

Low Current Amplifiers — 5–200 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications								DC Current mA Typ.	Noise Figure @ 200 MHz dB Max	Pkg/Style
			Output Level dBmV	2nd Order Test dB		Composite Triple Beat dB		Cross Modulation dB					
				6 CH	10 CH	6 CH	10 CH	6 CH	10 CH				
MHW1223LA★	22.7	6,10	50	-68	-65	-75	-66	-65	-60	95	7.0	1302/1	
MHW1253LA★	25.5	6,10	50	-68	-66	-75	-66	-65	-61	95	6.5	1302/1	
MHW1303LA★	30.8	6,10	50	-68	-65	-74	-64	-64	-58	95	5.7	1302/1	

Low Current Amplifiers — 5–150 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications							DC Current mA Typ.	Noise Figure @ 150 MHz dB Max	Pkg/Style
			Output Level dBmV	2nd Order Test dB		Composite Triple Beat dB		Cross Modulation dB				
				6 CH	10 CH	6 CH	10 CH	6 CH	10 CH			
MHW1353LA★	35.2	6,10	50	-68	-65	-73	-62	-63	-57	95	5.4	1302/1

(19)Typical

(30)Channels 2 and A @ 7

(35)Channels 2 and M30 @ M39

(36)Composite 2nd order; $V_{Out} = +44$ dBmV/ch

★New Product

CATV Distribution: Reverse Amplifiers (continued)

Low Current Amplifiers — 5–65 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	Maximum Distortion Specifications							DC Current mA Typ.	Noise Figure @ 65 MHz dB Max	Pkg/ Style
			Output Level dBmV	2nd Order Test dB		Composite Triple Beat dB		Cross Modulation dB				
				6 CH	10 CH	6 CH	10 CH	6 CH	10 CH			
MHW1224LA★	22.7	6,10	50	-68	-65	-75	-66	-65	-60	95	7.0	1302/1
MHW1254LA★	25.5	6,10	50	-68	-66	-75	-66	-65	-61	95	6.5	1302/1
MHW1304LA★	30.8	6,10	50	-68	-65	-74	-64	-64	-58	95	5.7	1302/1
MHW1354LA★	35	6,10	50	-68	-65	-73	-62	-63	-57	95	5.2	1302/1

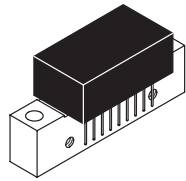
Low Current Amplifiers — 5–50 MHz Hybrids, $V_{CC} = 24$ Vdc, Class A

Device	Hybrid Gain (Nom.) dB	Channel Loading Capacity	I_{DC} mA Max	Maximum Distortion Specifications				Noise Figure @ 50 MHz dB Max	Package/ Style
				Output Level dBmV	2nd Order Test ⁽³⁰⁾ dB	Composite Triple Beat dB	Cross Modulation dB		
						4 CH	4 CH		
MHW1254L	25	4	135	+50	-70	-70	-62	4.5	714Y/1
MHW1304L	30	4	135	+50	-70	-66	-57	4.5	714Y/1

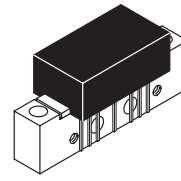
⁽³⁰⁾Channels 2 and A @ 7

★New Product

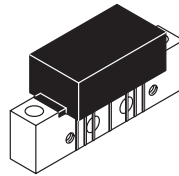
RF CATV Distribution Amplifiers Packages



CASE 714P
STYLE 2



CASE 714Y
STYLE 1, 2



CASE 1302
STYLE 1

SCALE 1:2

Section Two

Motorola RF CATV Distribution Amplifiers – Data Sheets

Device Number	Page Number	Device Number	Page Number
CA901	7.2-3	MHW7205C	7.2-32
CA922	7.2-5	MHW7205CL	7.2-33
CA922A	7.2-5	MHW7222B	7.2-34
MHW1223LA	7.2-7	MHW7272A	7.2-36
MHW1224	7.2-9	MHW7292	7.2-37
MHW1224LA	7.2-11	MHW8182B	7.2-38
MHW1244	7.2-9	MHW8185	7.2-39
MHW1253LA	7.2-13	MHW8185L	7.2-40
MHW1254L	7.2-15	MHW8185LR	7.2-41
MHW1254LA	7.2-16	MHW8185R	7.2-42
MHW1303LA	7.2-18	MHW8205	7.2-43
MHW1304L	7.2-20	MHW8205L	7.2-44
MHW1304LA	7.2-21	MHW8205R	7.2-45
MHW1353LA	7.2-23	MHW8222B	7.2-46
MHW1354LA	7.2-25	MHW8242A	7.2-48
MHW6342T	7.2-27	MHW8272A	7.2-49
MHW7182B	7.2-29	MHW8292	7.2-50
MHW7185C	7.2-30	MHW9182B	7.2-51
MHW7185CL	7.2-31	MHW9242A	7.2-52

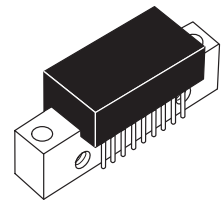
The RF Line VHF/UHF CATV Amplifiers

Designed for broadband applications requiring low-distortion amplification. Specifically intended for CATV/MATV market requirements. These amplifiers feature ion-implanted arsenic emitter transistors and an all gold metal system.

- Specified Characteristics at $V_{CC} = 24\text{ V}$, $T_C = 25^\circ\text{C}$:
 - Frequency Range — 40 to 860 MHz
 - Power Gain — 17 dB Typ @ $f = 40\text{ MHz}$
 - Noise Figure — 6.5 dB Typ @ $f = 500\text{ MHz}$
 - 120 dB μV DIN45004B @ 860 MHz
- All Gold Metallization for Improved Reliability
- Superior Gain, Return Loss and DC Current Stability with Temperature

CA901

17 dB
40–860 MHz
VHF/UHF
CATV/MATV
AMPLIFIERS



CASE 714P-03, STYLE 2
(CA)

MAXIMUM RATINGS ($T_A = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+14	dBm
Supply Voltage	V_{CC}	26	Vdc
Operating Case Temperature Range	T_C	-20 to +100	$^\circ\text{C}$
Storage Temperature Range	T_{stg}	-40 to +100	$^\circ\text{C}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$, $V_{CC} = 24\text{ V}$, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	860	MHz
Power Gain ($f = 40\text{ MHz}$)	P_G	16.5	17	17.5	dB
Slope (40–860 MHz)	S	0.2	0.8	1.5	dB
Gain Flatness	—	—	—	0.6	dB
Input/Output Return Loss $f = 40\text{--}100\text{ MHz}$ $f = 100\text{--}800\text{ MHz}$ $f = 800\text{--}860\text{ MHz}$	IRL/ORL	20 15 10/15	— 17 12/18	— — —	dB
Second Order Intermodulation Distortion ($V_{out} = +50\text{ dBmV}$ per ch.)	IMD_2	—	—	-60	dB
DIN45004B (See Figure 1) $f = 40\text{--}400\text{ MHz}$ $f = 400\text{--}860\text{ MHz}$	DIN	121 120	— —	— —	dB μV
Noise Figure $f = 500\text{ MHz}$ $f = 860\text{ MHz}$	NF	— —	6.5 7.0	7.5 8.0	dB
Supply Current	I_{DC}	—	235	255	mA

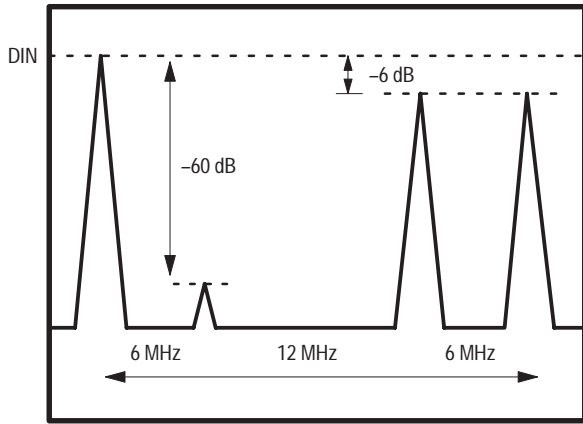


Figure 1. DIN45004B Test

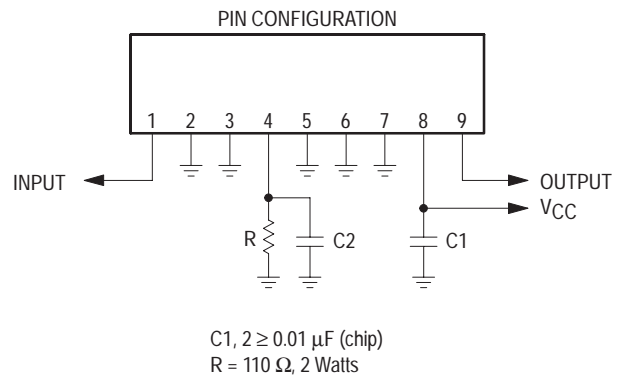


Figure 2. External Connections

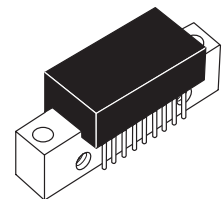
The RF Line VHF/UHF CATV Amplifiers

Designed for broadband applications requiring low-distortion and high output capability. Specifically intended for CATV/MATV market requirements. These amplifiers feature ion-implanted arsenic emitter transistors and an all gold metal system.

- Specified Characteristics at $V_{CC} = 24\text{ V}$, $T_C = 25^\circ\text{C}$
 - Frequency Range — 40 to 860 MHz
 - Power Gain — 17 dB Typ @ $f = 40\text{ MHz}$
 - Noise Figure — 7.0 dB Typ @ $f = 500\text{ MHz}$
 - 123 dB μV DIN45004B @ 860 MHz
- All Gold Metalization for Improved Reliability
- Superior Gain, Return Loss and DC Current Stability with Temperature
- Improved 2nd Order IMD Available (CA922A)

CA922
CA922A

17 dB
40–860 MHz
VHF/UHF
CATV/MATV
AMPLIFIERS



CASE 714P-03, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Supply Voltage	V_{CC}	26	V
RF Input Power Per Tone	P_{in}	+16	dBm
Storage Temperature	T_{stg}	-40 to +100	$^\circ\text{C}$
Operating Case Temperature Range	T_C	-20 to +100	$^\circ\text{C}$

ELECTRICAL CHARACTERISTICS ($T_C = 25^\circ\text{C}$, $V_{CC} = 24\text{ V}$, 75 Ohm System)

Characteristic	Symbol	Min	Typ	Max	Unit
Supply Current	I_{dc}	—	400	440	mA
Power Gain ($f = 40\text{ MHz}$)	PG	16.5	17	17.5	dB
Bandwidth	BW	40	—	860	MHz
Slope (40 – 860 MHz)	S	0.2	0.8	1.5	dB
Gain Flatness	FL	—	—	1.0	dB
Input/Output Return Loss $f = 40\text{--}100\text{ MHz}$ $f = 100\text{--}800\text{ MHz}$ $f = 800\text{--}860\text{ MHz}$	IRL/ORL	20 15 10/13	— 17 12/15	— — —	dB
Second Order Intermodulation Distortion ($V_O = +50\text{ dBmV/ch.}$)	IMD ₂	— —	— —	-63 -67	dB dB
DIN45004B (See Figure 1) $f = 40\text{--}400\text{ MHz}$ $f = 400\text{--}860\text{ MHz}$	DIN	124 123	— —	— —	dB μV
Noise Figure $f = 500\text{ MHz}$ $f = 860\text{ MHz}$	NF	— —	7.0 8.0	8.5 9.5	dB

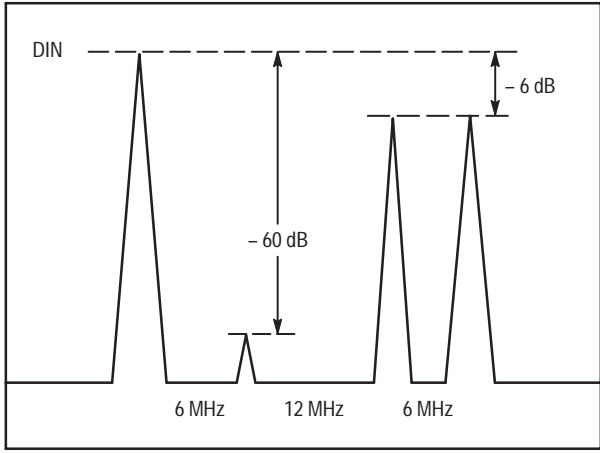


Figure 1. DIN45004B Test

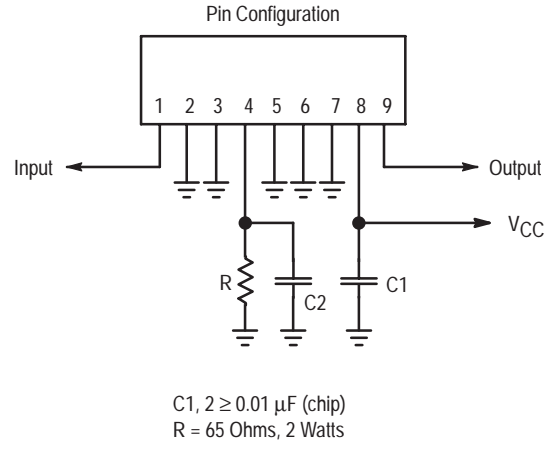


Figure 2. External Connections

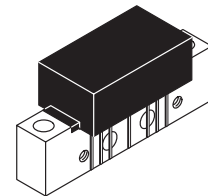
The RF Line Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1223LA

**5–200 MHz, 22.7 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	- 20 to +100	°C
Storage Temperature Range	T_{stg}	- 40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	200	MHz
Power Gain (f = 5 MHz)	G_p	22.1	22.7	23.5	dB
Slope (5–200 MHz)	S	- 0.2	—	0.7	dB
Gain Flatness (Peak To Valley) (5–200 MHz)	—	—	—	0.4	dB
Return Loss — Input/Output (@ f = 5–150 MHz) (@ f = 150–200 MHz)	IRL/ORL	20 18	— —	— —	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO_6	—	- 73	- 68	
10-Channel FLAT	CSO_{10}	—	- 72	- 65	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, $75\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	XMD ₆	—	-69	-65	
10-Channel FLAT	XMD ₁₀	—	-63	-60	
Composite Triple Beat ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CTB ₆	—	-78	-75	
10-Channel FLAT	CTB ₁₀	—	-69	-66	
Noise Figure ($f = 5$ – 200 MHz)	NF	—	6.3	7	dB
DC Current	I_{DC}	85	95	110	mA

The RF Line

Low Distortion

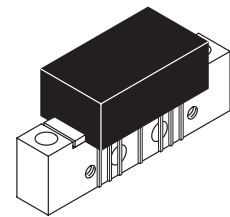
Wideband Amplifiers

MHW1224
MHW1244

Designed specifically for broadband applications requiring low distortion characteristics. Specified for use as return amplifiers for mid-split and high-split 2-way cable TV systems. Features all gold metallization system.

- Guaranteed Broadband Power Gain @ $f = 5.0\text{--}200\text{ MHz}$
- Guaranteed Broadband Noise Figure @ $f = 5.0\text{--}175\text{ MHz}$
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- All Ion-Implanted Arsenic Emitter Transistor Chips with $6.0\text{ GHz } f_T$'s
- Circuit Design Optimized for Good RF Stability Under High VSWR Load Conditions
- Transformers Designed to Insure Good Low Frequency Gain Stability versus Temperature

22.0 dB
24.0 dB
5.0–200 MHz
CATV HIGH-SPLIT
REVERSE AMPLIFIERS



CASE 714Y-03, STYLE 1

ABSOLUTE MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+65	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, $75\ \Omega$ system)

Characteristic	Symbol	MHW1224	MHW1244	Units
Power Gain @ 10 MHz	G_P	22.0 ± 0.5	24.0 ± 0.5	dB
Frequency Range (Response/Return Loss) Note 1	BW	5.0–200		MHz
Cable Slope Equivalent (5.0–200 MHz)	S	-0.2 Min/+0.8 Max		dB
Gain Flatness (5.0–200 MHz)	F	± 0.2 Max		dB
Input/Output Return Loss (5.0–200 MHz) Note 1	IRL/ORL	18.0 Min		dB
Cross Modulation Distortion @ +50 dBmV per ch.				
12-Channel FLAT (5.0–120 MHz)	XM_{12}	-67 Typ	-66 Typ	dB
22-Channel FLAT (5.0–175 MHz) (2) (3)	XM_{22}	-62 Max	-61 Max	dB
26-Channel FLAT (5.0–200 MHz)	XM_{26}	-62 Typ	-61 Typ	dB

NOTES:

1. Response and return loss characteristics are tested and guaranteed for the full 5.0–200 MHz frequency range.
2. Motorola 100% distortion and noise figure testing is performed over the 5.0–175 MHz frequency range. Cross modulation and composite triple beat testing are with 22-channel loading; Video carriers used are:

T7–T13	7.0–43.0 MHz	7-Channels
2–6	55.25–83.25 MHz	5-Channels
A–7	121.25–175.25 MHz	10-Channels
3. Video carriers used for 12-Channel typical performances are T7–6; For 26-Channel typical performance, Channels 8, 9, 10 and 11 are added to the 22-Channel carriers listed above.

ELECTRICAL CHARACTERISTICS — continued ($V_{CC} = 24 \text{ Vdc}$, $T_C = +30^\circ\text{C}$, 75Ω system)

Characteristic	Symbol	MHW1224	MHW1244	Units
Composite Triple Beat Distortion @ +50 dBmV per ch. 22-Channel FLAT (5.0–175 MHz) 26-Channel FLAT (5.0–200 MHz) Notes 2 and 3	CTB ₂₂ CTB ₂₆	–69 Max –68.5 Typ	–68 Max –67.5 Typ	dB dB
Individual Triple Beat Distortion @ +50 dBmV per ch. Mid-Split (5.0–120 MHz) T11, T12 and CH2 @ 123.25 MHz High-Split (5.0–175 MHz) T13, CH2 and CH5 @ 175.5 MHz	TB ₃ TB ₃	–88 Typ –85 Typ	–87 Typ –84 Typ	dB dB
Second Order Distortion @ +50 dBmV per ch. High-Split (5.0–175 MHz) CH2, CHA @ 176.5 MHz	IMD	–72 Max	–72 Max	dB
Noise Figure High-Split (5.0–175 MHz) Note 2	NF	5.5 Max	5.0 Max	dB
DC Current	I _{DC}	210 Typ/240 Max		mAdc

NOTES:

- Response and return loss characteristics are tested and guaranteed for the full 5.0–200 MHz frequency range.
- Motorola 100% distortion and noise figure testing is performed over the 5.0–175 MHz frequency range. Cross modulation and composite triple beat testing are with 22-channel loading; Video carriers used are:

T7–T13	7.0–43.0 MHz	7-Channels
2–6	55.25–83.25 MHz	5-Channels
A–7	121.25–175.25 MHz	10-Channels
- Video carriers used for 12-Channel typical performances are T7–6; For 26-Channel typical performance, Channels 8, 9, 10 and 11 are added to the 22-Channel carriers listed above.

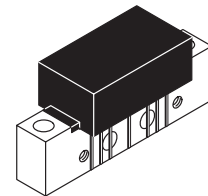
The RF Line Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1224LA

**5–65 MHz, 22.7 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	- 20 to +100	°C
Storage Temperature Range	T_{stg}	- 40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	65	MHz
Power Gain (f = 5 MHz)	G_p	22.1	22.7	23.2	dB
Slope (5–65 MHz)	S	- 0.2	—	0.5	dB
Gain Flatness (Peak To Valley) (5–65 MHz)	—	—	—	0.4	dB
Return Loss — Input/Output (@ f = 5–65 MHz)	IRL/ORL	20	—	—	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO ₆	—	- 73	- 68	
10-Channel FLAT	CSO ₁₀	—	- 72	- 65	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, $75\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	XMD ₆	—	-69	-65	
10-Channel FLAT	XMD ₁₀	—	-63	-60	
Composite Triple Beat ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CTB ₆	—	-78	-75	
10-Channel FLAT	CTB ₁₀	—	-69	-66	
Noise Figure ($f = 5$ – 65 MHz)	NF	—	6.3	7	dB
DC Current	I_{DC}	85	95	110	mA

The RF Line

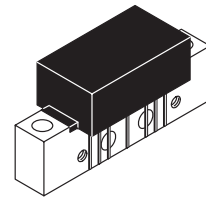
Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1253LA

**5–200 MHz, 25.5 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	- 20 to +100	°C
Storage Temperature Range	T_{stg}	- 40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	200	MHz
Power Gain (f = 5 MHz)	G_p	25	25.5	26	dB
Slope (5–200 MHz)	S	- 0.2	—	0.7	dB
Gain Flatness (Peak To Valley) (5–200 MHz)	—	—	—	0.4	dB
Return Loss — Input/Output (@ f = 5–150 MHz) (@ f = 150–200 MHz)	IRL/ORL	20 18	— —	— —	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO_6	—	- 73	- 68	
10-Channel FLAT	CSO_{10}	—	- 71	- 66	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24 \text{ Vdc}$, $T_C = 30^\circ\text{C}$, 75Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50 \text{ dBmV}$ per Ch., Worst Case)	6-Channel FLAT	—	-69	-65	dB
	10-Channel FLAT	—	-64	-61	
Composite Triple Beat ($V_{out} = +50 \text{ dBmV}$ per Ch., Worst Case)	6-Channel FLAT	—	-78	-75	dB
	10-Channel FLAT	—	-69	-66	
Noise Figure ($f = 5\text{--}200 \text{ MHz}$)	NF	—	5.8	6.5	dB
DC Current	I_{DC}	85	95	110	mA

The RF Line

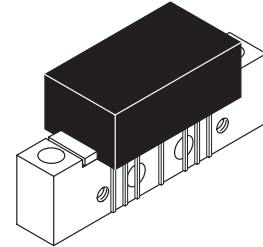
Low Distortion Wideband Reverse Amplifier Module

Designed specifically for broadband applications requiring low distortion characteristics. Specified for use as return amplifiers for low-split, 2-way cable TV systems. Features all gold metallization system.

- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- Circuit Design Optimized for Good RF Stability Under High VSWR Load Conditions
- Transformers Designed to Insure Good Low Frequency Gain Stability versus Temperature

MHW1254L

**24 Vdc, 50 MHz, 25 dB
CATV LOW CURRENT AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{IN}	+70	dBmV
Operating Case Temperature Range	T_C	- 20 to +100	°C
Storage Temperature Range	T_{stg}	- 40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 ohm system, unless otherwise noted)

Characteristic	Symbol	Min	Max	Unit
Bandwidth	BW	5.0	50	MHz
Power Gain (f = 5.0 MHz)	G_p	24.3	25.8	dB
Return Loss (@ f = 5.0–50 MHz)	RL	20	—	dB
Second Order Distortion ($V_{out} = +50$ dBmV/ch)	IMD	—	-70	dBc
Cross Modulation ($V_{out} = +50$ dBmV/ch)	XMD ₄	—	-62	dBc
Triple Beat Distortion ($V_{out} = +50$ dBmV/ch)	TB ₃	—	-70	dBc
Noise Figure (f = 50 MHz)	NF	—	4.5	dB
DC Current	IDC	100	135	mA

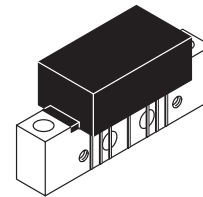
The RF Line
**Low Distortion Wideband
Reverse Amplifier Modules**

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1254LA

**5–65 MHz, 25.5 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	65	MHz
Power Gain (f = 5 MHz)	G_p	25	25.5	26	dB
Slope (5–65 MHz)	S	-0.2	—	0.5	dB
Gain Flatness (Peak To Valley) (5–65 MHz)	—	—	—	0.4	dB
Return Loss — Input/Output (@ f = 5–65 MHz)	IRL/ORL	20	—	—	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO_6	—	-73	-68	
10-Channel FLAT	CSO_{10}	—	-71	-66	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, $75\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-69	-65	dB
	10-Channel FLAT	—	-64	-61	
Composite Triple Beat ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-78	-75	dB
	10-Channel FLAT	—	-69	-66	
Noise Figure ($f = 5$ –65 MHz)	NF	—	5.8	6.5	dB
DC Current	I_{DC}	85	95	110	mA

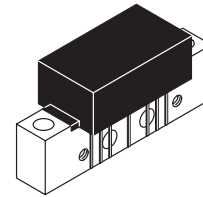
The RF Line Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1303LA

**5–200 MHz, 30.8 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	200	MHz
Power Gain (f = 5 MHz)	G_p	30	30.8	31.2	dB
Slope (5–200 MHz)	S	0	—	1.0	dB
Gain Flatness (Peak To Valley) (5–200 MHz)	—	—	—	0.7	dB
Return Loss — Input/Output (@ f = 5–65 MHz) (@ f = 65–200 MHz)	IRL/ORL	20 18	— —	— —	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO_6	—	-73	-68	
10-Channel FLAT	CSO_{10}	—	-70	-65	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, $75\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-67	-64	dB
	10-Channel FLAT	—	-61	-58	
Composite Triple Beat ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-76	-74	dB
	10-Channel FLAT	—	-67	-64	
Noise Figure ($f = 5$ –200 MHz)	NF	—	5	5.7	dB
DC Current	I_{DC}	85	95	110	mA

The RF Line

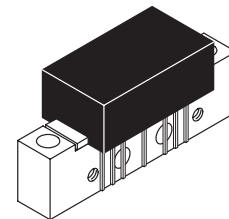
Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low distortion characteristics. Specified for use as return amplifiers for low-split 2-way cable TV systems. Features all gold metallization system.

- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- Circuit Design Optimized for Good RF Stability Under High VSWR Load Conditions
- Transformers Designed to Insure Good Low Frequency Gain Stability versus Temperature

MHW1304L

24 Vdc
50 MHz
30 dB
CATV LOW CURRENT AMPLIFIER



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{IN}	+70	dBmV
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 ohm system, unless otherwise noted)

Characteristic	Symbol	Min	Max	Unit
Bandwidth All	BW	5.0	50	MHz
Power Gain (f = 5.0 MHz)	G_p	29.2	30.8	dB
Return Loss (@ f = 5.0–50 MHz)	RL	18	—	dB
Second Order Distortion ($V_{out} = +50$ dBmV/ch)	IMD	—	-70	dBc
Cross Modulation ($V_{out} = +50$ dBmV/ch)	XMD_4	—	-57	dBc
Triple Beat Distortion ($V_{out} = +50$ dBmV/ch)	TB_3	—	-66	dBc
Noise Figure (f = 50 MHz)	NF	—	4.5	dB
DC Current	I_{DC}	100	135	mA

The RF Line

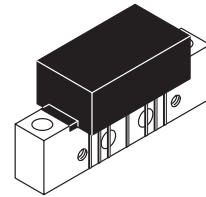
Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1304LA

**5–65 MHz, 30.8 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	- 20 to +100	°C
Storage Temperature Range	T_{stg}	- 40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	65	MHz
Power Gain (f = 5 MHz)	G_p	30	30.8	31.2	dB
Slope (5–65 MHz)	S	- 0.2	—	0.5	dB
Gain Flatness (Peak To Valley) (5–65 MHz)	—	—	—	0.5	dB
Return Loss — Input/Output (@ f = 5–65 MHz)	IRL/ORL	20	—	—	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO_6	—	- 73	- 68	
10-Channel FLAT	CSO_{10}	—	- 70	- 65	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, $75\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	XMD ₆	—	-67	-64	
10-Channel FLAT	XMD ₁₀	—	-61	-58	
Composite Triple Beat ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CTB ₆	—	-76	-74	
10-Channel FLAT	CTB ₁₀	—	-67	-64	
Noise Figure ($f = 5$ –65 MHz)	NF	—	5	5.7	dB
DC Current	I_{DC}	85	95	110	mA

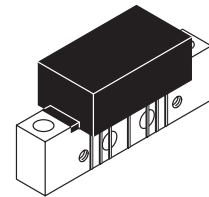
The RF Line Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1353LA

**5–150 MHz, 35.2 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	- 20 to +100	°C
Storage Temperature Range	T_{stg}	- 40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	150	MHz
Power Gain (f = 5 MHz)	G_p	34.5	35.2	35.7	dB
Slope (5–150 MHz)	S	0	—	1	dB
Gain Flatness (Peak To Valley) (5–150 MHz)	—	—	—	0.7	dB
Return Loss — Input/Output (@ f = 5–65 MHz) (@ f = 65–150 MHz)	IRL/ORL	20 18	— —	— —	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO_6	—	- 73	- 68	
10-Channel FLAT	CSO_{10}	—	- 69	- 65	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, $75\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-66	-63	dB
	10-Channel FLAT	—	-60	-57	
Composite Triple Beat ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-75	-73	dB
	10-Channel FLAT	—	-65	-62	
Noise Figure ($f = 5$ – 150 MHz)	NF	—	4.4	5.4	dB
DC Current	I_{DC}	85	95	110	mA

The RF Line

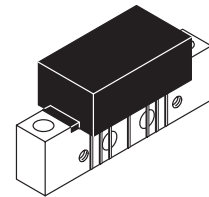
Low Distortion Wideband Reverse Amplifier Modules

Designed specifically for broadband applications requiring low multi-channel distortion characteristics. Specified for use as return amplifiers for 2-way cable TV systems.

- Designed for Low Power Consumption
- Specified for 6 and 10 Channel Performance
- Guaranteed Broadband Power Gain
- Guaranteed Broadband Noise Figure
- All Gold Metallization
- Designed to Ensure Good Gain Stability versus Temperature

MHW1354LA

**5–65 MHz, 35 dB
CATV LOW CURRENT AMPLIFIER**



CASE 1302-01, STYLE 1

MAXIMUM RATINGS

Parameter	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+60	dBmV
Operating Case Temperature Range	T_C	- 20 to +100	°C
Storage Temperature Range	T_{stg}	- 40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = 30$ °C, 75 Ω system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Bandwidth All	BW	5	—	65	MHz
Power Gain (f = 5 MHz)	G_p	34.5	35	35.7	dB
Slope (5–65 MHz)	S	- 0.2	—	0.5	dB
Gain Flatness (Peak To Valley) (5–65 MHz)	—	—	—	0.5	dB
Return Loss — Input/Output (@ f = 5–65 MHz)	IRL/ORL	20	—	—	dB
Composite Second Order ($V_{out} = +50$ dBmV per Ch., Worst Case)					dB
6-Channel FLAT	CSO ₆	—	- 73	- 68	
10-Channel FLAT	CSO ₁₀	—	- 69	- 65	

ELECTRICAL CHARACTERISTICS – continued ($V_{CC} = 24$ Vdc, $T_C = 30^\circ\text{C}$, $75\ \Omega$ system, unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-66	-63	dB
	10-Channel FLAT	—	-60	-57	
Composite Triple Beat ($V_{out} = +50$ dBmV per Ch., Worst Case)	6-Channel FLAT	—	-75	-73	dB
	10-Channel FLAT	—	-65	-62	
Noise Figure ($f = 5$ – 65 MHz)	NF	—	4.4	5.2	dB
DC Current	I_{DC}	85	95	110	mA

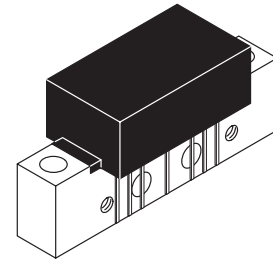
The RF Line
**77-Channel (550 MHz)
CATV Amplifier**

The MHW6342T is designed specifically for 550 MHz CATV applications. Features ion-implanted arsenic emitter transistors with 7 GHz f_T and an all gold metallization system.

- Specified for 77-Channel Performance
- Broadband Power Gain — @ $f = 40-550$ MHz
 $G_p = 34.5$ dB (Typ) @ 50 MHz
 35.2 dB (Typ) @ 550 MHz
- Broadband Noise Figure @ 550 MHz
 $NF = 5.5$ dB (Typ)
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- 7 GHz Ion-Implanted Transistors

MHW6342T

**34 dB GAIN
550 MHz
77-CHANNEL
CATV AMPLIFIER**



CASE 1302-01, STYLE 1

ABSOLUTE MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+55	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	550	MHz
Power Gain 50 MHz	G_p	33.5	34.5	35.5	dB
Power Gain 550 MHz	G_p	34.5	35.2	—	dB
Slope	S	0	0.7	2	dB
Gain Flatness (Peak To Valley)	—	—	0.3	0.8	dB
Return Loss — Input/Output ($Z_0 = 75$ Ohms)	IRL/ORL	18 16	— —	— —	dB
Second Order Intermodulation Distortion ($V_{out} = +46$ dBmV per ch., Ch 2, M13, M22) ($V_{out} = +44$ dBmV per ch., Ch 2, M30, M39)	IMD	— —	-80 -74	— —	dB
Cross Modulation Distortion ($V_{out} = +46$ dBmV per ch.) ($V_{out} = +44$ dBmV per ch.)	XMD60 XMD77	— —	-62 -63	— -57	dB

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24 \text{ Vdc}$, $T_C = +30^\circ\text{C}$, 75Ω system unless otherwise noted)

Composite Triple Beat ($V_{out} = +46 \text{ dBmV}$ per ch.) ($V_{out} = +44 \text{ dBmV}$ per ch.)	60-Channel FLAT 77-Channel FLAT	CTB ₆₀ CTB ₇₇	— —	-64 -63	— -57	dB
Composite Second Order ($V_{out} = +46 \text{ dBmV/ch}$, 60-Channel FLAT) ($V_{out} = +44 \text{ dBmV/ch}$, 77-Channel FLAT)		CSO ₆₀ CSO ₇₇	— —	-70 -65	— -57	dB
Noise Figure	550 MHz	NF	—	5.5	6.5	dB
DC Current		I_{DC}	—	310	340	mA

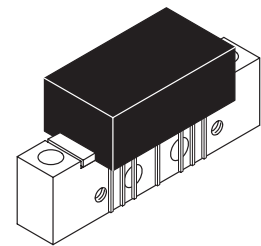
The RF Line

110-Channel 750 MHz CATV Amplifier

- Specified for 77 and 110-Channel Performance
- Broadband Power Gain — @ f = 750 MHz
G_p = 19 dB (Typ)
- Broadband Noise Figure
NF = 5.0 dB (Typ) @ 750 MHz
- All Gold Metallization
- Improved Distortion Performance

MHW7182B

**18 dB GAIN
750 MHz
110-CHANNEL
CATV AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	750	MHz
Power Gain	G _p	18	18.5	19	dB
		18.2	19	20	
Slope	S	0	0.4	1	dB
Gain Flatness (40–750 MHz, Peak to Valley)	—	—	0.3	0.6	dB
Return Loss — Input/Output (Z _O = 75 Ohms)	IRL/ORL				
@ 40 MHz		20	—	—	dB
@ f > 40 MHz (Derate)		—	—	0.005	dB/MHz
Composite Second Order					dBc
(V _{out} = +40 dBmV/ch., Worst Case)	CSO ₁₁₀	—	-70	-63	
(V _{out} = +44 dBmV/ch., Worst Case)	CSO ₇₇	—	-70	-64	
Cross Modulation Distortion @ Ch 2					dBc
(V _{out} = +40 dBmV/ch., FM = 55 MHz)	XMD ₁₁₀	—	-66	-64	
(V _{out} = +44 dBmV/ch., FM = 55 MHz)	XMD ₇₇	—	-61	-59	
Composite Triple Beat					dBc
(V _{out} = +40 dBmV/ch., Worst Case)	CTB ₁₁₀	—	-68	-66	
(V _{out} = +44 dBmV/ch., Worst Case)	CTB ₇₇	—	-66	-64	
Noise Figure	NF	—	4.0	5.0	dB
		—	4.5	—	
		—	5.0	6.5	
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	180	220	240	mA

The RF Line
High Output Power Doubler
750 MHz CATV Amplifier

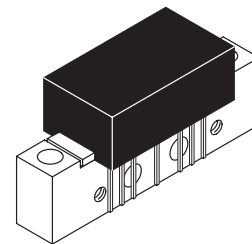
MHW7185C

- Specified for 77 and 110-Channel Performance
- Broadband Power Gain — @ $f = 40-750$ MHz
 $G_p = 19.4$ dB (Typ)
- Broadband Noise Figure
 $NF = 6.2$ dB (Typ) @ 750 MHz
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors

19.4 dB GAIN
750 MHz
110-CHANNEL
CATV AMPLIFIER

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+70	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C



CASE 714Y-03, STYLE 1

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

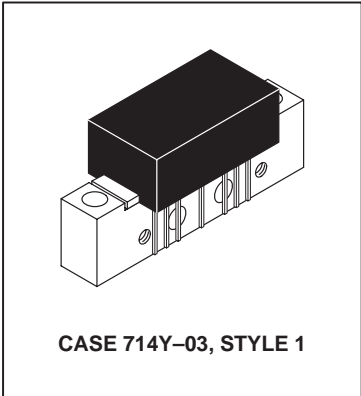
Characteristic		Symbol	Min	Typ	Max	Unit
Frequency Range		BW	40	—	750	MHz
Power Gain	50 MHz 750 MHz	G_p	18.3 19	18.8 19.4	19.3 20	dB
Slope	40-750 MHz	S	0	0.4	1.0	dB
Gain Flatness (40-750 MHz, Peak to Valley)		—	—	0.3	0.6	dB
Return Loss — Input/Output ($Z_0 = 75$ Ohms)	@ 40 MHz @ $f > 40$ MHz (Derate)	IRL/ORL	19 —	— —	— 0.006	dB dB/MHz
Composite Second Order ($V_{out} = +44$ dBmV/ch., Worst Case)	110-Channel FLAT 77-Channel FLAT	CSO_{110} CSO_{77}	— —	-72 -80	-64 -68	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +44$ dBmV/ch., FM = 55 MHz)	110-Channel FLAT 77-Channel FLAT	XMD_{110} XMD_{77}	— —	-66 -70	-63 -68	dBc
Composite Triple Beat ($V_{out} = +44$ dBmV/ch., Worst Case)	110-Channel FLAT 77-Channel FLAT	CTB_{110} CTB_{77}	— —	-64 -71	-62 -69	dBc
Noise Figure	50 MHz 550 MHz 750 MHz	NF	— — —	5.0 5.8 6.2	6.0 — 7.5	dB
DC Current ($V_{DC} = 24$ V, $T_C = 30^\circ\text{C}$)		I_{DC}	365	400	435	mA

The RF Line
High Output Power Doubler
750 MHz CATV Amplifier

MHW7185CL

- Specified for 77 and 110-Channel Performance
- Broadband Power Gain — @ f = 750 MHz
G_p = 19.2 dB (Typ)
- Broadband Noise Figure
NF = 6.5 dB (Typ) @ 750 MHz
- All Gold Metallization
- Lower DC Current Consumption
- Superior DC Current Stability with Temperature

19.2 dB GAIN
750 MHz
110-CHANNEL
CATV AMPLIFIER



MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic		Symbol	Min	Typ	Max	Unit
Frequency Range		BW	40	—	750	MHz
Power Gain	50 MHz	G _p	18	18.5	19	dB
	750 MHz		18.7	19.2	19.7	
Slope		S	0.3	0.6	1.3	dB
Gain Flatness (40–750 MHz, Peak to Valley)		—	—	0.3	0.6	dB
Return Loss — Input/Output (Z ₀ = 75 Ohms)		IRL/ORL	20	—	—	dB
@ 40 MHz						
@ f > 40 MHz (Derate)		—	—	0.007	—	dB/MHz
Composite Second Order (V _{out} = +44 dBmV/ch., Worst Case)	110-Channel FLAT	CSO ₁₁₀	—	-70	-64	dBc
	77-Channel FLAT	CSO ₇₇	—	-83	-68	
Cross Modulation Distortion @ Ch 2 (V _{out} = +44 dBmV/ch., FM = 55 MHz)	110-Channel FLAT	XMD ₁₁₀	—	-66	-63	dBc
	77-Channel FLAT	XMD ₇₇	—	-69	-67	
Composite Triple Beat (V _{out} = +44 dBmV/ch., Worst Case)	110-Channel FLAT	CTB ₁₁₀	—	-63.5	-61	dBc
	77-Channel FLAT	CTB ₇₇	—	-70	-68	
Noise Figure	50 MHz	NF	—	5.3	6.2	dB
	550 MHz		—	5.8	—	
	750 MHz		—	6.5	7.5	
DC Current (V _{DC} = 24 V, T _C = -20 to +100°C)		I _{DC}	345	370	385	mA

The RF Line
High Output Power Doubler
750 MHz CATV Amplifier

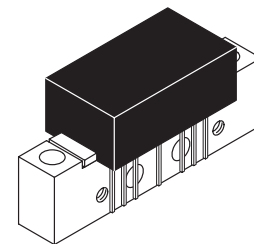
MHW7205C

- Specified for 77 and 110-Channel Performance
- Broadband Power Gain — @ $f = 40\text{--}750\text{ MHz}$
 $G_p = 20.2\text{ dB (Typ)}$
- Broadband Noise Figure
 $NF = 6.2\text{ dB (Typ) @ }750\text{ MHz}$
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors
- Composite Triple Beat — @ 110-Channel Loading
 $CTB = -63\text{ dB (Typ)}$

20.2 dB GAIN
750 MHz
110-CHANNEL
CATV AMPLIFIER

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+70	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C



CASE 714Y-03, STYLE 1

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

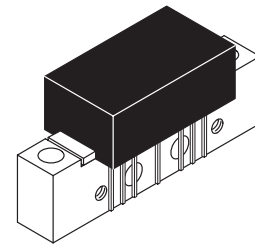
Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	750	MHz	
Power Gain	G_p	50 MHz	19.3	19.8	20.3	dB
		750 MHz	20	20.2	21	
Slope	S	0	0.4	1.0	dB	
Gain Flatness (40-750 MHz, Peak to Valley)	—	—	0.3	0.6	dB	
Return Loss — Input/Output ($Z_0 = 75\text{ Ohms}$)	IRL/ORL	@ 40 MHz	19	—	—	dB
		@ $f > 40\text{ MHz}$ (Derate)	—	—	0.006	dB/MHz
Composite Second Order ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	CSO ₁₁₀ CSO ₇₇	110-Channel FLAT	—	-70	-63	dBc
		77-Channel FLAT	—	-80	-68	
Cross Modulation Distortion @ Ch 2 ($V_{out} = +44\text{ dBmV/ch.}$, FM = 55 MHz)	XMD ₁₁₀ XMD ₇₇	110-Channel FLAT	—	-67	-62	dBc
		77-Channel FLAT	—	-70	-68	
Composite Triple Beat ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	CTB ₁₁₀ CTB ₇₇	110-Channel FLAT	—	-63	-61	dBc
		77-Channel FLAT	—	-71	-69	
Noise Figure	NF	50 MHz	—	5.0	6.0	dB
		550 MHz	—	5.8	—	
		750 MHz	—	6.2	7.5	
DC Current ($V_{DC} = 24\text{ V}$, $T_C = 30^\circ\text{C}$)	I_{DC}	365	400	435	mA	

The RF Line
High Output Power Doubler
750 MHz CATV Amplifier

MHW7205CL

20 dB GAIN
750 MHz
110-CHANNEL
CATV AMPLIFIER

- Specified for 77 and 110-Channel Performance
- Broadband Power Gain — @ f = 750 MHz
G_p = 20 dB (Typ)
- Broadband Noise Figure
NF = 6.2 dB (Typ) @ 750 MHz
- Composite Triple Beat — @ 110-Channel Loading
CTB = -63 dB (Typ)
- Lower DC Current Consumption and Superior DC Stability with Temperature



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	750	MHz	
Power Gain	G _p	50 MHz	19	19.5	20	dB
		750 MHz	19.7	20	21.2	
Slope	S	40–750 MHz	0.2	0.5	1.7	dB
Gain Flatness (40–750 MHz, Peak to Valley)	—	—	0.3	0.8	dB	
Return Loss — Input/Output (Z ₀ = 75 Ohms)	IRL/ORL	@ 40 MHz	20	—	—	dB
		@ f > 40 MHz (Derate)	—	—	0.007	dB/MHz
Composite Second Order	CSO ₁₁₀ CSO ₇₇	110-Channel FLAT	—	-69	-63	dBc
(V _{out} = +44 dBmV/ch., Worst Case)		77-Channel FLAT	—	-80	-67	
Cross Modulation Distortion @ Ch 2	XMD ₁₁₀ XMD ₇₇	110-Channel FLAT	—	-65	-62	dBc
(V _{out} = +44 dBmV/ch., FM = 55 MHz)		77-Channel FLAT	—	-69	-66	
Composite Triple Beat	CTB ₁₁₀ CTB ₇₇	110-Channel FLAT	—	-63	-61	dBc
(V _{out} = +44 dBmV/ch., Worst Case)		77-Channel FLAT	—	-70	-68	
Noise Figure	NF	50 MHz	—	5.0	6.2	dB
		550 MHz	—	5.8	—	
		750 MHz	—	6.2	7.5	
DC Current (V _{DC} = 24 V, T _C = -20 to +100°C)	I _{DC}	345	365	385	mA	

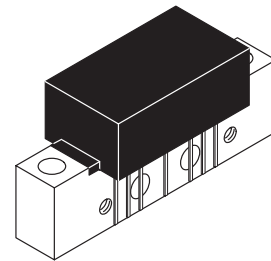
The RF Line 110-Channel (750 MHz) CATV Amplifier

The MHW7222B is designed specifically for up to 750 MHz CATV systems as amplifiers in trunk, bridge and line extender applications. This amplifier features ion-implanted, arsenic emitter transistors, an all gold metallization system and offers improved ruggedness and distortion performance.

- Specified for 110-Channel Performance
- Broadband Power Gain — @ $f = 40\text{--}750\text{ MHz}$
 $G_p = 22.7\text{ dB Typ @ }750\text{ MHz}$
- Broadband Noise Figure
 $NF = 5.0\text{ dB Typ @ }750\text{ MHz}$
- All Gold Metallization

MHW7222B

**750 MHz
22 dB GAIN
110-CHANNEL
CATV AMPLIFIER**



CASE 1302-01, STYLE 1

ABSOLUTE MAXIMUM RATINGS

Rating	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+70	dBmV
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, $75\ \Omega$ system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	750	MHz
Power Gain $f = 50\text{ MHz}$ $f = 750\text{ MHz}$	G_p	21.4 22.2	21.9 22.7	22.4 23.2	dB
Slope ($f = 40\text{--}750\text{ MHz}$)	S	0.2	0.7	1.2	—
Gain Flatness (Peak To Valley) ($f = 40\text{--}750\text{ MHz}$)	G_f	—	0.4	0.6	—
Input/Output Return Loss @ $f = 40\text{ MHz}$	IRL/ORL	20	25	—	dB
Derate Return Loss @ $f > 40\text{ MHz}$	RLD	—	—	0.006	dB/MHz
Composite Second Order ($V_{out} = +40\text{ dBmV/ch}$; 110 Channels) ($V_{out} = +44\text{ dBmV/ch}$; 77 Channels)	CSO ₁₁₀ CSO ₇₇	— —	-67 -67	-60 -60	dB

ELECTRICAL CHARACTERISTICS — continued

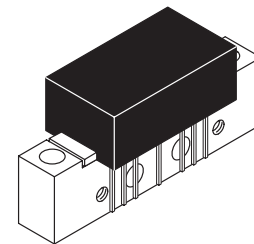
Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +40$ dBmV/ch, 110-Channel @ $F_m = 55.25$ MHz) ($V_{out} = +44$ dBmV/ch, 77-Channel @ $F_m = 55.25$ MHz)	XMD ₁₁₀ XMD ₇₇	— —	-63 -59	-60 -56	dBc
Composite Triple Beat ($V_{out} = +40$ dBmV/ch, 110-Channels, Worst Case) ($V_{out} = +44$ dBmV/ch, 77-Channels, Worst Case)	CTB ₁₁₀ CTB ₇₇	— —	-64 -65	-61 -62	dBc
Noise Figure f = 50 MHz f = 750 MHz	NF	— —	3.7 5	4.5 6.5	dB
DC Current	I_{DC}	180	220	240	mA

The RF Line
**110-Channel (750 MHz) CATV
Line Extender Amplifier**

- 24 V Supply Voltage
- Specified for 110-Channel Performance
- Typical Noise Figure
NF = 5.5 dB @ 750 MHz
- All Gold Metallization
- Improved CTB Performance over Previous Versions

MHW7272A

**27 dB GAIN
750 MHz
110-CHANNEL
CATV AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+55	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

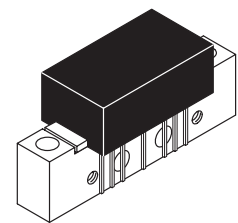
Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	750	MHz
Power Gain 50 MHz 750 MHz	G_p	26.2 27	27.2 27.7	27.8 29	dB
Slope 40–750 MHz	S	0	0.7	1.5	dB
Gain Flatness (40–750 MHz, Peak to Valley)	—	—	0.4	0.8	dB
Return Loss — Input/Output ($Z_0 = 75$ Ohms) @ 40 MHz @ $f > 40$ MHz (Derate)	IRL/ORL	20 —	— —	— 0.007	dB dB/MHz
Composite Second Order ($V_{out} = +40$ dBmV/ch., Worst Case) 110-Channel FLAT	CSO_{110}	—	-70	-64	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +40$ dBmV/ch., FM = 55 MHz) 110-Channel FLAT	XMD_{110}	—	-63	-60	dBc
Composite Triple Beat ($V_{out} = +40$ dBmV/ch., Worst Case) 110-Channel FLAT	CTB_{110}	—	-68	-64	dBc
Noise Figure 50 MHz 750 MHz	NF	— —	— 5.5	5.5 6.5	dB
DC Current ($V_{DC} = 24$ V, $T_C = 30^\circ\text{C}$)	I_{DC}	280	310	350	mA

The RF Line
**110-Channel (750 MHz) CATV
Line Extender Amplifier**

- 24 V Supply Voltage
- Specified for 110-Channel Performance
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors

MHW7292

**29 dB GAIN
750 MHz
110-CHANNEL
CATV AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+55	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

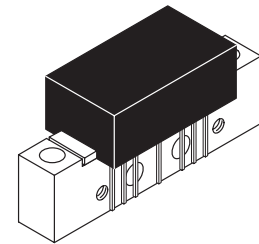
Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	750	MHz
Power Gain 50 MHz 750 MHz	G_p	28.2 29	29 29.8	29.8 31	dB
Slope 40–750 MHz	S	0	0.7	2	dB
Gain Flatness (40–750 MHz, Peak to Valley)	—	—	0.4	0.8	dB
Return Loss — Input/Output ($Z_0 = 75$ Ohms) @ 40 MHz @ $f > 40$ MHz (Derate)	IRL/ORL	20 —	— —	— 0.007	dB dB/MHz
Composite Second Order ($V_{out} = +40$ dBmV/ch., Worst Case) 110-Channel FLAT	CSO ₁₁₀	—	-70	-60	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +40$ dBmV/ch., FM = 55 MHz) 110-Channel FLAT	XMD ₁₁₀	—	-62	-60	dBc
Composite Triple Beat ($V_{out} = +40$ dBmV/ch., Worst Case) 110-Channel FLAT	CTB ₁₁₀	—	-62	-60	dBc
Noise Figure 50 MHz 750 MHz	NF	— —	— 5.5	5.5 6.5	dB
DC Current ($V_{DC} = 24$ V, $T_C = 30^\circ\text{C}$)	I_{DC}	280	310	350	mA

The RF Line
128-Channel 860 MHz
CATV Amplifier

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ f = 860 MHz
G_p = 19.1 dB (Typ)
- Broadband Noise Figure
NF = 5.5 dB (Typ) @ 860 MHz
- All Gold Metallization
- Improved CTB Distortion Performance

MHW8182B

18 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	860	MHz
Power Gain 50 MHz 860 MHz	G _p	18 18.2	18.5 19.1	19 20.5	dB
Slope 40–860 MHz	S	0	0.7	2.5	dB
Gain Flatness (40–860 MHz, Peak to Valley)	—	—	0.3	0.6	dB
Return Loss — Input/Output (Z ₀ = 75 Ohms) @ 40 MHz @ f > 40 MHz (Derate)	IRL/ORL	20 —	— —	— 0.005	dB dB/MHz
Composite Second Order (V _{out} = +38 dBmV/ch., Worst Case) (V _{out} = +40 dBmV/ch., Worst Case) (V _{out} = +44 dBmV/ch., Worst Case)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT CSO ₁₂₈ CSO ₁₁₀ CSO ₇₇	— — —	-71 -70 -70	-64 -63 -64	dBc
Cross Modulation Distortion @ Ch 2 (V _{out} = +38 dBmV/ch., FM = 55 MHz) (V _{out} = +40 dBmV/ch., FM = 55 MHz) (V _{out} = +44 dBmV/ch., FM = 55 MHz)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT XMD ₁₂₈ XMD ₁₁₀ XMD ₇₇	— — —	-68 -66 -61	-65 -64 -59	dBc
Composite Triple Beat (V _{out} = +38 dBmV/ch., Worst Case) (V _{out} = +40 dBmV/ch., Worst Case) (V _{out} = +44 dBmV/ch., Worst Case)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT CTB ₁₂₈ CTB ₁₁₀ CTB ₇₇	— — —	-69 -68 -66	-66 -66 -64	dBc
Noise Figure 50 MHz 550 MHz 750 MHz 860 MHz	NF	— — — —	4.0 4.5 5.0 5.5	5.0 — 6.5 7.5	dB
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	180	220	240	mA

The RF Line
High Output Power Doubler
860 MHz CATV Amplifier

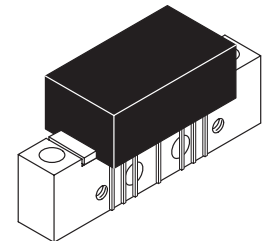
MHW8185

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ f = 40–860 MHz
G_p = 19.4 dB (Typ)
- Broadband Noise Figure
NF = 7 dB (Typ) @ 860 MHz
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors

19.4 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C



CASE 714Y-03, STYLE 1

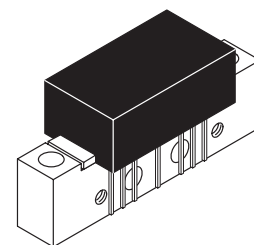
ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	860	MHz	
Power Gain	G _p	50 MHz	18.3	19.3	dB	
		860 MHz	19	20.5		
Slope	S	0	.5	1.5	dB	
Gain Flatness (40–860 MHz, Peak to Valley)	—	—	0.3	1.0	dB	
Return Loss — Input/Output (Z _O = 75 Ohms)	IRL/ORL	@ 40 MHz	19	—	dB	
		@ f > 40 MHz (Derate)	—	—		0.006
Composite Second Order	CSO ₁₂₈ CSO ₁₁₀ CSO ₇₇	(V _{out} = +40 dBmV/ch., Worst Case)	—	-70	-62	dBc
		128-Channel FLAT	—	-72	-64	
		110-Channel FLAT	—	-80	-68	
	77-Channel FLAT	—	—	—	—	
Cross Modulation Distortion @ Ch 2	XMD ₁₂₈ XMD ₁₁₀ XMD ₇₇	(V _{out} = +40 dBmV/ch., FM = 55 MHz)	—	-72	-64	dBc
		128-Channel FLAT	—	-67	-63	
		110-Channel FLAT	—	-70	-68	
	77-Channel FLAT	—	—	—	—	
Composite Triple Beat	CTB ₁₂₈ CTB ₁₁₀ CTB ₇₇	(V _{out} = +40 dBmV/ch., Worst Case)	—	-67	-64	dBc
		128-Channel FLAT	—	-64	-62	
		110-Channel FLAT	—	-71	-69	
	77-Channel FLAT	—	—	—	—	
Noise Figure	NF	50 MHz	—	5.0	6.0	dB
		550 MHz	—	5.8	—	
		750 MHz	—	6.2	—	
		860 MHz	—	7.0	8.0	
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	365	400	435	mA	

The RF Line
High Output Power Doubler
870 MHz CATV Amplifier

MHW8185L

19.4 dB GAIN
870 MHz
128-CHANNEL
CATV AMPLIFIER



CASE 714Y-03, STYLE 1

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ $f = 40\text{--}870\text{ MHz}$
 $G_p = 19.4\text{ dB (Typ)}$
- Lower DC Current Consumption
- Superior DC Current Stability with Temperature

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+70	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

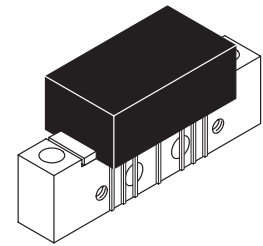
ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, $75\ \Omega$ system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	870	MHz	
Power Gain 50 MHz 870 MHz	G_p	18 19	18.5 19.4	19 20.5	dB	
Slope 40-870 MHz	S	0.4	0.9	1.4	dB	
Gain Flatness (40-870 MHz, Peak-to-Valley)	—	—	0.3	0.8	dB	
Return Loss — Input/Output ($Z_0 = 75\ \Omega$) @ 40 MHz @ $f > 40\text{ MHz}$ (Derate)	IRL/ORL	20 —	— —	— 0.007	dB dB/MHz	
Composite Second Order ($V_{out} = +40\text{ dBmV/ch.}$, Worst Case) ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case) ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	CSO_{128} CSO_{110} CSO_{77}	— — —	-69 -70 -85	-62 -64 -68	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +40\text{ dBmV/ch.}$, FM = 55 MHz) ($V_{out} = +44\text{ dBmV/ch.}$, FM = 55 MHz) ($V_{out} = +44\text{ dBmV/ch.}$, FM = 55 MHz)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	XMD_{128} XMD_{110} XMD_{77}	— — —	-72 -66 -69	-64 -63 -67	dBc
Composite Triple Beat ($V_{out} = +40\text{ dBmV/ch.}$, Worst Case) ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case) ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	CTB_{128} CTB_{110} CTB_{77}	— — —	-66 -63 -70	-63 -61 -68	dBc
Noise Figure 50 MHz 550 MHz 750 MHz 870 MHz	NF	— — — —	5.3 5.8 6.6 7.8	6.2 — — 8.5	dB	
DC Current ($V_{DC} = 24\text{ V}$, $T_C = -20\text{ to }+100^\circ\text{C}$)	I_{DC}	345	365	385	mA	

The RF Line
High Output Power Doubler
870 MHz CATV Amplifier

MHW8185LR

19.4 dB GAIN
870 MHz
128-CHANNEL
CATV AMPLIFIER



CASE 714Y-03, STYLE 2

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ $f = 40\text{--}870\text{ MHz}$
 $G_p = 19.4\text{ dB (Typ)}$
- Lower DC Current Consumption
- Superior DC Current Stability with Temperature

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+70	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, $75\ \Omega$ system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	870	MHz
Power Gain	G_p	18	18.5	19	dB
		19	19.4	20.5	
Slope	S	0.4	0.9	1.4	dB
Gain Flatness (40-870 MHz, Peak-to-Valley)	—	—	0.3	0.8	dB
Return Loss — Input/Output ($Z_0 = 75\ \Omega$)	IRL/ORL				
@ 40 MHz		20	—	—	dB
@ $f > 40\text{ MHz}$ (Derate)		—	—	0.007	dB/MHz
Composite Second Order					dBc
($V_{out} = +40\text{ dBmV/ch.}$, Worst Case)	128-Channel FLAT	CSO ₁₂₈	—	-69	-62
($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	110-Channel FLAT	CSO ₁₁₀	—	-70	-64
($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	77-Channel FLAT	CSO ₇₇	—	-85	-68
Cross Modulation Distortion @ Ch 2					dBc
($V_{out} = +40\text{ dBmV/ch.}$, FM = 55 MHz)	128-Channel FLAT	XMD ₁₂₈	—	-72	-64
($V_{out} = +44\text{ dBmV/ch.}$, FM = 55 MHz)	110-Channel FLAT	XMD ₁₁₀	—	-66	-63
($V_{out} = +44\text{ dBmV/ch.}$, FM = 55 MHz)	77-Channel FLAT	XMD ₇₇	—	-69	-67
Composite Triple Beat					dBc
($V_{out} = +40\text{ dBmV/ch.}$, Worst Case)	128-Channel FLAT	CTB ₁₂₈	—	-66	-63
($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	110-Channel FLAT	CTB ₁₁₀	—	-63	-61
($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	77-Channel FLAT	CTB ₇₇	—	-70	-68
Noise Figure	NF				dB
	50 MHz	—	5.3	6.2	
	550 MHz	—	5.8	—	
	750 MHz	—	6.6	—	
	870 MHz	—	7.8	8.5	
DC Current ($V_{DC} = 24\text{ V}$, $T_C = -20\text{ to }+100^\circ\text{C}$)	I_{DC}	345	365	385	mA

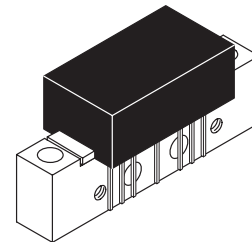
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The RF Line
High Output Mirror Power Doubler
860 MHz CATV Amplifier

MHW8185R

19.4 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER



CASE 714Y-03, STYLE 2

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ f = 860 MHz
G_p = 19.4 dB (Typ)
- Broadband Noise Figure
NF = 7 dB (Typ) @ 860 MHz
- Pin Configuration Mirrors that of MHW8185
- Typical CTB @ 860 MHz under 128-Channel FLAT Loading = -67 dBc
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	860	MHz
Power Gain	G _p	18.3 19	18.8 19.4	19.3 20.5	dB
Slope	S	0	.5	1.5	dB
Gain Flatness (40–860 MHz, Peak to Valley)	—	—	0.3	1.0	dB
Return Loss — Input/Output (Z _O = 75 Ohms)	IRL/ORL	—	—	—	dB
@ 40 MHz		19	—	—	dB
@ f > 40 MHz (Derate)		—	—	0.006	dB/MHz
Composite Second Order					dBc
(V _{out} = +40 dBmV/ch., Worst Case)	CSO ₁₂₈	—	-70	-62	
(V _{out} = +44 dBmV/ch., Worst Case)	CSO ₁₁₀	—	-72	-64	
	CSO ₇₇	—	-80	-68	
Cross Modulation Distortion @ Ch 2					dBc
(V _{out} = +40 dBmV/ch., FM = 55 MHz)	XMD ₁₂₈	—	-72	-64	
(V _{out} = +44 dBmV/ch., FM = 55 MHz)	XMD ₁₁₀	—	-67	-63	
	XMD ₇₇	—	-70	-68	
Composite Triple Beat					dBc
(V _{out} = +40 dBmV/ch., Worst Case)	CTB ₁₂₈	—	-67	-64	
(V _{out} = +44 dBmV/ch., Worst Case)	CTB ₁₁₀	—	-64	-62	
	CTB ₇₇	—	-71	-69	
Noise Figure	NF	—	5.0 5.8 6.2 7.0	6.0 — — 8.0	dB
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	365	400	435	mA

NOT RECOMMENDED FOR NEW DESIGN

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The RF Line
High Output Power Doubler
860 MHz CATV Amplifier

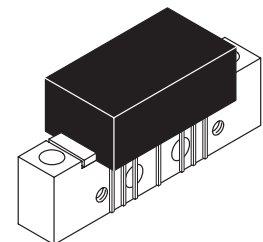
MHW8205

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ f = 40–860 MHz
G_p = 20.2 dB (Typ)
- Broadband Noise Figure
NF = 7 dB (Typ) @ 860 MHz
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors
- Composite Triple Beat — @ 128-Channel Loading
CTB = -66 dB (Typ)

20.2 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C



CASE 714Y-03, STYLE 1

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	860	MHz	
Power Gain	G _p	50 MHz	19.3	19.8	20.3	dB
		860 MHz	20	20.2	21.5	
Slope	S	0	.4	1.5	dB	
Gain Flatness (40–860 MHz, Peak to Valley)	—	—	0.3	1.0	dB	
Return Loss — Input/Output (Z _O = 75 Ohms)	IRL/ORL	@ 40 MHz	19	—	—	dB
		@ f > 40 MHz (Derate)	—	—	0.006	dB/MHz
Composite Second Order	CSO ₁₂₈ CSO ₁₁₀ CSO ₇₇	(V _{out} = +40 dBmV/ch., Worst Case)	—	-69	-60	dBc
		128-Channel FLAT	—	-70	-63	
		110-Channel FLAT	—	-80	-68	
	77-Channel FLAT	—	—	—	—	
Cross Modulation Distortion @ Ch 2	XMD ₁₂₈ XMD ₁₁₀ XMD ₇₇	(V _{out} = +40 dBmV/ch., FM = 55 MHz)	—	-72	-64	dBc
		128-Channel FLAT	—	-67	-62	
		110-Channel FLAT	—	-71	-68	
	77-Channel FLAT	—	—	—	—	
Composite Triple Beat	CTB ₁₂₈ CTB ₁₁₀ CTB ₇₇	(V _{out} = +40 dBmV/ch., Worst Case)	—	-66	-63	dBc
		128-Channel FLAT	—	-63	-61	
		110-Channel FLAT	—	-71	-69	
	77-Channel FLAT	—	—	—	—	
Noise Figure	NF	50 MHz	—	5.0	6.0	dB
		550 MHz	—	5.8	—	
		750 MHz	—	6.2	—	
		860 MHz	—	7.0	8.0	
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	365	400	435	mA	

The RF Line
High Output Power Doubler
870 MHz CATV Amplifier

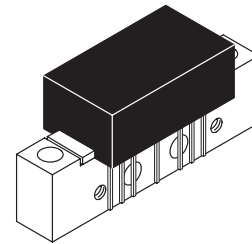
MHW8205L

20.4 dB GAIN
870 MHz
128-CHANNEL
CATV AMPLIFIER

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ $f = 870$ MHz
 $G_p = 20.4$ dB (Typ)
- Broadband Noise Figure
 $NF = 7.7$ dB (Typ) @ 870 MHz
- 7 GHz f_T Ion-Implanted Transistors
- Composite Triple Beat — @ 128-Channel Loading
 $CTB = -66$ dB (Typ)
- Lower DC Current Consumption and Superior DC Stability with Temperature

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+70	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C



CASE 714Y-03, STYLE 1

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

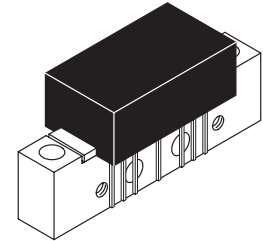
Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	870	MHz	
Power Gain 50 MHz 870 MHz	G_p	19 19.8	19.5 20.4	20 21.3	dB	
Slope 40–870 MHz	S	0.2	0.8	1.7	dB	
Gain Flatness (40–870 MHz, Peak to Valley)	—	—	0.5	1.0	dB	
Return Loss — Input/Output ($Z_0 = 75$ Ohms) @ 40 MHz @ $f > 40$ MHz (Derate)	IRL/ORL	20 —	— —	— 0.007	dB dB/MHz	
Composite Second Order ($V_{out} = +40$ dBmV/ch., Worst Case) ($V_{out} = +44$ dBmV/ch., Worst Case)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	CSO ₁₂₈ CSO ₁₁₀ CSO ₇₇	— — —	-69 -70 -80	-60 -63 -67	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +40$ dBmV/ch., FM = 55 MHz) ($V_{out} = +44$ dBmV/ch., FM = 55 MHz)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	XMD ₁₂₈ XMD ₁₁₀ XMD ₇₇	— — —	-72 -65 -69	-64 -62 -66	dBc
Composite Triple Beat ($V_{out} = +40$ dBmV/ch., Worst Case) ($V_{out} = +44$ dBmV/ch., Worst Case)	128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	CTB ₁₂₈ CTB ₁₁₀ CTB ₇₇	— — —	-66 -63 -70	-63 -61 -68	dBc
Noise Figure 50 MHz 550 MHz 750 MHz 870 MHz	NF	— — — —	5.0 5.8 6.2 7.7	6.2 — — 8.5	dB	
DC Current ($V_{DC} = 24$ V, $T_C = -20^\circ\text{C}$ to $+100^\circ\text{C}$)	I_{DC}	345	365	385	mA	

The RF Line
High Output Mirror Power Doubler
860 MHz CATV Amplifier

MHW8205R

- Specified for 77, 110 and 128-Channel Performance
- Broadband Power Gain — @ f = 40–860 MHz
G_p = 20.2 dB (Typ)
- Broadband Noise Figure
NF = 7 dB (Typ) @ 860 MHz
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors
- Composite Triple Beat — @ 128-Channel Loading
CTB = -66 dB (Typ)

20.2 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER



CASE 714Y-03, STYLE 2

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	860	MHz	
Power Gain	G _p	50 MHz	19.3	19.8	20.3	dB
		860 MHz	20	20.2	21.5	
Slope	S	0	.4	1.5	dB	
Gain Flatness (40–860 MHz, Peak to Valley)	—	—	0.3	1.0	dB	
Return Loss — Input/Output (Z _O = 75 Ohms)	IRL/ORL	@ 40 MHz	19	—	—	dB
		@ f > 40 MHz (Derate)	—	—	0.006	dB/MHz
Composite Second Order	CSO ₁₂₈ CSO ₁₁₀ CSO ₇₇	(V _{out} = +40 dBmV/ch., Worst Case)	—	-69	-60	dBc
		128-Channel FLAT	—	-70	-63	
		110-Channel FLAT	—	-80	-68	
	77-Channel FLAT	—	—	—	—	
Cross Modulation Distortion @ Ch 2	XMD ₁₂₈ XMD ₁₁₀ XMD ₇₇	(V _{out} = +40 dBmV/ch., FM = 55 MHz)	—	-72	-64	dBc
		128-Channel FLAT	—	-67	-62	
		110-Channel FLAT	—	-71	-68	
	77-Channel FLAT	—	—	—	—	
Composite Triple Beat	CTB ₁₂₈ CTB ₁₁₀ CTB ₇₇	(V _{out} = +40 dBmV/ch., Worst Case)	—	-66	-63	dBc
		128-Channel FLAT	—	-63	-61	
		110-Channel FLAT	—	-71	-69	
	77-Channel FLAT	—	—	—	—	
Noise Figure	NF	50 MHz	—	5.0	6.0	dB
		550 MHz	—	5.8	—	
		750 MHz	—	6.2	—	
		860 MHz	—	7.0	8.0	
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	365	400	435	mA	

NOT RECOMMENDED FOR NEW DESIGN

NOT RECOMMENDED FOR NEW DESIGN

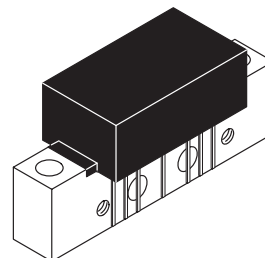
The RF Line 128-Channel (860 MHz) CATV Amplifier

The MHW8222B is designed specifically for up to 860 MHz CATV systems as amplifiers in trunk, bridge and line extender applications. This amplifier features ion-implanted, arsenic emitter transistors, an all gold metallization system and offers improved ruggedness and distortion performance.

- Specified for 77, 110, 128-Channel Performance
- Broadband Power Gain — @ $f = 40\text{--}860\text{ MHz}$
 $G_p = 22.7\text{ dB Typ @ } 860\text{ MHz}$
- Broadband Noise Figure
 $NF = 5.6\text{ dB Typ @ } 860\text{ MHz}$
- All Gold Metallization
- Improved Distortion Performance

MHW8222B

**860 MHz
22 dB GAIN
128-CHANNEL
CATV AMPLIFIER**



CASE 1302-01, STYLE 1

ABSOLUTE MAXIMUM RATINGS

Rating	Symbol	Value	Unit
DC Supply Voltage	V_{CC}	+28	Vdc
RF Input Voltage (Single Tone)	V_{in}	+70	dBmV
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, $75\ \Omega$ system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	860	MHz
Power Gain $f = 50\text{ MHz}$ $f = 860\text{ MHz}$	G_p	21.4 21.8	21.9 22.7	22.4 24	dB
Slope ($f = 40\text{--}860\text{ MHz}$)	S	0.1	0.8	1.5	—
Gain Flatness (Peak To Valley) $(f = 40\text{--}860\text{ MHz})$	G_f	—	0.4	0.6	—
Input/Output Return Loss @ $f = 40\text{ MHz}$	IRL/ORL	20	24	—	dB
Derate Return Loss @ $f > 40\text{ MHz}$	RLD	—	—	0.009	dB/MHz
Composite Second Order ($V_{out} = +38\text{ dBmV/ch}$; 128 Channels) ($V_{out} = +40\text{ dBmV/ch}$; 110 Channels) ($V_{out} = +44\text{ dBmV/ch}$; 77 Channels)	CSO ₁₂₈ CSO ₁₁₀ CSO ₇₇	— — —	-68 -64 -65	-60 -61 -62	dB

ELECTRICAL CHARACTERISTICS — continued

Characteristic	Symbol	Min	Typ	Max	Unit
Cross Modulation Distortion ($V_{out} = +38$ dBmV/ch, 128-Channel @ $F_m = 55.25$ MHz) ($V_{out} = +40$ dBmV/ch, 110-Channel @ $F_m = 55.25$ MHz) ($V_{out} = +44$ dBmV/ch, 77-Channel @ $F_m = 55.25$ MHz)	XMD ₁₂₈ XMD ₁₁₀ XMD ₇₇	— — —	-65 -63 -59	-63 -60 -56	dBc
Composite Triple Beat ($V_{out} = +38$ dBmV/ch, 128-Channels, Worst Case) ($V_{out} = +40$ dBmV/ch, 110-Channels, Worst Case) ($V_{out} = +44$ dBmV/ch, 77-Channels, Worst Case)	CTB ₁₂₈ CTB ₁₁₀ CTB ₇₇	— — —	-66 -64 -65	-64 -61 -62	dBc
Noise Figure f = 50 MHz f = 750 MHz f = 860 MHz	NF	— — —	3.7 5 5.6	4.5 6.5 7	dB
DC Current	I_{DC}	180	220	240	mA

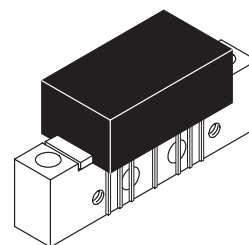
The RF Line

128-Channel (860 MHz) CATV Line Extender Amplifier

MHW8242A

- Specified for 128-Channel Performance
- Broadband Power Gain — @ $f = 40\text{--}860\text{ MHz}$
 $G_p = 24\text{ dB (Typ)}$
- Broadband Noise Figure
 $NF = 7.5\text{ dB (Max) @ } 860\text{ MHz}$
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors
- Improved CTB Performance

**24 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+55	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

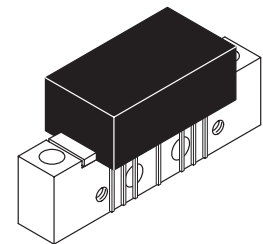
Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	860	MHz
Power Gain	G_p	23.2 24	24 25	24.8 26	dB
Slope	S	0	0.8	1.8	dB
Gain Flatness (40–860 MHz, Peak To Valley)	—	—	0.4	0.8	dB
Return Loss — Input/Output ($Z_0 = 75\text{ Ohms}$)	IRL/ORL	20 —	— —	— 0.007	dB dB/MHz
Composite Second Order ($V_{out} = +38\text{ dBmV/ch.}$, Worst Case) ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	CSO ₁₂₈ CSO ₇₇	— —	-69 -78	-62 —	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +38\text{ dBmV/ch.}$, FM = 55 MHz) ($V_{out} = +44\text{ dBmV/ch.}$, FM = 55 MHz)	XMD ₁₂₈ XMD ₇₇	— —	-65 -58	-62 —	dBc
Composite Triple Beat ($V_{out} = +38\text{ dBmV/ch.}$, Worst Case) ($V_{out} = +44\text{ dBmV/ch.}$, Worst Case)	CTB ₁₂₈ CTB ₇₇	— —	-68 -64	-64 —	dBc
Noise Figure	NF	— —	4.8 5.8	5.5 7.5	dB
DC Current	I_{DC}	280	318	350	mA

The RF Line 128-Channel (860 MHz) CATV Line Extender Amplifier

- Specified for 128-Channel Performance
- Broadband Power Gain — @ $f = 50$ MHz
 $G_p = 27.2$ dB (Typ)
- Broadband Noise Figure
NF = 6 dB (Typ) @ 860 MHz
- All Gold Metallization
- Improved CTB Performance over Previous Version

MHW8272A

**27 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+55	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24$ Vdc, $T_C = +30^\circ\text{C}$, 75 Ω system unless otherwise noted)

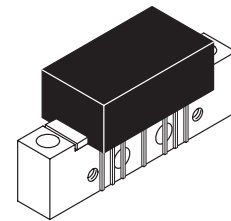
Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	860	MHz
Power Gain	G_p	26.2	27.2	27.8	dB
50 MHz		27	27.7	29.5	
Slope	S	0	0.6	2	dB
Gain Flatness (40–860 MHz, Peak to Valley)	—	—	0.4	0.8	dB
Return Loss — Input/Output ($Z_0 = 75$ Ohms)	IRL/ORL	20	—	—	dB
@ 40 MHz		—	—	0.007	
Composite Second Order ($V_{out} = +38$ dBmV/ch., Worst Case)	CSO ₁₂₈	—	-69	-64	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +38$ dBmV/ch., FM = 55 MHz)	XMD ₁₂₈	—	-65	-62	dBc
Composite Triple Beat ($V_{out} = +38$ dBmV/ch., Worst Case)	CTB ₁₂₈	—	-69	-64	dBc
Noise Figure	NF	—	—	5.5	dB
50 MHz		—	6.0	7.0	
DC Current ($V_{DC} = 24$ V, $T_C = 30^\circ\text{C}$)	I_{DC}	280	310	350	mA

The RF Line
**128-Channel (860 MHz) CATV
Line Extender Amplifier**

- Specified for 128-Channel Performance
- Broadband Power Gain — @ f = 40–860 MHz
G_p = 29 dB (Typ)
- Broadband Noise Figure
NF = 6 dB (Typ) @ 860 MHz
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- 7 GHz f_T Ion-Implanted Transistors

MHW8292

**29 dB GAIN
860 MHz
128-CHANNEL
CATV AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+55	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
Frequency Range	BW	40	—	860	MHz
Power Gain	G _p	28.2 29	29 —	29.8 31.5	dB
Slope	S	0	1.0	2.5	dB
Gain Flatness (40–860 MHz, Peak to Valley)	—	—	0.4	0.8	dB
Return Loss — Input/Output (Z ₀ = 75 Ohms) @ 40 MHz @ f > 40 MHz (Derate)	IRL/ORL	20 —	— —	— 0.007	dB dB/MHz
Composite Second Order (V _{out} = +38 dBmV/ch., Worst Case)	CSO ₁₂₈	—	—	-56	dBc
Cross Modulation Distortion @ Ch 2 (V _{out} = +38 dBmV/ch., FM = 55 MHz)	XMD ₁₂₈	—	—	-60	dBc
Composite Triple Beat (V _{out} = +38 dBmV/ch., Worst Case)	CTB ₁₂₈	—	—	-60	dBc
Noise Figure	NF	— —	— 6.0	5.5 7.0	dB
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	280	310	350	mA

NOT RECOMMENDED FOR NEW DESIGN

NOT RECOMMENDED FOR NEW DESIGN

The RF Line
**152-Channel 1000 MHz
CATV Amplifier**

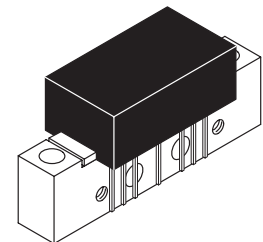
MHW9182B

- Specified for 152-Channel Performance
- Broadband Power Gain — @ f = 1000 MHz
G_p = 19.4 dB (Typ)
- Broadband Noise Figure
NF = 6 dB (Typ) @ 1000 MHz
- All Gold Metallization
- Improved Ruggedness and Composite Second Order Distortion Performance

**19.4 dB GAIN
1000 MHz
152-CHANNEL
CATV AMPLIFIER**

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V _{in}	+70	dBmV
DC Supply Voltage	V _{CC}	+28	Vdc
Operating Case Temperature Range	T _C	-20 to +100	°C
Storage Temperature Range	T _{stg}	-40 to +100	°C



CASE 714Y-03, STYLE 1

ELECTRICAL CHARACTERISTICS (V_{CC} = 24 Vdc, T_C = +30°C, 75 Ω system unless otherwise noted)

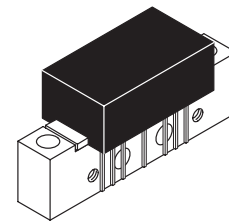
Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	1000	MHz	
Power Gain	G _p	18	18.5	19	dB	
50 MHz		18.7	19.4	20.7		
Slope	S	0.4	0.9	1.4	dB	
Gain Flatness (40–1000 MHz, Peak to Valley)	—	—	0.4	0.8	dB	
Return Loss — Input/Output (Z ₀ = 75 Ohms)	IRL/ORL	20	—	—	dB	
@ 40 MHz		—	—	0.006		dB/MHz
Composite Second Order	CSO ₁₁₀ CSO ₁₅₂	—	70	-63	dBc	
(V _{out} = +40 dBmV/ch., Worst Case)		110-Channel FLAT	—	-69		-63
(V _{out} = +38 dBmV/ch., Worst Case)	152-Channel FLAT	—	—	—	—	
Cross Modulation Distortion @ Ch 2	XMD ₁₁₀ XMD ₁₅₂	—	-66	-64	dBc	
(V _{out} = +40 dBmV/ch., FM = 55 MHz)		110-Channel FLAT	—	-65		-61
(V _{out} = +38 dBmV/ch., FM = 55 MHz)	152-Channel FLAT	—	—	—	—	
Composite Triple Beat	CTB ₁₁₀ CTB ₁₅₂	—	-68	-66	dBc	
(V _{out} = +40 dBmV/ch., Worst Case)		110-Channel FLAT	—	-64		-61
(V _{out} = +38 dBmV/ch., Worst Case)	152-Channel FLAT	—	—	—	—	
Noise Figure	NF	50 MHz	—	4.0	5.0	dB
		550 MHz	—	4.5	—	
		860 MHz	—	5.5	—	
		1000 MHz	—	6.0	7.5	
DC Current (V _{DC} = 24 V, T _C = 30°C)	I _{DC}	180	210	240	mA	

The RF Line
**152-Channel (1000 MHz) CATV
Line Extender Amplifier**

- Specified for 152-Channel Performance
- Broadband Power Gain — @ $f = 40\text{--}1000\text{ MHz}$
 $G_p = 24\text{ dB}$
- Broadband Noise Figure
 $NF = 8\text{ dB (Max) @ } 1000\text{ MHz}$
- Superior Gain, Return Loss and DC Current Stability with Temperature
- All Gold Metallization
- $7\text{ GHz } f_T$ Ion-Implanted Transistors

MHW9242A

**24 dB GAIN
1000 MHz
152-CHANNEL
CATV AMPLIFIER**



CASE 714Y-03, STYLE 1

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
RF Voltage Input (Single Tone)	V_{in}	+55	dBmV
DC Supply Voltage	V_{CC}	+28	Vdc
Operating Case Temperature Range	T_C	-20 to +100	°C
Storage Temperature Range	T_{stg}	-40 to +100	°C

ELECTRICAL CHARACTERISTICS ($V_{CC} = 24\text{ Vdc}$, $T_C = +30^\circ\text{C}$, $75\ \Omega$ system unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit	
Frequency Range	BW	40	—	1000	MHz	
Power Gain 50 MHz 1000 MHz	G_p	23.2 24	— —	24.8 26	dB	
Slope 40–1000 MHz	S	0	—	2.5	dB	
Gain Flatness (40–1000 MHz, Peak-to-Valley)	—	—	—	1.0	dB	
Return Loss — Input/Output ($Z_0 = 75\ \Omega$) @ 40 MHz @ $f > 40\text{ MHz}$ (Derate)	IRL/ORL	20 —	— —	— 0.01	dB dB/MHz	
Composite Second Order ($V_{out} = +38\text{ dBmV/ch}$; Worst Case) ($V_{out} = +38\text{ dBmV/ch}$; Worst Case) ($V_{out} = +40\text{ dBmV/ch}$; Worst Case) ($V_{out} = +44\text{ dBmV/ch}$; Worst Case)	152-Channel FLAT 128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	CSO ₁₅₂ CSO ₁₂₈ CSO ₁₁₀ CSO ₇₇	— — — —	-66 -69 -69 -78	-61 — — —	dBc
Cross Modulation Distortion @ Ch 2 ($V_{out} = +38\text{ dBmV/ch}$, FM = 55 MHz) ($V_{out} = +38\text{ dBmV/ch}$, FM = 55.25 MHz) ($V_{out} = +40\text{ dBmV/ch}$, FM = 55.25 MHz) ($V_{out} = +44\text{ dBmV/ch}$, FM = 55.25 MHz)	152-Channel FLAT 128-Channel FLAT 110-Channel FLAT 77-Channel FLAT	XMD ₁₅₂ XMD ₁₂₈ XMD ₁₁₀ XMD ₇₇	— — — —	-62 -65 -63 -58	-59 — — —	dBc

ELECTRICAL CHARACTERISTICS — continued

Characteristic	Symbol	Min	Typ	Max	Unit
Composite Triple Beat					dBc
($V_{out} = +38$ dBmV/ch., Worst Case) 152-Channel FLAT	CTB ₁₅₂	—	-64	-58	
($V_{out} = +38$ dBmV/ch, Worst Case) 128-Channel FLAT	CTB ₁₂₈	—	-68	—	
($V_{out} = +40$ dBmV/ch, Worst Case) 110-Channel FLAT	CTB ₁₁₀	—	-67	—	
($V_{out} = +44$ dBmV/ch, Worst Case) 77-Channel FLAT	CTB ₇₇	—	-64	—	
Noise Figure					dB
f = 50 MHz	NF	—	4.8	5.5	
f = 750 MHz		—	5.5	7.0	
f = 860 MHz		—	5.8	7.5	
f = 1000 MHz		—	—	8.0	
DC Current	I_{DC}	280	318	350	mA

Chapter Eight

Tape and Reel Specifications

Motorola offers the convenience of Tape and Reel packaging for our growing family of standard integrated circuit products. Reels are available to support the requirements of both first and second generation pick-and-place equipment. The packaging fully conforms to the latest EIA-481A specification. The antistatic embossed tape provides a secure cavity, sealed with a peel-back cover tape.

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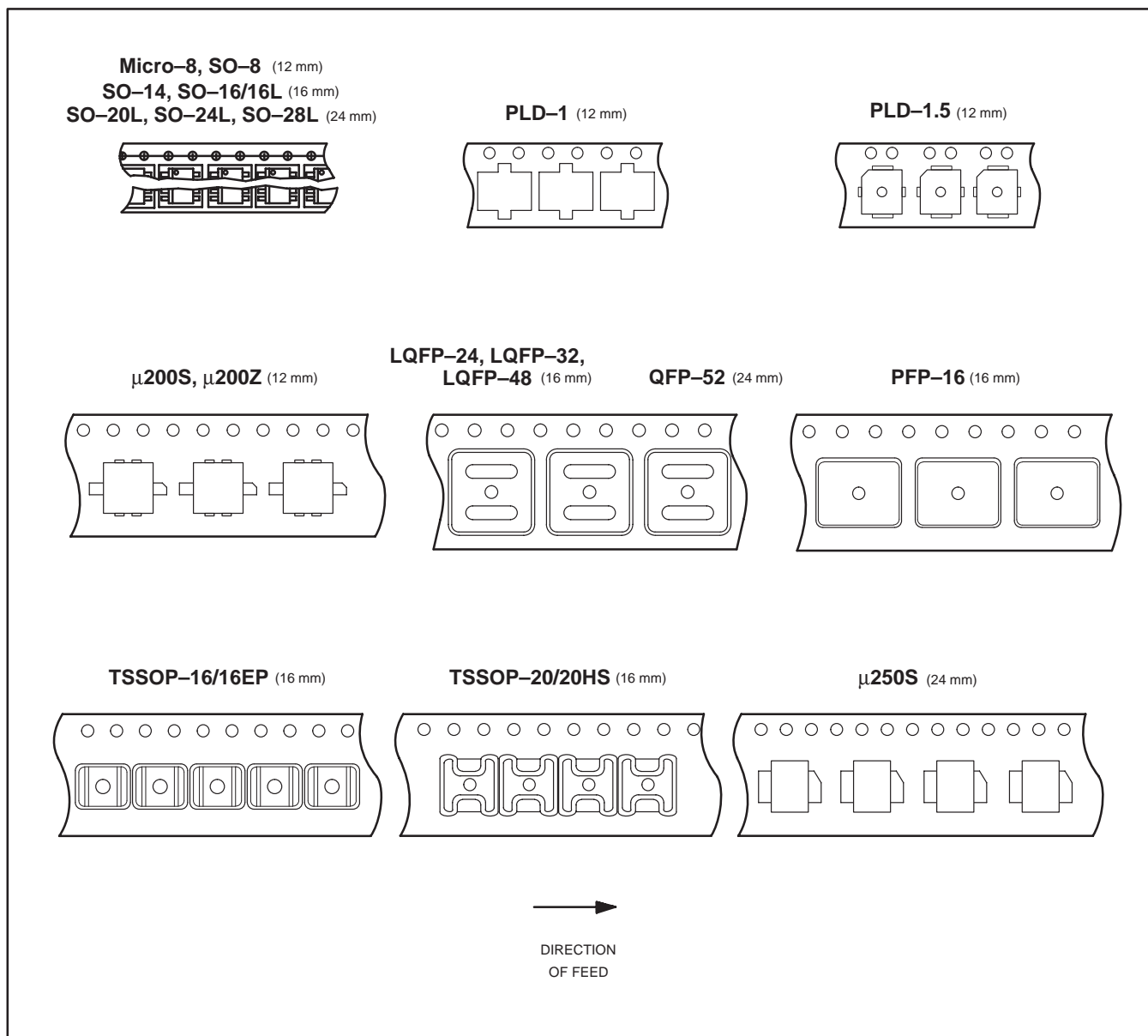
	Page
Tape and Reel Specifications	8.1-2
Embossed Tape and Reel Ordering Information . .	8.1-4
Embossed Tape and Reel Data for Discretes	8.1-5

RF and IF Tape and Reel Specifications

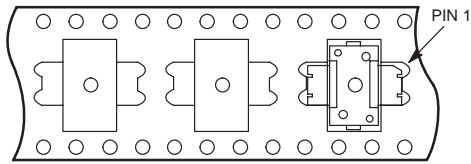
Embossed Tape and Reel is used to facilitate automatic pick and place equipment feed requirements. The tape is used as the shipping container for various products and requires a minimum of handling. The antistatic/conductive tape provides a secure cavity for the product when sealed with the "peel-back" cover tape.

- Two Reel Sizes Available (7" and 13")
- Used for Automatic Pick and Place Feed Systems
- Minimizes Product Handling
- EIA 481, -1, -2
- BCC32EP++, Micro-8, PLD-1, PLD-1.5, SO-8, μ 200S, μ 200Z in 12 mm Tape
- SO-14, SO-16/16L, LQFP24, LQFP-32, LQFP-48, TSSOP-16/16EP, TSSOP-20/20HS in 16 mm Tape
- QFP-52, SO-20L, SO-24L, SO-28L, TO-270, μ 250S in 24 mm Tape
- NI-600 in 32 mm Tape
- TO-272 in 44 mm Tape

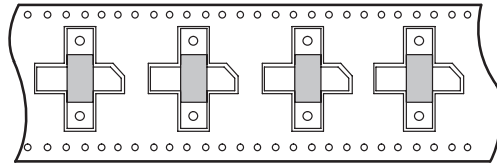
Use the standard device title and add the required suffix as listed in the option table on the following page. Note that the individual reels have a finite number of devices depending on the type of product contained in the tape. Also note the minimum lot size is one full reel for each line item, and orders are required to be in increments of the single reel quantity.



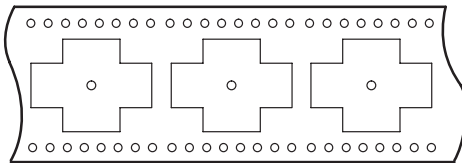
TO-270 (24 mm)



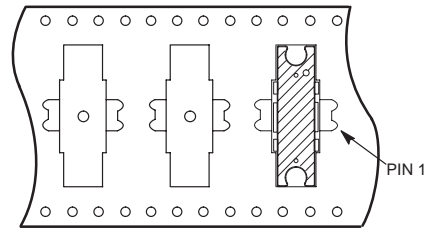
μ250 (32 mm)



NI-600 (32 mm)



TO-272 (44 mm)



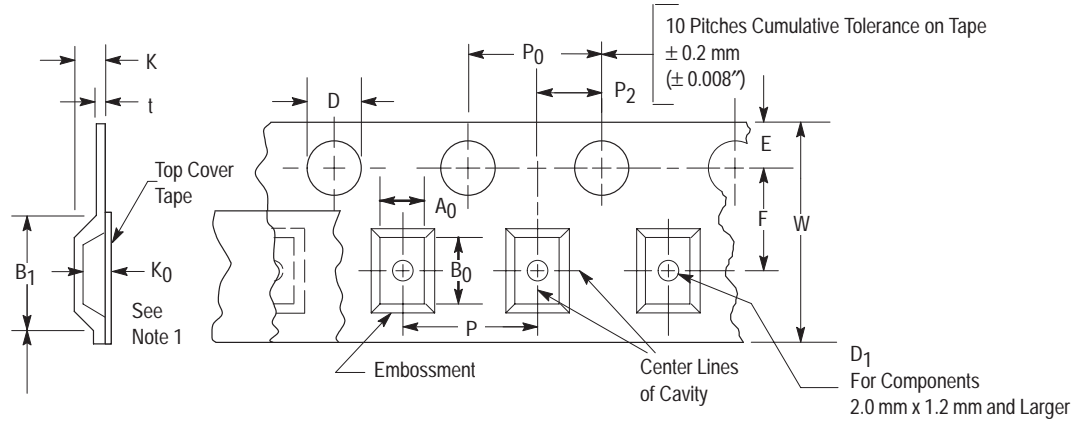
DIRECTION
OF FEED

RF and IF EMBOSSED TAPE AND REEL ORDERING INFORMATION

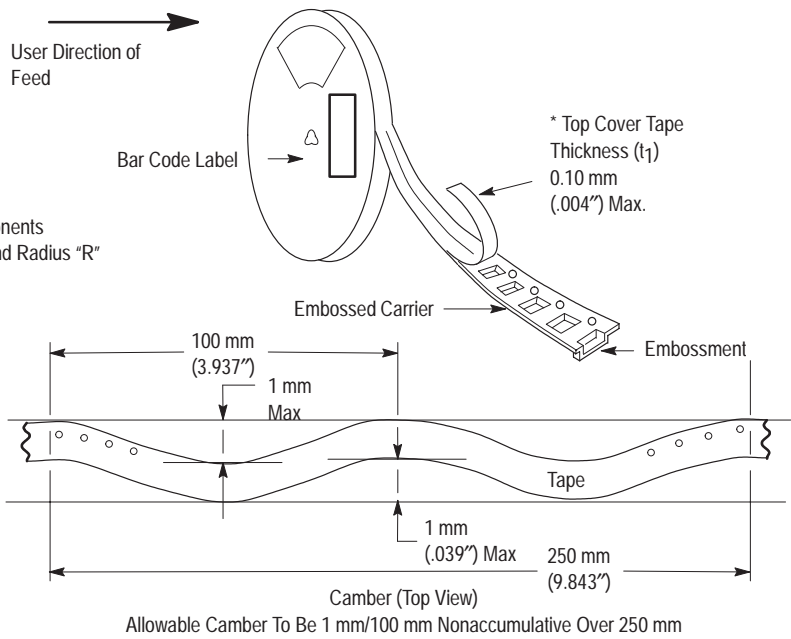
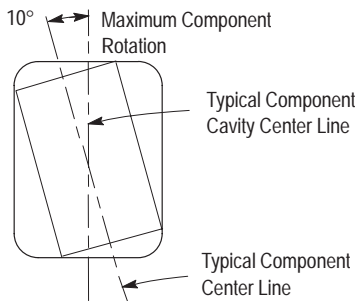
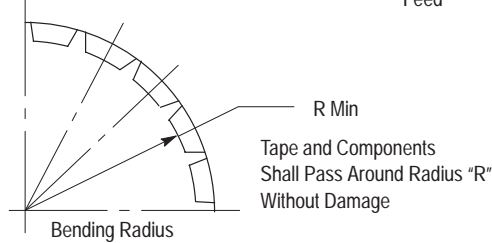
Package	Tape Width (mm)	Pitch mm (inch)	Reel Size mm (inch)	Devices Per Reel and Minimum Order Quantity	Device Suffix
BCC32EP++	12	8.0 ± 0.1 (.315 ± .004)	330 (13)	2,500	R2
Micro-8	12	8.0 ± 0.1 (.315 ± .003)	330 (13)	2,500	R2
PLD-1	12	8.0 ± 0.1 (.315 ± .004)	178 (7)	1,000	T1
PLD-1.5	12	8.0 ± 0.1 (.315 ± .004)	178 (7)	1,000	T1
PFP-16	16	12.0 ± 0.1 (.472 ± .004)	330 (13)	1,500	R2
LQFP-24	16	12.0 ± 0.1 (.472 ± .004)	330 (13)	2,000	R2
LQFP-32	16	12.0 ± 0.1 (.472 ± .004)	330 (13)	1,800	R2
LQFP-48	16	12.0 ± 0.1 (.472 ± .004)	330 (13)	2,000	R2
QFP-52	24	24.0 ± 0.1 (.945 ± .004)	330 (13)	1,500	R2
SO-8	12	8.0 ± 0.1 (.315 ± .004)	330 (13)	2,500	R2
SO-14	16	8.0 ± 0.1 (.315 ± .004)	330 (13)	2,500	R2
SO-16/16L	16	8.0 ± 0.1 (.315 ± .004)	330 (13)	2,500	R2
SO-20L	24	12.0 ± 0.1 (.472 ± .004)	330 (13)	1,000	R2
SO-24L	24	12.0 ± 0.1 (.472 ± .004)	330 (13)	1,000	R2
SO-28L	24	12.0 ± 0.1 (.472 ± .004)	330 (13)	1,000	R2
TSSOP-16/16EP	16	8.0 ± 0.1 (.315 ± .004)	330 (13)	2,500	R2
TSSOP-20/20HS	16	8.0 ± 0.1 (.315 ± .004)	330 (13)	2,500	R2
μ200S (458B)	12	12.0 ± 0.1 (.471 ± .004)	178 (7)	500	R1
μ200Z (458C)	12	12.0 ± 0.1 (.471 ± .004)	178 (7)	500	R1
μ250S (360C)	24	16.0 ± 0.1 (.631 ± .004)	330 (13)	500	R1
μ250 (360B)	32	24.0 ± 0.1 (.945 ± .004)	330 (13)	500	R1
NI-600 (465D)	32	32.0 ± 0.1 (1.26 ± .004)	330 (13)	250	R3
TO-270	24	16.0 ± 0.1 (.631 ± .004)	330 (13)	500	R1
TO-272	44	16.0 ± 0.1 (.631 ± .004)	330 (13)	500	T1

EMBOSSED TAPE AND REEL DATA FOR DISCRETES

CARRIER TAPE SPECIFICATIONS



For Machine Reference Only
Including Draft and RADII
Concentric Around B_0



DIMENSIONS

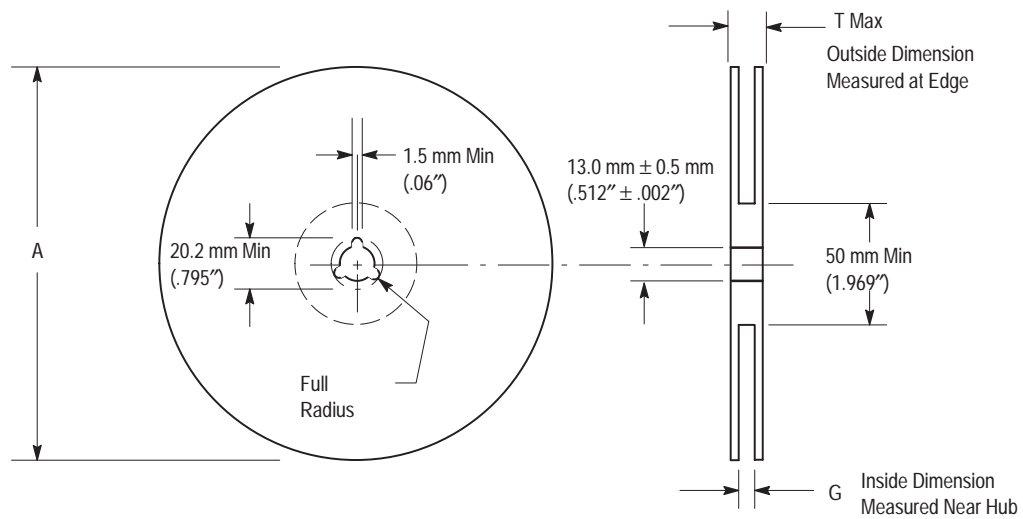
Tape Size	B_1 Max	D	D_1	E_1	F	K	P_0	P_2	R Min	T Max	W Max
12 mm	8.2 mm (.323")	1.5 + 0.1 mm - 0.0 (.059 + .004" - 0.0)	1.5 mm Min (.060")	1.75 ± 0.1 mm (.069 ± .004")	5.5 ± 0.05 mm (.217 ± .002")	6.4 mm Max (.252")	4.0 ± 0.1 mm (.157 ± .004")	2.0 ± 0.1 mm (.079 ± .002")	30 mm (1.18")	0.6 mm (.024")	12 ± .30 mm (.470 ± .012")
16 mm	12.1 mm (.476")				7.5 ± 0.10 mm (.295 ± .004")	7.9 mm Max (.311")					16.3 mm (.642")
24 mm	20.1 mm (.791")				11.5 ± 0.1 mm (.453 ± .004")	11.9 mm Max (.468")					24.3 mm (.957")
32 mm	23.0 mm (.906")	1.5 mm Min (.059")	1.5 mm Min (.059")	1.75 ± 0.1 mm (.069 ± .004")	14.2 ± 0.1 mm (.559 ± .004")	—	4.0 ± 0.1 mm (.157 ± .004")	2.0 ± 0.1 mm (.079 ± .004")	50 mm (1.969")	0.6 mm (.024")	32.2 mm (1.272")
44 mm	35.0 mm (1.378")	2.0 mm Min (.079")			11.5 ± 0.1 mm (.453 ± .004")	15.9 mm Max (.625")					2.0 ± 0.15 mm (.079 ± .006")

Metric dimensions govern — English are in parentheses for reference only.

NOTE 1: A_0 , B_0 , and K_0 are determined by component size. The clearance between the components and the cavity must be within .05 mm min. to .50 mm max., the component cannot rotate more than 10° within the determined cavity.

NOTE 3: Pitch information is contained in the Embossed Tape and Reel Ordering Information on pg. 8.1–4.

EMBOSSED TAPE AND REEL DATA FOR DISCRETES



Size	A Max	G	T Max
12 mm	330 mm (12.992")	12.4 mm + 2.0 mm, -0.0 (.49" + .079", -0.00)	18.4 mm (.72")
16 mm	360 mm (14.173")	16.4 mm + 2.0 mm, -0.0 (.646" + .078", -0.00)	22.4 mm (.882")
24 mm	360 mm (14.173")	24.4 mm + 2.0 mm, -0.0 (.961" + .070", -0.00)	30.4 mm (1.197")
32 mm	360 mm (14.163")	32.4 mm + 2.0 mm, -0.0 (1.276" + 0.79", -0.00)	0.6 mm (.024")
44 mm	330 mm (12.992")	44.4 mm + 2.0 mm, -0.0 (1.748" + 0.79", -0.00)	50.4 mm (1.984")

Reel Dimensions

Metric Dimensions Govern — English are in parentheses for reference only

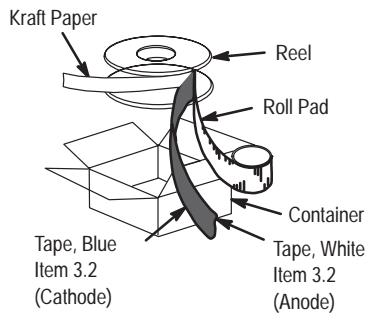


Figure 1. Reel Packing

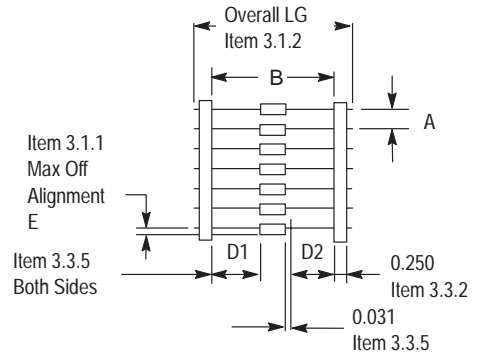


Figure 2. Component Spacing

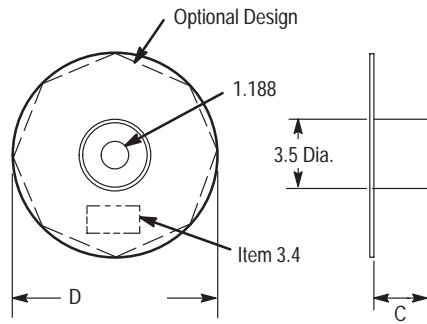


Figure 3. Reel Dimensions

Chapter Nine

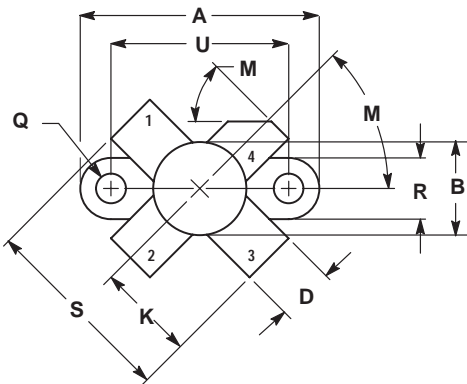
Packaging Information

The packaging availability for each device type is indicated on the individual data sheets and in the Selector Guide. All of the outline dimensions for the packages are given in this section.

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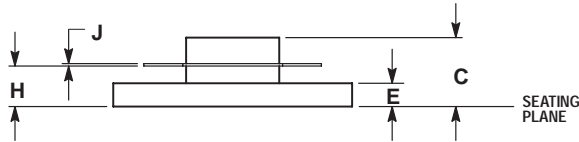
Case Dimensions



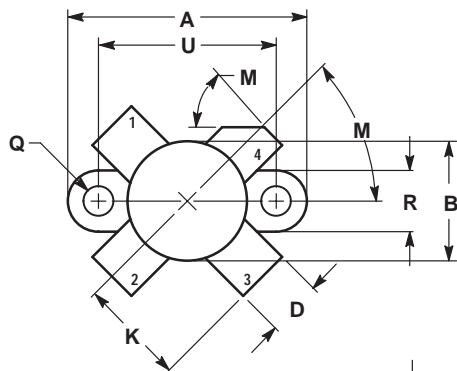
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.960	0.990	24.39	25.14
B	0.370	0.390	9.40	9.90
C	0.229	0.281	5.82	7.13
D	0.215	0.235	5.47	5.96
E	0.085	0.105	2.16	2.66
H	0.150	0.108	3.81	4.57
J	0.004	0.006	0.11	0.15
K	0.395	0.405	10.04	10.28
M	40°	50°	40°	50°
Q	0.113	0.130	2.88	3.30
R	0.245	0.255	6.23	6.47
S	0.790	0.810	20.07	20.57
U	0.720	0.730	18.29	18.54

- STYLE 2:
 PIN 1. SOURCE
 2. GATE
 3. SOURCE
 4. DRAIN



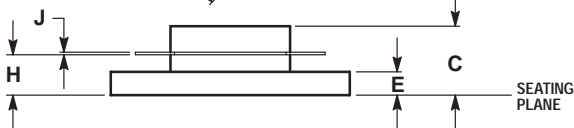
**CASE 211-07
 ISSUE N
 (.380" FLANGE)**



- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

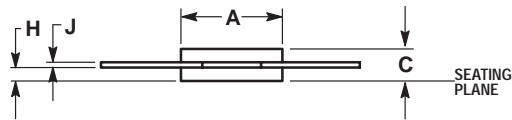
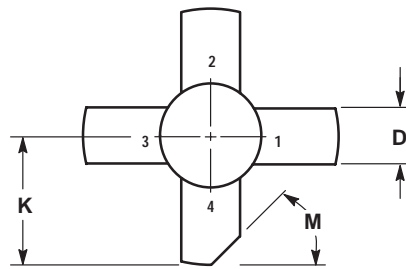
DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.960	0.990	24.39	25.14
B	0.465	0.510	11.82	12.95
C	0.229	0.275	5.82	6.98
D	0.216	0.235	5.49	5.96
E	0.084	0.110	2.14	2.79
H	0.144	0.178	3.66	4.52
J	0.003	0.007	0.08	0.17
K	0.435	----	11.05	----
M	45°NOM	----	45°NOM	----
Q	0.115	0.130	2.93	3.30
R	0.246	0.255	6.25	6.47
U	0.720	0.730	18.29	18.54

- STYLE 2:
 PIN 1. SOURCE
 2. GATE
 3. SOURCE
 4. DRAIN



**CASE 211-11
 ISSUE N
 (.500" FLANGE)**

CASE DIMENSIONS (continued)

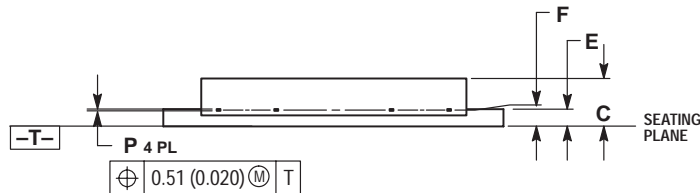
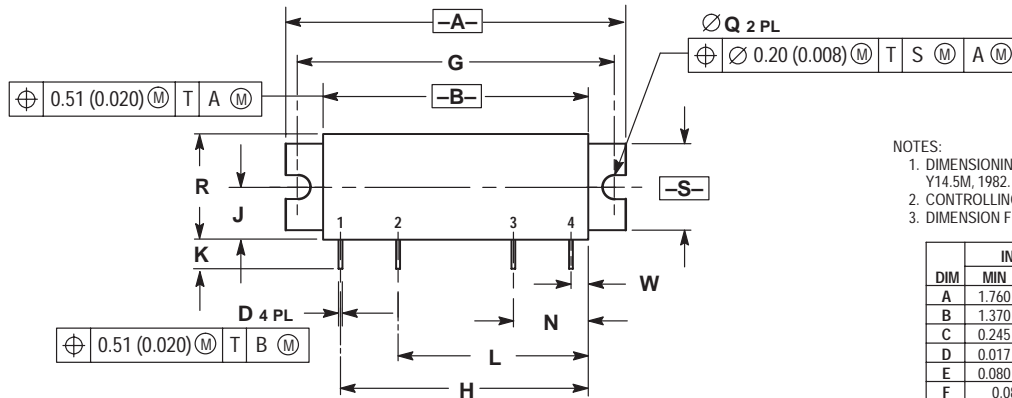


- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.
 3. SEATING PLANE = GROUND AND IS CONNECTED TO PIN 1 AND 3.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.271	0.286	6.88	7.26
C	0.112	0.136	2.84	3.45
D	0.215	0.235	5.46	5.97
H	0.055	0.065	1.40	1.65
J	0.003	0.007	0.08	0.18
K	0.435	---	11.05	---
M	45° REF		45° REF	

- STYLE 3:
 PIN 1. SOURCE
 2. GATE
 3. SOURCE
 4. DRAIN

**CASE 249-06
 ISSUE H
 (.280" PILL)**



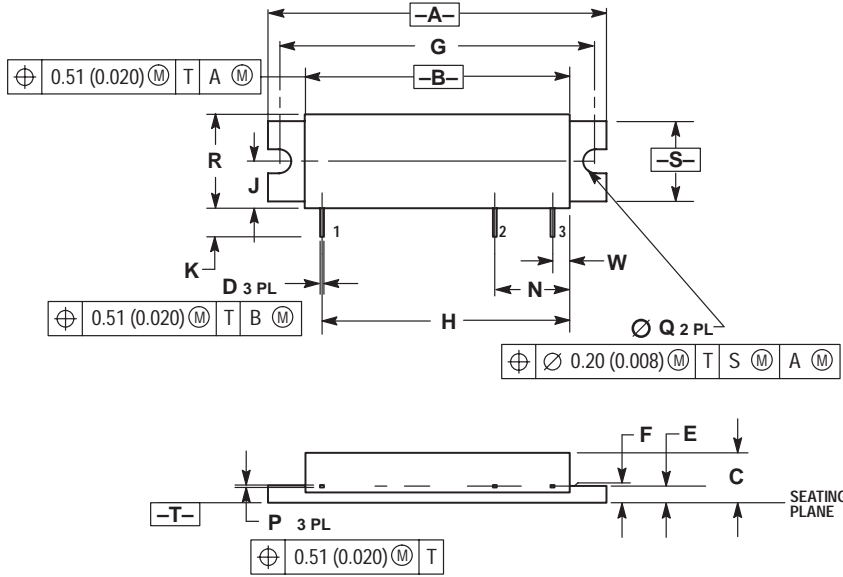
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.
 3. DIMENSION F TO CENTER OF LEADS.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	1.760	1.780	44.70	45.21
B	1.370	1.390	34.80	35.31
C	0.245	0.265	6.22	6.73
D	0.017	0.023	0.43	0.58
E	0.080	0.100	2.03	2.54
F	0.086 BSC		2.18 BSC	
G	1.650 BSC		41.91 BSC	
H	1.290 BSC		32.77 BSC	
J	0.266	0.280	6.76	7.11
K	0.125	0.165	3.18	4.19
L	0.990 BSC		25.15 BSC	
N	0.390 BSC		9.91 BSC	
P	0.008	0.013	0.20	0.33
Q	0.118	0.132	3.00	3.35
R	0.535	0.555	13.59	14.10
S	0.445	0.465	11.30	11.81
W	0.090 BSC		2.29 BSC	

- STYLE 1:
 PIN 1. RF INPUT
 2. VDD1
 3. VDD2
 4. RF OUTPUT
 CASE: GROUND
- STYLE 2:
 PIN 1. RF OUTPUT
 2. VDD2
 3. VDD1
 4. RF INPUT
 CASE: GROUND

**CASE 301AP-01
 ISSUE B**

CASE DIMENSIONS (continued)



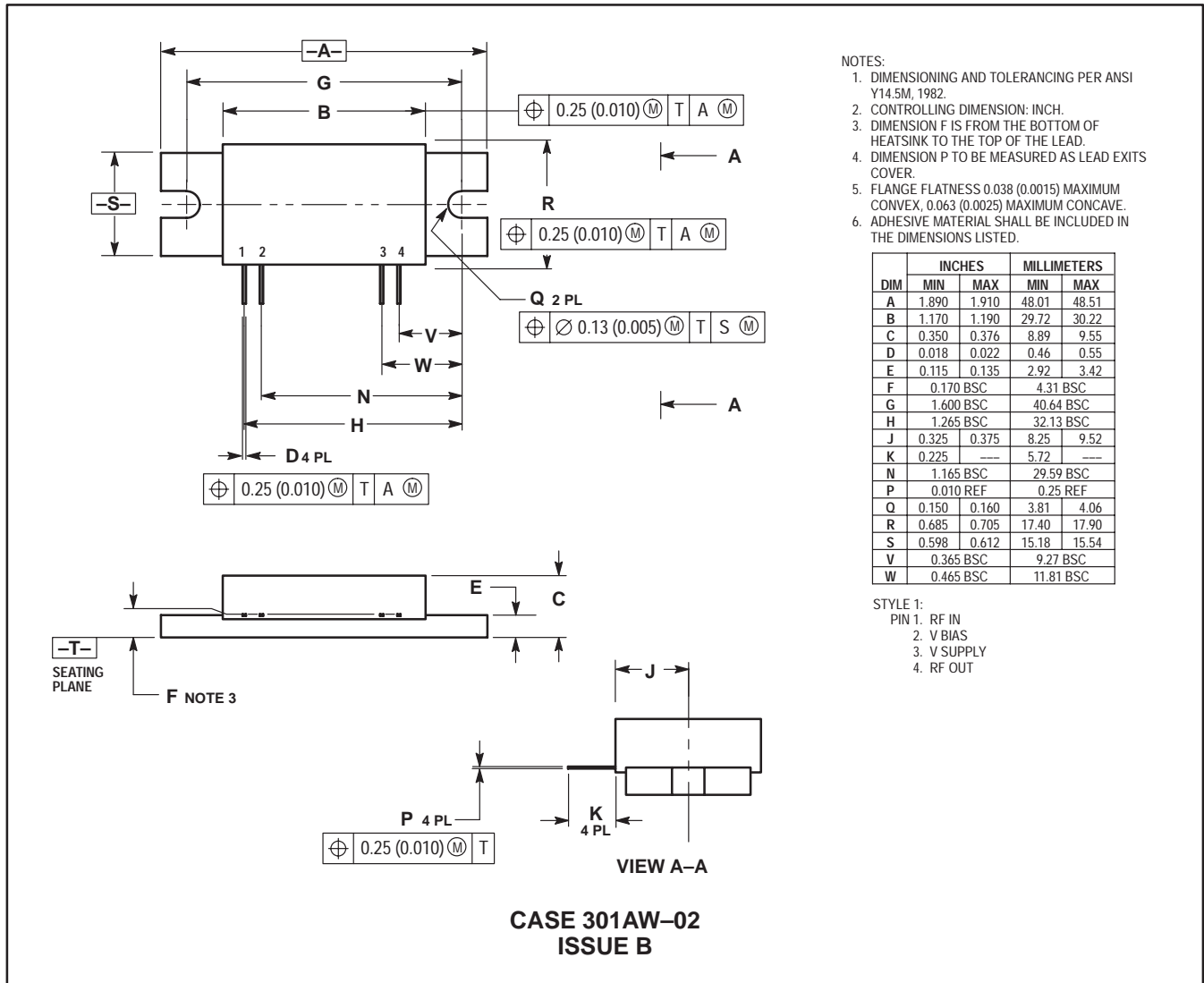
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.
 3. DIMENSION F TO CENTER OF LEADS.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	1.760	1.780	44.70	45.21
B	1.370	1.390	34.80	35.31
C	0.245	0.265	6.22	6.73
D	0.017	0.023	0.43	0.58
E	0.080	0.100	2.03	2.54
F	0.086 BSC		2.18 BSC	
G	1.650 BSC		41.91 BSC	
H	1.290 BSC		32.77 BSC	
J	0.266	0.280	6.76	7.11
K	0.125	0.165	3.18	4.19
N	0.390 BSC		9.91 BSC	
P	0.008	0.013	0.20	0.33
Q	0.118	0.132	3.00	3.35
R	0.535	0.555	13.59	14.10
S	0.445	0.465	11.30	11.81
W	0.090 BSC		2.29 BSC	

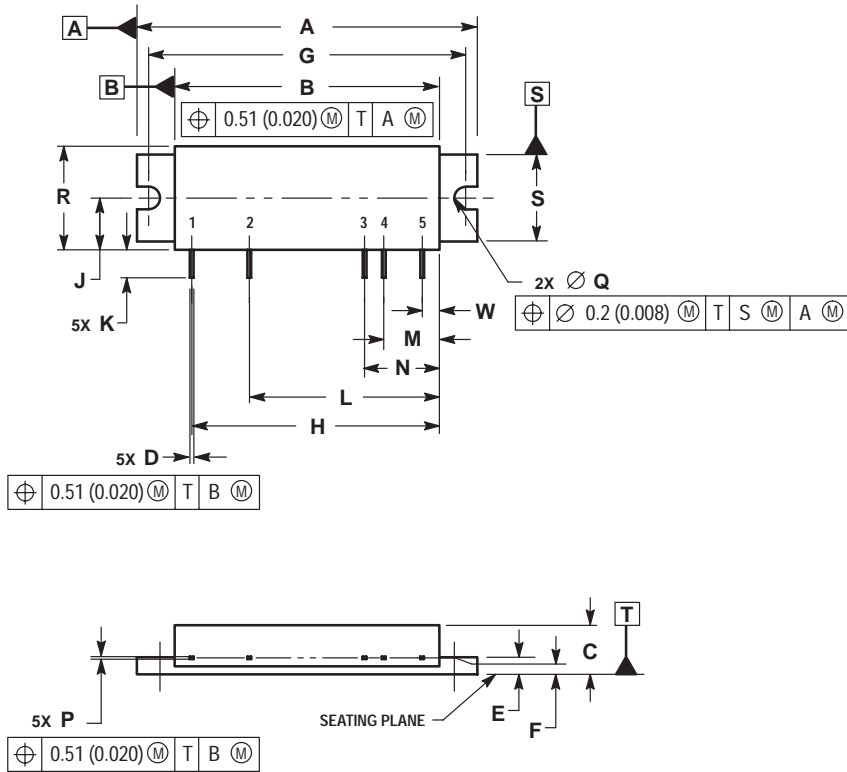
STYLE 1:
 PIN 1: RF INPUT
 2: VDD
 3: RF OUTPUT
 CASE: GROUND

CASE 301AS-01
 ISSUE A

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

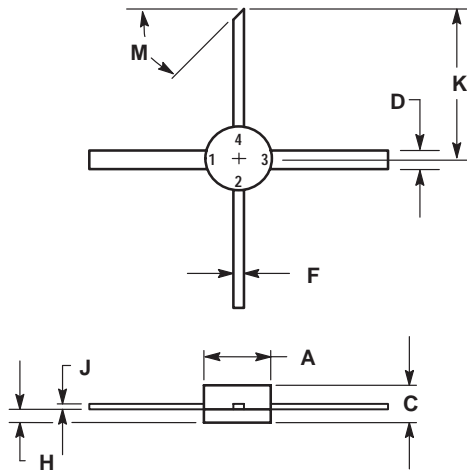


- NOTES:
 1. CONTROLLING DIMENSION: MILLIMETER.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ANSI Y14.5M, 1982.
 3. DIMENSION F TO CENTER LINE OF LEADS.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	44.7	45.21	1.760	1.780
B	34.8	35.31	1.370	1.390
C	6.22	6.73	0.245	0.265
D	0.43	0.58	0.017	0.023
E	2.03	2.54	0.080	0.100
F	2.18 BSC		0.086 BSC	
G	41.91 BSC		1.650 BSC	
H	32.77 BSC		1.290 BSC	
J	6.76	7.11	0.266	0.280
K	3.18	4.19	0.125	0.165
L	25.15 BSC		0.990 BSC	
M	7.37 BSC		0.290 BSC	
N	9.91 BSC		0.390 BSC	
P	0.2	0.33	0.008	0.013
Q	3	3.35	0.118	0.132
R	13.59	14.1	0.535	0.555
S	11.3	11.81	0.445	0.465
W	2.29 BSC		0.090 BSC	

- STYLE 1:
 PIN 5. RF INPUT
 6. VDD1
 7. VDD2
 8. VDD3
 9. RF OUTPUT
 CASE: GROUND

CASE 301AY-01
 ISSUE O



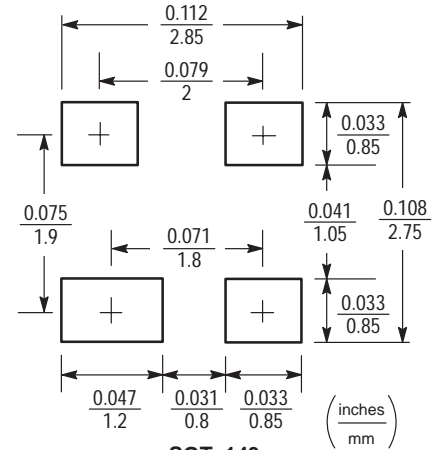
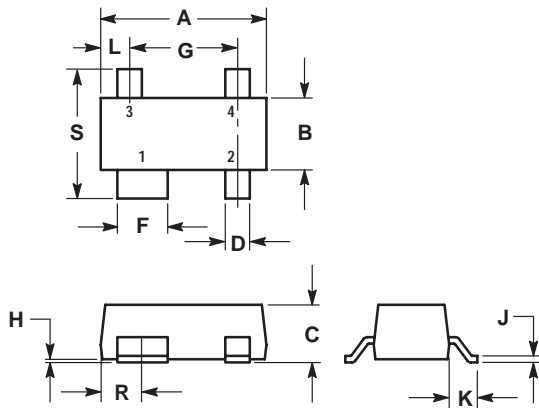
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.200	0.220	5.08	5.59
C	0.095	0.130	2.41	3.30
D	0.055	0.065	1.40	1.65
F	0.025	0.035	0.64	0.89
H	0.040	0.050	1.02	1.27
J	0.003	0.007	0.08	0.18
K	0.435	---	11.05	---
M	45 °REF		45 °REF	

- STYLE 2:
 PIN 1. SOURCE
 2. GATE
 3. SOURCE
 4. DRAIN

CASE 305A-01
 ISSUE A
 (.204" PILL)

CASE DIMENSIONS (continued)



**SOT-143
FOOTPRINT**

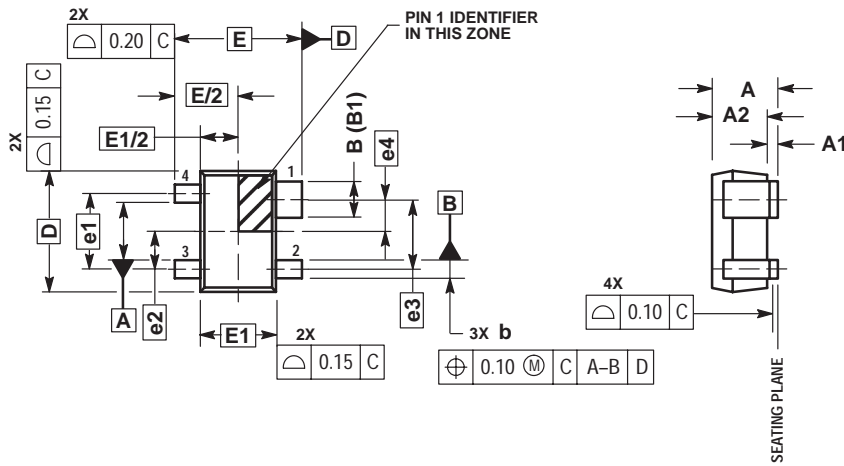
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: MILLIMETER.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.80	3.04	0.110	0.120
B	1.20	1.39	0.047	0.055
C	0.84	1.14	0.033	0.045
D	0.39	0.50	0.015	0.020
F	0.79	0.93	0.031	0.037
G	1.78	2.03	0.070	0.080
H	0.013	0.10	0.0005	0.004
J	0.08	0.15	0.003	0.006
K	0.46	0.60	0.018	0.024
L	0.445	0.60	0.0175	0.024
R	0.72	0.83	0.028	0.033
S	2.11	2.48	0.083	0.098

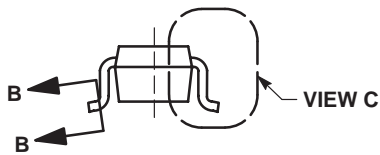
- STYLE 1:
 PIN 1. COLLECTOR
 2. EMITTER
 3. EMITTER
 4. BASE

**CASE 318A-05
 ISSUE R
 (SOT-143)**

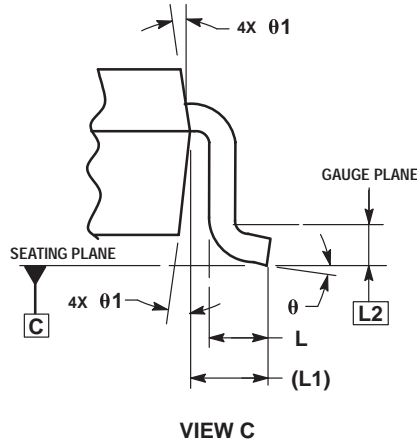
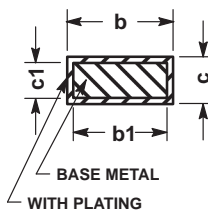
CASE DIMENSIONS (continued)



- NOTES:
1. DIMENSIONS ARE IN MILLIMETERS.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
 3. DIMENSION D DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.15mm PER END. DIMENSION E1 DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.15mm PER SIDE.
 4. DIMENSIONS D AND E1 ARE DETERMINED AT THE OUTMOST EXTREMES OF THE PLASTIC BODY EXCLUSIVE OF MOLD FLASH, TIE BAR BURRS, GATE BURRS AND INTERLEAD FLASH, BUT INCLUDING ANY MISMATCH BETWEEN THE TOP AND BOTTOM OF PLASTIC BODY.
 5. DATUMS A, B AND D TO BE DETERMINED 0.10mm FROM THE LEAD TIP.
 6. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.
 7. THESE DIMENSIONS APPLY TO THE FLAT SECTION OF THE LEAD BETWEEN 0.08mm AND 0.15mm FROM THE LEAD TIP.



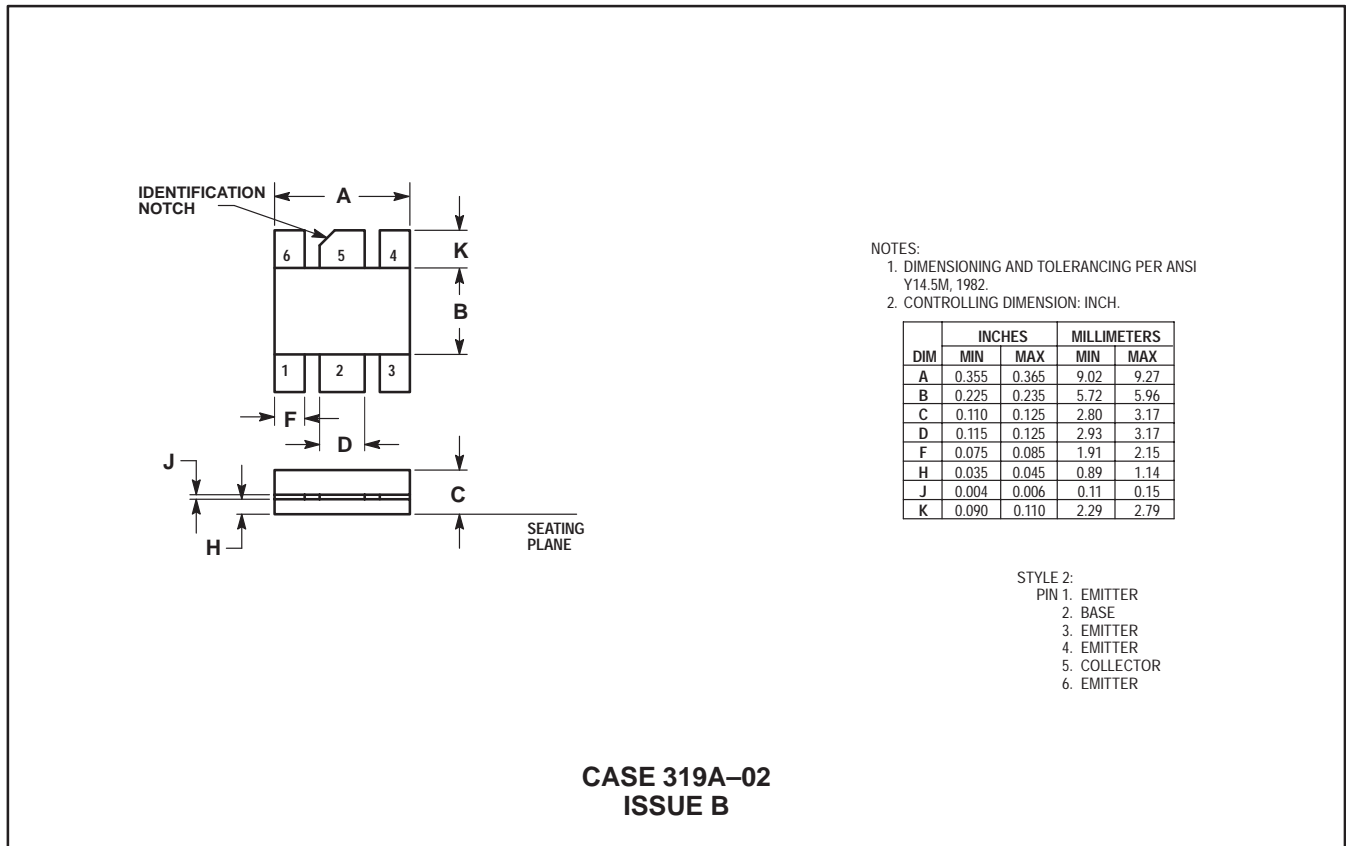
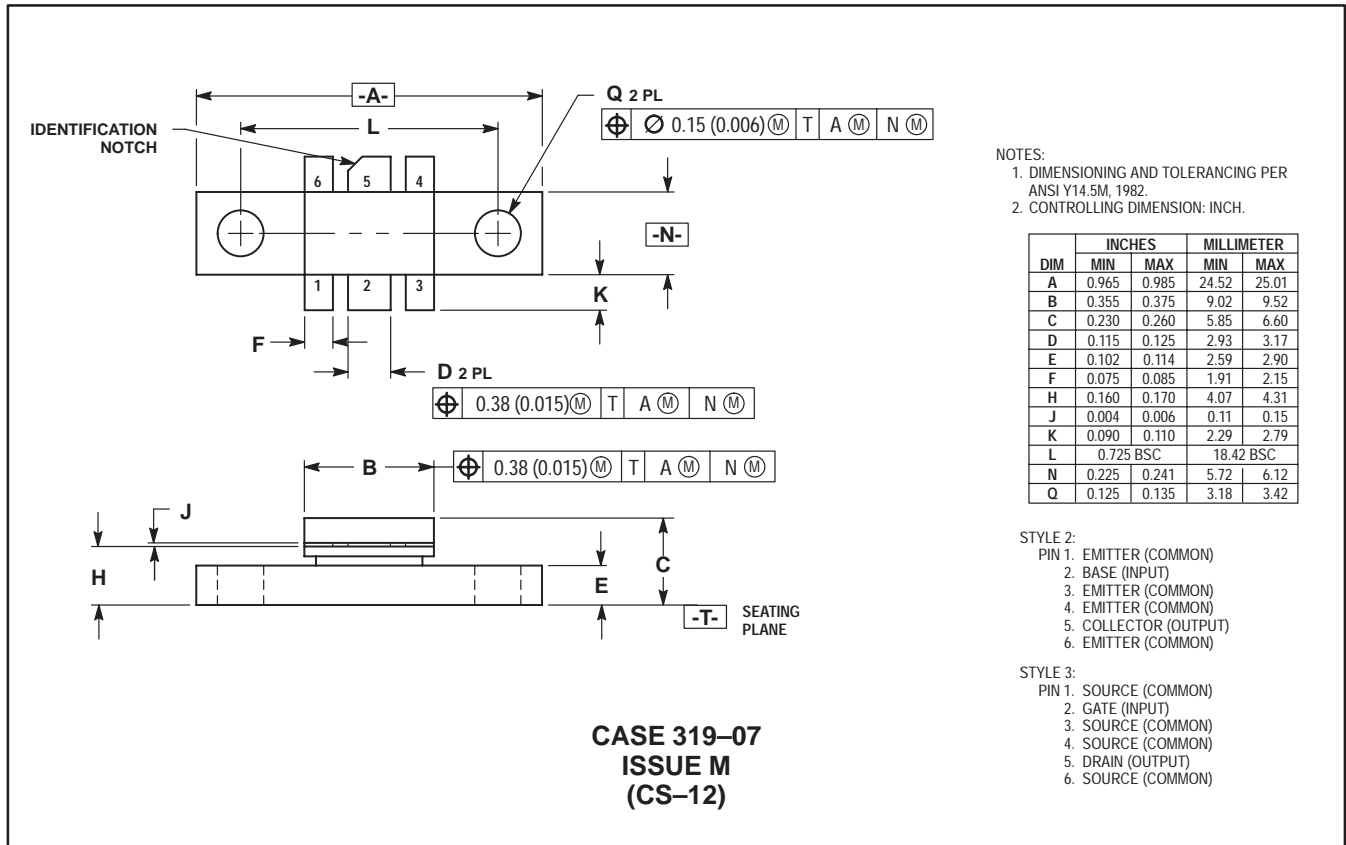
SECTION B-B
(SEE NOTE 7)



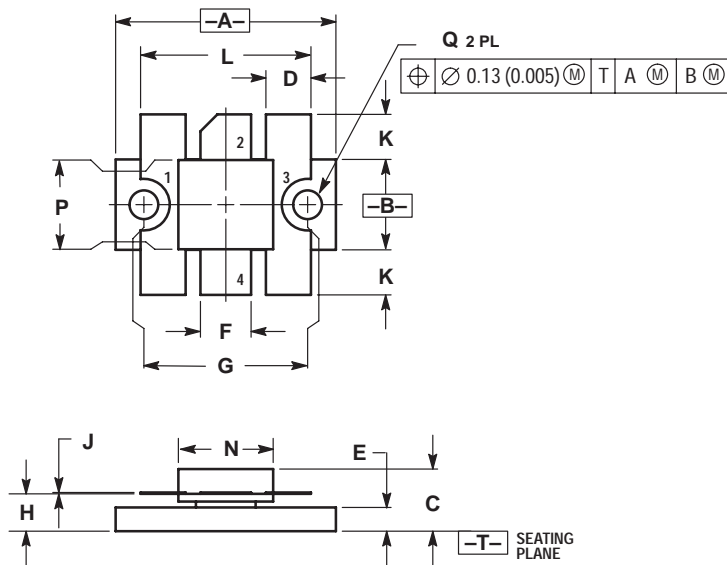
DIM	MILLIMETERS	
	MIN	MAX
A	---	1.10
A1	0.00	0.10
A2	0.80	1.00
b	0.25	0.40
b1	0.25	0.35
B	0.55	0.70
B1	0.55	0.65
c	0.10	0.25
c1	0.08	0.20
D	2.00	BSC
E	2.10	BSC
E1	1.25	BSC
e1	1.30	BSC
e2	0.65	BSC
e3	1.15	BSC
e4	0.50	BSC
L	0.26	0.46
L1	0.425	REF
L2	0.15	BSC
θ	0°	8°
θ1	4°	10°

CASE 318M-01
ISSUE O
(SOT-343)

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

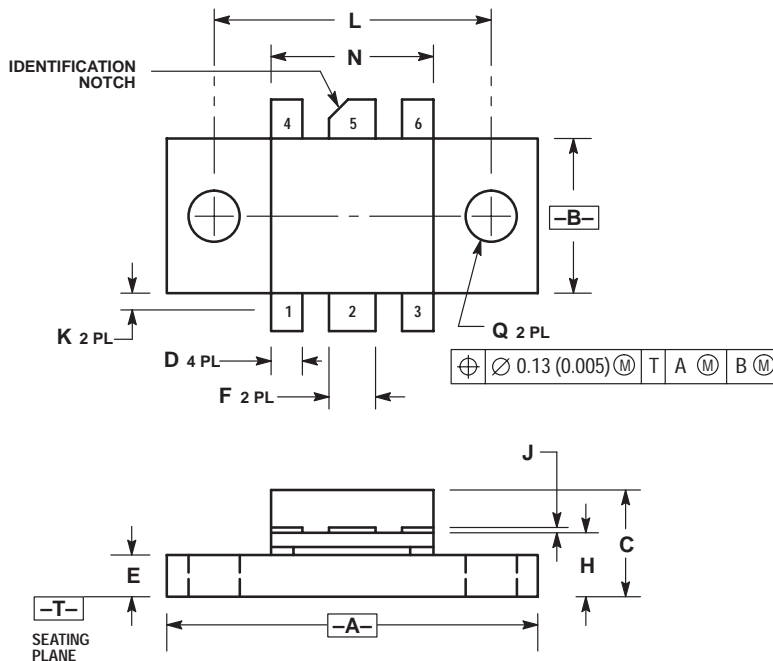


- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.965	0.985	24.51	25.02
B	0.390	0.410	9.91	10.41
C	0.250	0.290	6.73	7.36
D	0.190	0.210	4.83	5.33
E	0.095	0.115	2.42	2.92
F	0.215	0.235	5.47	5.96
G	0.725 BSC		18.42 BSC	
H	0.155	0.175	3.94	4.44
J	0.004	0.006	0.10	0.15
K	0.195	0.205	4.95	5.21
L	0.740	0.770	18.80	19.55
N	0.415	0.425	10.54	10.80
P	0.390	0.400	9.91	10.16
Q	0.120	0.135	3.05	3.42

- STYLE 2:
 PIN 1. SOURCE
 2. DRAIN
 3. SOURCE
 4. GATE

CASE 333-04
 ISSUE E



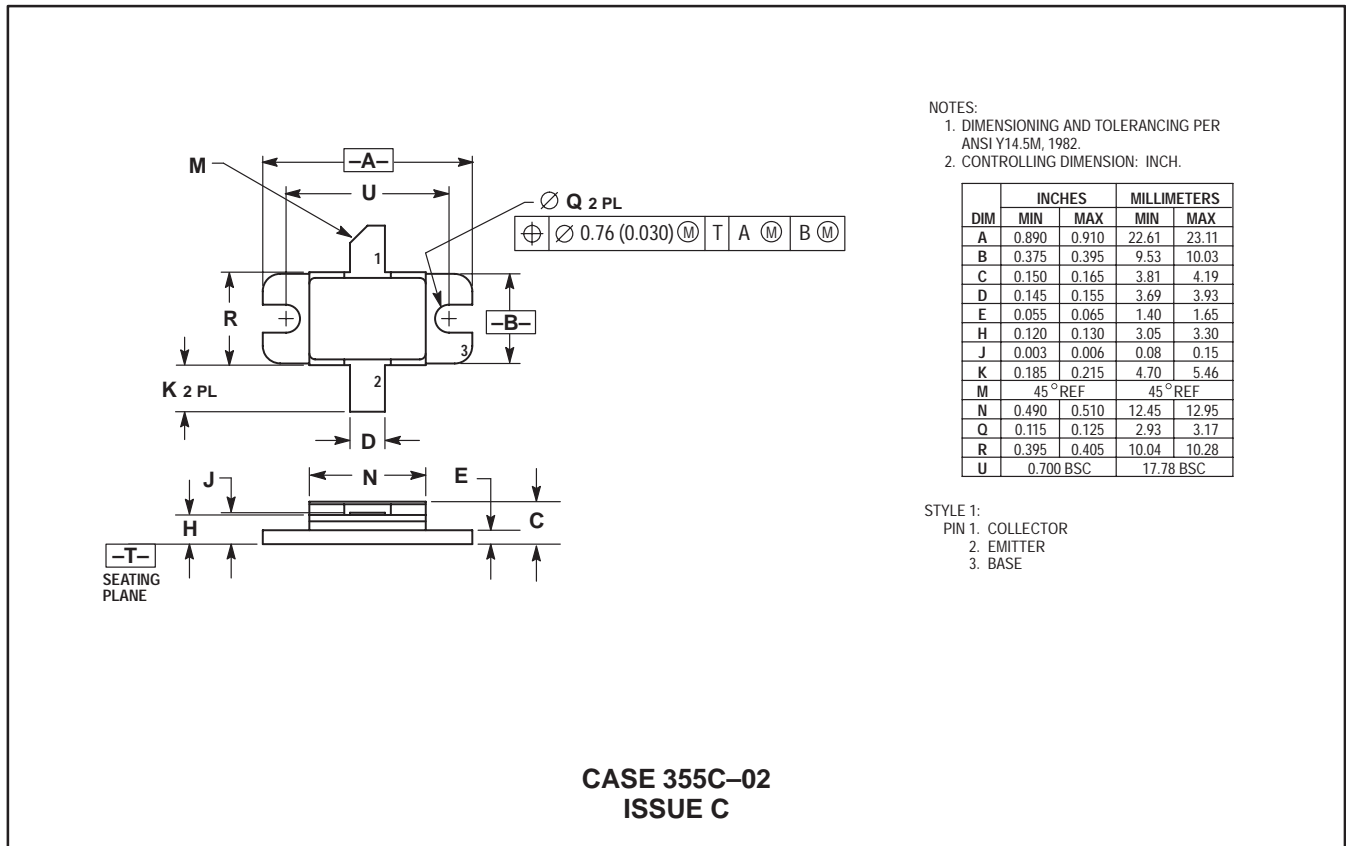
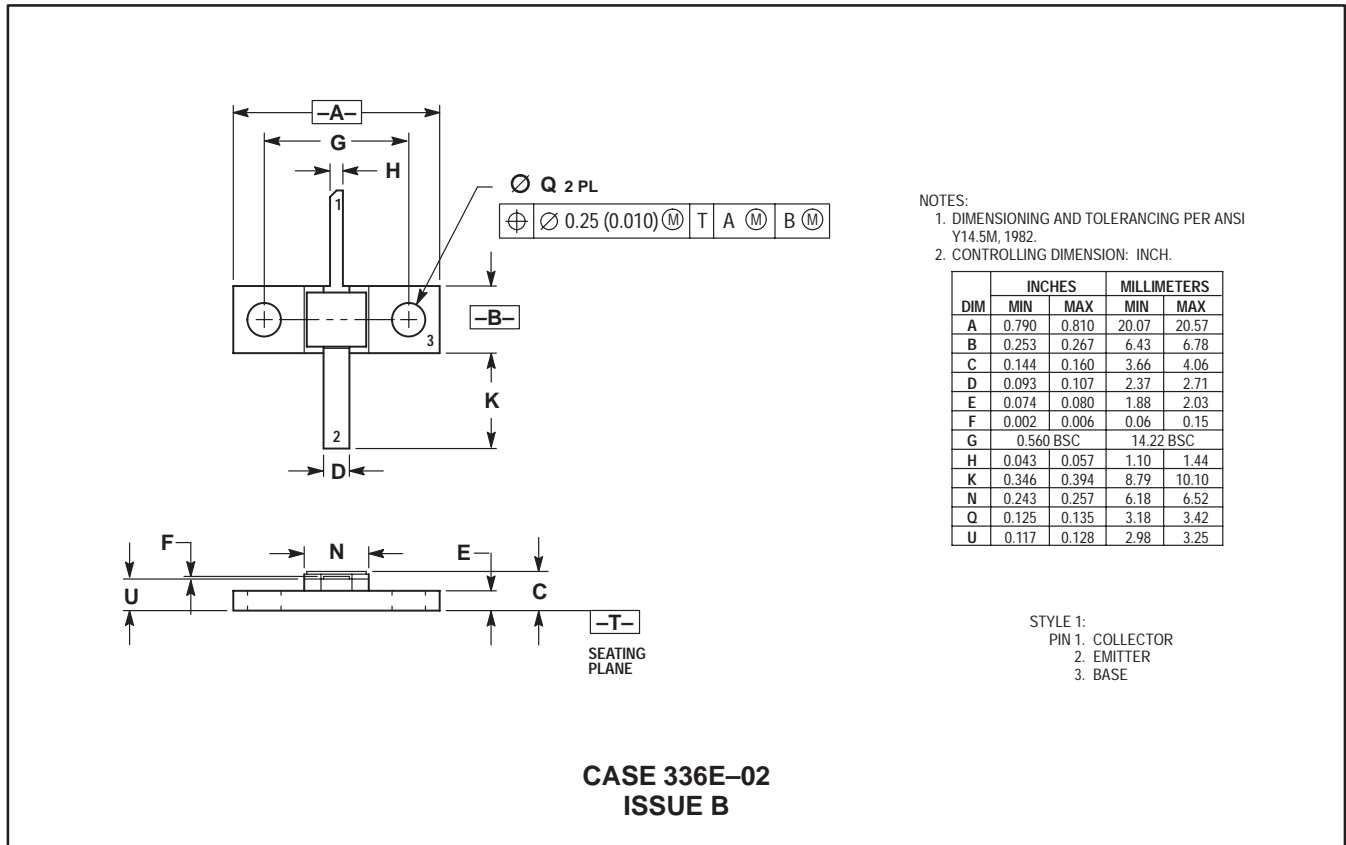
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.965	0.985	24.52	25.01
B	0.390	0.410	9.91	10.41
C	0.250	0.290	6.35	7.36
D	0.075	0.090	1.91	2.28
E	0.095	0.115	2.42	2.92
F	0.110	0.130	2.80	3.30
H	0.155	0.175	3.94	4.44
J	0.004	0.006	0.11	0.15
K	0.090	0.116	2.29	2.94
L	0.725 BSC		18.41 BSC	
N	0.415	0.435	10.55	11.04
Q	0.120	0.135	3.05	3.42

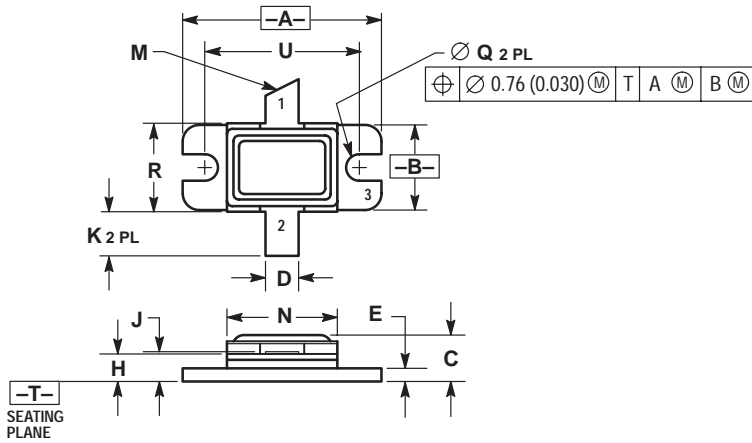
- STYLE 1:
 PIN 1. BASE
 2. EMITTER
 3. BASE
 4. BASE
 5. COLLECTOR
 6. BASE
- STYLE 2:
 PIN 1. EMITTER
 2. BASE
 3. EMITTER
 4. EMITTER
 5. COLLECTOR
 6. EMITTER

CASE 333A-02
 ISSUE C
 (MAAC PAC)

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

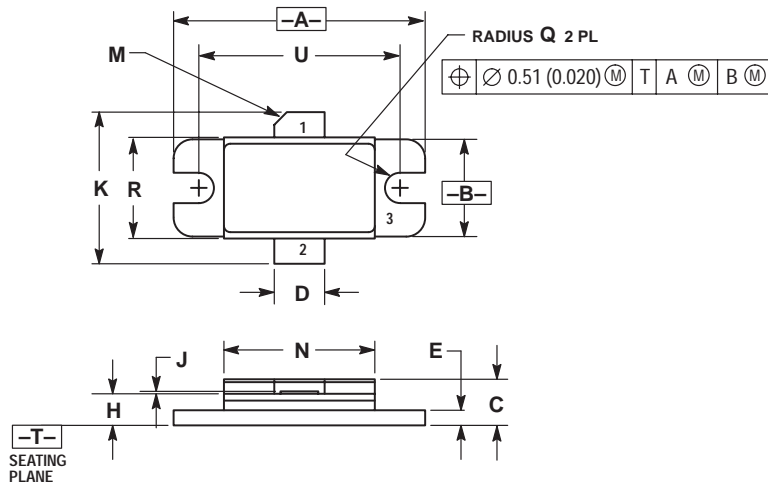


- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.890	0.910	22.61	23.11
B	0.375	0.395	9.53	10.03
C	0.190	0.210	4.83	5.33
D	0.145	0.155	3.69	3.93
E	0.055	0.065	1.40	1.65
H	0.120	0.130	3.05	3.30
J	0.003	0.006	0.08	0.15
K	0.185	0.215	4.70	5.46
M	45° REF		45° REF	
N	0.490	0.510	12.45	12.95
Q	0.115	0.125	2.93	3.17
R	0.395	0.405	10.04	10.28
U	0.700 BSC		17.78 BSC	

- STYLE 1:
 PIN 1. COLLECTOR
 2. EMITTER
 3. BASE

CASE 355E-01
 ISSUE B



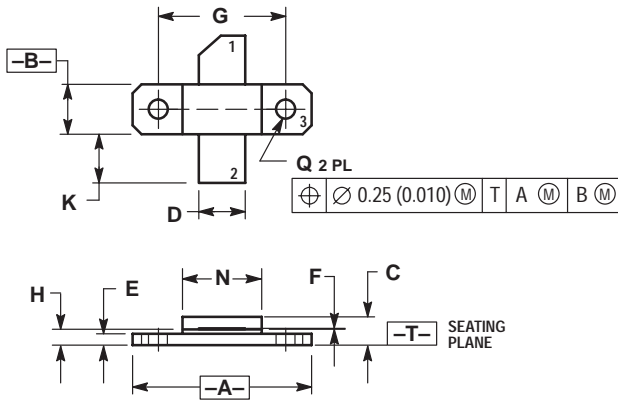
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.990	1.010	25.15	25.65
B	0.375	0.395	9.53	10.03
C	0.145	0.175	3.68	4.45
D	0.195	0.205	4.95	5.21
E	0.055	0.065	1.40	1.65
H	0.117	0.133	2.97	3.38
J	0.003	0.006	0.08	0.15
K	0.580	0.620	14.73	15.75
M	45° REF		45° REF	
N	0.590	0.610	14.99	15.49
Q	0.055	0.065	1.40	1.65
R	0.395	0.405	10.03	10.29
U	0.800 BSC		20.32 BSC	

- STYLE 1:
 PIN 1. COLLECTOR
 2. EMITTER
 3. BASE

CASE 355J-02
 ISSUE A

CASE DIMENSIONS (continued)

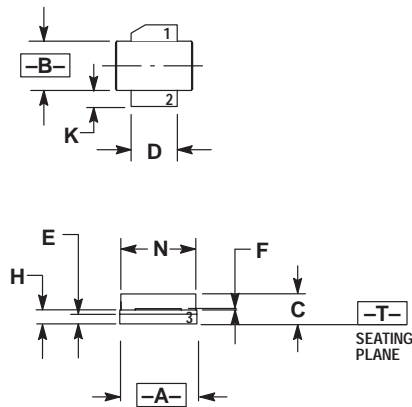


- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.
 3. DIMENSION H IS MEASURED 0.030" AWAY FROM EDGE OF FLANGE.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.790	0.810	20.07	20.57
B	0.220	0.240	5.59	6.09
C	0.125	0.175	3.18	4.45
D	0.205	0.225	5.21	5.71
E	0.050	0.070	1.27	1.77
F	0.004	0.006	0.11	0.15
G	0.562 BSC		14.27 BSC	
H	0.077	0.087	1.96	2.21
K	0.215	0.255	5.47	6.47
N	0.350	0.370	8.89	9.39
Q	0.120	0.140	3.05	3.55

- STYLE 1:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

CASE 360B-03
 ISSUE D



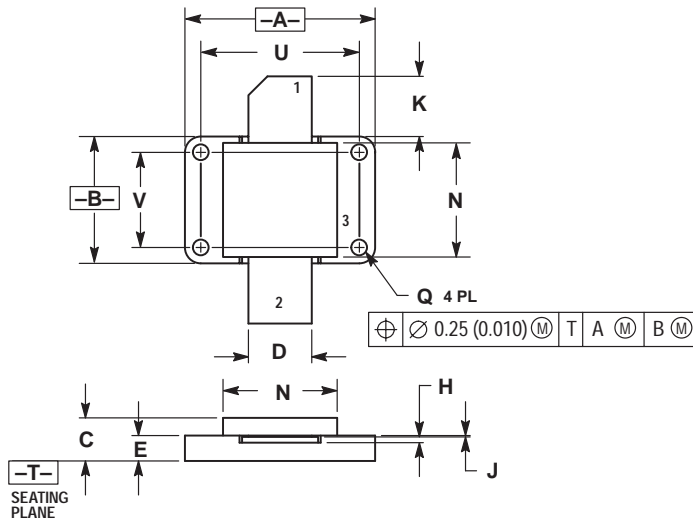
- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.370	0.390	9.40	9.91
B	0.220	0.240	5.59	6.09
C	0.105	0.155	2.67	3.94
D	0.205	0.225	5.21	5.71
E	0.035	0.045	0.89	1.14
F	0.004	0.006	0.11	0.15
H	0.057	0.067	1.45	1.70
K	0.085	0.115	2.16	2.92
N	0.350	0.370	8.89	9.39

- STYLE 1:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

CASE 360C-03
 ISSUE B

CASE DIMENSIONS (continued)

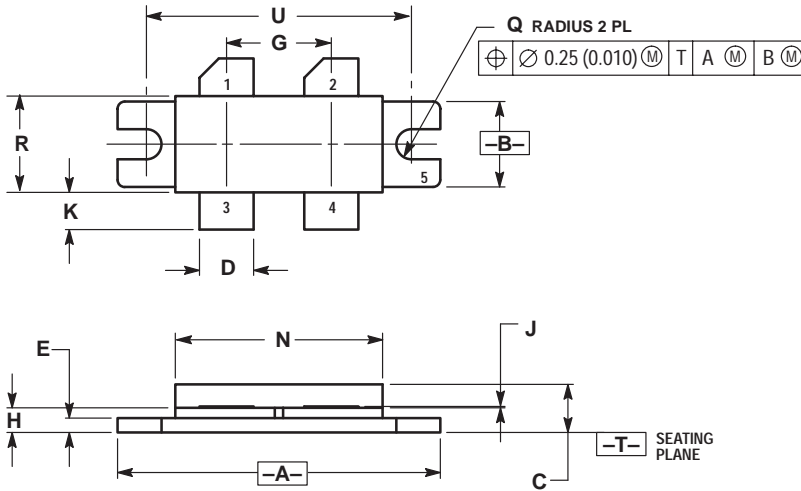


- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	1.490	1.510	37.85	38.35
B	0.990	1.010	25.15	25.65
C	0.330	0.365	8.38	9.27
D	0.490	0.510	12.45	12.95
E	0.195	0.205	4.95	5.21
H	0.045	0.055	1.14	1.39
J	0.004	0.006	0.10	0.15
K	0.425	0.500	10.80	12.70
N	0.890	0.910	22.87	23.11
Q	0.120	0.130	3.05	3.30
U	1.250 BSC		31.75 BSC	
V	0.750 BSC		19.05 BSC	

- STYLE 2:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

CASE 368-03
 ISSUE C
 (HOG PAC)



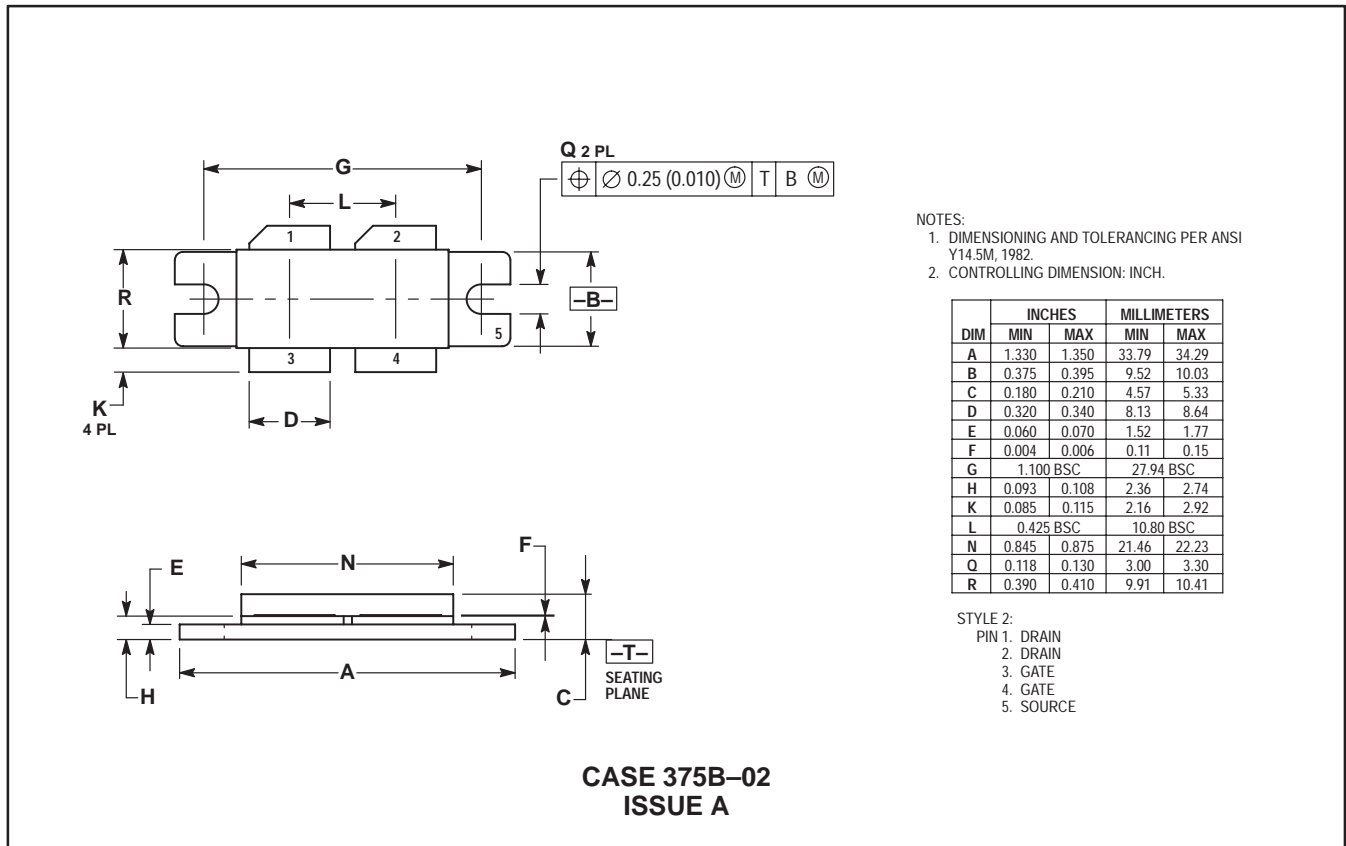
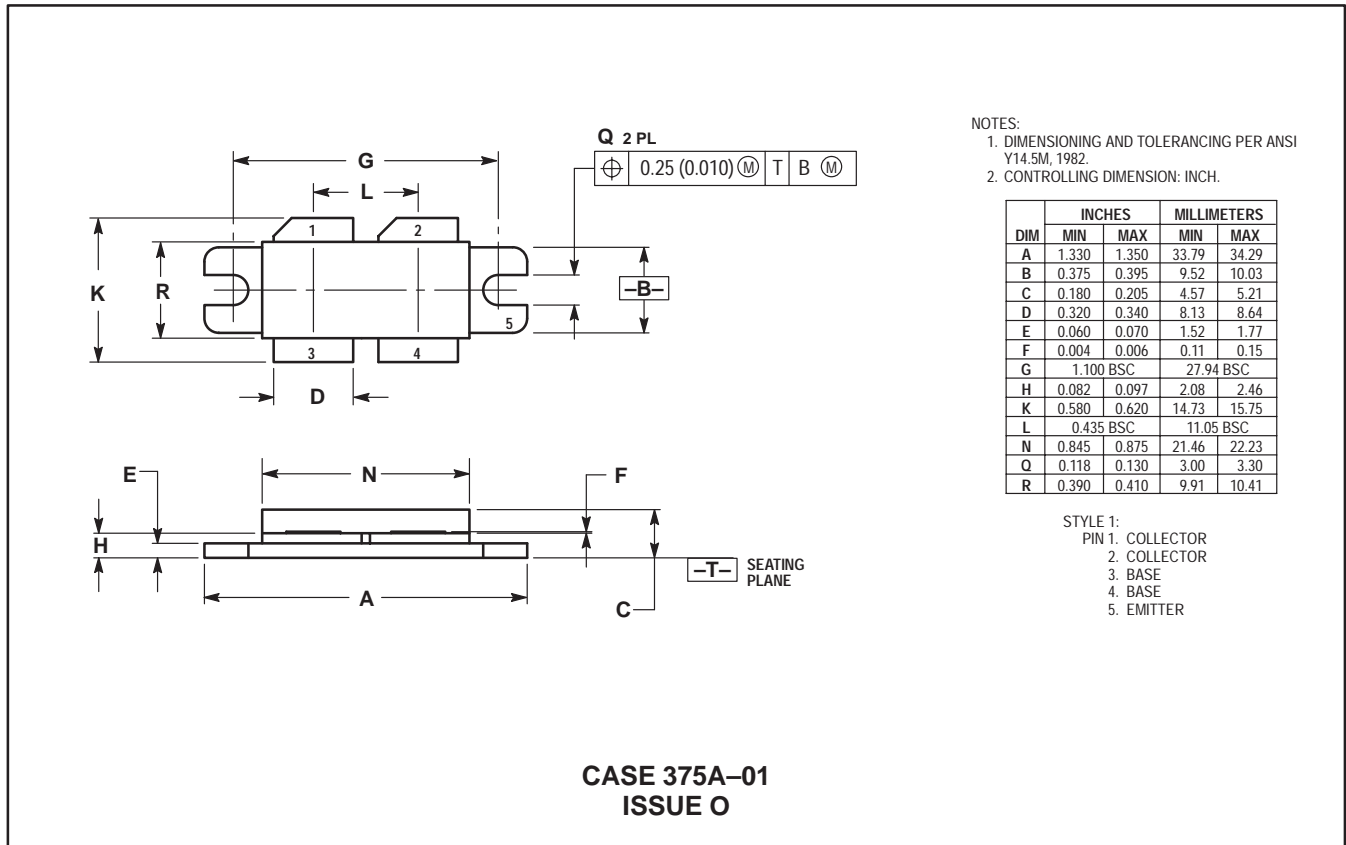
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	1.330	1.350	33.79	34.29
B	0.370	0.410	9.40	10.41
C	0.190	0.230	4.83	5.84
D	0.215	0.235	5.47	5.96
E	0.050	0.070	1.27	1.77
G	0.430	0.440	10.92	11.18
H	0.102	0.112	2.59	2.84
J	0.004	0.006	0.11	0.15
K	0.185	0.215	4.83	5.33
N	0.845	0.875	21.46	22.23
Q	0.060	0.070	1.52	1.78
R	0.390	0.410	9.91	10.41
U	1.100 BSC		27.94 BSC	

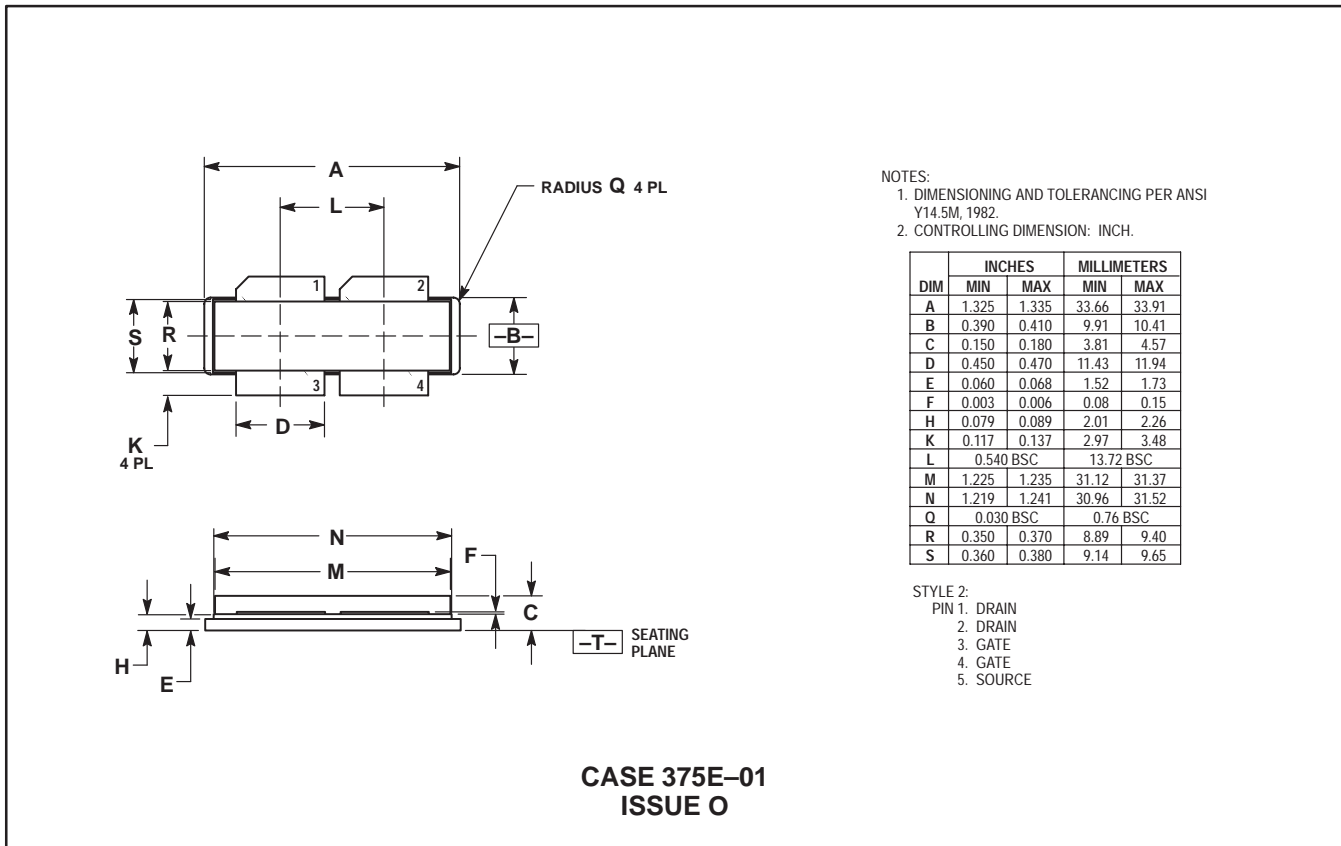
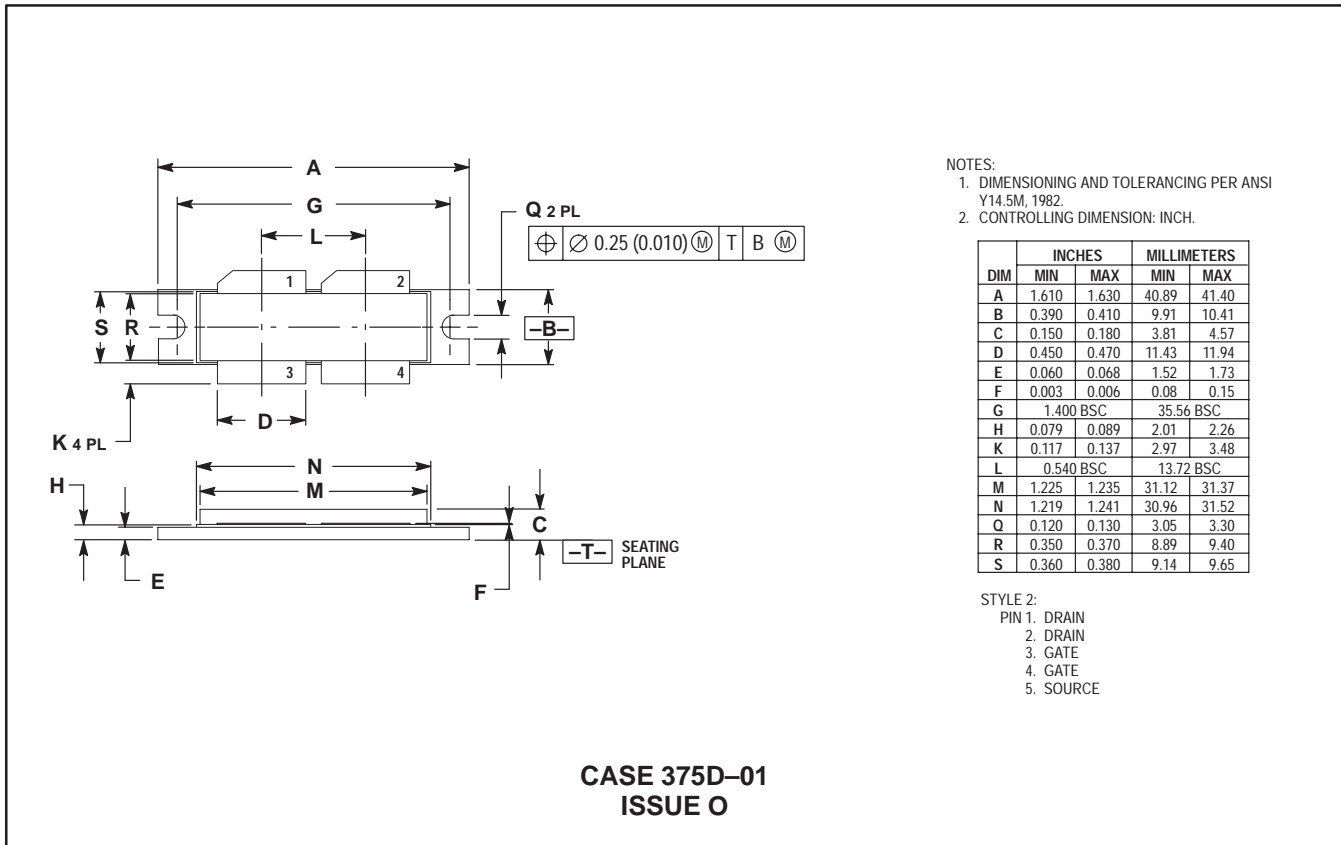
- STYLE 2:
 PIN 1. DRAIN
 2. DRAIN
 3. GATE
 4. GATE
 5. SOURCE

CASE 375-04
 ISSUE D

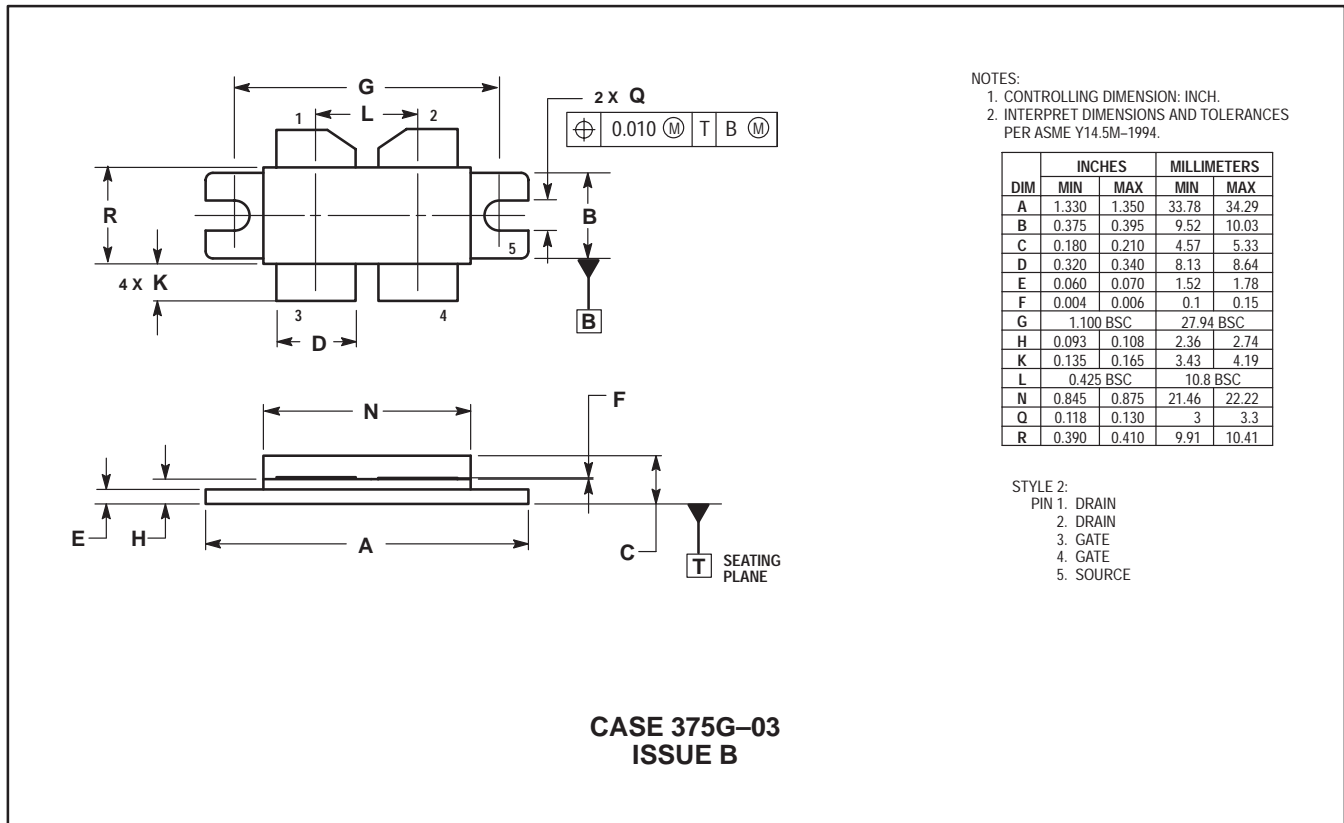
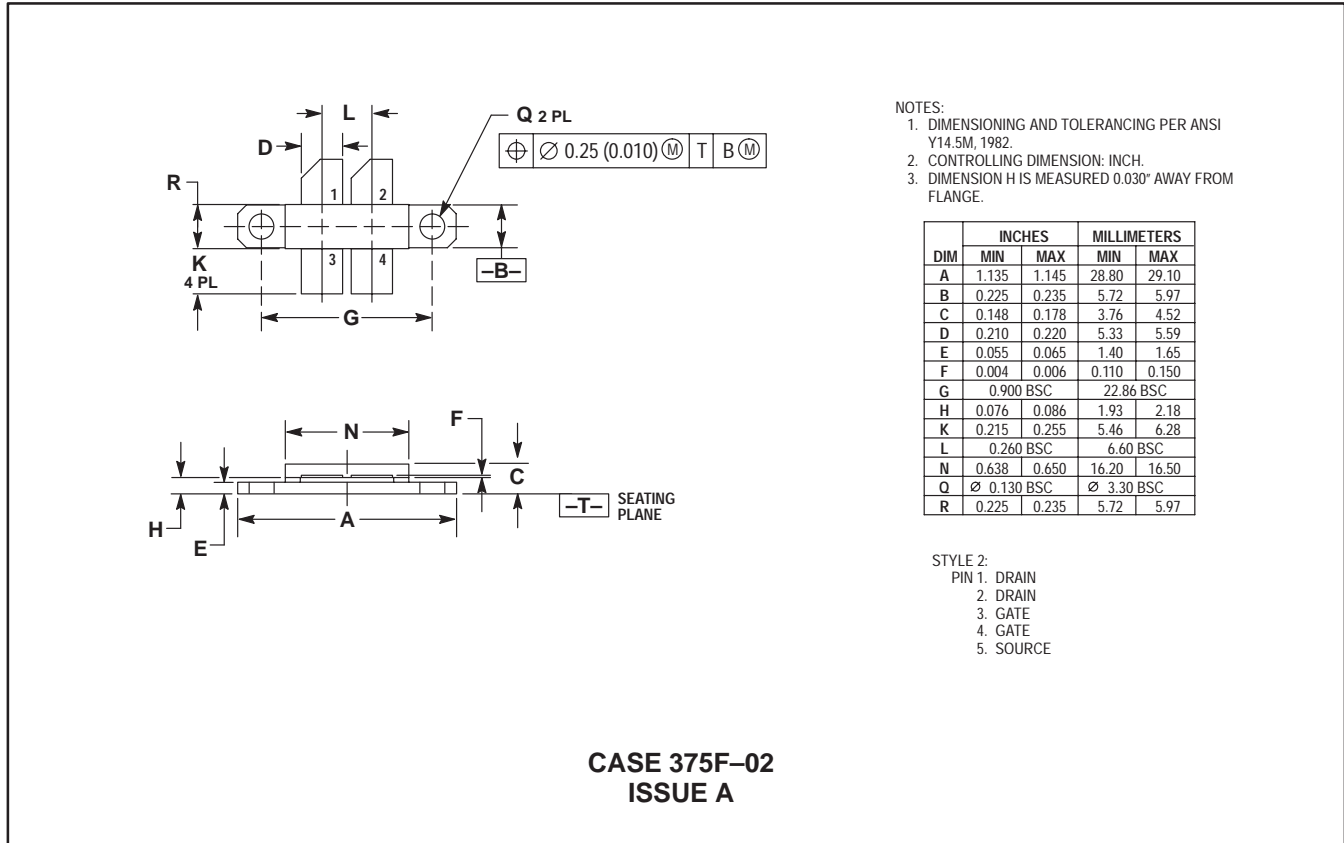
CASE DIMENSIONS (continued)



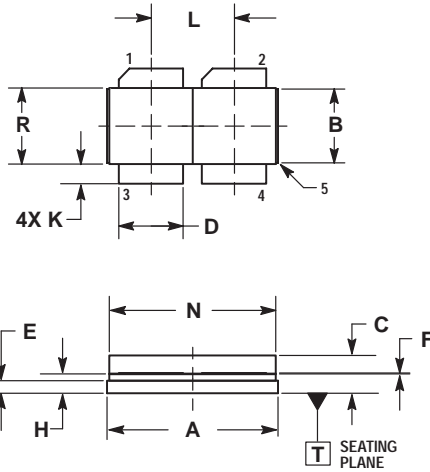
CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

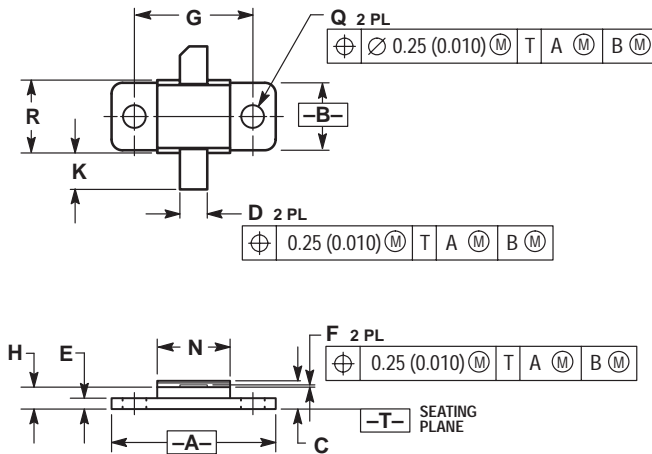


- NOTES:
 1. CONTROLLING DIMENSION: INCH.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M-1994.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	.880	.900	22.35	22.86
B	.375	.395	9.52	10.03
C	.180	.210	4.57	5.33
D	.320	.340	8.13	8.64
E	.060	.070	1.52	1.78
F	.004	.006	0.1	0.15
H	.093	.108	2.36	2.74
K	.085	.115	2.16	2.92
L	.425 BSC		10.8 BSC	
N	.845	.875	21.46	22.22
R	.390	.410	9.91	10.41

- STYLE 2:
 PIN 1. DRAIN
 2. DRAIN
 3. GATE
 4. GATE
 5. SOURCE

CASE 375H-01
 ISSUE O



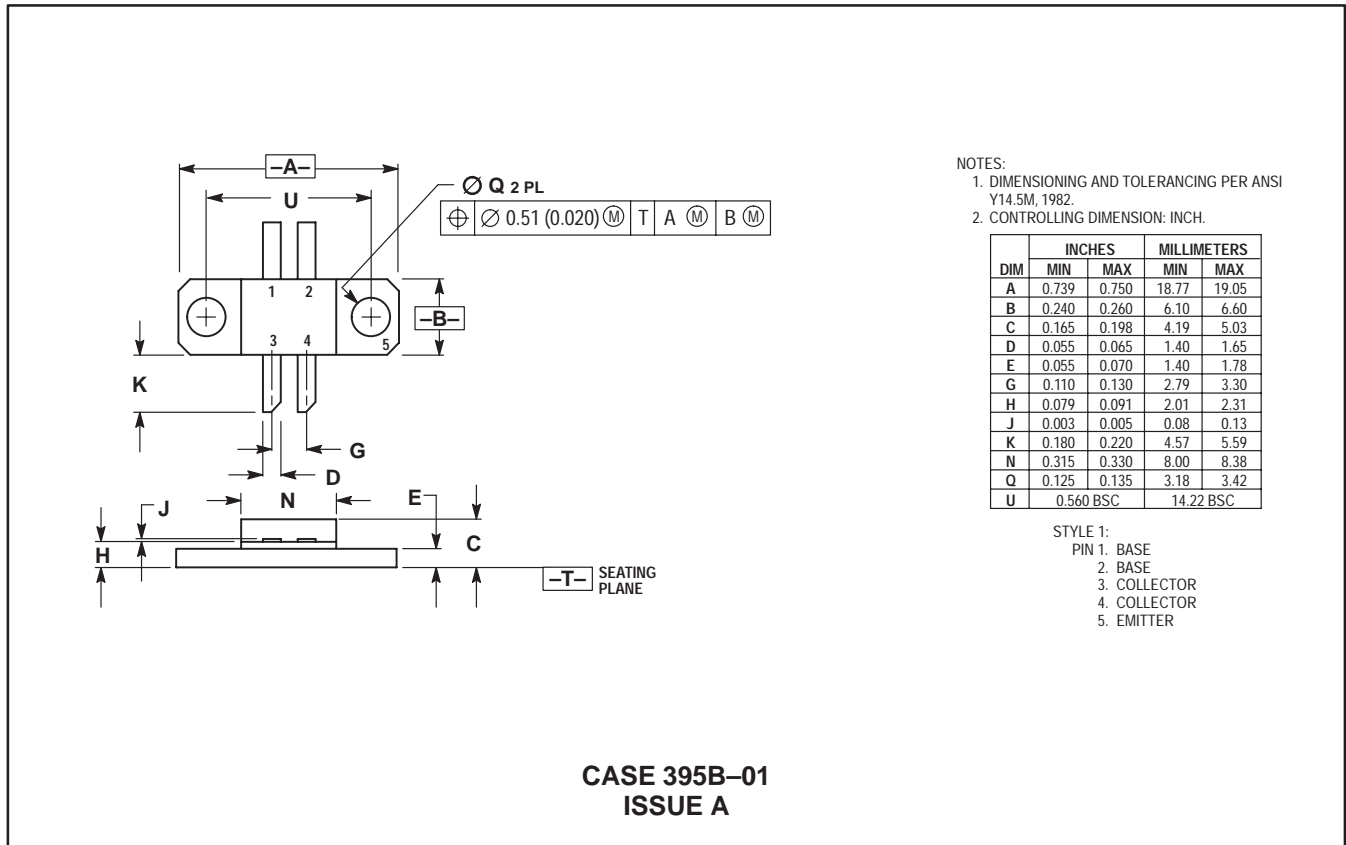
- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.890	0.910	22.61	23.11
B	0.370	0.400	9.40	10.16
C	0.145	0.160	3.69	4.06
D	0.140	0.160	3.56	4.06
E	0.055	0.065	1.40	1.65
F	0.003	0.006	0.08	0.15
G	0.650 BSC		16.51 BSC	
H	0.110	0.130	2.80	3.30
K	0.180	0.220	4.57	5.59
N	0.390	0.410	9.91	10.41
Q	0.115	0.135	2.93	3.42
R	0.390	0.410	9.91	10.41

- STYLE 1:
 PIN 1. COLLECTOR
 2. EMITTER
 3. BASE

CASE 376B-02
 ISSUE B

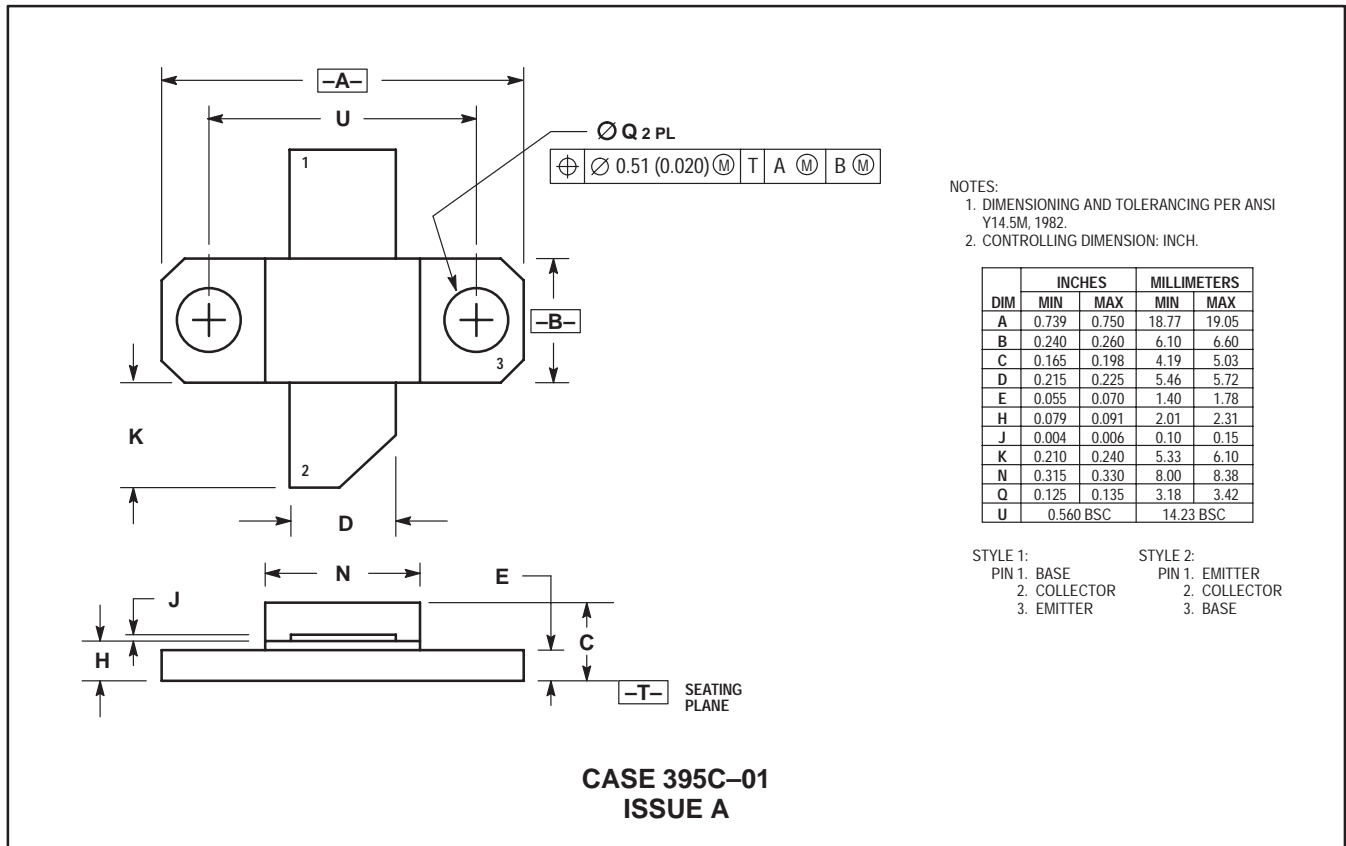
CASE DIMENSIONS (continued)



- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.739	0.750	18.77	19.05
B	0.240	0.260	6.10	6.60
C	0.165	0.198	4.19	5.03
D	0.055	0.065	1.40	1.65
E	0.055	0.070	1.40	1.78
G	0.110	0.130	2.79	3.30
H	0.079	0.091	2.01	2.31
J	0.003	0.005	0.08	0.13
K	0.180	0.220	4.57	5.59
N	0.315	0.330	8.00	8.38
Q	0.125	0.135	3.18	3.42
U	0.560 BSC		14.22 BSC	

- STYLE 1:
 PIN 1. BASE
 2. BASE
 3. COLLECTOR
 4. COLLECTOR
 5. EMITTER

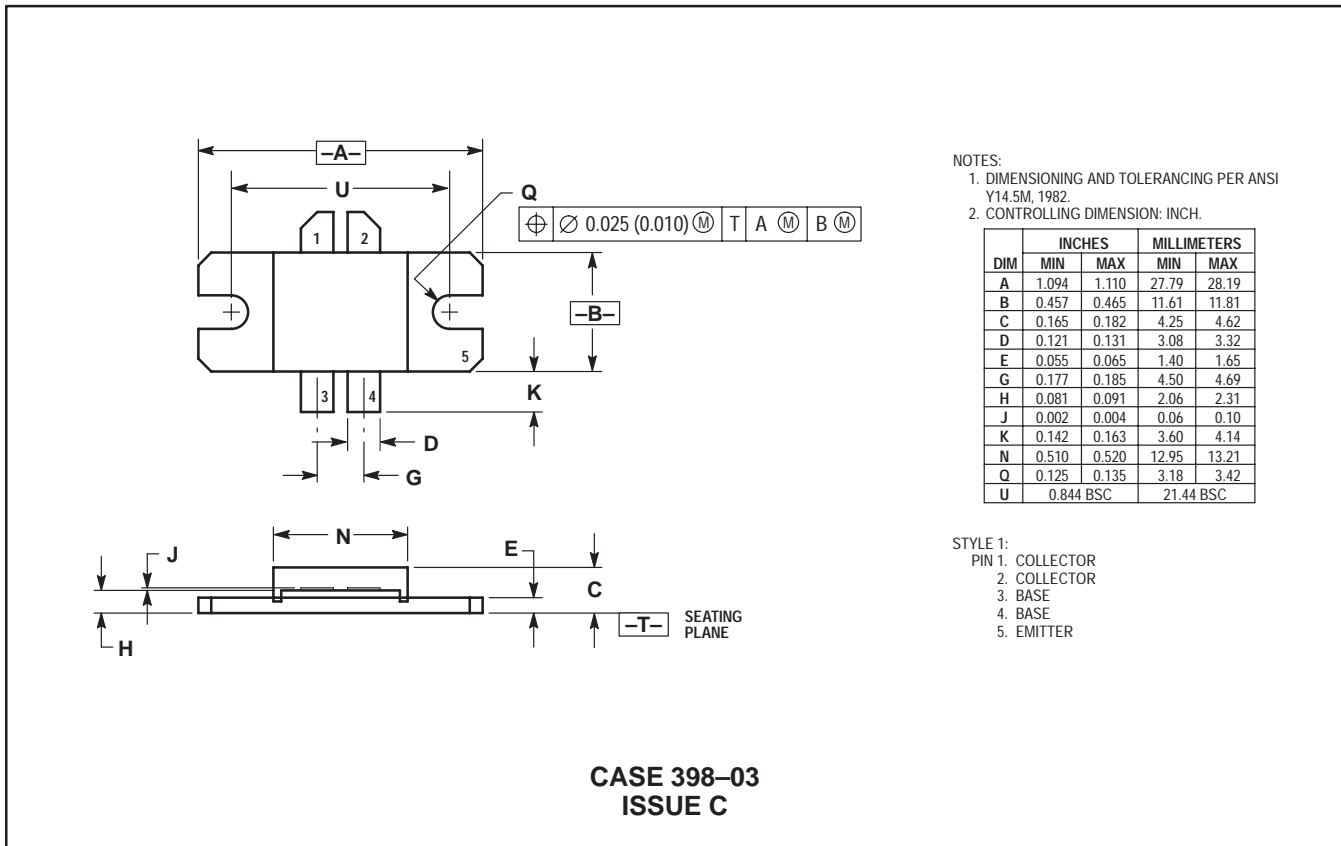
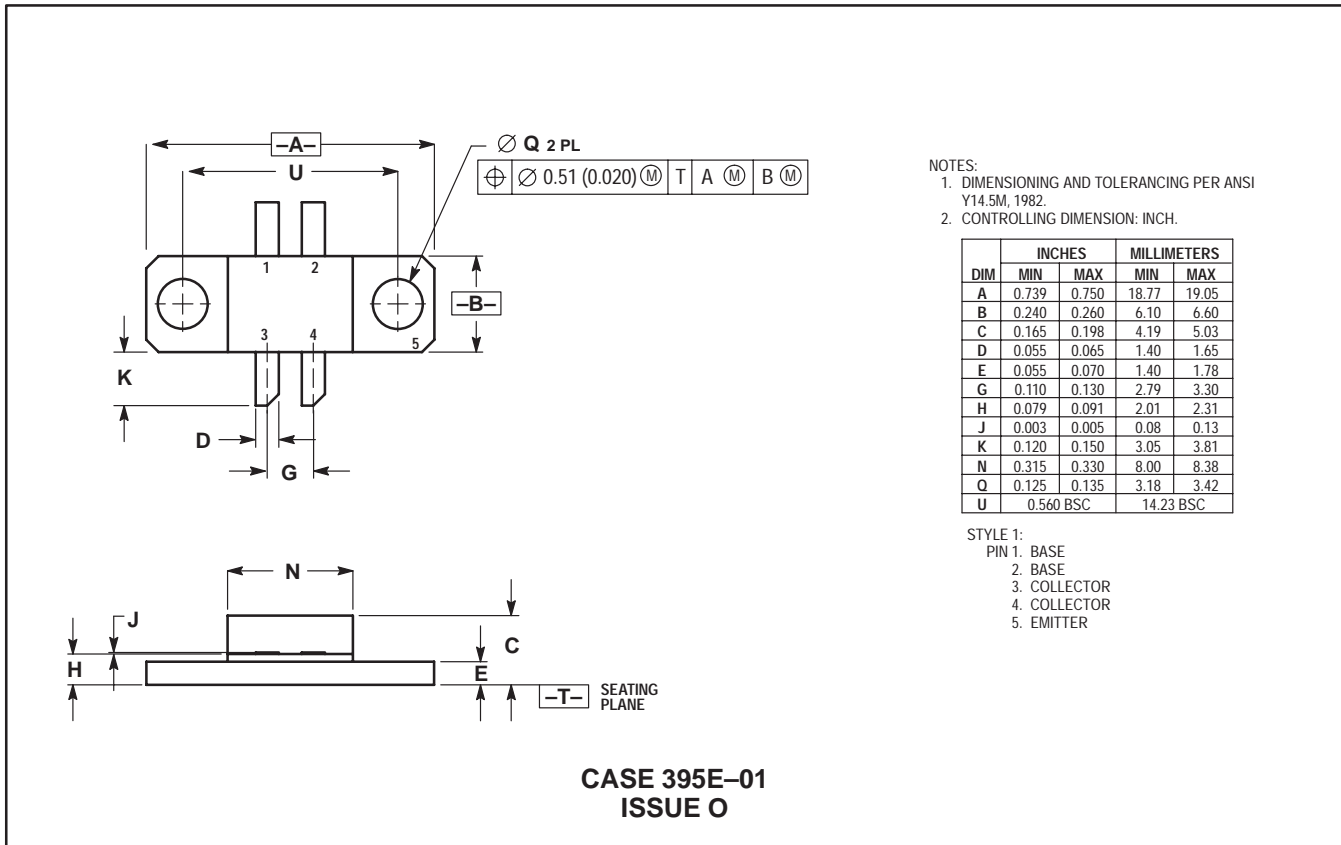


- NOTES:
 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.

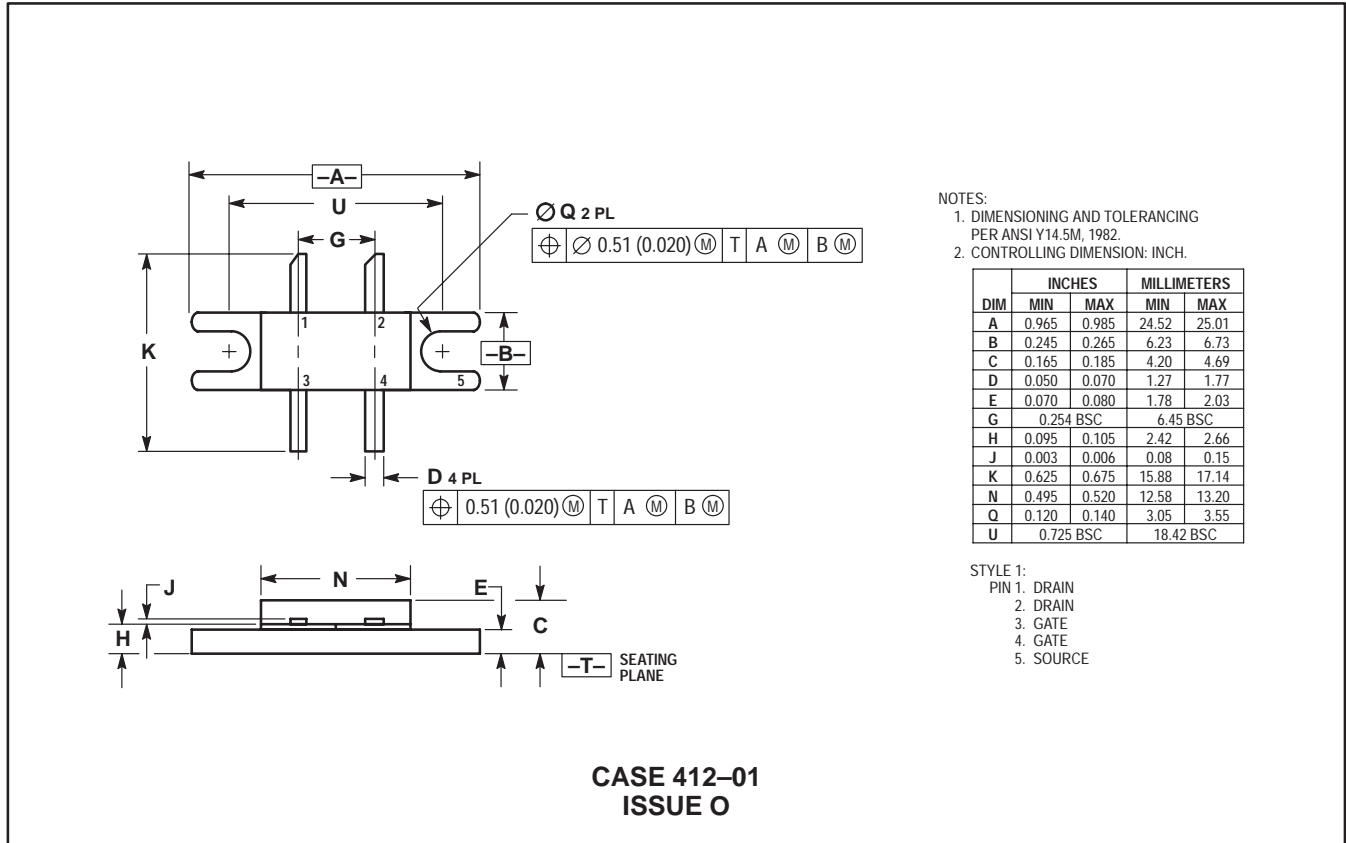
DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.739	0.750	18.77	19.05
B	0.240	0.260	6.10	6.60
C	0.165	0.198	4.19	5.03
D	0.215	0.225	5.46	5.72
E	0.055	0.070	1.40	1.78
H	0.079	0.091	2.01	2.31
J	0.004	0.006	0.10	0.15
K	0.210	0.240	5.33	6.10
N	0.315	0.330	8.00	8.38
Q	0.125	0.135	3.18	3.42
U	0.560 BSC		14.23 BSC	

- STYLE 1:
 PIN 1. BASE
 2. COLLECTOR
 3. EMITTER
- STYLE 2:
 PIN 1. EMITTER
 2. COLLECTOR
 3. BASE

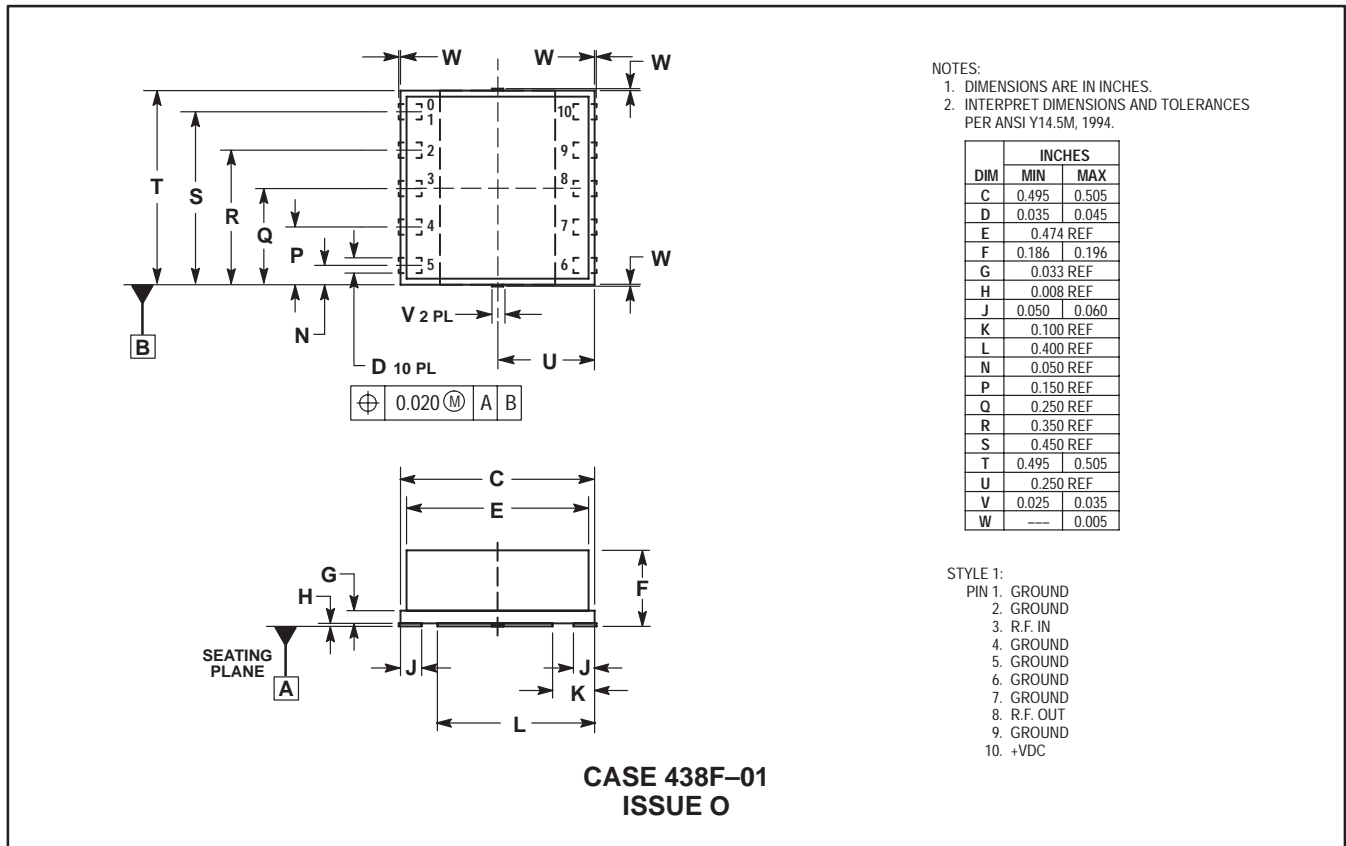
CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

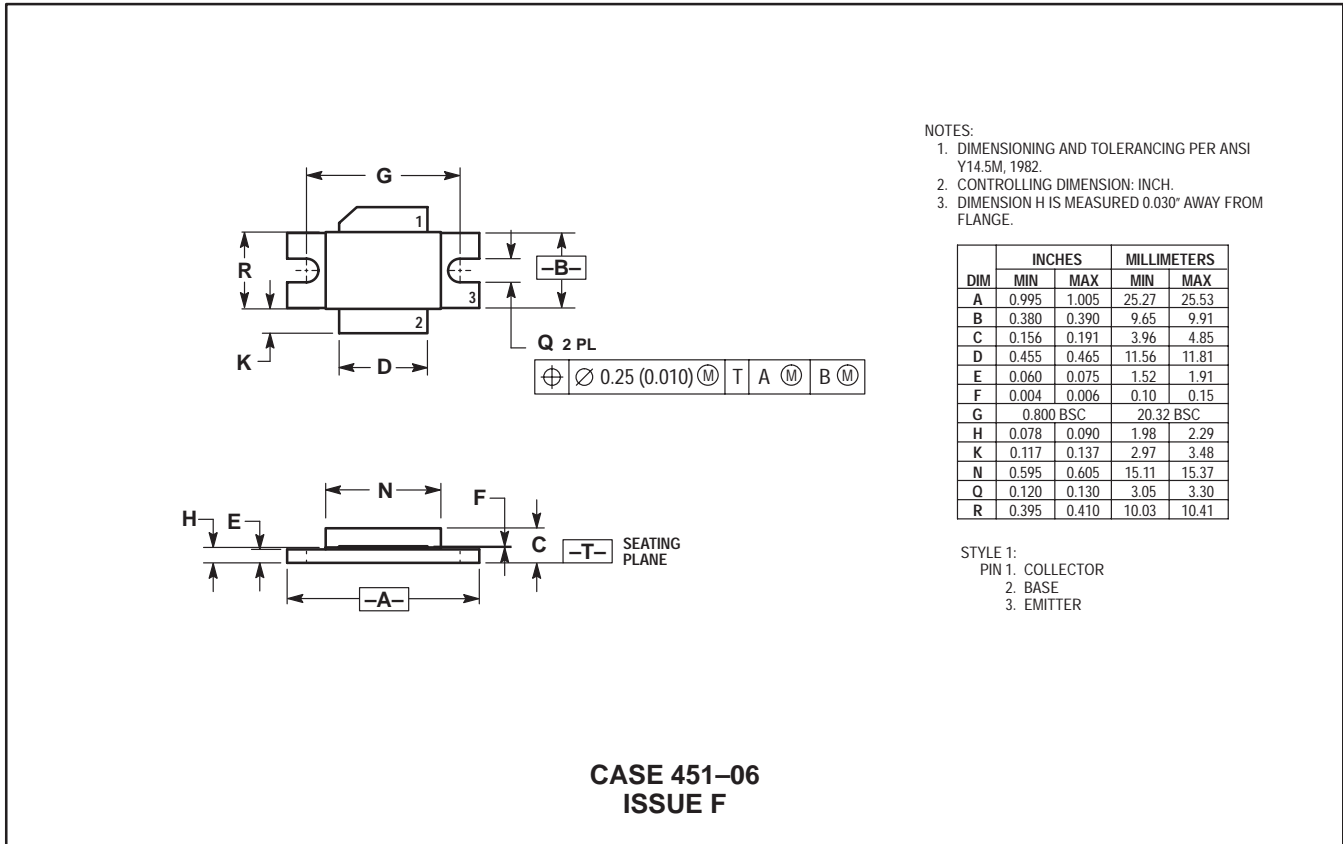
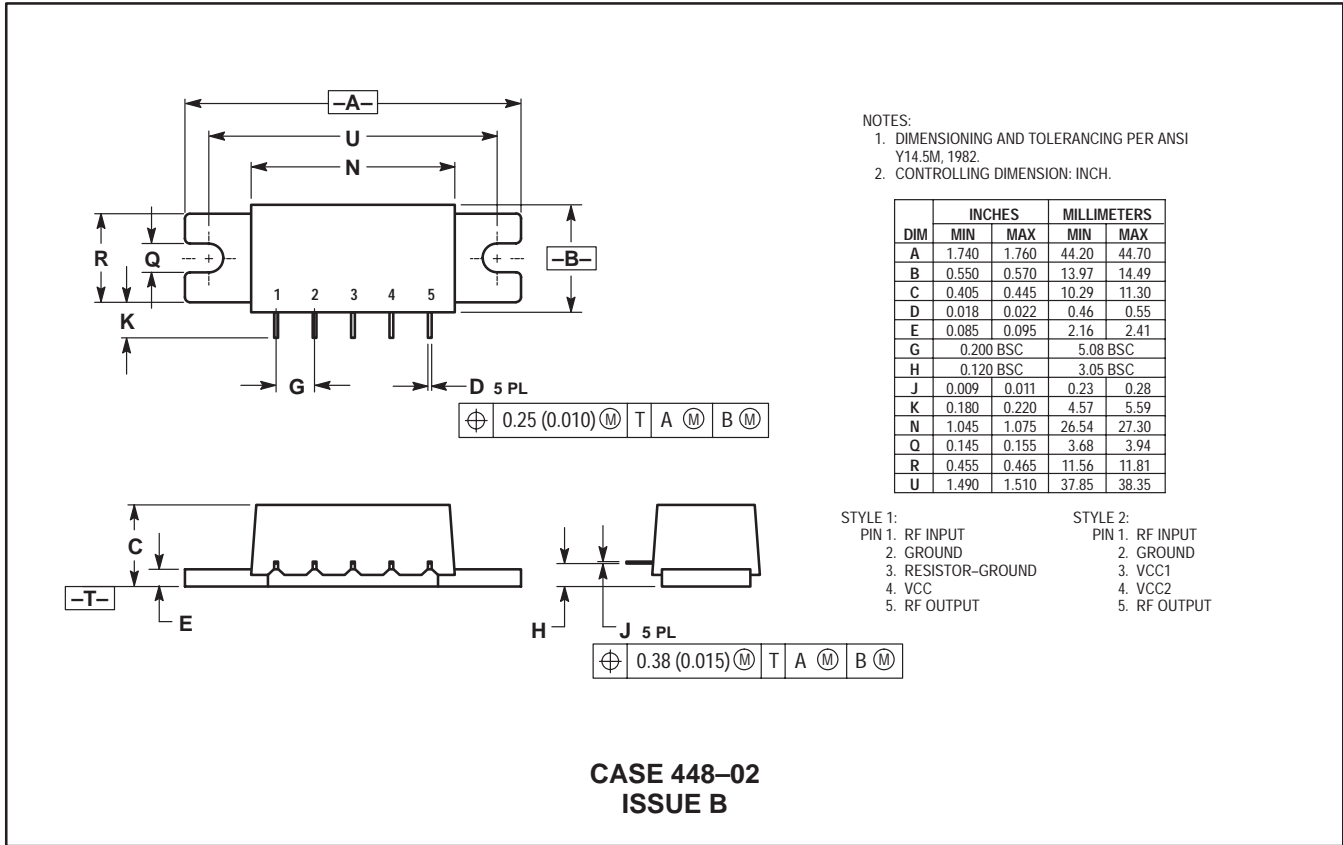


CASE 412-01
ISSUE O

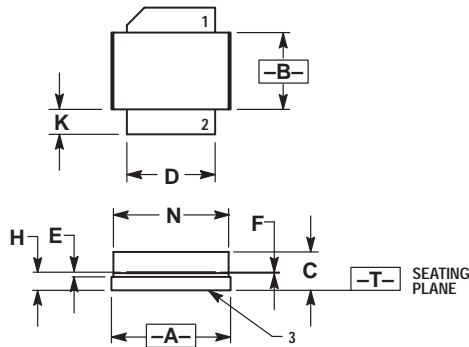


CASE 438F-01
ISSUE O

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)



NOTES:

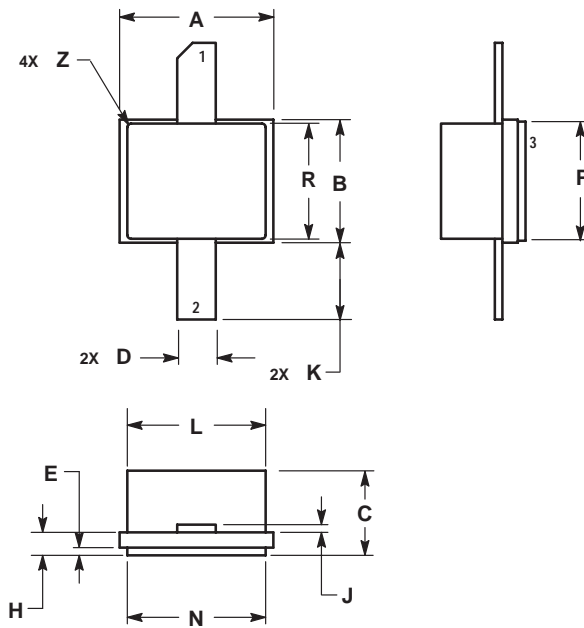
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: INCH.
3. DIMENSION H IS MEASURED 0.030° AWAY FROM FLANGE.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.615	0.625	15.62	15.88
B	0.395	0.410	10.03	10.41
C	0.156	0.191	3.96	4.85
D	0.455	0.465	11.56	11.81
E	0.060	0.075	1.52	1.91
F	0.004	0.006	0.10	0.15
H	0.078	0.090	1.98	2.29
K	0.117	0.137	2.97	3.48
N	0.595	0.605	15.11	15.37

STYLE 1:

- PIN 1. COLLECTOR
- BASE
- EMITTER

CASE 451A-03
ISSUE B



NOTES:

1. CONTROLLING DIMENSIONS: INCHES.
2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
3. ALL DIMENSIONS ARE SYMMETRICAL ABOUT CENTERLINE UNLESS OTHERWISE NOTED.

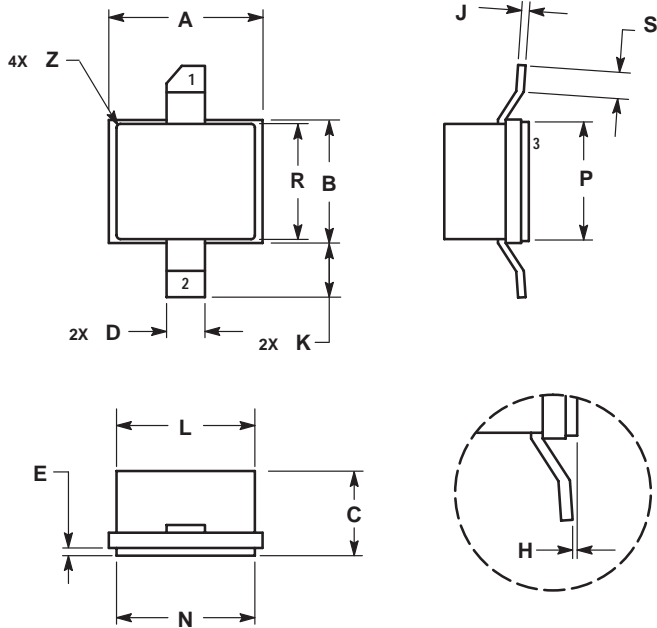
DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.197	0.203	5.004	5.156
B	0.157	0.163	3.988	4.140
C	0.085	0.110	2.159	2.794
D	0.047	0.053	1.194	1.346
E	0.004	0.010	0.102	0.254
H	0.025	0.031	0.635	0.787
J	0.004	0.010	0.102	0.254
K	0.060	0.110	1.524	2.794
L	0.177	0.183	4.496	4.648
N	0.180	0.200	4.572	5.080
P	0.140	0.160	3.556	4.064
R	0.147	0.153	3.734	3.886
Z	---	0.020	---	0.508

STYLE 1:

- PIN 1. DRAIN
- GATE
- SOURCE

CASE 458B-02
ISSUE C
(Micro 200S)

CASE DIMENSIONS (continued)

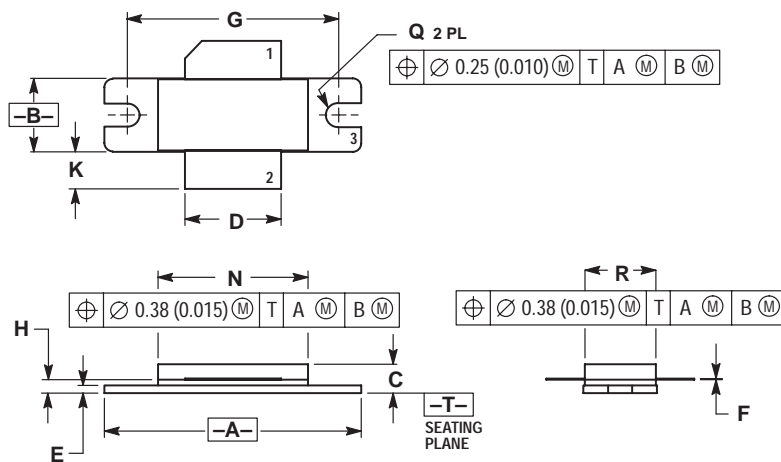


- NOTES:
1. CONTROLLING DIMENSIONS: INCHES.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
 3. DIMENSION H (PACKAGE COPLANARITY): THE BOTTOM OF LEADS AND REFERENCE PLANE T MUST BE COPLANAR WITHIN DIMENSION H.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.197	0.203	5.004	5.156
B	0.157	0.163	3.988	4.140
C	0.085	0.110	2.159	2.794
D	0.047	0.053	1.194	1.346
E	0.004	0.010	0.102	0.254
H	0.000	0.004	0.000	0.102
J	0.004	0.010	0.102	0.254
K	0.050	0.090	1.270	2.286
L	0.177	0.183	4.496	4.648
N	0.180	0.200	4.572	5.080
P	0.140	0.160	3.556	4.064
R	0.147	0.153	3.734	3.886
Z	---	0.020	---	0.508

- STYLE 1:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

CASE 458C-02
 ISSUE C
 (Micro 200Z)



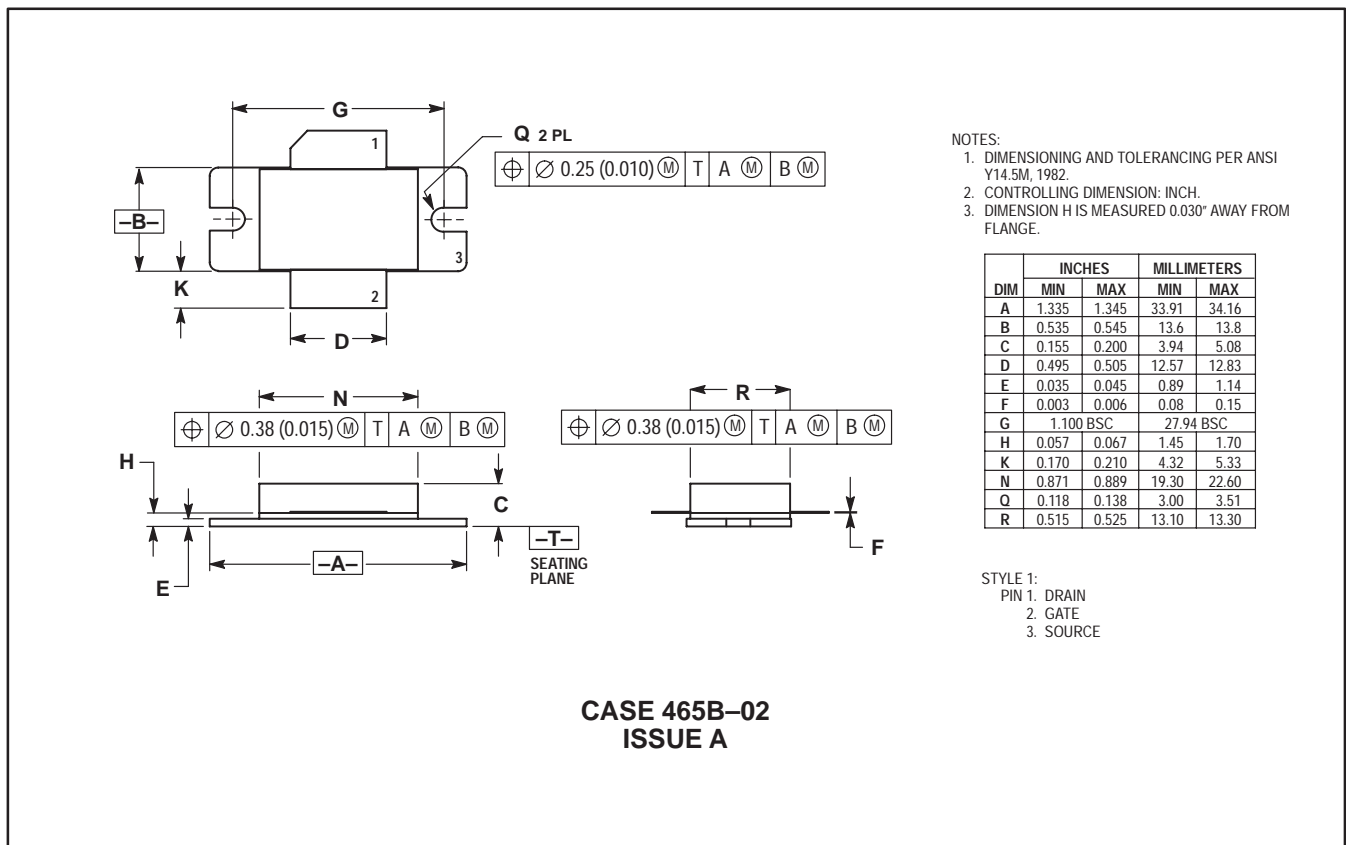
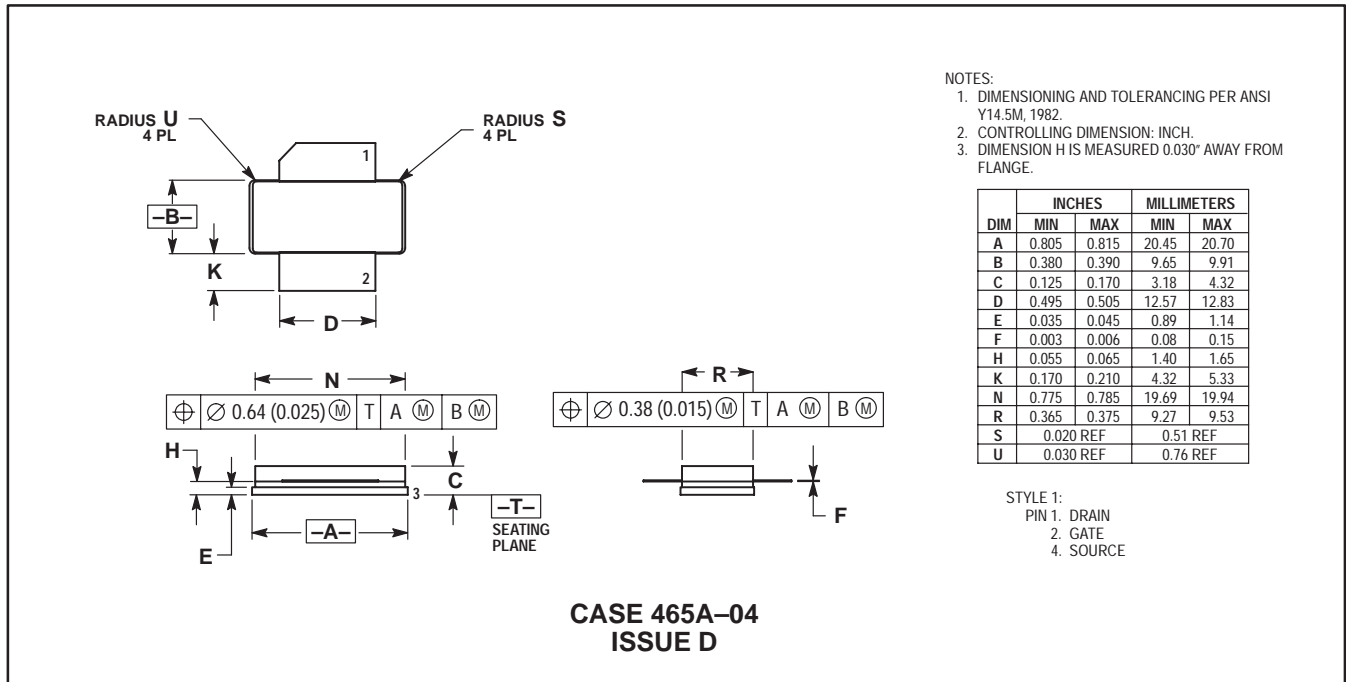
- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.
 3. DIMENSION H IS MEASURED 0.03" AWAY FROM FLANGE.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	1.335	1.345	33.91	34.16
B	0.380	0.390	9.65	9.91
C	0.125	0.170	3.18	4.32
D	0.495	0.505	12.57	12.83
E	0.035	0.045	0.89	1.14
F	0.003	0.006	0.08	0.15
G	1.100 BSC		27.94 BSC	
H	0.055	0.065	1.40	1.65
K	0.170	0.210	4.32	5.33
N	0.772	0.788	19.60	20.00
Q	0.118	0.138	3.00	3.51
R	0.365	0.375	9.27	9.53

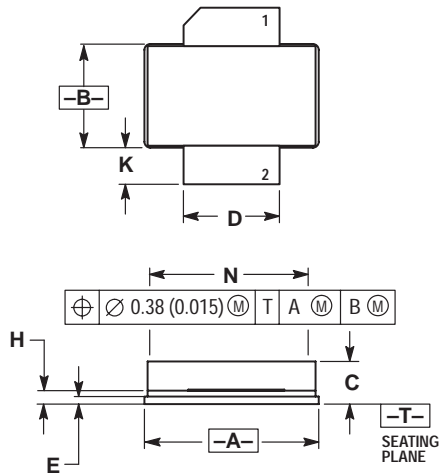
- STYLE 1:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

CASE 465-04
 ISSUE D

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

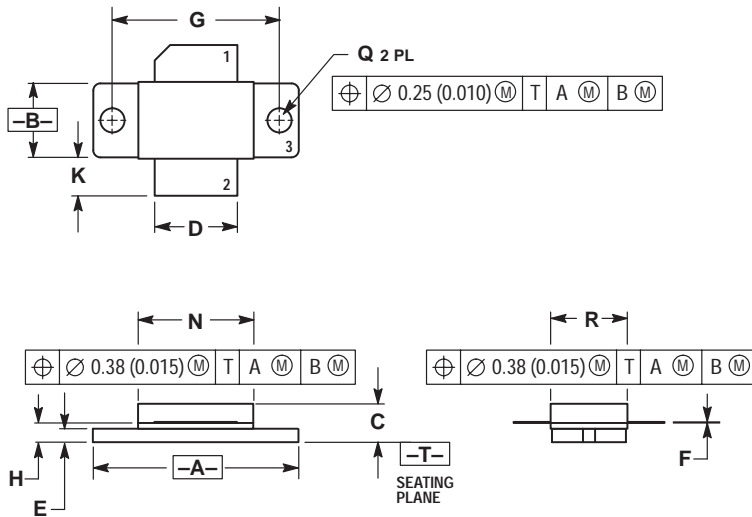


- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.
 3. DIMENSION H IS MEASURED 0.030" AWAY FROM FLANGE.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.905	0.915	22.99	23.24
B	0.535	0.545	13.6	13.8
C	0.155	0.200	3.94	5.08
D	0.495	0.505	12.57	12.83
E	0.035	0.045	0.89	1.14
F	0.003	0.006	0.08	0.15
H	0.057	0.067	1.45	1.70
K	0.170	0.210	4.32	5.33
N	0.871	0.889	19.30	22.60
R	0.515	0.525	13.10	13.30

- STYLE 1:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

CASE 465C-01
 ISSUE O



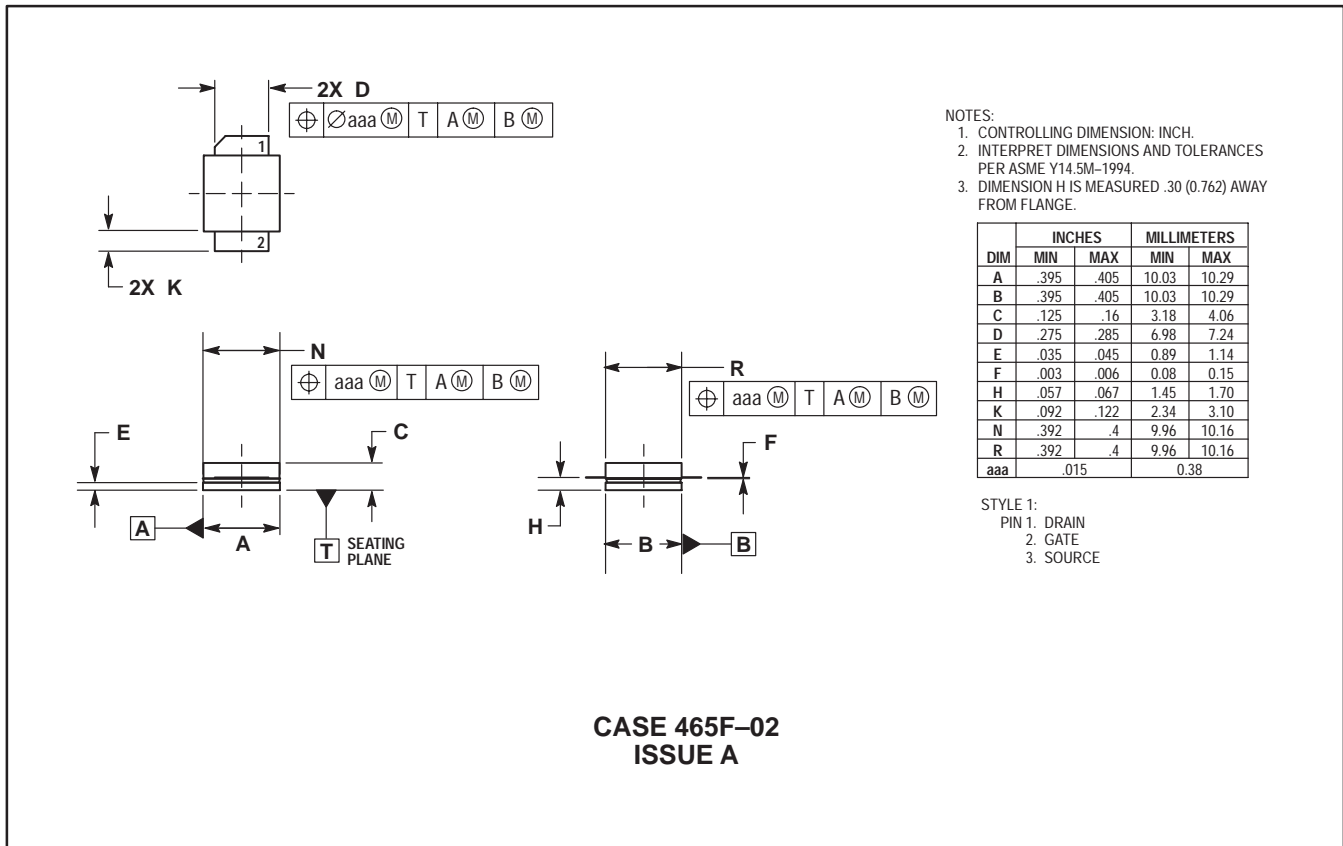
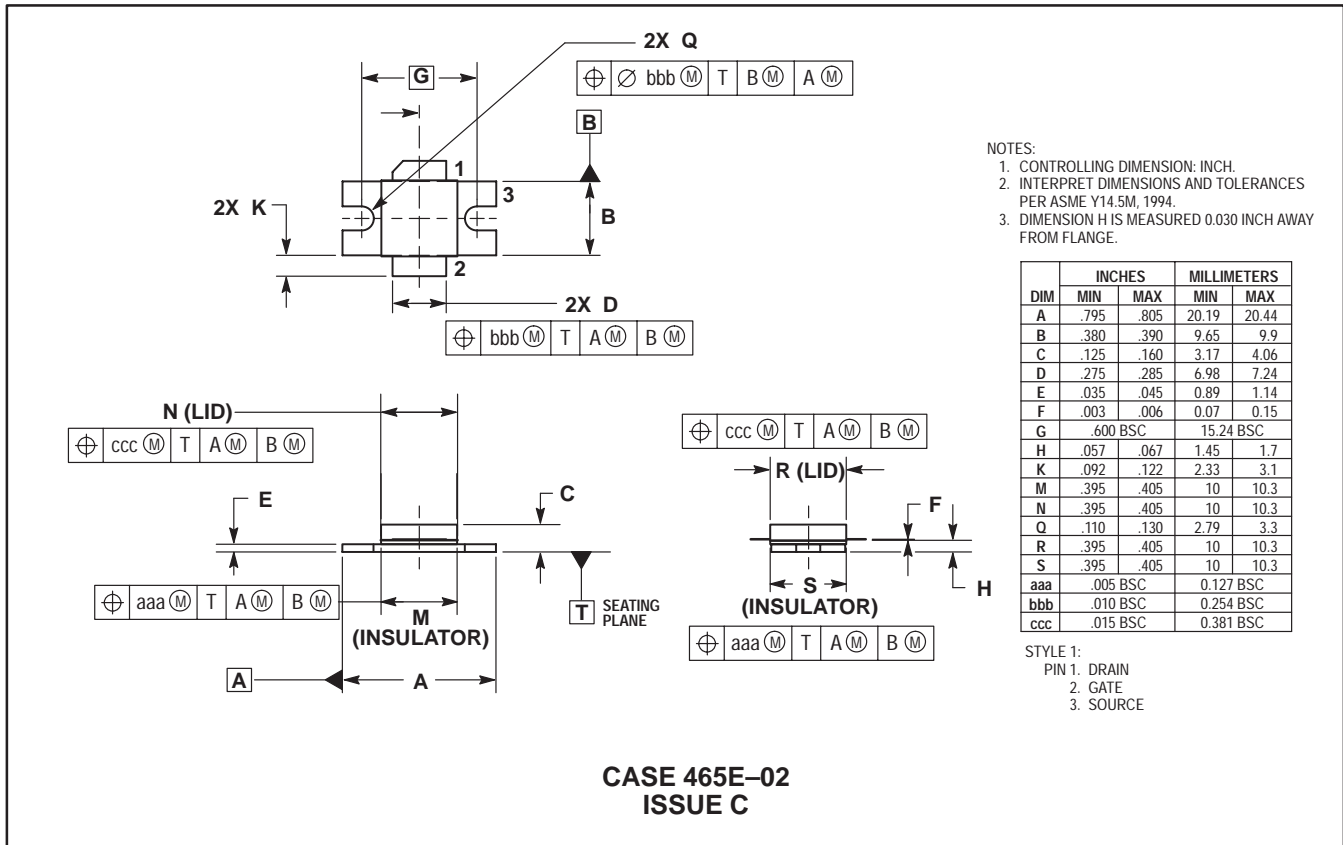
- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: INCH.
 3. DIMENSION H IS MEASURED 0.030" AWAY FROM FLANGE.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	1.065	1.075	27.05	27.31
B	0.380	0.390	9.65	9.91
C	0.160	0.205	4.06	5.21
D	0.425	0.435	10.80	11.05
E	0.060	0.070	1.52	1.78
F	0.004	0.006	0.10	0.15
G	0.870	BSC	22.10	BSC
H	0.096	0.106	2.44	2.70
K	0.185	0.215	4.70	5.46
N	0.591	0.601	15.01	15.27
Q	0.124	0.130	3.15	3.30
R	0.392	0.404	9.96	10.26

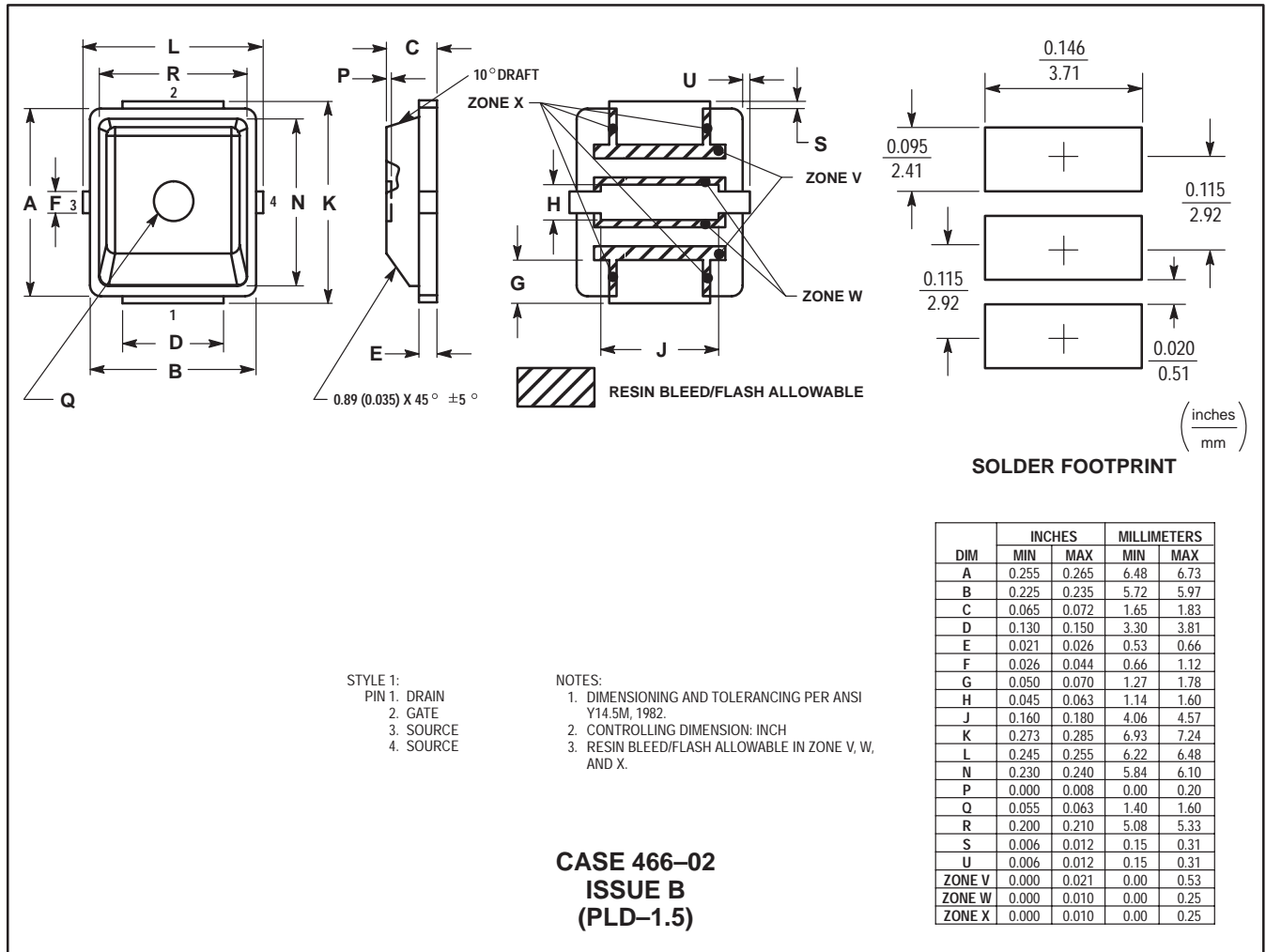
- STYLE 1:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

CASE 465D-02
 ISSUE A

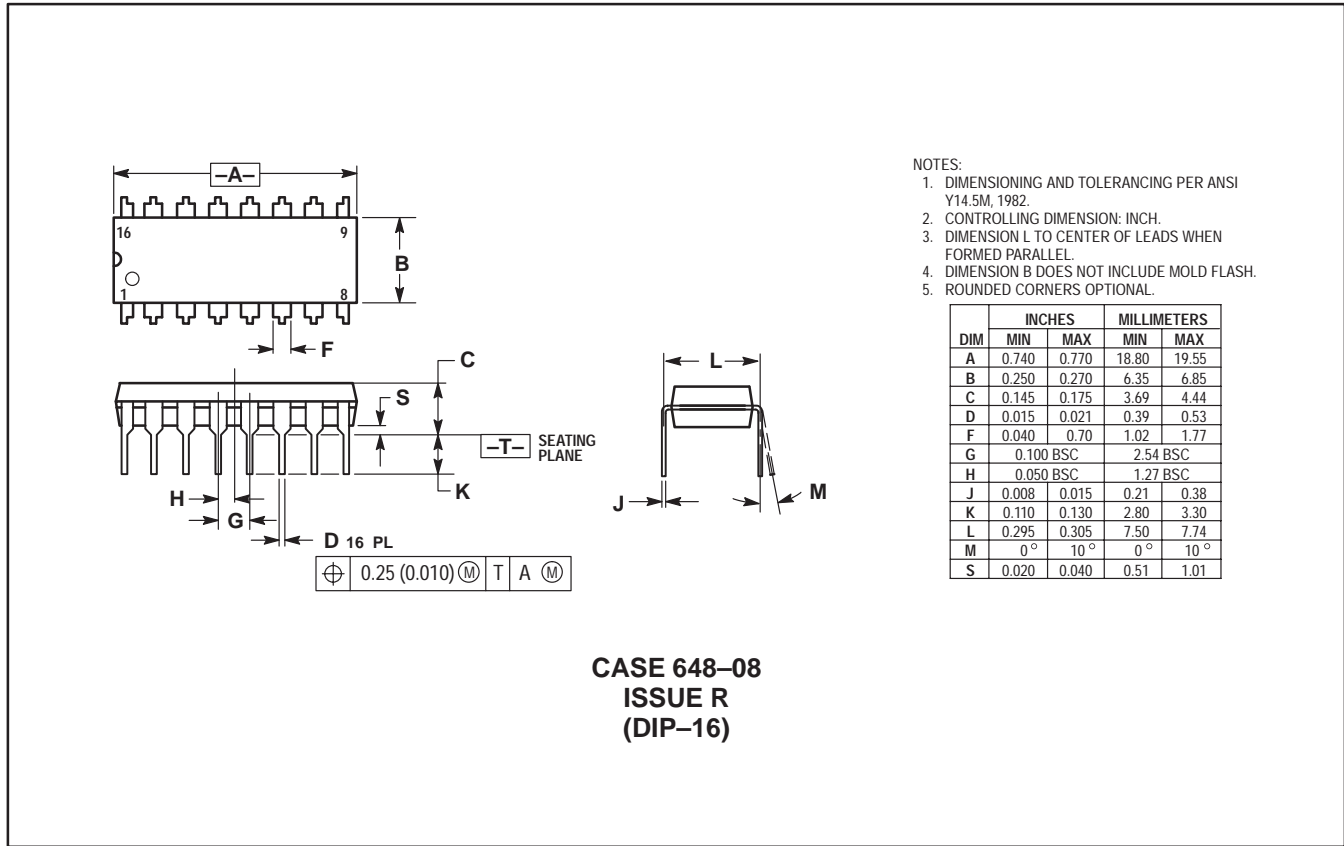
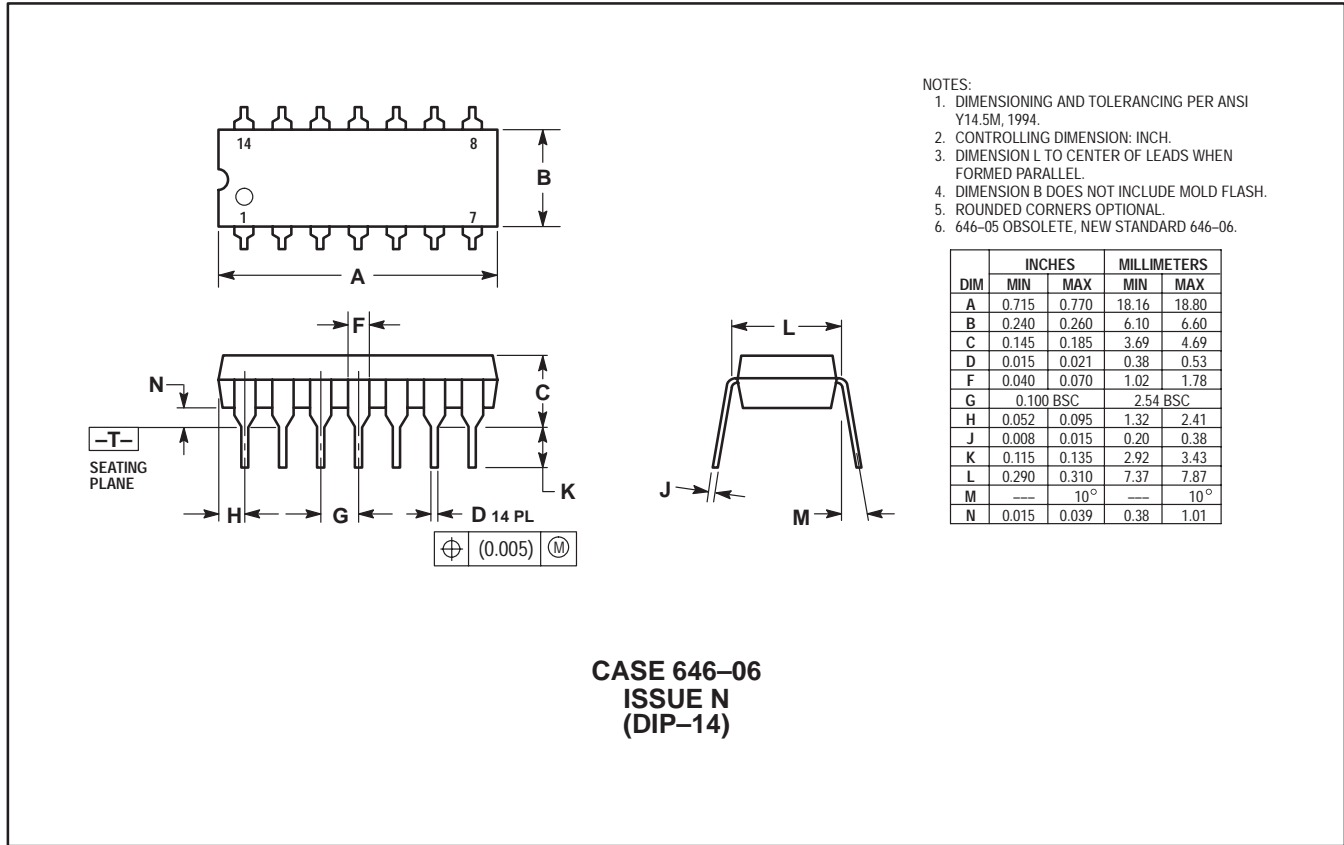
CASE DIMENSIONS (continued)



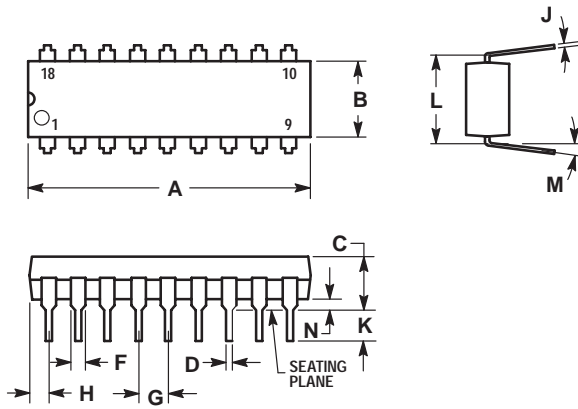
CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)



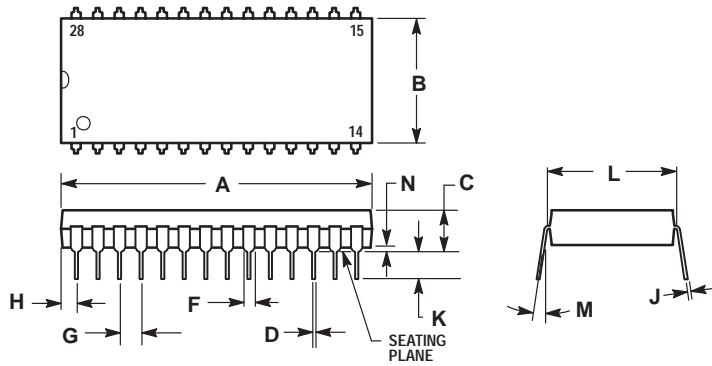
NOTES:

1. POSITIONAL TOLERANCE OF LEADS (D), SHALL BE WITHIN 0.25 (0.010) AT MAXIMUM MATERIAL CONDITION, IN RELATION TO SEATING PLANE AND EACH OTHER.
2. DIMENSION L TO CENTER OF LEADS WHEN FORMED PARALLEL.
3. DIMENSION B DOES NOT INCLUDE MOLD FLASH.
4. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.875	0.915	22.22	23.24
B	0.240	0.260	6.10	6.60
C	0.140	0.180	3.56	4.57
D	0.014	0.022	0.36	0.56
F	0.050	0.070	1.27	1.78
G	0.100 BSC		2.54 BSC	
H	0.040	0.060	1.02	1.52
J	0.008	0.012	0.20	0.30
K	0.115	0.135	2.92	3.43
L	0.300 BSC		7.62 BSC	
M	0°	15°	0°	15°
N	0.020	0.040	0.51	1.02

CASE 707-02
ISSUE C
(DIP-18)

CASE DIMENSIONS (continued)

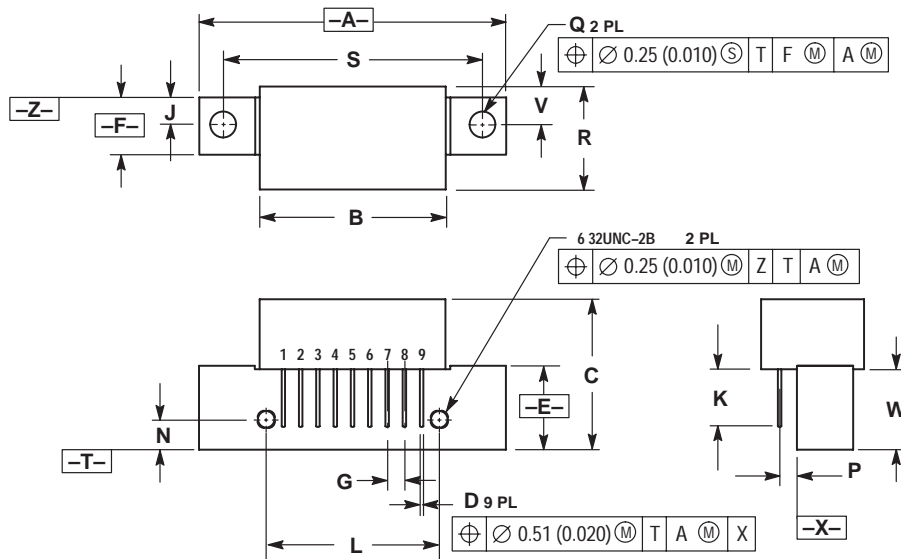


NOTES:

1. POSITIONAL TOLERANCE OF LEADS (D), SHALL BE WITHIN 0.25 (0.010) AT MAXIMUM MATERIAL CONDITION, IN RELATION TO SEATING PLANE AND EACH OTHER.
2. DIMENSION L TO CENTER OF LEADS WHEN FORMED PARALLEL.
3. DIMENSION B DOES NOT INCLUDE MOLD FLASH.
4. CONTROLLING DIMENSION: INCH.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	1.435	1.465	36.45	37.21
B	0.540	0.560	13.72	14.22
C	0.155	0.200	3.94	5.08
D	0.014	0.022	0.36	0.56
F	0.040	0.060	1.02	1.52
G	0.100 BSC		2.54 BSC	
H	0.065	0.085	1.65	2.16
J	0.008	0.015	0.20	0.38
K	0.115	0.135	2.92	3.43
L	0.600 BSC		15.24 BSC	
M	0°	15°	0°	15°
N	0.020	0.040	0.51	1.02

CASE 710-02
ISSUE B
(DIP-28)



NOTES:

1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: INCH.

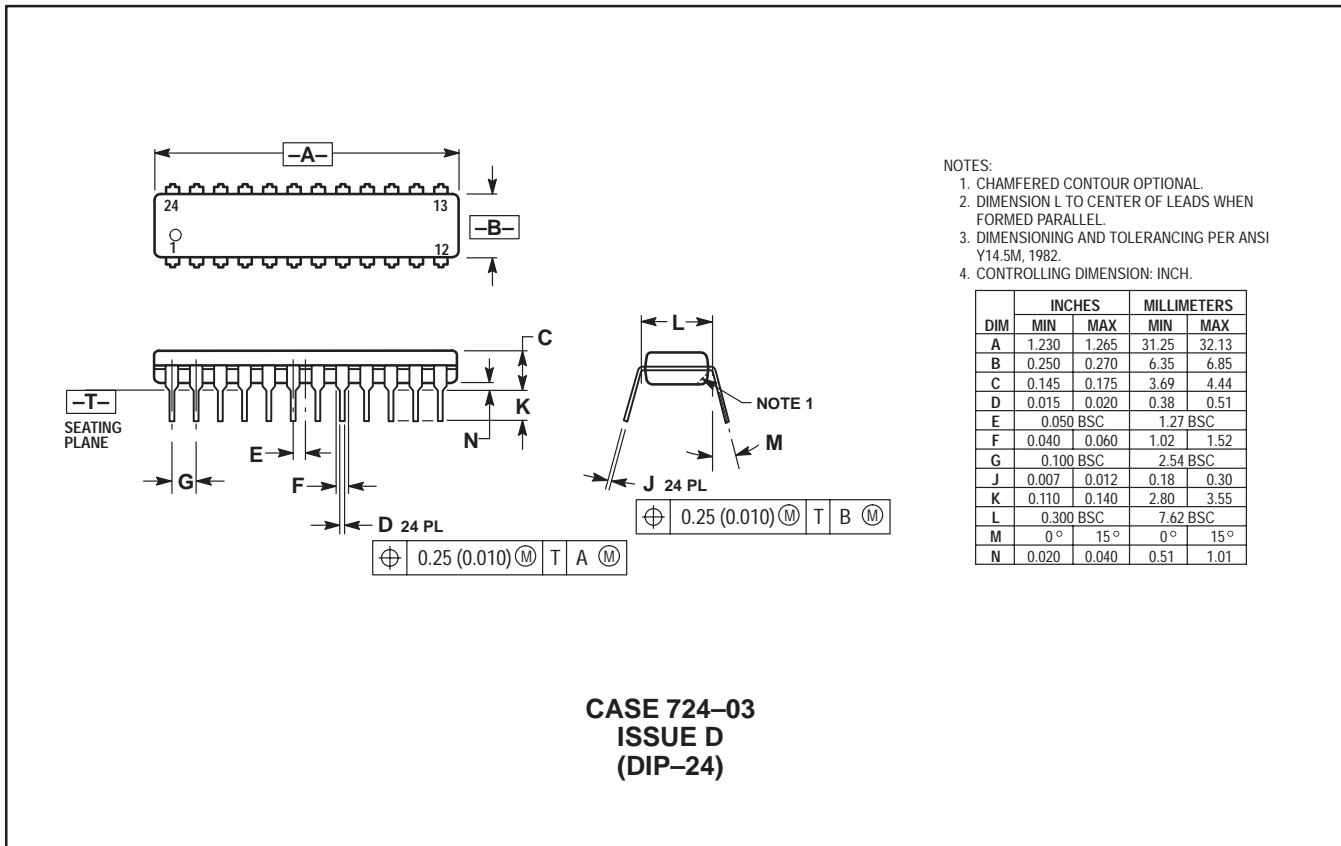
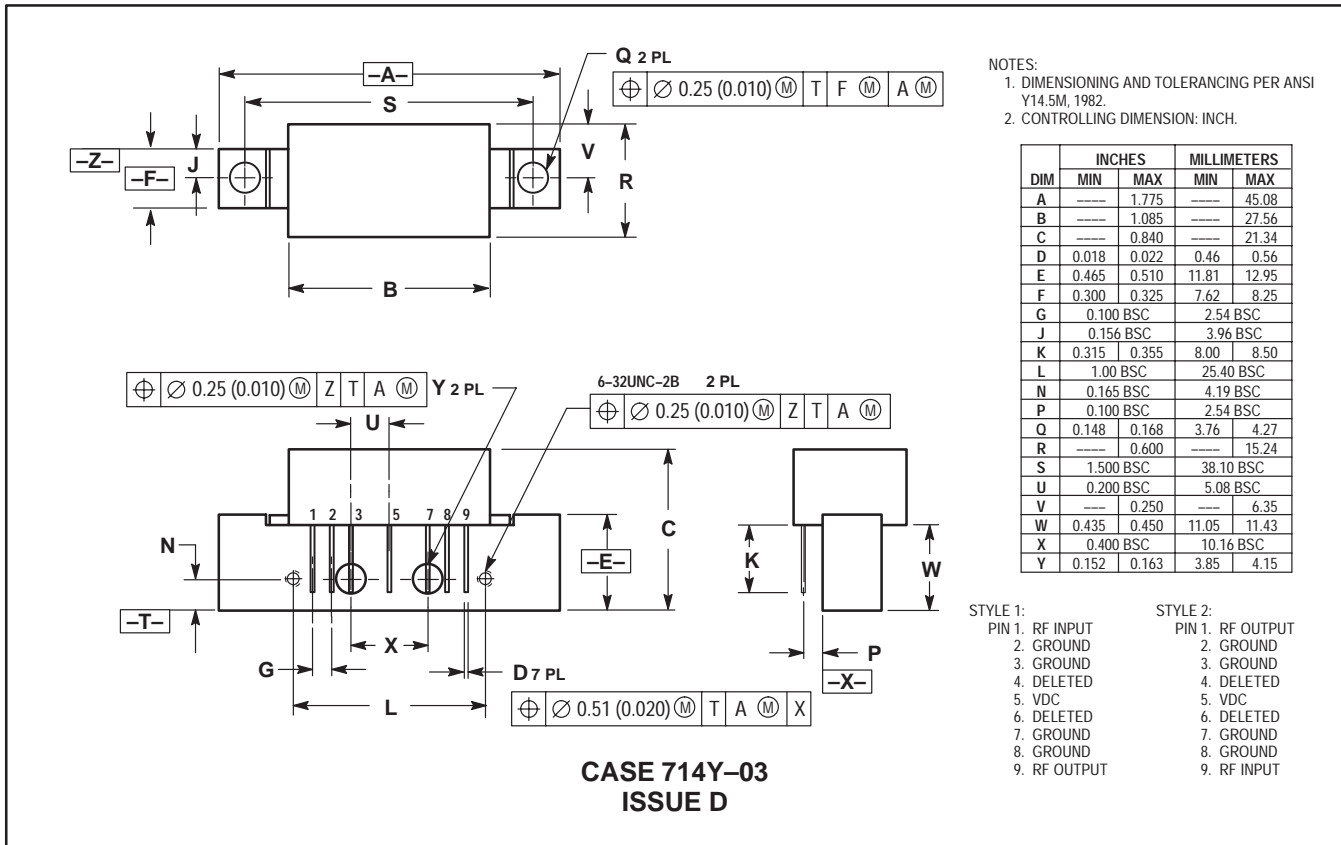
DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	---	1.775	---	45.08
B	---	1.085	---	27.56
C	---	0.870	---	22.10
D	0.018	0.022	0.46	0.56
E	0.465	0.510	11.81	12.95
F	0.300	0.325	7.62	8.25
G	0.100 BSC		2.54 BSC	
J	0.156 BSC		3.96 BSC	
K	0.330	0.370	8.38	9.40
L	1.000 BSC		25.40 BSC	
N	0.165 BSC		4.19 BSC	
P	0.100 BSC		2.54 BSC	
Q	0.148	0.168	3.76	4.27
R	---	0.595	---	15.11
S	1.500 BSC		38.10 BSC	
V	0.209	0.239	5.31	6.07
W	0.425	---	10.80	---

STYLE 2:

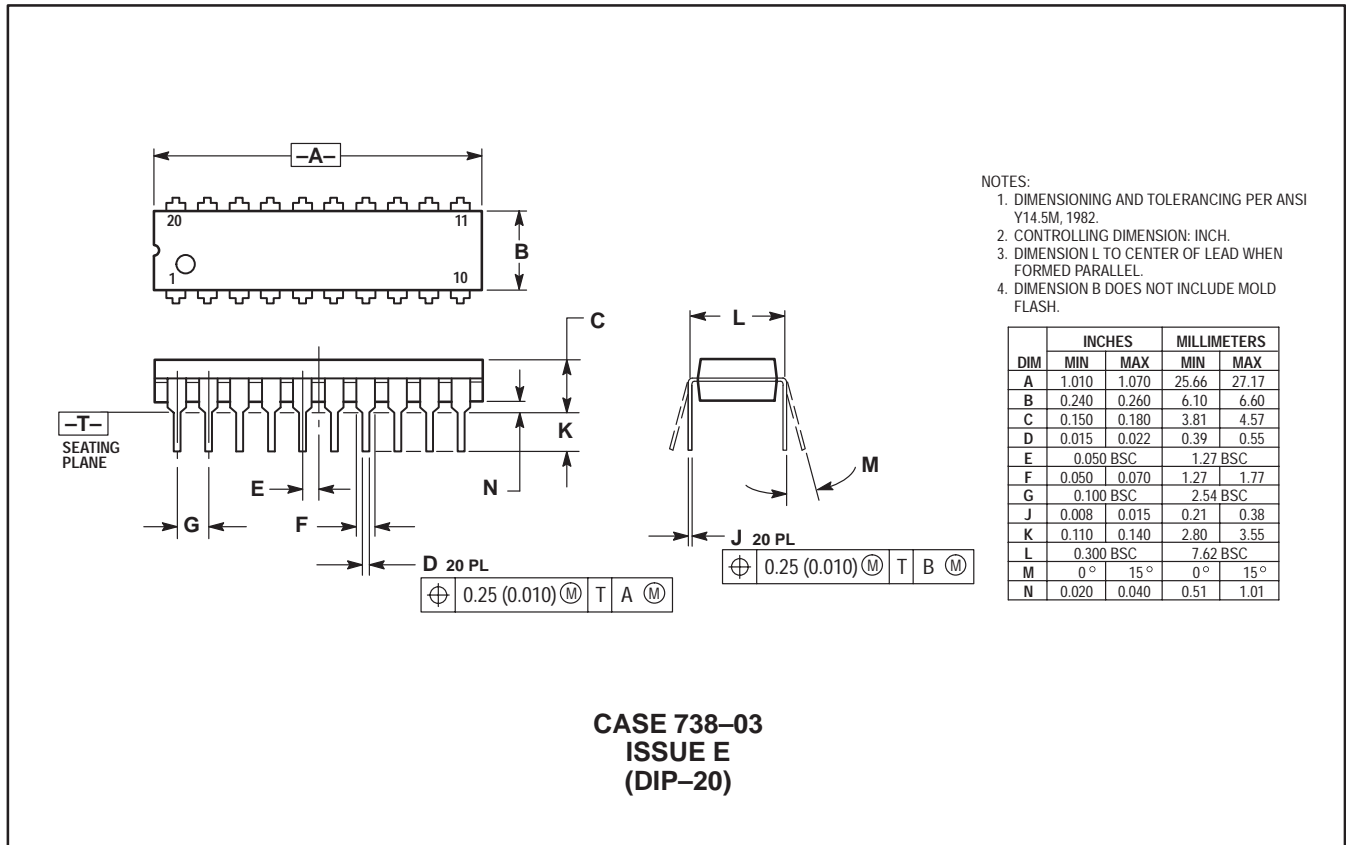
- PIN 1: RF INPUT
 2: GROUND
 3: GROUND
 4: RESISTOR-GROUND
 5: GROUND
 6: GROUND
 7: GROUND
 8: V_{CC} 1
 9: RF OUTPUT

CASE 714P-03
ISSUE B

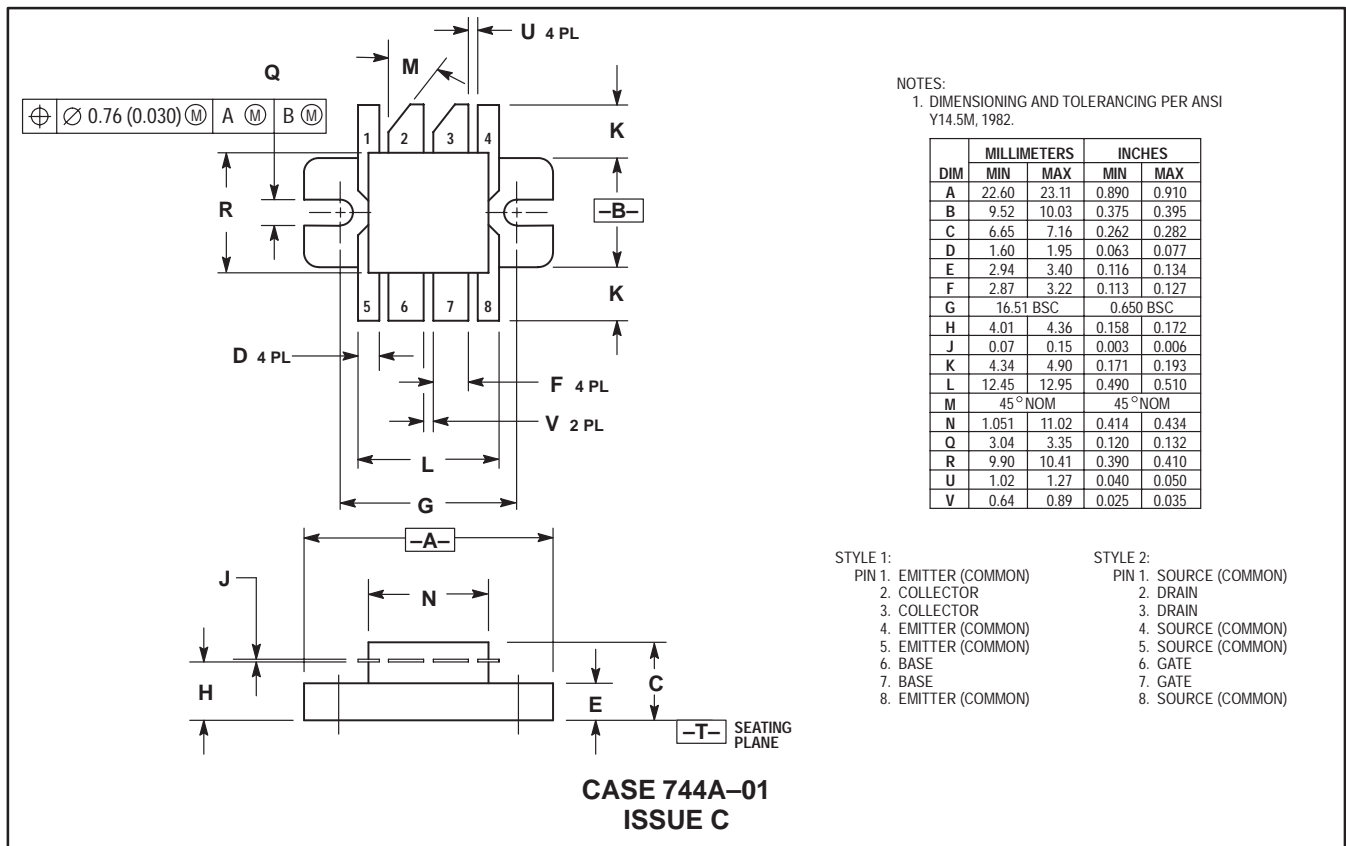
CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

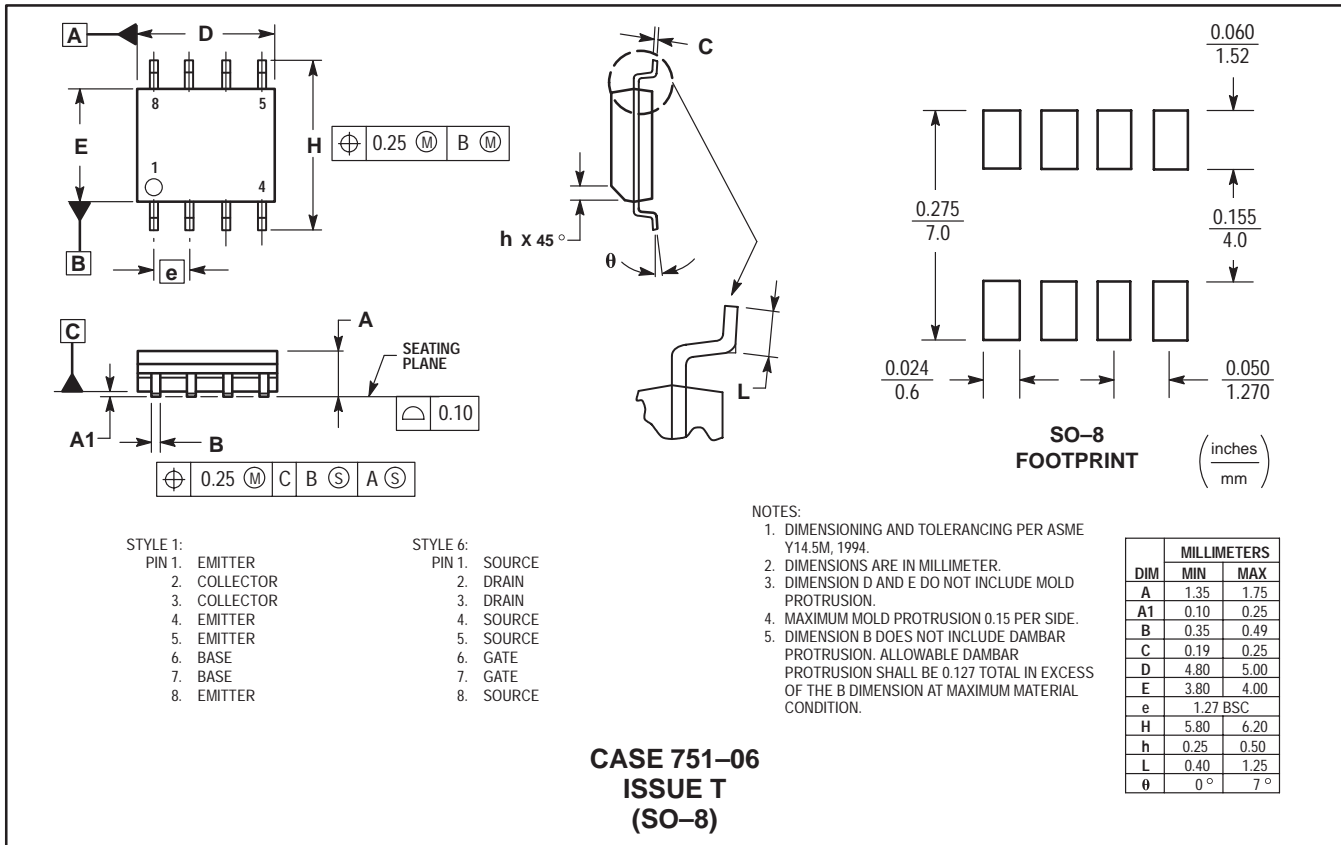


**CASE 738-03
ISSUE E
(DIP-20)**

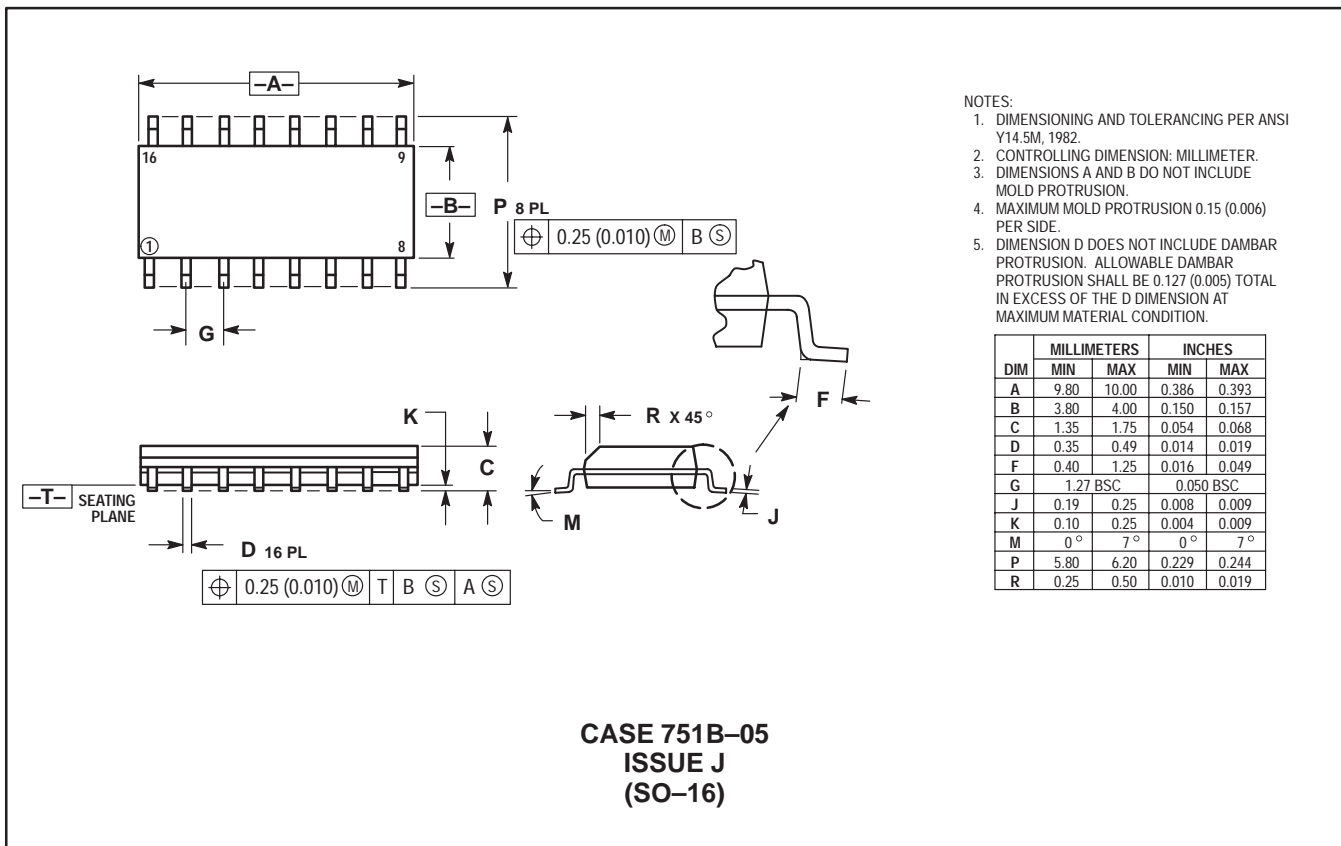


**CASE 744A-01
ISSUE C**

CASE DIMENSIONS (continued)

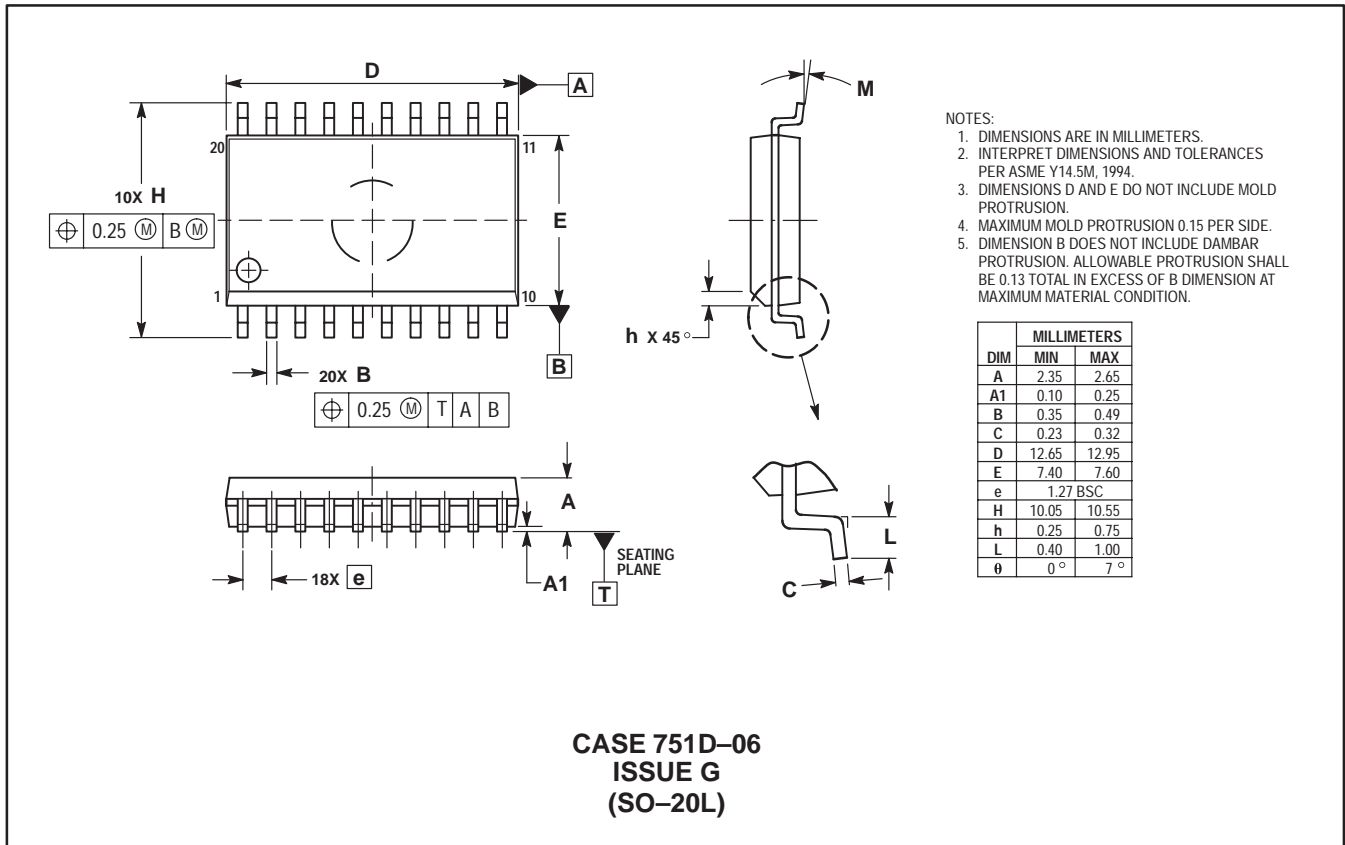


CASE 751-06
ISSUE T
(SO-8)

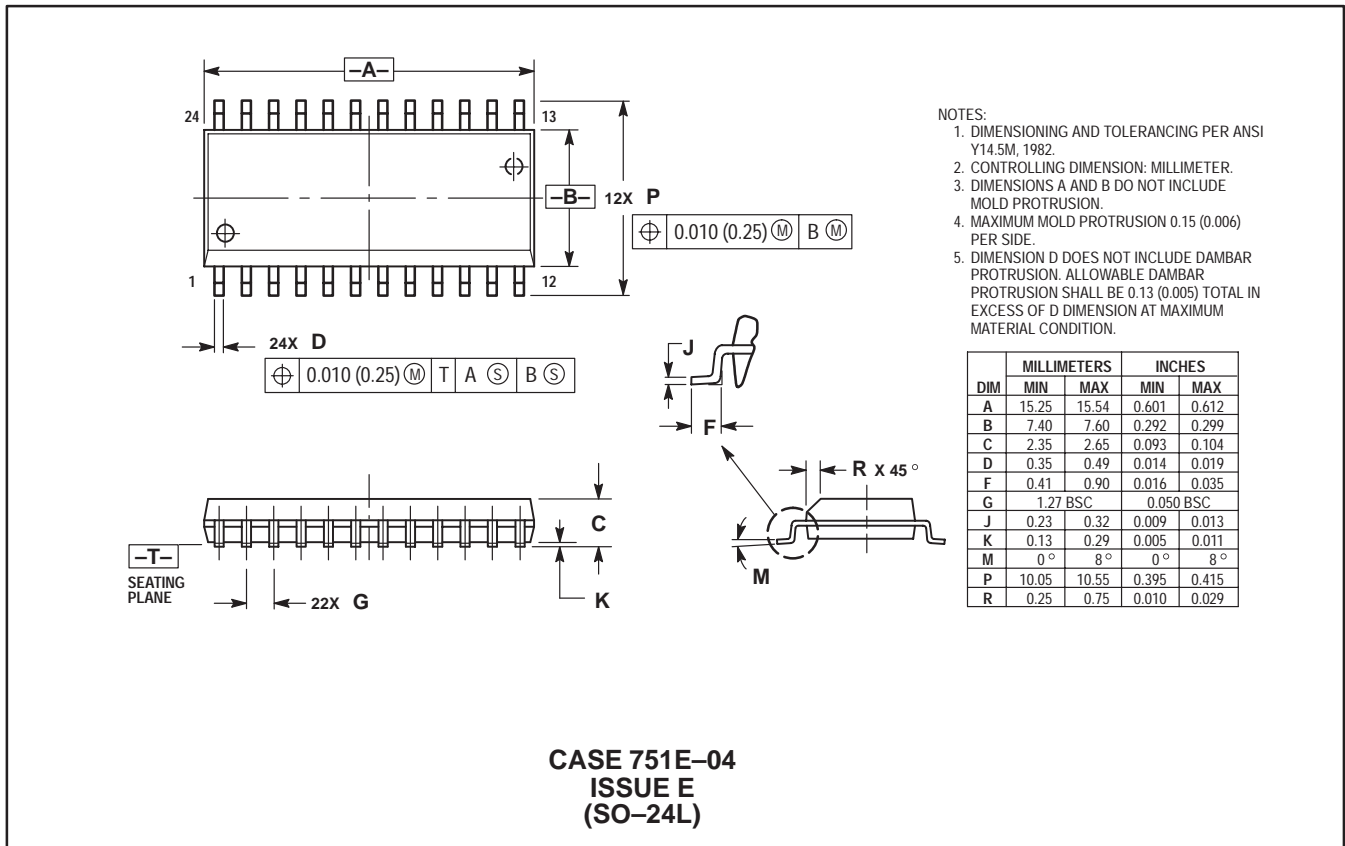


CASE 751B-05
ISSUE J
(SO-16)

CASE DIMENSIONS (continued)

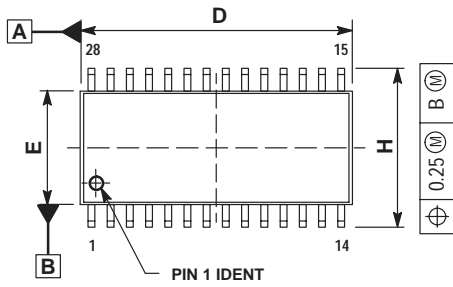


**CASE 751D-06
ISSUE G
(SO-20L)**



**CASE 751E-04
ISSUE E
(SO-24L)**

CASE DIMENSIONS (continued)

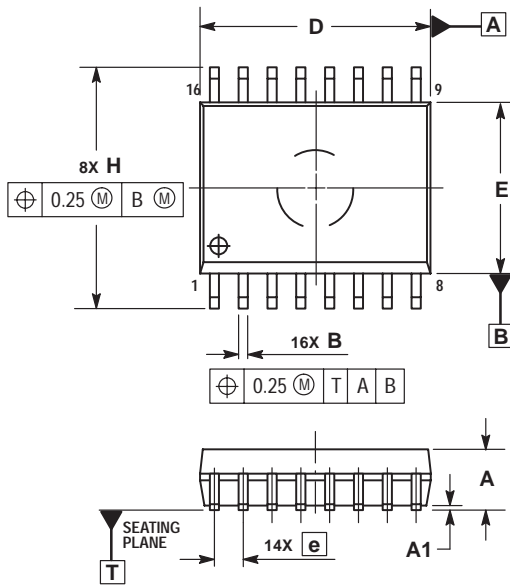


NOTES:

1. DIMENSIONS ARE IN MILLIMETERS.
2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
3. DIMENSIONS D AND E DO NOT INCLUDE MOLD PROTRUSIONS.
4. MAXIMUM MOLD PROTRUSION 0.015 PER SIDE.
5. DIMENSION B DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.13 TOTAL IN EXCESS OF B DIMENSION AT MAXIMUM MATERIAL CONDITION.

MILLIMETERS		
DIM	MIN	MAX
A	2.35	2.65
A1	0.13	0.29
B	0.35	0.49
C	0.23	0.32
D	17.80	18.05
E	7.40	7.60
e	1.27 BSC	
H	10.05	10.55
L	0.41	0.90
θ	0°	8°

CASE 751F-05
ISSUE F
(SO-28L)



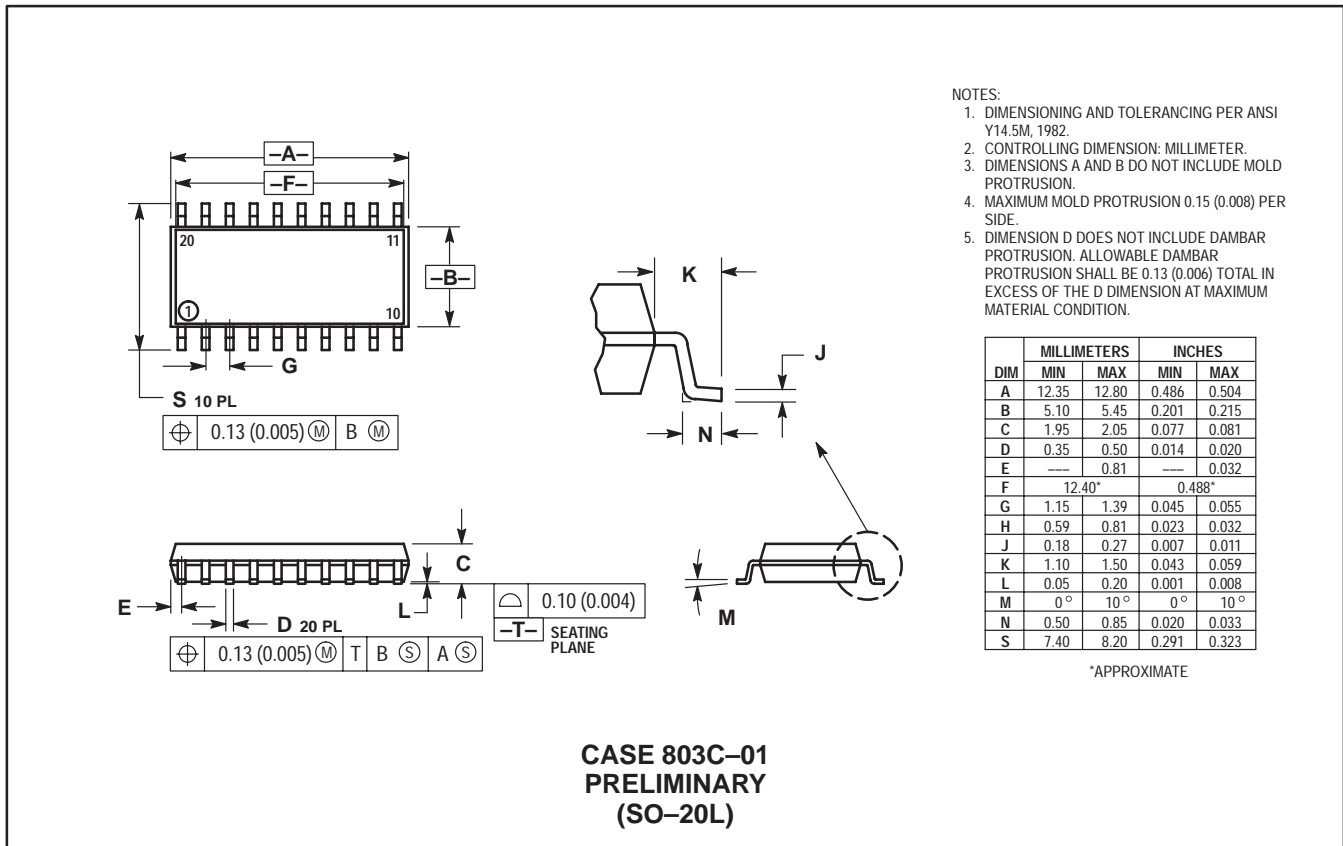
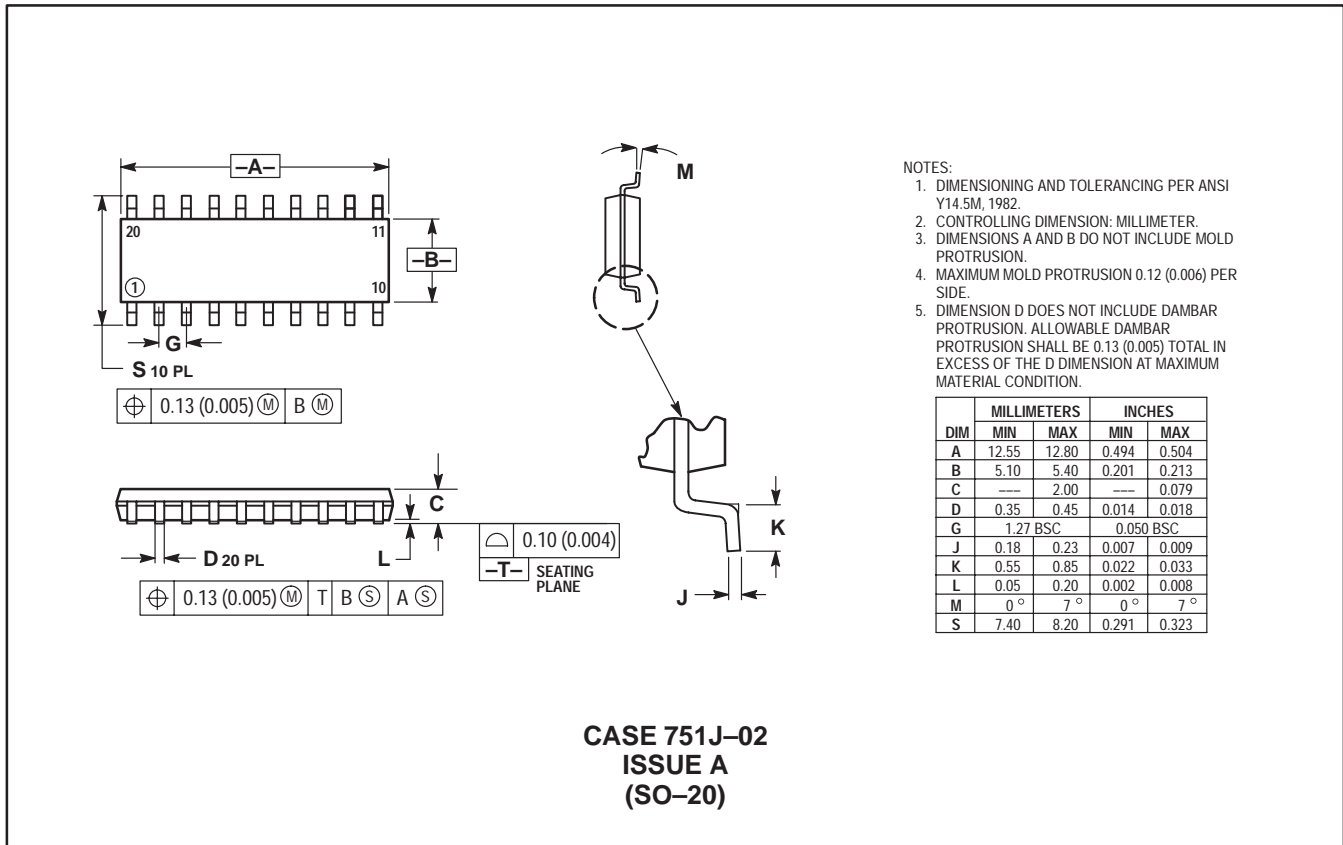
NOTES:

1. DIMENSIONS ARE IN MILLIMETERS.
2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
3. DIMENSIONS D AND E DO NOT INCLUDE MOLD PROTRUSION.
4. MAXIMUM MOLD PROTRUSION 0.15 PER SIDE.
5. DIMENSION B DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.13 TOTAL IN EXCESS OF THE B DIMENSION AT MAXIMUM MATERIAL CONDITION.

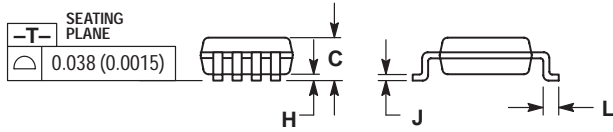
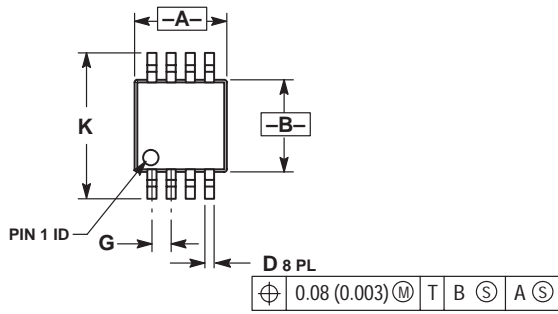
MILLIMETERS		
DIM	MIN	MAX
A	2.35	2.65
A1	0.10	0.25
B	0.35	0.49
C	0.23	0.32
D	10.15	10.45
E	7.40	7.60
e	1.27 BSC	
H	10.05	10.55
h	0.25	0.75
L	0.40	1.00
M	0°	7°

CASE 751G-04
ISSUE C
(SO-16W)

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)



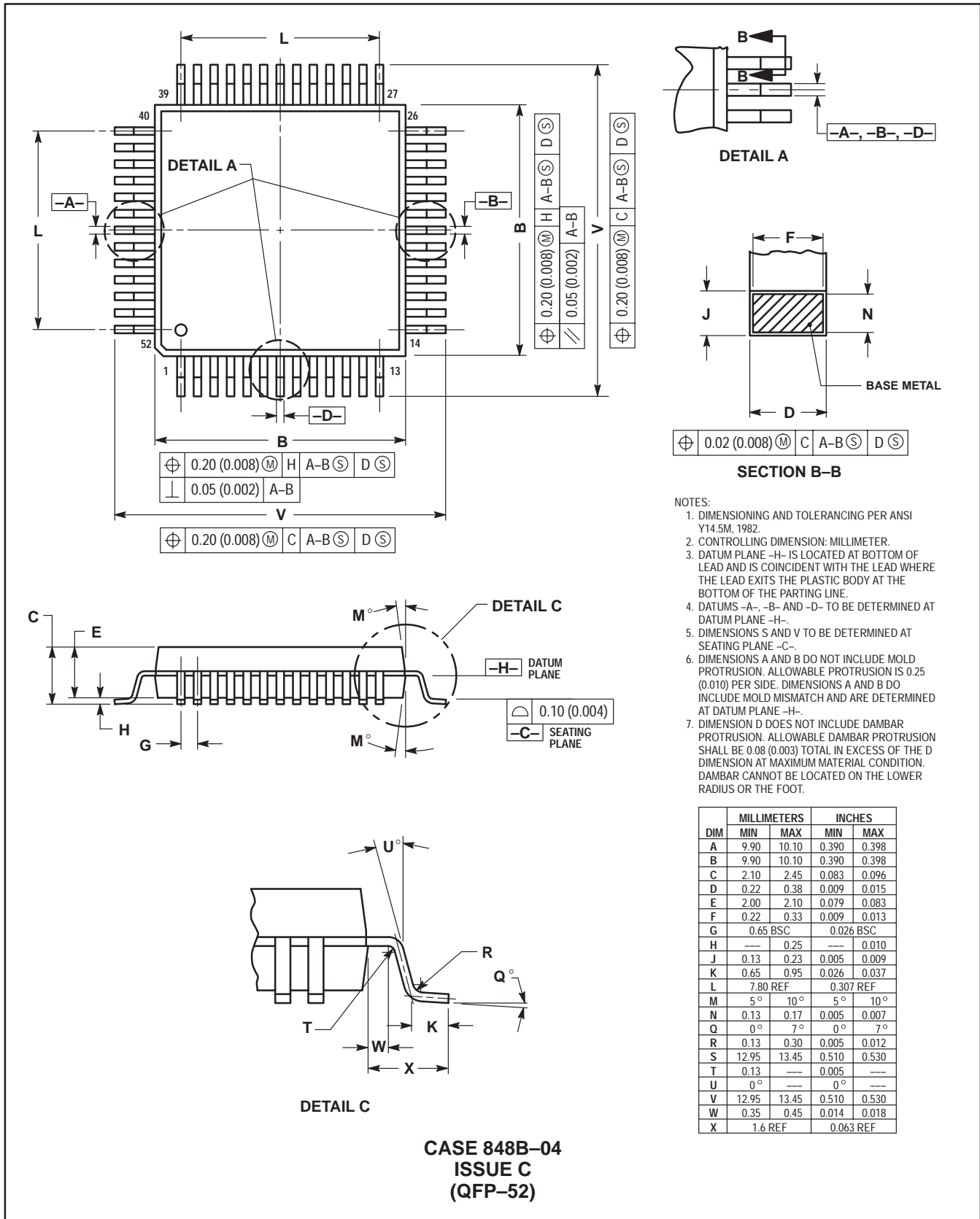
NOTES:

1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: MILLIMETER.
3. DIMENSION A DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.15 (0.006) PER SIDE.
4. DIMENSION B DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 (0.010) PER SIDE.

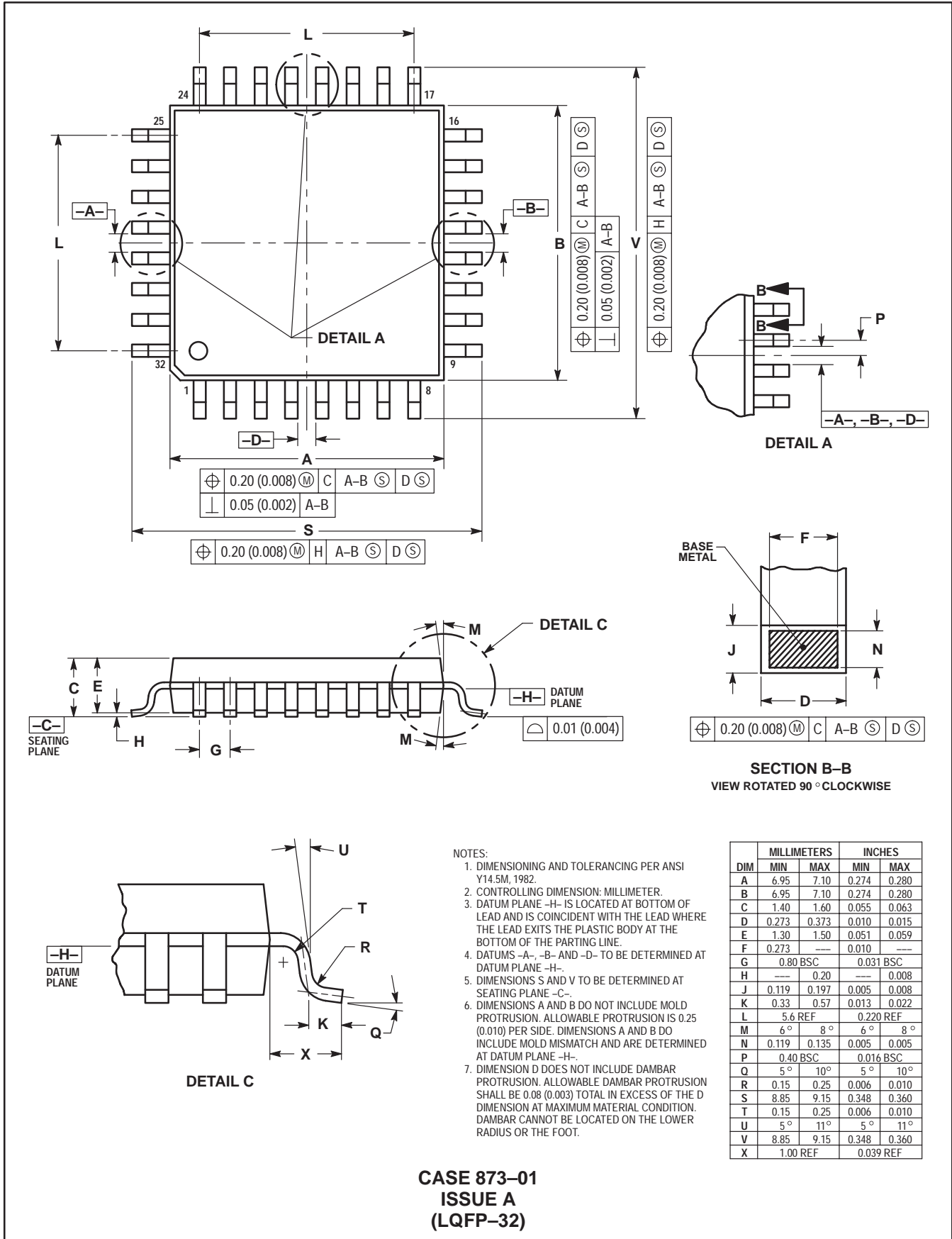
DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.90	3.10	0.114	0.122
B	2.90	3.10	0.114	0.122
C	---	1.10	---	0.043
D	0.25	0.40	0.010	0.016
G	0.65 BSC		0.026 BSC	
H	0.05	0.15	0.002	0.006
J	0.13	0.23	0.005	0.009
K	4.75	5.05	0.187	0.199
L	0.40	0.70	0.016	0.028

CASE 846A-02
ISSUE D
(Micro-8)

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

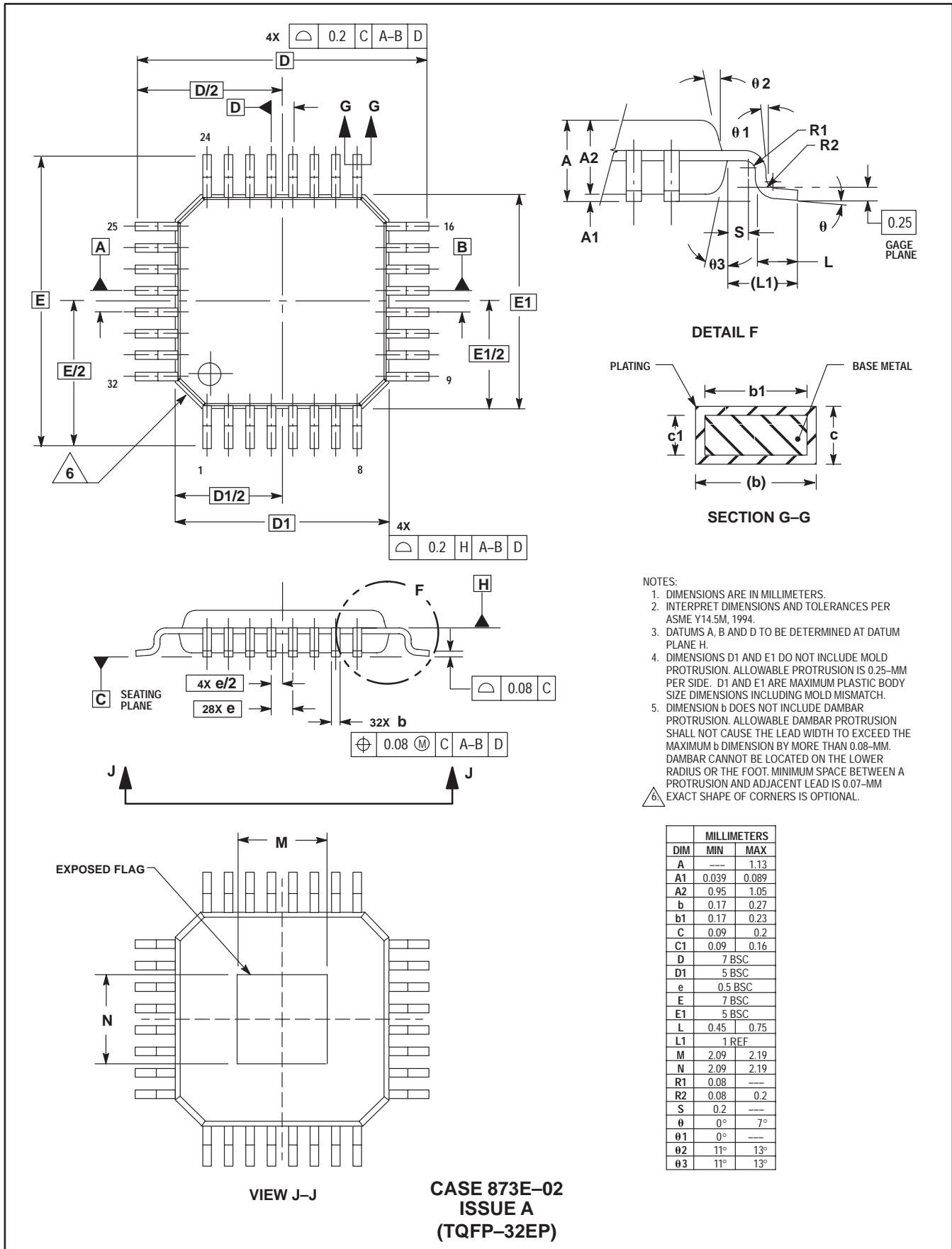


- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: MILLIMETER.
 3. DATUM PLANE -H- IS LOCATED AT BOTTOM OF LEAD AND IS COINCIDENT WITH THE LEAD WHERE THE LEAD EXITS THE PLASTIC BODY AT THE BOTTOM OF THE PARTING LINE.
 4. DATUMS -A-, -B- AND -D- TO BE DETERMINED AT DATUM PLANE -H-.
 5. DIMENSIONS S AND V TO BE DETERMINED AT SEATING PLANE -C-.
 6. DIMENSIONS A AND B DO NOT INCLUDE MOLD PROTRUSION. ALLOWABLE PROTRUSION IS 0.25 (0.010) PER SIDE. DIMENSIONS A AND B DO INCLUDE MOLD MISMATCH AND ARE DETERMINED AT DATUM PLANE -H-.
 7. DIMENSION D DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.08 (0.003) TOTAL IN EXCESS OF THE D DIMENSION AT MAXIMUM MATERIAL CONDITION. DAMBAR CANNOT BE LOCATED ON THE LOWER RADIUS OR THE FOOT.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	6.95	7.10	0.274	0.280
B	6.95	7.10	0.274	0.280
C	1.40	1.60	0.055	0.063
D	0.273	0.373	0.010	0.015
E	1.30	1.50	0.051	0.059
F	0.273	---	0.010	---
G	0.80	BSC	0.031	BSC
H	---	0.20	---	0.008
J	0.119	0.197	0.005	0.008
K	0.33	0.57	0.013	0.022
L	5.6	REF	0.220	REF
M	6°	8°	6°	8°
N	0.119	0.135	0.005	0.005
P	0.40	BSC	0.016	BSC
Q	5°	10°	5°	10°
R	0.15	0.25	0.006	0.010
S	8.85	9.15	0.348	0.360
T	0.15	0.25	0.006	0.010
U	5°	11°	5°	11°
V	8.85	9.15	0.348	0.360
X	1.00	REF	0.039	REF

CASE 873-01
ISSUE A
(LQFP-32)

CASE DIMENSIONS (continued)

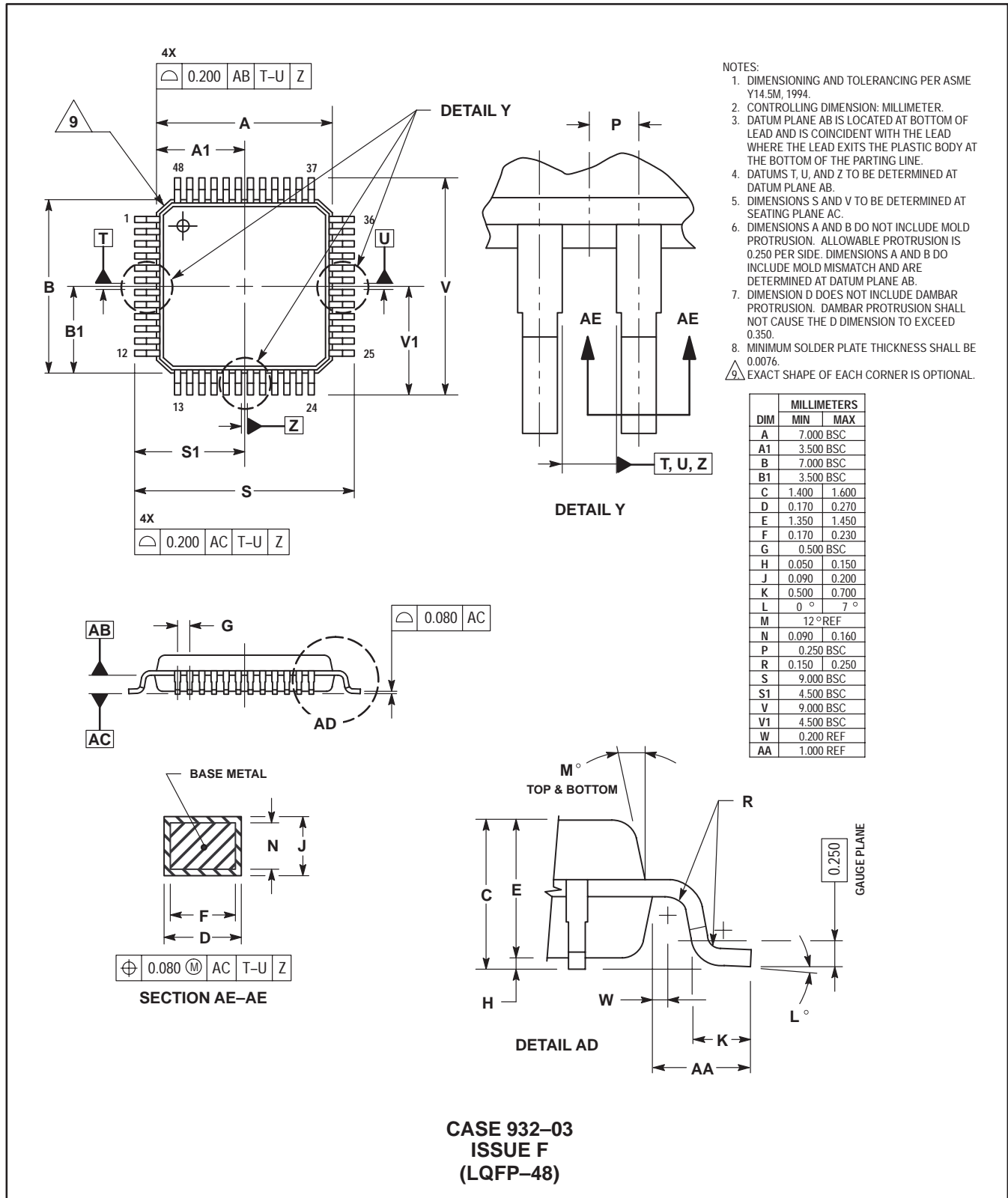


- NOTES:
1. DIMENSIONS ARE IN MILLIMETERS.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
 3. DATUMS A, B AND D TO BE DETERMINED AT DATUM PLANE H.
 4. DIMENSIONS D1 AND E1 DO NOT INCLUDE MOLD PROTRUSION. ALLOWABLE PROTRUSION IS 0.25-MM PER SIDE. D1 AND E1 ARE MAXIMUM PLASTIC BODY SIZE DIMENSIONS INCLUDING MOLD MISMATCH.
 5. DIMENSION b DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL NOT CAUSE THE LEAD WIDTH TO EXCEED THE MAXIMUM b DIMENSION BY MORE THAN 0.08-MM. DAMBAR CANNOT BE LOCATED ON THE LOWER RADIUS OR THE FOOT. MINIMUM SPACE BETWEEN A PROTRUSION AND ADJACENT LEAD IS 0.07-MM.
 6. EXACT SHAPE OF CORNERS IS OPTIONAL.

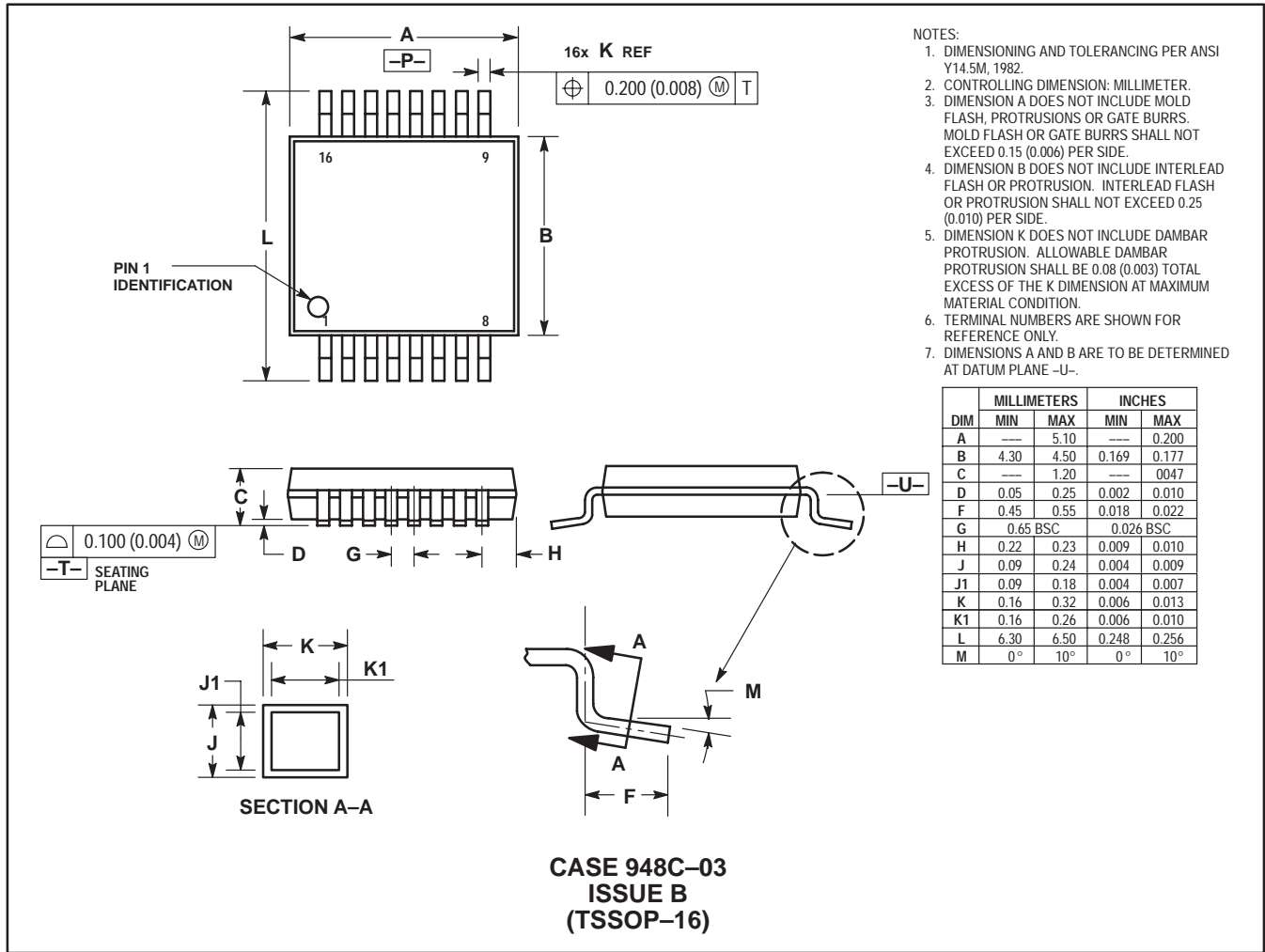
DIM	MILLIMETERS	
	MIN	MAX
A	---	1.13
A1	0.039	0.089
A2	0.95	1.05
b	0.17	0.27
b1	0.17	0.23
C	0.09	0.2
C1	0.09	0.16
D	7 BSC	
D1	5 BSC	
e	0.5 BSC	
E	7 BSC	
E1	5 BSC	
L	0.45	0.75
L1	1 REF	
M	2.09	2.19
N	2.09	2.19
R1	0.08	---
R2	0.08	0.2
S	0.2	---
θ	0°	7°
θ1	0°	---
θ2	11°	13°
θ3	11°	13°

CASE 873E-02
ISSUE A
(TQFP-32EP)

CASE DIMENSIONS (continued)



CASE DIMENSIONS (continued)

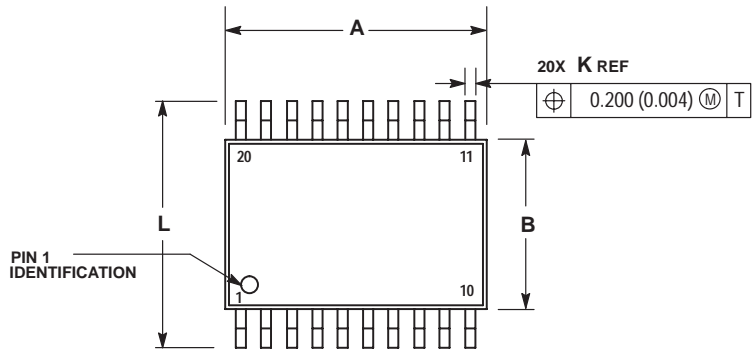


- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: MILLIMETER.
 3. DIMENSION A DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH OR GATE BURRS SHALL NOT EXCEED 0.15 (0.006) PER SIDE.
 4. DIMENSION B DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 (0.010) PER SIDE.
 5. DIMENSION K DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.08 (0.003) TOTAL EXCESS OF THE K DIMENSION AT MAXIMUM MATERIAL CONDITION.
 6. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.
 7. DIMENSIONS A AND B ARE TO BE DETERMINED AT DATUM PLANE -U-.

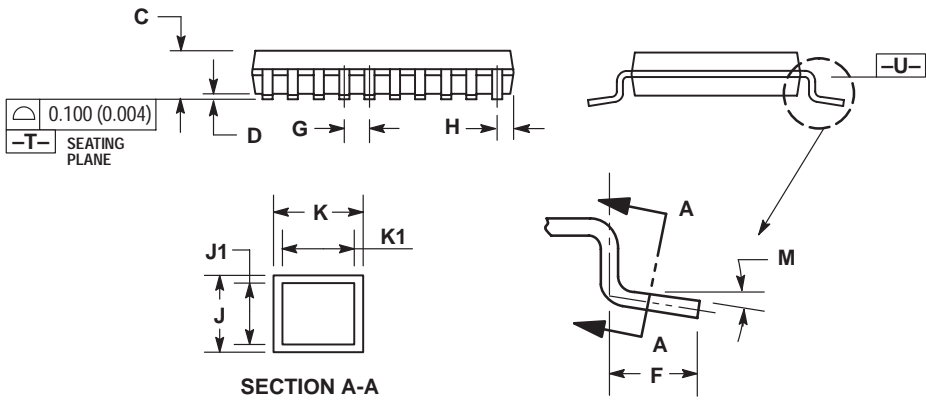
DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	---	5.10	---	0.200
B	4.30	4.50	0.169	0.177
C	---	1.20	---	0.047
D	0.05	0.25	0.002	0.010
F	0.45	0.55	0.018	0.022
G	0.65 BSC		0.026 BSC	
H	0.22	0.23	0.009	0.010
J	0.09	0.24	0.004	0.009
J1	0.09	0.18	0.004	0.007
K	0.16	0.32	0.006	0.013
K1	0.16	0.26	0.006	0.010
L	6.30	6.50	0.248	0.256
M	0°	10°	0°	10°

CASE 948C-03
ISSUE B
(TSSOP-16)

CASE DIMENSIONS (continued)



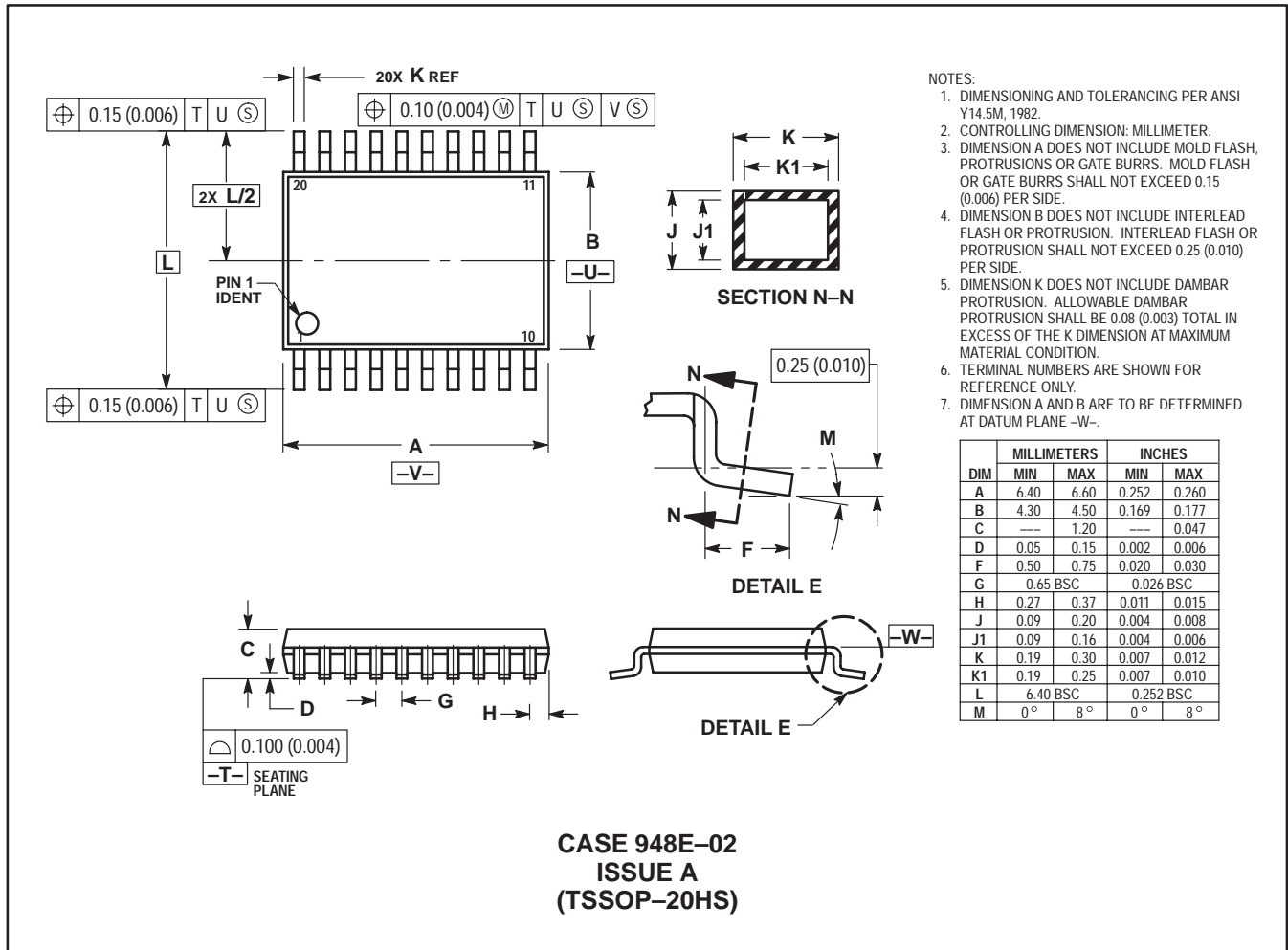
- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: MILLIMETER.
 3. DIMENSION A DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH OR GATE BURRS SHALL NOT EXCEED 0.15 (0.006) PER SIDE.
 4. DIMENSION B DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 (0.010) PER SIDE.
 5. DIMENSION K DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.08 (0.003) TOTAL IN EXCESS OF THE K DIMENSION AT MAXIMUM MATERIAL CONDITION.
 6. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.
 7. DIMENSIONS A AND B ARE TO BE DETERMINED AT DATUM PLANE -U-.



DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	---	6.60	---	0.260
B	4.30	4.50	0.169	0.177
C	---	1.20	---	0.047
D	0.05	0.25	0.002	0.010
F	0.45	0.55	0.018	0.022
G	0.65 BSC		0.026 BSC	
H	0.275	0.375	0.011	0.015
J	0.09	0.24	0.004	0.009
J1	0.09	0.18	0.004	0.007
K	0.16	0.32	0.006	0.013
K1	0.16	0.26	0.006	0.010
L	6.30	6.50	0.248	0.256
M	0°	10°	0°	10°

CASE 948D-03
ISSUE B
(TSSOP-20)

CASE DIMENSIONS (continued)

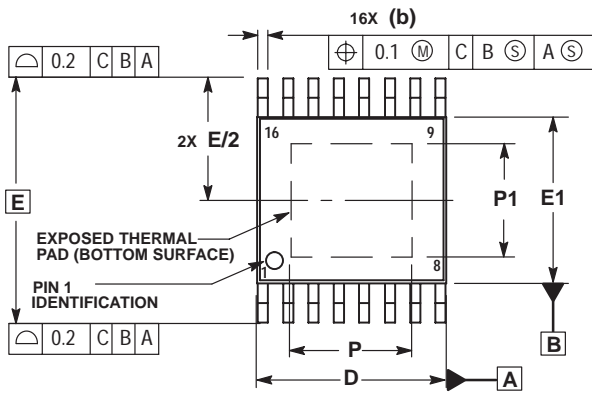


- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
 2. CONTROLLING DIMENSION: MILLIMETER.
 3. DIMENSION A DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH OR GATE BURRS SHALL NOT EXCEED 0.15 (0.006) PER SIDE.
 4. DIMENSION B DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 (0.010) PER SIDE.
 5. DIMENSION K DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.08 (0.003) TOTAL IN EXCESS OF THE K DIMENSION AT MAXIMUM MATERIAL CONDITION.
 6. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.
 7. DIMENSION A AND B ARE TO BE DETERMINED AT DATUM PLANE -W-.

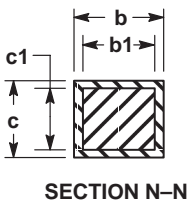
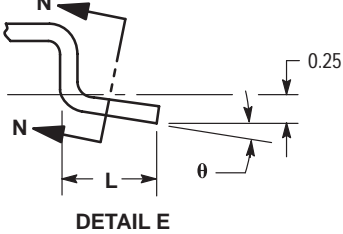
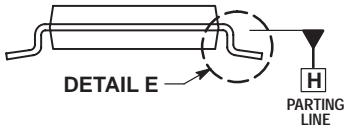
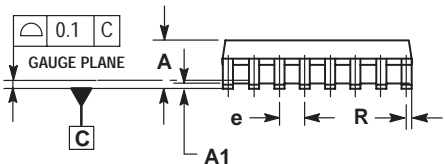
DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	6.40	6.60	0.252	0.260
B	4.30	4.50	0.169	0.177
C	---	1.20	---	0.047
D	0.05	0.15	0.002	0.006
F	0.50	0.75	0.020	0.030
G	0.65 BSC		0.026 BSC	
H	0.27	0.37	0.011	0.015
J	0.09	0.20	0.004	0.008
J1	0.09	0.16	0.004	0.006
K	0.19	0.30	0.007	0.012
K1	0.19	0.25	0.007	0.010
L	6.40 BSC		0.252 BSC	
M	0°	8°	0°	8°

**CASE 948E-02
ISSUE A
(TSSOP-20HS)**

CASE DIMENSIONS (continued)



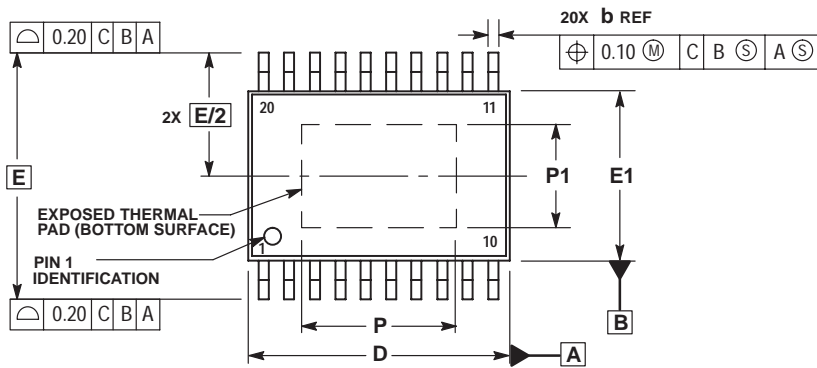
- NOTES:
1. DIMENSIONS ARE IN MILLIMETERS.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
 3. DIMENSION D DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH OR GATE BURRS SHALL NOT EXCEED 0.15 PER SIDE.
 4. DIMENSION E1 DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 PER SIDE.
 5. DIMENSION b DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.08 TOTAL IN EXCESS OF THE b DIMENSION AT MAXIMUM MATERIAL CONDITION.
 6. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.
 7. DIMENSIONS D AND E1 ARE TO BE DETERMINED AT DATUM PLANE H.



DIM	MILLIMETERS	
	MIN	MAX
A	---	1.2
A1	0	0.15
b	0.19	0.3
b1	0.19	0.25
c	0.09	0.2
c1	0.09	0.16
D	4.9	5.1
E	6.40 BSC	
E1	4.3	4.5
e	0.65 BSC	
L	0.5	0.75
P	---	3.9
P1	---	3
R	0.18	0.28
θ	0°	8°

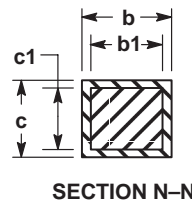
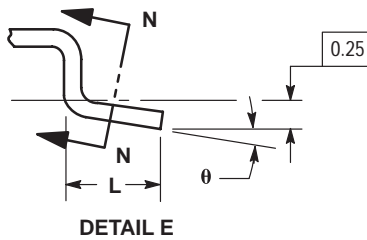
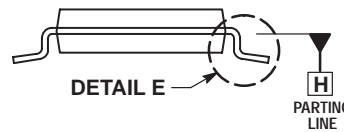
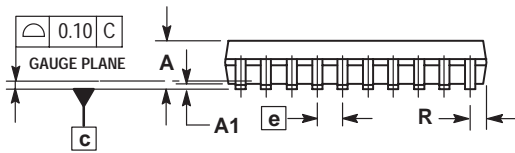
CASE 948L-01
ISSUE A
(TSSOP-16EP)

CASE DIMENSIONS (continued)



NOTES:

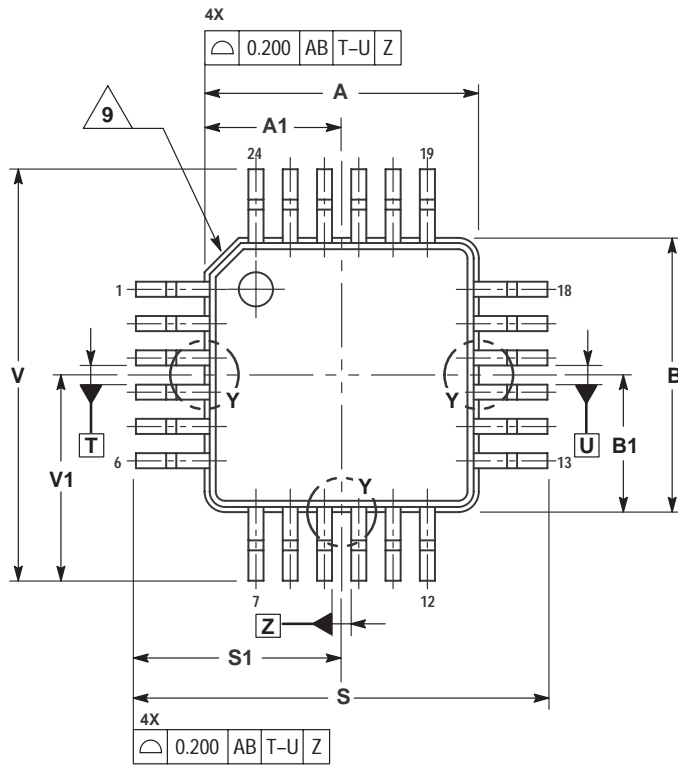
1. DIMENSIONS ARE IN MILLIMETERS.
2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
3. DIMENSION D DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH OR GATE BURRS SHALL NOT EXCEED 0.15 PER SIDE.
4. DIMENSION E1 DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 PER SIDE.
5. DIMENSION b DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.08 TOTAL IN EXCESS OF THE b DIMENSION AT MAXIMUM MATERIAL CONDITION.
6. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.
7. DIMENSIONS D AND E1 ARE TO BE DETERMINED AT DATUM PLANE H.



DIM	MILLIMETERS	
	MIN	MAX
A	---	1.20
A1	0.00	0.10
b	0.19	0.30
b1	0.19	0.25
c	0.09	0.20
c1	0.09	0.16
D	6.40	6.60
E	6.40 BSC	
E1	4.30	4.50
e	0.65 BSC	
L	0.50	0.75
P	---	4.80
P1	---	3.00
R	0.27	0.37
θ	0°	8°

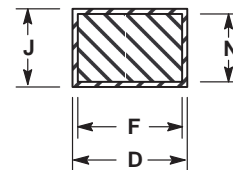
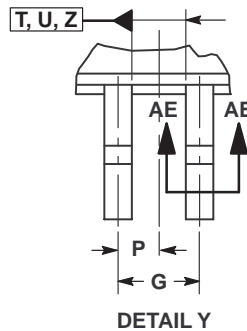
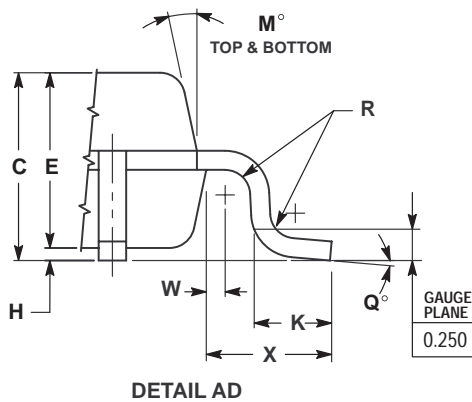
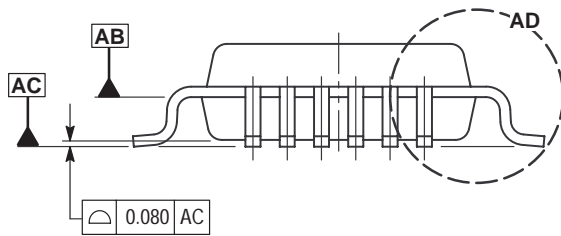
CASE 948M-01
ISSUE O
(TSSOP-20EP)

CASE DIMENSIONS (continued)



- NOTES:
1. CONTROLLING DIMENSION: MILLIMETER.
 2. DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
 3. DATUM PLANE AB IS LOCATED AT BOTTOM OF LEAD AND IS COINCIDENT WITH THE LEAD WHERE THE LEAD EXITS THE PLASTIC BODY AT THE BOTTOM OF THE PARTING LINE.
 4. DATUMS T, U, AND Z TO BE DETERMINED AT DATUM PLANE AB.
 5. DIMENSIONS S AND V TO BE DETERMINED AT DATUM PLANE AC.
 6. DIMENSIONS A AND B DO NOT INCLUDE MOLD PROTRUSION. ALLOWABLE PROTRUSION IS 0.250 PER SIDE. DIMENSIONS A AND B DO INCLUDE MOLD MISMATCH AND ARE DETERMINED AT DATUM PLANE AB.
 7. DIMENSION D DOES NOT INCLUDE DAMBAR PROTRUSION. DAMBAR PROTRUSION SHALL NOT CAUSE THE D DIMENSION TO EXCEED 0.350.
 8. MINIMUM SOLDER PLATE THICKNESS SHALL BE 0.0076.
9. EXACT SHAPE OF EACH CORNER IS OPTIONAL.

DIM	MILLIMETERS	
	MIN	MAX
A	4.000	BSC
A1	2.000	BSC
B	4.000	BSC
B1	2.000	BSC
C	1.400	1.600
D	0.170	0.270
E	1.350	1.450
F	0.170	0.230
G	0.500	BSC
H	0.050	0.150
J	0.090	0.200
K	0.500	0.700
M	12°	REF
N	0.090	0.160
P	0.250	BSC
Q	0°	7°
R	0.150	0.250
S	6.000	BSC
S1	3.000	BSC
V	6.000	BSC
V1	3.000	BSC
W	0.200	REF
X	1.000	REF

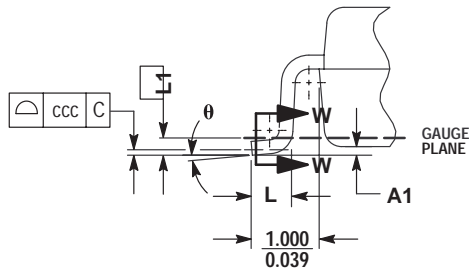
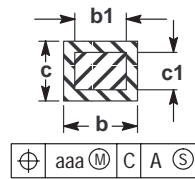
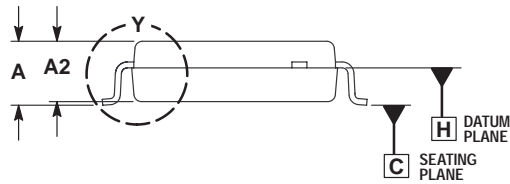
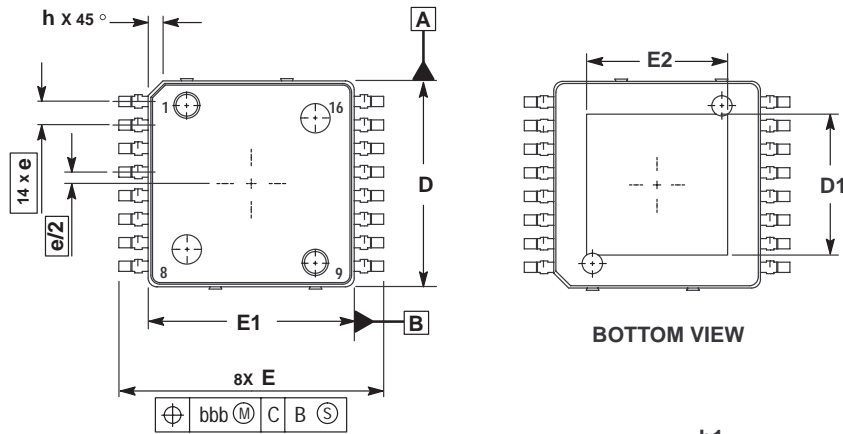


⊕ 0.080 AC T-U Z

SECTION AE-AE

CASE 977-02
ISSUE A
(LQFP-24)

CASE DIMENSIONS (continued)



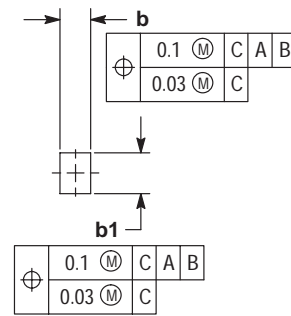
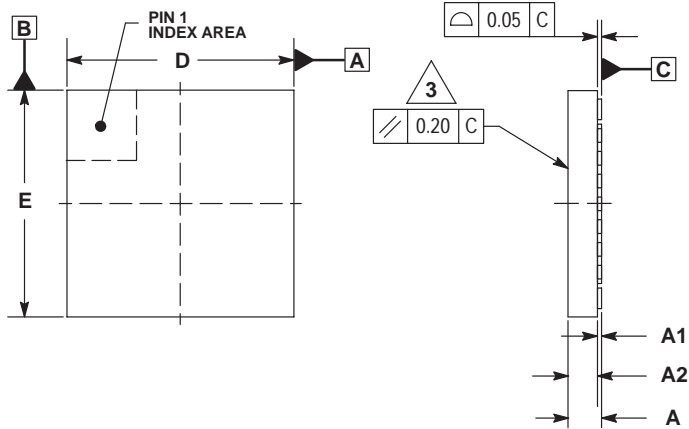
- NOTES:
1. CONTROLLING DIMENSION: MILLIMETER.
 2. DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
 3. DATUM PLANE -H- IS LOCATED AT BOTTOM OF LEAD AND IS COINCIDENT WITH THE LEAD WHERE THE LEAD EXITS THE PLASTIC BODY AT THE BOTTOM OF THE PARTING LINE.
 4. DIMENSIONS D AND E1 DO NOT INCLUDE MOLD PROTRUSION. ALLOWABLE PROTRUSION IS 0.250 PER SIDE. DIMENSIONS D AND E1 DO INCLUDE MOLD MISMATCH AND ARE DETERMINED AT DATUM PLANE -H-.
 5. DIMENSION b DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION IS 0.127 TOTAL IN EXCESS OF THE b DIMENSION AT MAXIMUM MATERIAL CONDITION.
 6. DATUMS -A- AND -B- TO BE DETERMINED AT DATUM PLANE -H-.

DIM	MILLIMETERS	
	MIN	MAX
A	2.000	2.300
A1	0.025	0.100
A2	1.950	2.100
D	6.950	7.100
D1	4.372	5.180
E	8.850	9.150
E1	6.950	7.100
E2	4.372	5.180
L	0.466	0.720
L1	0.250 BSC	
b	0.300	0.432
b1	0.300	0.375
c	0.180	0.279
c1	0.180	0.230
e	0.800 BSC	
h	---	0.600
θ	0°	7°
aaa	0.200	
bbb	0.200	
ccc	0.100	

DETAIL Y

CASE 978-03
ISSUE B
(PFP-16)

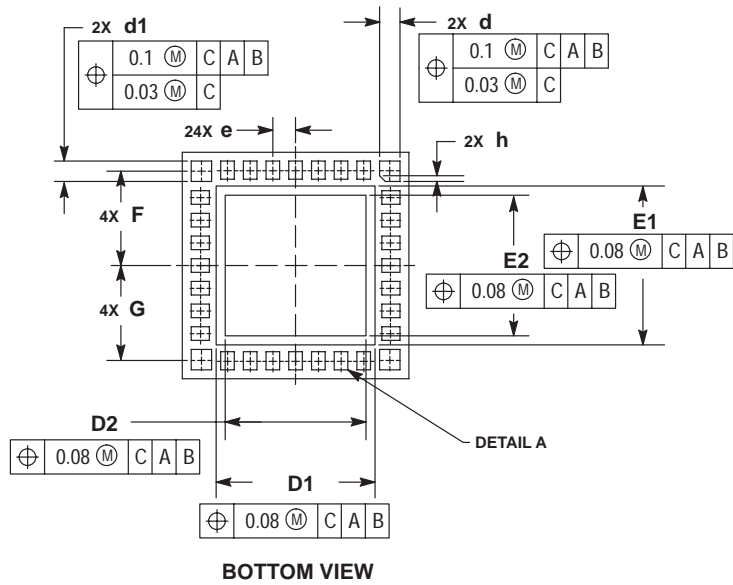
CASE DIMENSIONS (continued)



DETAIL A

NOTES:

1. DIMENSIONS ARE IN MILLIMETERS.
2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
3. PARALLELISM MEASUREMENT SHALL EXCLUDE ANY EFFECTS OF MARKING.
4. THERE IS TO BE MINIMUM SPACE BETWEEN ALL PADS OF 0.14 WHICH MUST BE FREE OF ALL PLATING BLEEDOUT.
5. THERE IS TO BE MINIMUM SPACE BETWEEN THE GROUND RING AND THE PERIPHERAL PADS OF 0.09 WHICH MUST BE FREE OF ALL PLATING BLEEDOUT.

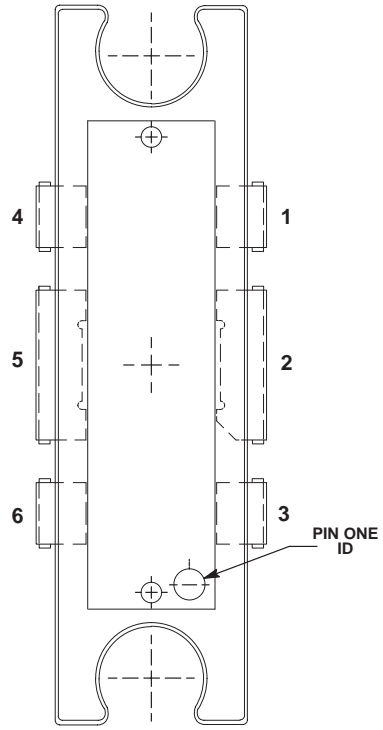
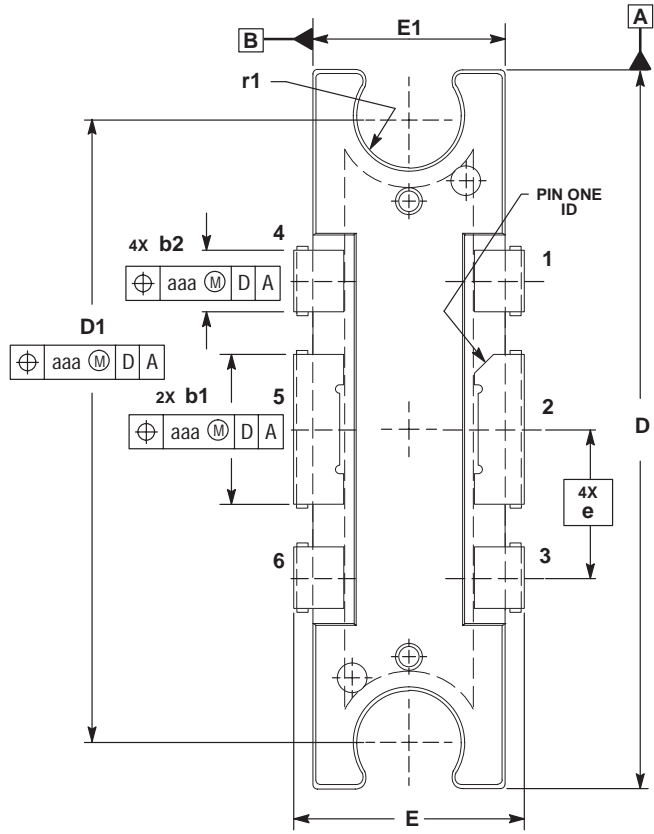


BOTTOM VIEW

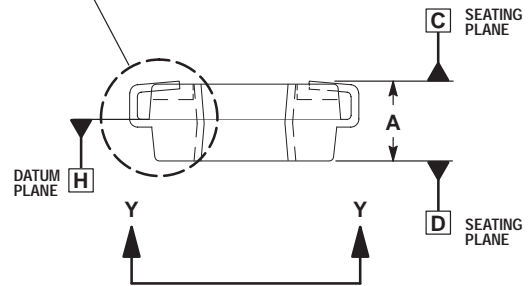
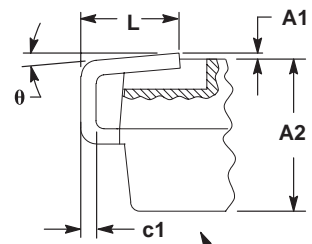
DIM	MILLIMETERS	
	MIN	MAX
A	---	0.80
A1	0.05	0.10
A2	0.60	0.70
b	0.24	0.36
b1	0.34	0.46
D	5.00 BSC	
D1	3.40	3.60
D2	3.00	3.20
d	0.39	0.51
d1	0.39	0.51
E	5.00 BSC	
E1	3.40	3.60
E2	3.00	3.20
e	0.50 BSC	
F	2.10 BSC	
G	2.075 BSC	
h	0.10	0.30

CASE 1261A-01
ISSUE C
(BCC32EP++)

CASE DIMENSIONS (continued)



VIEW Y-Y



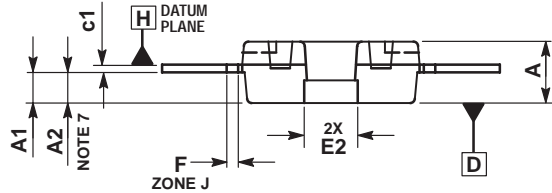
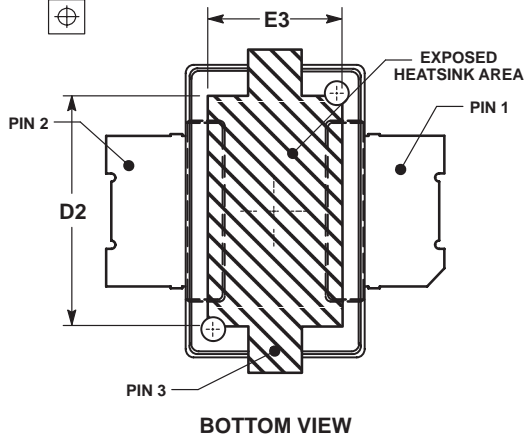
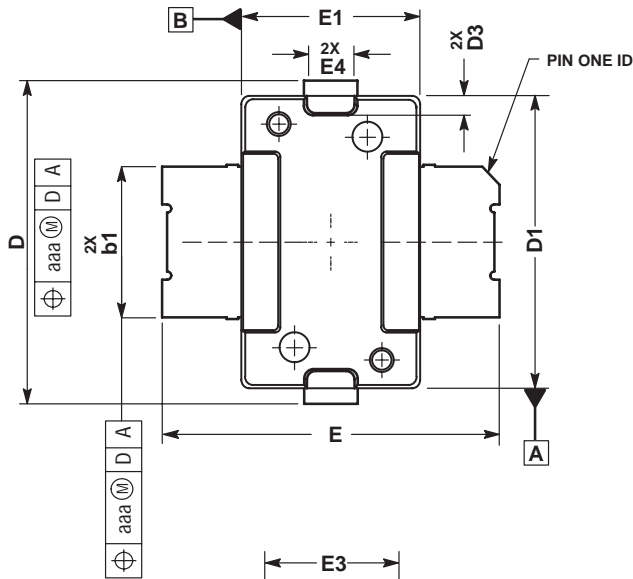
- NOTES:
1. CONTROLLING DIMENSION: INCH .
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.
 3. DATUM PLANE -H- IS LOCATED AT TOP OF LEAD AND IS COINCIDENT WITH THE LEAD WHERE THE LEAD EXITS THE PLASTIC BODY AT THE TOP OF THE PARTING LINE.
 4. DIMENSION D AND E1 DO NOT INCLUDE MOLD PROTRUSION. ALLOWABLE PROTRUSION IS 0.006 PER SIDE. DIMENSION D AND E1 DO INCLUDE MOLD MISMATCH AND ARE DETERMINED AT DATUM PLANE -H-.
 5. DIMENSIONS b1 AND b2 DO NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.005 TOTAL IN EXCESS OF THE b1 AND b2 DIMENSIONS AT MAXIMUM MATERIAL CONDITION.
 6. DATUMS -A- AND -B- TO BE DETERMINED AT DATUM PLANE -H-.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.098	0.110	2.489	2.794
A1	0.000	0.004	0.000	0.102
A2	0.098	0.106	2.489	2.692
D	0.926	0.934	23.520	23.724
D1	0.806	0.814	20.472	20.676
E	0.296	0.304	7.518	7.722
E1	0.246	0.254	6.248	6.452
L	0.060	0.070	1.524	1.778
b1	0.193	0.199	4.902	5.055
b2	0.078	0.084	1.981	2.134
c1	0.007	0.011	0.178	0.279
e	0.193 BSC		4.902 BSC	
r1	0.063	0.068	1.600	1.727
θ	0°	6°	0°	6°
aaa	0.004		0.102	

- STYLE 1:
- PIN 1. SOURCE (COMMON)
 - DRAIN
 - SOURCE (COMMON)
 - SOURCE (COMMON)
 - GATE
 - SOURCE (COMMON)

CASE 1264-06
ISSUE F
(TO-270)

CASE DIMENSIONS (continued)



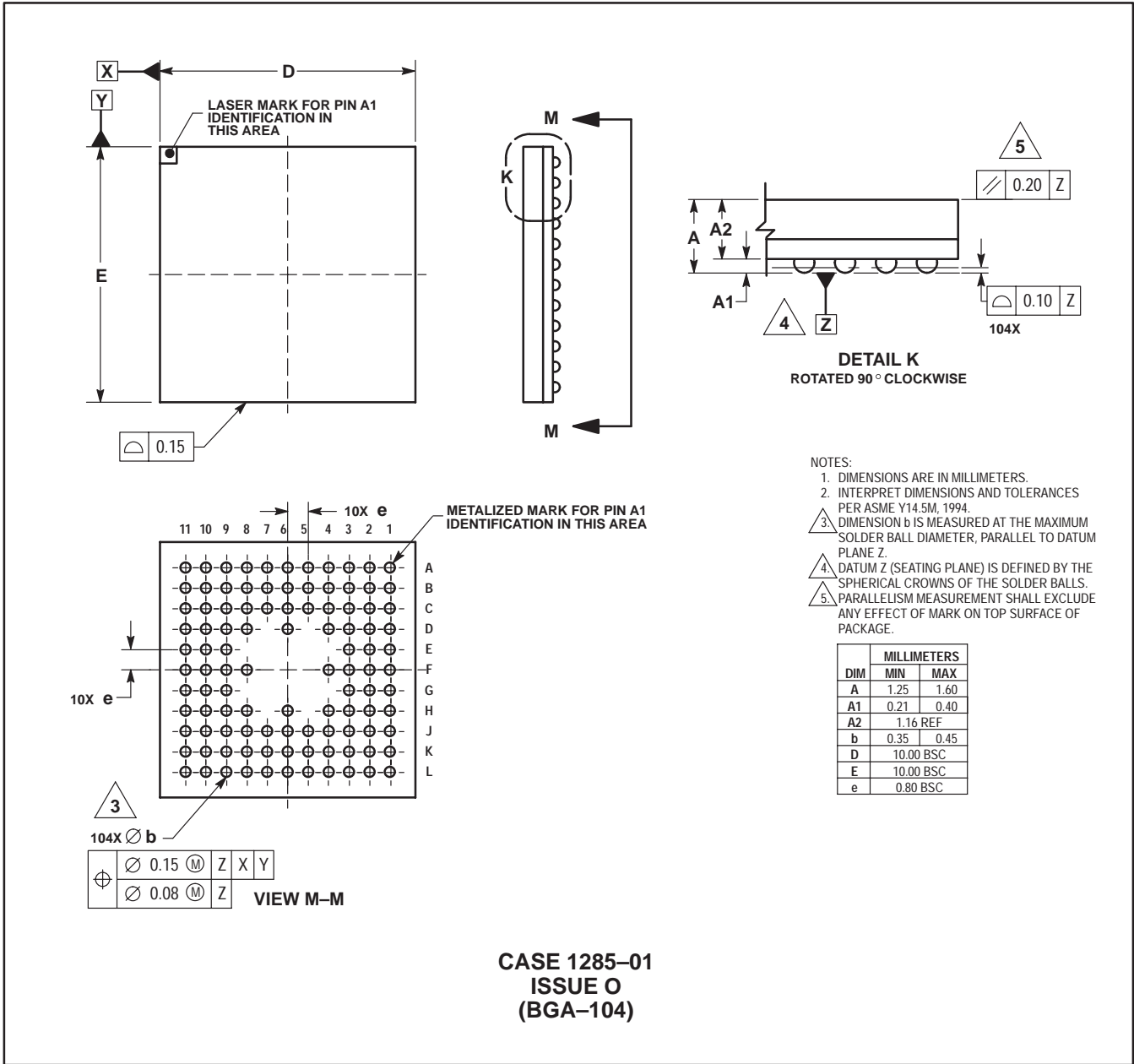
- NOTES:
1. CONTROLLING DIMENSION: INCH.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M-1994.
 3. DATUM PLANE -H- IS LOCATED AT TOP OF LEAD AND IS COINCIDENT WITH THE LEAD WHERE THE LEAD EXITS THE PLASTIC BODY AT THE TOP OF THE PARTING LINE.
 4. DIMENSIONS "D1" AND "E1" DO NOT INCLUDE MOLD PROTRUSION. ALLOWABLE PROTRUSION IS .006 PER SIDE. DIMENSIONS "D1" AND "E1" DO INCLUDE MOLD MISMATCH AND ARE DETERMINED AT DATUM PLANE -H-.
 5. DIMENSION b1 DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE .005 TOTAL IN EXCESS OF THE b1 DIMENSION AT MAXIMUM MATERIAL CONDITION.
 6. DATUMS -A- AND -B- TO BE DETERMINED AT DATUM PLANE -H-.
 7. DIMENSION A2 APPLIES WITHIN ZONE "J" ONLY.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	.076	.084	1.93	2.13
A1	.038	.044	0.96	1.12
A2	.040	.042	1.02	1.07
D	.416	.424	10.57	10.77
D1	.376	.384	9.55	9.75
D2	.290	.320	7.37	8.13
D3	.016	.024	0.41	0.61
E	.436	.444	11.07	11.28
E1	.236	.244	5.99	6.20
E2	.066	.074	1.68	1.88
E3	.150	.180	3.81	4.57
E4	.058	.066	1.47	1.68
F	.025 BSC		0.64 BSC	
b1	.193	.199	4.90	5.06
c1	.007	.011	0.18	0.28
aaa	.004		0.10	

STYLE 1:
 PIN 1. DRAIN
 2. GATE
 3. SOURCE

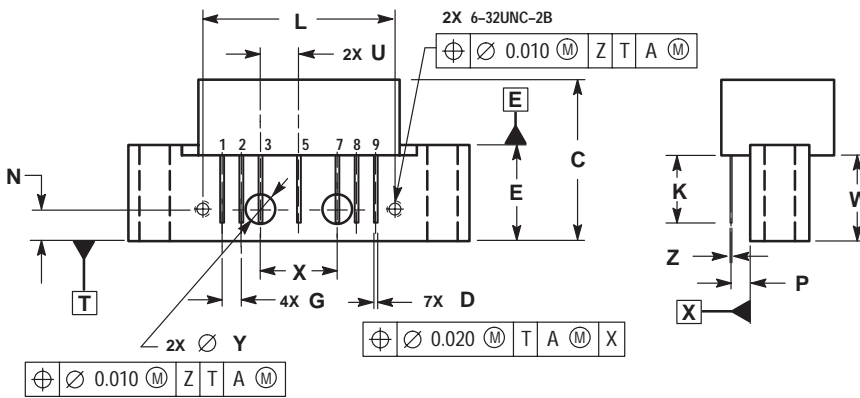
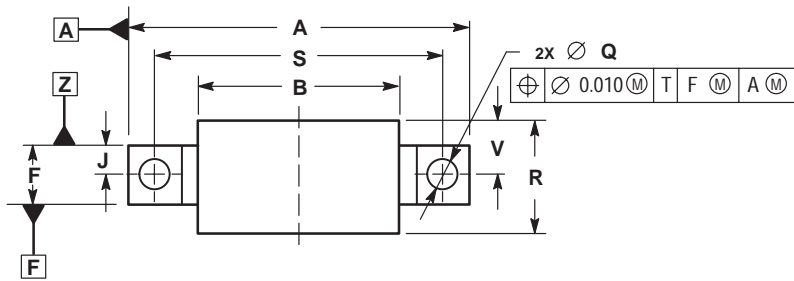
CASE 1265-06
 ISSUE E
 (TO-272)

CASE DIMENSIONS (continued)



CASE 1285-01
ISSUE O
(BGA-104)

CASE DIMENSIONS (continued)



- NOTES:
 1. DIMENSIONS ARE IN INCHES.
 2. INTERPRET DIMENSIONS AND TOLERANCES PER ASME Y14.5M, 1994.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	---	1.775	---	45.085
B	---	1.085	---	27.559
C	---	0.840	---	21.336
D	0.015	0.021	0.381	0.533
E	0.465	0.510	11.811	12.954
F	0.300	0.325	7.62	8.255
G	0.100 BSC		2.540 BSC	
J	0.156 BSC		3.962 BSC	
K	0.315	0.355	8.001	9.017
L	1.000 BSC		25.400 BSC	
N	0.165 BSC		4.191 BSC	
P	0.100 BSC		2.540 BSC	
Q	0.148	0.168	3.759	4.267
R	---	0.600	---	15.24
S	1.500 BSC		38.100 BSC	
U	0.200 BSC		5.080 BSC	
V	---	0.250	---	6.350
W	0.435	---	11.049	---
X	0.400 BSC		10.160 BSC	
Y	0.152	0.163	3.861	4.140
Z	0.009	0.011	0.229	0.279

- STYLE 1:
 PIN 1. RF INPUT
 2. GROUND
 3. GROUND
 4. DELETED
 5. VDC
 6. DELETED
 7. GROUND
 8. GROUND
 9. RF OUTPUT

CASE 1302-01
 ISSUE B

Chapter Ten

Applications and Product Literature

Motorola's Applications Literature provides guidance to the effective use of its semiconductor families across a broad range of practical applications. Many different topics are discussed in a way that is not possible in a device data sheet, from detailed circuit designs complete with PCB layouts, through matters to consider when embarking on a design, to complete overviews of product families and their design philosophies.

Information is presented in the form of Application Notes, Article Reprints and detailed Engineering Bulletins.

Table of Contents

	Page
Applications Literature	10.1-2
Product Literature	10.1-3

Literature

Application Notes, Engineering Bulletins and Article Reprints of special interest to designers of RF and RF/IF equipment are listed below. This technical documentation is available on the Motorola Semiconductor Product Sector Web site or is available through the Motorola Literature Distribution Center. Phone and fax numbers for ordering literature are listed on the back cover of this book and in our Accessing Data On-line section.

Application Notes

- | | | | |
|--------|---|--------|--|
| AN139A | Understanding Transistor Response Parameters | AN1029 | TV Transposers Band IV and
VP _O = 0.5 W/1.0 W |
| AN211A | Field Effect Transistors in Theory and Practice | AN1030 | 1 W/2 W Broadband TV Amplifier Band IV and V |
| AN215A | RF Small-Signal Design Using Two-Port
Parameters | AN1032 | How Load VSWR Affects Non-Linear Circuits |
| AN238 | Transistor Mixer Design Using 2-Port
Parameters | AN1033 | Match Impedances in Microwave Amplifiers |
| AN267 | Matching Network Designs with Computer
Solutions | AN1034 | Three Balun Designs for Push-Pull Amplifiers |
| AN282A | Systemizing RF Power Amplifier Design | AN1037 | Solid-State Power Amplifier — 300 Watt FM,
88–108 MHz |
| AN419 | UHF Amplifier Design Using Data Sheet
Design Curves | AN1038 | 1.2 V, 40 – 900 MHz Broadband Amplifier
with the TP3400 Transistor |
| AN423 | Field Effect Transistor RF Amplifier Design
Techniques | AN1039 | 470 – 860 MHz — Broadband Amplifier – 5 W |
| AN535 | Phase-Locked-Loop Design Fundamentals | AN1040 | Mounting Considerations for Power
Semiconductors |
| AN548A | Microstrip Design Techniques for UHF Amplifiers | AN1041 | Mounting Procedures for Very High Power
RF Transistors |
| AN555 | Mounting Stripline-Opposed-Emitter (SOE)
Transistors | AN1107 | Understanding RF Data Sheet Parameters |
| AN593 | Broadband Linear Power Amplifiers Using
Push-Pull Transistors | AN1207 | The MC145170 in Basic HF and VHF Oscillators |
| AN721 | Impedance Matching Networks Applied to
RF Power Transistors | AN1253 | An Improved PLL Design Method Without
ω_n and ζ |
| AN749 | Broadband Transformers and Power Combining
Techniques for RF | AN1277 | Offset Reference PLLs for Fine Resolution or
Fast Hopping |
| AN758 | A Two-Stage 1 kW Solid-State Linear Amplifier | AN1526 | RF Power Device Impedances: Practical
Considerations |
| AN762 | Linear Amplifiers for Mobile Operation | AN1528 | Packaging Considerations for RF Transistors |
| AN779 | Low-Distortion 1.6 to 30 MHz SSB Driver
Designs | AN1529 | RF Power Circuit Concepts Using FETs and BJTs |
| AN790 | Thermal Rating of RF Power Transistors | AN1530 | Motorola Advanced Amplifier Concept Package |
| AN791 | A Simplified Approach to VHF Power
Amplifier Design | AN1531 | Parameter Extraction Techniques for RF Power
Transistors Models |
| AN827 | The Technique of Direct Programming by Using a
Two-Modulus Prescaler | AN1539 | An IF Communication Circuit Tutorial |
| AN860 | Power MOSFETs versus Bipolar Transistors | AN1575 | Worldwide Cordless Telephone Frequencies |
| AN878 | VHF MOS Power Applications | AN1580 | Mounting and Soldering Recommendations for
the Motorola Power Flat Pack Package |
| AN923 | 800 MHz Test Fixture Design | AN1599 | Power Control with the MRFIC0913 GaAs
Integrated Power Amplifier and MC33169
Support IC |
| AN955 | A Cost Effective VHF Amplifier for Land
Mobile Radios | AN1602 | 3.6 V and 4.8 V GSM/DCS1800 Dual Band PA
Application with DECT Capability Using
Standard Motorola RFIC's |
| AN1022 | Mechanical and Thermal Considerations in Using
RF Linear Hybrid Amplifiers | AN1617 | Mounting Recommendations for Copper
Tungsten Flanged Transistors |
| AN1024 | RF Linear Hybrid Amplifiers | AN1639 | Phase Noise Measurement Using the Phase
Lock Technique |
| AN1025 | Reliability Considerations in Design and Use of
RF Integrated Circuits | AN1643 | RF LDMOS Power Modules for GSM Base
Station Application: Optimum Biasing Circuit |
| AN1026 | Extending the Range of an Intermodulation
Distortion Test | AN1658 | Converting MC13110/13111 Based Designs to
the MC13110A,B/13111A,B |
| AN1027 | Reliability/Performance Aspects of CATV
Amplifier Design | AN1670 | 60 Watts, GSM 900 MHz, LDMOS Two-Stage
Amplifier |
| AN1028 | 35/50 Watt Broadband (160 – 240 MHz)
Push-Pull TV Amplifier Band III | AN1671 | MC145170 PSpice Modeling Kit |

Literature (continued)

- AN1673 Solder Reflow Mounting Method for the MRF286 and Similar Packages
- AN1674 Mounting Method with Mechanical Fasteners for the MRF286 and Similar Packages
- AN1687 A Full-Featured Wireless Interface for RS-232 Communications
- AN1691 Practical Solutions for Medium Data Rate Wireless Communications
- AN1696 Broadband Intermodulation Performance Development Using the Rohde & Schwarz Vector Network Analyzer ZVR
- AN1697 GSM900/DCS/1800 Dual-Band 3.6 V Power Amplifier Solution with Open Loop Control Scheme
- AN1900 CDMA Upmixer Design Considerations Using the MRFIC1854
- AN4005 Thermal Management and Mounting Method for the PLD 1.5 RF Power Surface Mount Package

Article Reprints

- AR141 Applying Power MOSFETs in Class D/E RF Power Amplifier Design
- AR164 Good RF Construction Practices and Techniques
- AR165S RF Power MOSFETs
- AR176 New MOSFETs Simplify High Power RF Amplifier Design
- AR254 Phase-Locked Loop Design Articles
- AR305 Building Push-Pull, Multioctave, VHF Power Amplifiers
- AR313 Wideband RF Power Amplifier
- AR346 RF Power FETs – Their Characteristics and Applications, Parts 1 & 2
- AR347 A Compact 1-kW 2–50 MHz Solid State Linear Amplifier
- AR510 VSWR Protection of Solid State RF Power Amplifiers
- AR511 Biasing Solid State Amplifiers to Linear Operation
- AR571 Silicon MOSFET Technology for Wireless Communications
- AR573 Modeling a New Generation for RF Devices: MOSFETs of L-Band Applications
- AR579 CAD of a Broadband, Class-C 65 Watt UHF Power Amplifier
- AR580 MOSFET RF Power: An Update — Parts 1 and 2
- AR581 Procedure Performs Thermal Measurements on Pulsed Devices
- AR582 MIMP Analyzes Impedance Matching Networks
- AR583 Power MOSFETs Handle Bipolar Amp Applications
- AR586 Power MOSFETs versus Bipolar Transistors
- AR589 QSPLIT Utility Displays S-Parameter Data
- AR594 GaAs RF ICs Target 2.4-GHz Frequency Band
- AR596 Design and Performance of a Low Voltage, Low Noise 900 MHz Amplifier
- AR606 PCS and RF Components
- AR612 Plastic Packages Hold Power RF MOSFETs
- AR614 Advantages of LDMOS in High Power Linear Amplification
- AR624 Aluminum-Based Metallization Enhances Device Reliability
- AR628 Impedance Measurements for High Power RF Transistors Using the TRL Method
- AR629 Digital Predistortion Techniques for RF Power Amplifiers with CDMA Applications

Engineering Bulletins

- EB19 Controlled – Q RF Technology — What It Means, How It's Done
- EB27A Get 300 Watts PEP Linear Across 2 to 30 MHz from This Push-Pull Amplifier
- EB38 Measuring the Intermodulation Distortion of Linear Amplifiers
- EB63 140 W (PEP) Amateur Radio Linear Amplifier 2 – 30 MHz
- EB74 A 10 Watt, 225 – 400 MHz Amplifier — MRF331
- EB77 A 60-Watt, 225 – 400 MHz Amplifier — 2N6439
- EB89 A 1-Watt, 2.3 GHz Amplifier
- EB104 Get 600 Watts RF from Four Power FETs
- EB105 A 30 Watt, 800 MHz Amplifier Design
- EB107 Mounting Considerations for Motorola RF Power Modules
- EB202 RF Transistor Design
- EB209 Mounting Method for RF Power Leadless Surface Mount Transistors
- EB211 Thermal Management and Solder Mounting Method for the MRF286, 60 Watt Power Device in a CuW (Copper Tungsten) Base Package

Product Literature

- DL110/D Wireless RF, IF and Transmitter Device Data Book
- SG46/D Wireless RF, IF and Transmitter Selector Guide
- CD301/D Wireless RF, IF and Transmitter Data Library CD-ROM
- BR1502/D Wireless Infrastructure Solutions
- BR1504/D RF Power Solutions
- BR3031/D Wireless Infrastructure DSP Solutions
- SG384/D RF LDMOS Infrastructure Technology Selector Guide

Chapter Eleven

Motorola Distributor & Worldwide Sales Offices

MOTOROLA AUTHORIZED DISTRIBUTOR AND WORLDWIDE SALES OFFICES

NORTH AMERICAN DISTRIBUTORS

UNITED STATES

ALABAMA

Huntsville

Allied Electronics, Inc. (256) 721-3500
 Arrow Electronics (256) 864-3300
 FAI (256) 837-9209
 Future Electronic (256) 971-2010
 Avnet Electronics (256) 837-8700
 Newark (256) 837-9091
 Arrow (formerly Wyle) (256) 830-1119

Mobile

Allied Electronics, Inc. (334) 476-1875

ARIZONA

Phoenix

Allied Electronics, Inc. (602) 831-2002
 FAI (602) 731-4661
 Future Electronics (602) 968-7140
 Avnet Electronics (602) 736-7000
 Arrow (formerly Wyle) (602) 804-7000

Tempe

Arrow Electronics (602) 966-6600
 Newark (602) 966-6340
 Penstock (602) 967-1620

KANSAS

Little Rock

Newark (501) 225-8130

CALIFORNIA

Agoura Hills

Future Electronics (818) 871-1740

Calabassas

Arrow Electronics (818) 880-9686
 Arrow (formerly Wyle) (818) 880-9000

Culver City

Avnet Electronics (310) 558-2000

Irvine

Arrow Electronics (949) 587-0404
 Arrow Zeus (949) 581-4662
 FAI (949) 753-4778
 Future Electronics (949) 453-1515
 Avnet Electronics (949) 789-4100
 Arrow (formerly Wyle) (949) 753-9953
 Arrow (formerly Wyle) (949) 789-9953

Los Angeles

FAI (818) 879-1234
 Arrow (formerly Wyle) (818) 880-9000

Manhattan Beach

Penstock (310) 546-8953

Orange County

Allied Electronics, Inc. (949) 727-3010

Palo Alto

Newark (650) 812-6300

Riverside

Allied Electronics, Inc. (909) 980-6522
 Newark (909) 980-2105

Rocklin

Avnet Electronics (916) 632-4500

Roseville

Arrow (formerly Wyle) (916) 783-9953

Sacramento

Allied Electronics, Inc. (916) 632-3104
 FAI (916) 782-7882
 Newark (916) 565-1760
 Arrow (formerly Wyle) (916) 638-5282

San Diego

Allied Electronics, Inc. (619) 279-2550
 Arrow Electronics (619) 565-4800
 Arrow Zeus (619) 565-4800
 FAI (619) 623-2888
 Future Electronics (619) 625-2800

San Diego – Continued

Avnet Electronics (619) 571-7540
 Penstock (619) 623-9100
 Newark (619) 453-8211
 Arrow (formerly Wyle) (619) 558-6600

San Fernando Valley

Allied Electronics, Inc. (818) 598-0130

San Jose

Allied Electronics, Inc. (408) 383-0366
 Arrow Electronics (408) 441-9700
 Arrow Zeus (408) 629-4789
 Arrow Electronics (408) 428-6400
 FAI (408) 434-0369
 Future Electronics (408) 434-1122
 Richardson Electronics (800) 737-6937

Santa Clara

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